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E-CLOUD Build-up in Grooved Chambers

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Outline of work



- Augment existing version of POSINST to model e-cloud build-up in the presence of grooved walls
 - Electron orbits are properly followed and collisions located on the groove surface where they occur but ...
 - ... when solving the Poisson equation for the electron self-field the boundaries are those of the smooth chamber (field enhancement at the groove edges not accounted)
- - Rectangular chamber cross section
 - Grooves are placed on top and bottom of wall
 - (Isosceles) triangular grooves with option to account for rounded tips
- ► Motivations:
 - Characterization of e-cloud dynamics more from 'first principles' instead of passing through an intermediate calculation of an 'effective' secondary yield for the grooved wall.
 - Validate previous calculations by M.Pivi, G. Stupakov, and L.Wang.
 - Help settle some alleged disagreement with other calculations
 - Provide modeling tools for ongoing and future measurements

Calculations done so far:



Parameter choice specific for the ILC-DR dipoles.
 Input deck for POSINST provided by M.Pivi with setting used for previous smooth-chamber DR simulations

- - -Groove angle and height
 - -Radius of the rounded groove tips
 - -Magnitude of magnetic field
- Contact with previous calculations by extracting and effective SEY (by comparison with e-cloud build-up curves for smooth chambers)

ILC DR basic parameters used in simulations



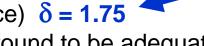
Beam/dipole parameters:

Dipole magnetic field	0.194 T
Beam sizes in bends	σ _x =0.62 mm, σ _y =8μm, σ _z =6mm
Particle/bunch	N=2*10 ¹⁰

Bunch-train structure parameters:

RF bucket spacing	1.52 ns (=0.46m) [f _{RF} =650 MHz, C=6.11Km]
Bunch spacing	6.1 ns (one every four RF buckets)
No. bunches/train	111
Train length	0.68 μs (=204m)

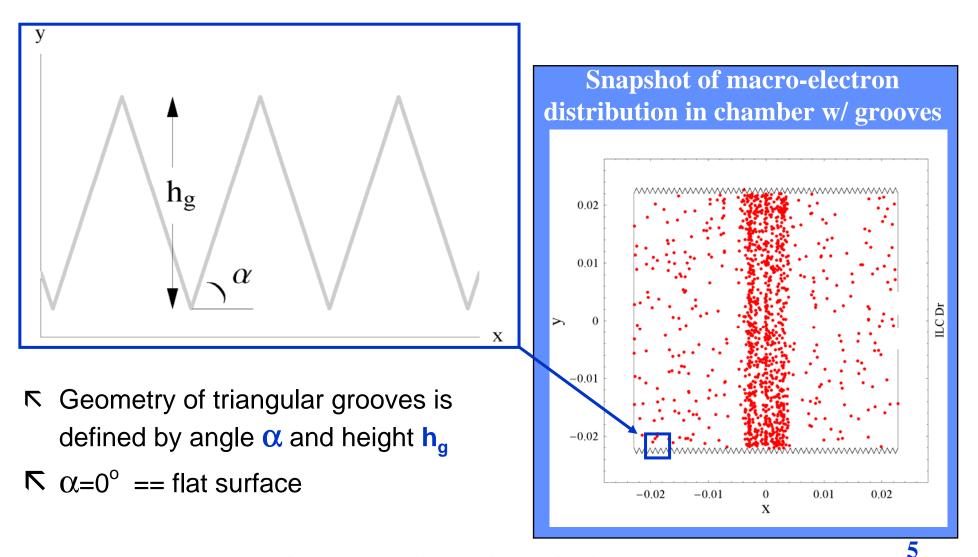
- K Chamber sizes: 2.3*2.3 cm (rectangular)
- $rac{1.75}{5}$ Max SEY (for smooth surface) δ = 1.75



