

# *How e-cloud effect affects the ILC DR Vacuum System*

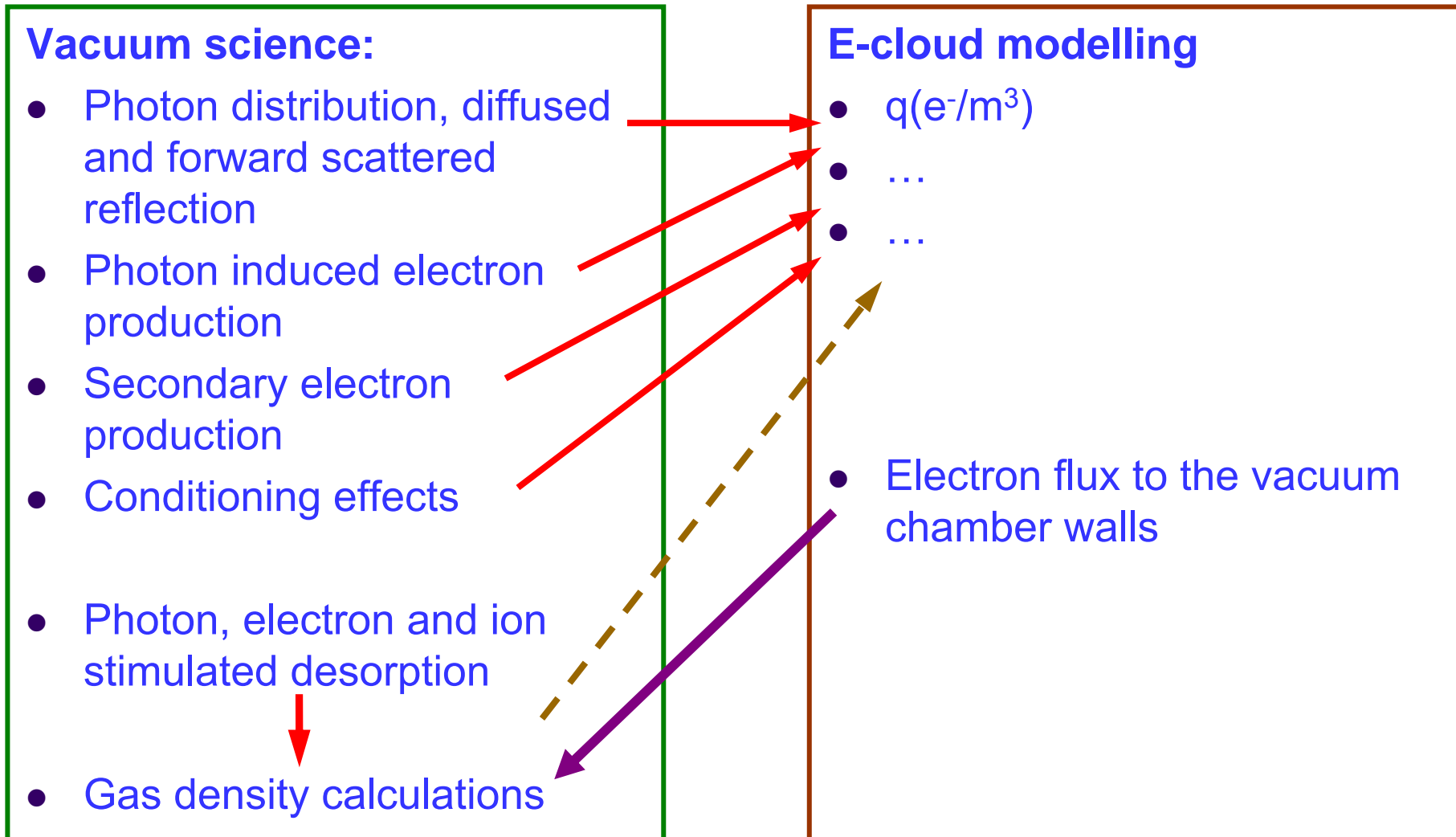
Dr. Oleg B. Malyshev

ASTeC

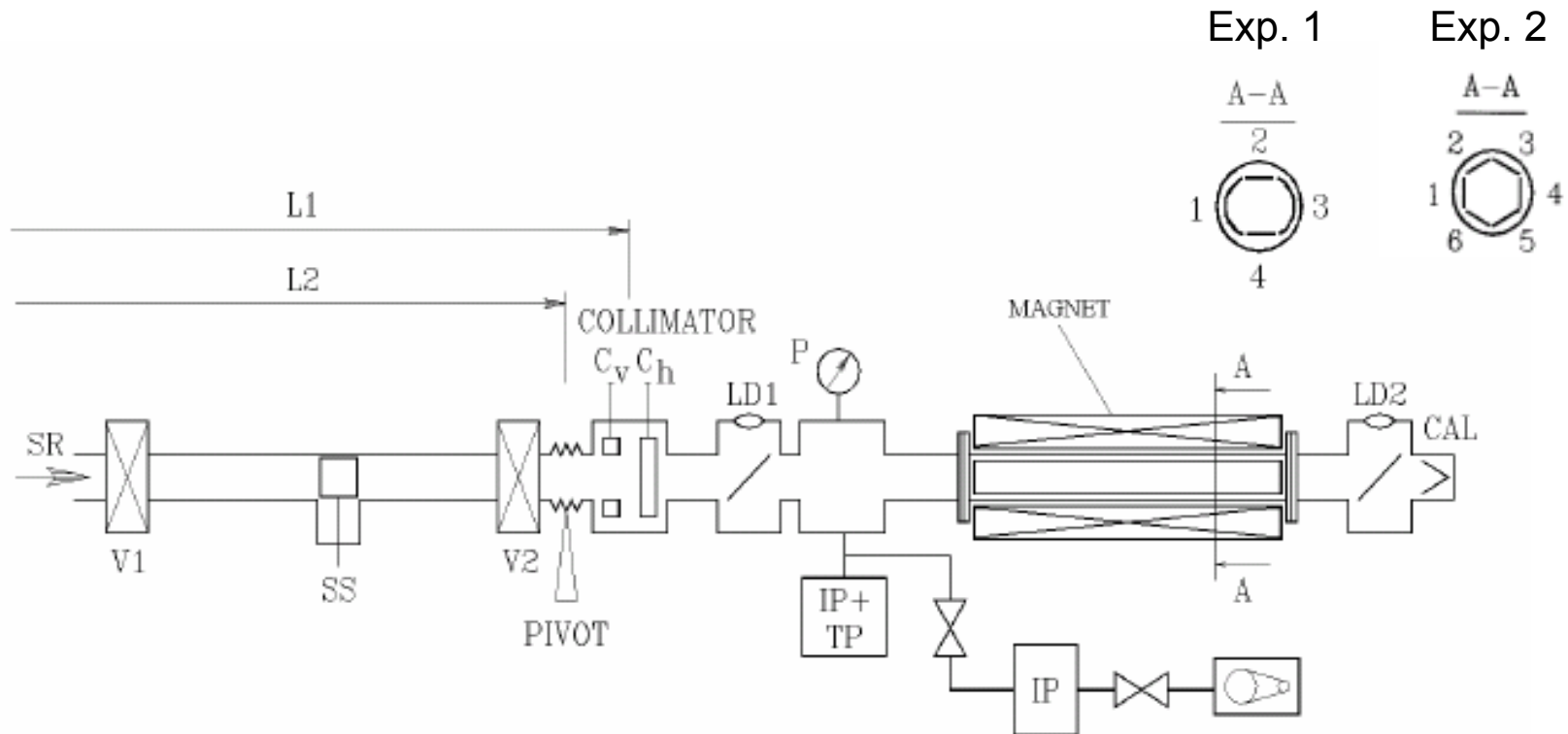
Daresbury Laboratory



## Vacuum studies vs e-cloud modelling



# Photon reflectivity and azimuthal distribution



**Figure 1. Set-up for measurements of the azimuthal photoelectron distribution in magnetic field and of the photon reflectivity**

