

4th PBC Tech Workshop: Cryogenics

28th Sep 2022

<https://indico.cern.ch/event/1180067/>



Ultralight Cryogenic Structures for HEP experiments

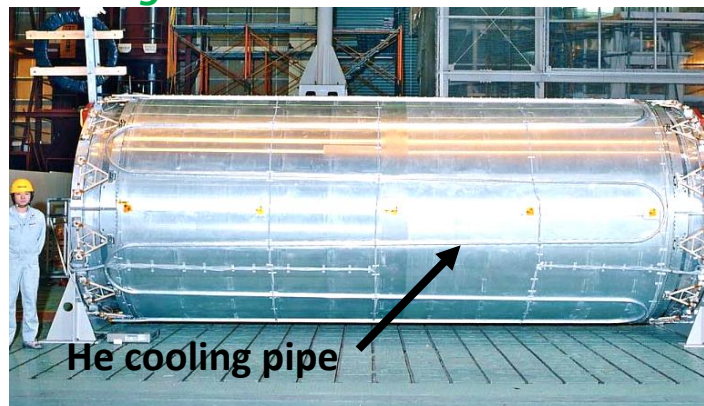


EP R&D WP4:

Low Mass Cryostats for future Magnets & Calorimeter

Maria Soledad Molina Gonzalez

SC Magnet

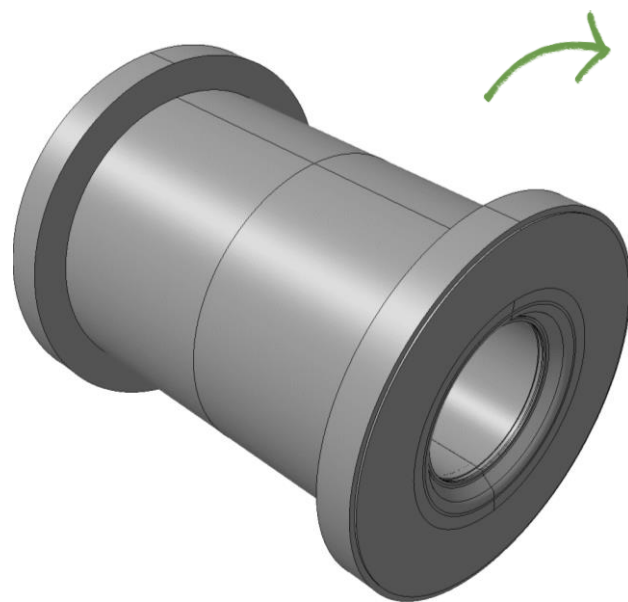


LAr ECAL calorimeter



Cryostat for SC Magnet:

-Thermal insulation (10e-5 mbar , 293K)



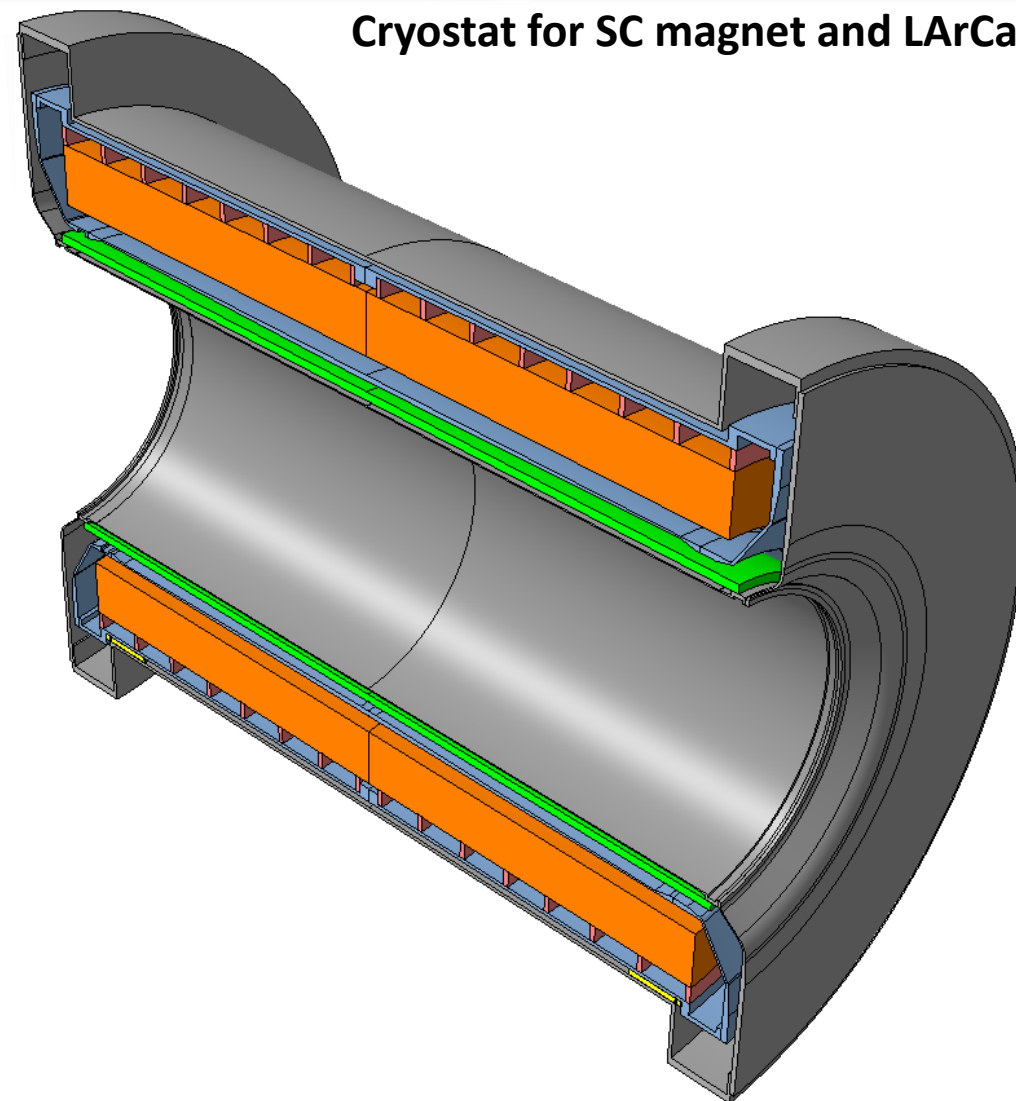
Cryostat for LArCal:

-LAr tightness (3 bars, 87K)

-Thermal insulation (10e-5 mbar, 293K)

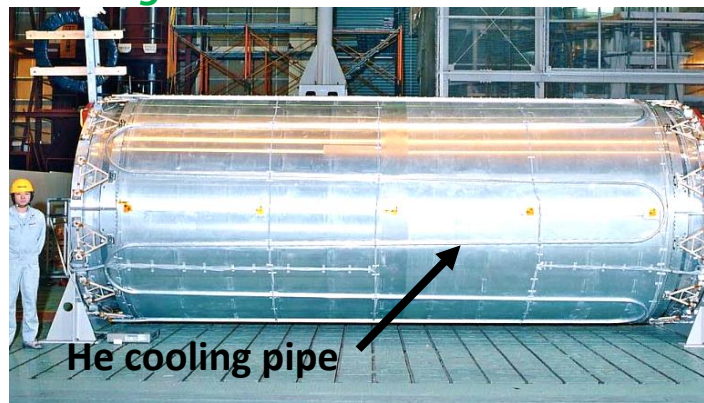


Cryostat for SC magnet and LArCal:



→ Design a cryostat to support LAr Calorimeters (ECAL) and SC magnets in future larger experiments (FCCee-hh)

SC Magnet



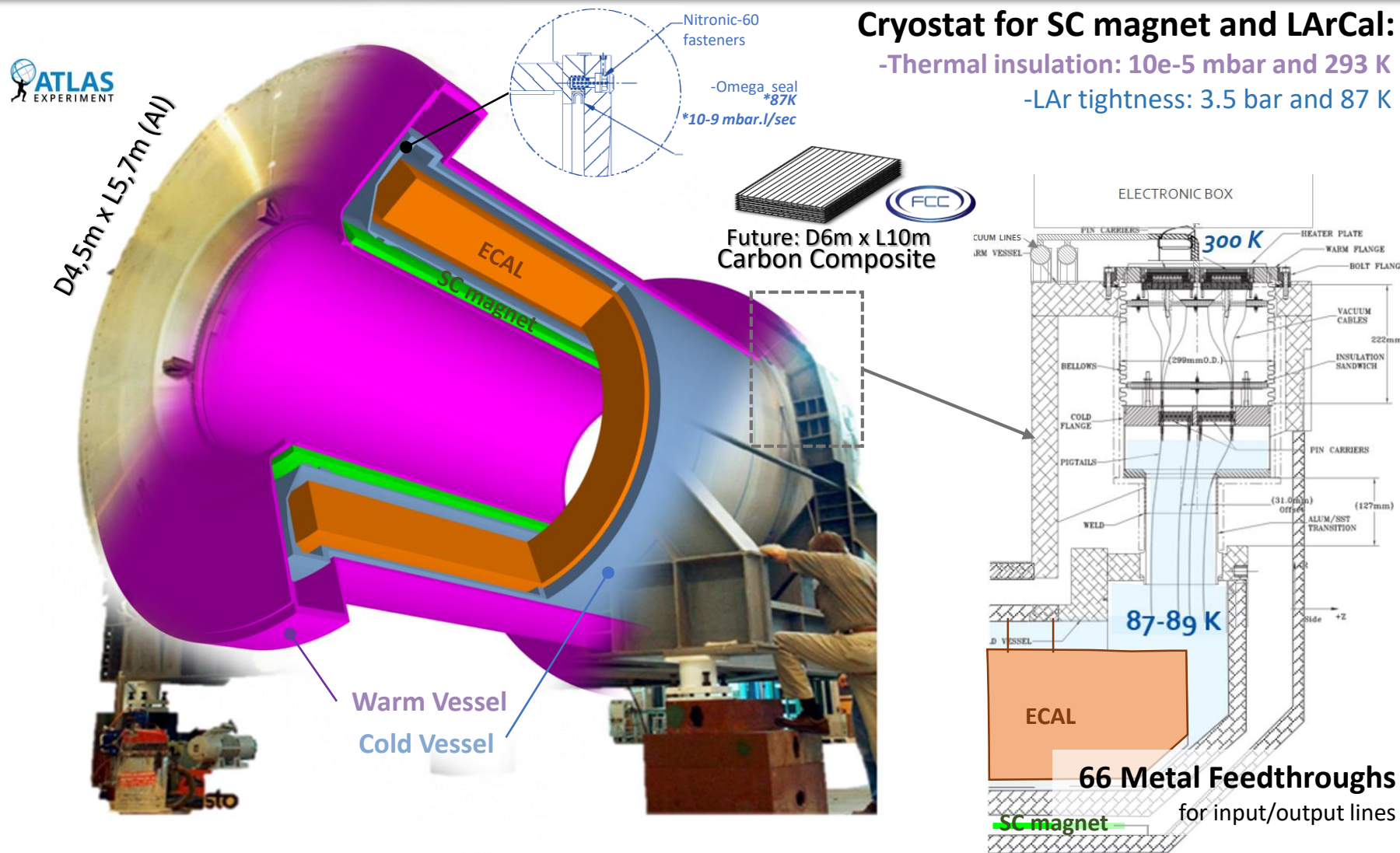
He cooling pipe

Ultra-thin cryostat for compact assembly of experiments

LAr ECAL calorimeter



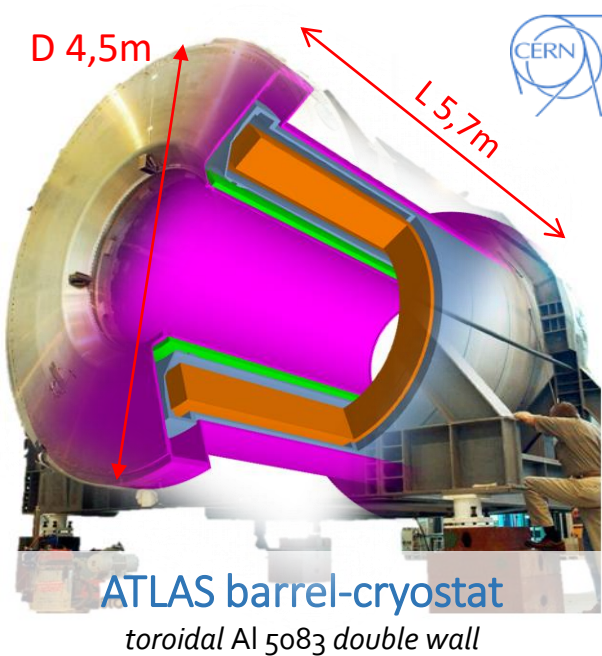
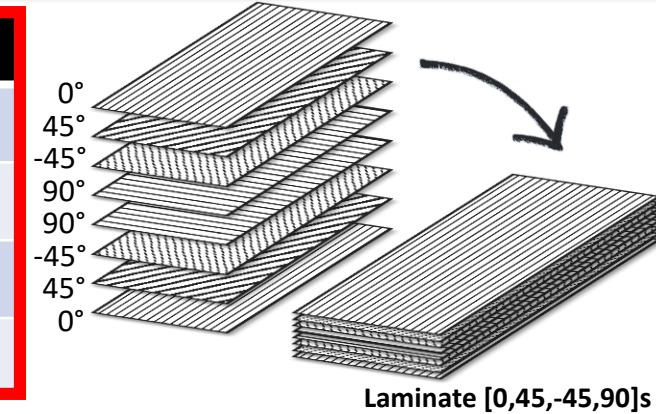
Low material budget cryostat for better detector performance



→ Carbon composite (CFRP) to design cryostats with lower material budget to improve future detectors performance.

Carbon Fiber Reinforced Polymer (CFRP)

Properties at Troom *	SS 304 (CMS)	Invar 36	Al 5083 (ATLAS)	G10 (GFRP)	CTD-133 (CFRP)
Tensile Strength [MPa]	505	448	290	262 / 48.2	2082 / 48.2
Density [Kg/m ³]	8 000	8 050	2 600	1 800	1 130
Rad. Length [mm]			88.9	167	260
CTE [$\mu\text{m}/(\text{m} \times \text{K})$]	17.3	1.30	23.8	9.9 / 11.9	-0.3 / 50



Done / Ongoing / R&D ++

1. He-leak-tight (Troom & 87 K)?
2. Interfaces CFRP-Metal FTs?
3. Large Scale Manufacturability?
4. LAr-leak-tight (87 K) long term?
5. Vacuum tight (87K) long term?
6. Radiation Resistance (0.1MGy)?
7. Full carbon Composite Cryostat

Bread Board Models

Engineering Model (CAD)
+
(Bread Board Model)

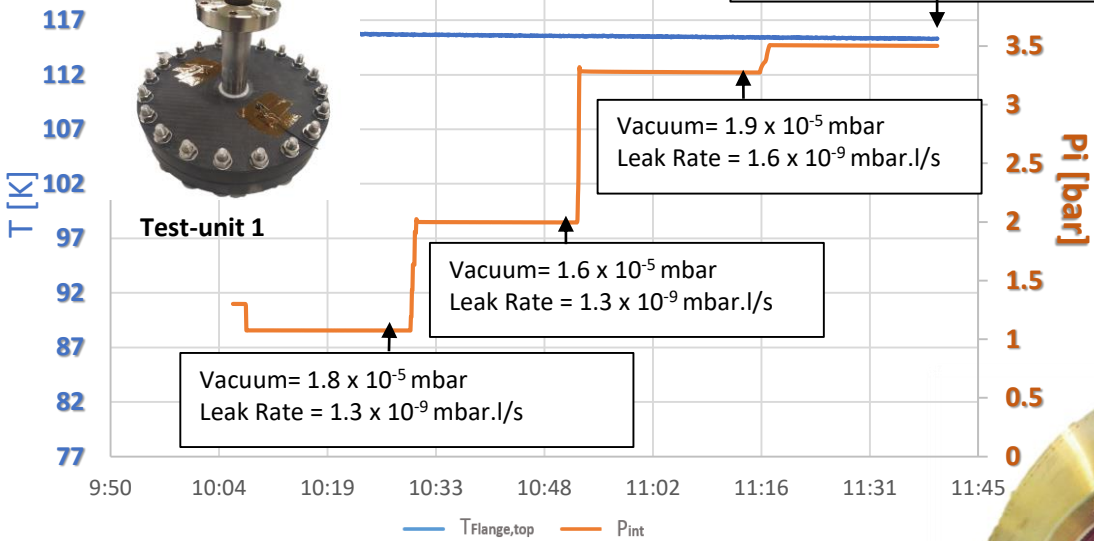
Engineering Model (CAD)
+
1mD Concept Demonstrator

