

# Transverse stability in RCS and TESLA cavity Preliminary considerations

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# Single-turn stability limit in MC RCS from David Amorim. [2022-09-06 HEMAC RCS1 impedance resonator scan v2.pdf \(cern.ch\)](https://cern.ch/2022-09-06_HEMAC_RCS1_impedance_resonator_scan_v2.pdf)

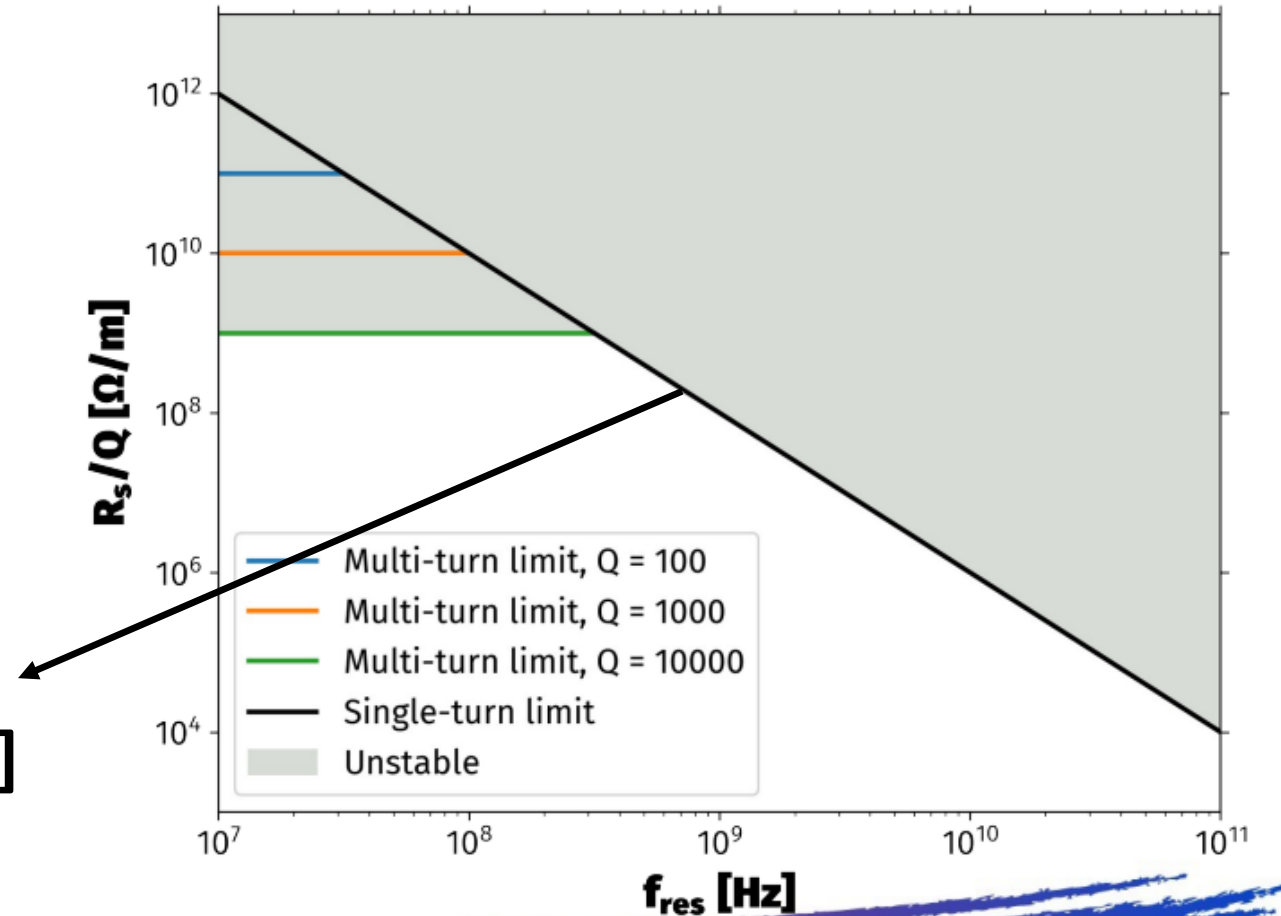
- Some RCS parameters:

