



Environmental noise monitoring at AdV+

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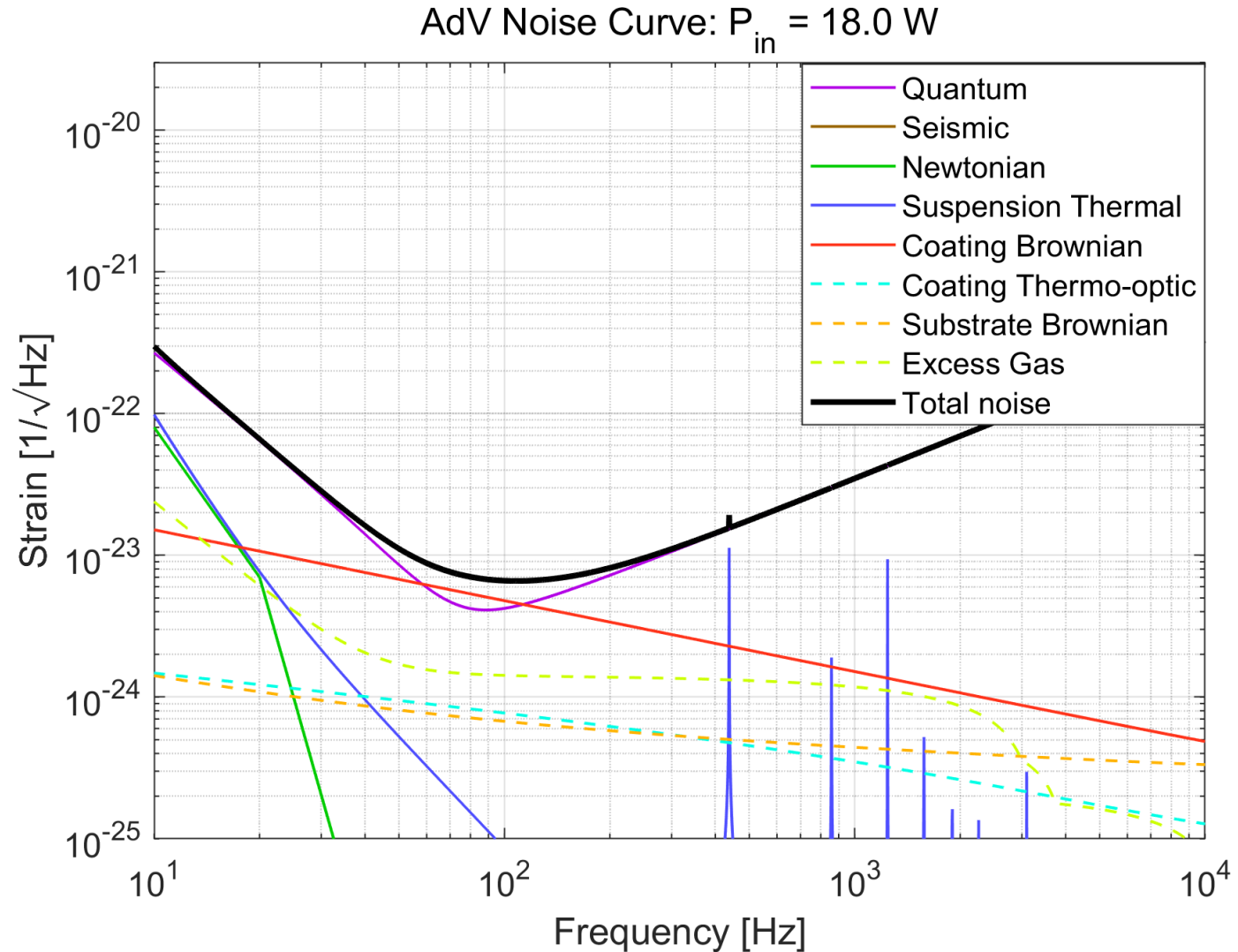
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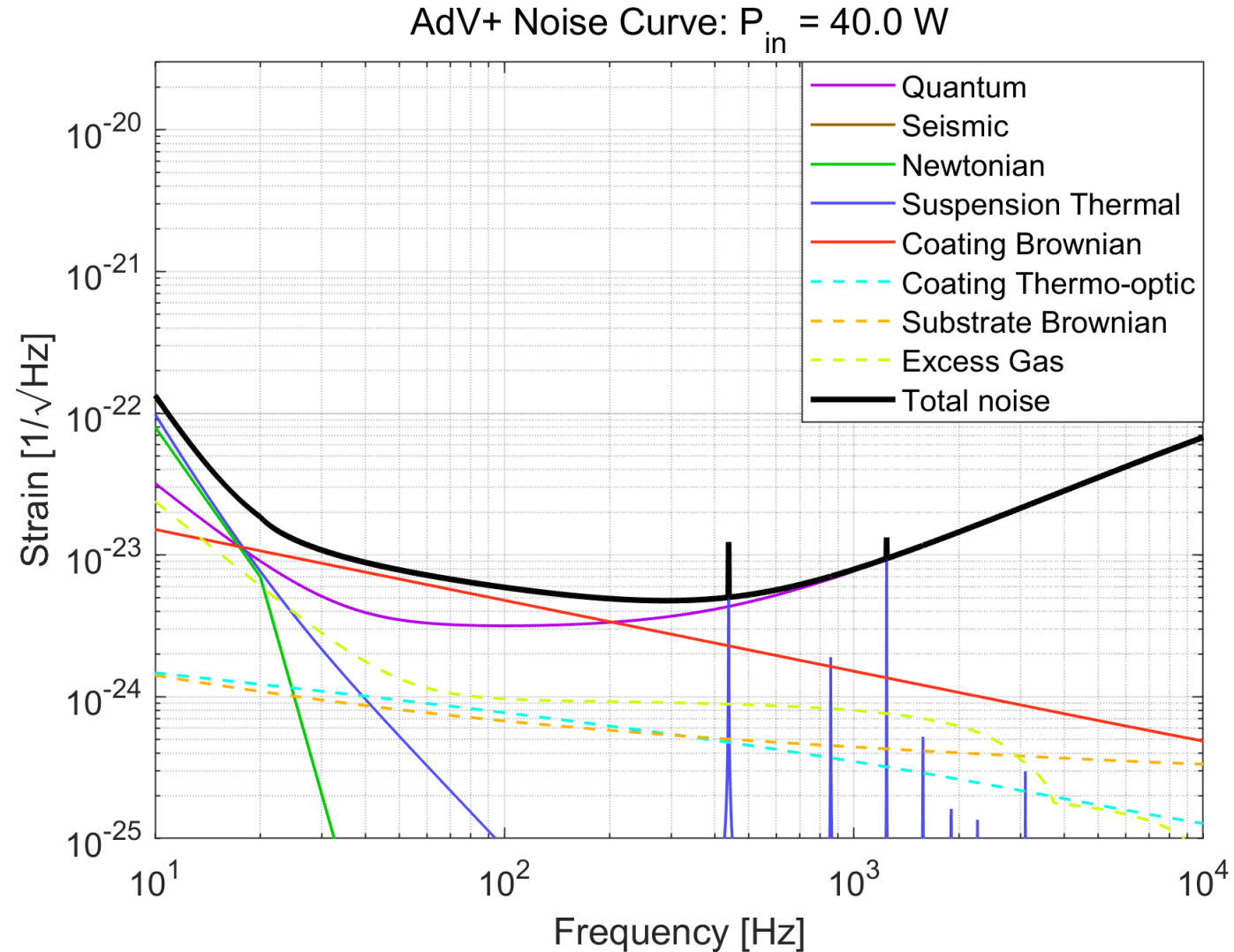
AdV Noise budget

- Radiation pressure noise and shot noise were the fundamental limits to the detector sensitivity during O3



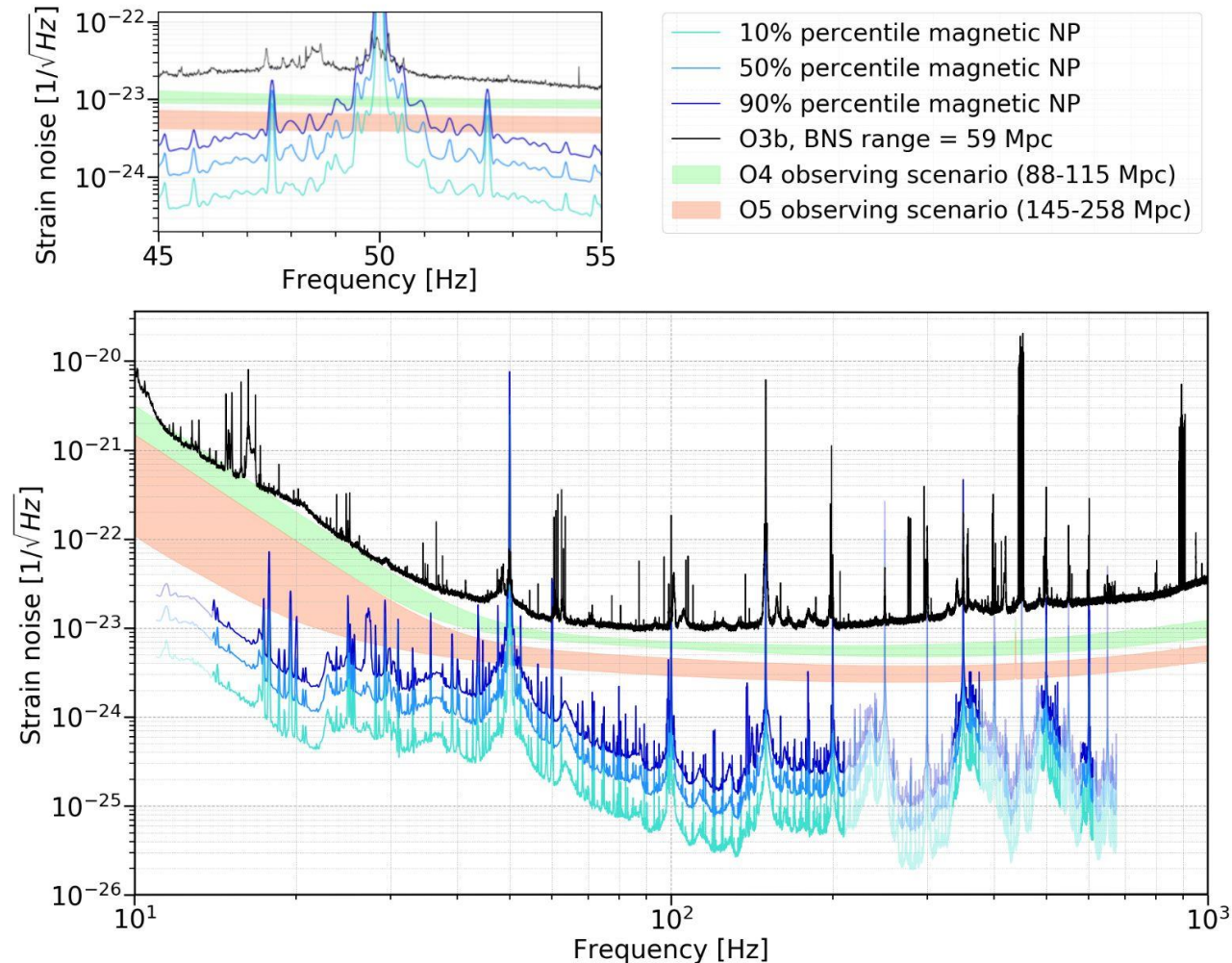
AdV+ Noise budget

- Newtonian noise is expected to have dominant contribution to the O4b sensitivity (lower limit)



AdV+ Magnetic noise projection

- Magnetic noise is expected to limit several frequency bands during O5 ([Fiori et al, 2020](#))



Newtonian noise - fundamentals

- Mirror acceleration

- $\delta \vec{a}(\vec{r}_0, t) = G \int dV \rho(\vec{r}) \times \frac{1}{|\vec{r} - \vec{r}_0|^3} \left(\xi(\vec{r}, t) - 3 \left(\vec{e}_{rr_0} \xi(\vec{r}, t) \right) \right) \vec{e}_{rr_0},$

