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# CE Beamtube Requirements, Plan and Status

# 3<sup>rd</sup> Generation Gravitational Wave Detector NSF vacuum workshop Jan 2019



Participants in the NSF Workshop on Large Ultrahigh Vacuum Systems for Frontier Scientific Instrumentation, LIGO Livingston, Jan. 28-31, 2019

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Alex Chen	FNAL
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Bob Childs	MIT PSFC
Dennis Coyne	LIGO
Caltech	
Fred Dylla (retired)	AIP
James Fedchak	NIST
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Yulin Li	Cornell
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Dennis Manos	William & Mary
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Antonio Pasqualetti	Virgo
Matt Poelker	Jefferson
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David Reitze	LIGO
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Martin Tellalian	McDermott
Takayuki Tomaru	KEK
Rainer Weiss	LIGO MIT
Michael Zucker	LIGO MIT

3<sup>rd</sup> Generation Detector Vacuum System Design Workshop held in 2019.

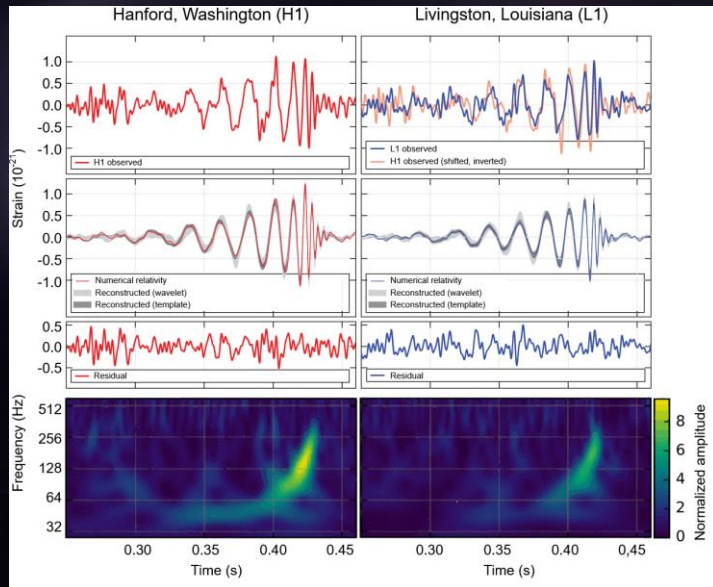
Final report publicly available at <https://dcc.ligo.org/LIGO-P1900072>

# Topics

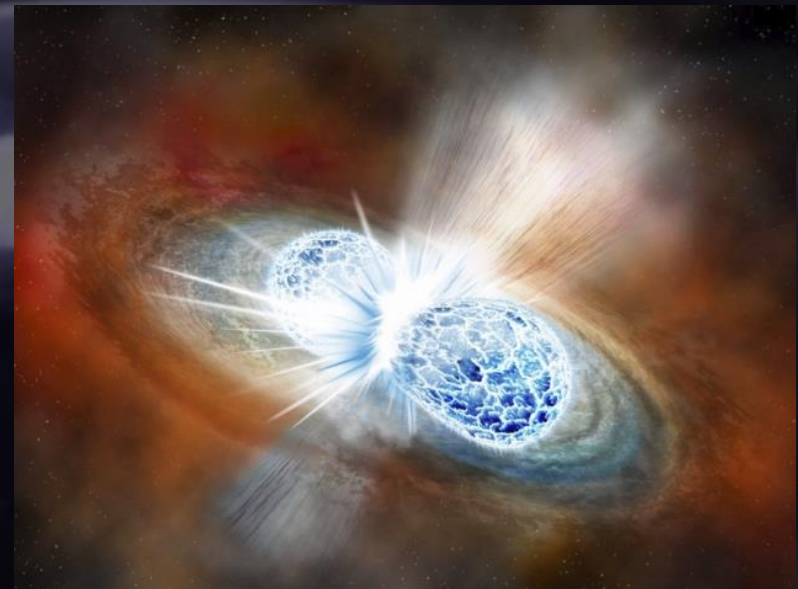
- 2015 - Gravitational Wave Astronomy 1<sup>st</sup> Detection and Multi-Messenger event
- Rational for building CE
- Design Trade Space: Improving Detector Sensitivity
- Scaling to 40 km beampipes
- Beamtube Requirements
  - Mechanical Design
  - Vacuum Conditions
- Outgassing Research
  - Water and hydrogen
  - Coatings
  - LTREX chamber
- Alternate Materials and Concepts
  - Carbon Steel
  - Nested (coaxial) System
- Summary and Status

