



Introduction to Cryogenics

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Contributions from S. Claudet and Ph. Lebrun

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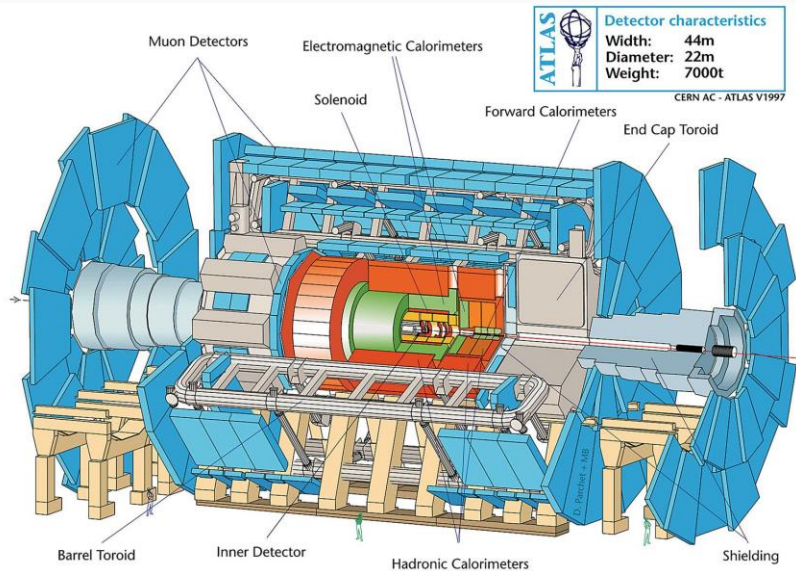
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Content

- Introduction to cryogenic installations
- Motivation => reducing thermal energy in a system
- Heat transfer and thermal insulation
- Helium cryogenics, He I => He II
- Conclusions
- References

Overview of cryogenics at CERN - Detectors



CMS DETECTOR

Total weight : 14,000 tonnes
Overall diameter : 15.0 m
Overall length : 28.7 m
Magnetic field : 3.8 T

STEEL RETURN YOKE
12,500 tonnes

SILICON TRACKERS
Pixel (100x150 μm) ~16m² ~66M channels
Microstrips (80x180 μm) ~200m² ~9.6M channels

SUPERCONDUCTING SOLENOID
Niobium titanium coil carrying ~18,000A

MUON CHAMBERS
Barrel: 250 Drift Tube, 480 Resistive Plate Chambers
Endcaps: 468 Cathode Strip, 432 Resistive Plate Chambers

PRESHOWER
Silicon strips ~16m² ~137,000 channels

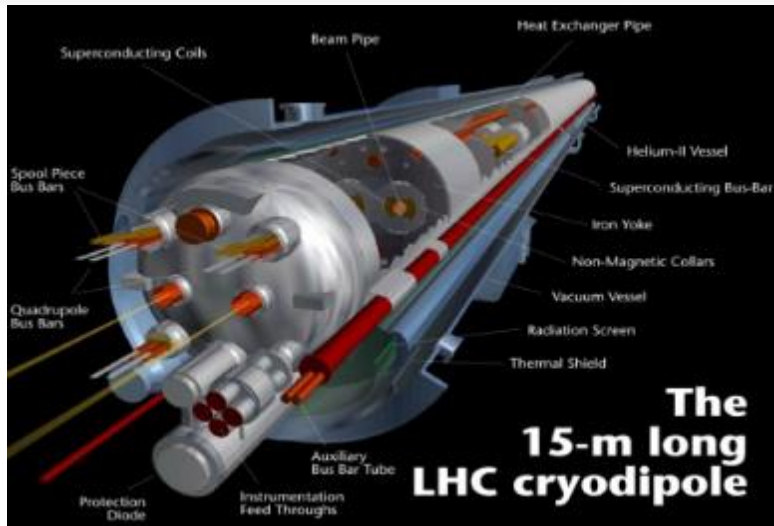
FORWARD CALORIMETER
Steel + Quartz fibres ~2,000 Channels

CRYSTAL
ELECTROMAGNETIC
CALORIMETER (ECAL)
~76,000 scintillating PbWO₄ crystals

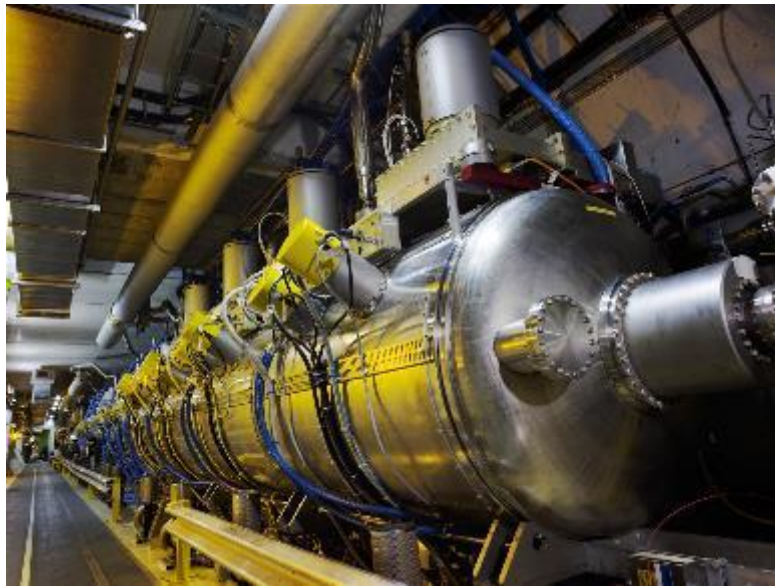
HADRON CALORIMETER (HCAL)
Brass + Plastic scintillator ~7,000 channels

- Superconducting coils of LHC detectors @ 4.5 K (ATLAS, CMS)
- LAr Calorimeter - LN₂ cooled
- Different types of cryogenics (Helium, Nitrogen and Argon)

Overview of cryogenics at CERN - LHC

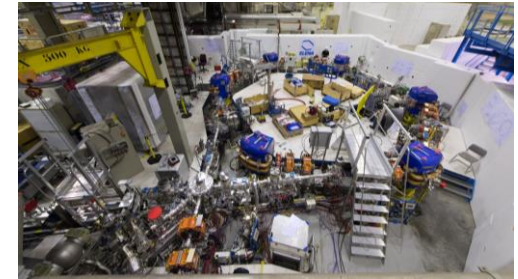


- Helium at different operating temperatures (thermal shields, beam screens, distribution and magnets,...)
- Superconducting (SC) magnets of the LHC ring
- Accelerating SC cavities



Overview of cryogenics at CERN

- North area =>
- SM18
- Antimatter Factory =>
- HIE-Isolde
- Test facilities =>
- Neutrino Platform
- ...



Sources: CERN-PHOTO-201509-239, CERN-EX-0606017, CERN-PHOTO-201607-170-3, OPEN-PHO-ACCEL-2016-016-7, CERN-PHOTO-201703-077-4

Cryogenic fluids - Thermophysical properties

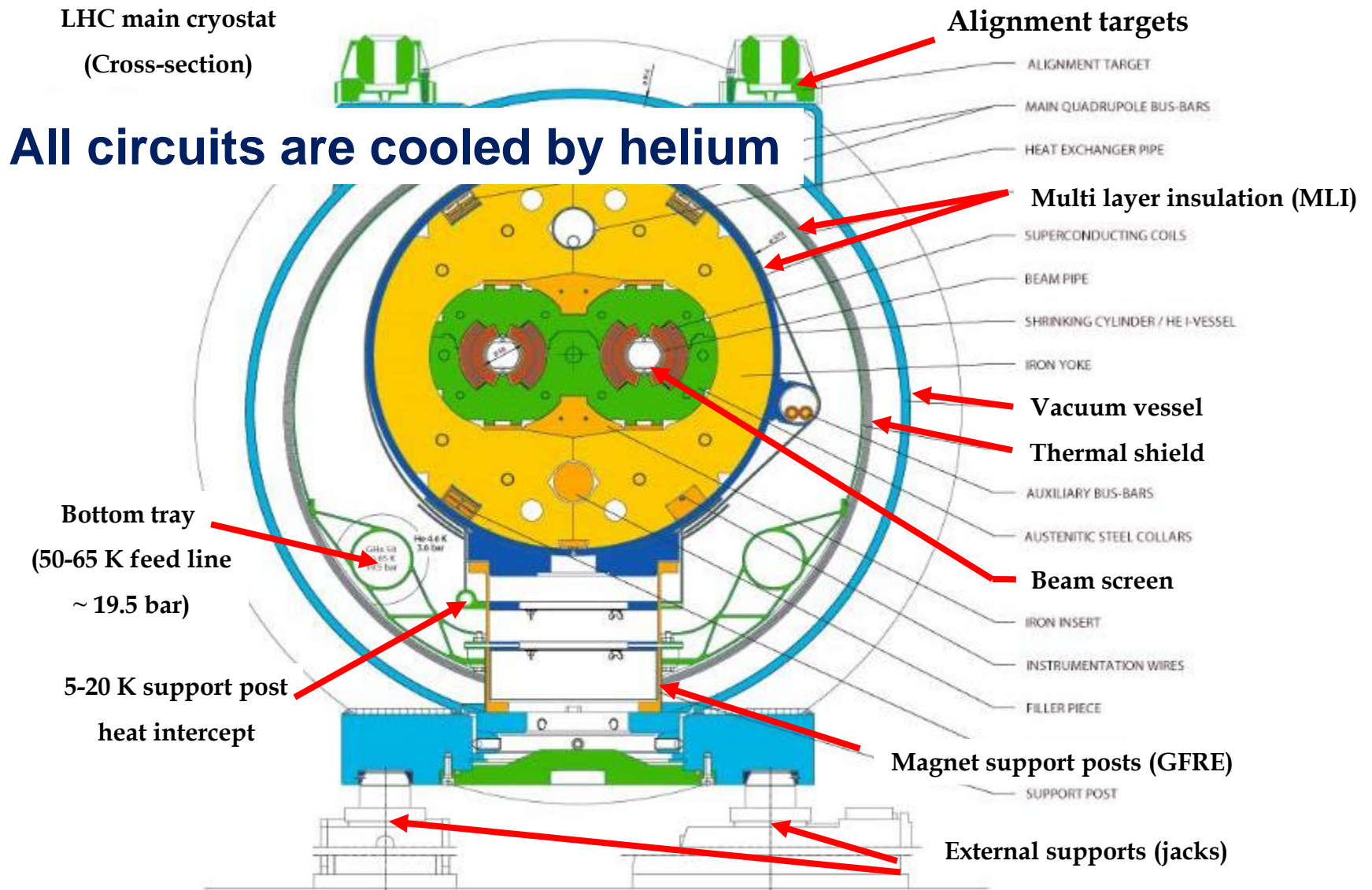
Fluid	⁴ He	N ₂	Ar	H ₂	O ₂	Kr	Ne	Xe	Air	Water
Boiling temperature (K) @ 1.013 bar	4.2	77.3	87.3	20.3	90.2	119.8	27.1	165.1	78.8	373
Latent heat of evaporation @ T _b in kJ/kg	20.9	199.1	163.2	448	213.1	107.7	87.2	95.6	205.2	2260
Volume ratio gas _(273 K) / liquid	709	652	795	798	808	653	1356	527	685	-----
Volume ratio saturated vapor to liquid (1.013 bar)	7.5	177.0	244.8	53.9	258.7	277.5	127.6	297.7	194.9	1623.8
Specific mass of liquid (at T _b) – kg/m ³	125	804	1400	71	1140	2413	1204	2942	874	960

Cryogenics and Superconductivity

Characteristic temperatures of low-energy phenomena

Phenomenon	Temperature
Debye temperature of metals	few 100 K
High-temperature superconductors	~ 100 K
Low-temperature superconductors	~ 10 K
Intrinsic transport properties of metals	< 10 K
Cryo-pumping	few K
Cosmic microwave background	2.725 K
Superfluid ^4He	< 2.17 K
Bolometers for cosmic radiation	< 1 K
ADR stages, Bose-Einstein condensates	$\sim \mu\text{K}$

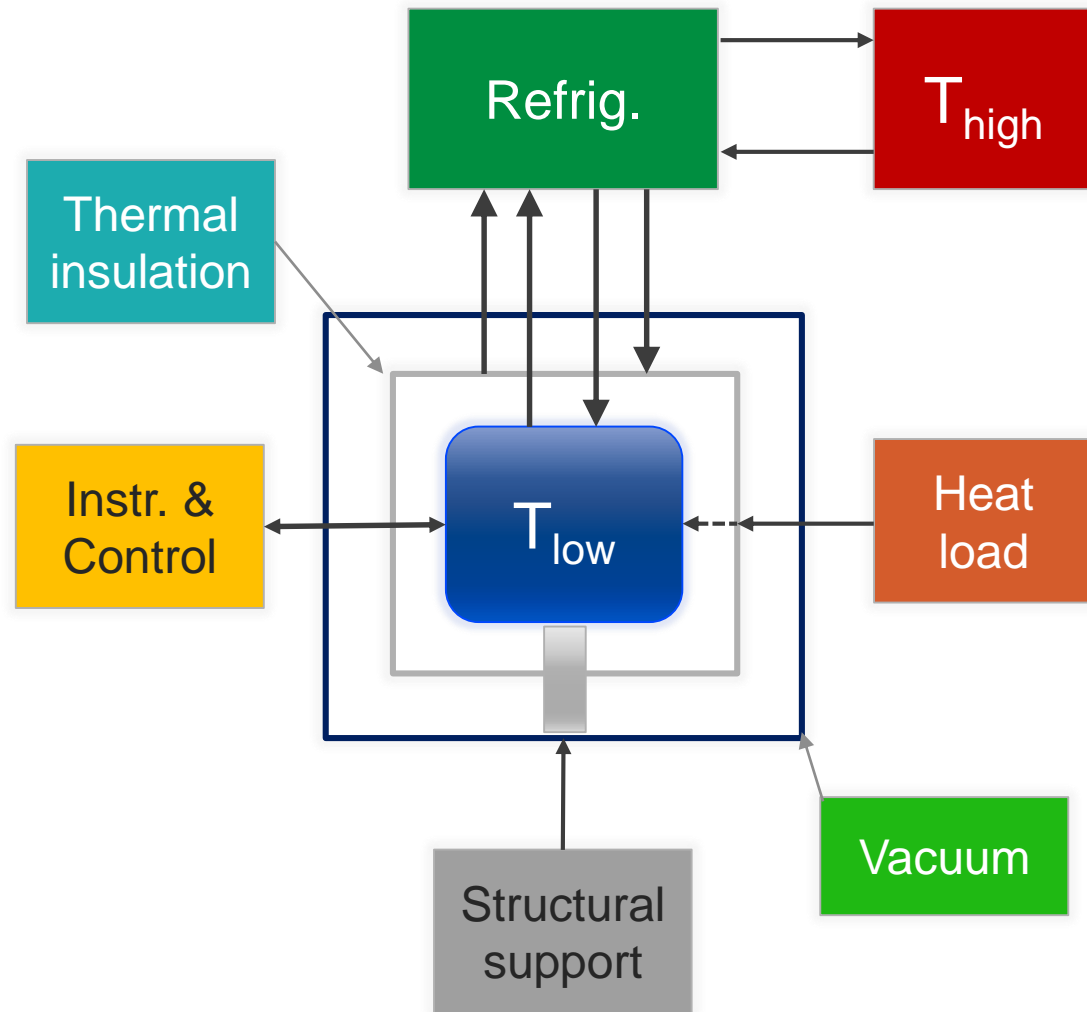
Cryogenic application: Dipole magnets of the LHC