- where $\xi(\vec{r}, t)$ is the seismic displacement field, ρ the density

- and $\vec{e}_{rr_0} = (\vec{r} - \vec{r}_0)/|\vec{r} - \vec{r}_0|$

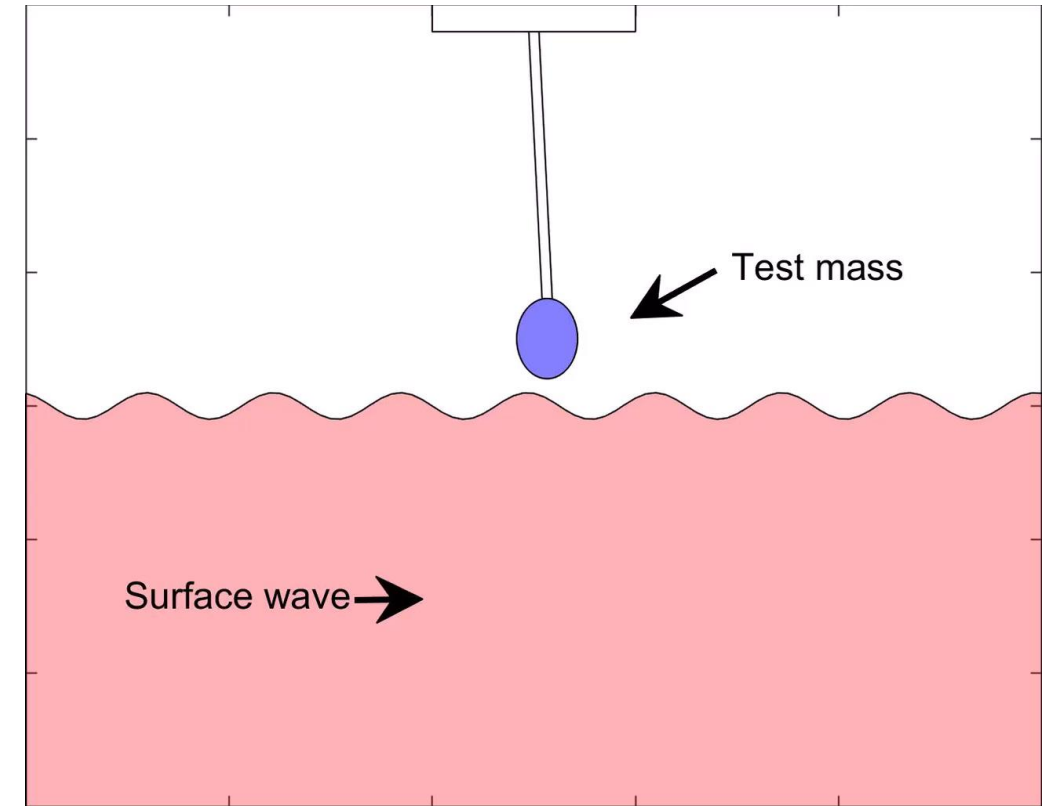
- Relies on finite element/difference simulations of elastic wave equation
 - Elastic properties of the medium and the noise source properties need to be known

- For surface detectors, the linear dependence of NN and seismic surface displacement allows for designing a Wiener filter given by the residual

- $R(\omega) = 1 - \frac{\vec{C}_{SN}(\omega) \cdot (\vec{C}_{SS}(\omega))^{-1} \cdot \vec{C}_{NS}(\omega)}{C_{NN}(\omega)},$ where $\vec{C}_{SN}, \vec{C}_{SS}, \vec{C}_{NN},$

- correspond to the cross and auto-spectral densities between observed seismic noise and 'expected' Newtonian noise

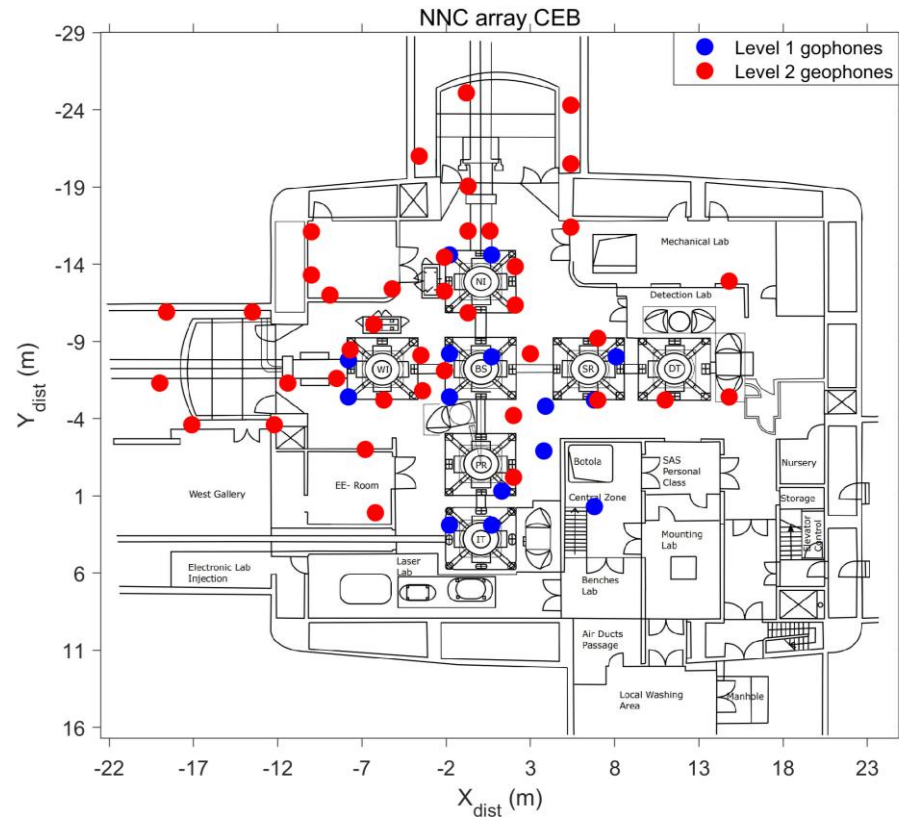
- ([Badaracco & Harms 2019](#))



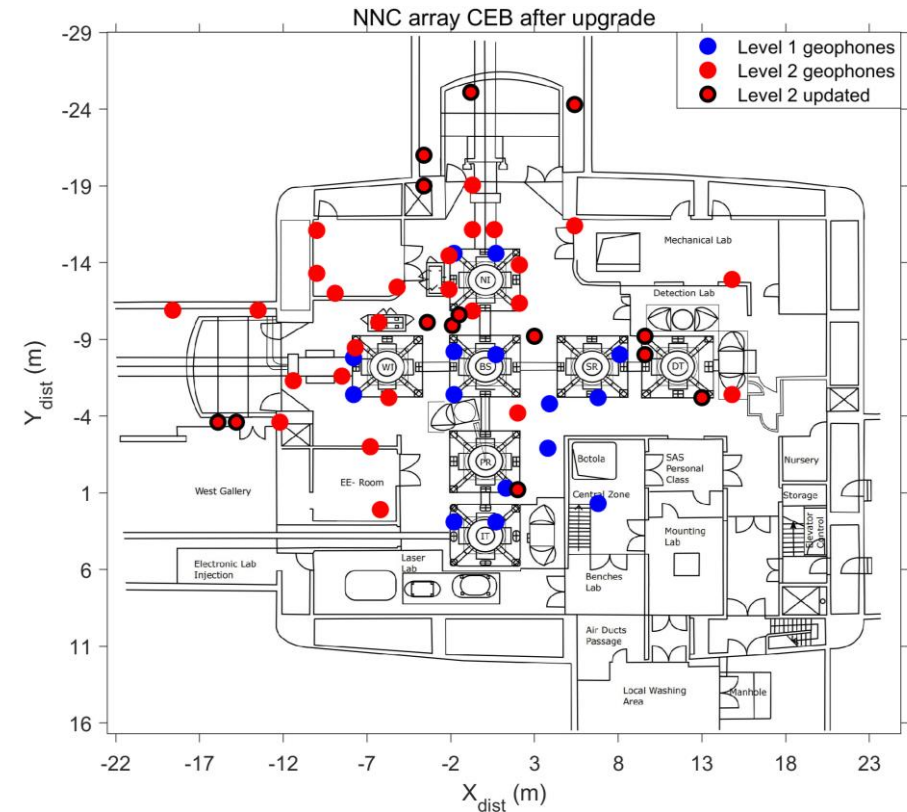
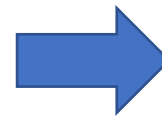
A toy representation of seismic surface wave inducing mirror motion due to gravitational coupling, $v = 25\text{m/s}$ $f = 20\text{ Hz}$

Newtonian noise cancellation – Central Building Array layout

- A total of 55, 5 Hz geophones deployed in the central building (CEB)
 - 15 geophones level 1
 - 40 geophones level 2
- Station positions were updated in May 2022 for optimal Newtonian noise cancellation
 - Data acquired continuously at 500 sps and integrated with Virgo DAQ



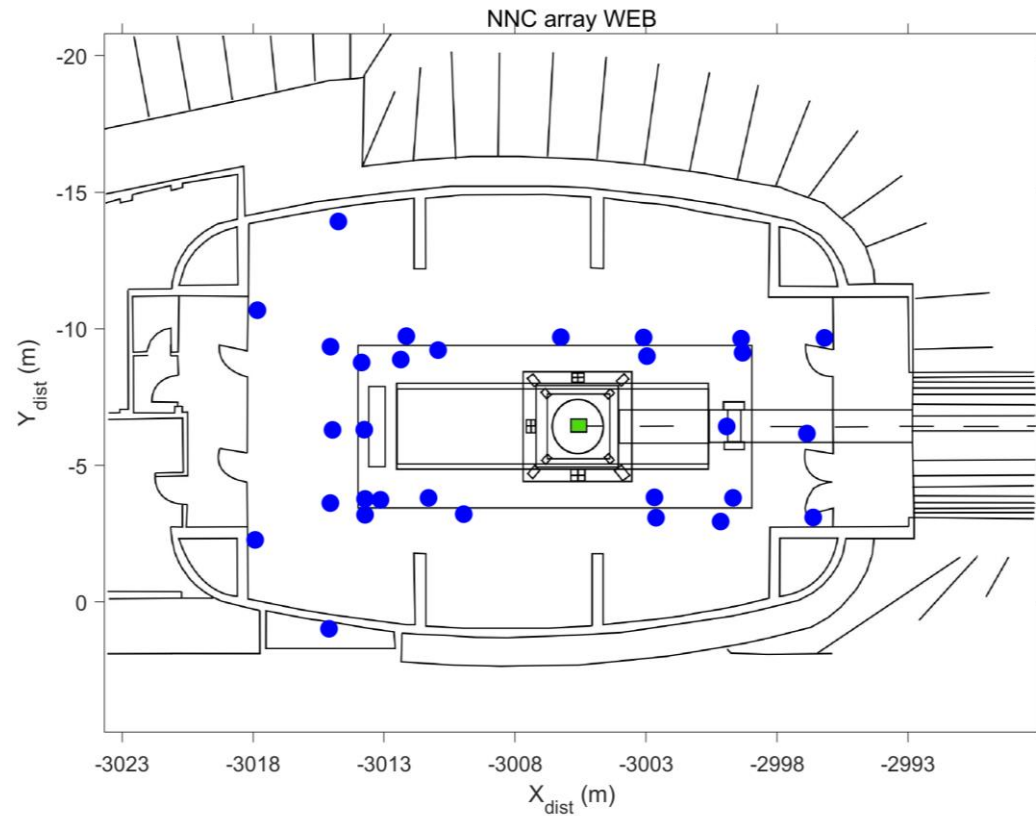
*Geophone locations in the CEB prior to the upgrade in May 2022;
The blue and the red dots represent the level 1 and level 2
geophones respectively*



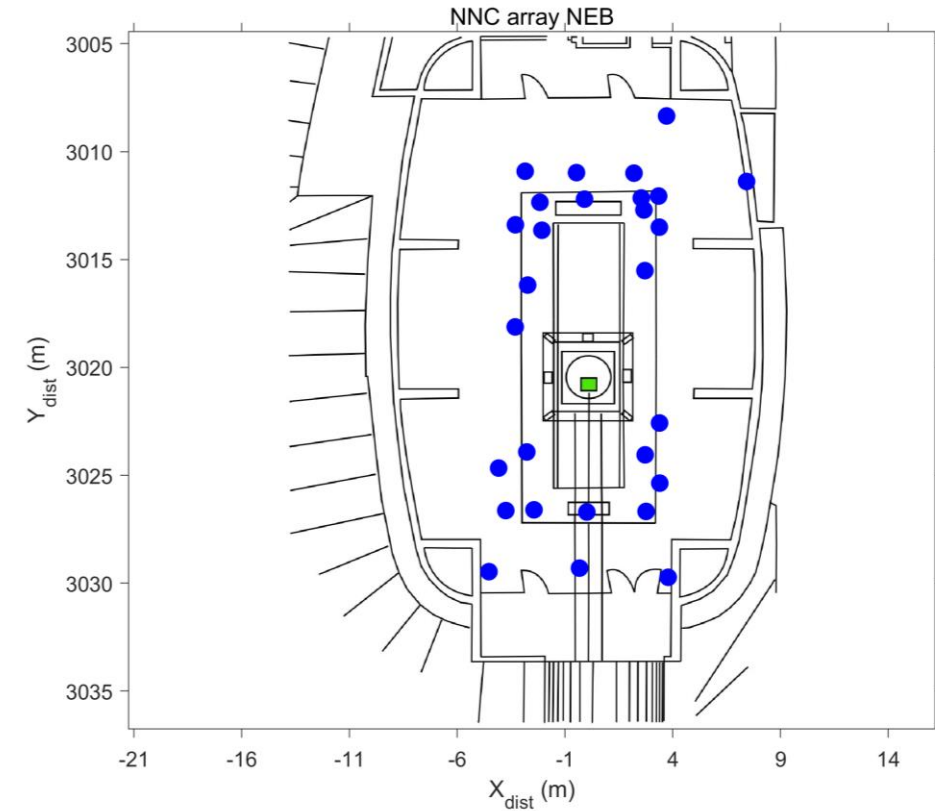
*Geophone locations in the CEB after the upgrade in May 2022; Red
dots with black edges correspond to the geophones whose
positions were changed*