## Forward scattered reflectivity at 20 mrad grazing incidence

	Sample Reflectivity (power) (%)	Reflectivity (photons) (%)
Stainless steel as-received	<b>2</b>	<b>22</b>
Cu co-laminated as-received	<b>50</b>	<b>95</b>
Cu co-laminated oxidised	<b>20</b>	<b>65</b>

**I.e. the reflected photons are mainly low energy photons**

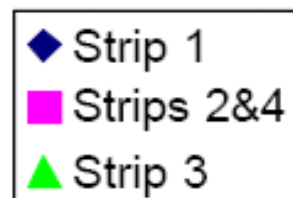
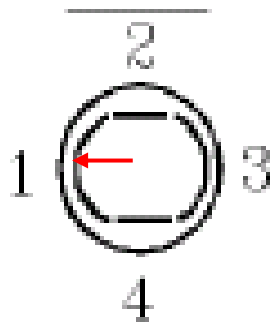
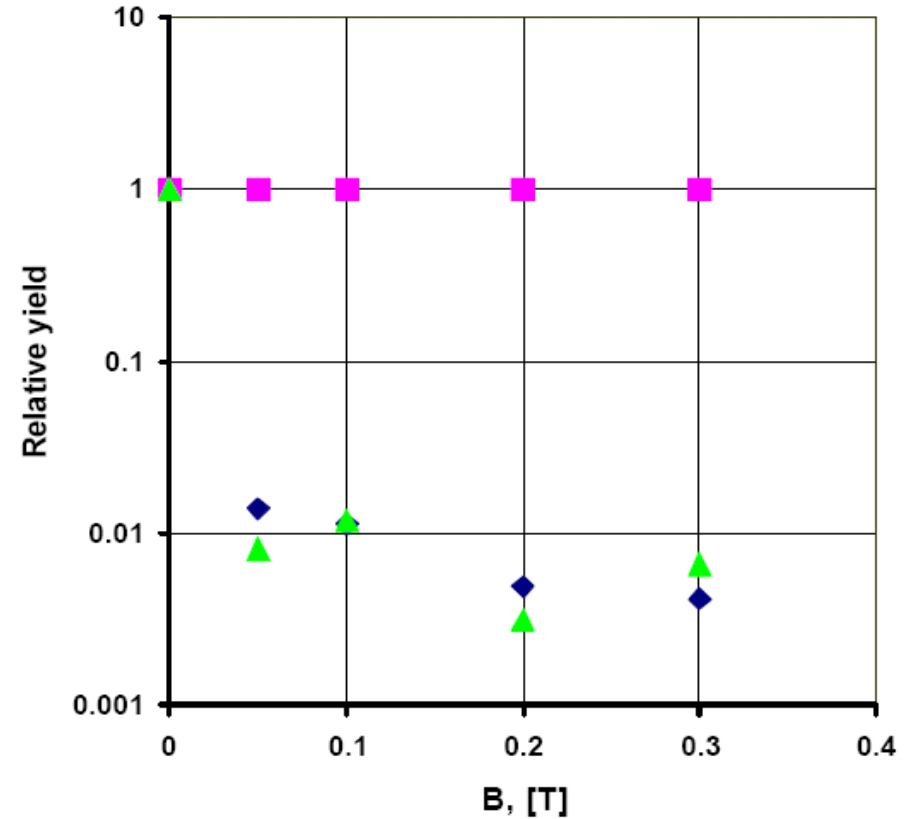
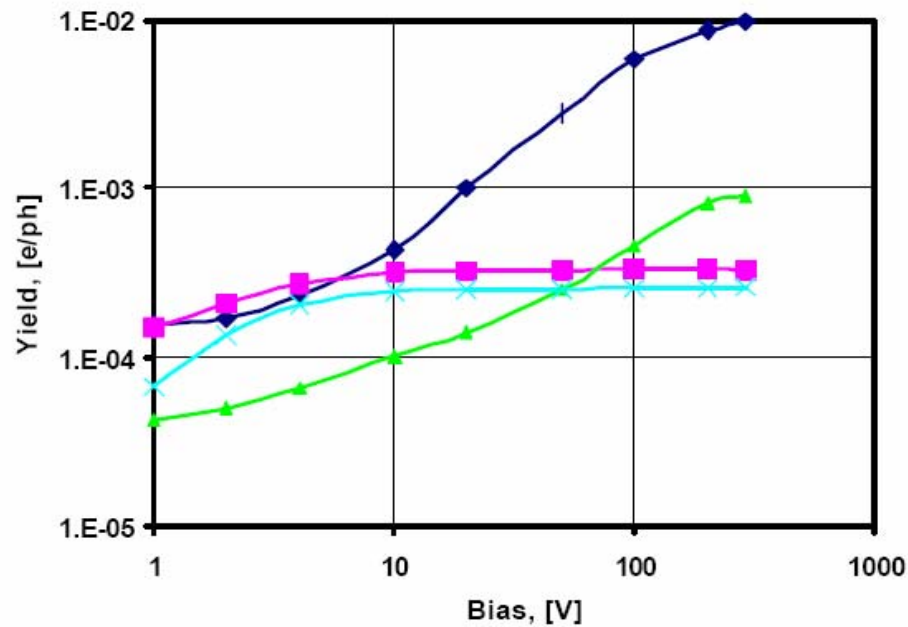
*V.V. Anashin et al. / Nuclear Instruments and Methods in Physics Research A 448 (2000) 76-80.*

*See also: V. Baglin, I.R. Collins, O. Grobner, EPAC'98, Stockholm, June 1998.*

## Photon azimuthal distribution – 6 strips experiment

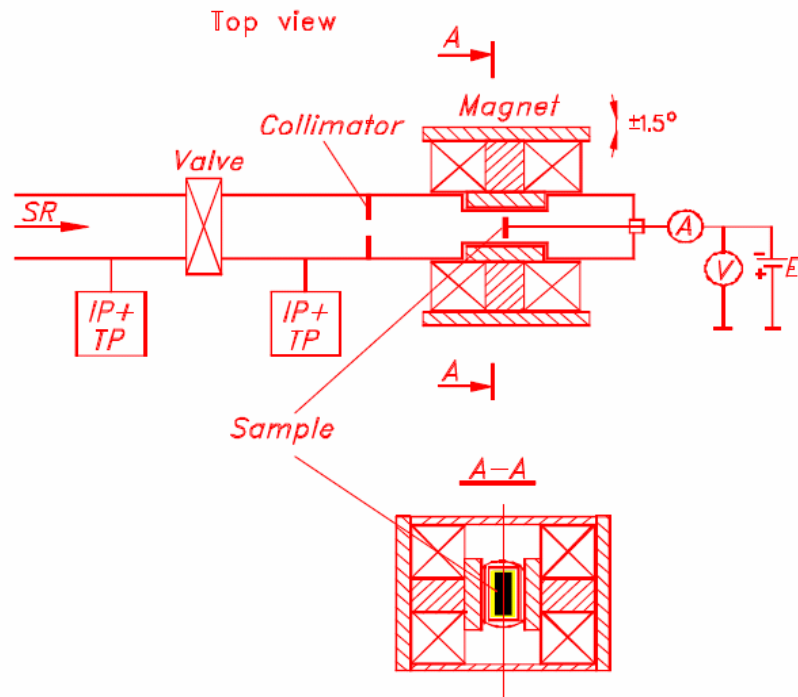
Sample	$\varepsilon_c$ (eV)	Strip 1	Strip 2 or Strip 3	Strip 4 or Strip 5	Strip 6
$I_i / \sum_{i=1}^6 I_i$					
Stainless steel	<b>243</b>	<b>74</b>	<b>3.8</b>	<b>8</b>	<b>2.5</b>
Bright Cu	<b>245</b>	<b>90</b>	<b>1.9</b>	<b>2</b>	<b>1.8</b>
Oxidised Cu	<b>205</b>	<b>95</b>	<b>1</b>	<b>1.1</b>	<b>1</b>
$I_i(1-R) / \sum_{i=1}^6 I_i$					
Stainless steel	<b>243</b>	<b>60</b>	<b>2.5</b>	<b>6.0</b>	<b>1.5</b>
Bright Cu	<b>245</b>	<b>4.5</b>	<b>0.1</b>	<b>0.1</b>	<b>0.1</b>
Oxidised Cu	<b>205</b>	<b>30</b>	<b>0.3</b>	<b>0.4</b>	<b>0.3</b>

# Photon azimuthal distribution – 4 strips experiment



V.V. Anashin, O.B. Malyshev, N.V. Fedorov and A.A. Krasnov.  
 Azimuthal distribution of photoelectrons for an LHC beam screen prototype in a magnetic field. Vacuum Technical Note 99-06. LHC-VAC, CERN April 1999.