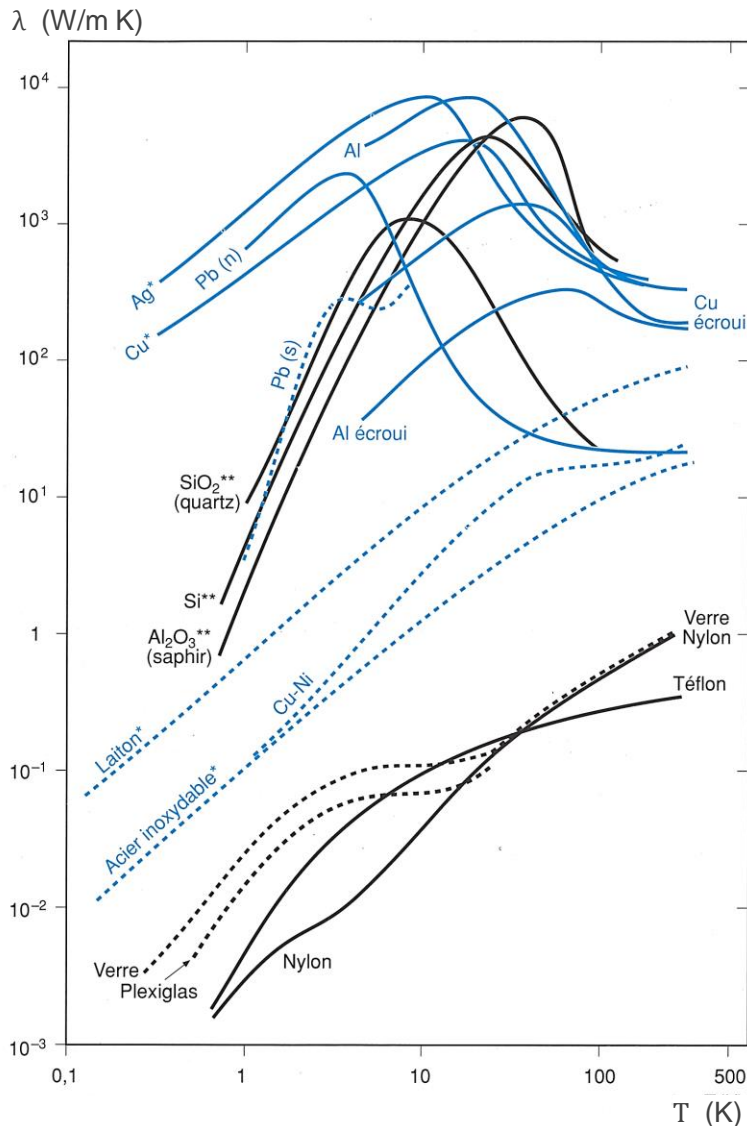
Heat Transfer and Thermal Insulation

Cryogenic System Design

- Low temperature environment
- Source of refrigeration
- Heat exchange strategy
- Sample environment
- Thermal insulation
- Structural support
- Instrumentation and control



Thermal conductivity, solid conduction – how to cool?



Heat transport in solids

Fourier's law: $\dot{Q} = -\lambda(T) \frac{A}{l} \nabla T$

Pure dielectric crystals: phonons

Dielectrics/Insulators: phonons

Pure metals: free electron gas and phonons

Alloyed metals: electrons and phonons

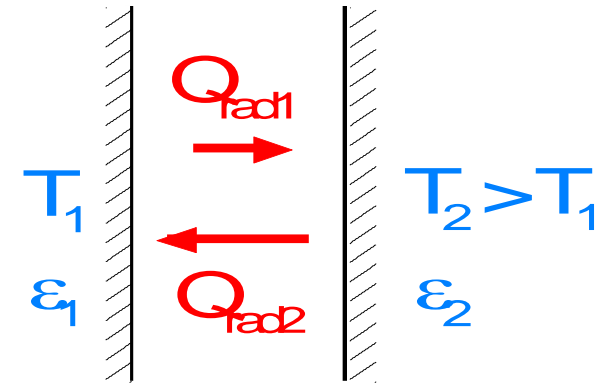
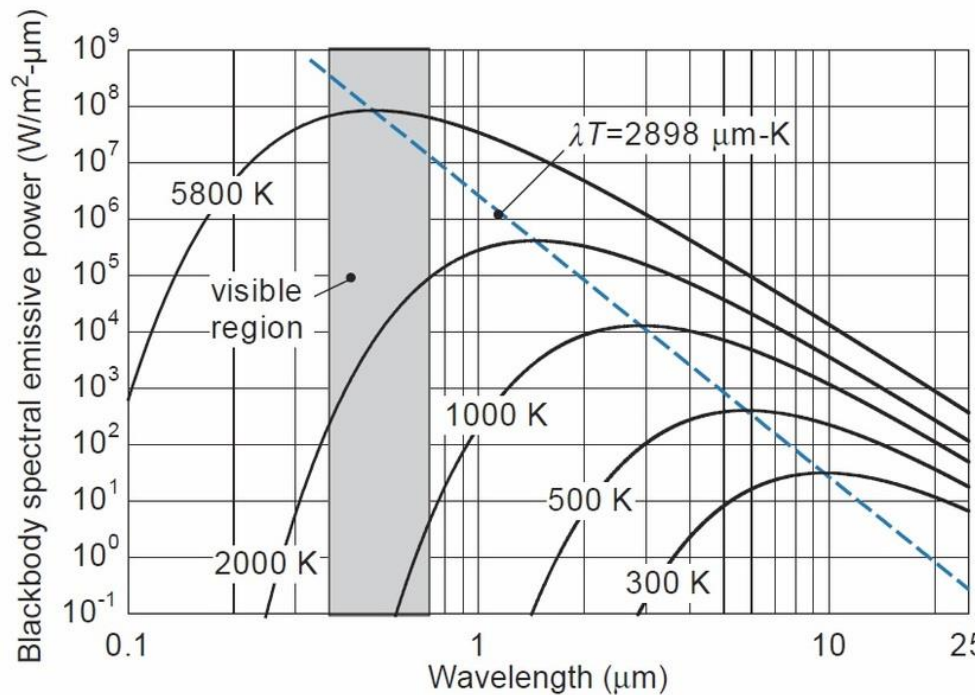
From: Cryogenie, Institut International du Froid, Paris

Radiative heat transfer – Black body

Wien's law (Maximum of black body power spectrum)

$$\lambda_{max} T = 2898 \mu\text{m K}$$

$$\Rightarrow 10 \mu\text{m} \text{ for } T = 300 \text{ K}$$



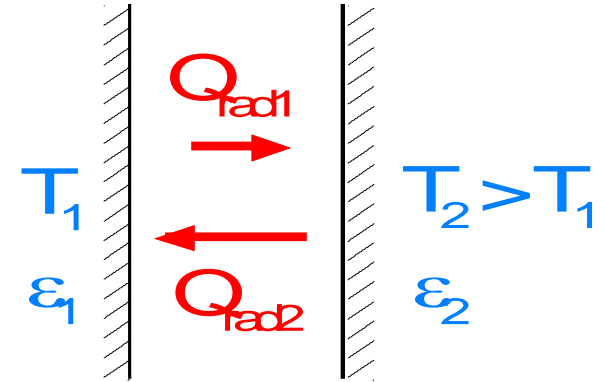
Source:
https://www.researchgate.net/figure/Blackbody-spectral-emissive-power-as-a-function-of-wavelength-for-various-values-of_fig4_320298109

Radiative heat transfer – Grey body

- Wien's law (Maximum of black body power spectrum)

$$\lambda_{max} T = 2898 \mu\text{m K}$$

$$\Rightarrow 10 \mu\text{m} \text{ for } T = 300 \text{ K}$$



- Stefan-Boltzmann's law

Black body

$$\dot{Q}_{rad} = \sigma A T^4$$

$\sigma = 5.67 \times 10^{-8} \text{ W}/(\text{m}^2 \text{ K}^4)$
(Stefan-Boltzmann's constant)

- “Grey” body

$$\dot{Q}_{rad} = \epsilon \sigma A T^4$$

ϵ - emissivity of surface

- “Grey” surfaces at T_1 and T_2

$$\dot{Q}_{rad} = E \sigma A (T_1^4 - T_2^4)$$

E - function of ϵ_1 , ϵ_2 , geometry

Emissivity of technical materials at low temperatures

	Surface at 77 K	Surface at 4.2 K
Stainless steel, as found	0.34	0.12
Stainless steel, mech. polished	0.12	0.07
Stainless steel, electropolished	0.10	0.07
Stainless steel + Al foil	0.05	0.02
Aluminium, as found	0.12	0.07
Aluminium, mech. polished	0.10	0.06
Aluminium, electropolished	0.08	0.04
Copper, as found	0.12	0.06
Copper, mech. polished	0.06	0.02

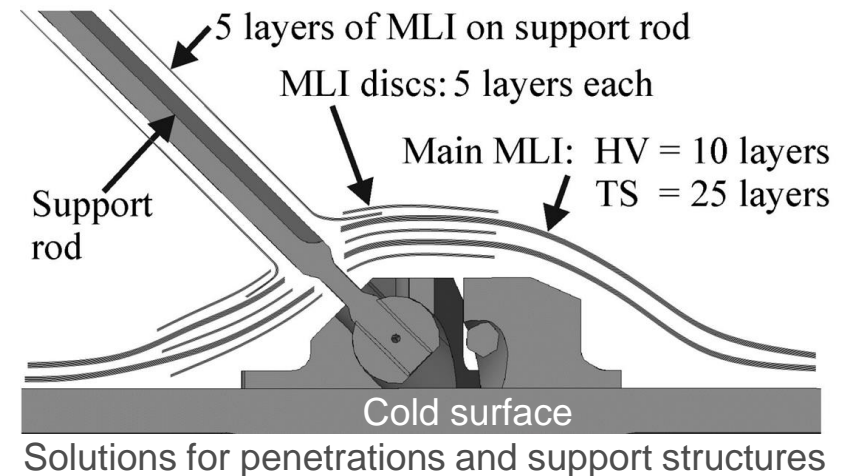
Condensed layers from gas phase easily vary these values !

From: Ph. Lebrun, CAS School on Vacuum in Accelerators, 2006

Multi-layer insulation (MLI)

Complex system involving three heat transfer processes

- $Q_{MLI} = Q_{radiation} + Q_{solid} + Q_{residual}$
- With n reflective layers of equal emissivity, $Q_{radiation} \sim 1/(n+1)$
- Parasitic contacts between layers, Q_{solid} increases with layer density
- $Q_{residual}$ due to residual gas trapped between layers, scales as $1/n$ in molecular regime
- Non-linear behavior requires layer-to-layer modeling



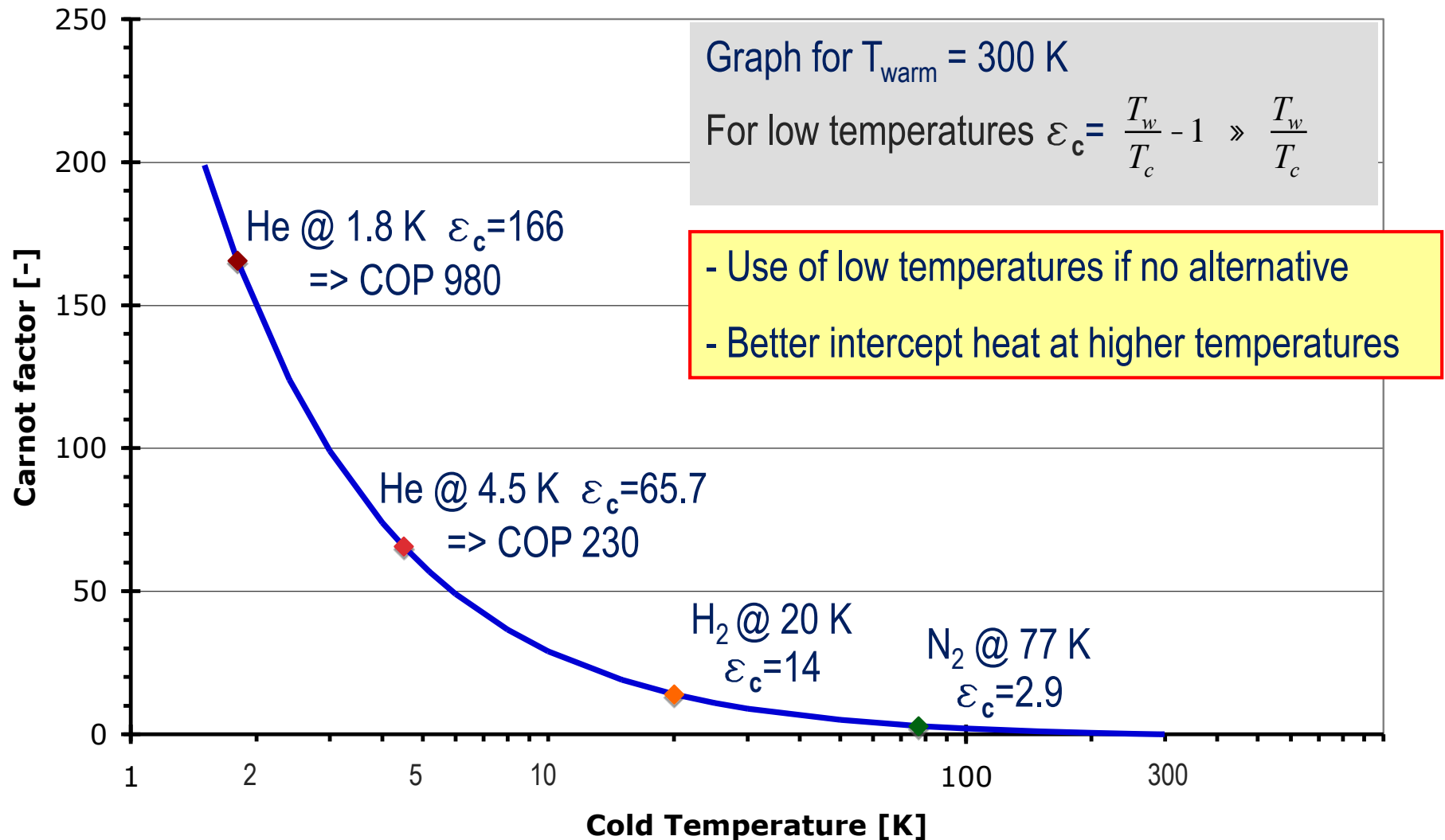
Large surface application

Typical heat fluxes between flat plates (cold side vanishingly low)