→ State of the Art: Aerospace Industry is adopting CFRP solutions for LH2 large scale cryotanks in short term applications

Breadboard Model: Leak-tightness

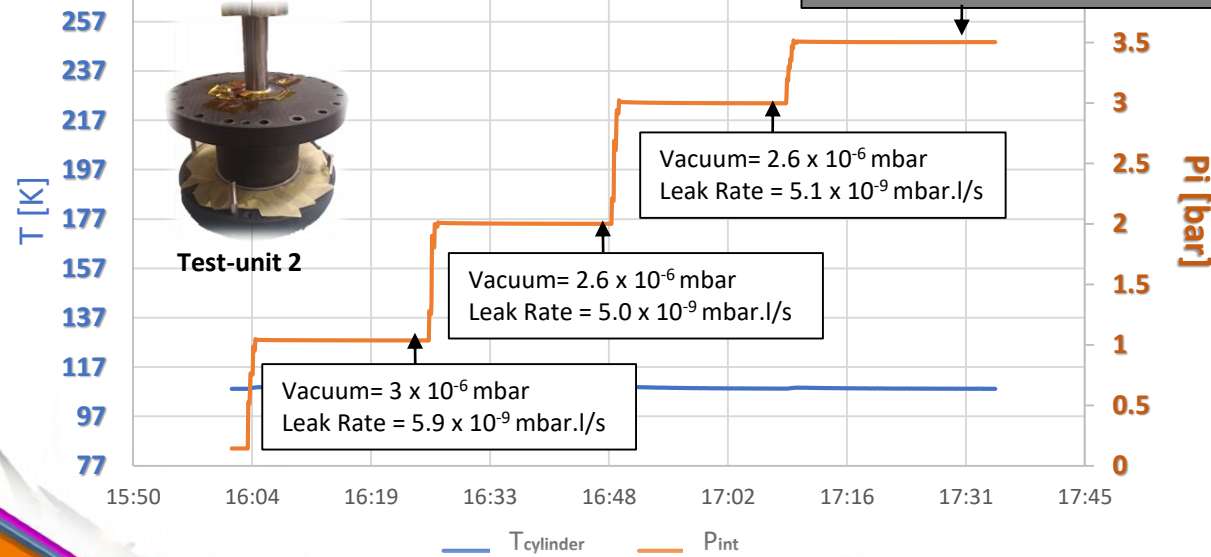
CFRP Flanges - Pressure test - T115K

Vacuum= 2.25×10^{-5} mbar
Leak Rate = 1.3×10^{-9} mbar.l/s ✓



CFRP vessel - Pressure test - T108K

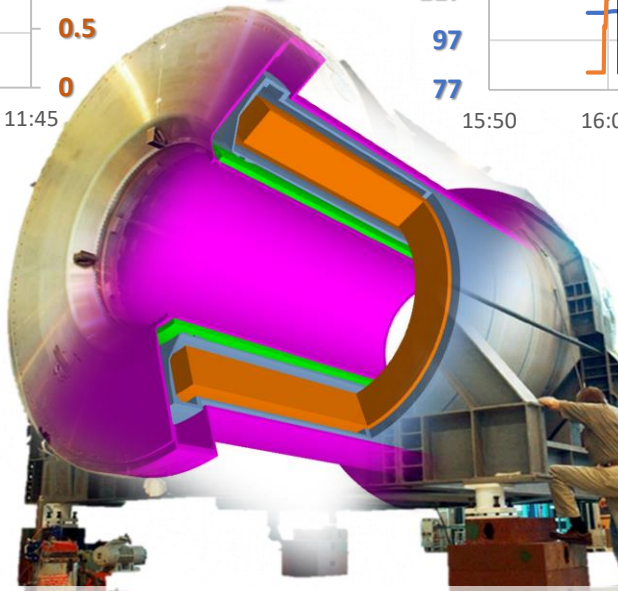
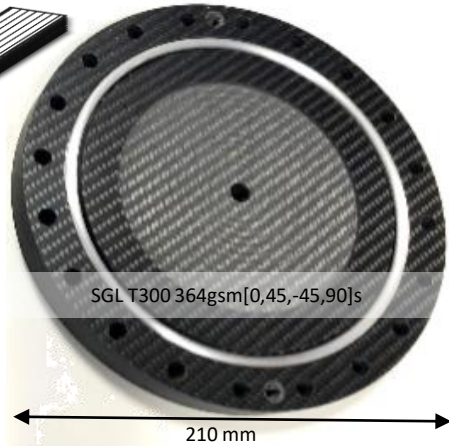
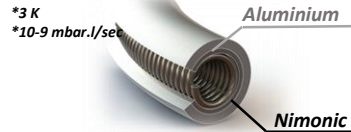
Vacuum= 2.6×10^{-6} mbar
Leak Rate = 5.1×10^{-9} mbar.l/s ✓



Dismountable joint for cryogenics

Helicoflex metallic seal validated at T=115K* and Pint,max = 3.5 bar

Helicoflex (UHV at CERN)



-Thermal insulation: $10e-5$ mbar and 293 K
-LAR tightness ($10e-9$ mbar.l/s*): 3.5 bar and 87 K

Liner-less wall for cryogenics:

CTD-133 toughened resin validated at T=108K* and Pint,max = 3.5 bar



Microcrack resistant epoxy resin

12 x 145gsm CTD133	5mm
12 x 70gsm CTD133	
12 x 70gsm CTD133	
12 x 145gsm CTD133	

Linerless Hybrid laminate: [0/-15/15/-30/30/-45/45/-60/60/-75/75/90]_s

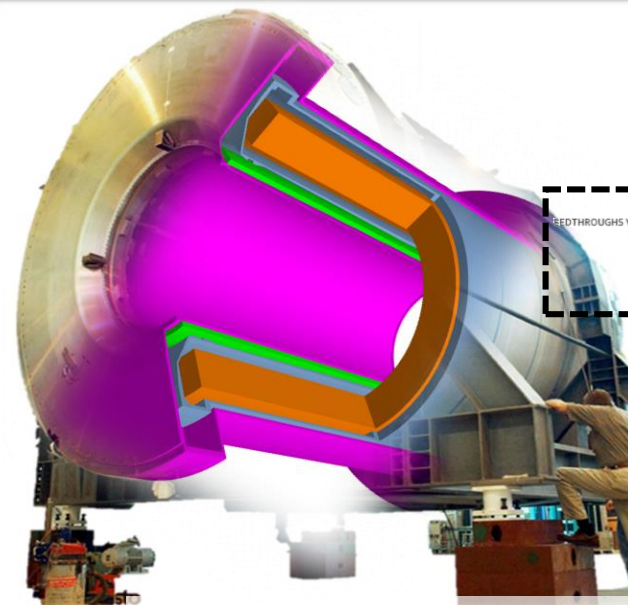
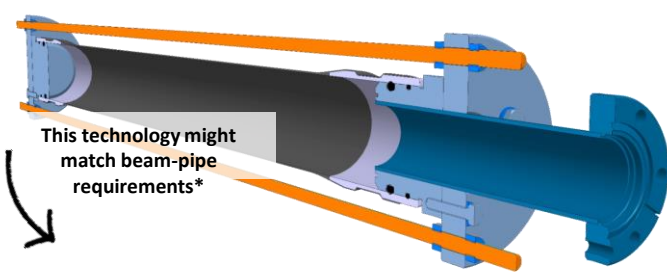
→ Two prototypes built and tested to address thin-wall tightness and sealed joint for CFRP cryostats.

Breadboard Models: Metal-CFRP interface



- Glass fiber + resin
- Carbon fiber + resin
- Glass fiber + resin
- SS end-fitting

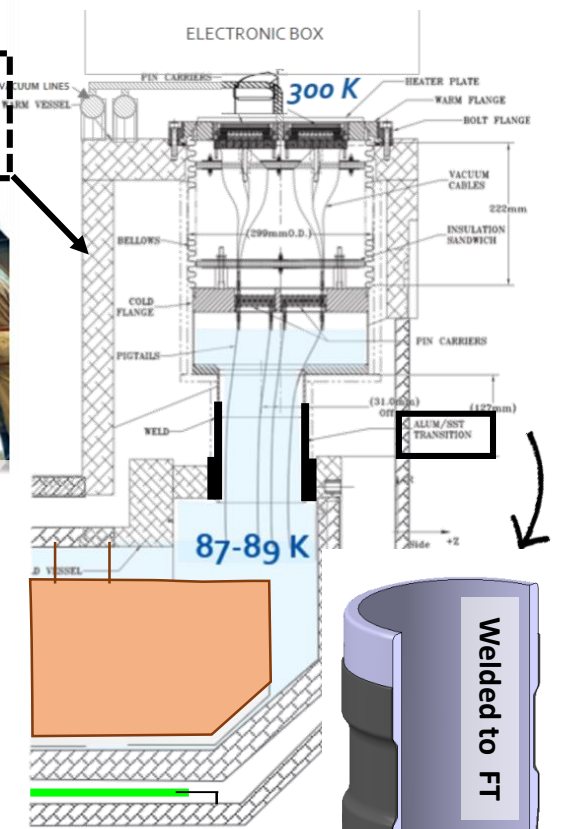
connova
 This joint is design to be optimal at cold temperatures: polymeric fibers contacts more than metal and carbon fiber)*



66 Metallic Feedthroughs (FTs) for input/output lines



Cryostat for SC magnet and LArCal:
 -Thermal insulation: 10e-5 mbar and 293 K
 -LAr tightness: 3.5 bar and 87 K



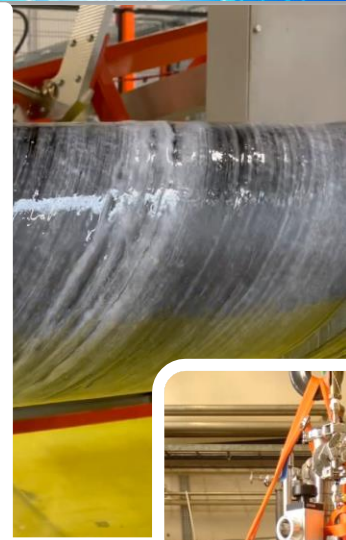
Glued to CFRP cryostat

Tube	Resin	Fiber	Wall thickness	End-Fittings	He leak rate (293 K)	He leak rate (100K)
1	CTD-7.1	T800H	0.7 mm	SS 314	10e-9 mbar.l/sec	-
2	Araldite	T800H	1.5 mm	SS 314	10e-11 mbar.l/sec	leak < 10e-7 mbar.l/sec
3	CTD-7.1	T800H	1.5 mm	SS 314	10e-10 mbar.l/sec	-
4	Araldite	T800H	0.7 mm	SS 314	leak < 10e-7 mbar.l/sec	-

Pipe offers leaktightness, but metal-CFRP interface requires optimization*

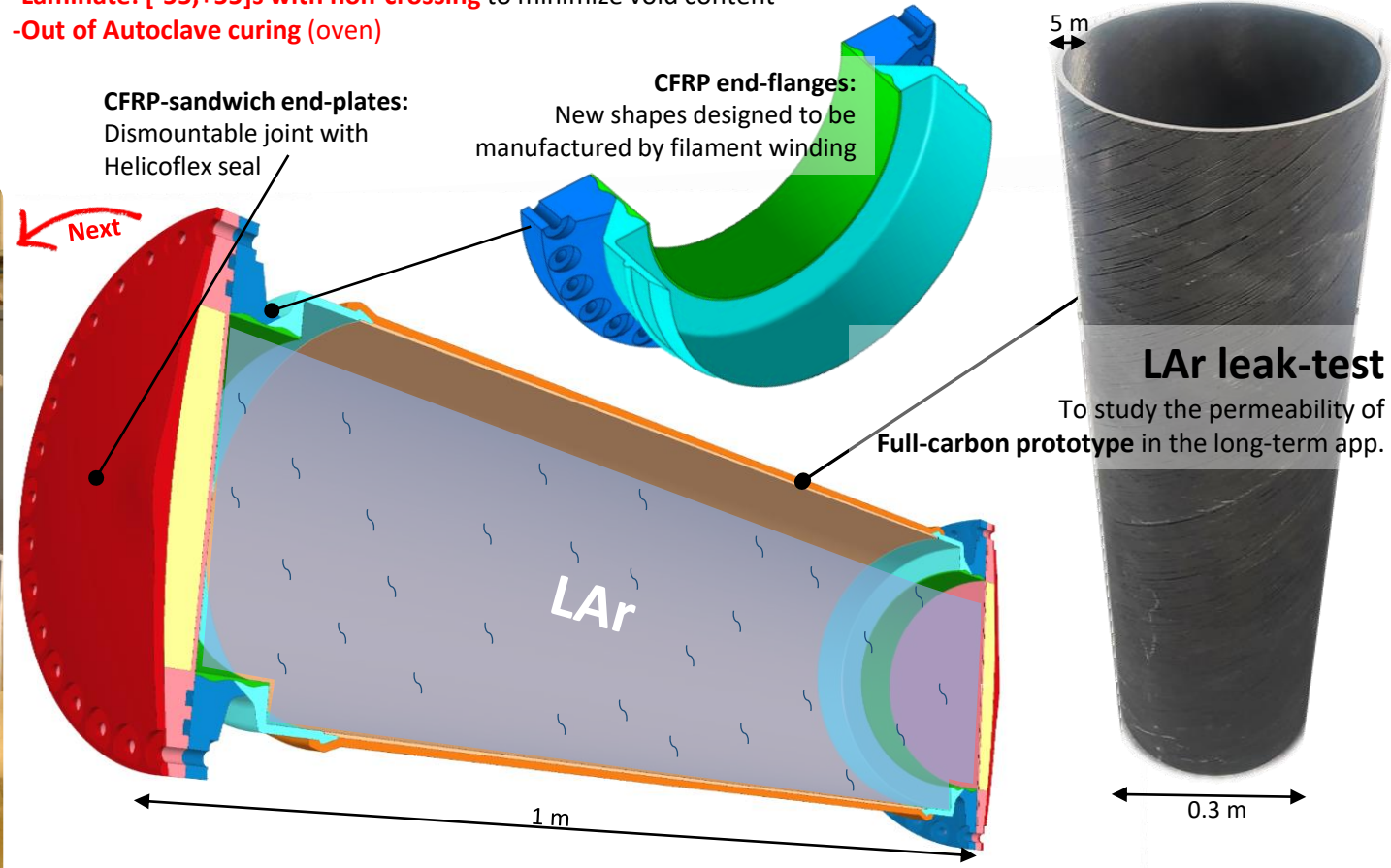
→ Leak-tight interface between carbon composite cryostat and metallic feedthroughs is under study.

Engineering model: Large scale manufacturing

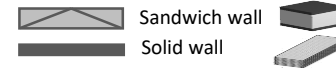
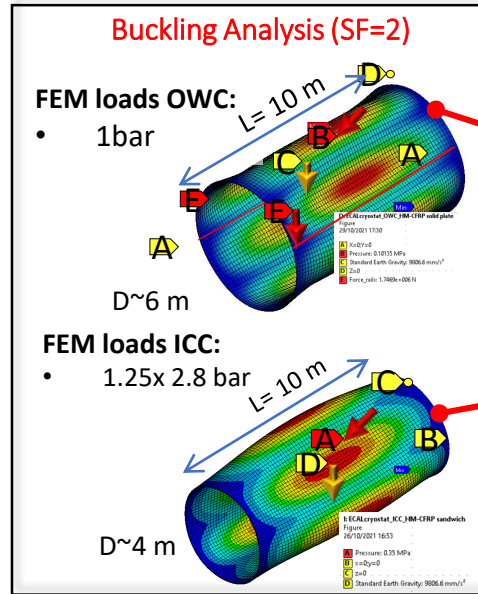
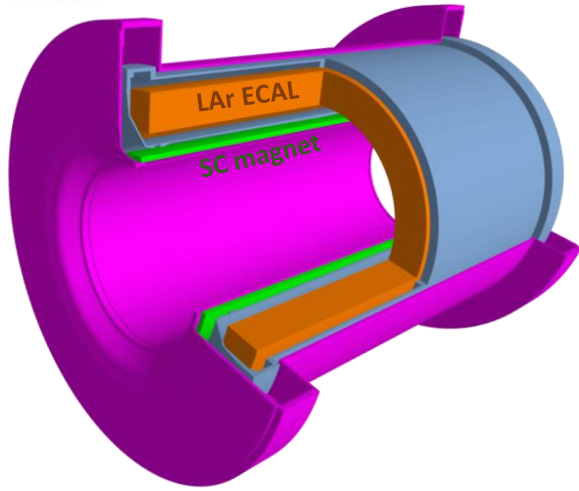


Process development for Wet Filament Winding as an alternative to RAFP tech.