- $f_{RF} = 1.3\text{GHz}$
- $C = 5990\text{m}$
- $E_{inj} = 63.1\text{GeV}/c$
- $dE = 14.2\text{ GeV}/c$  per turn
- $N_{turns} = 20$
- $V_{RF} = 20.1\text{ GV}$
- $\text{Sigma}_z = 25\text{mm}$

- Single turn stability limit:

$$R_s/Q * f^2 = 100 \text{ [M}\Omega/\text{m} * \text{GHz}^2]$$

Stability limit versus resonator parameters



# ILC cavity parameters, reminder from: [R/Q in linac SRF cavity parameter model for HEC RF system design \(cern.ch\)](http://cern.ch)

## An example: 1.3 GHz SRF cavity for the ILC

Proceedings of 2005 Particle Accelerator Conference, Knoxville, Tennessee

### DESIGN OF A LOW LOSS SRF CAVITY FOR THE ILC

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LL-shape cell parameters	
Frequency [MHz]	1300
Iris radius: a[mm]	30
Bpeak/Eacc [mT/(MV/m)]	3.6
R/Q [Ohm]	133.7
Loss factor [V/pC]	1.72
Length L[mm] ( $\lambda/2$ )	115.4
Iris thickness d[mm]	15
EaccMax [MV/m]@Bmax100mT(?tbc)	28

Do we need short range wake?  
Do we need anything else?

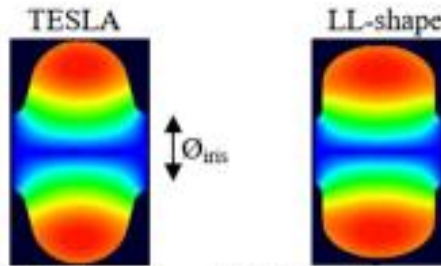


Table 1. RF parameters of both inner cells.

Parameter	Unit	TESLA	LL-Shape
$\phi_{iris}$	[mm]	70	60
$\kappa_{acc}$	[%]	1.9	1.52
$E_{peak}/E_{acc}$	-	1.98	2.36
$B_{peak}/E_{acc}$	[mT/(MV/m) <sup>2</sup> ]	4.15	3.61
Lorentz factor <sup>2</sup> , $k_L$	[Hz/(MV/m) <sup>2</sup> ]	-0.74	-0.81
R/Q	[ $\Omega$ ]	113.8	133.7
G	[ $\Omega$ ]	271	284
R/Q-G	[ $\Omega$ - $\Omega$ ]	30840	37970
$k_z(\sigma_z=1\text{mm})$	[V/(pC-cm <sup>2</sup> )]	0.23	0.38
$k_{\parallel}(\sigma_z=1\text{mm})$	[V/pC]	1.46	1.72

Table 3: FM and HOM data.