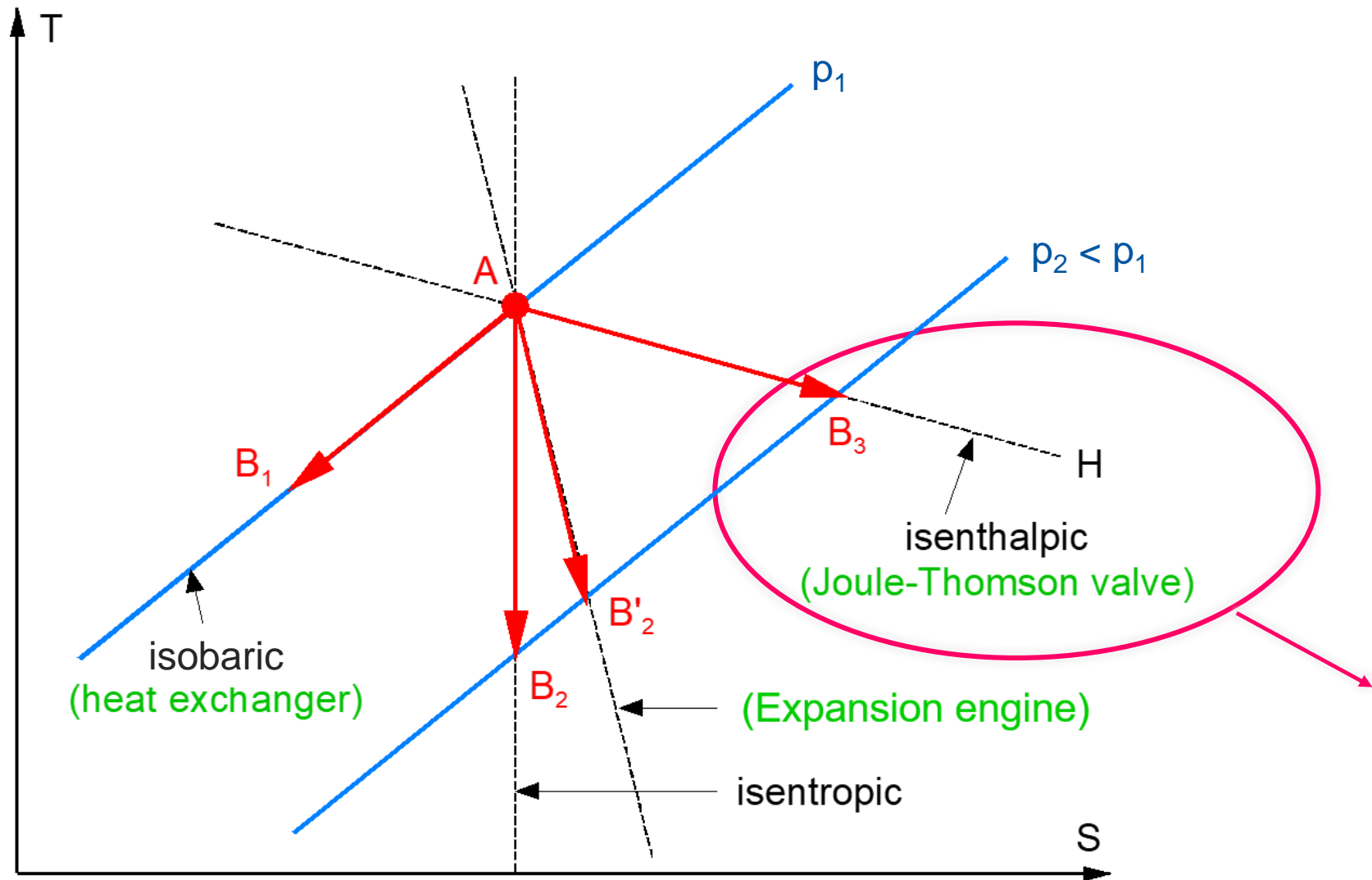
Configuration	W/m ²
Black-body radiation from 293 K	420
Black-body radiation from 80 K	2.3

Refrigeration and Liquefaction

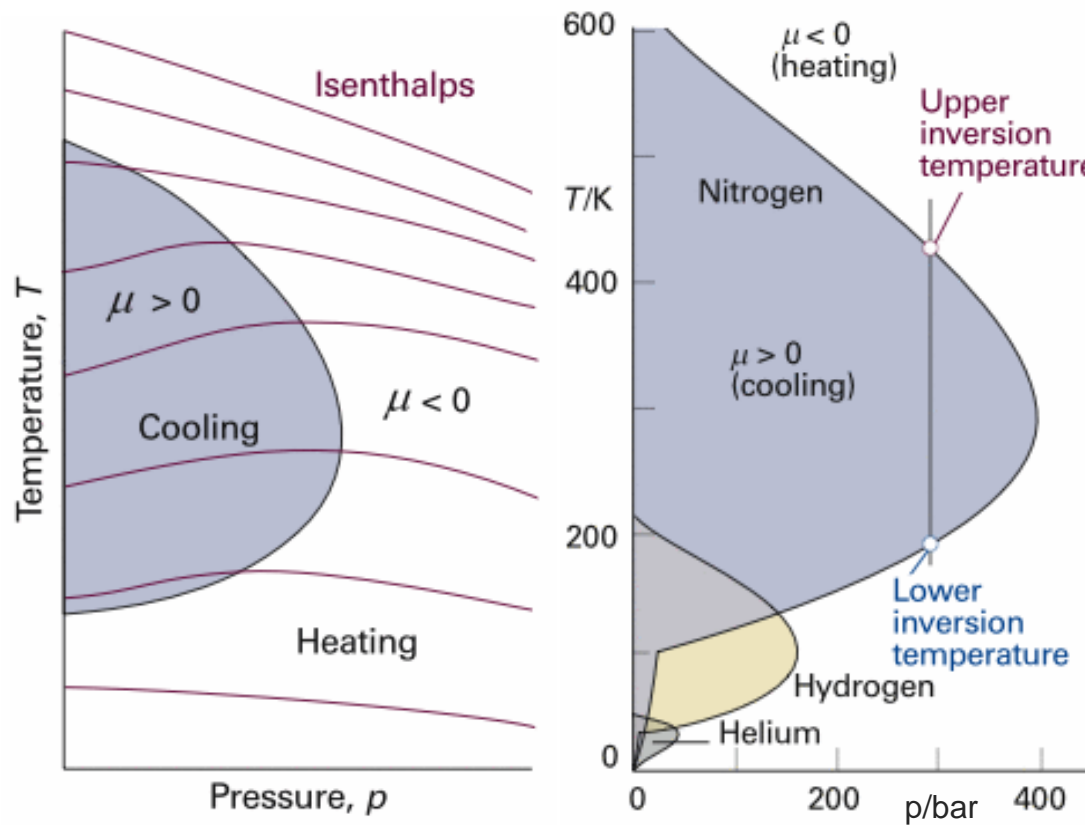
Thermodynamics of cryogenic refrigeration



Elementary cooling processes in a T-s diagram

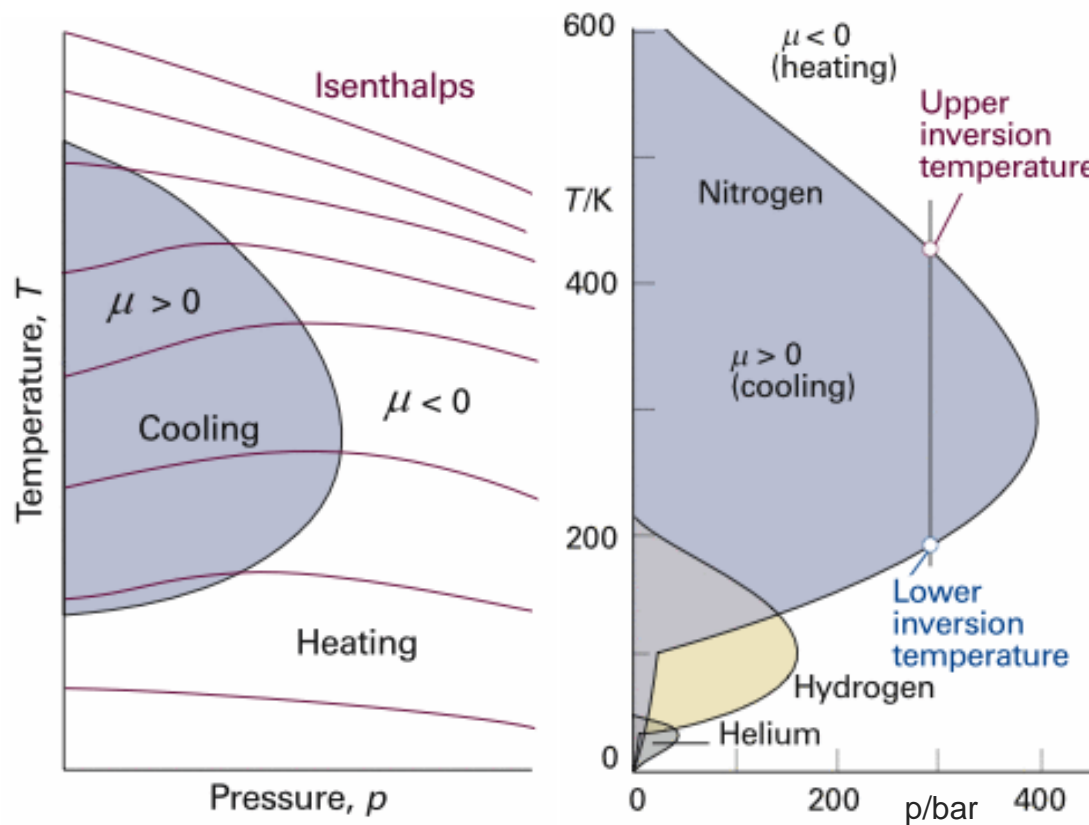


Maximum Joule-Thomson inversion temperatures



Source: http://faculty.chem.queensu.ca/people/faculty/mombourquette/Chem221/3_FirstLaw/ChangeFunctions.asp

Maximum Joule-Thomson inversion temperatures

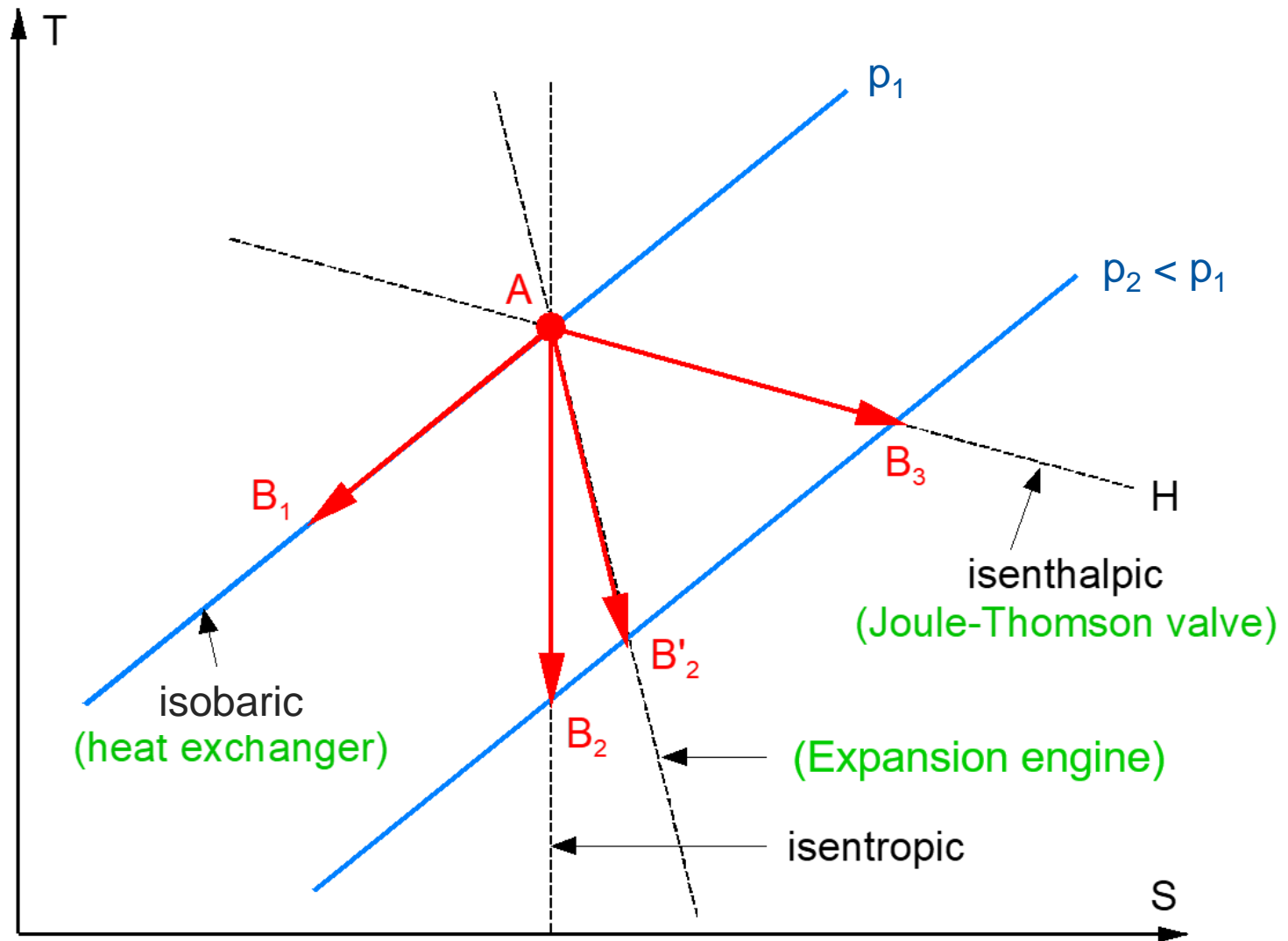


Cryogen	Max. inversion temperature [K]
Helium	43
Hydrogen	202
Neon	260
Air	603
Nitrogen	623
Argon	723

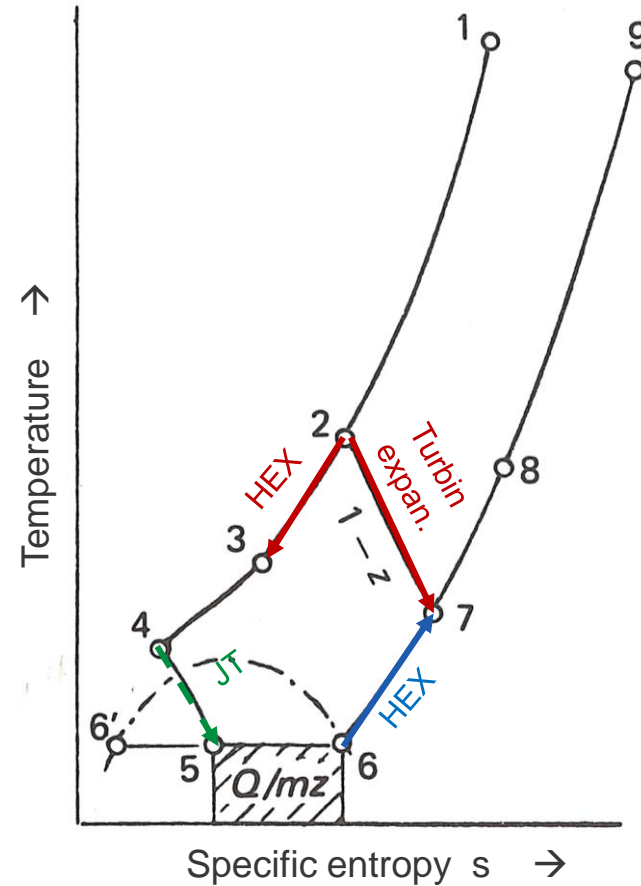
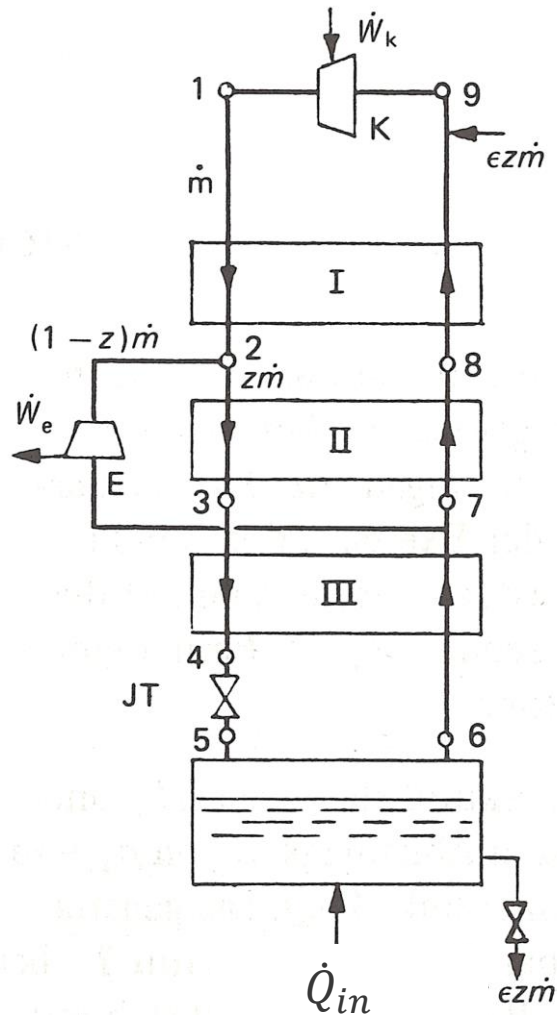
Source: Refprop® NIST

- Air can be cooled down and liquefied by J-T expansion from room temperature,
- Helium and hydrogen need precooling down to below the inversion temperature by heat exchange or work-extracting expansion (e.g. in turbines)