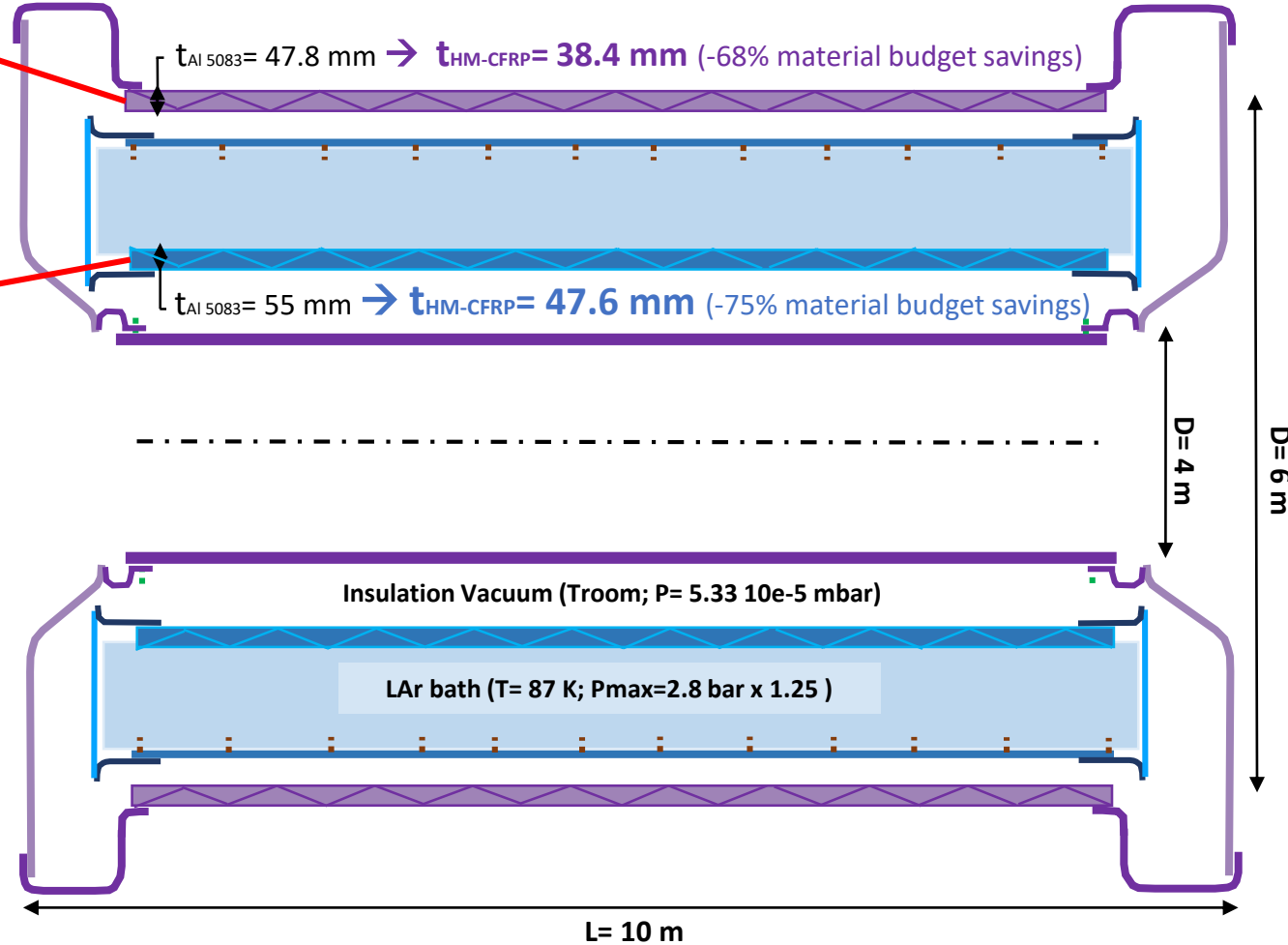
- Optimize resin bath preparation and size to minimize void content: CTD-7.1 and LY 556
- Optimize carbon fiber young modulus (as high as the winding process allows it): M40J
- Optimize carbon fiber tension to increase cross-ply density (permeation resistance).
- Laminate: [-55,+55]s with non-crossing to minimize void content
- Out of Autoclave curing (oven)



→ Automated process for large-scale production is under development to achieve a laminate with minimal void content.



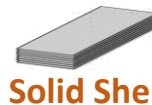
Baseline geometry FCC-hh LAr barrel ECAL



Sandwich Shell



Skin [0,45,-45,90]s
Core : Al Honeycomb
Skin [0,45,-45,90]s



Radiation length X_0 [mm]



Al = 88.9
HM CFRP = 260
Honeycomb Al = 6000

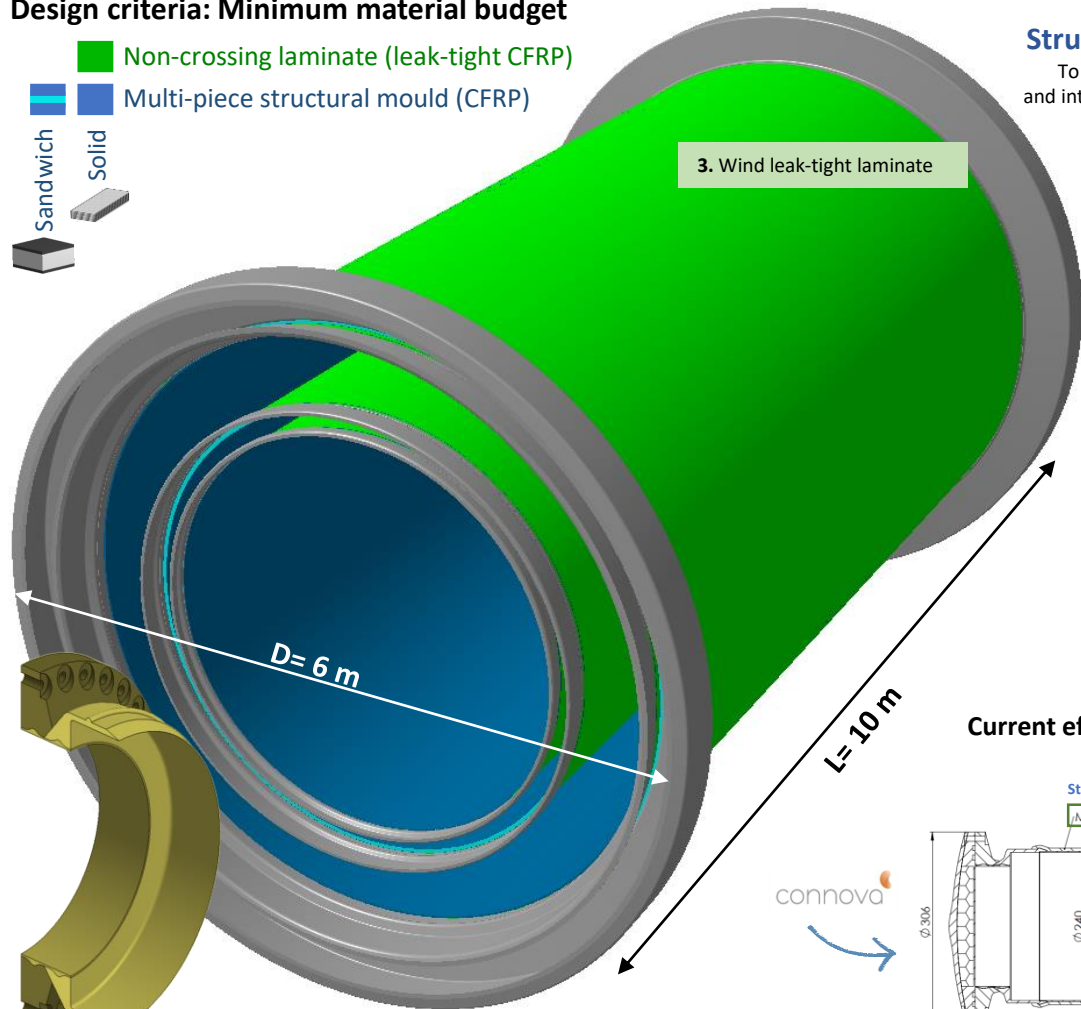
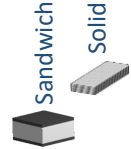
Criteria: Safety Factor = 2	Sandwich shell				Solid shell			
	HM CFRP		Al		HM CFRP		Al	
	OWC	ICC	OWC	ICC	OWC	ICC	OWC	ICC
Material budget X/X_0	0.03	0.043	0.094	0.17	0.092	0.12	0.34	0.44
X_0 % savings	-68%	-75%	REF	REF	-2%	-29%	262%	159%
Skin Th. [mm]	3.2	4.8	3.9	7.5				
Core Th. [mm]	32	38	40	40				
Total Th. [mm]	38.4	47.6	47.8	55	24	30.4	30	39
Thickness % savings	-20%	-13%	REF	REF	-50%	-45%	-37%	-29%

→ CFRP cryostat walls will provide savings in terms of material budget/thickness with respect to an aluminum cryostat

Full-CFRP Cryostat (R&D ++)

Design criteria: Minimum material budget

-  Non-crossing laminate (leak-tight CFRP)
-  Multi-piece structural mould (CFRP)



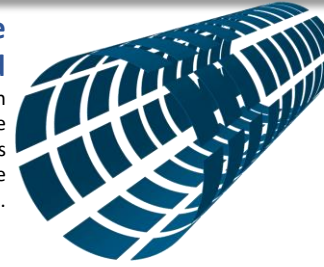
End-Flanges

Fully manufactured by filament winding:

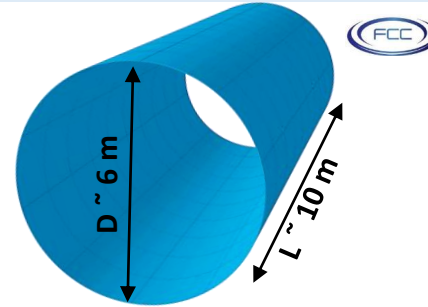
- *Leak-tight integration with cylindrical walls
- *Carrying axial and radial loads

Multipiece Structural Mould

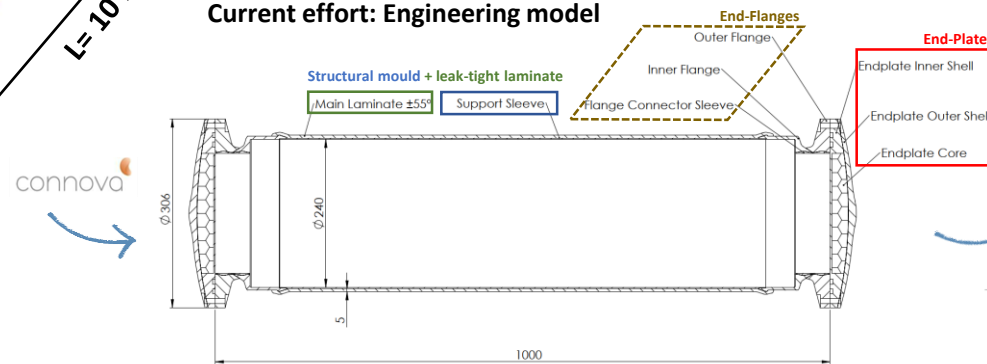
To simplify production and integration due to the large dimensions expected in future detectors.



2. Assembly of the large cylindrical structural-mould



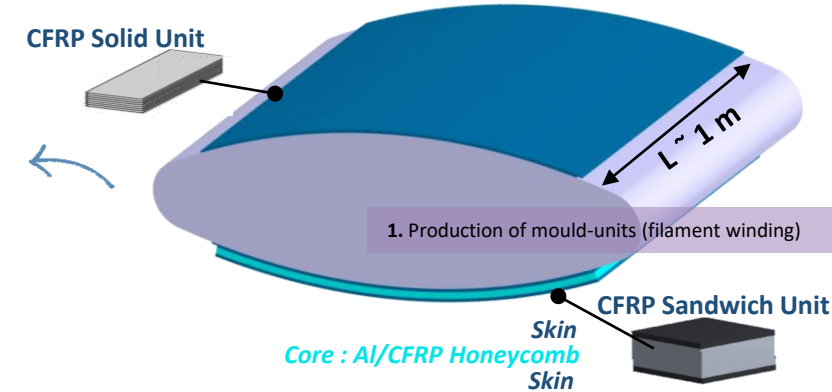
Current effort: Engineering model



Development of a large multifunctional carbon composite mould

A) Tool: to wind cryostat walls (toughened epoxy resin at cryogenics)

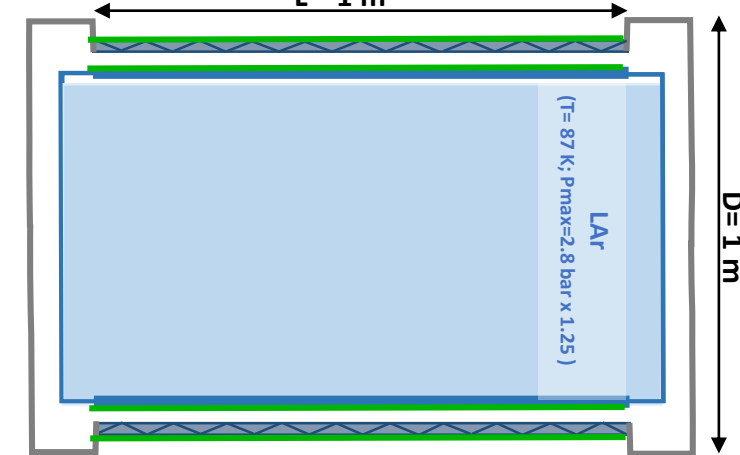
B) Structural part: carry the loads expected in each of the cylindrical walls of future cryostats



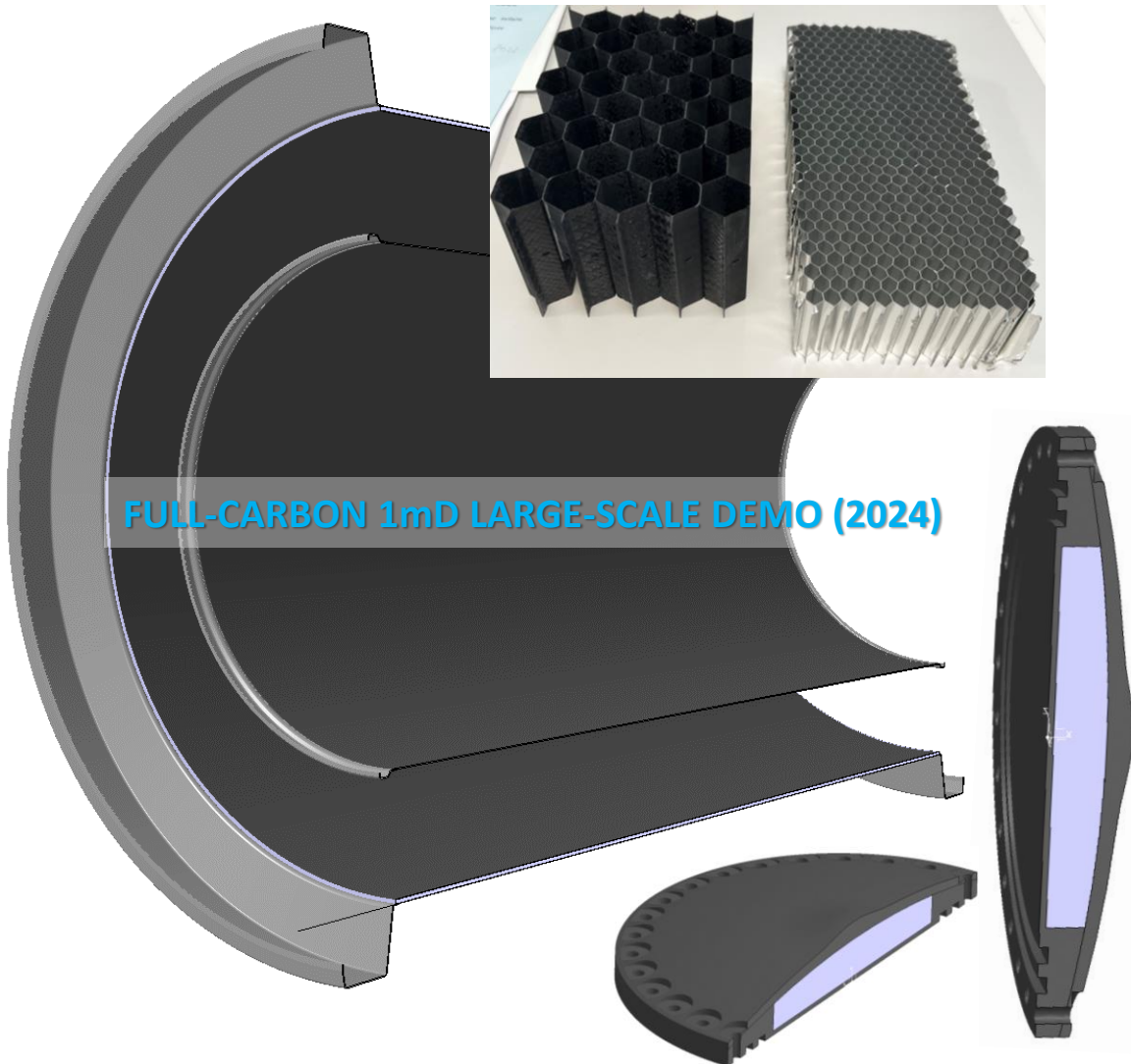
FULL-CARBON LARGE-SCALE concept demonstrator (2024)