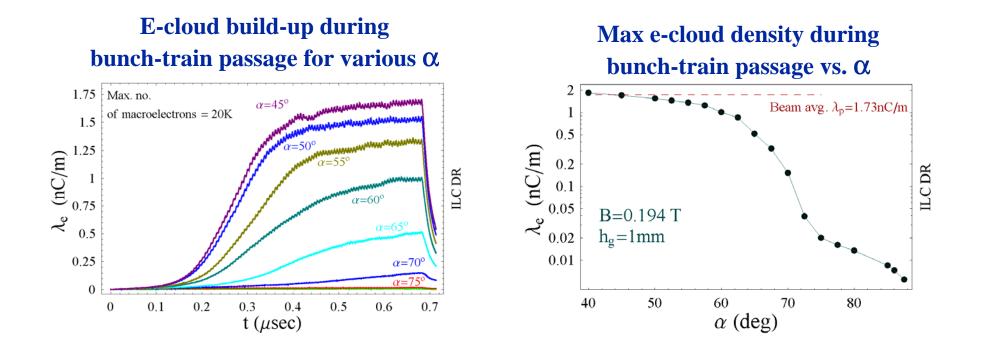
Max. no. of macro-e = 20K found to be adequate (i.e. get small noise in longitudinal e-density)

Geometry of triangular grooves





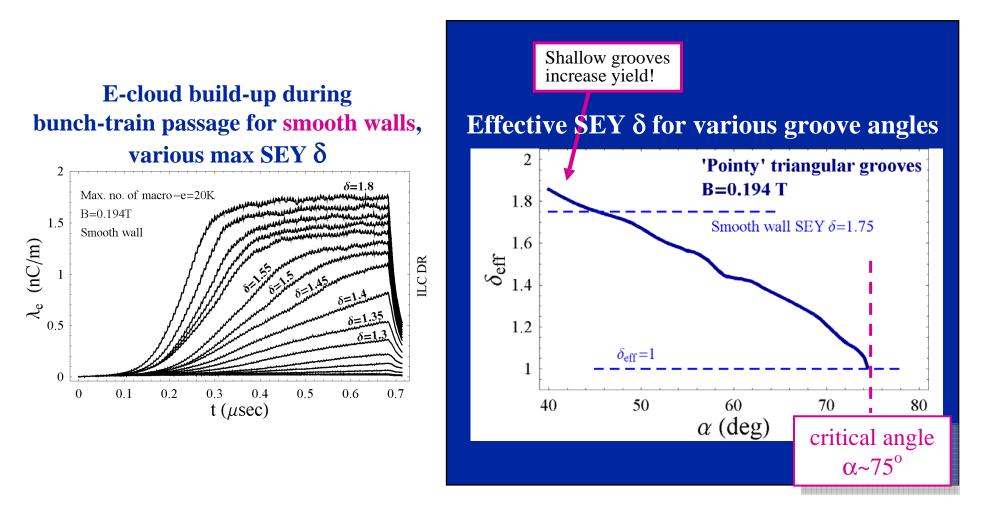




 $rac{}$ E-cloud density suppressed by a factor ~200 for groove angles α >75°

Extract an effective SEY from comparison with data from smooth chamber

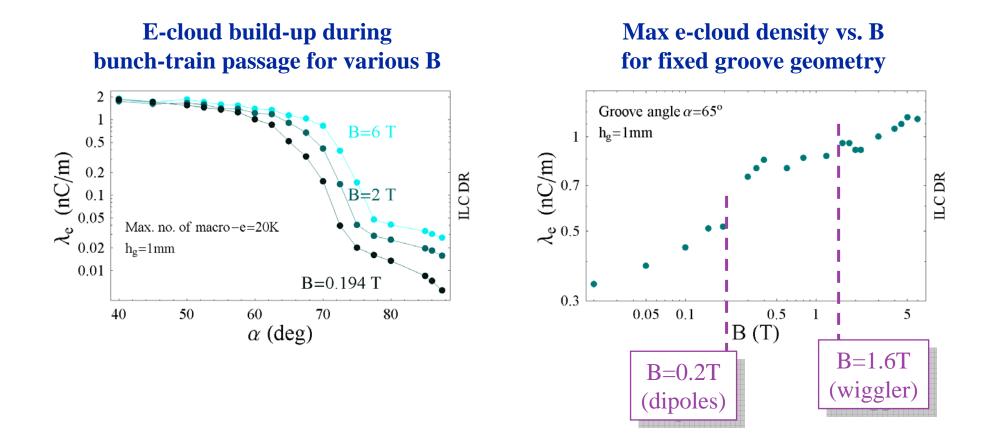




The effective SEY for surface with groove angle α is defined as the SEY of a smooth chamber that results in the same max of e-cloud accumulation