Mode	f [MHz]	(R/Q) <sup>2</sup> [ $\Omega/\text{cm}^2$ ]	Q <sub>ext</sub>
M: TM010-9	1300.00	1161	$8 \cdot 10^3$
D: TE111-7a	1717.15	5.0	$4 \cdot 10^2$
D: TE111-7b	1717.21	5.0	$5 \cdot 10^2$
D: TE111-8a	1738.12	3.0	$6 \cdot 10^2$
D: TE111-8b	1738.15	3.0	$8 \cdot 10^2$
D: TM110-2a	1882.15	3.4	$6 \cdot 10^3$
D: TM110-2b	1882.47	3.4	$6 \cdot 10^3$
D: TM110-4a	1912.04	4.6	$9 \cdot 10^3$
D: TM110-4b	1912.21	4.6	$1 \cdot 10^4$
D: TM110-5a	1927.10	15.6	$1.5 \cdot 10^4$
D: TM110-5b	1927.16	15.6	$1.5 \cdot 10^4$
D: TM110-6a	1940.25	12.1	$2 \cdot 10^4$
D: TM110-6b	1940.27	12.1	$2 \cdot 10^4$
M: TM011-6	2177.48	192	$10^4$
M: TM011-7	2182.81	199	$10^4$
D: 3-rd-1a	2451.07	31.6	$1 \cdot 10^5$
D: 3-rd-1b	2451.15	31.6	$2 \cdot 10^5$
D: 3-rd-1-2a	2457.04	22.2	$5 \cdot 10^4$
D: 3-rd-1-2b	2457.09	22.2	$5 \cdot 10^4$
D: 5-th-7a	3057.43	0.5	$3 \cdot 10^5$
D: 5-th-7b	3057.45	0.5	$3 \cdot 10^5$
D: 5-th-8a	3060.83	0.4	$8 \cdot 10^5$
D: 5-th-8b	3060.88	0.4	$9 \cdot 10^5$

Max R/Q ←

<sup>2</sup>n = 0 for monopoles, n = 2 for dipoles; M-monopole, D-dipole; a, b indicate polarizations.

# One HOM from LL ILC cavity and S-turn stability

- Some RF cavity parameters:
  - Active Acc. Gradient: 30 MV/m
  - Cavity length:  $L_{\text{cav}} \sim 1\text{m}$
  - $V_{\text{cav}}$ : 30MV
  - $N_{\text{cav}} = 20100/30 = \mathbf{670}$
- Max R/Q HOM:  $R/Q = 32 \text{ linac}\Omega/\text{cm}^2 \Rightarrow R_s/Q = R/Q/2 * c/\omega = \mathbf{3.1 \text{ k}\Omega/\text{m}}$  per cavity
- For 670 cavities:  $R_s/Q = \mathbf{2.1 \text{ M}\Omega/\text{m}}$
- $f = \mathbf{2.45 \text{ GHz}}$ ,
- $N_{\text{cav}} * R_s/Q * f^2 = \mathbf{12.6 [\text{M}\Omega/\text{m} * \text{GHz}^2]} < \mathbf{100}$ , Single turn stability limit from David
- **It is below stability limit by about factor 8 for one HOM.**
- **In fact, all HOMs must be taken into account for S-turn stability calculation**

# Stability for several HOMs

- Wake of single mode expressed as

$$W(t) = \frac{2\pi f_{res} R_s}{Q \sqrt{1 - \frac{1}{4Q^2}}} \exp\left(-\frac{2\pi f_{res}}{2Q} t\right) \sin\left(2\pi f_{res} \sqrt{1 - \frac{1}{4Q^2}} t\right)$$

- In SRF  $Q \ll 1$ , and for short bunch  $t_{max} \ll 1/f_{res}$

$$W(t) = \omega_{res} \frac{R_s}{Q} \omega_{res} t$$

- Stability limit:  $R_s/Q * f_{res}^2 = 100 \Rightarrow$

$$\frac{dW(t)}{dt} = \omega_{res} \frac{R_s}{Q} \omega_{res} = 4\pi^2 100 \left[\frac{M\Omega}{m} GHz^2\right]$$