Collaboration

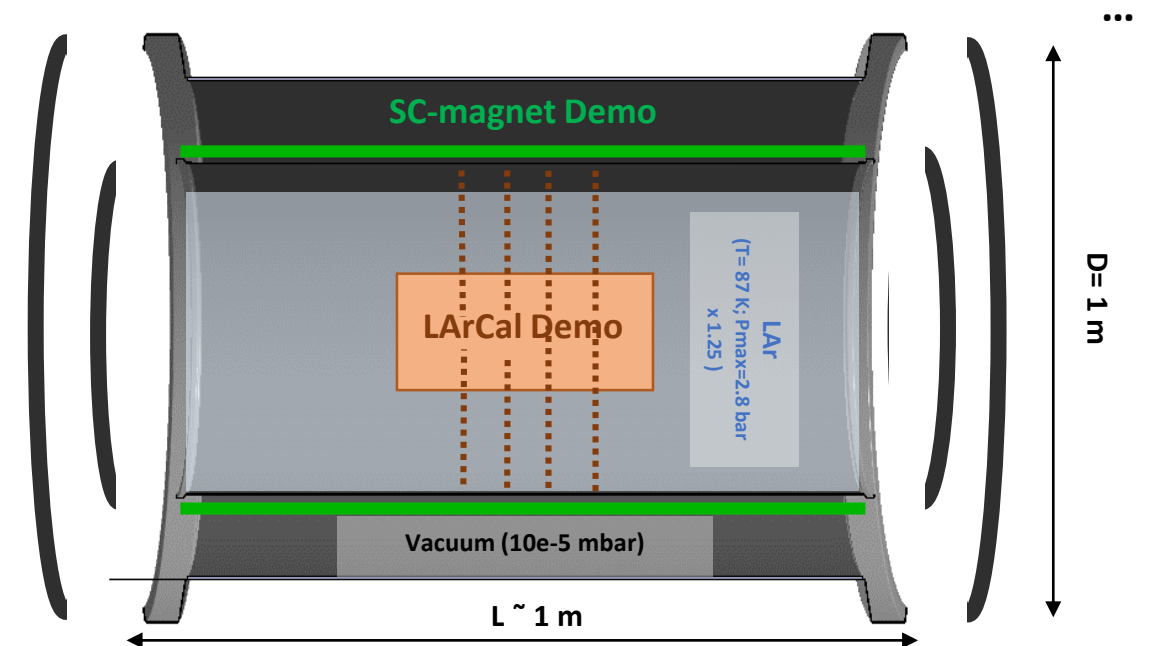
- *CERN Cryolab for testing campaign
- *WP3 and WP8 for a common demo



→ Full carbon composite demonstrator based on learnings from breadboard models and large-scale concept development.



- WP3 LArCal** - Requirements & Concept Demonstrator
- WP8 SC magnet** - Requirements & Concept Demonstrator
- Connova & Workshape** –Prototyping & Large-Scale Manufacturing, Material
- CERN Cryolab** - Assessment & Testing (Lar and He leaktightness)
- CERN EN/MM** – Mech characterization at Troom and 87K
- CERN SY/STI** - Radiation Hardness
- ALICE 3** – Cryostat and services for a Large SC Magnet (Cryo & Power)
- AMS** - Full carbon HC core



→ Full carbon composite demonstrator based on learnings from breadboard models and large-scale concept development



Thank you very much

Back-Up

1. What has been done?

- a) Design requirements, materials and processes
- b) CFRP liner-less wall leak-tight at cryogenics (breadboard model tested)
- c) Dismountable joint between CFRP parts at cryogenics (breadboard model tested)



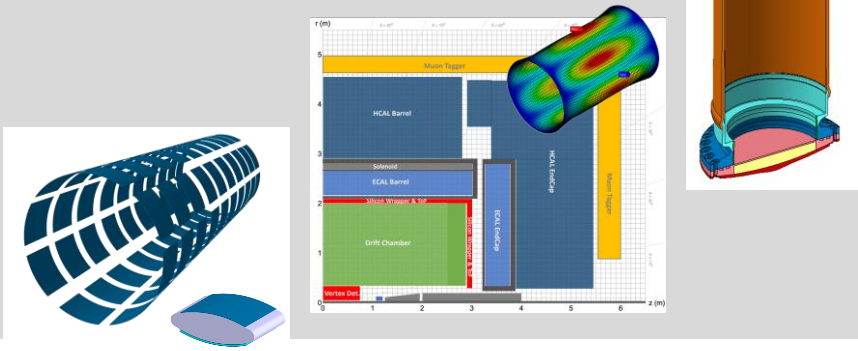
2. Ongoing ...

- a) Interface between CFRP cryostat and metallic feed-throughs (samples to be tested)
- b) Automated manufacturing process for large-scale CFRP cryostat (engineering model to be tested)



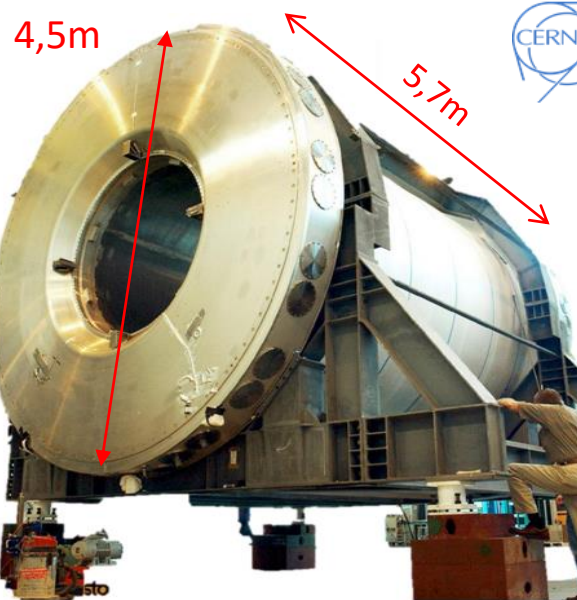
3. What is next?

- a) Detailed analysis of a large CFRP cryostat for FCC Detector Concept
- b) 1m diameter concept demonstrator (R&D ++)



Thank you very much !

ATLAS barrel-cryostat toroidal Al 5083 double wall



6 x 10m in future cryostats*

1. Tightness in long term

Cold vessel: LAr leak-tight
Warm vessel: Vacuum tight

2. Operating conditions:

Cold vessel: $T = 87\text{ K}$; $P_{\text{int,max}} = 2.8\text{ bar}$
Warm vessel: T_{room} ; $P_{\text{int}} = 10^{-5}\text{ mbar}$

3. Radiation Resistance:

Total lifetime dose < 0.1 MGy

4. Minimize material budget

Al 5083 thin wall+ buckling resistant design *



1. Tightness in short term

Tank wall: LH2 (LOX) leak-tight
Tank skirt: Vacuum tight

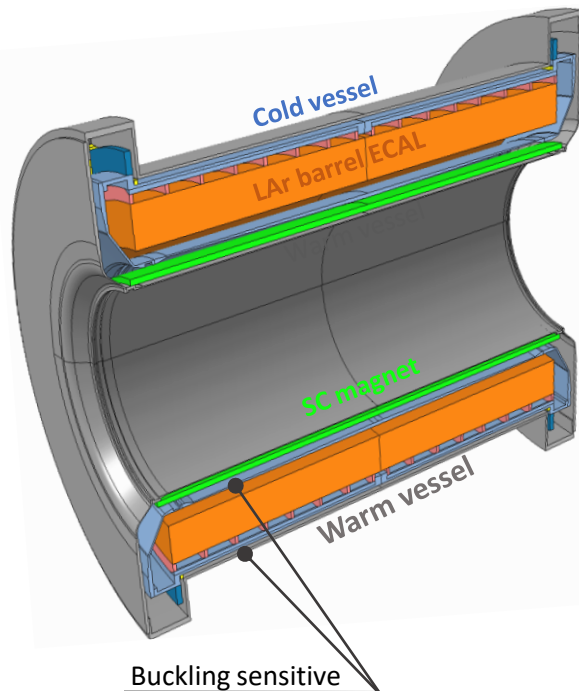
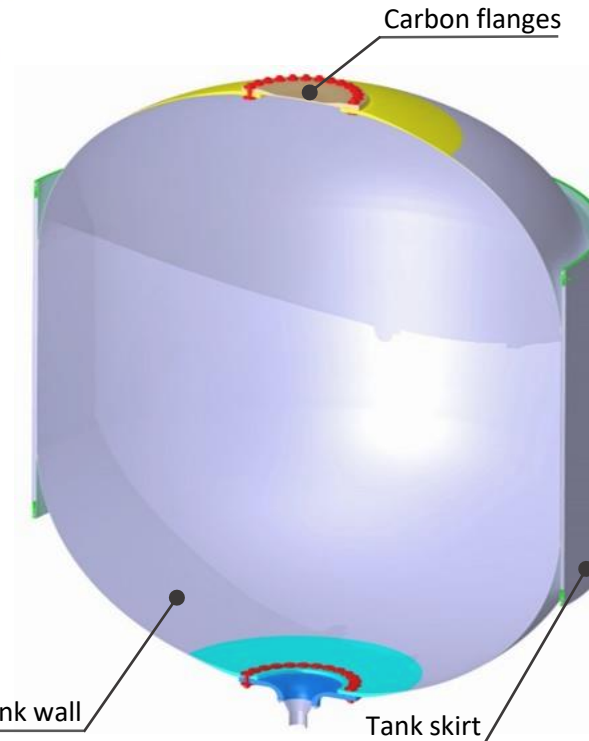
2. Operating condition:

Tank wall: $T = 20\text{ K}$; $P_{\text{int,max}} = 3.2\text{ bar}$
Tank skirt: T_{room} ; $P_{\text{int}} = 10^{-5}\text{ mbar}$

3. Minimize mass

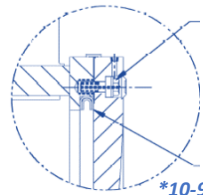
CFRP thin wall + stiffening skirt

NASA's CCTD LH2 cryotank All carbon composite thin wall



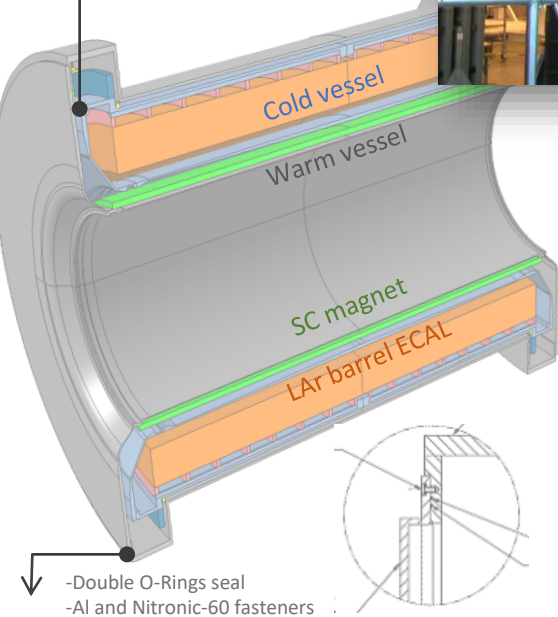
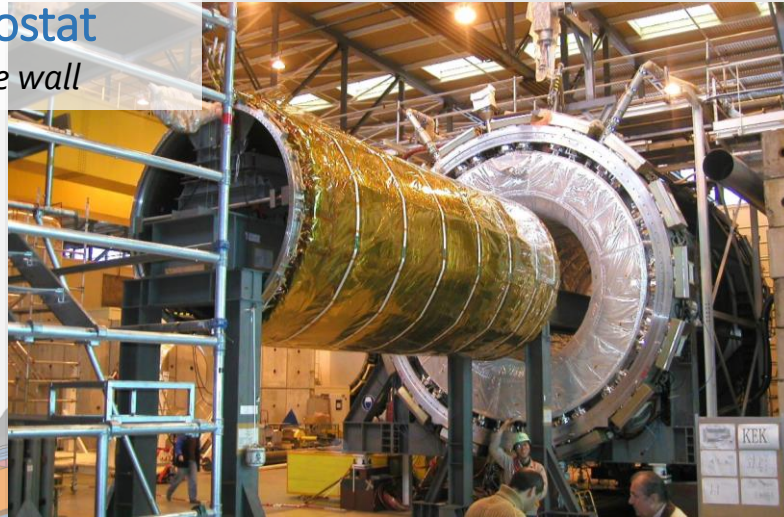
✓ Cryostats to house the SC-magnet and LAr-ECAL have similar requirements with cryotanks to storage LH2 in launch vehicles

ATLAS barrel-cryostat toroidal Al 5083 double wall



*87K
*10-9 mbar.l/sec

-Omega seal
-Nitronic-60 fasteners



1. Material:

Aluminum 5083

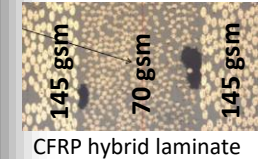
2. Process:

Forming, welding and machining

3. Joints:

Fasteners; polymeric seals (warm)
Fasteners; metallic seal → welded (cold)

NASAS's CCTD LH2 cryotank Linerless carbon composite thin wall



CFRP hybrid laminate

1. Material

Leak-tight linerless wall: CFRP hybrid laminate (thick and thin plies)

- a) Resin: Microcrack resistant (CTD, 5320-1, MTM45-1, M56, TC250...)
- b) Carbon Fiber: higher modulus compatible with manufacturing process

2. Process:

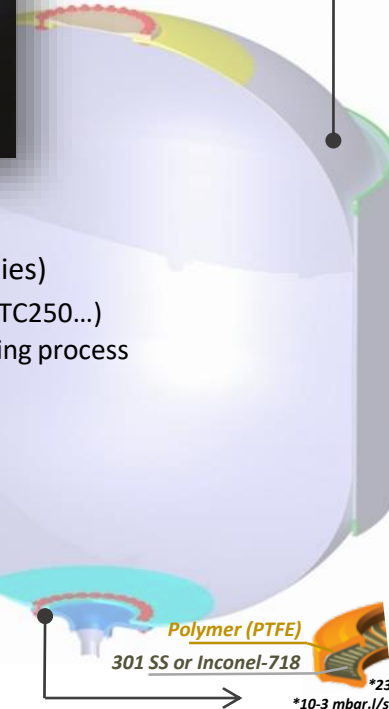
Robotic Automated fiber placement (RAFP)

Out of Autoclave (OoA) curing

3. Joints

Permanent: Hot-bonded and co-cured

Dismountable: Fasteners, Belleville washers and Furon Seal

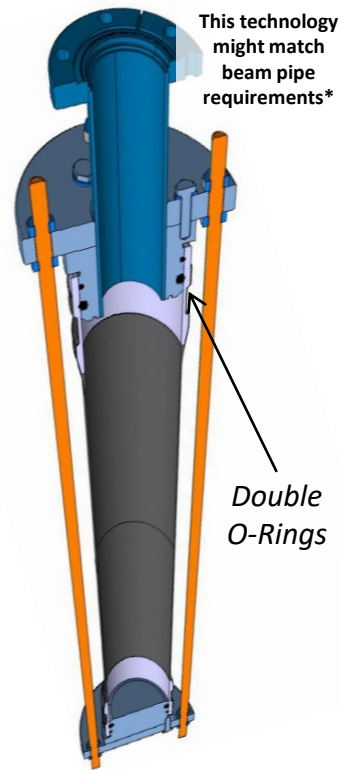


Polymer (PTFE)
301 SS or Inconel-718

*23 K
*10-3 mbar.l/sec

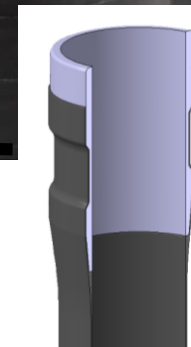
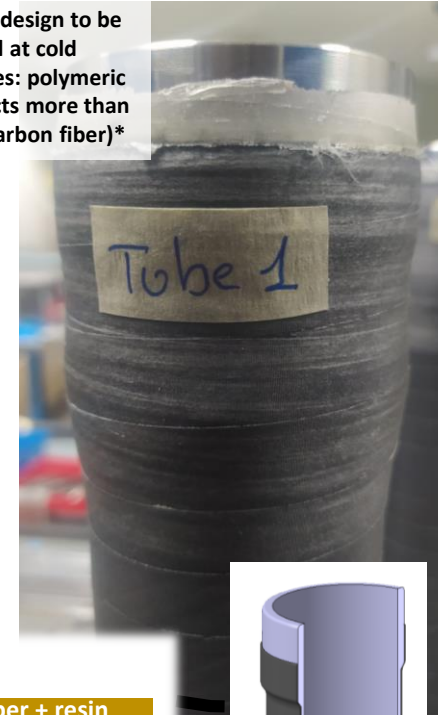
✓ R&D required to adapt aerospace technology choices to HEP low mass cryostats