# Photoelectron current in magnetic field



V.V. Anashin, O.B. Malyshev, N.V. Fedorov and A.A. Krasnov. Photoelectron current in magnetic field. Vacuum Technical Note 99-03. LHC-VAC, CERN April 1999.

- Sample SS. The stainless steel sample made from a rolled sheet.
- Sample Cu/SS-1 (=). The copper laminated stainless steel made from a sheet; the rolling lines are across the sample.
- Sample Cu/SS-2 (|||). The copper laminated stainless steel made from a sheet; the rolling lines are along the sample.
- Sample Cu/SS-3 (||| ox). The copper laminated stainless steel made from a sheet; the rolling lines are along the sample. Oxidation.
- Sample Cu/SS-4 (\\_/\_). The copper laminated stainless steel made from a sheet with turned-in, long edges, i.e. 5-mm wide strips at the long edges were turned to 10–15° towards the SR; the rolling lines are along the sample.
- Sample OFHC (⊥⊥⊥). The copper sample machined from a bulk OFHC with ribs along the sample. No special treatment. The ribs are 1 mm in height and
- 0.2 mm in width. The distance between the ribs is 3 mm.
- Sample Au/SS. The stainless steel sample electro-deposited with 6- $\mu$ m Au.

## Results

1) The photoelectron yield is different for studied samples at zero potential, but the same at the accelerating potential of 300V,

$k = (1.5 \pm 0.3) \times 10^{-2} \text{ e-}/\gamma$ . The photoelectron yield from the layer of gold is about two times higher.

2) The magnetic field suppress the photoelectron yield up to **30–100 times** when the surface is parallel to the magnetic field, but this effect is much less at

the angle of  $1.5^\circ$  (5–10 times).

3) The photoelectron yield decreases with the accumulated photon dose: the photoelectron yield reduced 2–3 times at the accumulated photon dose of about

$10^{22} \text{ photons/cm}^2$ .

1-2 March, 2007

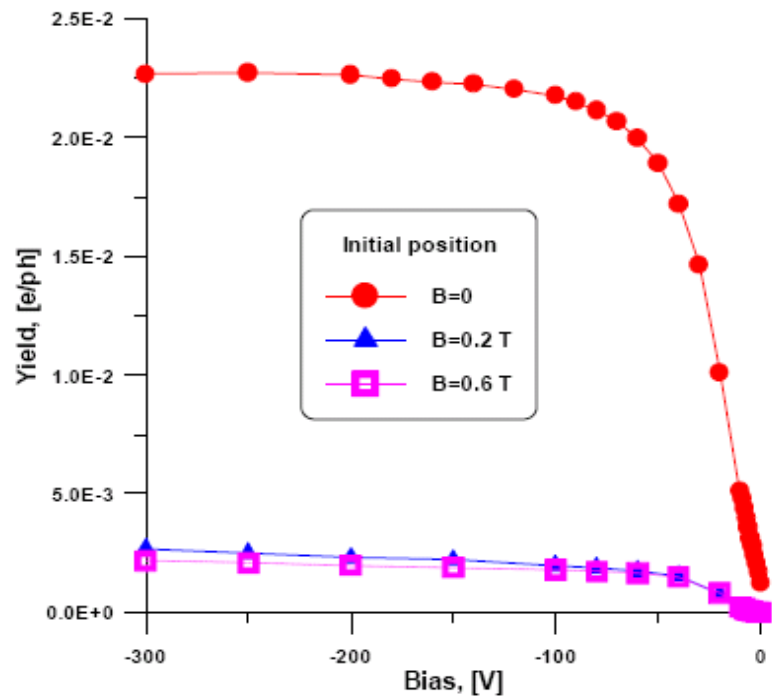
ECL-2, CERN

Experiment No. and Sample	Beams		Measurements without magnetic field			Magnetic field efficiency:	
	$E_{e^+}$ , [MeV]	$E_c$ , [eV]	$\kappa$ ; [e <sup>-</sup> /γ] U=-300V	$\frac{\kappa(0V)}{\kappa(-300V)}$	Reflectivity $\frac{\kappa(+300V)}{\kappa(-300V)}$	U = 0 $\frac{\kappa(0.6T)}{\kappa(0T)}$	U = -300V $\frac{\kappa(0.6T)}{\kappa(0T)}$
Exp. 1, SS	518	259	0.016	0.036	0.024	0.023	0.028
Exp. 2, Cu/SS-1 (≡)	514	253	0.015	0.15	0.044	0.010	0.029
Exp. 3, Cu/SS-2 (   )	470	194	0.014	0.11	0.015	0.021	0.030
Exp. 4, Cu/SS-3 (   ox)	392	112	0.014	0.052	0.033	0.018	0.015
Exp. 5, OFHC (⊥⊥⊥)	380	102	0.0084	0.055	0.023	0.024	0.013
Exp. 6, Cu/SS-4 (∧_/_)	220	20	0.014	0.07	—	0.02	0.06
Exp. 7, Cu/SS-4 (∧_/_)	560	319	0.018	0.05	0.180	0.01	0.08
Exp. 8, Au/SS	580	356	0.027	0.06	0.045	0.028	0.042



# Examples of measurement results

Exp. 1.1. Photoelectron emission from stainless steel sample in magnetic field

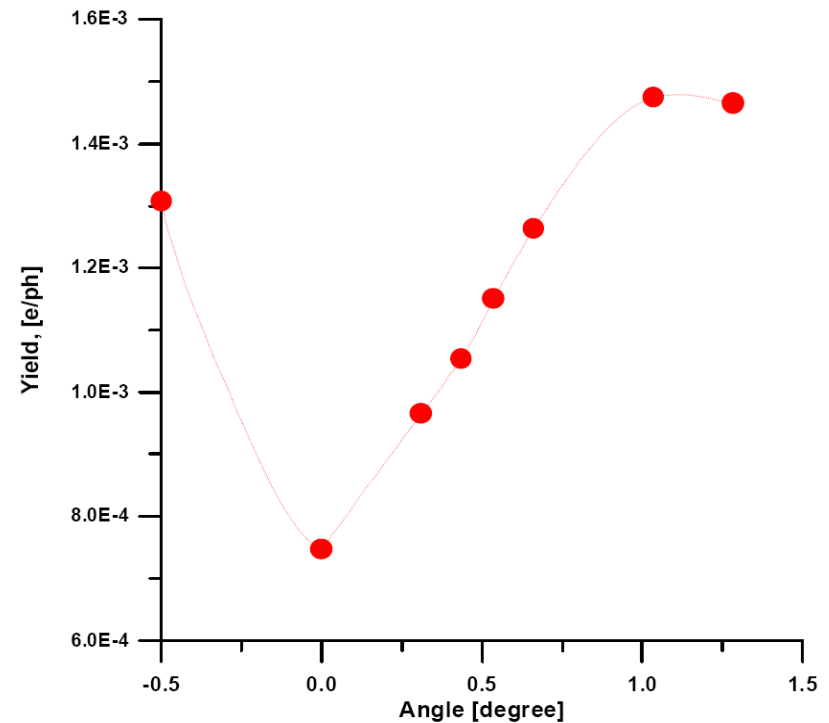


PEY (and SEY) depends on potential gradient at the surface!