Combining all three processes in a cryoplant

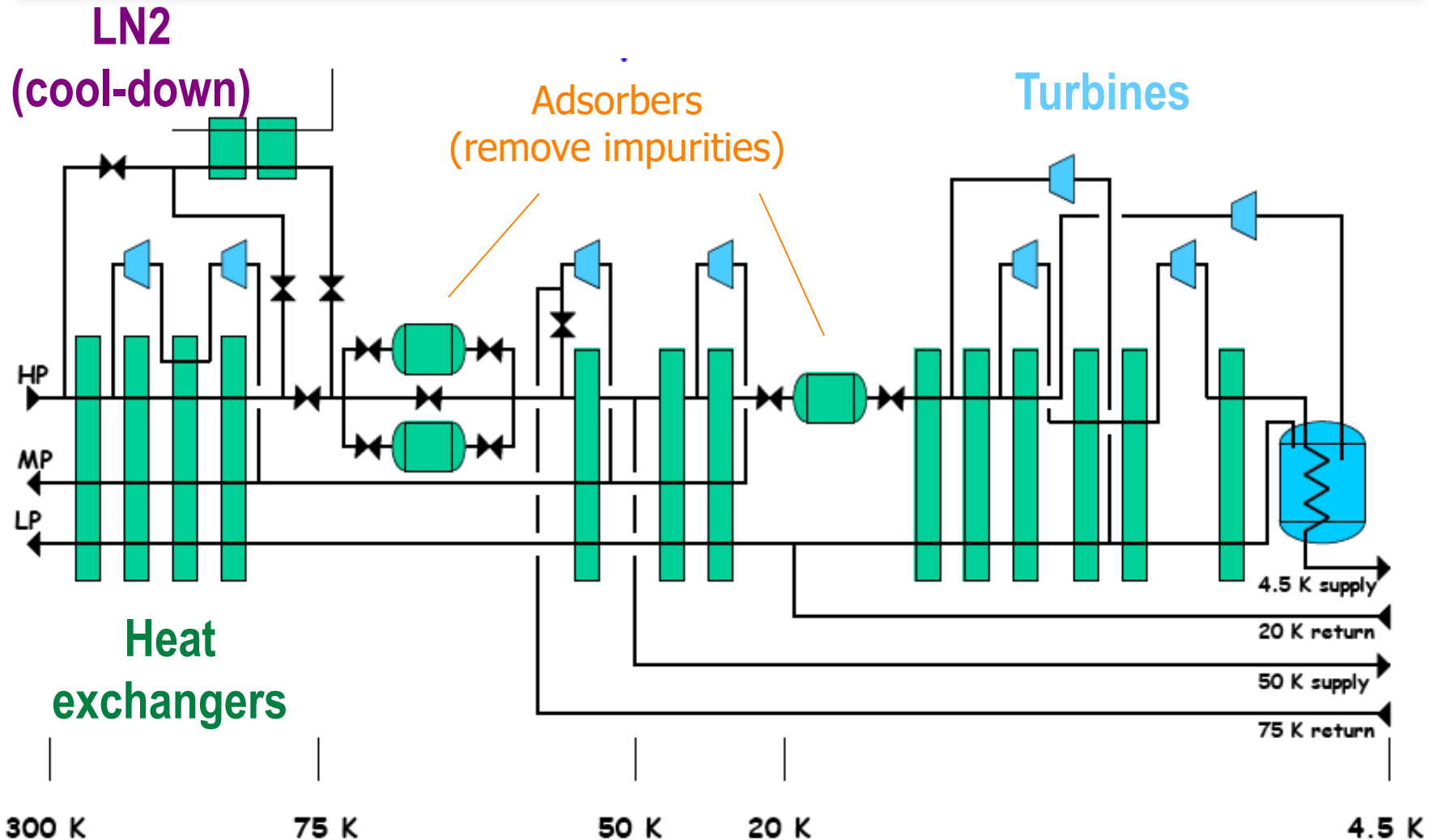


Claude cycle (Turbo Brayton + JT)

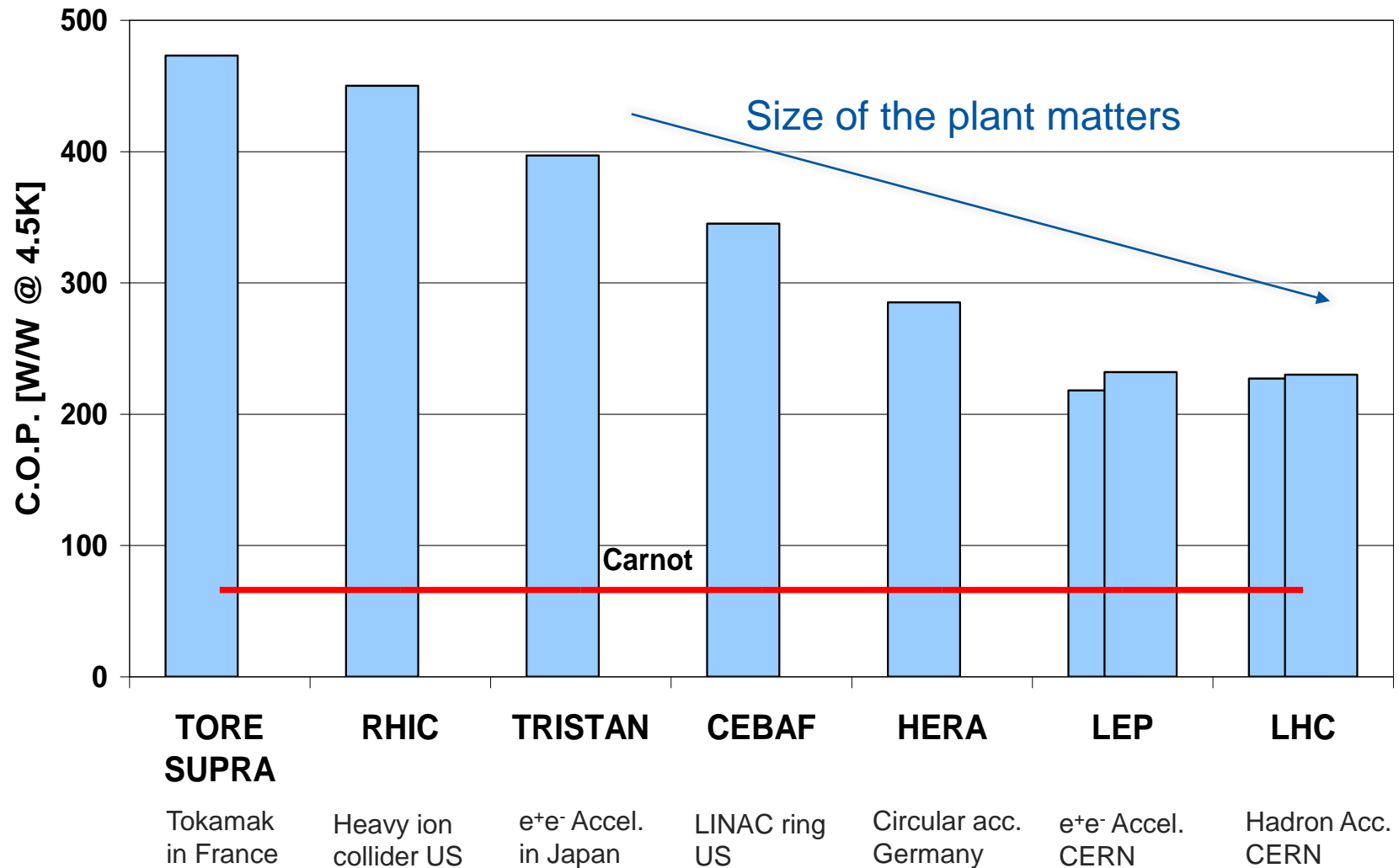


Source: Frey, Haefer, Tieftemperaturtechnologie, VDI Verlag 1981, ISBN 3-18-400503-8, adapted.

Process diagram, LHC refrigerator 18 kW @ 4.5 K



COP of large cryogenic helium refrigerators



LHC 18 kW @ 4.5 K helium cryoplants



Th. shields: 33 kW @ 50 K to 75 K
Beam screen: 23 kW @ 4.6 K to 20 K
Current leads: 41 g/s liquefaction