Newtonian noise cancellation – End Buildings Array layout

- A total of 30, 5 Hz geophones deployed in the West End Building (WEB)
- A total of 28, 5 Hz geophones deployed in the North End Building (NEB)



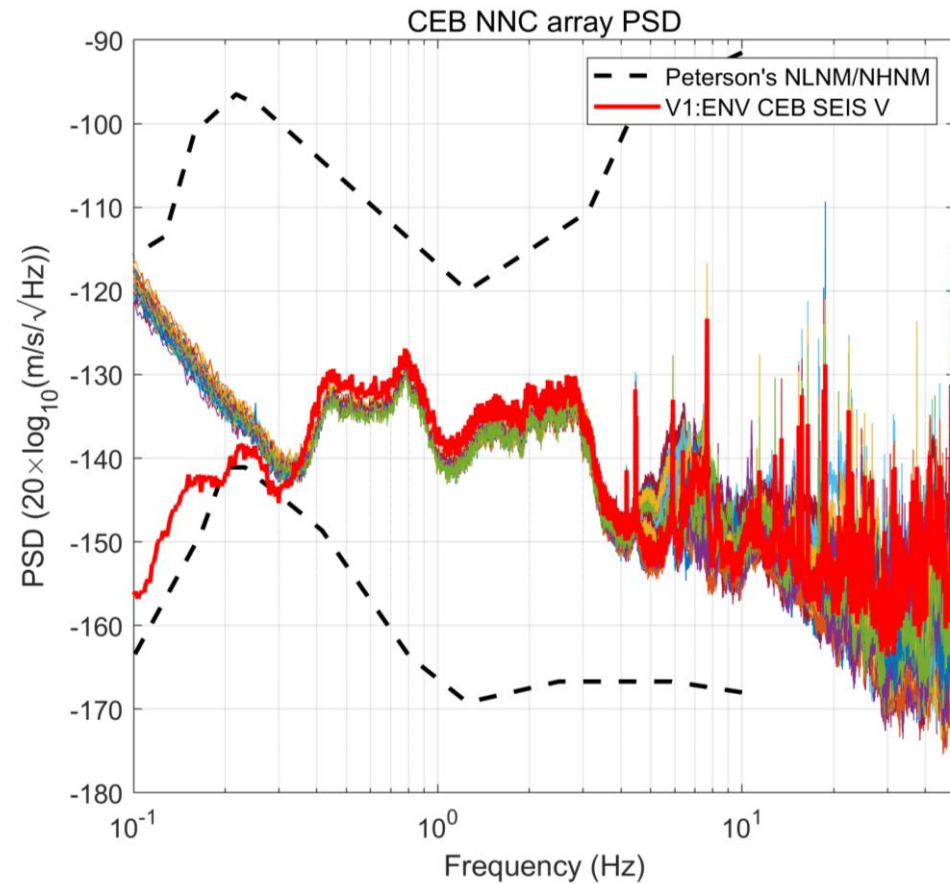
*Geophone locations in the WEB represented using the blue dots;
Coordinate system origin at the CEB beamsplitter*



*Geophone locations in the NEB represented using the blue dots;
Coordinate system origin at the CEB beamsplitter*

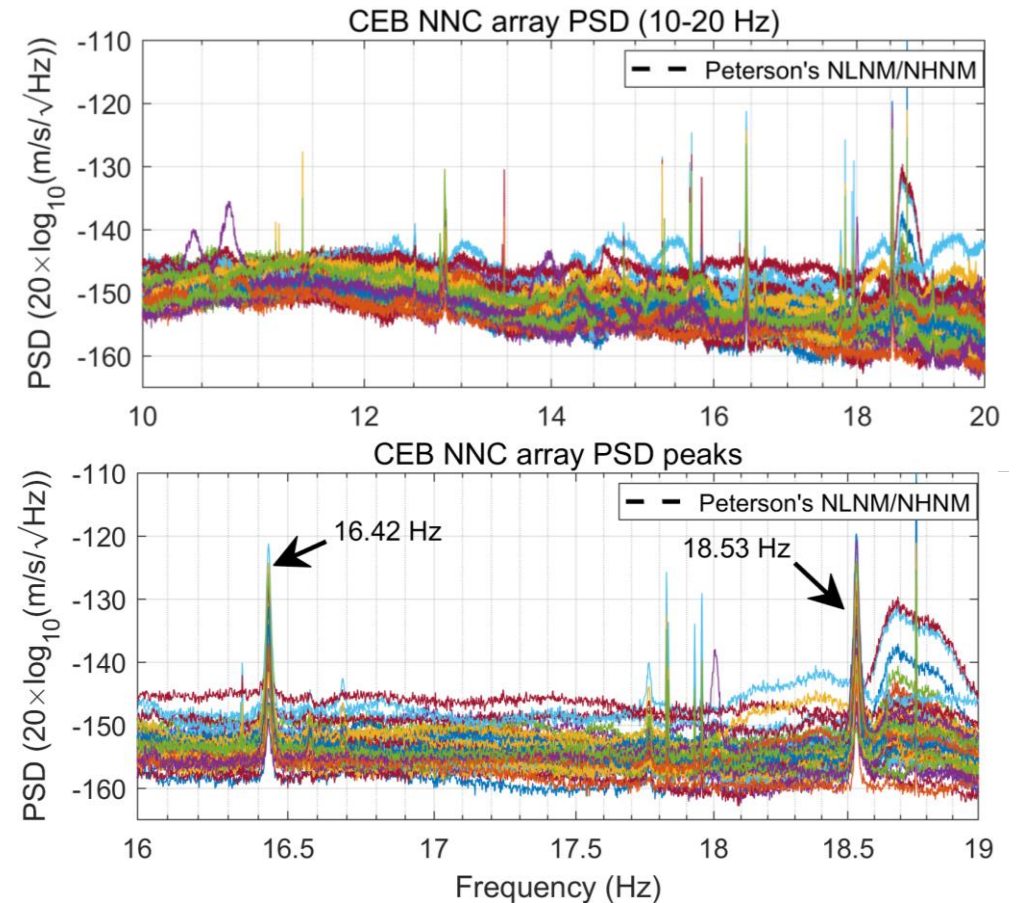
NNC array – Noise PSD characteristics

- Performance of the NNC 5 Hz geophones are comparable to the GURALP seismometer in the CEB down to 0.4 Hz



Mode of the PSD estimates for the CEB NNC geophones and the CEB GURALP seismometer (red curve) starting at GPS time 1359417600; PSD win length 600 s, 300 s overlap, total duration 86400 s

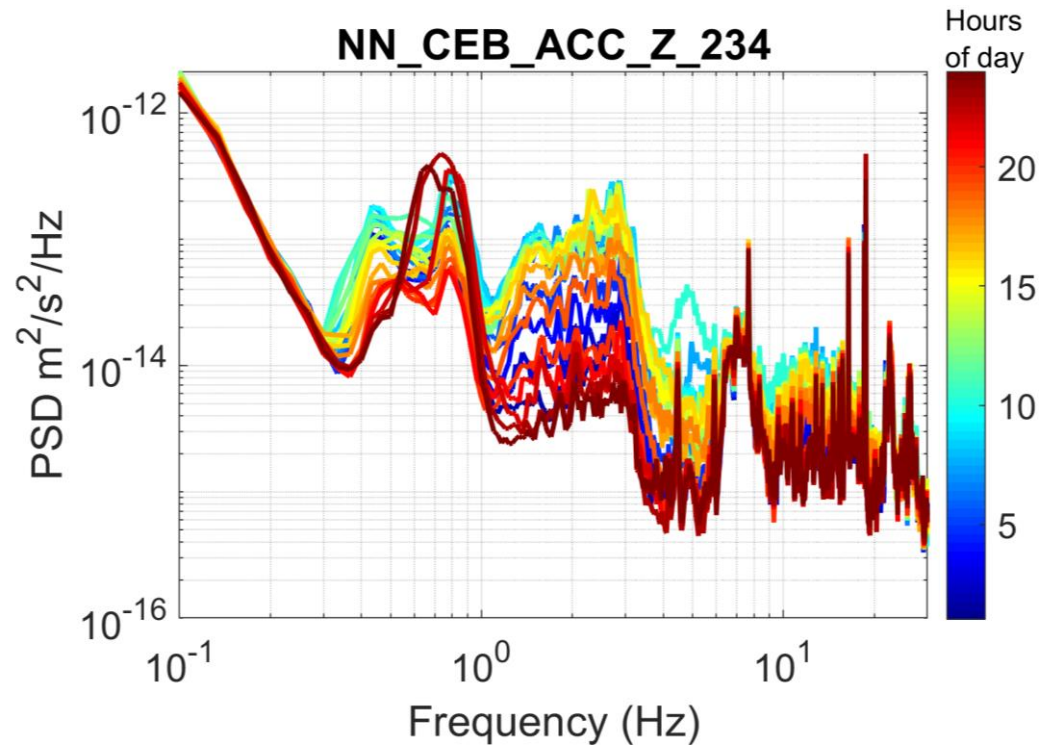
- Spatial variation between 10-20 dB for frequencies between 10-20 Hz
- Both broadband and sharp spectral noise observed



Seismic noise in band 10-40 Hz is composed of broadband as well as sharp spectral noise originating from machines at the site

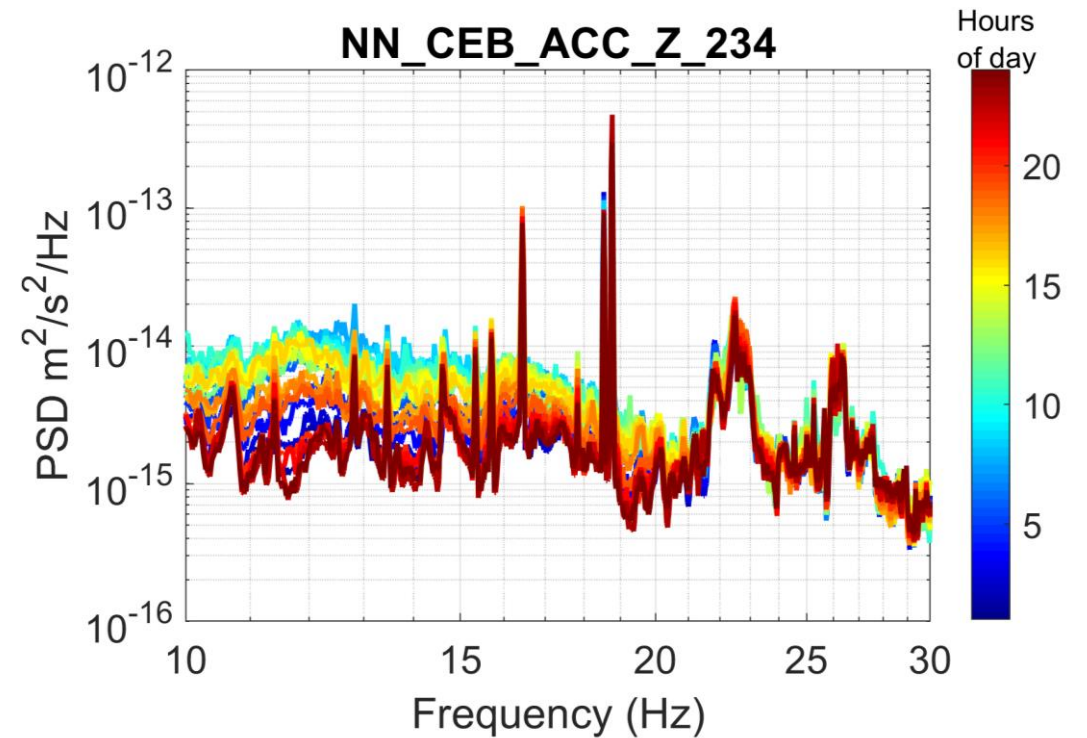
Noise characteristics – day-night variation

- Maximum seismic noise PSDs are observed at around noon every-day
- An order of magnitude difference in PSDs can be observed between noisy and quiet times, especially in the frequency band 2-6 Hz