# Gravitational Wave Astronomy

- Predicted by general relativity- acceleration of mass.
- Distortion of space-time “strain waves”. Measure  $10^{-19}$  m change in LIGO arms.
- First detection September 14<sup>th</sup> 2015- Black hole pair “inspiral”.
- Neutron star pair- August 17 2017- First GW+EM signals “multi-messenger”.



GW150914



GW170817

# Rational for CE ?

- **CE would be a “3<sup>rd</sup> generation” GW detector**
  - Major upgrade vs LIGO, 10x increase arm length 4 km -> 40 km
  - 10x increase in strain sensitivity (scales with L). See farther back in time.
  - Larger “volume” of observation. Potential 1000x increase in detection frequency.
  - Ground based detector similar to LIGO, leverages > 20 yrs. of operational experience.
  - Minimal reliance on “new” technologies that may not become available.
  - Minimal increase in noise sources, same overall design as LIGO.

# Trade Space-Increased GW Detector Sensitivity

- Increase length of arms-the current CE proposal ( $\Delta L/L$ )
  - Sensitivity scales with  $L$ .
  - Noise sources stay approximately constant.
  - Many cost drivers- land, materials, earthwork, site topology (30 m earth curvature), seismic.
  - LISA: Move to space. “Free” vacuum, unlimited room, explore much lower frequencies. Trade is complexity and costs, mission life and redundancy. JWST cost \$10B, a cost growth about 100%, 15 years behind schedule. Add \$1B to launch.
- Increase “N” number of arm transits (add path length and photon density)
  - Optics reflectivity determines N, for LIGO about 200 trips, cavity finesse. Coatings about 15 ppm XMNS currently with ~10 ms arm storage time. Optical losses accumulate as N increases, also don’t want light storage time close to GW period, so this approach has limits.
  - Reflective coatings are near state of the art, but also want coatings with lowest Brownian (thermal) noise possible .....significantly “better” coatings under intense research, 2x improvement?
- Reduce noise sources-other options (thermal, seismic)
  - Cryogenics- increased complexity, optics are now the vacuum pumps (cryofilms- optical scattering noise).
  - Lower (vacuum) arm pressure → lower forward scattering-reduced phase noise , XUHV not practical.
  - Better suspensions (seismic), lower coating defects, larger or different test masses, scattering, etc. R&D.
- Increase laser/arm power (quantum noise)
  - A-LIGO arm power goal 800 kW <10 mm beam. Optics damage threshold? Lossy areas/defects in coating “burn”, increased radiation pressure, thermal lensing, shot noise, laser stability (need for length measurement).
  - Molecular films and particles (scatter and ablation, vaporize dust particles (loss and scatter)).

See <https://dcc.cosmicexplorer.org/public/0163/P2100003/007/ce-horizon-study.pdf> for a discussion of trades associated with alternate CE detector designs

# Concentrate on arm length trade

- 40 km arms will add 10x strain sensitivity
  - "See" cosmic events from 1<sup>st</sup> epoch of time.
  - Measure strain  $< 10^{-22}$   $\Delta L \approx 4 \times 10^{-18} \text{m}$ .
  - Minimal new technology drivers (optics, coatings, etc.).
- Vacuum system becomes technology and cost driver
  - 90M liter UHV system.
  - Where to build and how to manage the 30 meter height change (earth curvature/40 km).
  - Cost of SST (Cr, Ni) is volatile (surcharge, cost escalation risk). Alternate materials?
  - Most requirements (diameter, vacuum levels, straightness are similar to the existing LIGO system).
  - Can we bake such a large system?