4 MW compressor power
COP 220-230 W_{el}/W @ 4.5 K



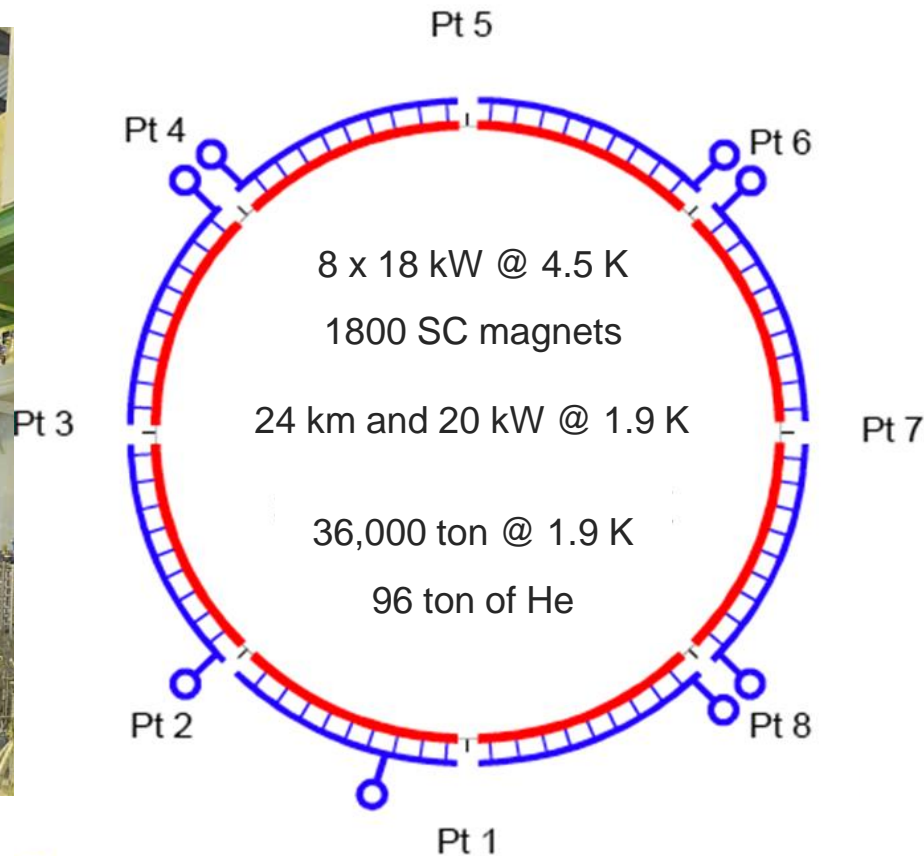
Air Liquide



Linde



LHC 18 kW @ 4.5 K helium cryoplants



○ Cryogenic plant

Air Liquide

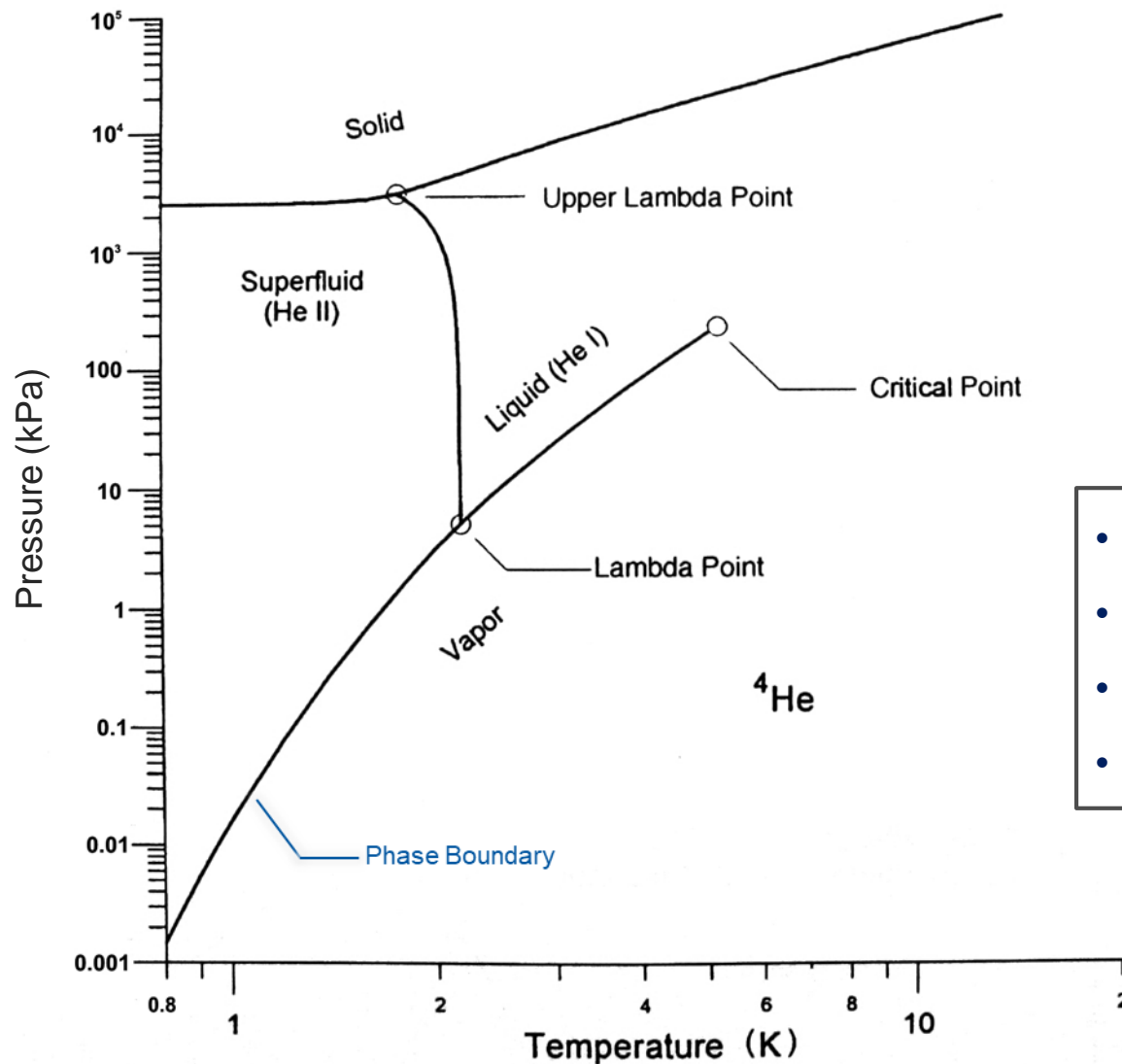


Linde



K to 75 K
5 K to 20 K
fraction
compressor power
10 W/W @ 4.5 K

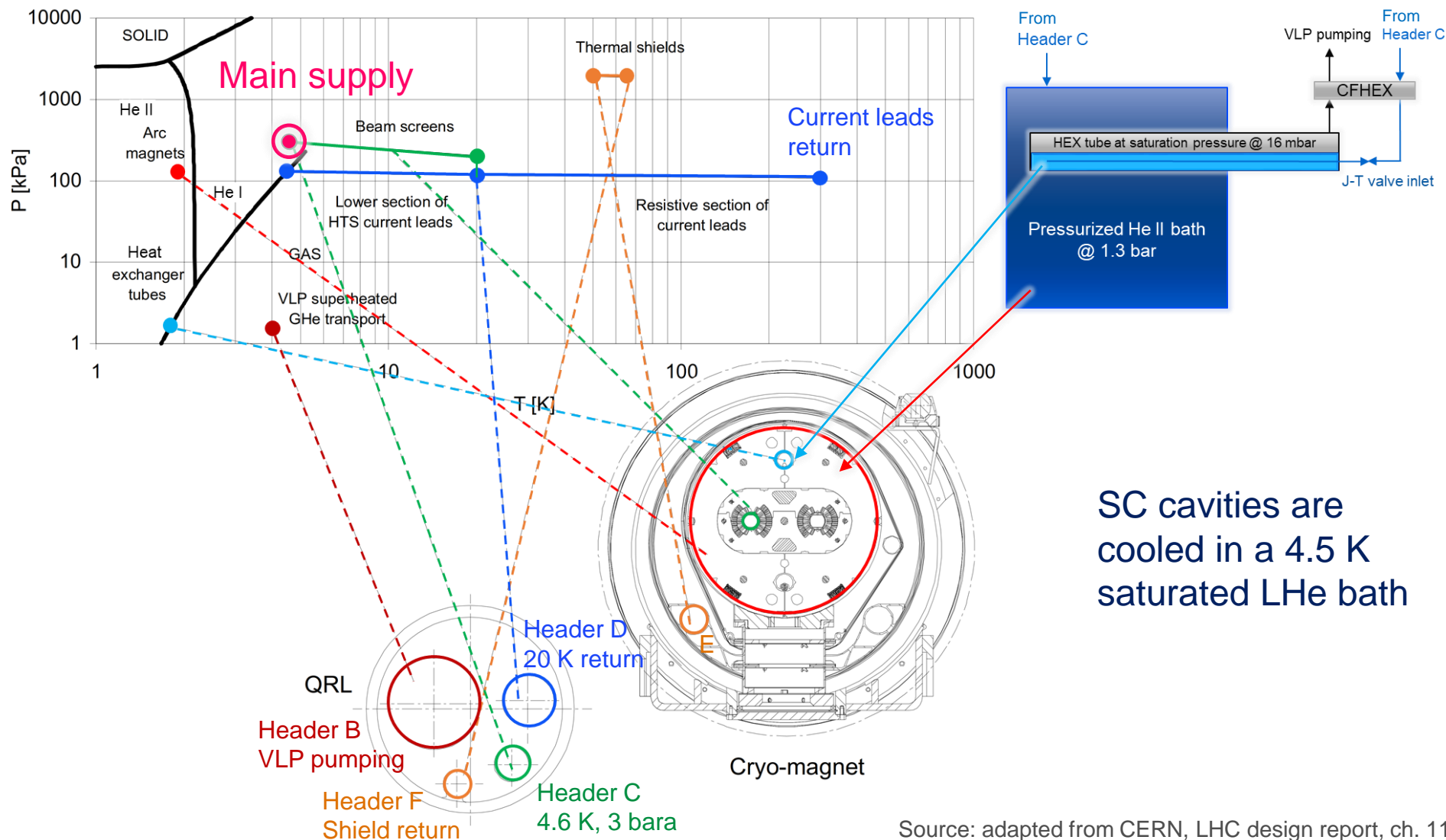
^4He phase diagram



- Helium has no triple point
- Solid He only above 25 bar
- Lambda line \Rightarrow He I / He II separ.
- He II with very special properties

From Weisend, Handbook of Cryogenic Engineering, 1984.

LHC Cooling scheme



Source: adapted from CERN, LHC design report, ch. 11

Cryogenic Fluid Properties

He I and He II

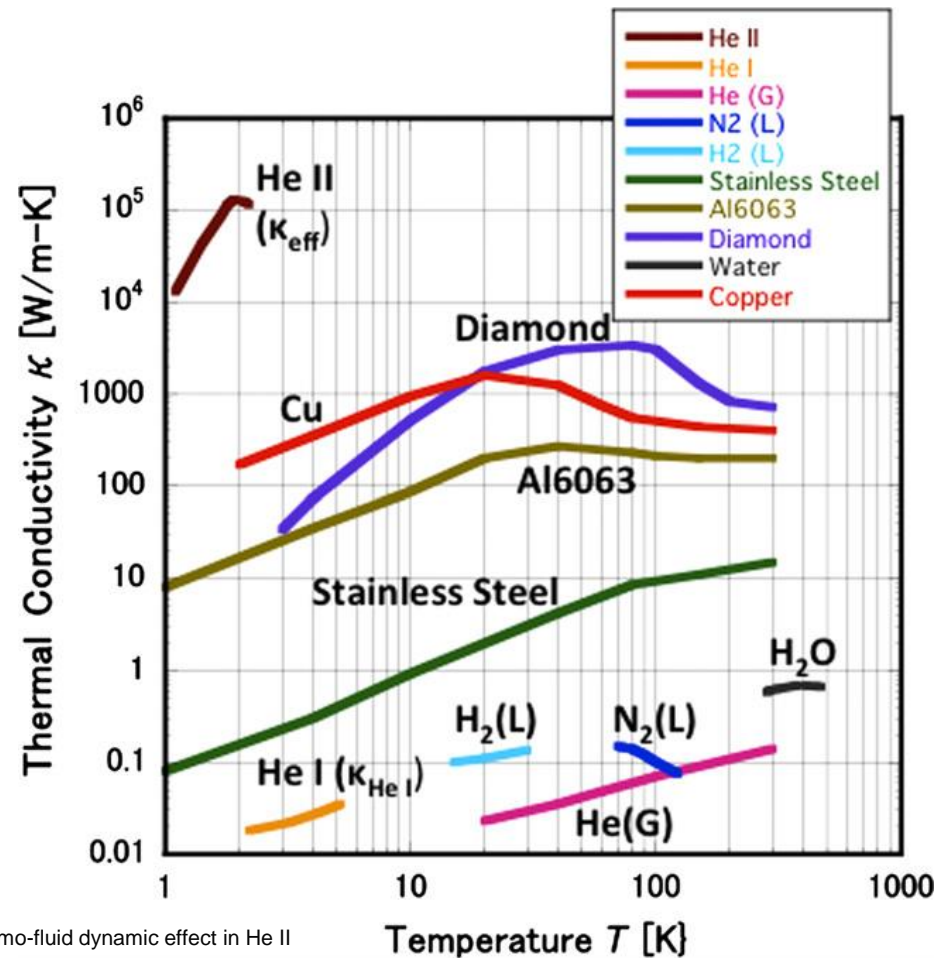
From He I to He II

Normal fluid helium => He I

- Like a standard fluid: viscosity etc.

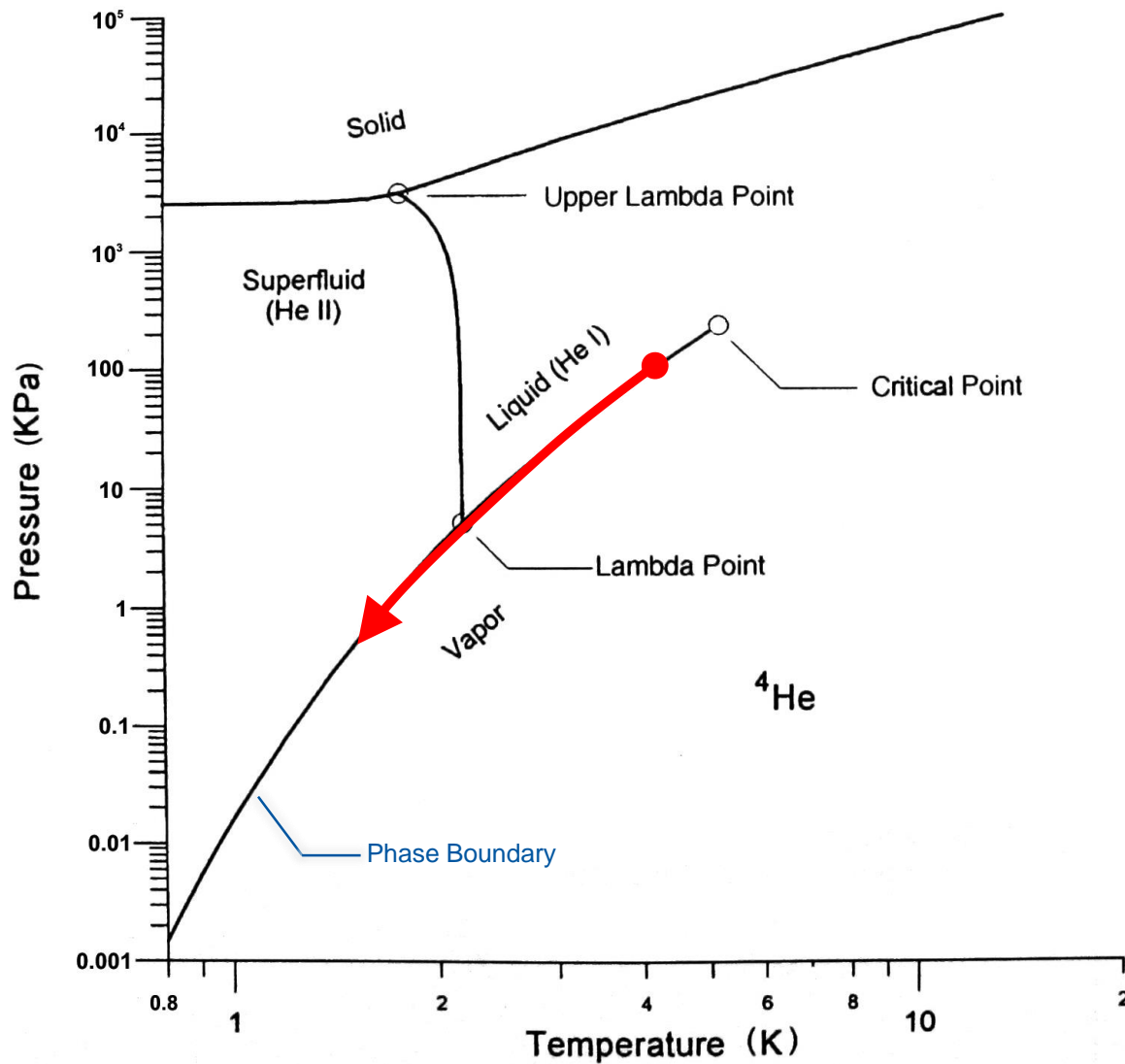
Superfluid helium => He II

- Temperature < 2.17 K
- Peak in heat capacity c_p at T_λ
- Very high thermal conductivity
- Low / vanishing viscosity



Murakami, Experimental study of thermo-fluid dynamic effect in He II cavitating flow, Cryogenics, 2012.

Phase diagram of ^4He

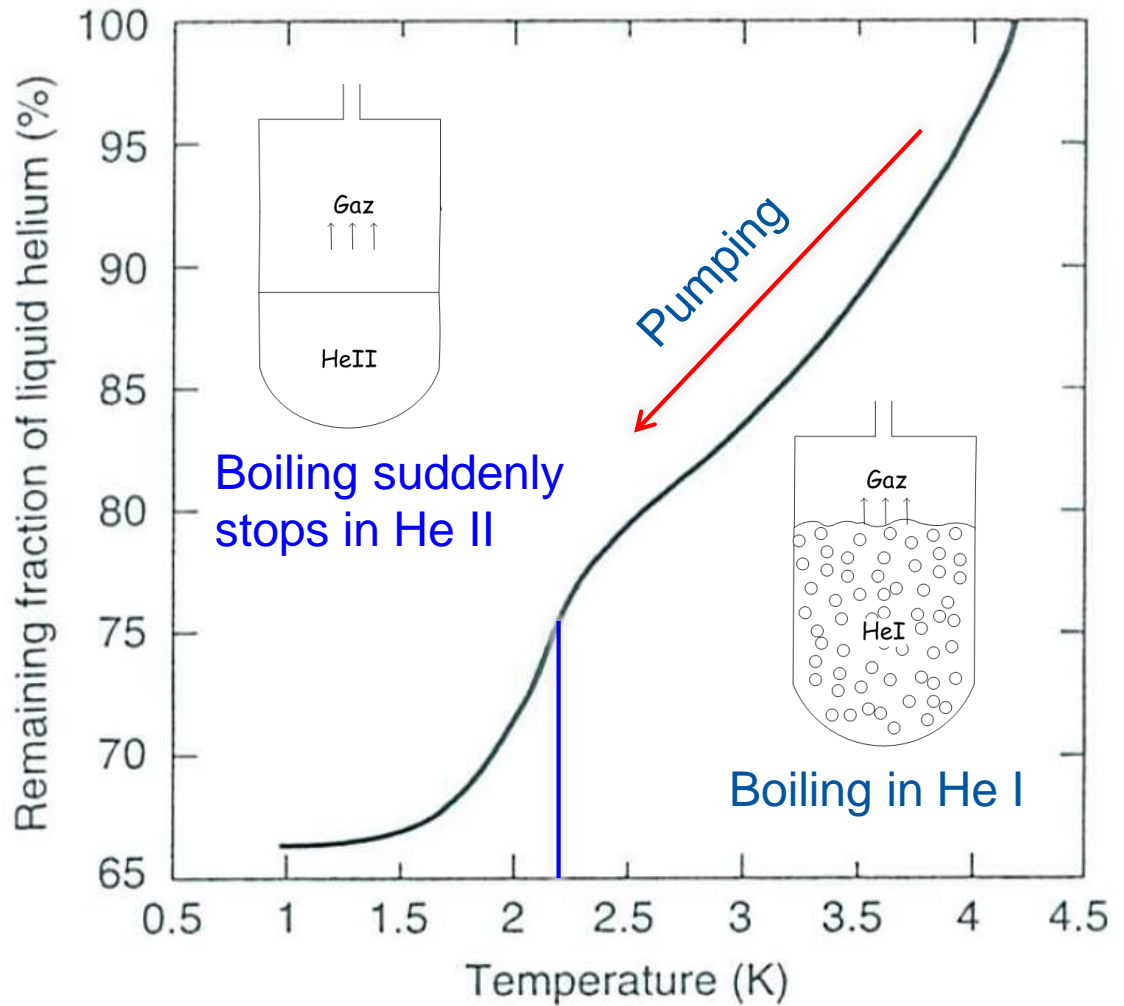
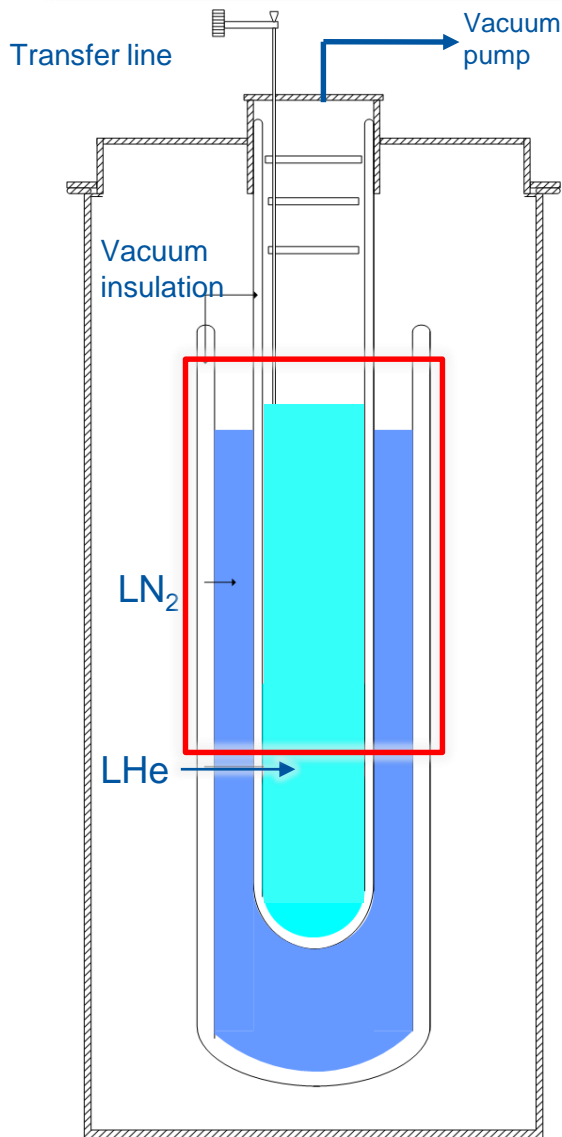