Breadboard Models: Carbon-Metal Interface II



Atlas cryostat: 64 signal FT + 2 HV TF + Solenoid chimney

This joint is design to be optimal at cold temperatures: polymeric fibers contacts more than metal and carbon fiber)*



- Glass fiber + resin
- Carbon fiber + resin
- Glass fiber + resin
- SS end-fitting



Tube	Resin	Fiber	Wall thickness	End-Fittings	He leak rate (Room)
1	CTD-7.1	T800H	0.7	SS 314	10e-9 mbar.l/sec
2	Araldite	T800H	1.5	SS 314	10e-11 mbar.l/sec
3	CTD-7.1	T800H	1.5	SS 314	10e-10 mbar.l/sec
4	Araldite	T800H	0.7	SS 314	leak < 10e-7 mbar.l/sec -> interface

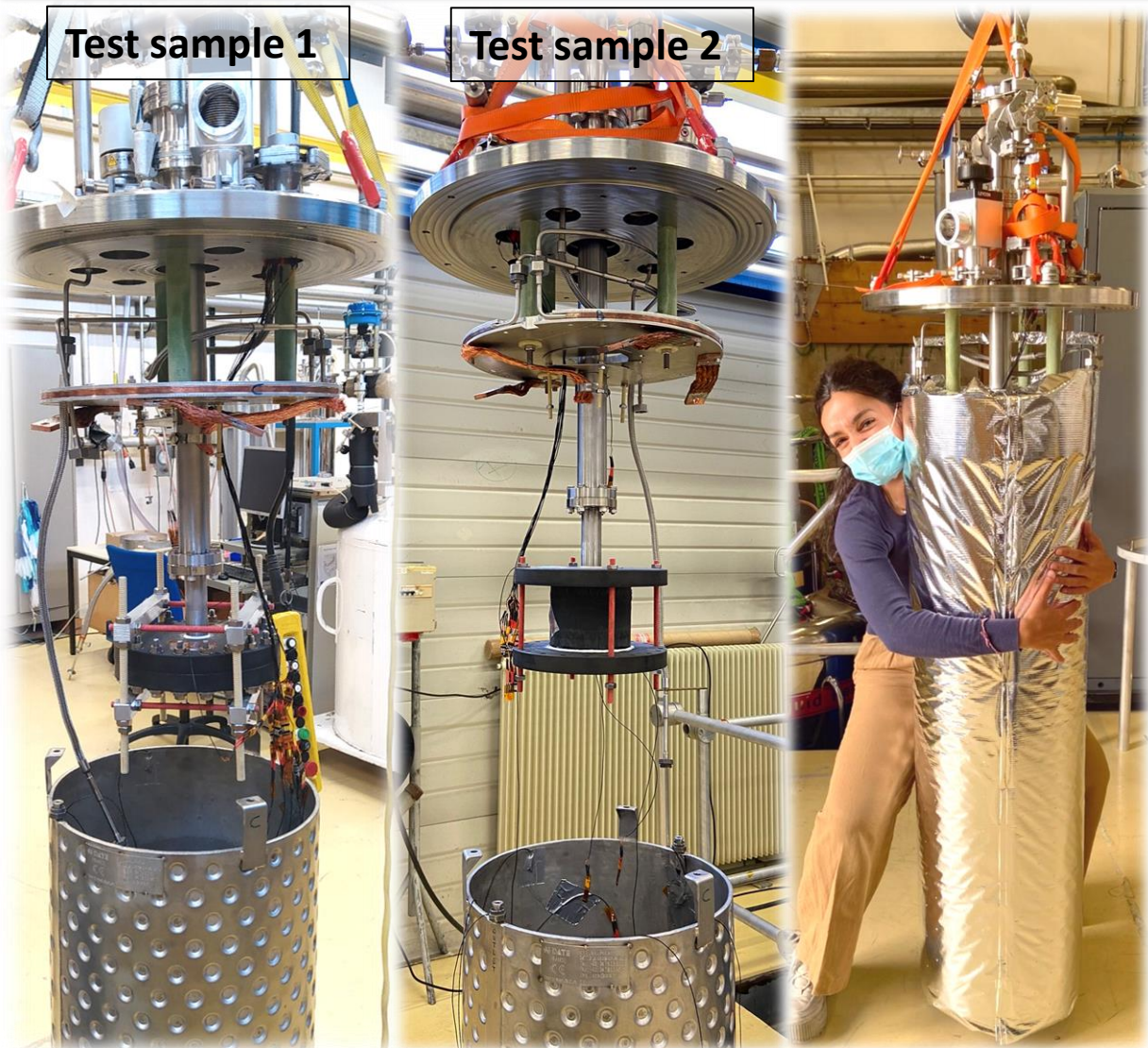
We are in need of collaboration to validate it this joint at 87K*

→ Non conventional bonding between metal-carbon parts needs to be validated at LAr temperature (87 K)

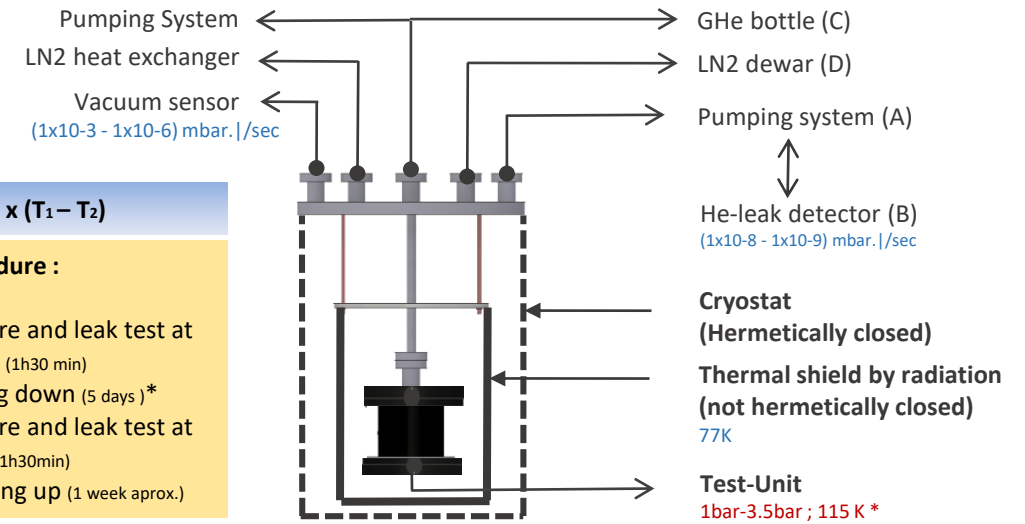
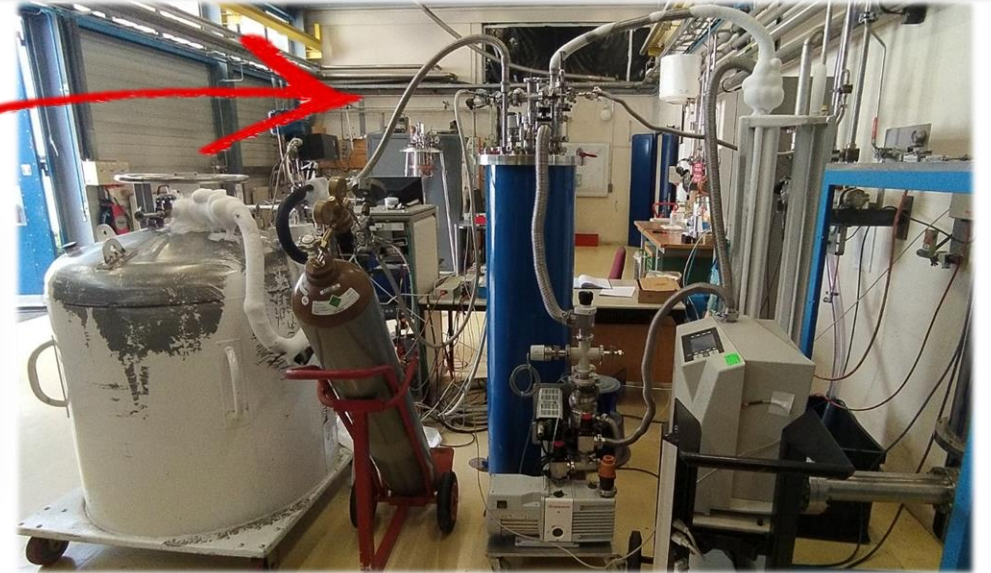
He-leak Test (CERN Cryolab Collaboration)

Test sample 1

Test sample 2



Thanks a lot to :
 Martin Aleksa
 Johan Bremer
 Michel Chalifour
 Maria A. Barba
 Agostino Vacca
 Laetitia Dufay-Chanat
 Sebastien Prunet



$Q_{rad} = \epsilon \times \sigma \times (T_1 - T_2)$

Test Procedure :

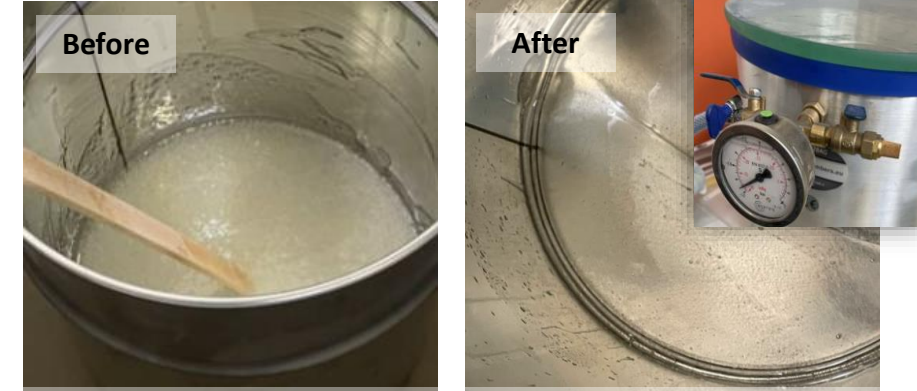
1. Pressure and leak test at Troom (1h30 min)
2. Cooling down (5 days)*
3. Pressure and leak test at Tcryo (1h30min)
4. Warming up (1 week aprox.)

→ Experimental setup allowed us to check He leakage at 3.5 bar and ~110K (test setup limit)

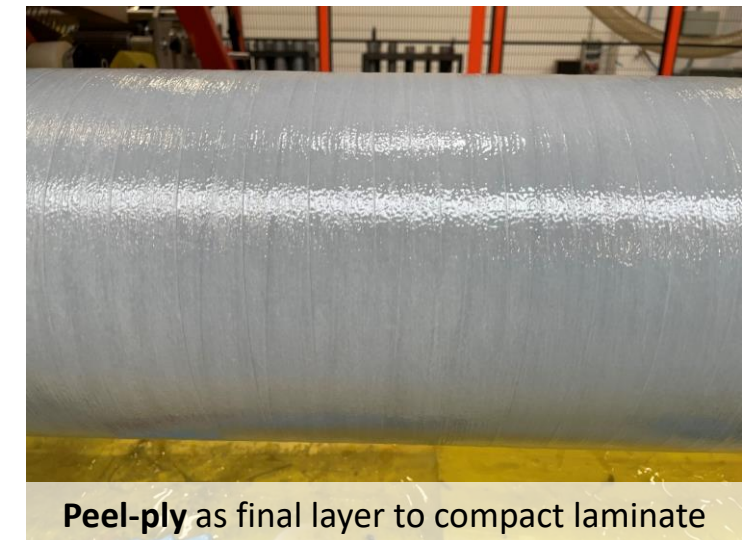


Process development for Wet Filament Winding as alternative to RAFP

- Optimize CTD-7.1 resin bath preparation and size.
- Optimize carbon fiber tension to increase cross plies density (permeation resistance)
- Laminate: [-55,+55]s with non-crossings to minimize void content
- Out of Autoclave curing (oven)



Micro-crack resistant resin at cryogenics includes toughened additives. Vacuum evacuation of resin system is needed to improve void content before winding and to get high mechanical properties.

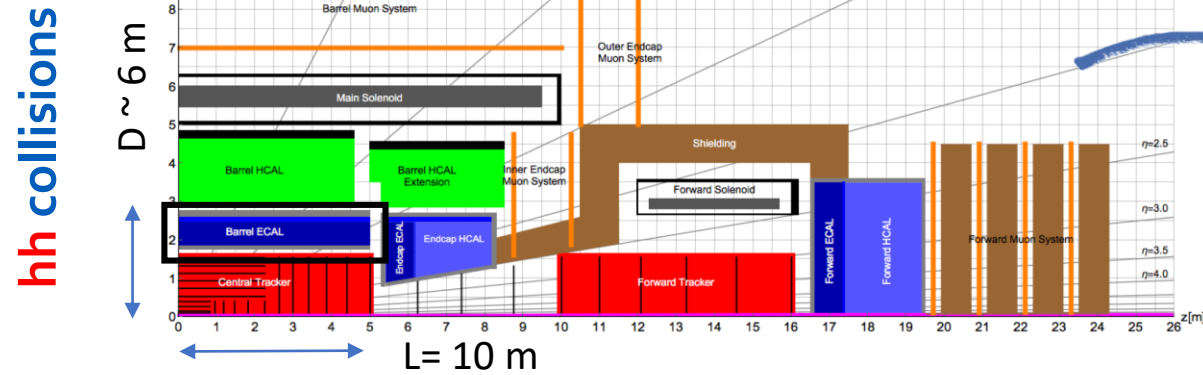


Peel-ply as final layer to compact laminate and evacuate voids

→ Next samples to address filament winding technology as an efficient manufacturing process for larger scale

Baseline geometry, FCC-hh LAr barrel ECAL :

The aluminium cryostat is 5 cm thick, representing 56 % of X_0 at $\eta=0$

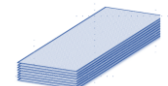


Sandwich Shell



Skin [0,45,-45,90]s
Core : Al Honeycomb
Skin [0,45,-45,90]s

Solid Shell



Radiation length X_0 [mm]
Al = 88.9
HM CFRP = 260
Honeycomb Al = 6000

Criteria: Safety Factor = 2	Sandwich shell				Solid shell			
	HM CFRP		Al		HM CFRP		Al	
	OWC	ICC	OWC	ICC	OWC	ICC	OWC	ICC
Material budget X/ X_0	0.03	0.043	0.094	0.17	0.092	0.12	0.34	0.44
X_0 % savings	-68%	-75%	REF	REF	-2%	-29%	262%	159%
Skin Th. [mm]	3.2	4.8	3.9	7.5				
Core Th. [mm]	32	38	40	40				
Total Th. [mm]	38.4	47.6	47.8	55	24	30.4	30	39
Thickness % savings	-20%	-13%	REF	REF	-50%	-45%	-37%	-29%