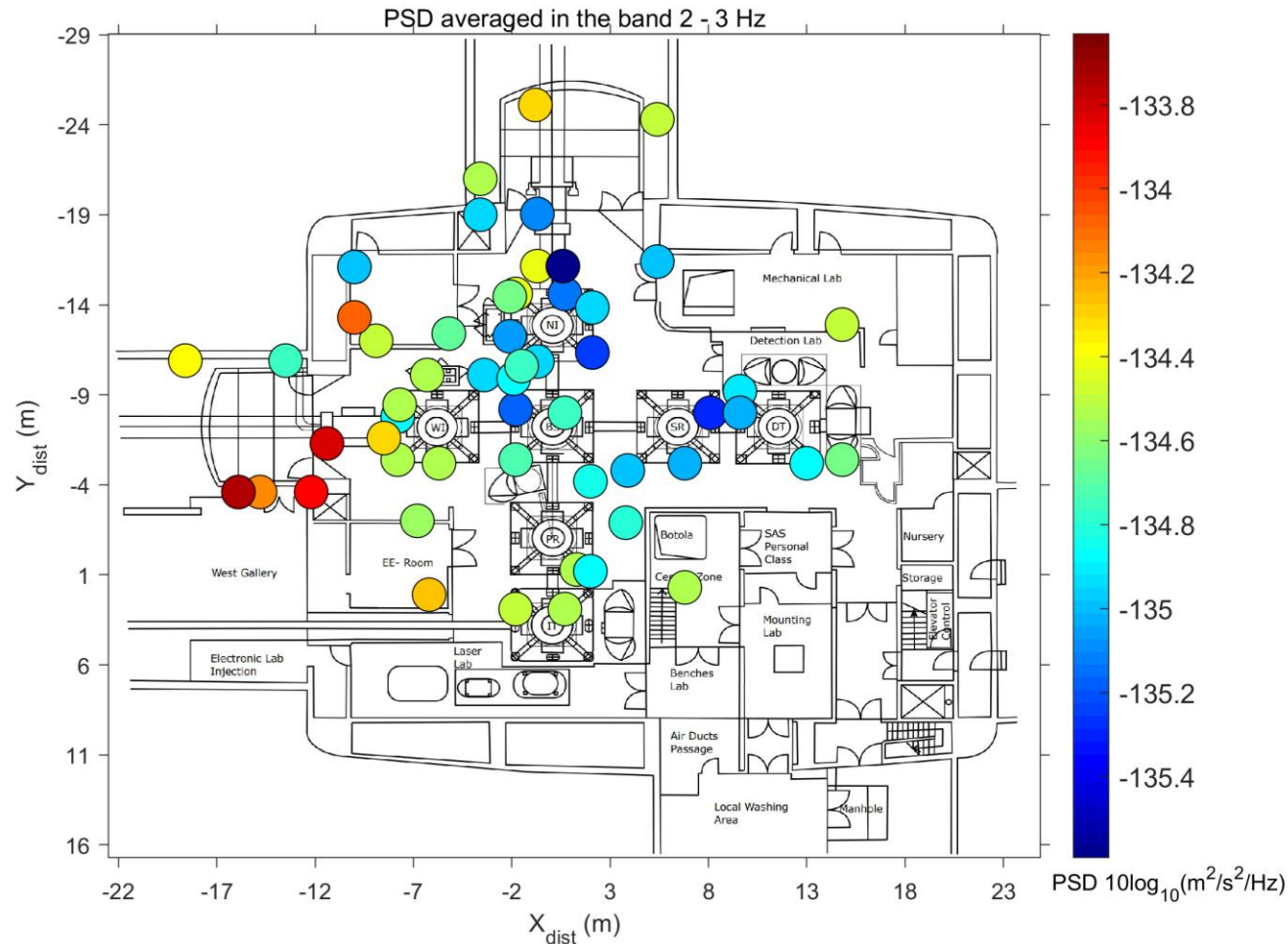
Average PSDs estimated every hour of the day showing strong diurnal variation between 2-15 Hz

- For frequencies above 10 Hz a factor 4-5 difference in PSDs are observed
- Above 20 Hz most noises are generated by machinery at the site and a day-night variation is not observed



Average PSDs estimated every hour of the day showing weak or no diurnal variation for frequencies greater than 25 Hz

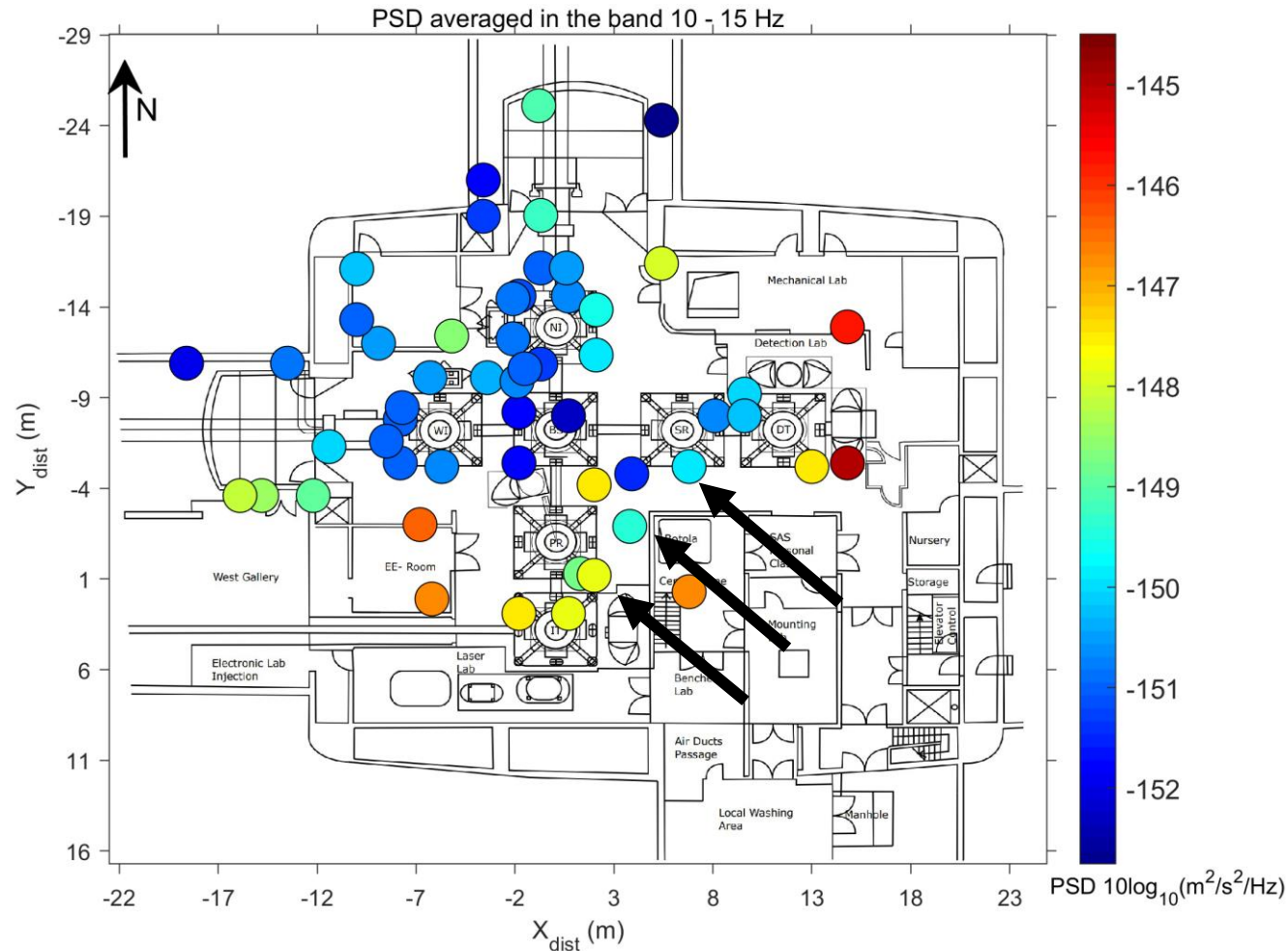
Noise PSD characteristics – Spatial variation in the 2-3 Hz band



Spatial distribution of seismic noise PSDs averaged in the frequency band 2-3 Hz.

- PSDs computed every 600 s with an overlap of 300 s between consecutive windows
 - Averaged for a week of data
 - Starting time – 1359417618 s
- Spatial variation of the noise PSDs are within 2 dBs
- Noise originates far-away from sources like roads, bridges etc.
 - Little attenuation while propagating through the NNC array

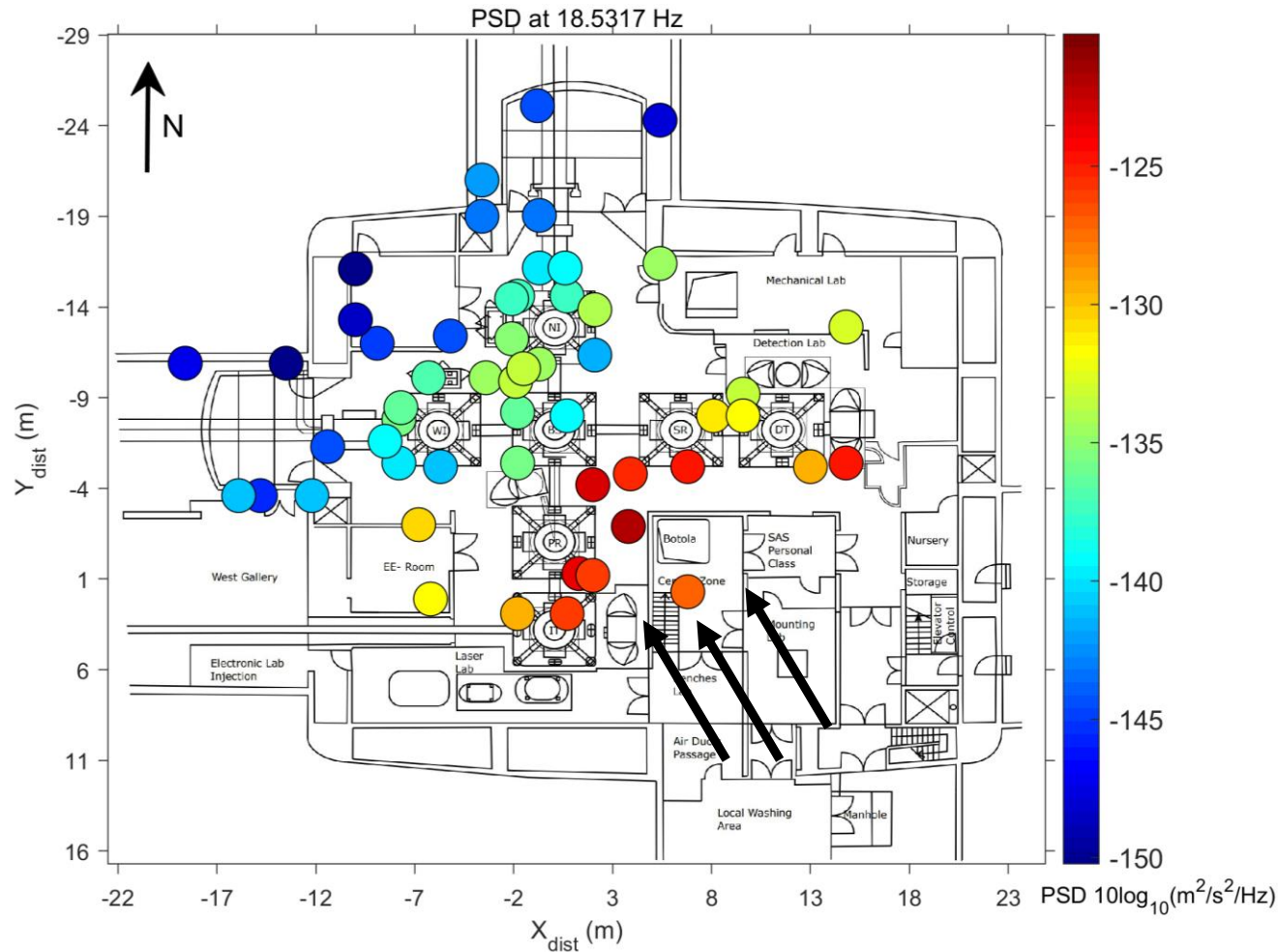
Noise PSD characteristics – Spatial variation in the 10 - 15 Hz band



- Noise PSDs averaged in the frequency band 10-15 Hz show a variation of about 7 dB
 - About 2-3 dB lower than that observed for the 6-8 Hz band
- Noise propagation “dominantly” SE - NW

Spatial distribution of seismic noise PSDs averaged in the frequency band 10-15 Hz.