- In fact, Stability limit ==  $\frac{dW(t)}{dt} = const$

- In the case of N modes:

$$W(t) = \sum_i W_i(t)$$

$$\frac{dW(t)}{dt} = \sum_i \frac{dW_i(t)}{dt}$$

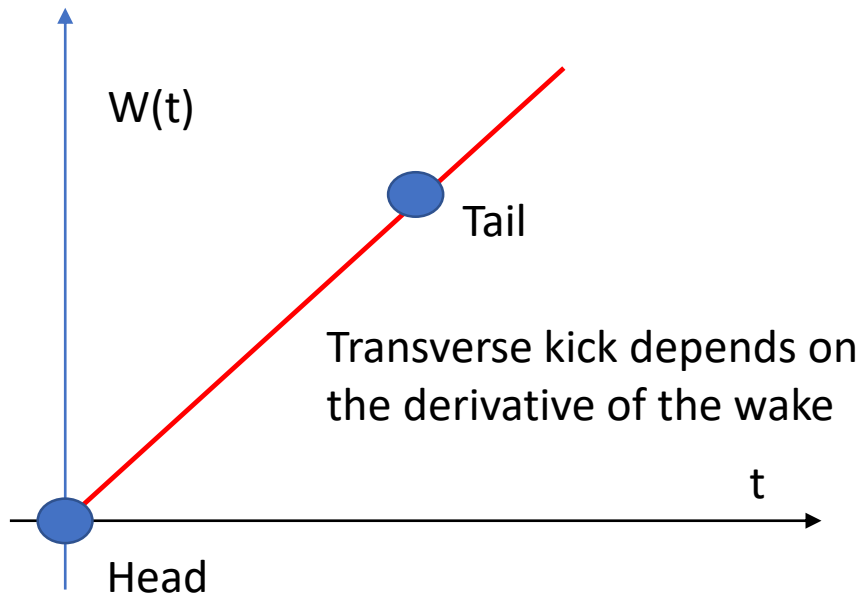
- Stability limit for total S-turn wake:

$$\sum_i \frac{dW_i(t)}{dt} = \sum_i \left[\frac{R_s}{Q} \omega_{res}^2\right]_i < 4\pi^2 100 \left[\frac{M\Omega}{m} GHz^2\right]$$

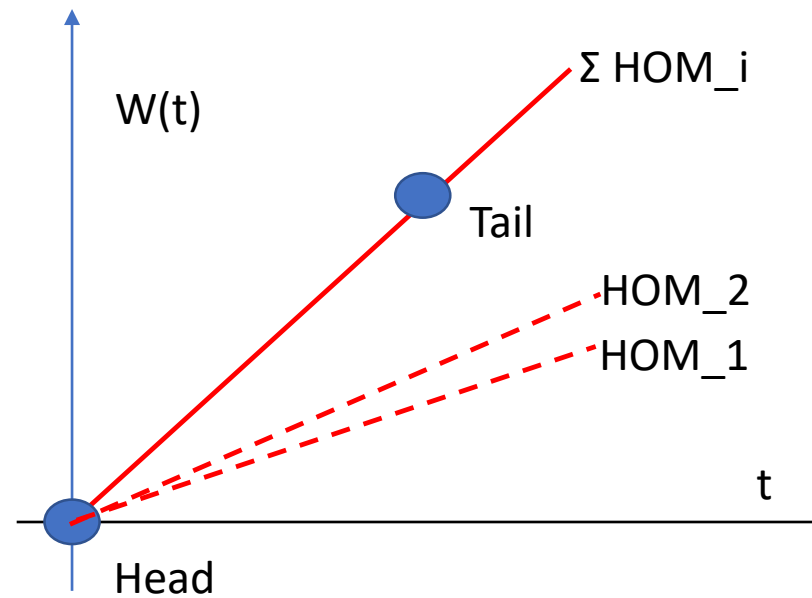
- Taking into account the bunch spectrum limit the number of relevant HOMs in the sum