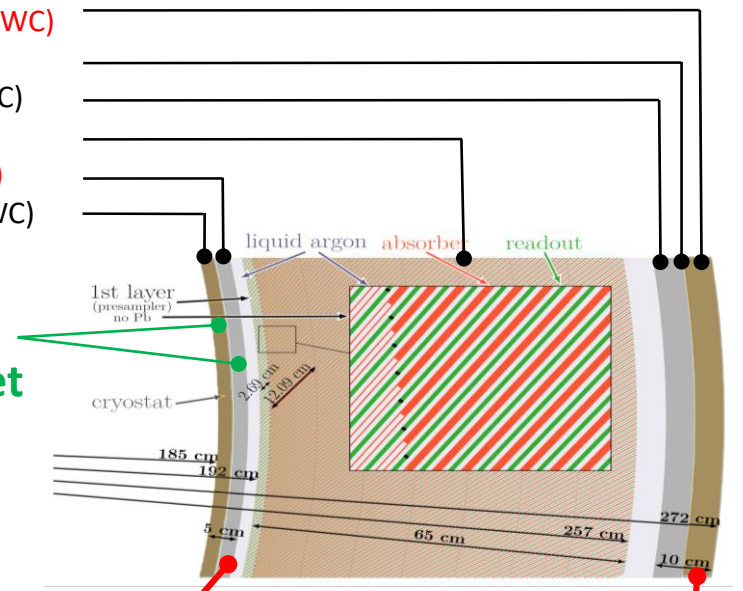
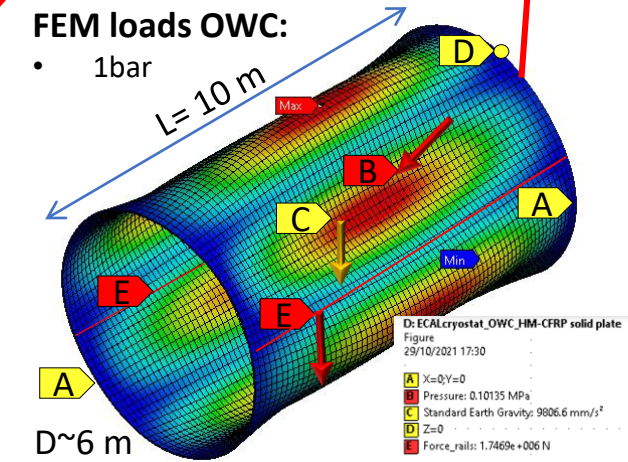
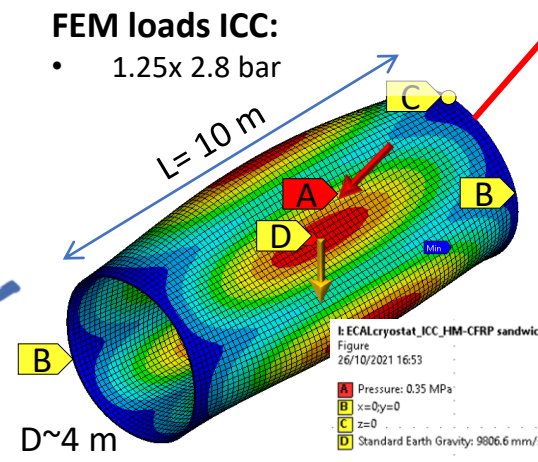
- Outer warm cylinder (OWC)
- Insulation vacuum
- Outer cold cylinder (OCC)
- LAr ECAL
- Inner cold cylinder (ICC)
- Inner warm cylinder (IWC)

Minimum material budget

Buckling resistance

FEM loads ICC:
• 1.25x 2.8 bar

FEM loads OWC:
• 1bar

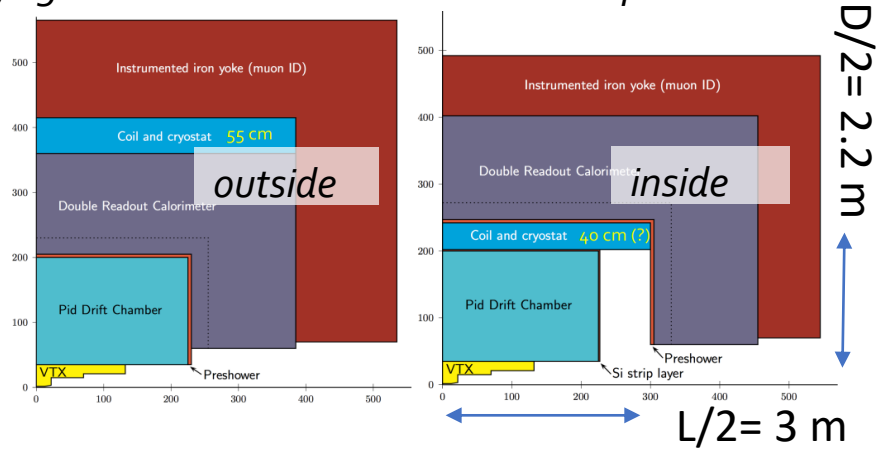


→ CFRP cryostat walls will provide savings in terms of material budget/thickness respect to Aluminum

Baseline geometry, FCC-ee

a very challenging 2T solenoid "ultra-thin and transparent"

e⁺e⁻ collisions



Sandwich



Skin [0,45,-45,90]s
Core : Al Honeycomb
Skin [0,45,-45,90]s

Radiation length X₀[mm]

Al = 88.9
HM CFRP = 260
Honeycomb Al= 6000

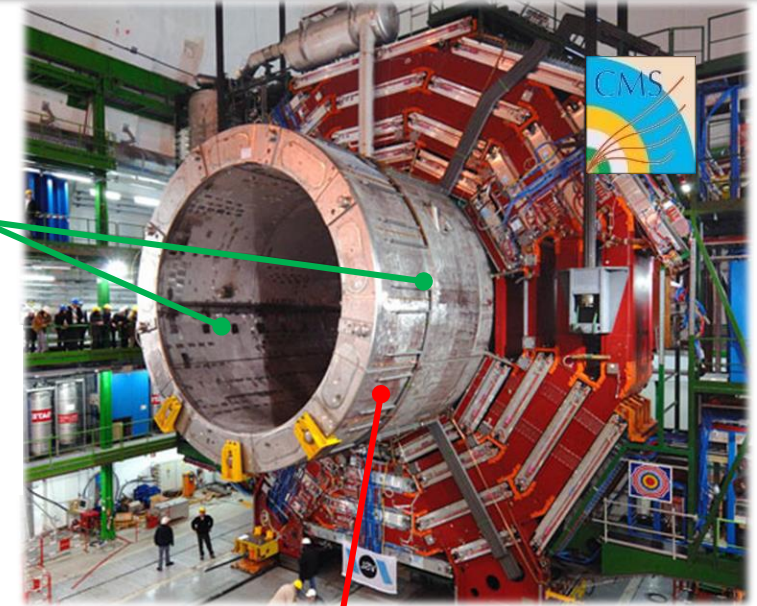
Criteria: Safety Factor = 2	Honeycomb Al		Solid shell	
	HM CFRP	Al	HM CFRP	Al
Material budget X/X ₀	0.017	0.045	0.065	0.24
X ₀ % savings	-62%	REF	44%	433%
Skin Th. [mm]	1.6	1.7		
Core Th. [mm]	26	40		
Total Th. [mm]	29.2	43.4	16.8	20.9
Thickness % savings	-33.00%	REF	-61%	-52%



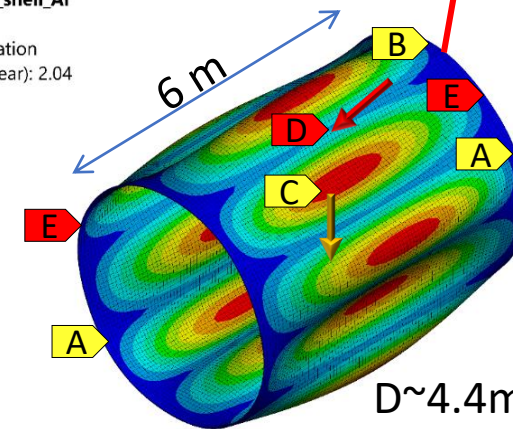
Minimum material budget

Buckling resistance

Patm → Vacuum



G: Buckling_Outer_shell_Al
Total Deformation
Type: Total Deformation
Load Multiplier (Linear): 2.04
Unit: mm



FEM loads OWC:

- 1 bar

A: Outer_shell_Al
Static Structural
Time: 1. s

- A X=0; Y=0
- B Z=0
- C Standard Earth Gravity: 9.81e+003 mm/s²
- D Pressure: -0.101 MPa
- E Force: 3.5e+005 N



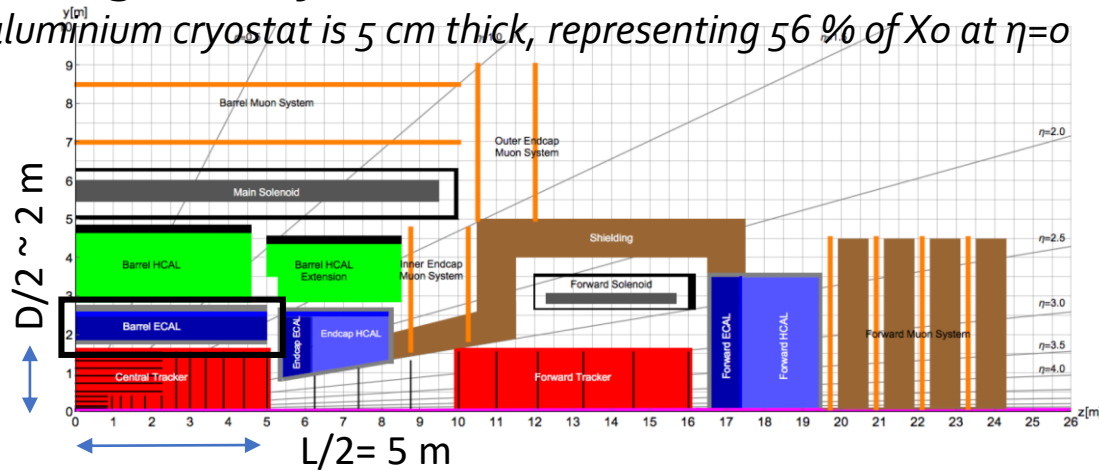
→ CFRP cryostat wall will help to provide savings in terms of material budget/thickness respect to Aluminum

Radiation Environment in future experiments

Baseline geometry, FCC-hh LAr barrel ECAL :

The aluminium cryostat is 5 cm thick, representing 56 % of X_0 at $\eta=0$

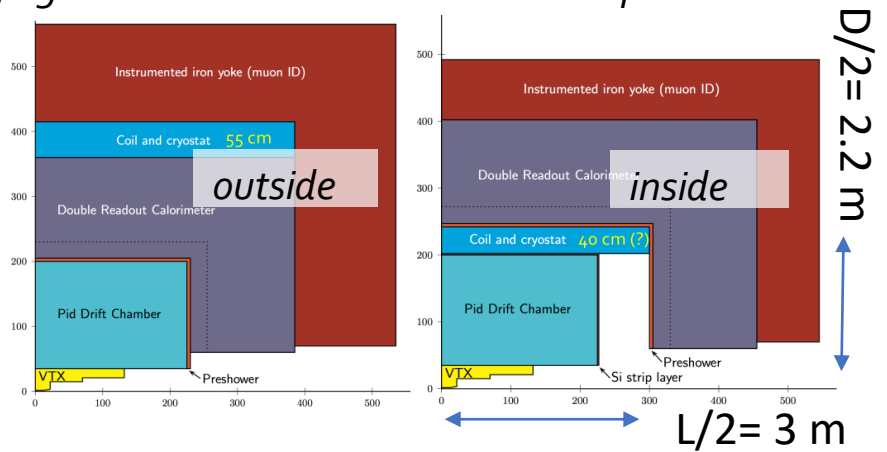
hh collisions



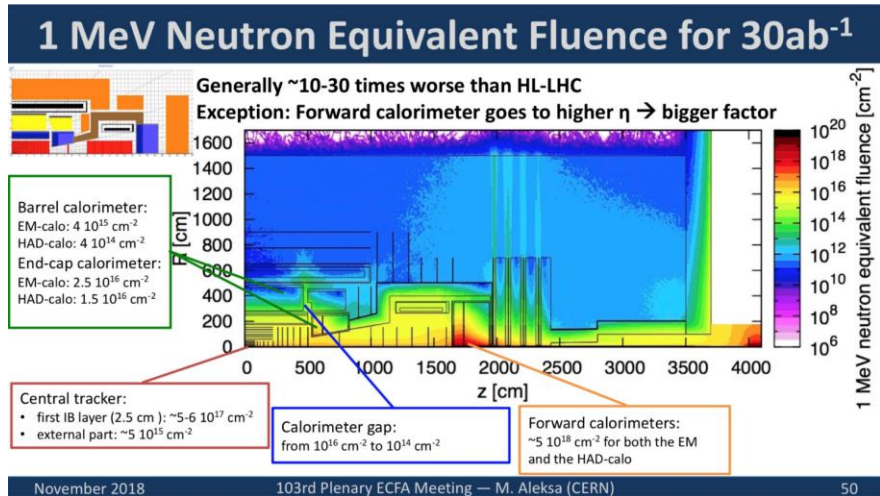
Baseline geometry, FCC-ee

a very challenging 2T solenoid "ultra-thin and transparent"

e+e- collisions



FLUKA simulations



FCC^{hh}: The estimated **radiation** levels at the barrel EM-calorimeter are relevant to the **choice of resin and glue.**

FCC^{ee}: radiation level is almost **negligible.**

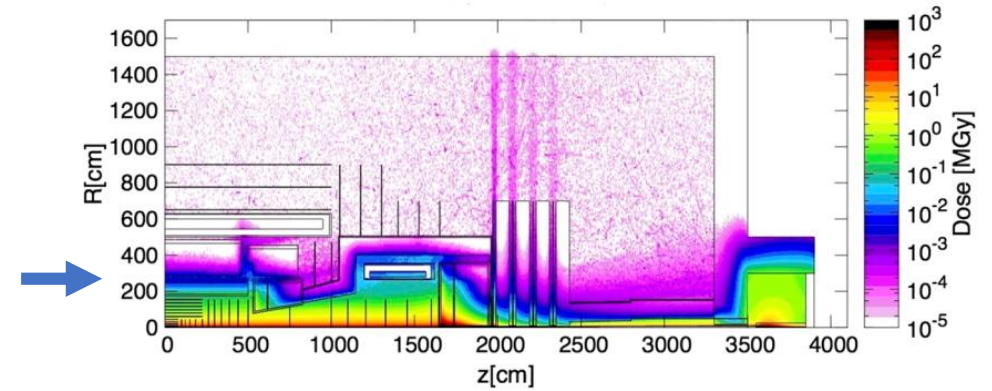
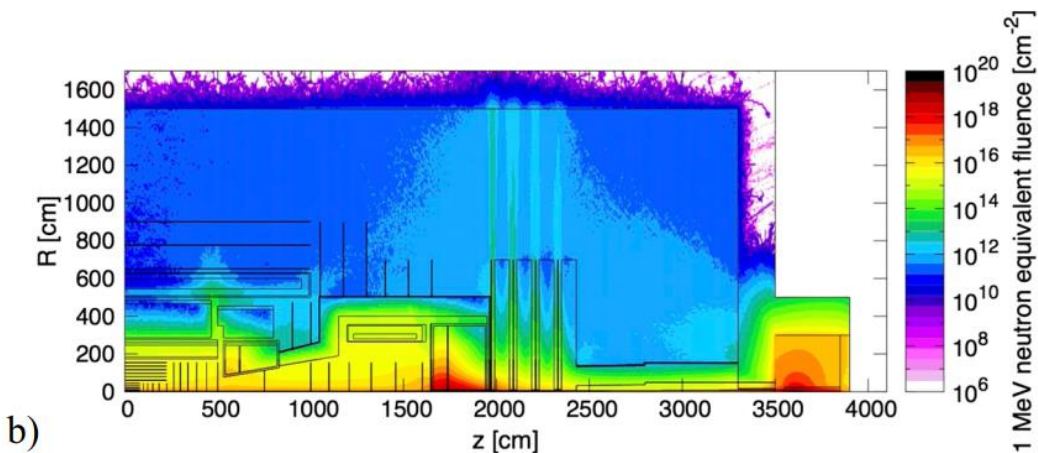
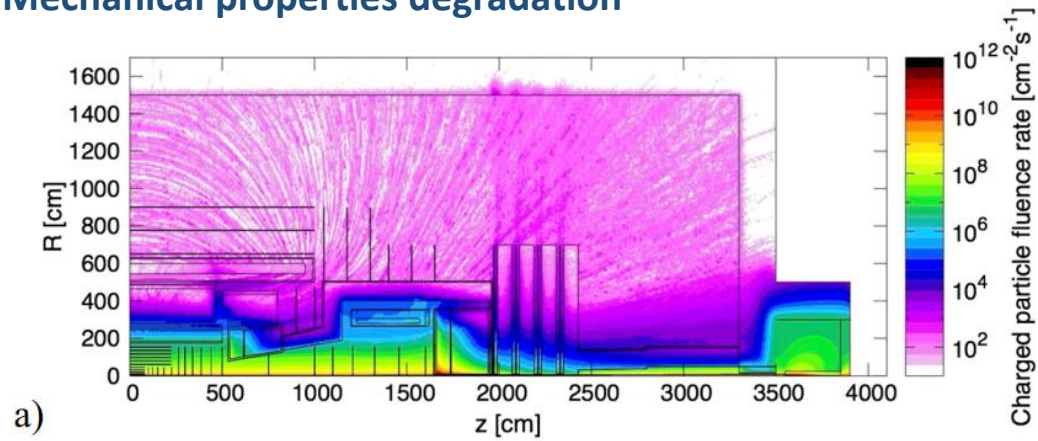
→ The CFRP cryostat for FCC^{hh} ECAL must be resistant to radiation in long term application ($30ab^{-1}$ of integrated luminosity)