Noise PSD characteristics – Spatial variation for the 18.5 Hz noise peak



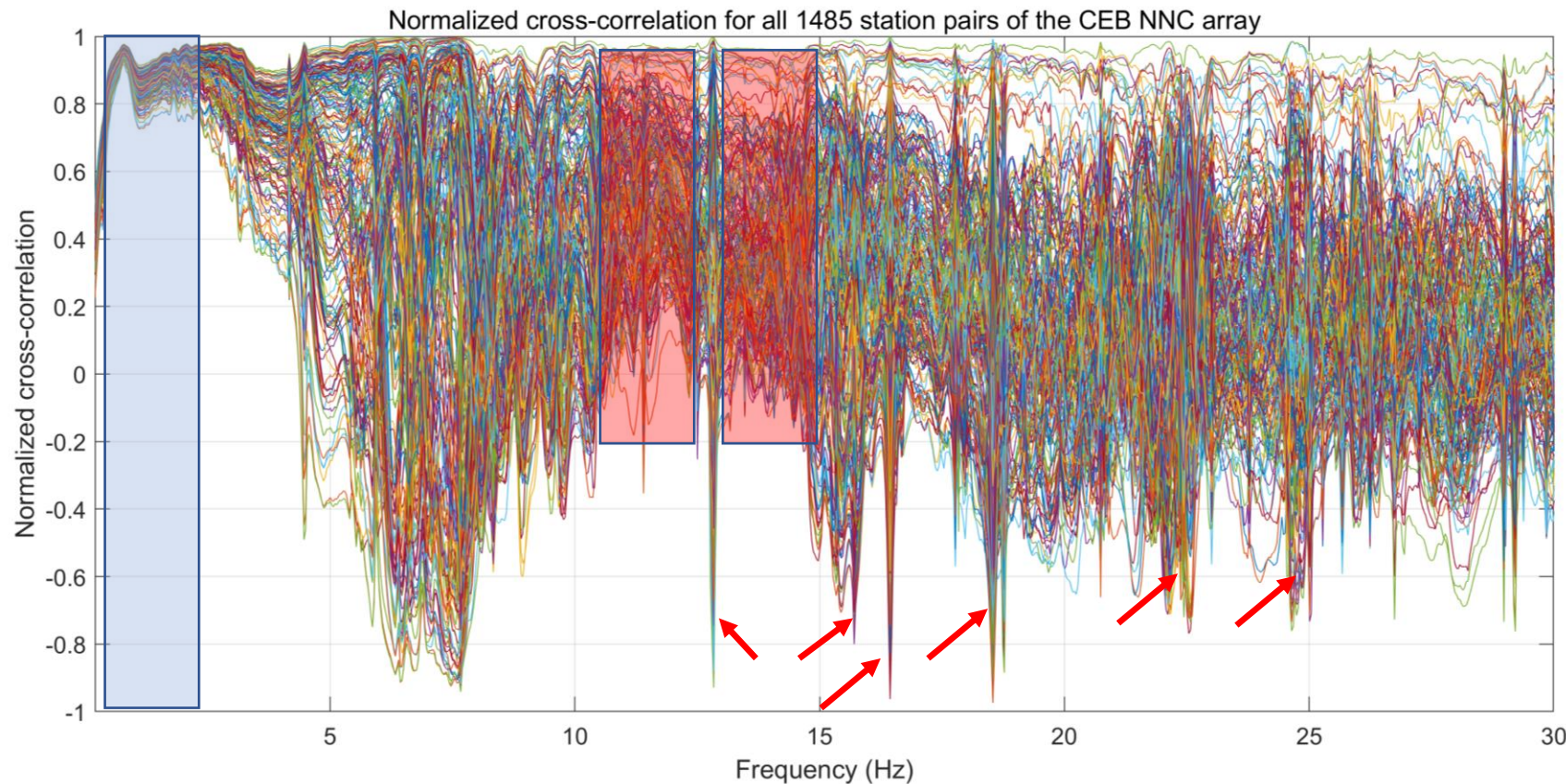
Spatial distribution of seismic noise PSDs for the peak at 18.5317 Hz

- Spatial variation of seismic noise PSDs can be used to infer location of noise sources within the building
- String PSD variation of about 30 dB observed
- Spatial variation of the noise PSDs for the 18.5317 Hz shows a dominant SSE-NNW
- Supply fan of the Air Handling Unit located in the CEB cleanroom has already been identified to be the source of this noise (<https://tds.virgo-gw.eu/?content=3&r=20911>)

Noise phase characteristics – normalized interstation cross-correlations

- Normalized cross-correlation between stations i and j for M windows can be expressed as

- $$CC_{ij} = \text{real} \left(\frac{\sum_{k=1}^M X_i(f) X_j^*(f)}{\sqrt{\sum_{k=1}^M X_i(f) X_i^*(f) \sum_{k=1}^M X_j(f) X_j^*(f)}} \right), \text{ where } X(f) = \text{fft}(x(t))$$



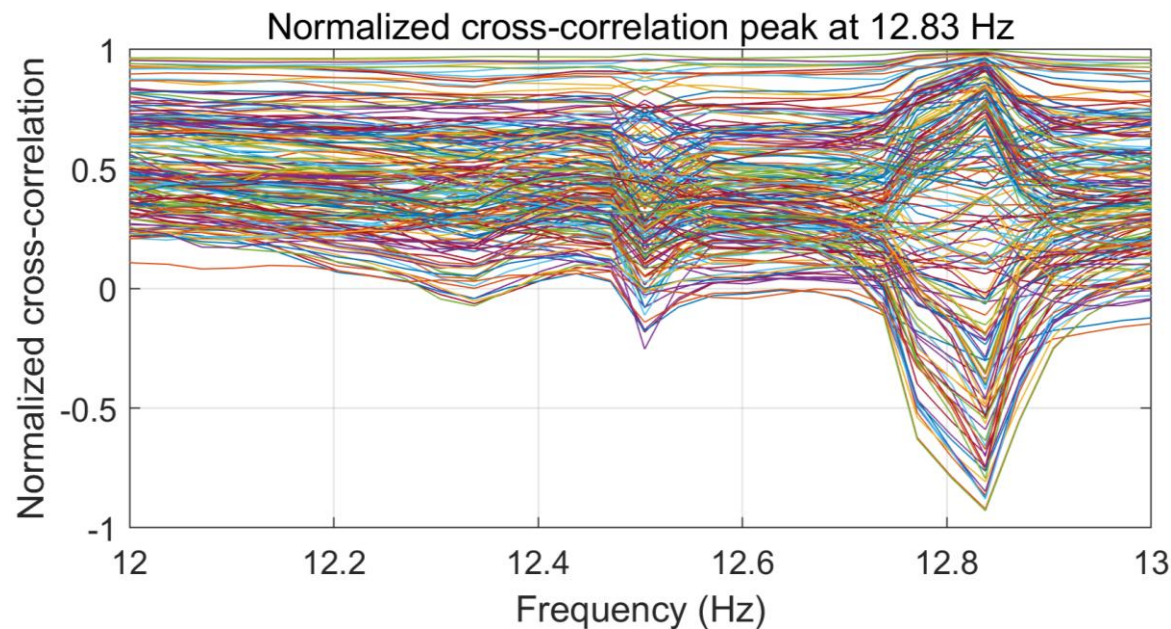
- Cross-correlations ≥ 0.8 for the frequency band 0.4-3 Hz

- Dominated by anisotropic distribution of surface wave sources

- Mixture of horizontally and near-vertical propagating waves (body waves)
 - Cross-correlation functions with no zero-crossing

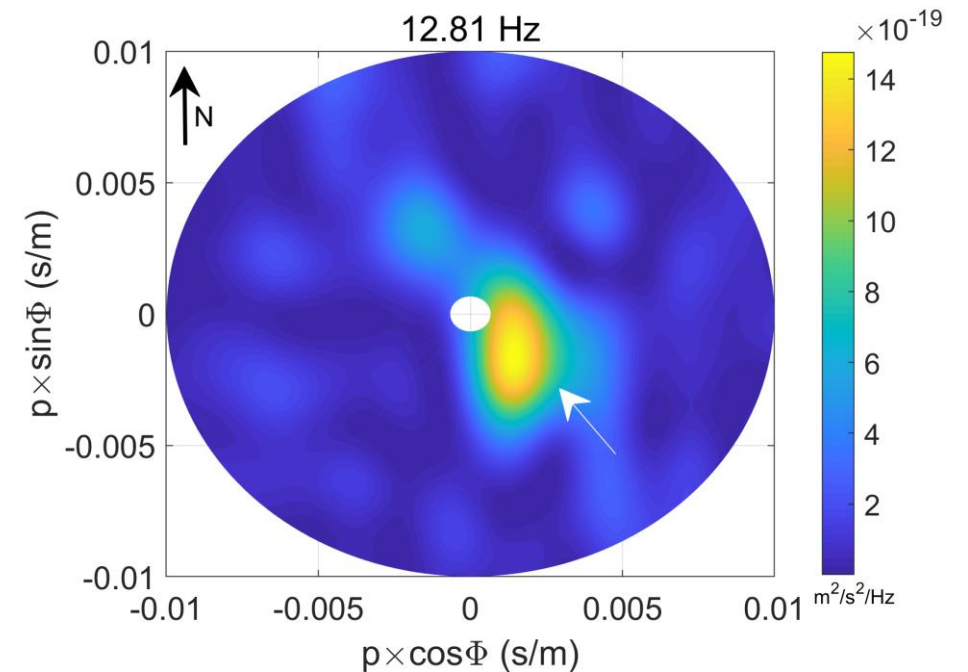
Noise phase characteristics – cross-correlations for anisotropic noise source distribution

- For any noise source distribution between azimuth ϕ_1 and ϕ_2 and vertical angle θ_1 and θ_2 , the theoretical CCF can be expressed as
 - $CCF = \sum_{\theta=\theta_1}^{\theta=\theta_2} \sum_{\phi=\phi_1}^{\phi=\phi_2} F(\theta, \phi, f) \cos\left(\frac{2\pi f}{v} (\sin\theta \cos\phi \hat{i} + \sin\theta \sin\phi \hat{j} + \cos\theta \hat{k}) (\vec{r}_i - \vec{r}_j)\right)$ **s.t.** $\sum_{\theta=\theta_1}^{\theta=\theta_2} \sum_{\phi=\phi_1}^{\phi=\phi_2} F(\theta, \phi, f) = 1$



Frequency domain cross-correlation corresponding to the peak at 12.8376 Hz, showing strong positive (≈ 1), and negative (≈ -1) correlations

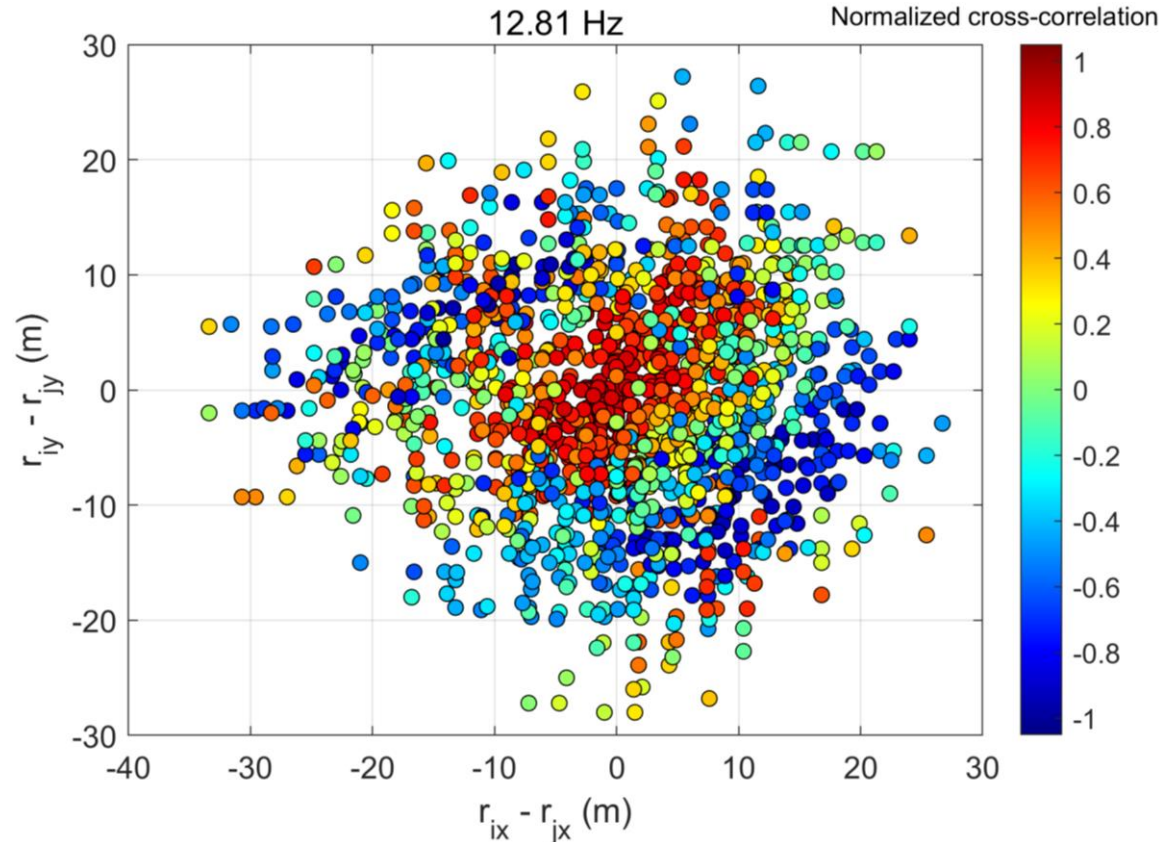
Beamform



Beampower expressed in polar coordinates (p, ϕ) showing a dominant plane wave propagation between azimuths $290^\circ - 340^\circ$