1-2 March, 2007

ECL-2, CERN

Exp.2. Copper laminated stainless steel. Dependence on angle between substrate surface and magnetic field.



Grooves alignment in respect to magnetic field

O.B. Malyshev

## Input parameters in e-cloud models

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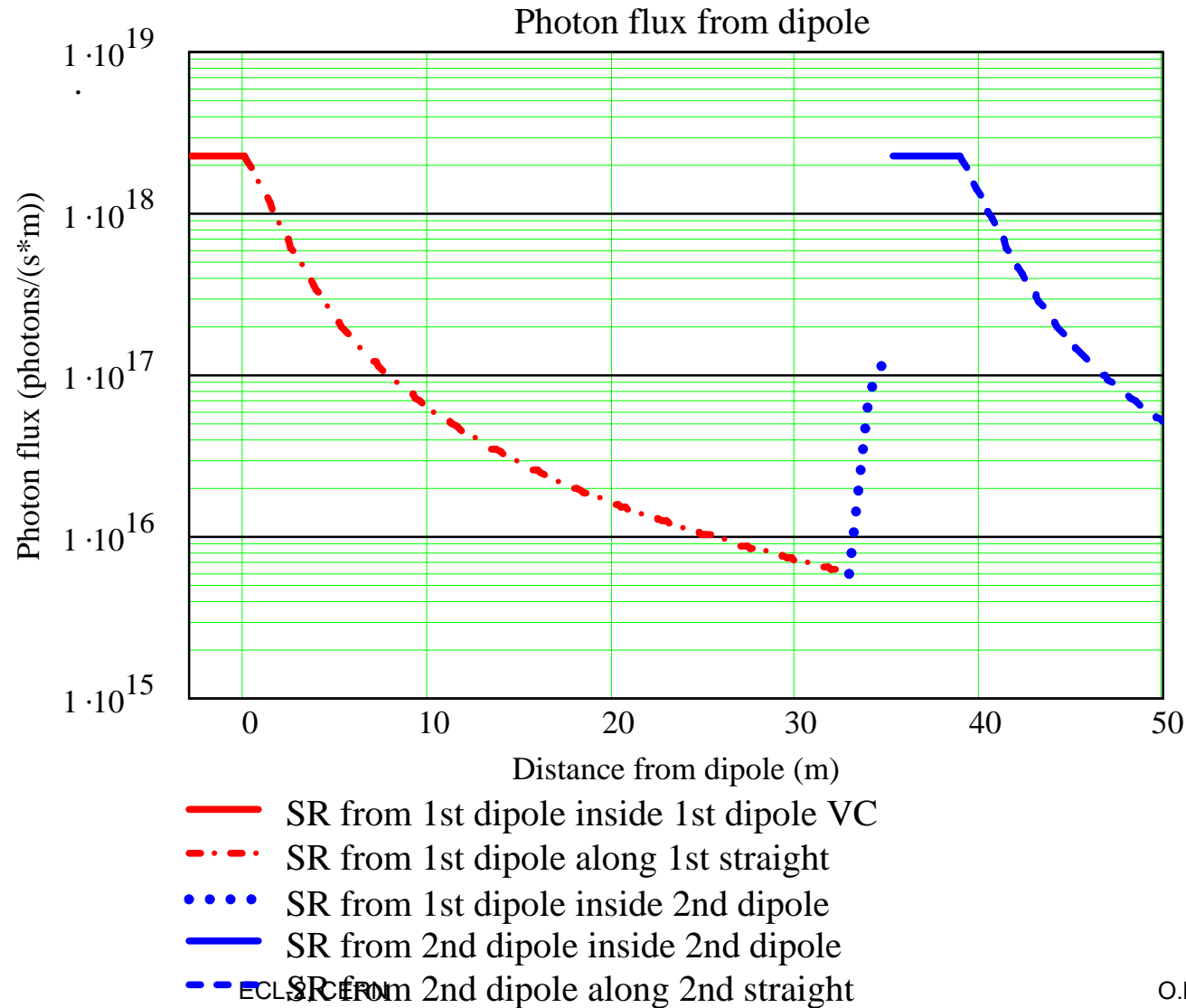
- Photon distribution, diffused and forward scattered reflection
- Photon induced electron production
- Secondary electron production
- Conditioning effects
  
- Effect of magnetic field

## Required vacuum for ILC DRs

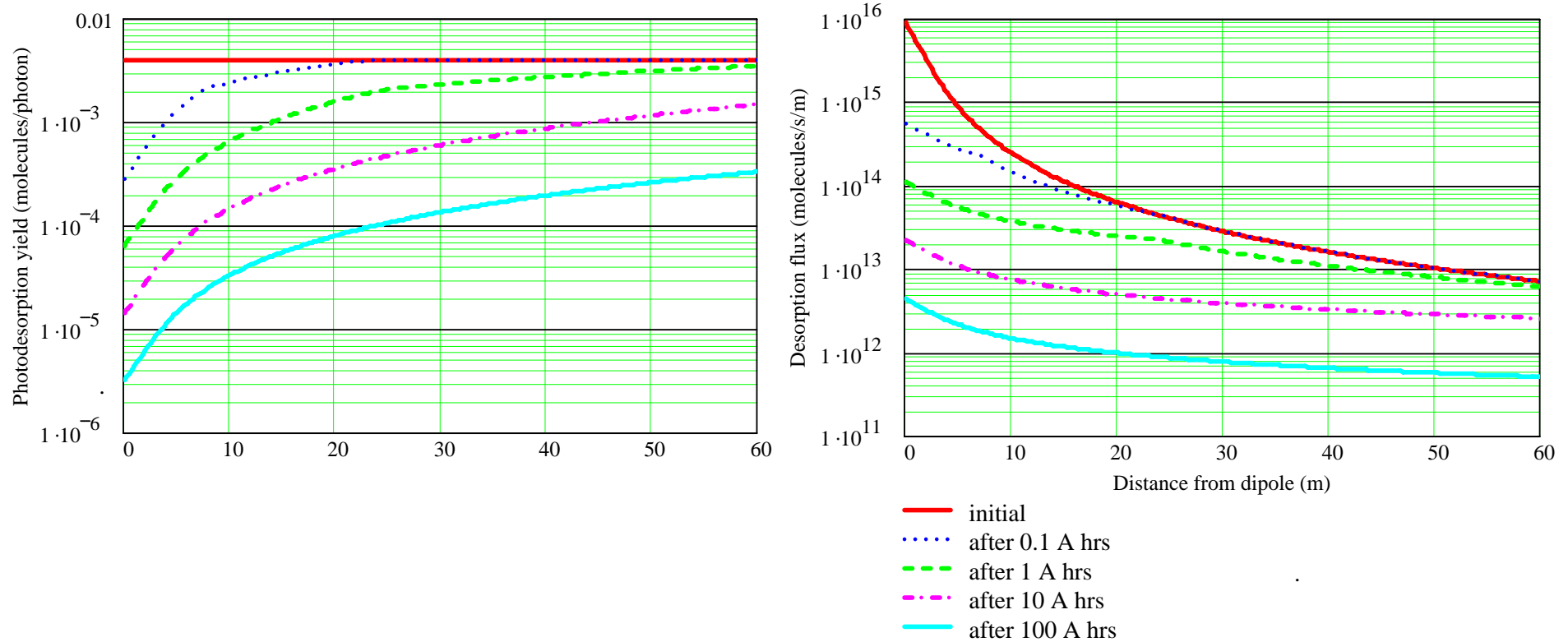
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- The need to avoid fast ion instability leads to very demanding specifications for the vacuum in the electron damping ring [Lanfa Wang, private communication]:
  - < 0.5 nTorr CO in the arc cell,
  - < 2 nTorr CO in the wiggler cell and
  - < 0.1 nTorr CO in the straight section
- In the positron damping ring required vacuum level was not specified and assumed as 1 nTorr (common figure for storage rings)