A wave's strength is measured by the *strain* induced in the detector,

$$h = \Delta L / L$$

We can calculate expected strain at Earth;

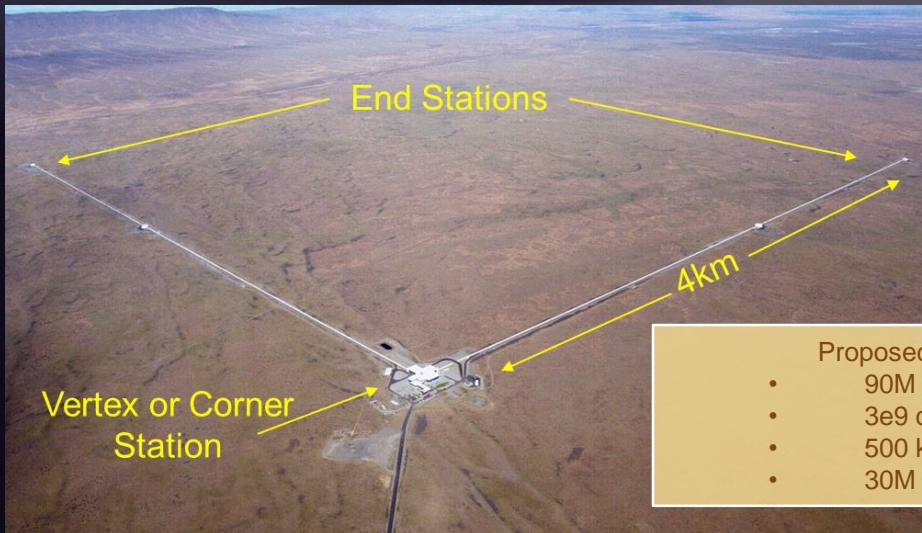
$$|h| \approx 4\rho^2 GMR^2 f_{orbit}^2 / c^4 r \approx 10^{-22} \left( \frac{R}{20\text{km}} \right)^2 \left( \frac{M}{M_\odot} \right) \left( \frac{f_{orbit}}{400\text{Hz}} \right)^2 \left( \frac{100\text{Mpc}}{r} \right)$$

Existing interferometer arms are 4,000 meters long,

$$\Delta L = h \times L \approx 10^{-22} \times 4,000 \text{ m} \approx 4 \cdot 10^{-19} \text{ m}$$

# Scaling to 40 km

- 40 km system largest cost driver will be the the vacuum system
  - Cost scaling: Beamtubes (8 km) were \$76M (1994) estimated \$700M in 2028.
  - Chromium and nickel are commodities, price can be volatile. LIGO Contractor would not commit to FFP.
  - Are there alternate materials?
  - Can we eliminate the concrete enclosure?
  - What about bakeout?
  - We will assume an above-ground facility.



- Proposed CE beamtube 80 km
  - 90M liter  $\times 10^{-9}$  Torr
  - $3e9$  cm<sup>2</sup> of surface area
  - 500 km of welds
  - 30M kg of material (1.27 cm wall)