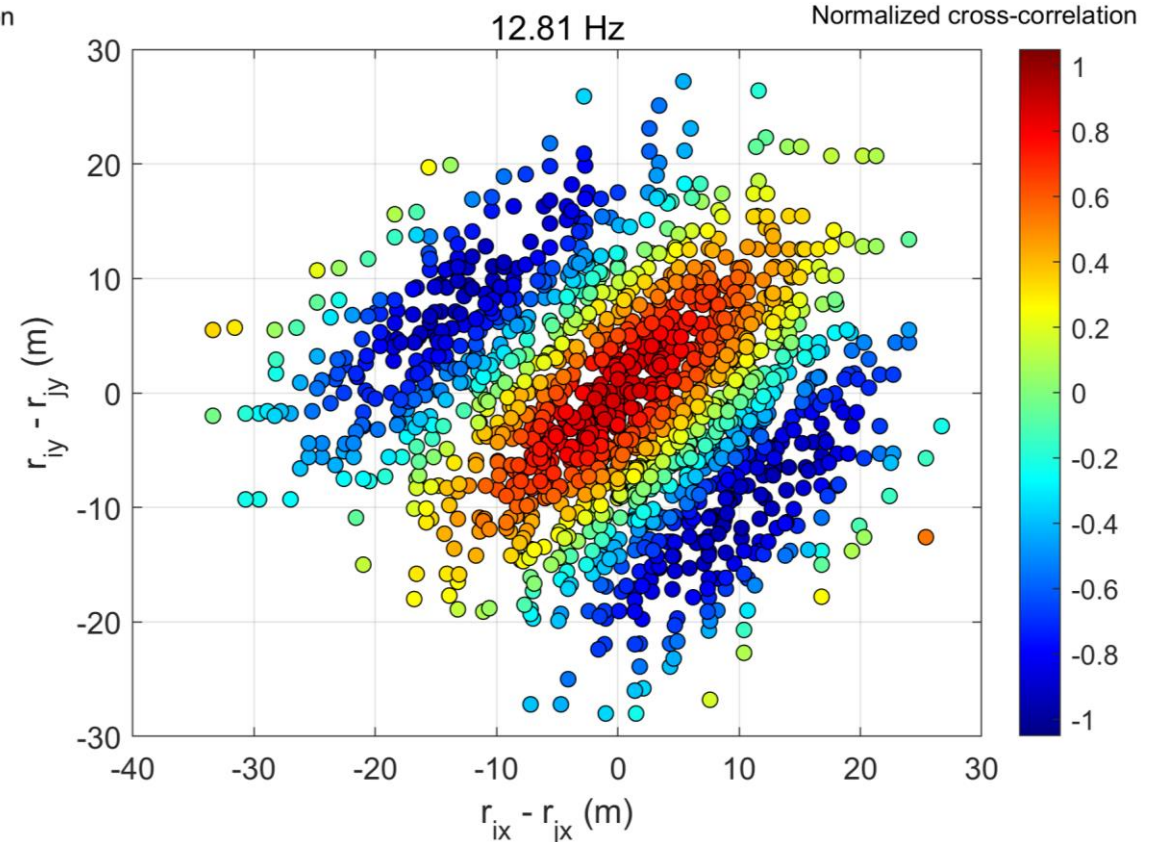
Noise phase characteristics – spatial distribution of cross-correlation for 12.81 Hz peak

Observed cross-correlations



Spatial distribution of noise cross-correlations at 12.8 Hz show a horizontally propagating wave

Estimated cross-correlations



Spatial distribution of theoretical noise cross-correlations for a dominantly horizontally propagating wave at $V = 370$ m/s. $\phi_1 = 290^\circ$, $\phi_2 = 340^\circ$

Wiener filter – NN prediction

- Given P input channels (geophones) and a filter h of L coefficients, the predicted NN can be expressed as
 - $y_{NN} = \sum_{p=1}^P \sum_{m=0}^L x_{n-m}^p h_m^p$, where x_k^p is the k^{th} input sample of the p^{th} geophone

- Since y_{NN} is not available, assuming $y_{DARM} \approx y_{NN}$, the optimal filter h is a solution to the problem
 - $\min[(y_{DARM} - y_{NN})^2] \Rightarrow \min[(y_{DARM} - \sum_{p=1}^P \sum_{m=0}^{L-1} x_{n-m}^p h_m^p)^2]$

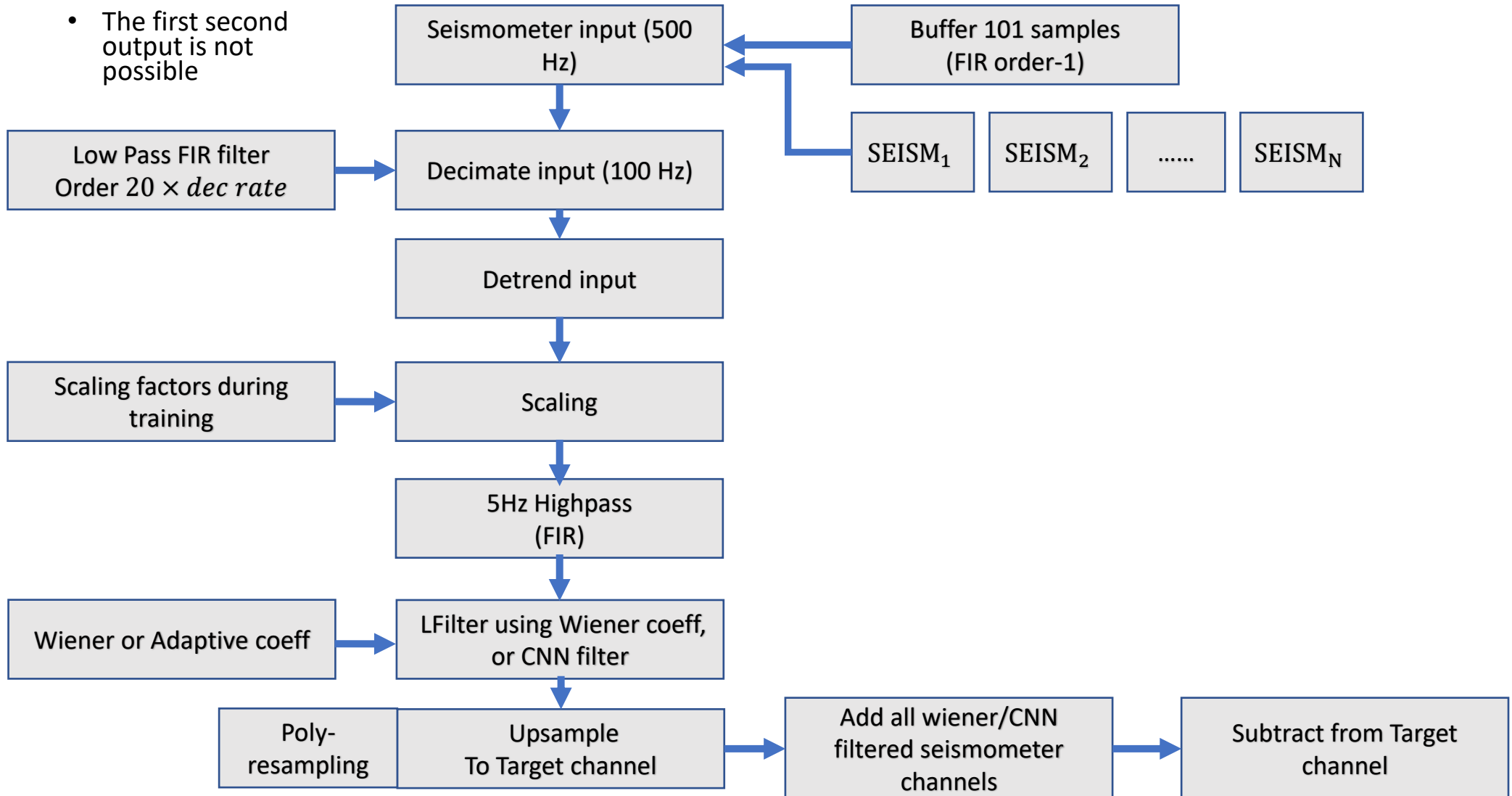
- Using the Wiener-Hopf formulation, the optimal filter h can be expressed as,
 - $h = R^{-1}Q$

where $R = \begin{pmatrix} \phi_{11} & \phi_{12} & \dots & \phi_{1P} \\ \phi_{21} & \phi_{22} & & \phi_{2P} \\ \vdots & & \ddots & \vdots \\ \phi_{(P-1)1} & \phi_{(P-1)2} & \dots & \phi_{(P-1)P} \\ \phi_{P1} & \phi_{P2} & & \phi_{PP} \end{pmatrix} \Rightarrow \text{Full Rank}$

and $\phi_{ij} = \begin{pmatrix} C_{ij}(0) & C_{ij}(1) & \dots & C_{ij}(L-1) \\ C_{ij}(-1) & C_{ij}(0) & & C_{ij}(L-2) \\ \vdots & & \ddots & \vdots \\ C_{ij}(-L+2) & C_{ij}(-L+1) & \dots & C_{ij}(1) \\ C_{ij}(-L+1) & C_{ij}(-L) & \dots & C_{ij}(0) \end{pmatrix}, C_{ij}(\tau) = x(t)x(t+\tau)$

$$Q = \begin{pmatrix} \phi_{1y} \\ \phi_{2y} \\ \phi_{3y} \\ \vdots \\ \vdots \\ \vdots \\ \vdots \\ \phi_{Py} \end{pmatrix}$$

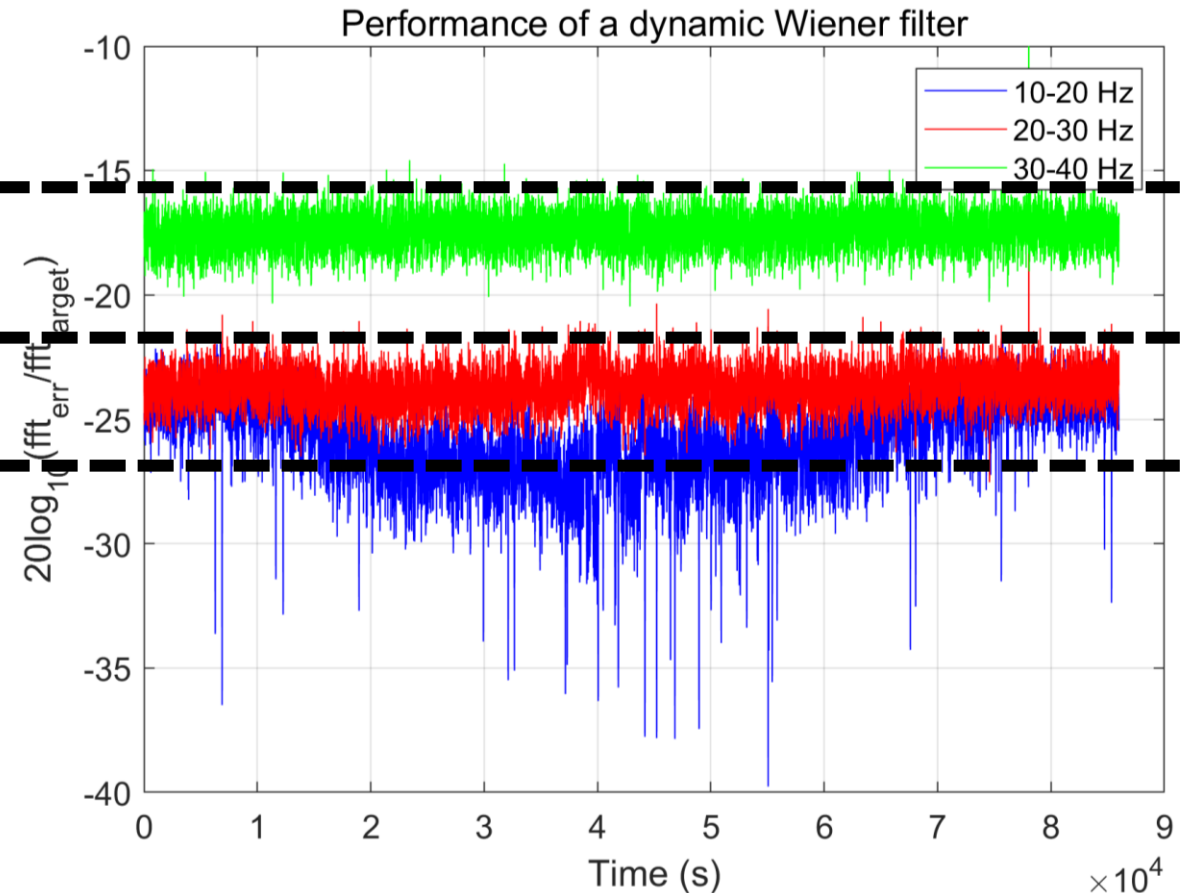
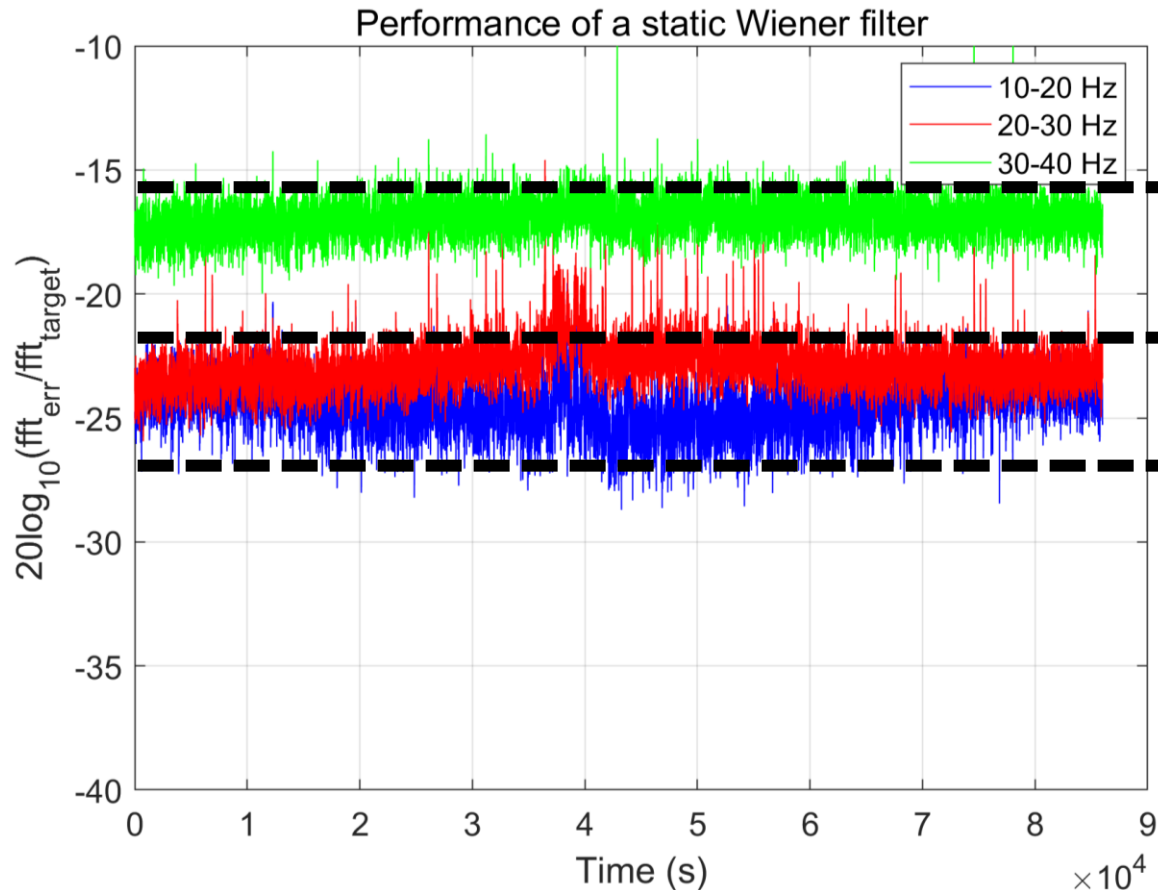
Noise cancellation steps