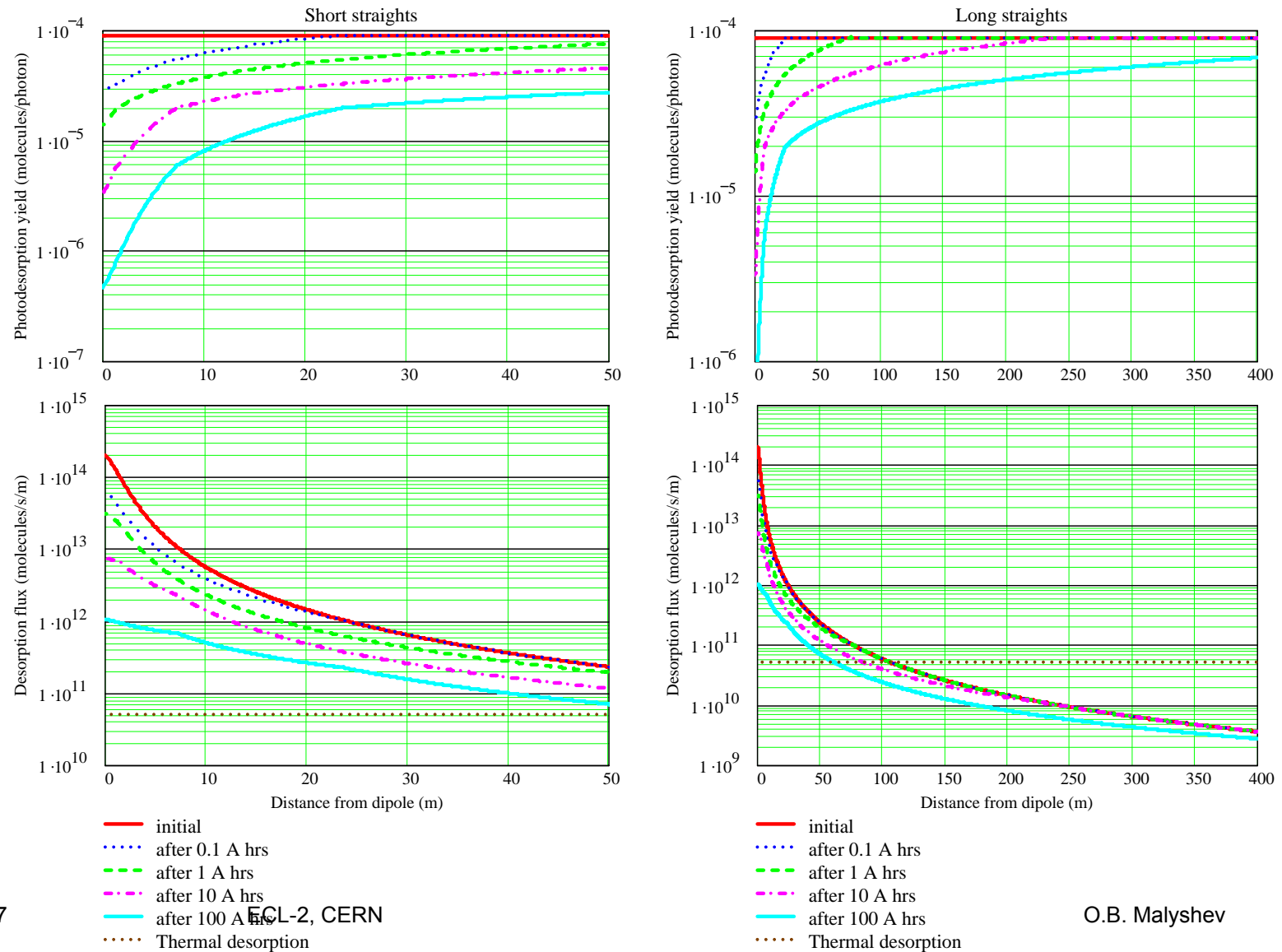
## Photon flux onto the 50-mm diameter vacuum chamber walls inside the ILC DR dipoles and along the short straights



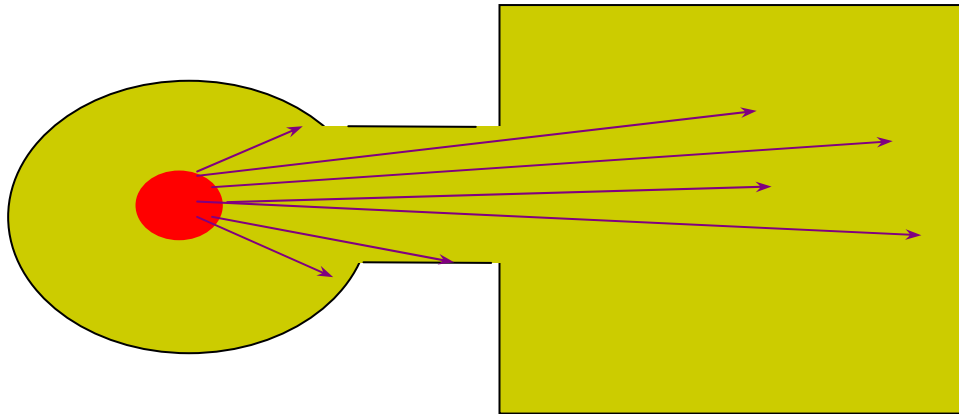
# Photodesorption yield and flux during conditioning



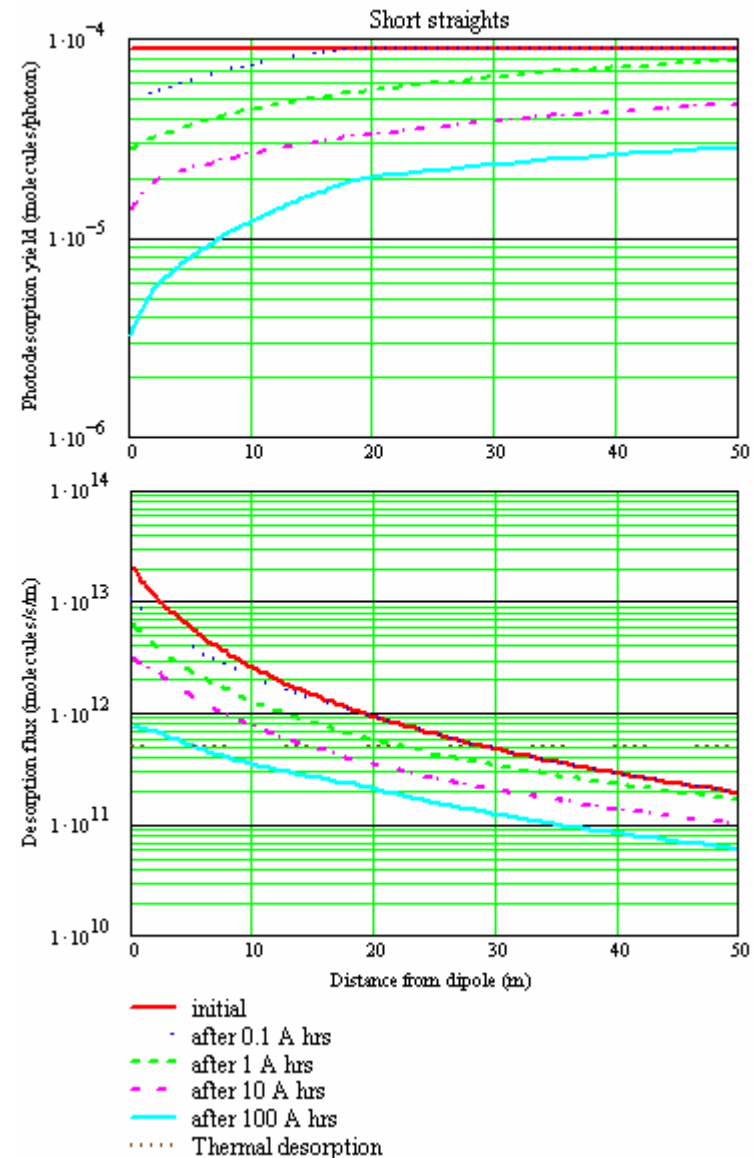
## Photodesorption yield and flux along the damping ring straights made of stainless steel *tubular vacuum chamber* and baked in-situ at 300°C for 24 hrs.