# Physical interpretation of stability limit

$$W(t) = \omega_{res} \frac{R_s}{Q} \omega_{res} t$$



$$W(t) = \sum_i W_i(t)$$



# Stability for several HOMs up to 3 GHz

mode	f[GHz]	R/Q[linacOhm/cm <sup>2</sup> ]	Rs/Q[kohm/m]	Ncav*Rs/Q[Mohm/m]	Rs/Q*f <sup>2</sup> [MOhm/m*GHz <sup>2</sup> ]
D:TE111-7	1.717	5	0.695202139	0.465785433	1.373176912
D:TE111-8	1.738	3	0.412081268	0.27609445	0.833983043
D:TE110-2	1.882	3.4	0.431291291	0.288965165	1.023492653
D:TE110-4	1.912	4.6	0.574356228	0.384818673	1.406798553
D:TE110-5	1.927	15.6	1.932654732	1.29487867	4.808310518
D:TE110-6	1.94	12.1	1.489001143	0.997630766	3.75468315
<b>D:3rd-1</b>	<b>2.451</b>	<b>31.6</b>	<b>3.077904652</b>	<b>2.062196117</b>	<b>12.38843902</b>
D:3rd-2	2.457	22.2	2.157045016	1.445220161	8.724575883
D:5th-7	3.057	0.5	0.039046846	0.026161387	0.244484672
D:5th-8	3.06	0.4	0.031206852	0.020908591	0.195779679
					<b>34.75372408</b>

**This is closer to the stability limits calculated by David:  $Rs/Q * f^2 = 100$**

**BUT it is still factor 3 lower. More detailed studies needed**

# Closed expression of total Transverse wake.

- Karl Bane (2003, SLAC-PUB-9663)
- Wake per meter length

$$W_x(s) = \frac{4Z_0cs_0}{\pi a^4} \phi(s) \left[ 1 - \left( 1 + \sqrt{\frac{s}{s_0}} \right) \exp \left( -\sqrt{\frac{s}{s_0}} \right) \right], \quad (15)$$

- Derivative of the wake
- per meter length :
- Total wake of 670 cavities:

$$s_0 = 0.169 \frac{a^{1.79} g^{0.38}}{L^{1.17}} \cdot \quad s_0 = 1.6 \text{mm} ! \quad (16)$$

$$\frac{dW_x(s)}{ds} = \frac{4Z_0c}{\pi a^4} e^{-\sqrt{s/s_0}} \quad \frac{dW_x(0)}{ds} = \frac{4Z_0c}{\pi a^4} \quad \frac{dW_x(0)}{dt} = \frac{4Z_0c^2}{\pi a^4}$$

$$\frac{dW(0)}{dt} L = \frac{4Z_0c^2L}{\pi a^4} \quad L = L_{cav} N_{cav} \quad L = 670m \quad a = 30mm \quad \frac{4Z_0c^2L}{\pi a^4} = 36000 \frac{M\Omega}{m} GHz^2$$