Wiener filter – Static vs Dynamic (CEB_SEIS_V as target)

- 10-20 Hz → 25-27 dB
- 20-30 Hz → 20-25 dB
- 30-40 Hz → 16-18 dB

- About 10 dB better performance for transients
- About 2 dB better performance for transients
- Similar performance in 30-40 Hz band



Adaptive filters

- Two broad classes of algorithms exist for solving the Wiener problem:

- Least Mean Square (LMS/NLMS)

- Stochastic gradient method ($O(LP)$)
- $h(n) = h(n-1) + \mu(n)x(n-1)e(n)$
 - $\mu(n) = \frac{\alpha}{x(n)x^T(n) + \delta}, 0 < \alpha < 2, \delta \approx 0$

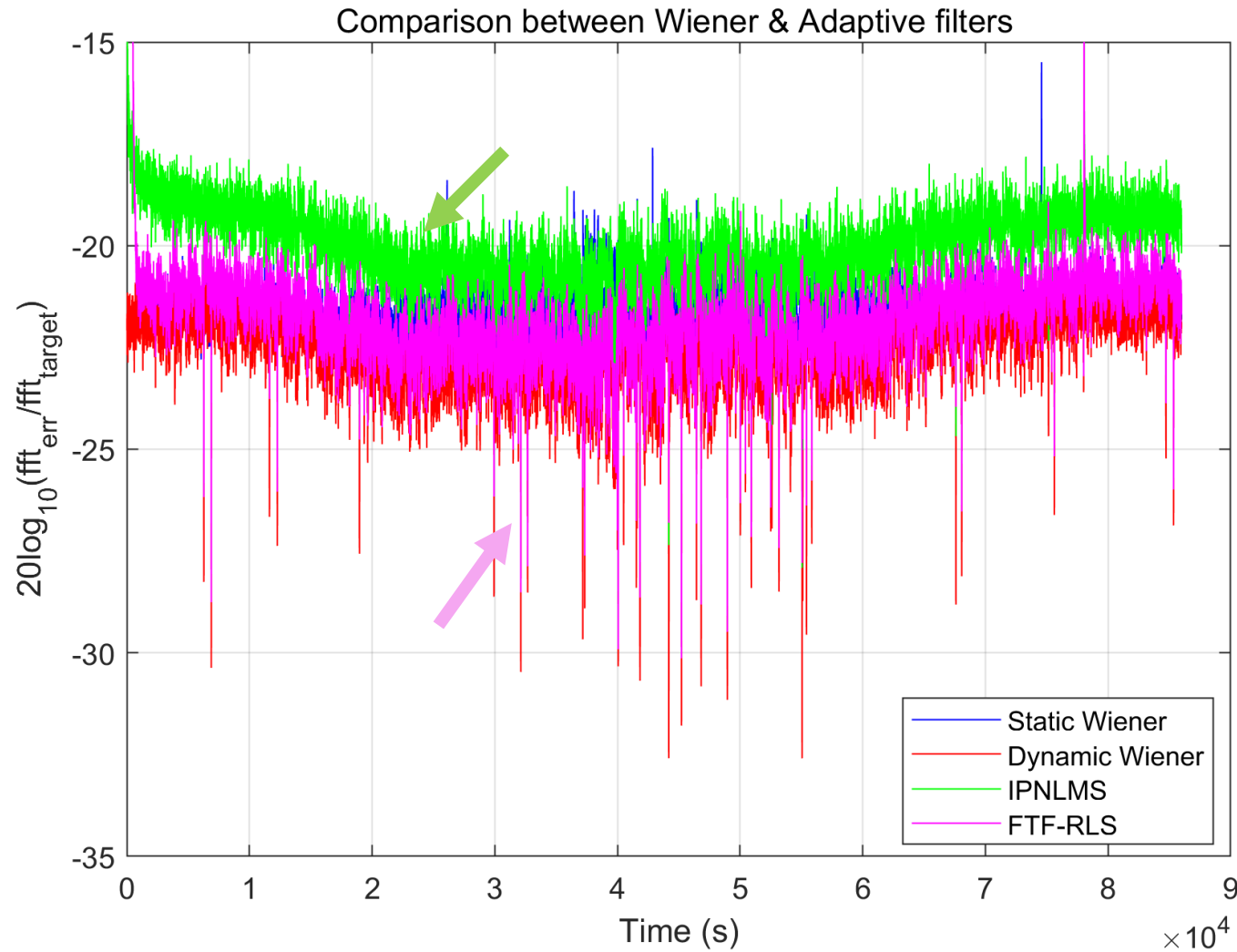
- IPNLMS ([Improved proportionate NLMS](#))

- $\mu(k) = \frac{\alpha}{\sum_{m=0}^{L-1} x^2(k-m)g_{ip,m}(k-1) + \delta_{IPNLMS}}$
- $g_{ip,l}(k-1) = \frac{1-\beta}{2L} + (1+\beta) \frac{h_l(k-1)}{2\|\mathbf{h}(k-1)\|_1 + \epsilon}$
- $\epsilon \approx 0, -1 \leq \beta < 1$

- Recursive least square (RLS)

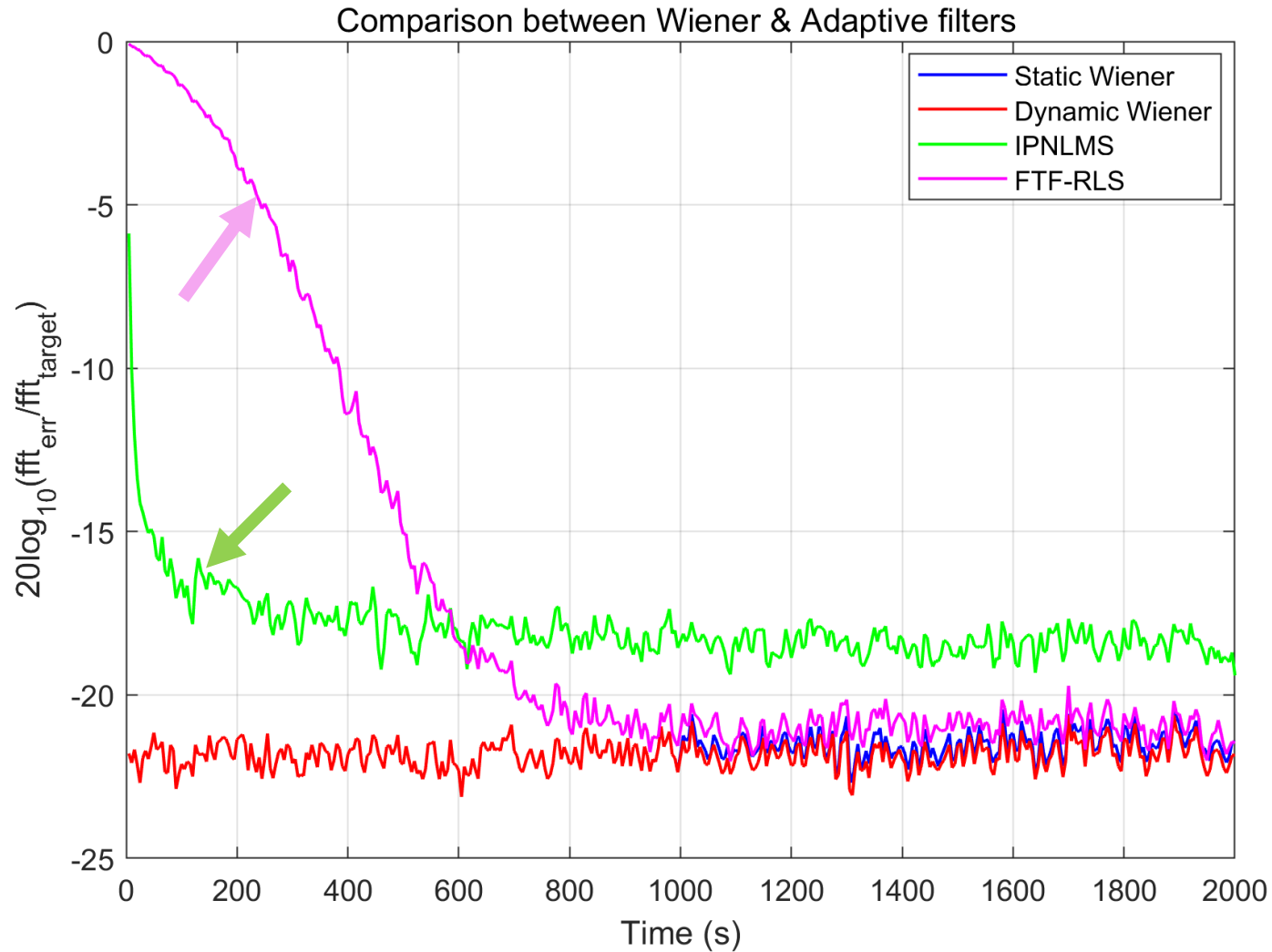
- $\min(\sum_{m=0}^{L-1} \lambda^{n-m} e^2(m))$
- $h(n) = h(n-1) + R_{xx}^{-1}(n)x(n)e(n)$ (Gauss-Newton like)
- $R_{xx}^{-1}(n) = \lambda^{-1}R_{xx}^{-1}(n-1) - \frac{\lambda^{-2}R_{xx}^{-1}(n-1)x(n)x^T(n)R_{xx}^{-1}(n-1)}{1 + \lambda^{-1}x(n)R_{xx}(n-1)x^T(n)}$
- Complexity $\approx O(L^2P^2)$ per sample (not feasible)
- Stabilized Fast Transversal algorithms ([Slock and Kailath, 1991](#))
 - $O(LP)$
 - Solves the exact quadratic problem
 - Good tracking even in noisy environment
 - Computationally expensive

Wiener vs Adaptive filters (CEB_SEIS_V as target)



- IPNLMS performs about 4 dB worse than Wiener/Dynamic-Wiener during quiet times
 - During short-burst transients IPNLMS does better than static Wiener filter but worse than Dynamic Wiener or FTF-RLS
-
- Performance of FTF RLS comparable to the dynamic Wiener filter