Radiation loads for Future Circular Collider

Radiation types:

- EM waves
- Particle Radiation (by charged and neutral particles) → Displacement damage: changes structures of atoms → Resin becomes brittle → Mechanical properties degradation

FLUKA simulations



Long term damage:
1MeV neutrons
(fast neutrons)

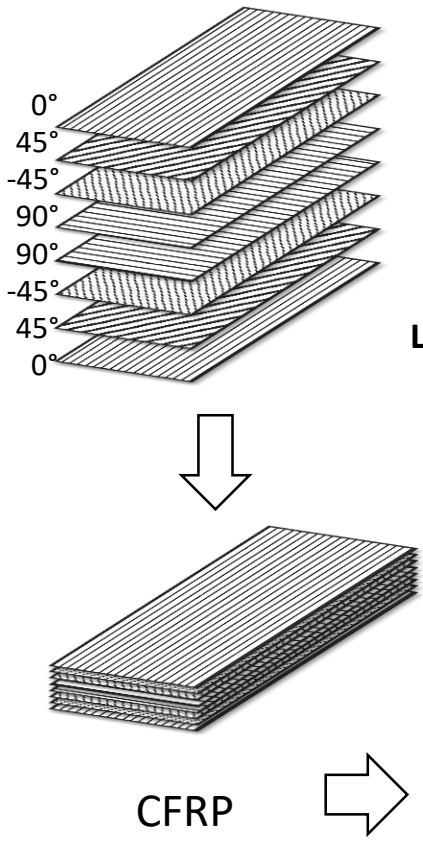
Validate material to be resistant to:

- 10e6 charged particles/ cm^2s
- 4×10^{15} neutrons/ cm^2 for 30ab-1 (~30 years)
- 10^4 photons/ cm^2s

10e-1 MGy total dose

→ Total ionizing dose for 30ab-1 of integrated luminosity expected in ECAL is 0.1 MGy (max. amount of rad over its lifetime)

Stacking of plies into a composite laminate with different angles of fibre reinforcement



Intermediate Modulus (IM-CFRP)

Carbon fiber:

IM10, $E1=310\text{GPa}$

Lamina:

Carbon Unidirectional Prepreg
IM10/8552 60% Vf

$E1=190\text{GPa}$, Thickness=0,1mm

0° Tensile strength = 3310MPa

0° Compression strength = 1793MPa

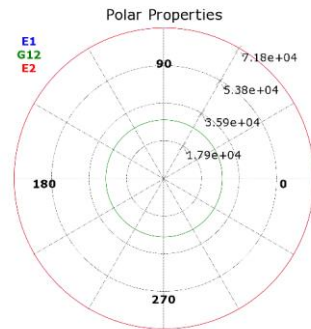
In-plane shear strength = 128MPa

Laminate:

Quasi-isotropic stack-up = [0,45,-45,90]s

Laminate stiffness $E1=E2=71.8\text{GPa}$

Laminate shear stiffness $G12=27.8\text{GPa}$



High Modulus (HM-CFRP)

Carbon fiber:

M60J, $E1=588\text{GPa}$

Lamina:

Carbon Unidirectional Prepreg
M60J/EX-1515 60% Vf

$E1=360\text{GPa}$, Thickness=0,1mm

0° Tensile strength = 2010MPa

0° Compression strength = 790MPa

90° Tensile strength = 34MPa

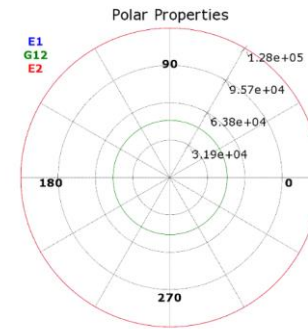
In-plane shear strength = 55MPa

Laminate:

Quasi-isotropic stack-up = [0,45,-45,90]s

Laminate stiffness $E1=E2=128\text{GPa}$

Laminate shear stiffness $G12=49\text{GPa}$



Ultra High Modulus (UHM-CFRP)

Carbon fiber:

YS-95A, $E1=920\text{GPa}$

Lamina:

Carbon Unidirectional Prepreg
YS-95A/EX-1515 60% Vf

$E1=540\text{GPa}$, Thickness=0,1mm

0° Tensile strength = 1900MPa

0° Compression strength = 340MPa

90° Tensile strength = 25MPa

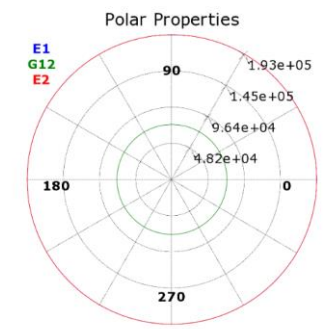
In-plane shear strength = 50MPa

Laminate:

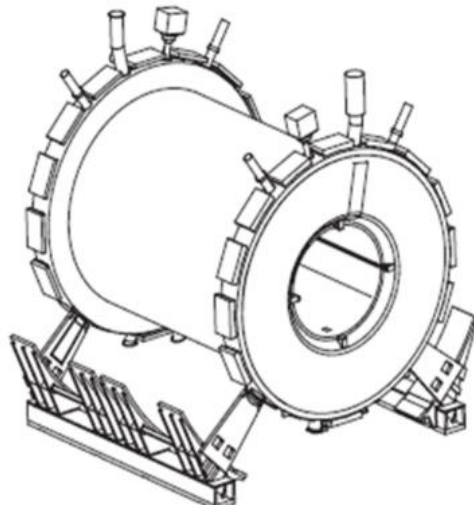
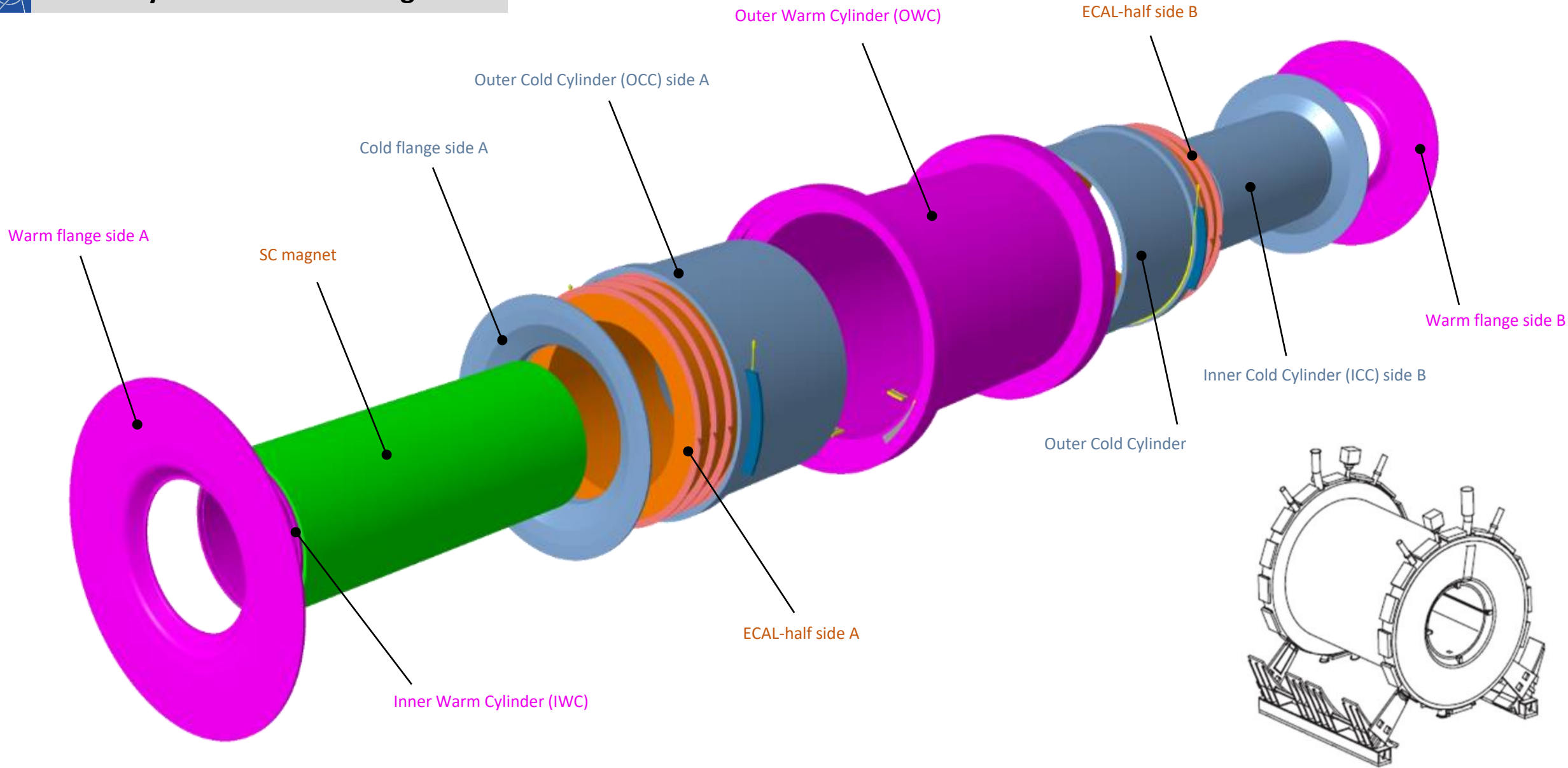
Quasi-isotropic stack-up = [0,45,-45,90]s

Laminate stiffness $E1=E2=193\text{GPa}$

Laminate shear stiffness $G12=73\text{GPa}$



→ Preliminary analysis showed the use of CFRP can improve metallic design for both, solid plate and sandwich structures

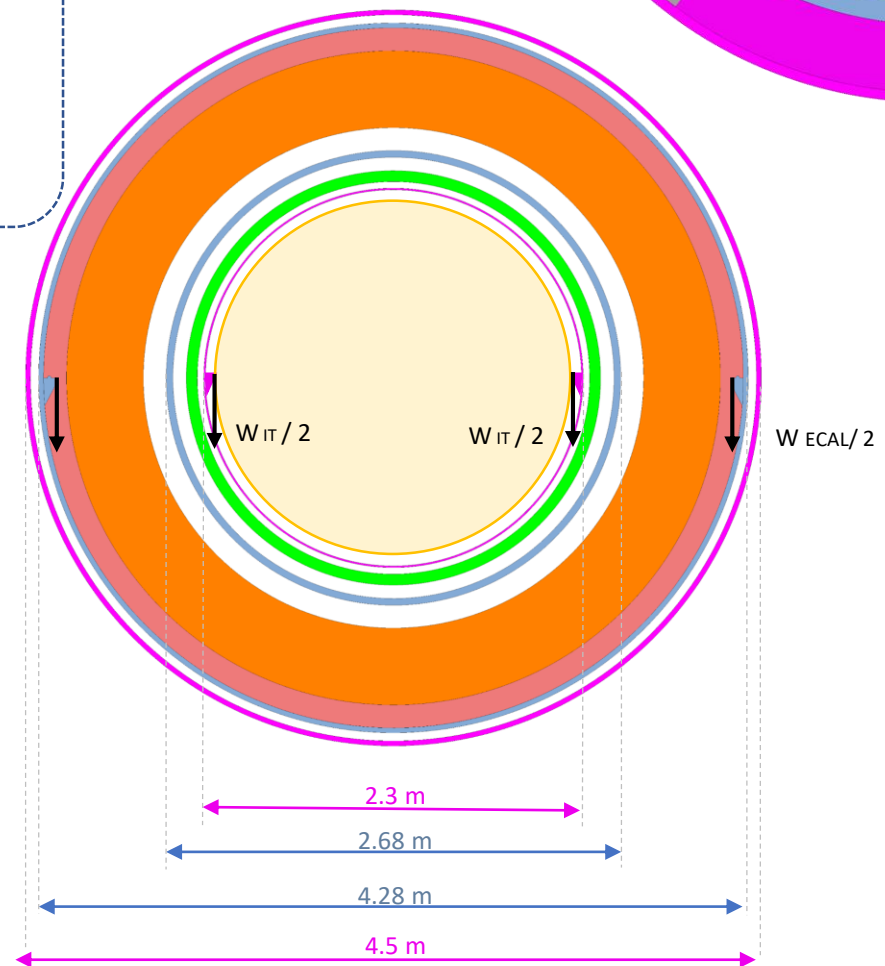
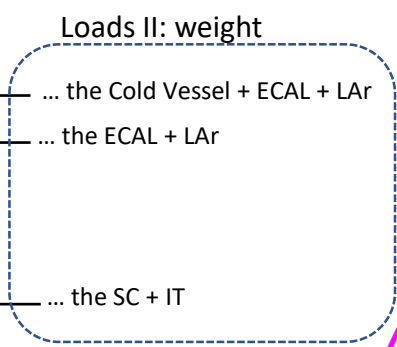
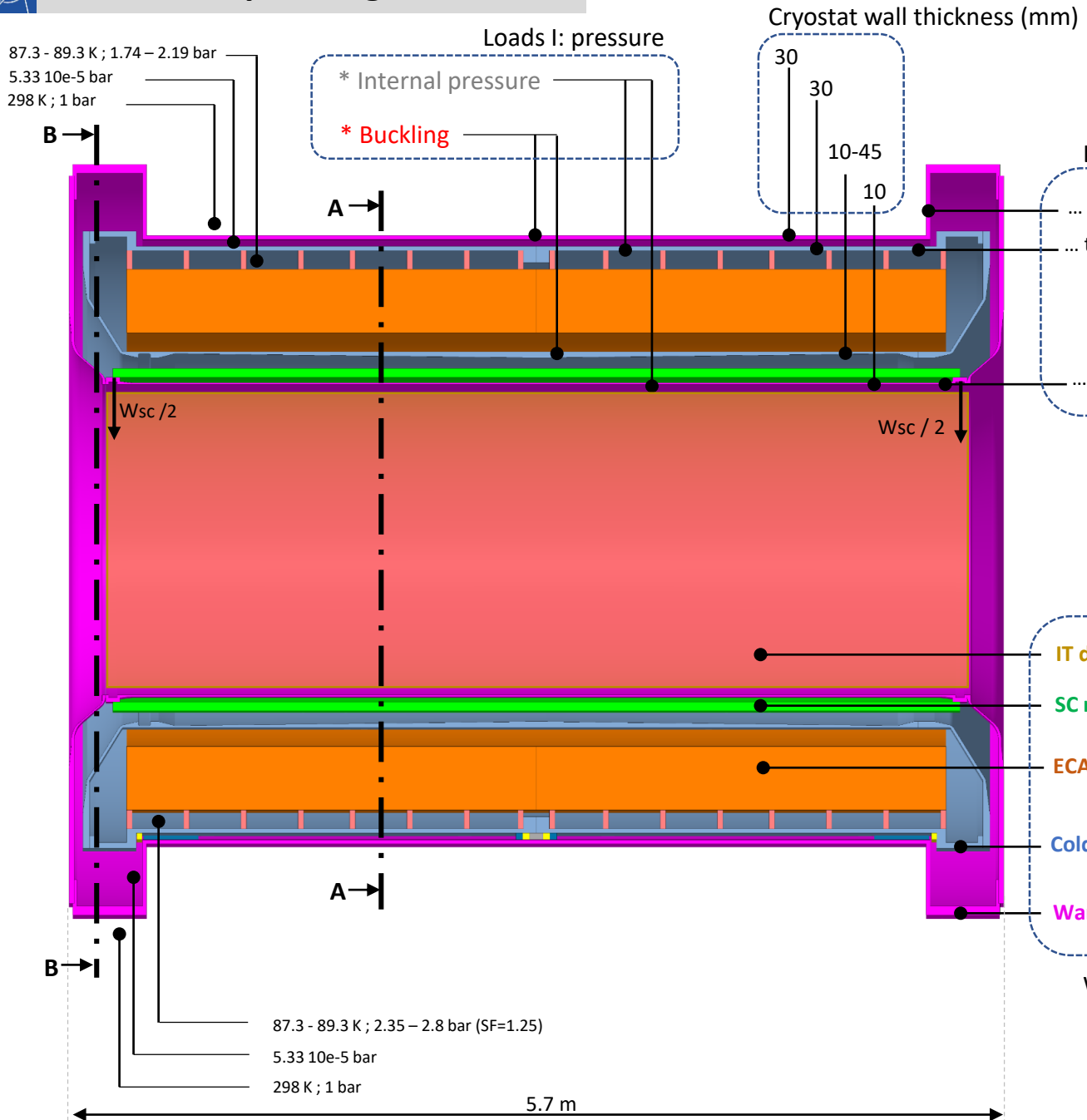