## Photodesorption yield and flux along a stainless steel vacuum chamber *with an ante-chamber* in the damping ring straights baked in-situ at 300°C for 24 hrs.



If ~10% of photons hit a beam vacuum chamber, photon stimulated desorption after 100 Ahr is almost the same as without antechamber, but thermal induced desorption is much larger.



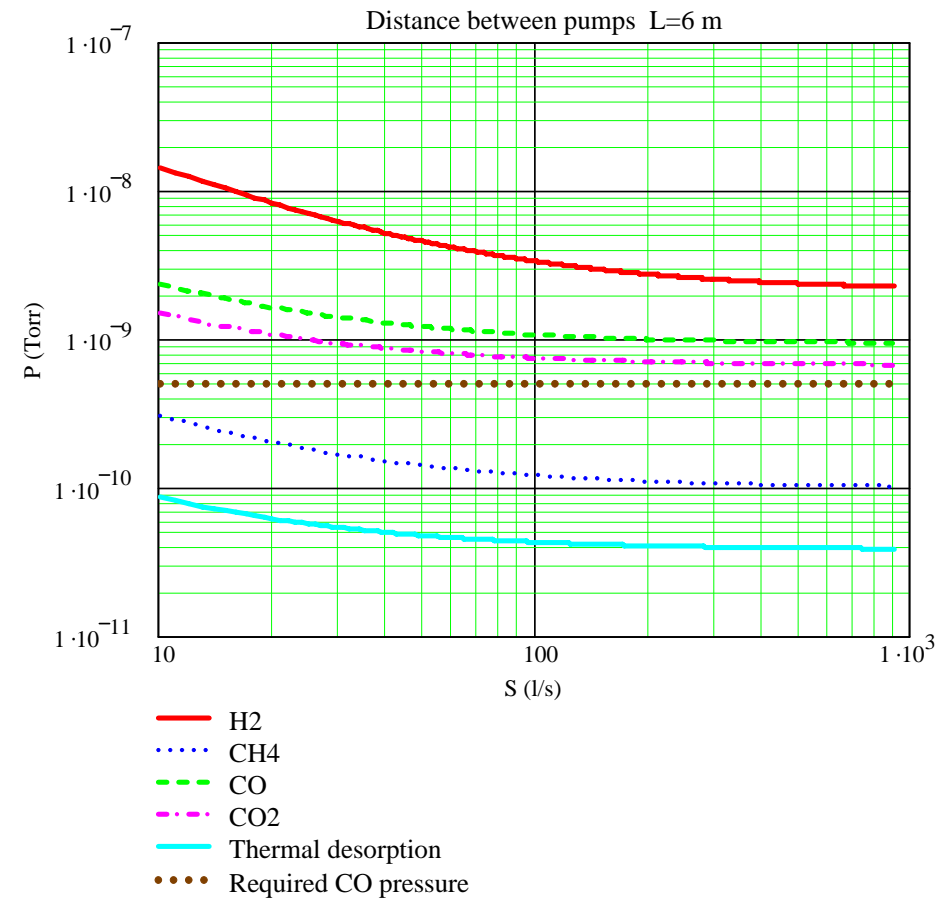
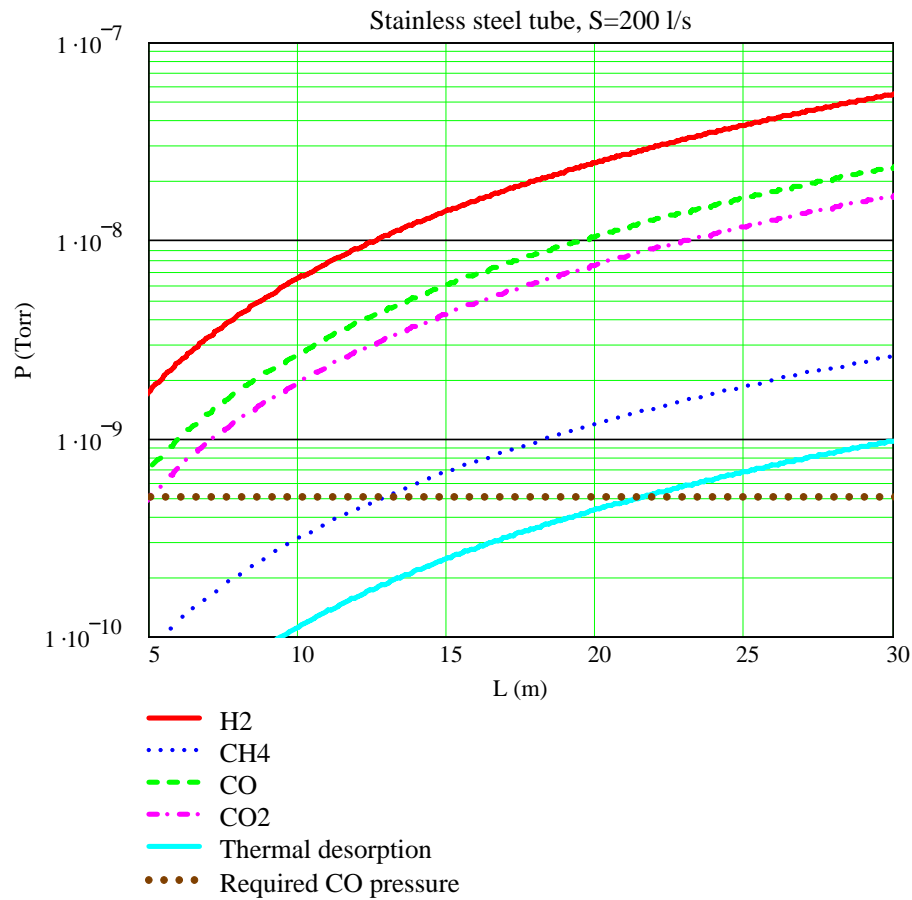
# Tubular chamber vs a vacuum chamber with antechamber

- **Assumption:**
  - 90% of photons are absorbed by SR absorbers and
  - 10% of photons are distributed along the beam vacuum chamber, a gas load analysis can be performed.
- **Results:**
  - The distributed gas desorption due to 10% of photons is after 100 Ahr of beam conditioning the distributed photon stimulated desorption due to 10% of photons is the same for both designs: with and without antechamber.
  - Meanwhile, in addition to photon stimulated desorption from the chamber there is thermal outgassing (10 times larger with an ante-chamber) and photon stimulated desorption from the lumped absorber.
  - Therefore the total outgassing inside the vacuum chamber with an antechamber is larger. Hence, one can conclude that the thermal outgassing will be reduced much faster in a tubular vacuum chamber conditioned with photons than in a vacuum chamber with an ante-chamber.
- **Therefore, the ante-chamber design:**
  - does indeed increase the vacuum conductance,
  - but this does not help in reducing the outgassing.
  - After 100 Ahr of beam conditioning the total outgassing along a tubular vacuum chamber is the same or lower than that along a vacuum chamber with an antechamber, and the SR absorbers make a gas load on the pumps even larger for an antechamber design.
  - Since the antechamber design is more expensive, it worth to explore only if it is necessary to deal with other problems such as beam induced electron multipacting and electron cloud.