$$T_{\lambda} \approx 2.1768 \text{ K @}$$

$$p_{\lambda} \approx 50.41 \text{ mbar}$$

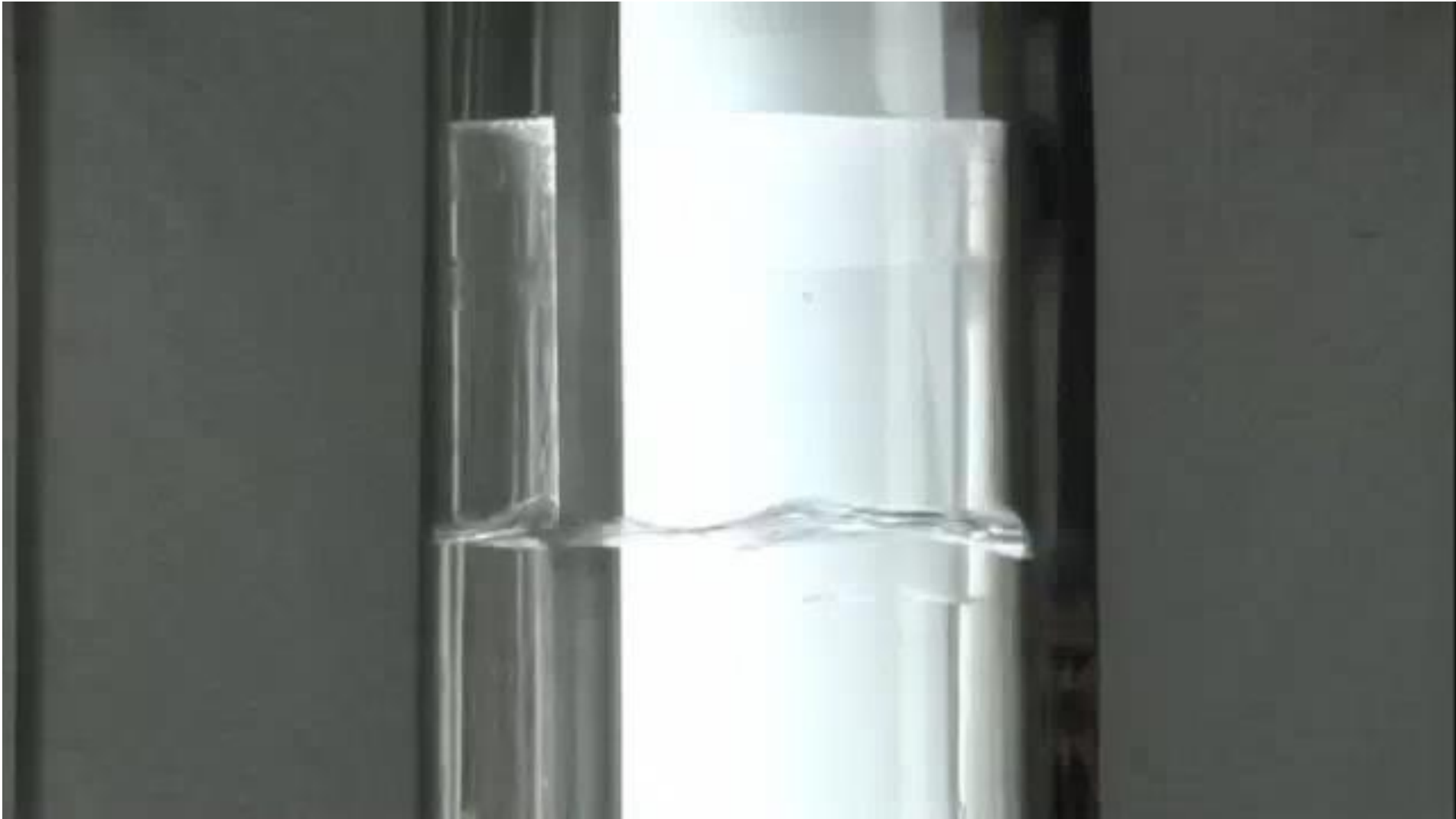
From Weisend, Handbook of Cryogenic Engineering, 1984.

Glass cryostat set-up



From Ekin, Experimental Techniques for Low Temperature Measurements, 2006.

Boiling effects during cooldown / Pumping on the He vapour

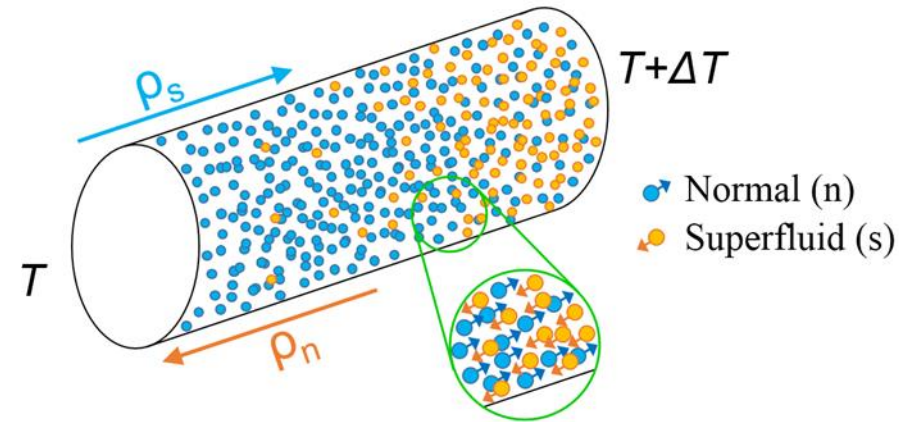
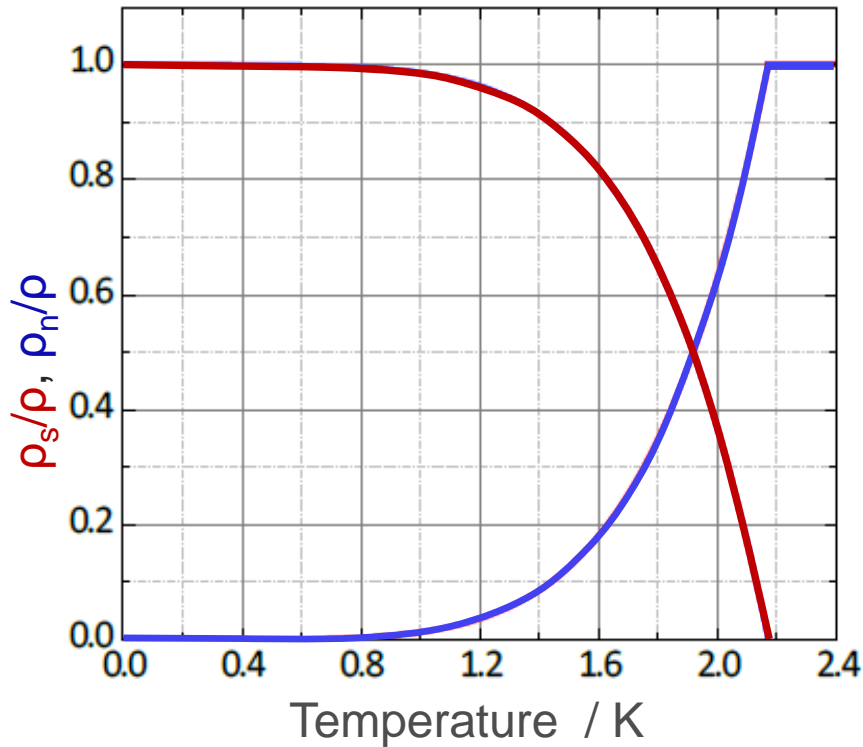


How to explain that unique behaviour ?

Two fluid **model** of L. Tisza:

He II is composed of two components

Two-fluid model of He II by Tisza, 1938



Superfluid component:

- no entropy: $S_s = 0$
- zero viscosity: $\eta_s = 0$

Normal component:

- carries total entropy: $S_n = S$
- finite viscosity: $\eta_n = \eta$

- ✓ Formal description of He II as the sum of a **normal** and a **superfluid** component.
- ✓ Ratio ρ_s/ρ_n depends on temperature

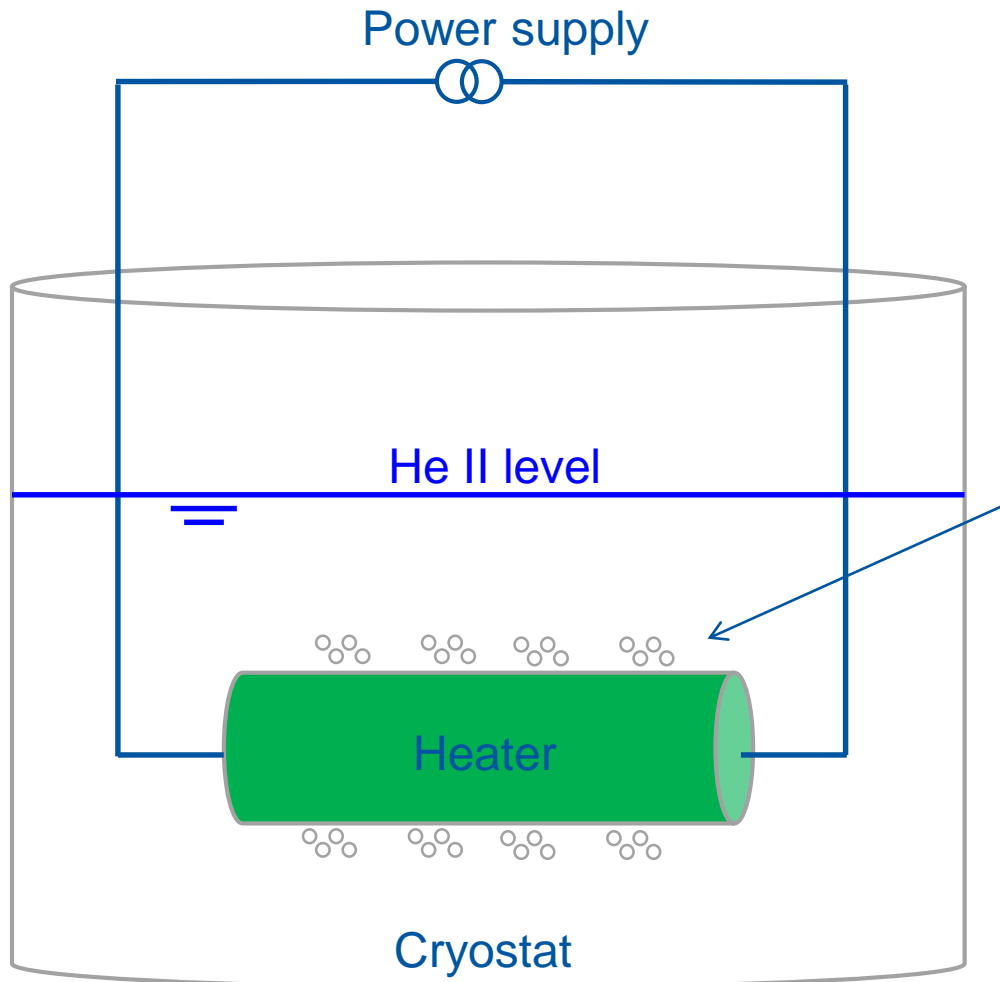
He II in practice

Superleak below T_λ



1963 movie by Alfred Leitner, Michigan State University

Critical heat flux in He II



Heat and mass flow are limited by a critical velocity:

$$v > v_{cr}$$

Superfluid behavior becomes non-linear (mutual friction)

$$k \downarrow \text{ and } \eta \uparrow$$

Formation of vapor bubbles at the surface of the heater

In He II re-condensation of the vapor

Surface tension let the bubbles implode

Implosion speed exceeds v_1

Shock wave \Rightarrow cavitation

Critical heat flux in He II ($T < T_\lambda$)



LHe I cooling ($T > T_\lambda$)



Concluding remarks

- Cryogenics serving superconducting systems is now part of all major accelerators and future projects.
- While advanced applications tend to favour “ $T < 2\text{ K}$ ”, many almost industrial applications are based on “ 4.5 K ” and R&D continues for “high temperature” applications.
- Even though cryogenic engineering follows well defined rules and standards, there are still variants depending on boundary conditions, project schedule ...
- I could only recommend that demonstrated experience is evaluated and adapted to specific requirements you may have.

Some references

- K. Mendelssohn, *The quest for absolute zero*, McGraw Hill (1966)
- R.B. Scott, *Cryogenic engineering*, Van Nostrand, Princeton (1959)
- G.G. Haselden, *Cryogenic fundamentals*, Academic Press, London (1971)
- R.A. Barron, *Cryogenic systems*, Oxford University Press, New York (1985)
- B.A. Hands, *Cryogenic engineering*, Academic Press, London (1986)
- S.W. van Sciver, *Helium cryogenics*, Plenum Press, New York (1986)
- K.D. Timmerhaus & T.M. Flynn, *Cryogenic process engineering*, Plenum Press, New York (1989)
- Proceedings of CAS School on Superconductivity and Cryogenics for Particle Accelerators and Detectors, Erice (2002)
 - U. Wagner, *Refrigeration*
 - G. Vandoni, *Heat transfer*
 - Ph. Lebrun, *Design of a cryostat for superconducting accelerator magnet*
 - Ph. Lebrun & L. Taviani, *The technology of superfluid helium*
- Proceedings of ICEC and CEC/ICMC conferences
- CERN, HSE, Cryogenic Safety courses 1-3

Thank you for your attention.

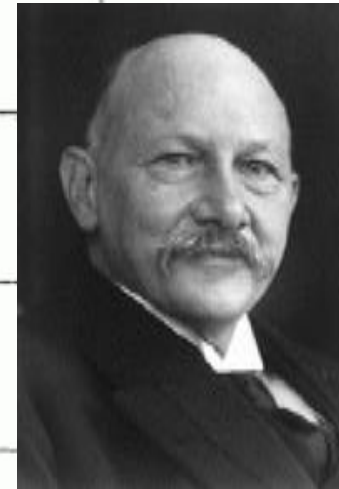
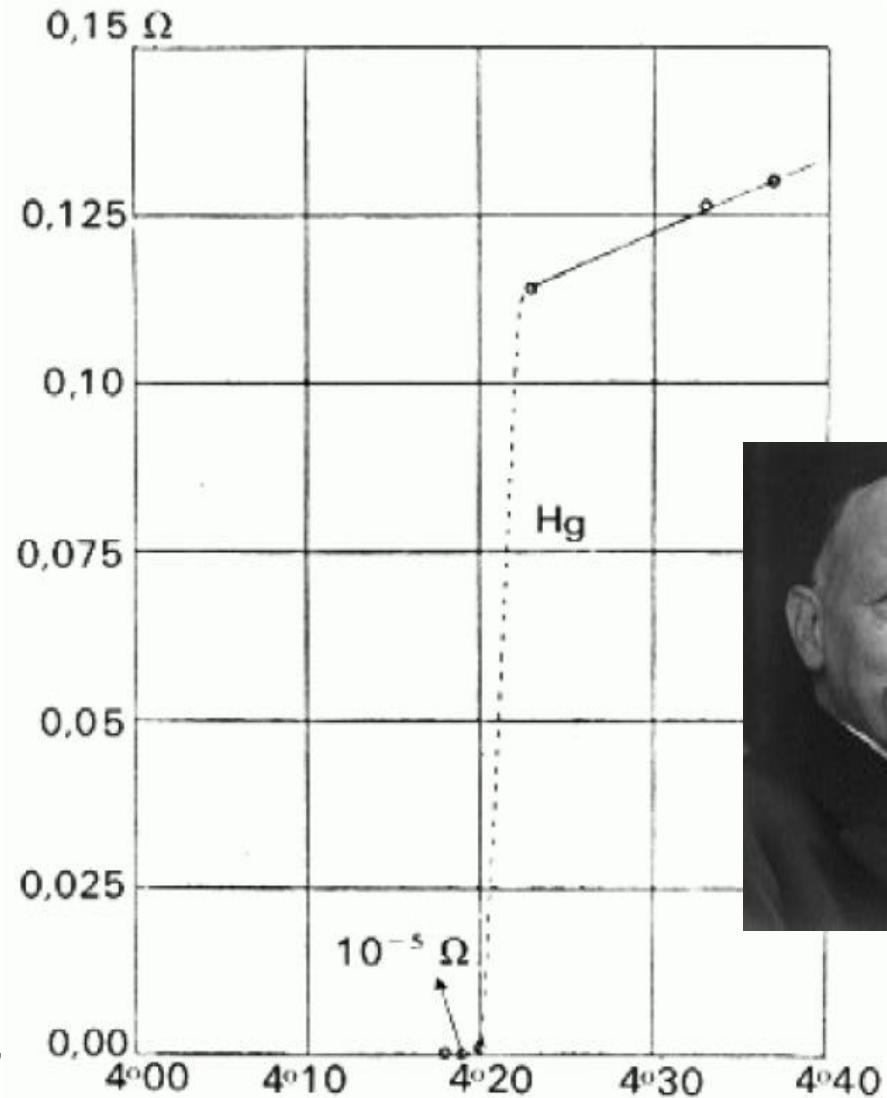


www.cern.ch

Spare slides

Superconductivity

- H. Kamerlingh Onnes
- Liquefied helium in 1909 at 4.2 K with 60 g He inventory
- Observed in 1911 for the first time superconductivity of mercury
- Nobel prize 1913