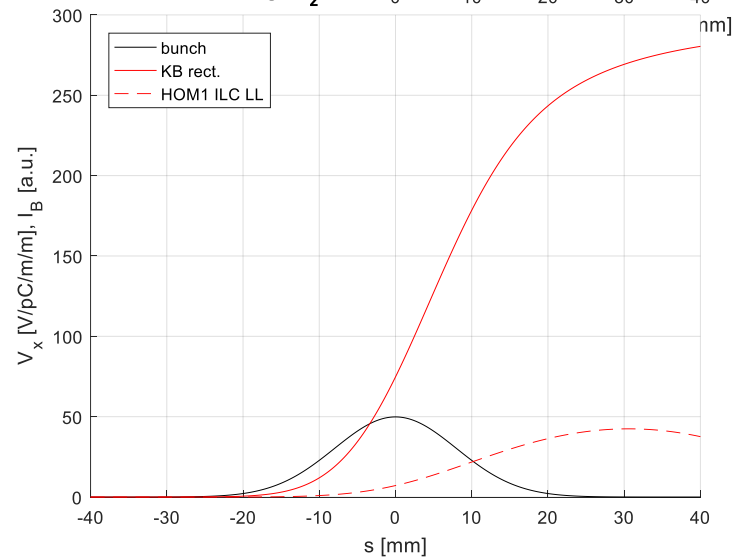
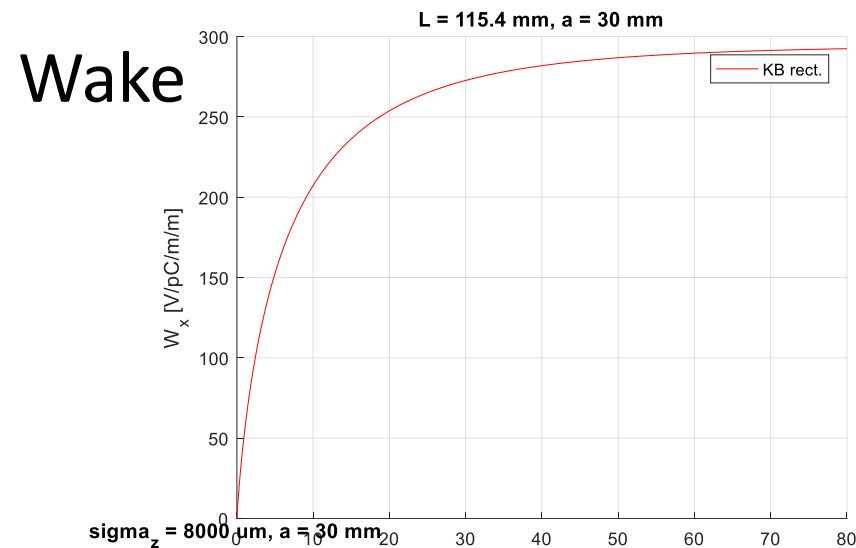
- Stability limit:

$$4\pi^2 100 \left[ \frac{M\Omega}{m} GHz^2 \right] = 3950 \left[ \frac{M\Omega}{m} GHz^2 \right] \quad \text{The wake derivative is about factor 9 larger than stability limit. Hm!?!}$$

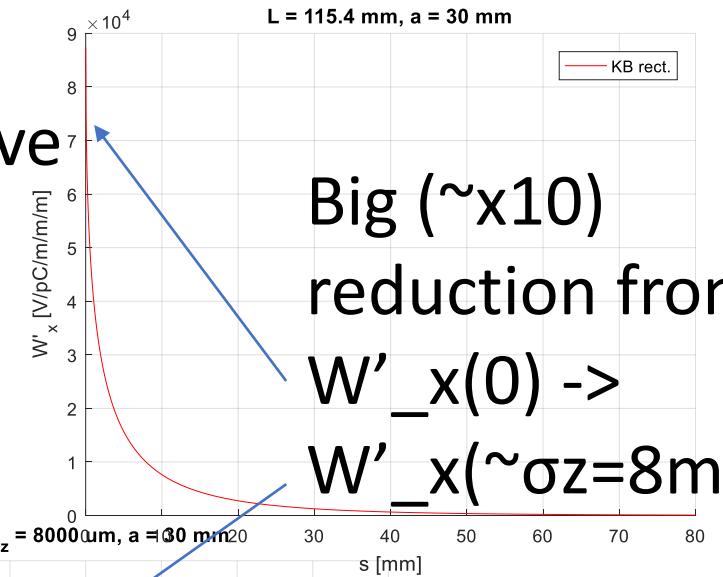
- Big discrepancy between KB model and HOM sum. Probably due to KB model applicability for  $s \ll s_0 = 1.6\text{mm}$ , where derivative is very high and for  $s > s_0$  it goes down -> less kick on the witness particle
- **Nevertheless KB model can be used for beam dynamic simulations where  $W_x$  will be convoluted with realistic bunch distribution**



# KB wake and discrepancy with HOM estimate



Wake derivative



Big ( $\sim x10$ )  
reduction from  
 $W'_x(0) \rightarrow$   
 $W'_x(\sim \sigma_z = 8 \text{ mm})$