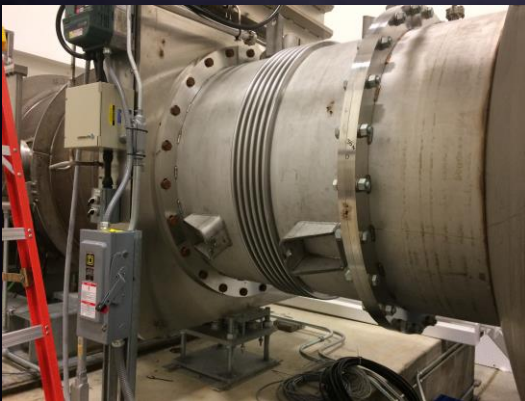


# Beamtube requirements- Mechanical

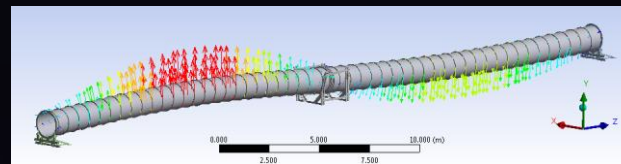
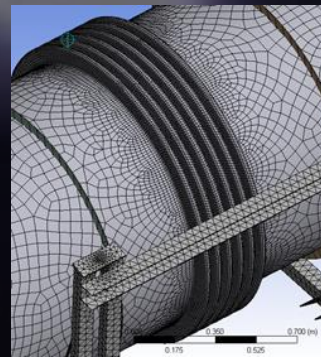
- 1.2 meter pipe-80 km total length (two arms)
- 1 meter clear aperture through the arm (alignment, straightness)
  - Straightness to 5 mm rms (beam transmission, diffraction). Differential GPS ~ 10mm/10km resolution? Concrete foundation.
  - Arms orthogonal to 5 mrad (max sensitivity, antenna directivity).
  - Low vibration (phase noise from scattered light). Low optical scatter surface, optical baffles. Seismic noise response.
  - Modal analysis. Suspension systems: bellows, anchor points, no stick-slip, bowing. Stresses-cycle fatigue (particularly w/alt. materials like aluminum-also post weld).
  - Bellows and anchor points to accommodate thermal expansion, atm. pressure, etc. Keep tube aligned. LIGO  $\Delta L/\text{temp} \sim 3.5$  meter.
  - Flanges for large gate valves, pumps, etc. Need to be compatible with standard SST construction.
  - Resist atm. pressure, buckling, vibrational modes, operational lifetime, etc. Support rings if thin wall or guard vac if nested.
  - Enclosure required? Accidental or malicious damage, ballistics, wind noise or resonance (Aeolian), lightning, corrosion?
- Beamtube materials costs (M's of kg). Cost of Cr and Ni also heat treatment if using SST (H<sub>2</sub>).



Hydroformed bellow and 48" GV



Modal analysis



Suspension and cover



# Beamtube requirements- Vacuum

- Vacuum requirements similar to LIGO
  - H<sub>2</sub> 1e13- Torr-liter/sec-cm<sup>2</sup>.
  - H<sub>2</sub>O 1e-16 Torr-liter/sec-cm<sup>2</sup>.
  - Low hydrocarbon flux.
  - Leak rate < 1e-10 Torr-liter/sec He
- Molecule size->polarization. Gas interaction scatter over path length. Phase noise, lowers h(f). Want both # density and amu low.
- Hydrogen diffusion, SST or Aluminum or Steel.
- Water expected to dominate spectrum.
- Keeping HC pressure low. Cleaning w/low waste stream-> low VOCs, ODP, phosphates, etc. Keep parts clean post cleaning-how?
- Bakeout required? Pumps, getters? Pump distribution? (no vibration)
- Low reflectance at 1 μm (laser frequency) desirable. Scattered light noise.

Parameter	Achieved in LIGO	Required for CE (1 μm)
L (m)	4,000	40,000
w <sub>0</sub> (mm)	62	83
h <sub>gas</sub> (Hz <sup>-1/2</sup> )	< 5 x 10 <sup>-25</sup>	< 5 x 10 <sup>-26</sup>
P[H <sub>2</sub> ] (Torr)	< 10 <sup>-9</sup>	< 10 <sup>-9</sup>
P[H <sub>2</sub> O] (Torr)	< 10 <sup>-10</sup>	< 10 <sup>-10</sup>
P[CO <sub>2</sub> ] (Torr)	< 2 x 10 <sup>-11</sup>	< 2 x 10 <sup>-11</sup>

$$h^2(f) = \frac{4\rho(2\pi\alpha)^2}{L^2v_0} \int_0^L e^{-\frac{2\pi\alpha(z)}{v_0}} \frac{dz}{w(z)}$$

$$v_0 = \sqrt{\frac{2kT}{m}}$$

ρ = particle density #/cm<sup>3</sup>; α = optical polarizability, cm<sup>3</sup>  
 v<sub>0</sub> = thermal velocity, cm/sec; k = Boltzmann constant  
 T = temperature, K; m = molecule mass, gm  
 L = arm length, cm; w(z) = optical beam radius at z, cm  
 f = frequency of gravitational wave, Hz; h(f) = GW strain, 1/√Hz

*The maximum allowed average pressure requirements for a 40 km detector with a sensitivity of h(f) = 1 × 10<sup>-25</sup> strain/√Hz at 300K and an optical wavelength of 1 μm.*