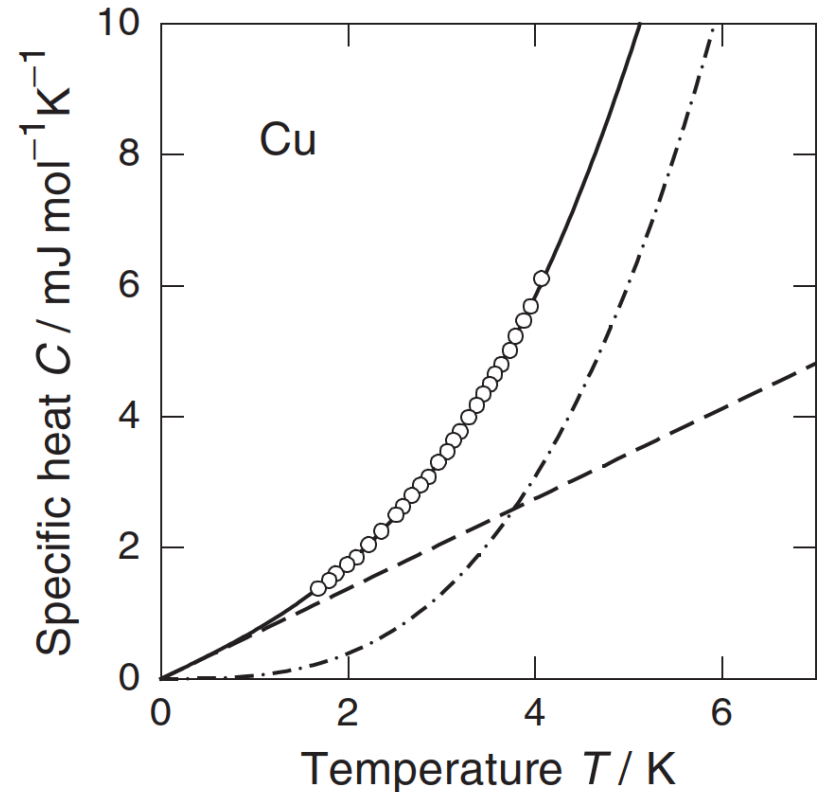
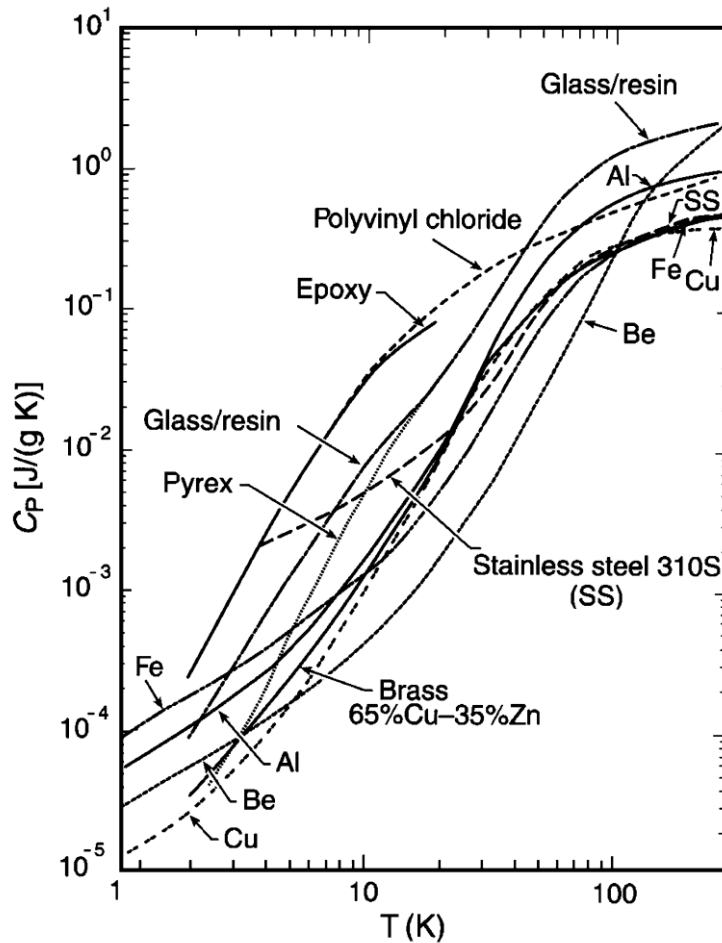


Historic graph showing the superconducting transition of mercury, measured in Leiden in 1911 by H. Kamerlingh Onnes.

Heat capacity of materials – what to cool?

Discrete lattice vibrations => Phonons

Metals have a contribution of free electron gas
=> dominant at very low temperature

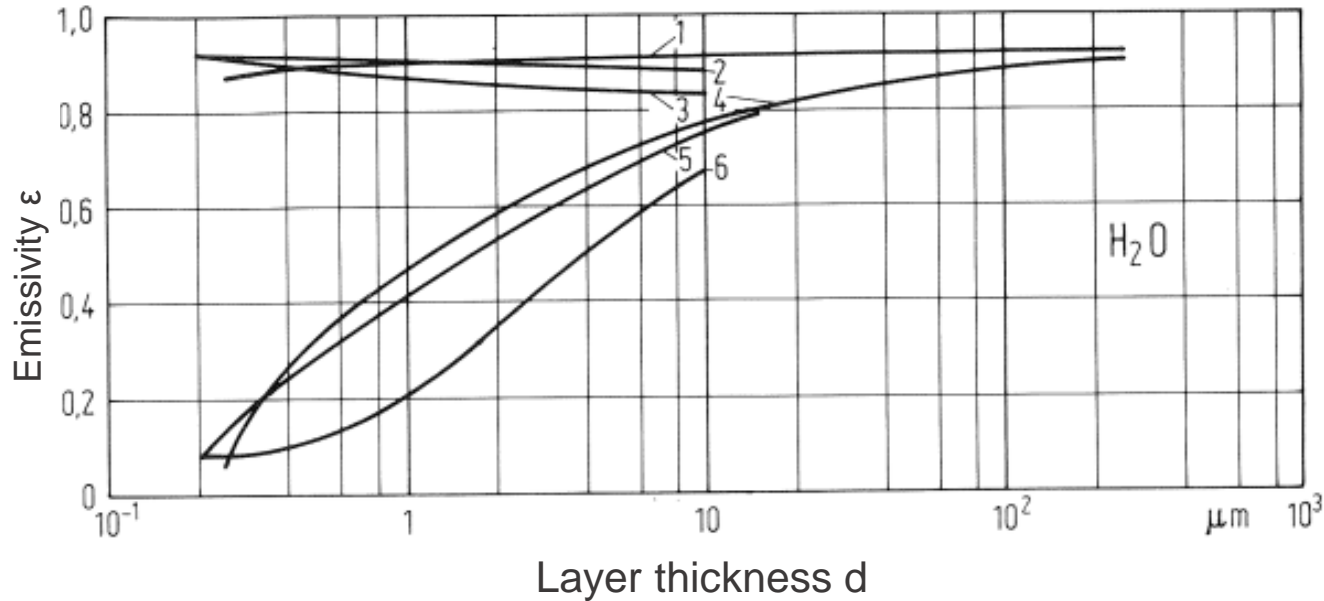


Source: Ekin, Experimental Techniques for Low-Temperature Measurements.

Source: Enss, Low temperature physics.

Emissivity of technical materials at low temperatures

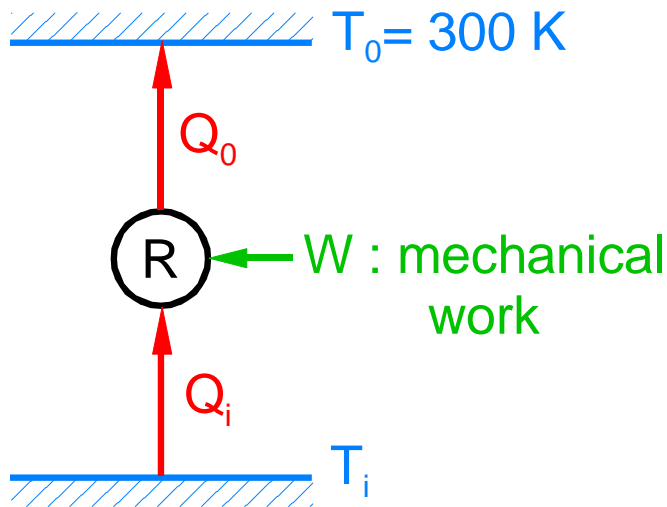
Emissivity of cold surface coated with water condensate dependent on layer thickness



	Cold surface, 77 K	Gas inlet
1	Al + Cat-a-Lac	Uniform over time, 0.06 Pa
2	Ni + Black Velvet 101-C10/3M	Sporadic
3	Ni + Black Velvet 101-C10/3M	Uniform over time, 0.1 Pa
4	Al, polished, $\epsilon = 0.07$	Uniform over time, 0.06 Pa
5	Ni, polished	Sporadic
6	Ni, polished	Uniform over time, 0.1 Pa

Source: Haefer, Kryovakuumtechnik, 1981

Thermodynamics of cryogenic refrigeration



First principle [Joule]

$$Q_0 = Q_i + W$$

Second principle [Clausius]

$$\frac{Q_0}{T_0} \geq \frac{Q_i}{T_i}$$

(= for reversible process)

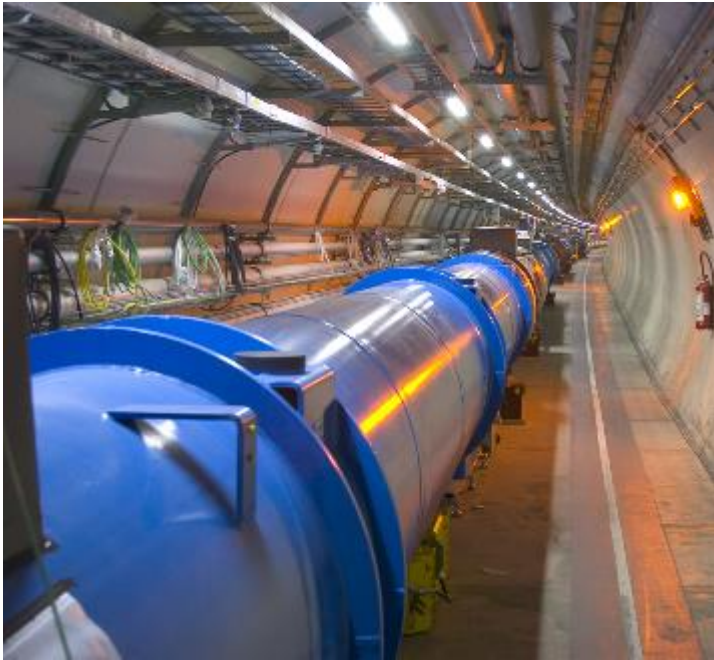
Hence, $W \geq T_0 \cdot \frac{Q_i}{T_i} - Q_i$ which can be written in different ways:

① $W \geq T_0 \cdot \Delta S_i - Q_i$ introducing entropy S as $\Delta S_i = \frac{Q_i}{T_i}$