A higher B-field degrades e-cloud suppression

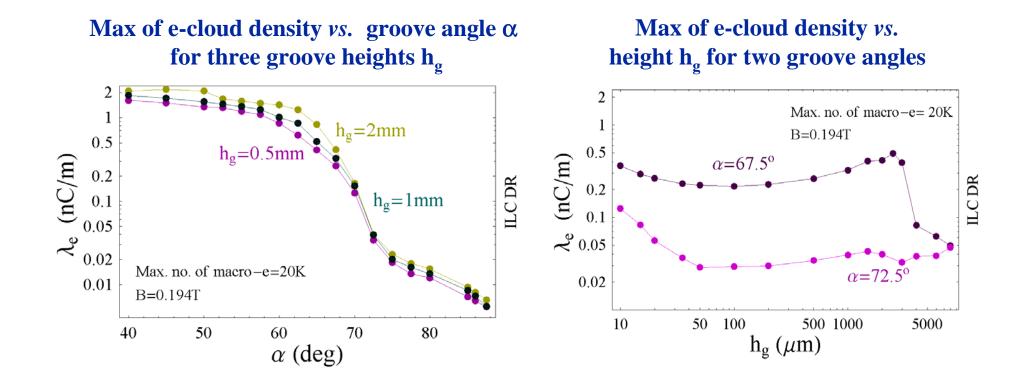




A larger cyclotron radius (smaller B-field) enhances chance that secondary electrons may be promptly reabsorbed in wall collision

Dependence on groove height



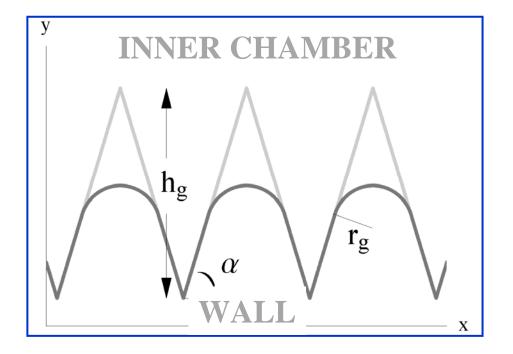


▷ Dependence appears to be generally mild over a large span of height variations

Triangular grooves with smooth tips



Smoothing groove tips may be desirable to ease impedance, manufacturing

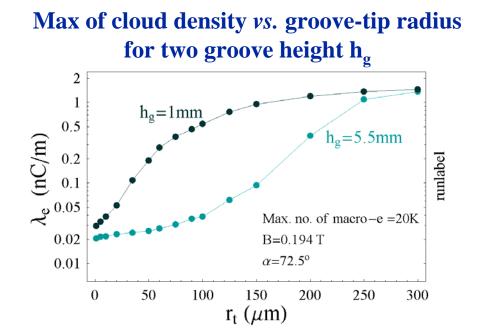


In present model only the groove edges on the chamber inner side are smoothened

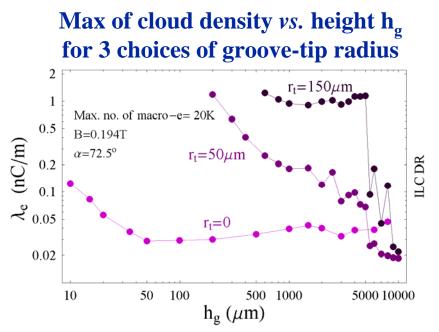
 $\Bar{\}$ Geometry of triangular grooves is defined by angle α , height h_g , and tip radius r_g

Smoother tips spoil effectiveness of grooves





Spoiling effect of smooth groove-tips can be compensated by making the grooves deeper.



Finite groove-tip radius enhances dependence of groove effectiveness on groove height





- Isosceles triangular grooves with steepness angle α >75[°]
 reduce effective SEY to < 1
 </p>
 - E-cloud build up for a 111 bunch train is reduced by a factor 200.
- Results seem about consistent with previous calculations by L.Wang (α ~70° for effective SEY < 1, SLAC-PUB-12001)</p>
- A larger magnetic field makes the grooving less effective.
 In wigglers the groove angle likely to have to be steeper to provide same e-cloud suppression effect as in dipoles
- Rounding of the tips spoils e-cloud suppression, which can be compensated by deepening the grooves