Gas species	ratio to H <sub>2</sub>	40km req torr	Gas species	ratio to H <sub>2</sub>	40km req torr
He	0.32	9.8 × 10 <sup>-9</sup>	Kr	8.27	1.4 × 10 <sup>-11</sup>
N <sub>2</sub>	0.89	1.3 × 10 <sup>-9</sup>	Xe	14.9	4.5 × 10 <sup>-12</sup>
H <sub>2</sub>	1.0	1.0 × 10 <sup>-9</sup>	AMU 100H <sub>n</sub> C <sub>m</sub>	38.4	7.0 × 10 <sup>-13</sup>
H <sub>2</sub> O	3.3	1.1 × 10 <sup>-10</sup>	AMU 200H <sub>n</sub> C <sub>m</sub>	88.8	1.4 × 10 <sup>-13</sup>
N <sub>2</sub>	4.2	6.5 × 10 <sup>-11</sup>	AMU 300H <sub>n</sub> C <sub>m</sub>	146	5.0 × 10 <sup>-14</sup>
A	4.51	4.9 × 10 <sup>-11</sup>	AMU 400H <sub>n</sub> C <sub>m</sub>	208	2.5 × 10 <sup>-14</sup>
CO	4.6	5.0 × 10 <sup>-11</sup>	AMU 500H <sub>n</sub> C <sub>m</sub>	277	1.4 × 10 <sup>-14</sup>
CH <sub>4</sub>	5.4	3.0 × 10 <sup>-11</sup>	AMU 600H <sub>n</sub> C <sub>m</sub>	345	9.0 × 10 <sup>-15</sup>
CO <sub>2</sub>	7.1	2.3 × 10 <sup>-11</sup>			

Note: Pressure requirements are set so that the noise from any single gas species can be no larger than 1/3 of the allowed strain noise. "Ratio to H<sub>2</sub>" means α/√v<sub>0</sub> for the gas relative to that of hydrogen.

Partial pressure requirements are similar to those achieved in LIGO

# Issue: Dealing with water outgassing

- Water *is* the problem.
- Distribution of binding energies
- Mid-range energies are the problem, high/low energies irrelevant.
- Either raise T (bake) or lower binding energy
- Coatings to lower energy?
- Many in the collaboration are studying this.

"Sojourn" time at room temperature vs energy\*

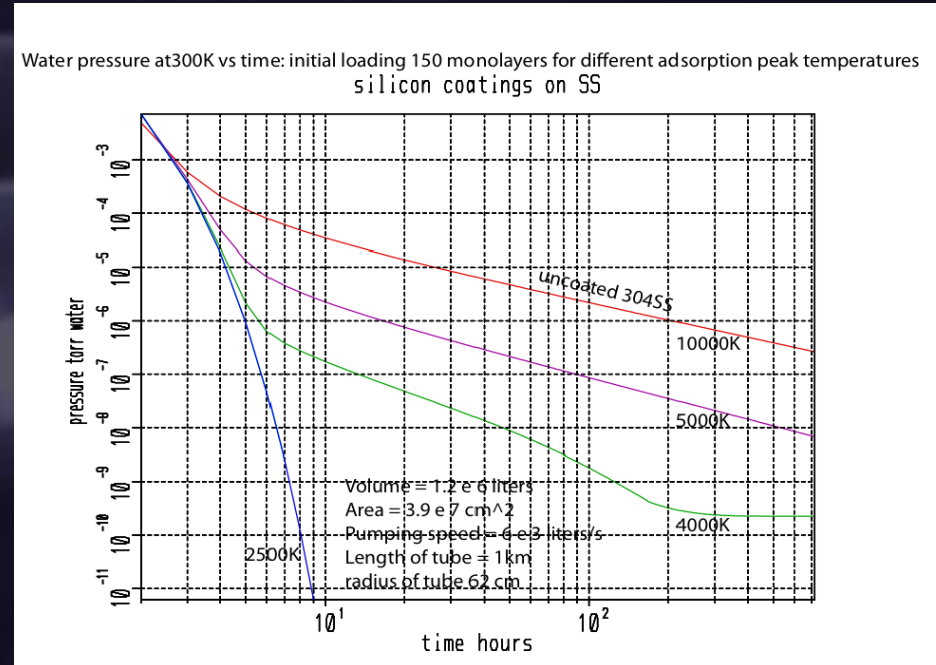
$E_b$ [kcal/mol]	$E_b$ [eV]	$\tau_a$	
1.4	0.06	$1.2 \times 10^{-12}$ s	} physisorption
3.5	0.16	$5 \times 10^{-11}$ s	
9.5	0.41	$1.2 \times 10^{-6}$ s	} weak chemisorption
14.3	0.62	$5.5 \times 10^{-3}$ s	
19	0.83	15 s	
21	0.93	15 min	} strong chemisorption
23	0.98	2 h	
24	1.04	$8 \times 10^4$ s ~ 1 d	
28	1.24	$2 \times 10^8$ s ~ 10 years	
35	1.55	$7 \times 10^{13}$ s ~ 20,000 years	