② $W \geq Q_i \left[\left(\frac{T_0}{T_i} - 1 \right) \right]$ Carnot factor

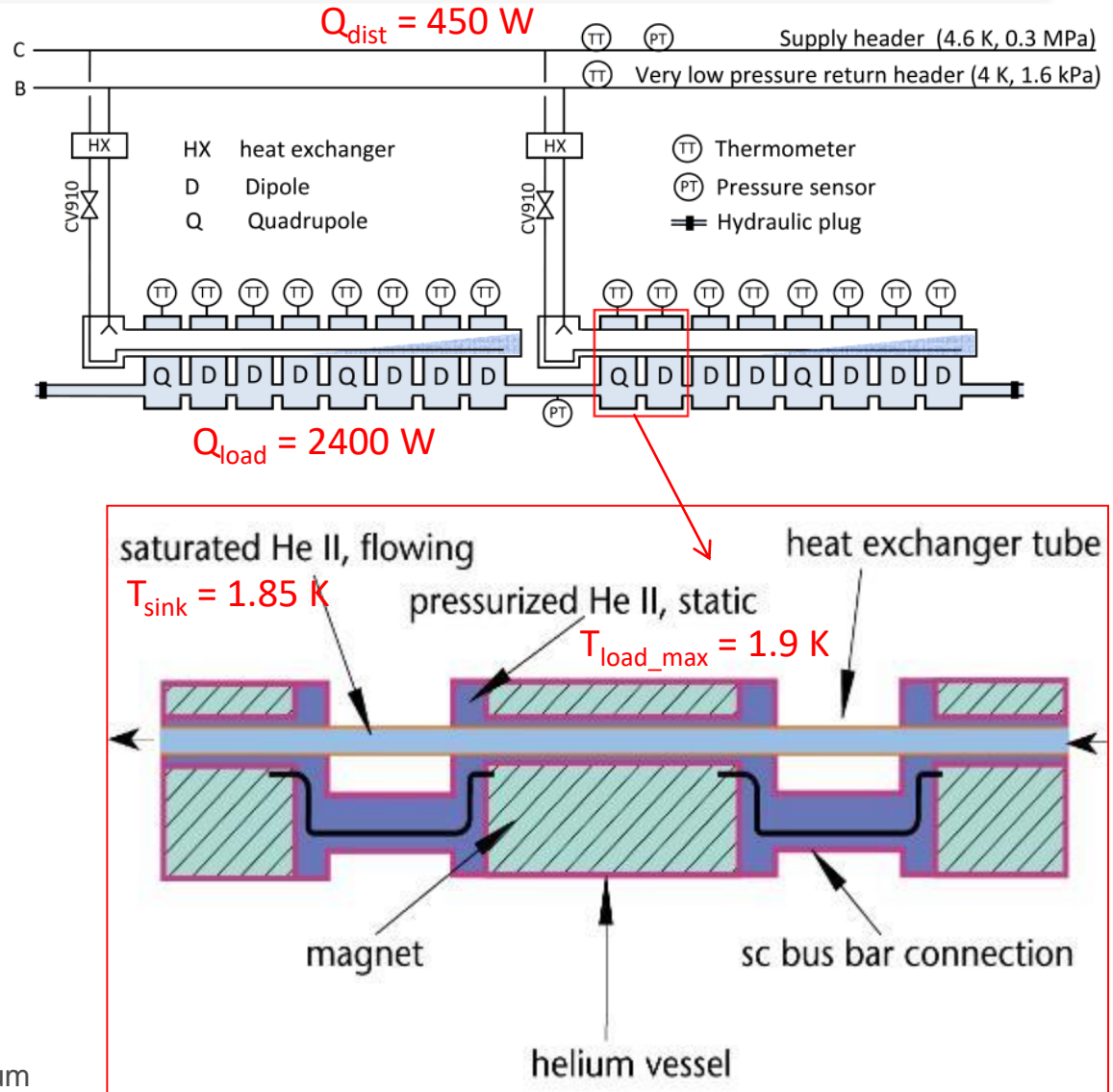
LHC cryogenic distribution scheme - QRL

Pressurized/saturated He II

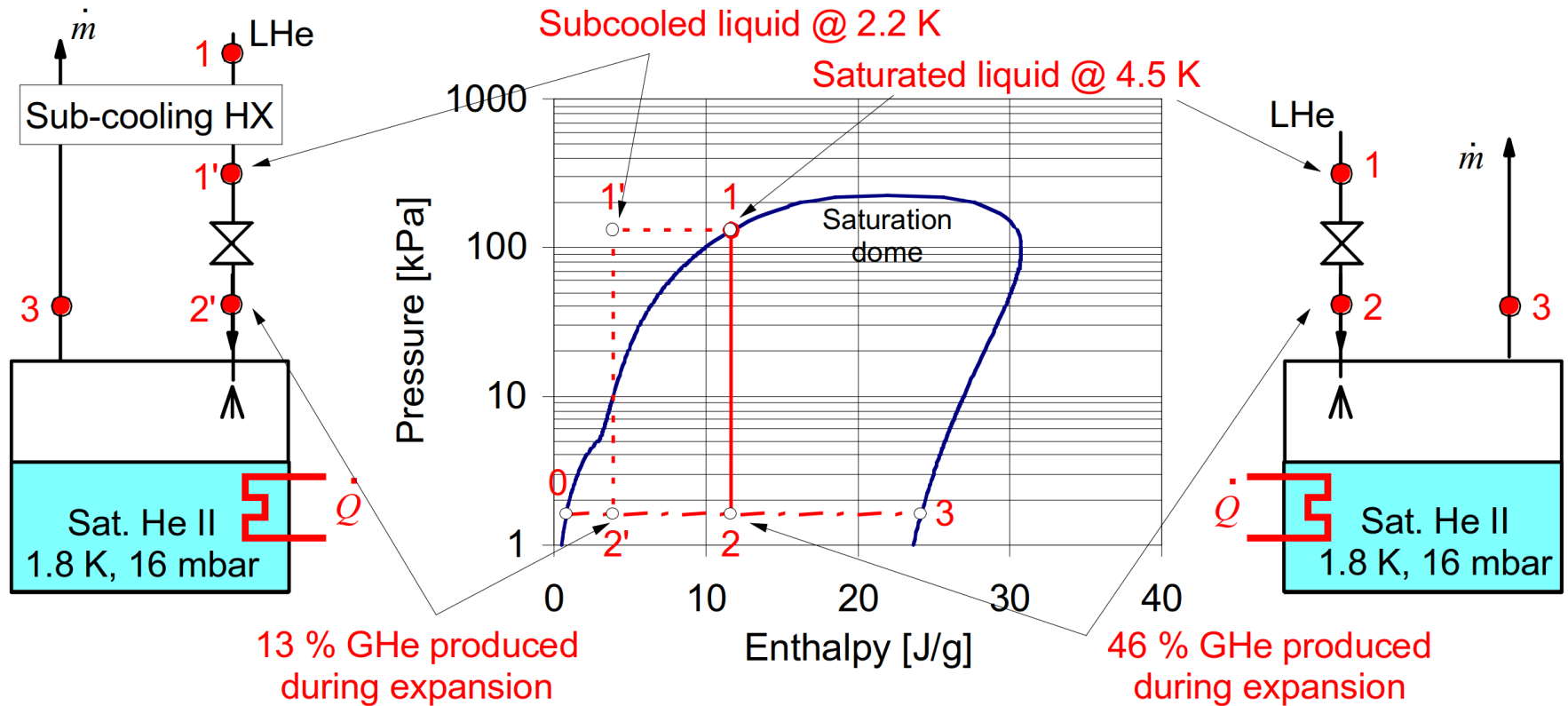


37'500 tons at 1.9 K

Source: Ph. Lebrun, Cooling with Superfluid Helium

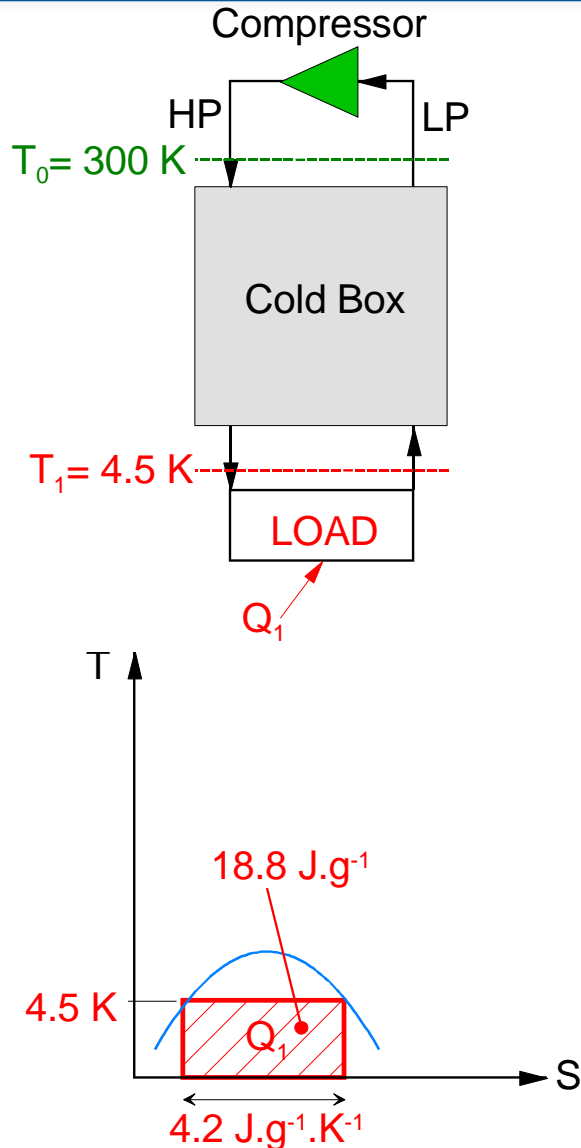


The effectiveness of J-T expansion

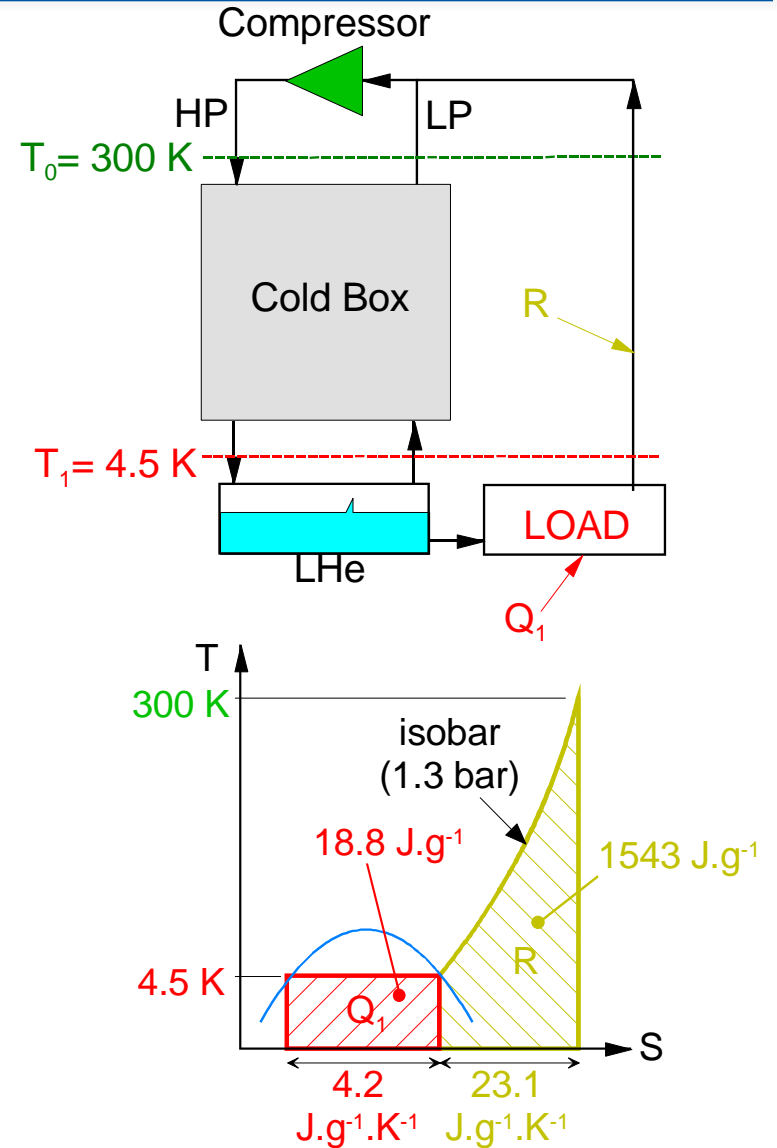


Source: Ph. Lebrun, Cooling with Superfluid Helium

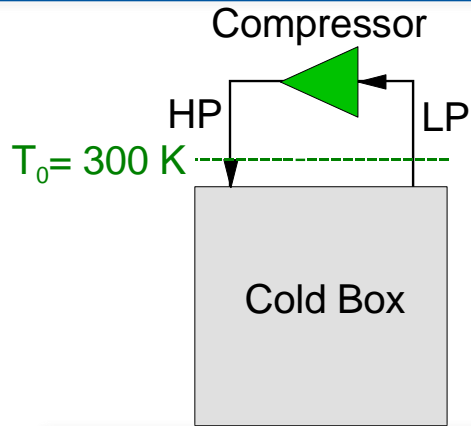
Refrigerator



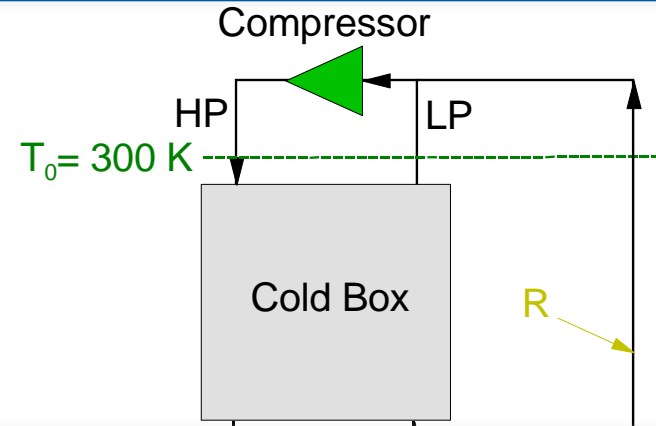
Liquefier



Refrigerator

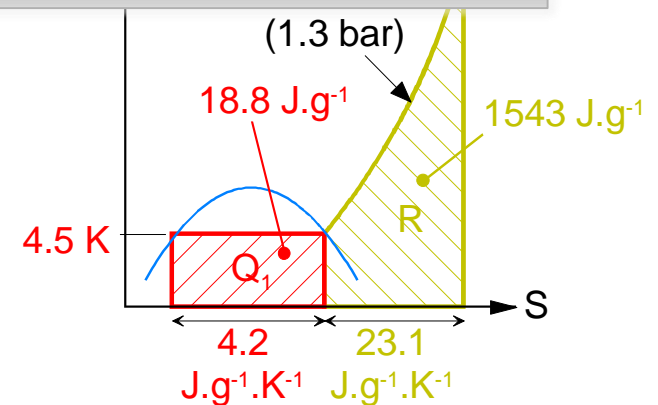
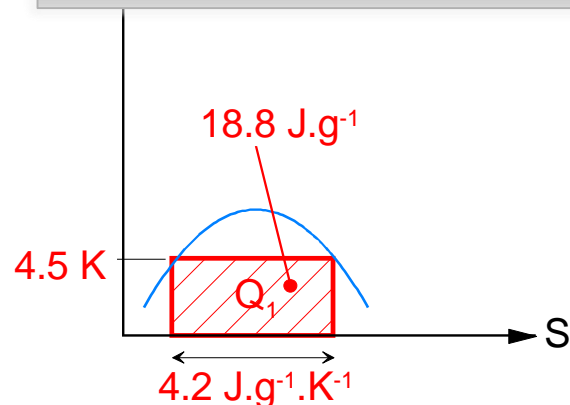


Liquefier



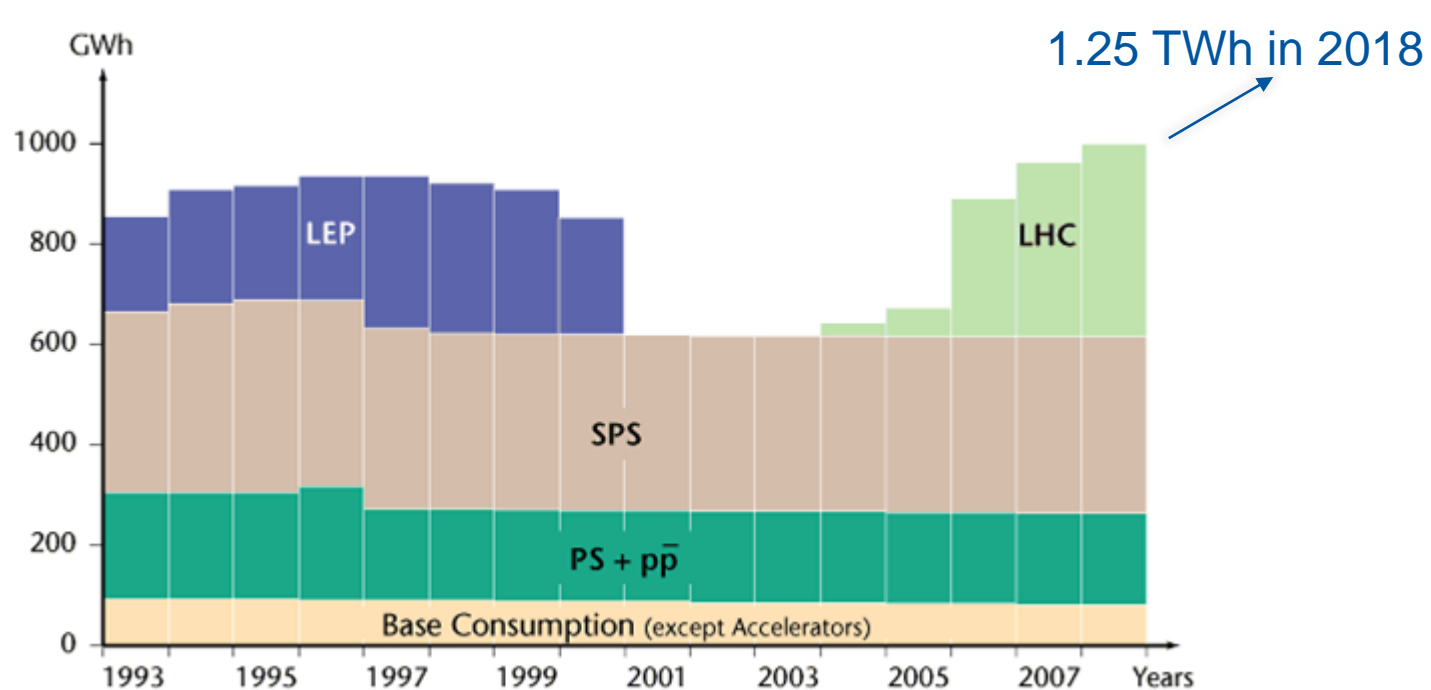
For refrigerators/liquefiers with the same efficiency:

$$1 \text{ g.s}^{-1} \text{ LHe} \equiv 100 \text{ W @ 4.5 K}$$



Energy consumption CERN, LHC and Cryo

CERN in total is around 200 MW with LHC contributing by 115 MW



Source: https://www.lhc-closer.es/taking_a_closer_look_at_lhc/0.energy_consumption

When the LHC is up and running the total average power for the whole CERN site will peak during July at about 180 MW of which:

- LHC cryogenics 27.5 MW (40 MW installed)
- LHC experiments 22 MW