ATLAS barrel-cryostat
toroidal Al 5083 double wall

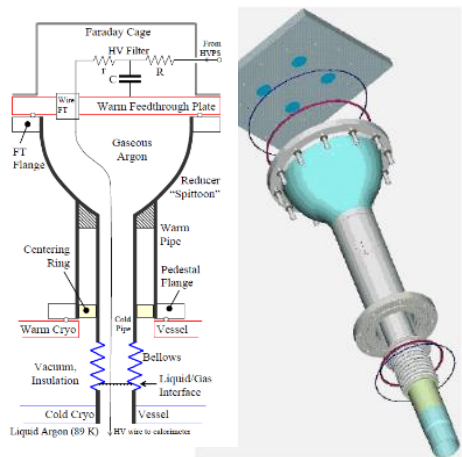


Loads and operating conditions

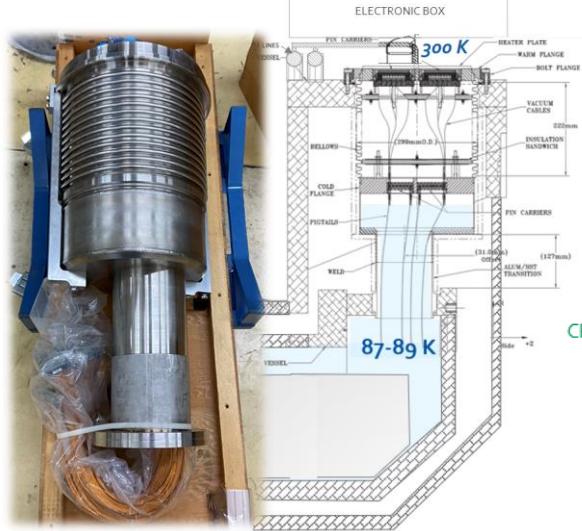
ATLAS barrel-cryostat toroidal Al 5083 double wall



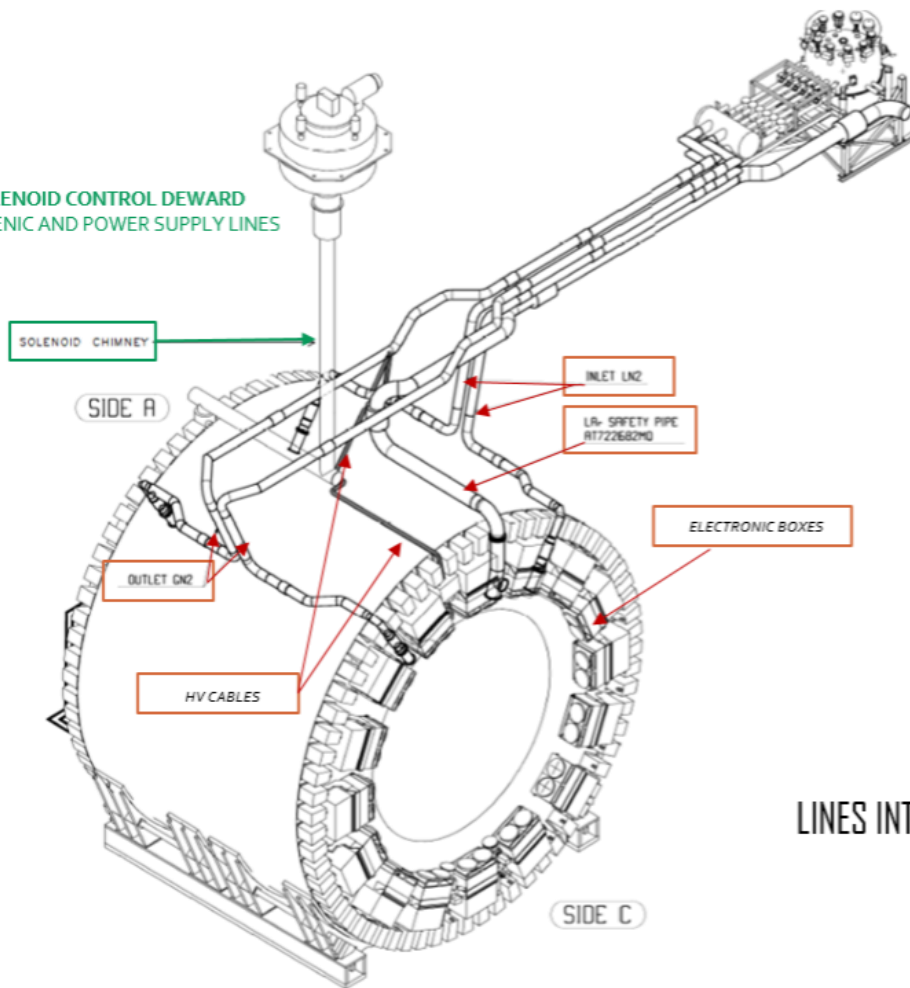
2 HV FEEDTHROUGHS



64 SIGNAL FEEDTHROUGHS



SOLENOID CONTROL DEWARD
CRYOGENIC AND POWER SUPPLY LINES



EM CALORIMETER CRYOSERVICE LINES
COOLING LOOP:
INLET LN₂ LINE-HEATEXCHANGER-OUTLETGN₂

EM CALORIMETER CRYOGENIC LINE
LAr safety line

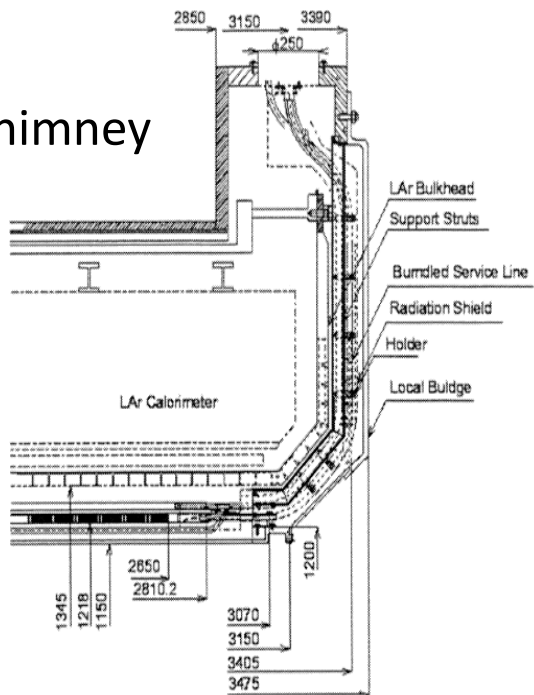
EM CALORIMETER HV LINES

2 HV Fe

EM CALORIMETER SIGNAL AND CALIBRATION LINES

64 signa

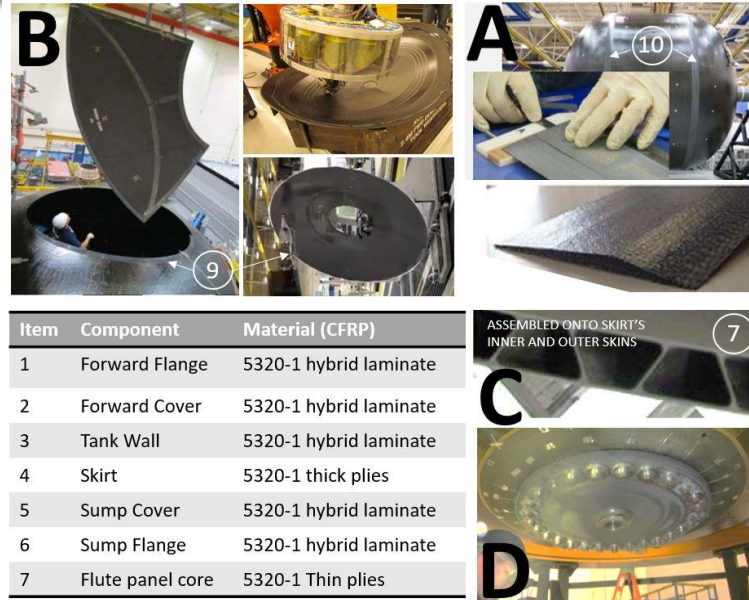
Solenoid chimney



LINES INTEGRATION INTO THE ATLAS CRYOSTAT

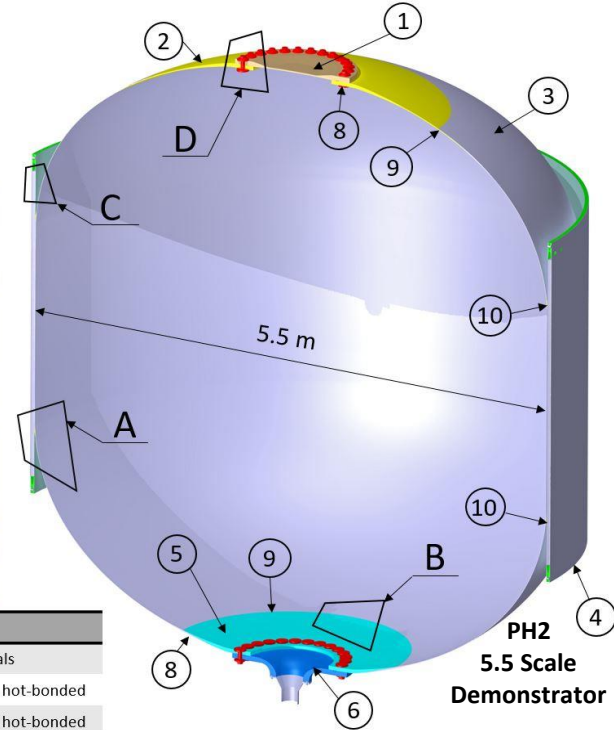
NASA's CCTD – State of the art of CFRP cryotanks

Part	Feature	2.4m in diameter Precursor Tank	5.5m in diameter Scale Demonstrator
Tank Wall	Construction	Monocoque wall with nominal thickness to withstand pressure load	Monocoque wall with nominal thickness to withstand pressure load
		*Pressure scaled up to achieve same stresses in tank joint than Scale Demonstrator	*Design Pressures 3 bars
	*Fiber Placement	Robotic Automated Fiber Placement (RAFP)	Robotic Automated Fiber Placement (RAFP)
	*Curing	Out-of-Autoclave processing (low pressure)	Out-of-Autoclave processing (low pressure)
	Layup	Hybrid laminate with centred 6 thin plies	Hybrid laminate with centred 6 thin plies
	Material	IM7/5321-1, 70 gsm and 145 gsm RAFP slit-tape tow (STT)	IM7/5321-1, 70 gsm and 145 gsm RAFP slit-tape tow (STT)
	Tooling	Multipiece C/E mandrel (24 segments), RAFP cell, Oven	Multipiece C/E mandrel (20 segments), RAFP cell, Oven
Skirt	SHM	Acoustic Emission sensor-based system	Acoustic Emission sensor-based system (20 sensors required)
	SE Y-Joint	Baseline hot-bonded softening strip	Optimized hot-bonded softening strip
	SE Scarf Joints	Scarf shape included in multipiece mandrel	Scarf shape included in multipiece mandrel
	NDI	Trough-Transmission Ultrasonic (TTU) and Pulse Echo (PE)	Trough-Transmission Ultrasonic (TTU), Pulse Echo (PE) and Flash thermography
	Construction	Monocoque thick skirt	Fluted core (Inner skin + flute panels + outer skin)
	*Fiber Placement	Robotic Automated Fiber Placement (RAFP)	Robotic Automated Fiber Placement (RAFP)
	*Curing	Out-of-Autoclave processing (low pressure)	Out-of-Autoclave processing (low pressure)
Forward Cover	Layup	Thick ply laminate	Inner skin thick ply laminate + flute panel laminate + Outer skin thick ply laminate
	Material	IM7/5321-1, 145 gsm RAFP slit-tape tow	Skins: IM7/5321-1, 145 gsm RAFP slit-tape tow Flute panel: C/E fabric (facesheets) and thin tapes (angled web members)
	Tooling	Skirt Alignment Fixture, RAFP cell, Oven	Flute layup mandrel, Skirt Alignment Fixture, RAFP cell, Oven
	SE Y-Joint	Co-bonded and hot-bonded softening strip	Co-bonded and hot-bonded softening strip
	End-Joint	None, designed to ease of handling	Load-bearing design, to vent leaks and to apply flight axial loads along tests
	Construction	Monocoque dome with nominal thickness to withstand pressure load	Monocoque dome with nominal thickness to withstand pressure load
		*Pressure scaled up to achieve same stresses in tank joint than Scale Demonstrator.	*Design Pressures 3 bars.
Sump Cover	*Fiber Placement	Single-headed Robotic Automated Fiber Placement (RAFP)	Single-headed Robotic Automated Fiber Placement (RAFP)
	*Curing	Autoclave processing (0.57 Mpa with 94.8kPa vacuum)	Autoclave processing (0.57 Mpa with 94.8 kPa vacuum)
	Layup	Hybrid laminate with centred 6 thin plies	Hybrid laminate with centred 6 thin plies
	Material	IM7/5321-1, 70 gsm and 145 gsm RAFP slit-tape tow (STT)	IM7/5321-1, 70 gsm and 145 gsm RAFP slit-tape tow (STT)
	Tooling	Forward cover mold, RAFP cell, Autoclave	Forward cover mold, RAFP cell, Autoclave
	SE Scarf Joint	Co-bonded and hot-bonded (scarf shape included in cover mould)	Co-bonded and hot-bonded (scarf shape included in cover mould)
	Construction	Monocoque dome with nominal thickness to withstand pressure load	Monocoque dome with nominal thickness to withstand pressure load
	*Pressure scaled up to achieve same stresses in tank joint than Scale Demonstrator.	*Design Pressures 3 bars.	
Forward Flange	*Fiber Placement	Single-headed Robotic Automated Fiber Placement (RAFP)	Single-headed Robotic Automated Fiber Placement (RAFP)
	*Curing	Autoclave processing (low pressure)	Autoclave processing (low pressure)
	Layup	Hybrid laminate with centred 6 thin plies	Hybrid laminate with centred 6 thin plies
	Material	IM7/5321-1, 70 gsm and 145 gsm hand-lay up layers or STT??	IM7/5321-1, 70 gsm and 145 gsm hand layup layers
	Tooling	Close-out mold, ancillary cure tools and stands (Al and steel), Autoclave	Flange mould, ancillary cure tools and stands (Al and steel), Autoclave
	Joint	co-bonded and hot-bonded scarf joint	Bolted joint (torque limited bolts, Belleville washers and Furon seals)
	Sump Flange	Construction	Carbon Composite thin close-out
*Fiber Placement		Hand layup	Hand layup
*Curing		Autoclave processing (0.57 Mpa with 94.8kPa vacuum)	Autoclave processing (0.57 Mpa with 94.8kPa vacuum)
Layup		Hybrid laminate with centred 6 thin plies	Hybrid laminate with centred 6 thin plies
Material		IM7/5321-1, 70 gsm and 145 gsm hand-lay up pre-preg layers	IM7/5321-1, 70 gsm and 145 gsm hand layup pre-preg layers
Tooling		Autoclave	Autoclave
Joint		Bolted joint (torque limited bolts, Belleville washers and Furon seals)	Bolted joint (torque limited bolts, Belleville washers and Furon seals)



Item	Component	Material (CFRP)
1	Forward Flange	5320-1 hybrid laminate
2	Forward Cover	5320-1 hybrid laminate
3	Tank Wall	5320-1 hybrid laminate
4	Skirt	5320-1 thick plies
5	Sump Cover	5320-1 hybrid laminate
6	Sump Flange	5320-1 hybrid laminate
7	Flute panel core	5320-1 Thin plies

Item	Joint	Material	Components	Note
8	Torque limited bolts	Metal ?	Flanges-Covers	Belleville washers and Furon seals
9	Scarf Joint	C/E	Covers-Tank wall	Structurally efficient co-bonded hot-bonded
10	Y-Joint (softening strip)	E/E	Skirt-Tank wall	Structurally efficient co-bonded hot-bonded



Equivalency Tests (PH1)	Out-of-Autoclave			Autoclave		
	ATK	Boeing	Lockheed Martin	Northrop Grumman		
	IM7/M56 145hlu, 70hlu	IM7/5320-1 145hlu, 70hlu	IM7/5320-1 145fp, 70fp	IM7/M56 145fp, 70hlu	IM7/ MTM45-1 145fp, 70hlu	IM7/TC250 145fp, 70hlu
						IM7/BXA 145fp
						IM10/8552-1 70fp
						IM7/BXA 70hlu
						IM7/8552-1 145hlu

Ply thickness: 145= 145gsm FAW ; 70= 70gsm FAW / Manufacturing technique: hlu= hand layup ; fp= fiber placed

→ NASA CCTD 5.5m in diameter demonstrator is the most advanced cryotank in literature reviewed (Successfully tested)