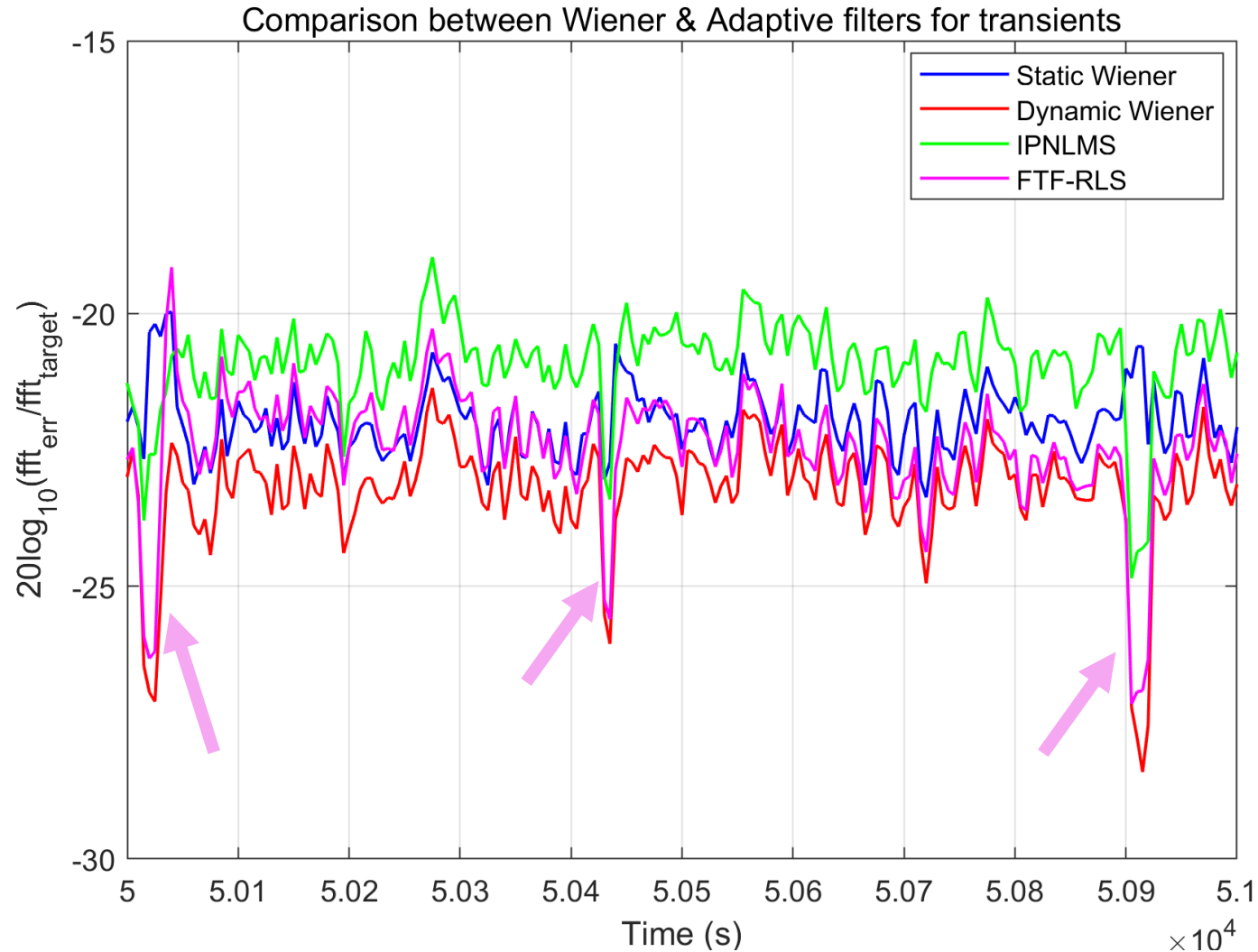
Wiener vs Adaptive filters at the onset (CEB_SEIS_V as target)



- IPNLMS converges quickly for $\alpha = 0.5$, and $\beta = -0.75$

- FTF RLS takes a bit longer ($\approx 800s$) to reach steady state, but performs comparable to the dynamic Wiener filter
- Slow convergence is due to $\lambda = 1 - \frac{1}{LP}$ (≈ 1)
- However, if λ is made smaller, the numerical stability of the algorithm is compromised

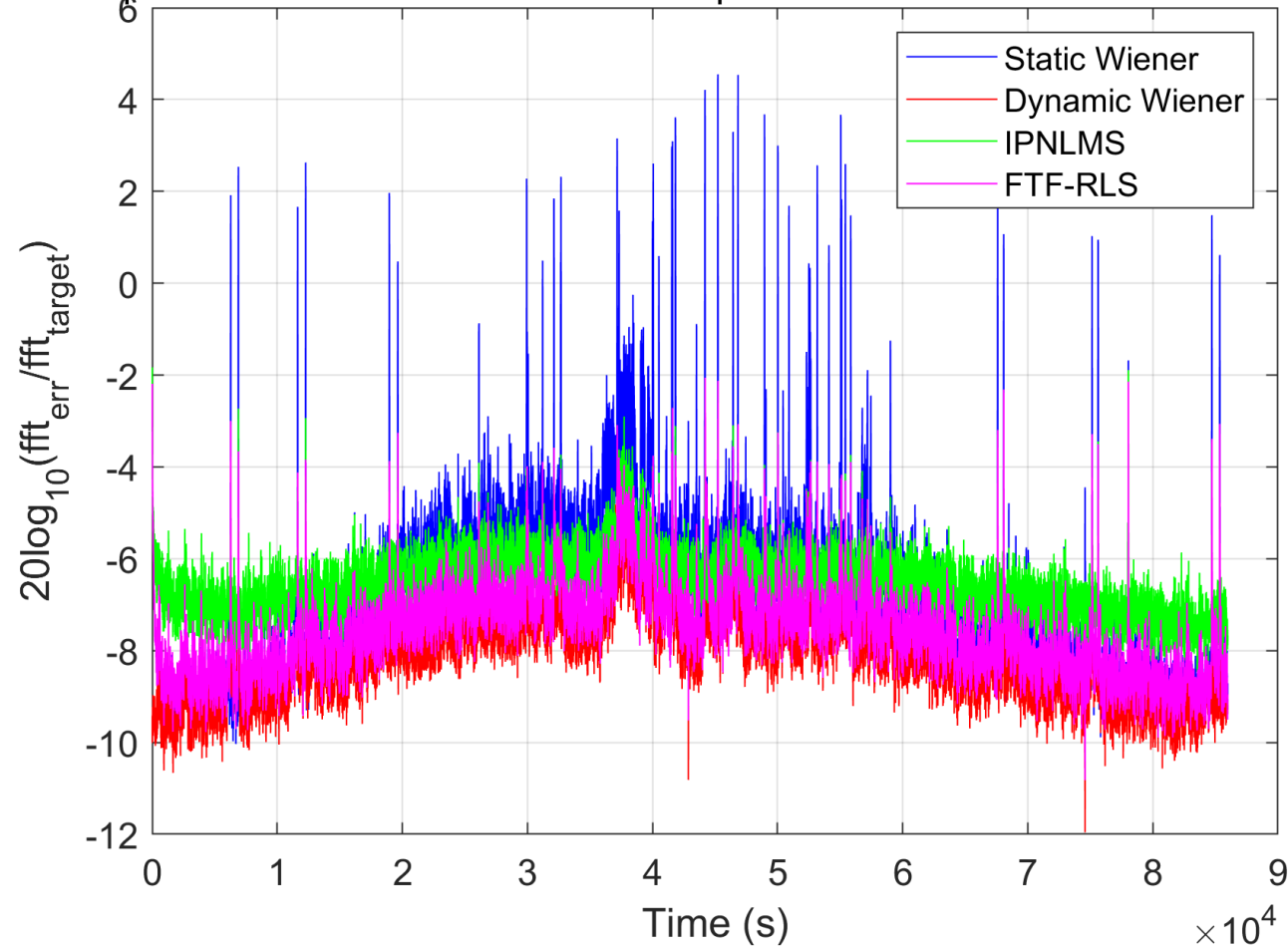
Wiener vs Adaptive filters during transients (CEB_SEIS_V as target)



- FTF RLS performs within a dB of the dynamic Wiener filter
- During quiet-times its performance is between the static and the dynamic Wiener filters
- Performance can be improved by modifying the rescue procedure
 - Soft-constrained initialization is in play
 - Decorrelate inputs to stabilize the condition number of the forward and backward predictor matrices

Wiener vs Adaptive filters (CEB_SEIS_N as target)

Comparison between Wiener and Adaptive filters with CEB SEIS N as target



- Maximum gain of about 10 dB during quiet times (was 25 dB for V-target)
- Performance worse by about 2-3 dB during noisy-times

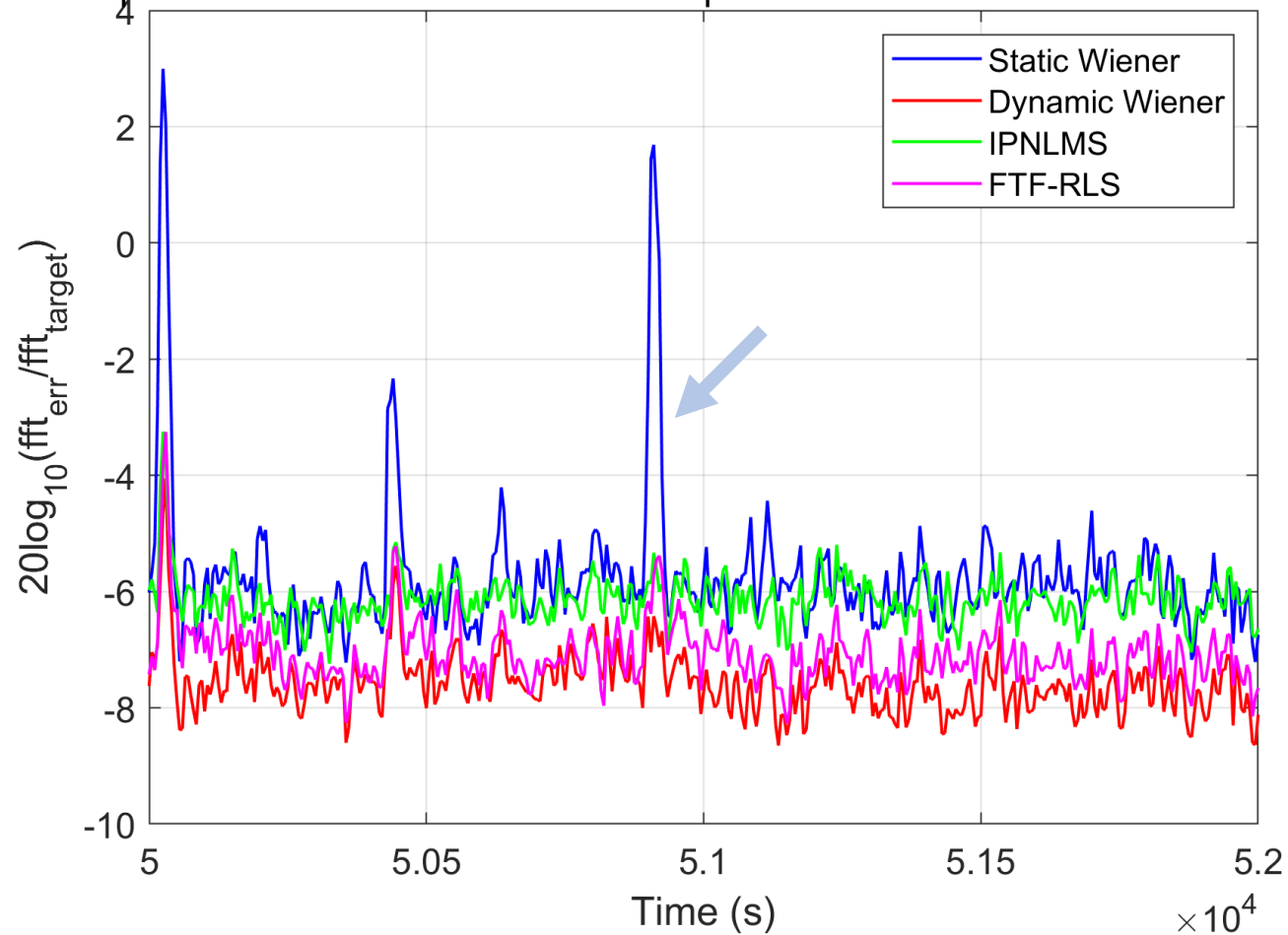
- Static Wiener filter performance worse for transients
 - Unfavorable wave-types

- IPNLMS performance comparable to or better than FTF-RLS for transients
- Performance worse by 3-4 dBs during quiet-times

- Performance of FTF RLS comparable to dynamic Wiener filter performance

Wiener vs Adaptive filters during transients (CEB_SEIS_N as target)

Comparison between Wiener and Adaptive filters with CEB SEIS N as target



- During noisy times, performance of all algorithms are comparable except for the static Wiener filter, which adds noise to the data-stream
- FTF RLS performance is close to dynamic Wiener filter and outperforms IPNLMS marginally (1 – 2 dB)
- Overall cancellation of the horizontal channel using vertical channels as input is a challenging problem and is a scenario similar to NN-cancellation

Conclusions

- 55 vertical component 4.5 Hz geophones in the CEB, 28 in the NEB and 30 in the WEB were installed
- Data digitization at 500 sps performed within the sensors and data readout was integrated with the Virgo DAQ system (time synchronized)
- Sensor locations - optimization studies based on seismic wavefield characteristics and simulated NN were performed
- An online NNC implementation has been done based on the static Wiener filter case (<https://git.ligo.org/virgo/virgoapp/NNCfilter/-/tree/NNCTest01>)
- Adaptive filter options were explored: LMS (different classes) and RLS (FTF, FLA)
- FTF-RLS were found to be robust, and were tested offline
- Performance could be enhanced by designing better rescue algorithms
- A challenging problem of subtracting the horizontal seismic noise channel by using the vertical channel was considered
 - Gain of about 10 dB during quiet times and about 7-8 dB during noisy times could be achieved
 - Performance worse by about 15 dB compared to the scenario when the vertical channel was used as target



Questions?