Water on SST ~ 1 eV

$$\tau_a = 1/\sigma = 10^{-13} \exp(E_b/kT)$$

# Pumpdown vs peak binding energy. Why coatings or other surface modifications could improve water desorption

- The  $1/t$  behavior of water pressure vs time. Typically wait  $>10^6$  sec at RT.
- Water binding energy on SST is around 1eV (24 kcal/mol).
- If a coating reduced the peak energy  $< 4000$  or 5000 K, bakeout would be unnecessary.
- Dubinin-Radushkevich Isotherm model shown (Weiss).
- Low-temperature bakeout-both Hanford and Livingston often 40C ambient temperature “summer bakeout” helps.
- Good  $p(t)$  models required.



A hydrophobic coating could make bakeout unnecessary

# LTREX experiment: An outgassing system using a residual section of LIGO beamtube



8m section of beamtube in storage at LLO ~ 20 yr



Tube being converted into UHV vacuum system



Delivery to Caltech



Installation

- 1.1 x 7.5 meter section of residual LIGO beamtube that stored at LLO since site construction. Removed from storage, flanges and end caps installed. Differentially pumped o-ring flanges. Helium leak testing and UHV performance verified. Mild (non-acid) cleaning processed to preserve surface chemistry. Matches LIGO beamtube surface- same low hydrogen air baked SST.
- Will be used for outgassing tests and dry-gas venting experiments and to verify isotherm models. Can we do a brief vent w/o rebake?
- Scale-up of Vortex tabletop system.



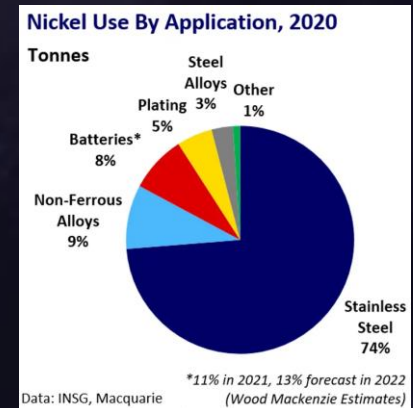
Currently under vacuum  $8 \times 10^{-9}$  Torr and being prepared for 150 C bakeout

# Alternate Construction methods

(how to beat the commodities market)

- Cheaper materials, alternate construction methods and/or processing
  - Ni is a commodity, used in SST, superalloys, also batteries including Li-ion, magnets, etc.
  - SST typically sells with a market surcharge.
  - Evaluate mild steel for beamtube (Park, et. al).
  - Use a low temperature (or skip) bakeout (LIGO electrical costs were \$1M/arm).
  - Are there coatings that reduce water desorption time?
  - Eliminate expense of concrete enclosure (BTE)?
  - A 1-meter diameter vacuum valve costs \$300k. Expect 1 valve/10km. Simplify?
  - Nested system: use very thin inner wall, i.e. use less of the expensive stuff.