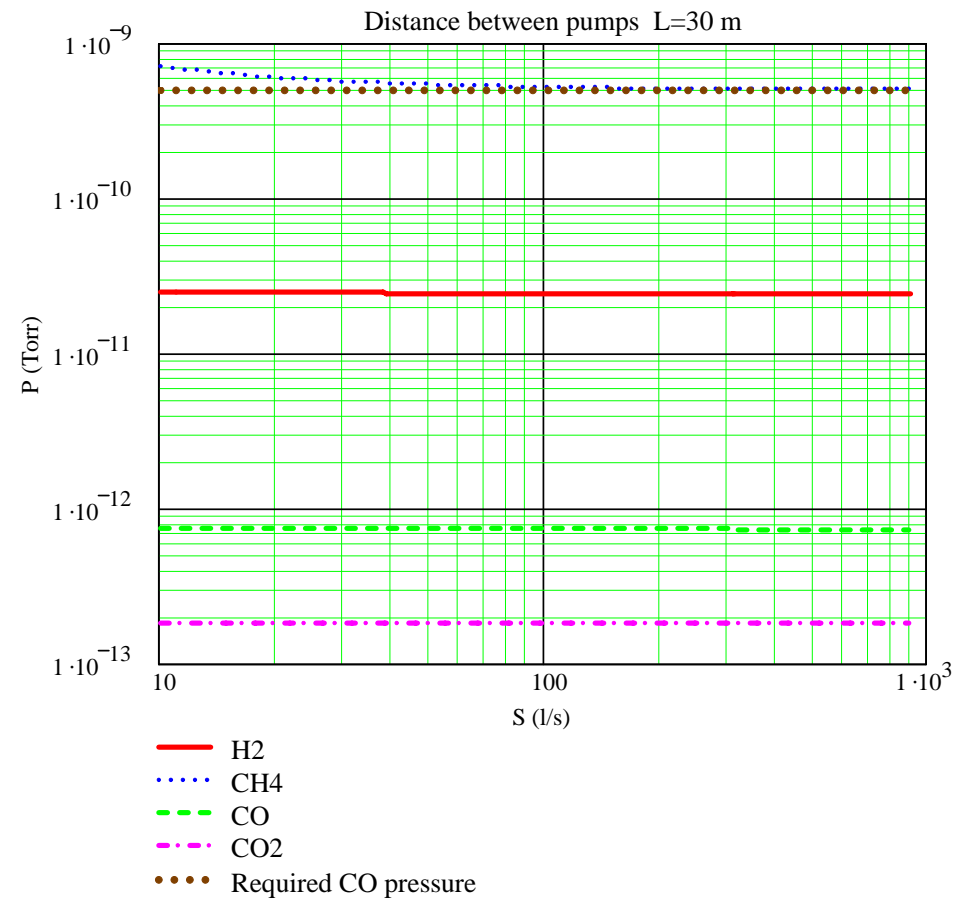
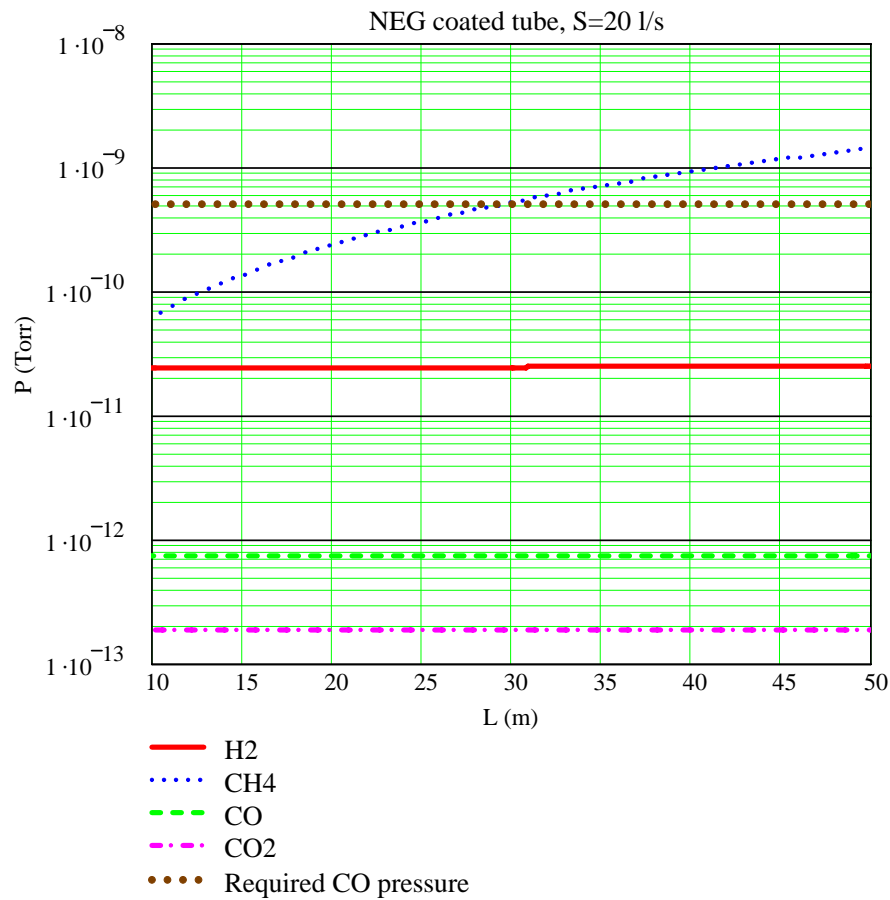
# Pressure along the arc: inside a stainless steel tube

after 100 Ahr beam conditioning:  $S_{\text{eff}} = 200 \text{ l/s every } 5 \text{ m}$



# Pressure along the arc: inside a NEG coated tube

after 100 Ahr beam conditioning:  $S_{\text{eff}} = 20 \text{ l/s}$  every 30 m



## Main result of the modelling

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- NEG coating of vacuum chamber along both the arcs and the wigglers as well as a few tens meters downstream of both looks to be the only possible solution to fulfil vacuum requirement for the ILC dumping ring

### Ideal vacuum chamber for vacuum design:

- Round or elliptical tube
  - Cheapest from technological point of view
- No antechamber
  - Beam conditioning is most efficient
  - Easy geometry for TiZrV coating
- NEG coated
  - Requires less number of pumps with less pumping speed
  - 180°C for NEG activation instead of 250-300°C bakeout
  - Choice of vacuum chamber material (stainless steel, copper and aluminium ) does not affect vacuum in this case
  - Residual gas CH<sub>4</sub> and H<sub>2</sub> (almost no CO and CO<sub>2</sub>)

*O. Malyshev. Vacuum Systems for the ILC Damping Rings. EUROTeV Report-2006-094.*

## How the e-cloud affect vacuum

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- The electron flux  $\sim 10^{16}$  e<sup>-</sup>/(s·m) with  $E \approx 200$  eV will desorb approximately the same gas flux as the photon flux of  $\sim 10^{18}$   $\gamma$ /(s·m).
- If the electron stimulated desorption is larger than photon stimulated desorption, that should be considered in vacuum design and conditioning scenario.
- Gas density will increase => gas ionisation will also increase =>
  - Electrons are added to e-cloud
  - Ions are accelerated and hit the wall of vacuum chamber => ion induced gas desorption and secondary electron production
- Gas density increase may change e-cloud density.

## How the e-cloud affect vacuum

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- The electron flux [ $e^-/(s \cdot m)$ ] and average energy [eV] and total power [W] of electrons are required for gas density calculations and vacuum design.
- Groves and antechamber will increase the necessary conditioning time and complicate the TiZrV coating. It is more expensive than NEG coated tube.
- Electrodes and insulating materials may dramatically increase gas density in a vacuum chamber due to thermal, photon, electron and ion induced gas desorption.
  - Choice of material and design must be UHV compatible.
  - The NEG coating might be difficult, impossible or inefficient, which will lead to much more expensive vacuum design.
  - If the 'e-cloud killer' requires a vertical space – it will require larger magnet gap and more expensive dipoles.

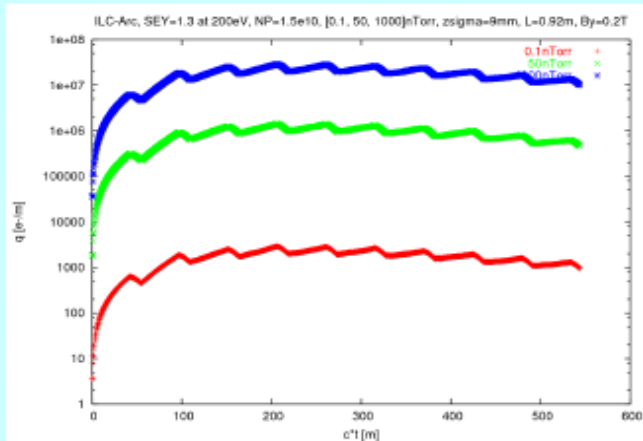
## If e-cloud is too large in a round tube

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- What is the main source of electrons:
  - Photo-electrons
    - Geometrical: reduction or localisation of direct and reflected photons
    - Surface treatment, conditioning, coating
  - Secondary electrons
    - All possible solution discussed during this workshop
  - Gas ionisation
    - Surface treatment and conditioning
    - Low outgasing coating
    - Better pumping
- Good solution against Photo-electrons or Secondary electrons might led to higher gas density and higher gas ionisation, and vice versa.

# Example 1: W. Bruns's results

Fixed SEY, varying Gaspressure and Bunchpopulation, no PEY



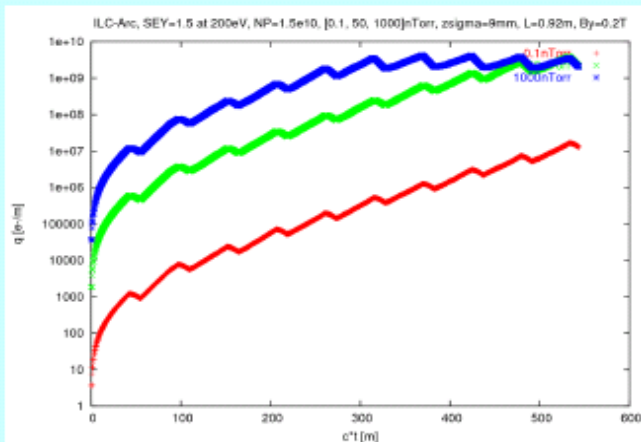
$$SEY=1.3 \quad q_{sat} \propto P,$$

here gas ionisation is the main source of electrons but  $q_{sat} < q_{max}$  for ILC DR

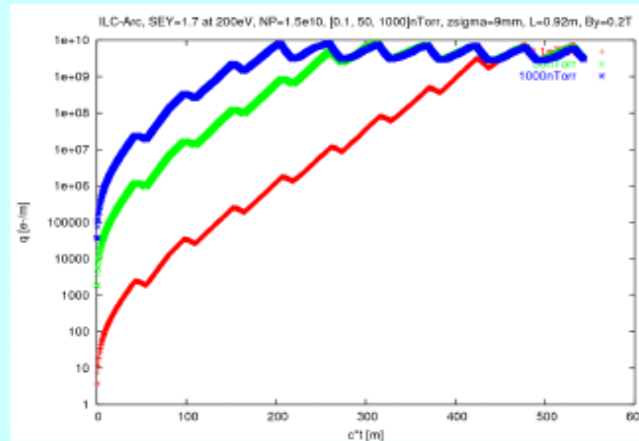
$SEY \geq 1.5 \quad q_{sat} > q_{max}$  for ILC DR,

here SEY is the main source of electrons

SEY=1.3, [0.1,50,1000] nTorr, nP=1.5e10



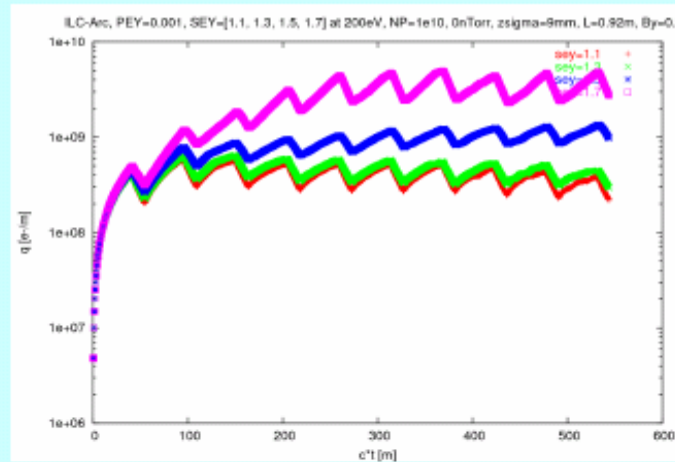
SEY=1.5, [0.1, 50, 1000]nTorr, nP=1.5e10



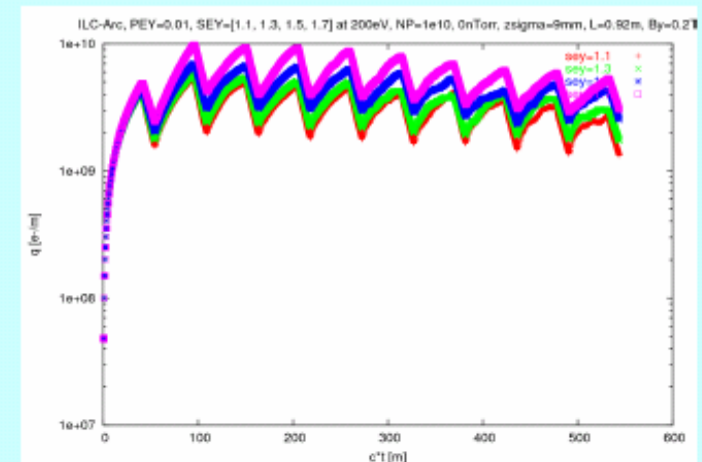
SEY=1.7, [0.1, 50, 1000]nTorr, nP=1.5e10

# Example 1: W. Bruns's results

## Fixed PEY, varying SEY and Bunchpopulation, no Gaspressure

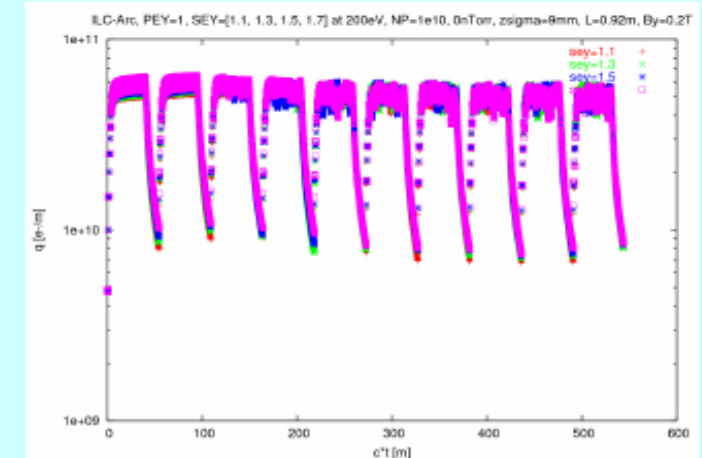


PEY=0.001, SEY=[1.3,1.5,1.7], nP=1e10



PEY=0.01, SEY=[1.3,1.5,1.7], nP=1e10

$PEY=0.001$   $q_{sat}=f(SEY)$  for  $SEY>1.3$ , hence  
 the main source of electrons are  
 photoelectrons for  $SEY\leq 1.3$ ,  
 secondary electrons for  $SEY > 1.3$ .  
 $PEY\geq 0.01$  is the main source of electrons are  
 photoelectrons



PEY=1, SEY=[1.3,1.5,1.7], nP=1e10