SST follows nickel price-surcharges

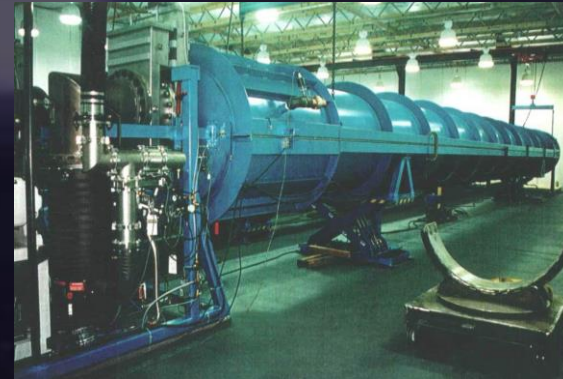


# Mild steel research summary

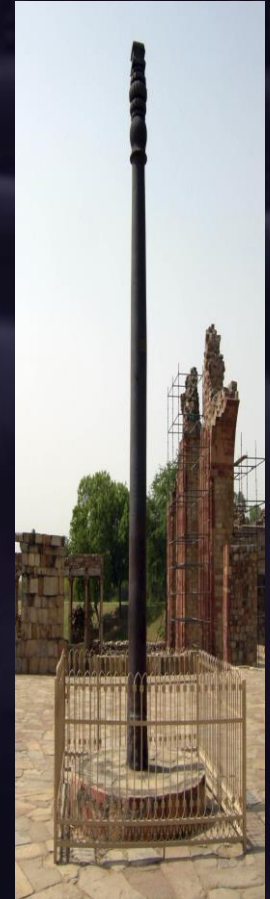
- Hydrogen bulk content and diffusion rate verified.
- Outgassing tests: CERN, NIST, others.
- Mild steel pipe: Preliminary report complete (Henkel). Boutique mill can easily provide standard material, possibly tweak alloy if warranted.
- Magnetite coating: Needs development: how to efficiently make coating, verify outgassing rate. Some preliminary results encouraging.
- SST to mild steel transitions  $\sim 7 \times 10^{-6}$ m/m-C CTE mismatch. Will make numerous CFF connections to std. vacuum equipment. Need to evaluate and manage.
- Scaling test of 20-40m beamtube, particularly induction heating test (LHO?)
- Vacuum component vendors typically do not allow mild steel fabrication in their shops due to “free-iron” contamination of the SST parts.

# Carbon (mild) steel pipe

- Gas/Petroleum pipeline
  - Inexpensive- estimated saving \$300M vs SST.
  - Available- 80 km is actually “small” order.
  - Shipped from factory with rail transport to site. (LIGO tube was made on-site).
  - QA system in place (fuel gas pipeline safety-US DOT).
  - **No helium leak testing**- revive LIGO leak test system?
  - ½” thickness- 380 kg/m. Tube is stable to atm pressure, buckling, resistant to mechanical damage.
  - No support rings needed. Suspension system (and cover) design TBD.
  - Corrosion? (epoxy, but what happens if it covers a vacuum leak?)
  - Magnetite ( $\text{Fe}_3\text{O}_4$ ). Outgassing and optical scatter, mild corrosion protection.
  - Other coatings?



Helium leak test system for 20m LIGO tubes



Iron pillar of Delhi  
400 AD  
 $\text{FePO}_4$   
“Parkerized”  
Coca-Cola



# Carbon steel pipe

- Pipe factory

- Nominal ½" wall thickness. 48" diameter.
- Self supporting (no stiffening rings needed).
- Spiral welded (LIGO same).
- Low hydrogen outgassing.
- Surfaces options.
  - Bare (corrosion "bad rust")?
  - Silica (CVD process) ?
  - Magnetite ( $\text{Fe}_3\text{O}_4$  "good rust")?
  - External-epoxy coating. Outgassing?
  - Magnetic, can be induction heated.



24m sections of spiral welded steel pipe.  
This mill makes about 500km/year\*

D. Henkel (invited talk 3/27 @ 13:30) surveyed pipe mills

# Hydrogen outgassing stainless steel vs carbon steel comparison

- H<sub>2</sub> diffusion from bulk
  - Hydrogen dissolved in the metal when molten.
  - t=0 concentration starts with the material manufacture
  - SST requires vacuum degassing or air oxidation to reduce H<sub>2</sub> diffusion
  - LIGO beamtube SST was oxidized prior to rolling
- Mild steel has extremely low intrinsic hydrogen
  - Vacuum degassing lowers dissolved gas, mainly hydrogen
  - Old textbook H<sub>2</sub> values obsolete.
  - Mild steel lower H<sub>2</sub> diffusion than the best LIGO SST
  - Verified low H<sub>2</sub> concentration and diffusion rate
    - Park et.al JVST A 26 (5) 2008
    - NIST (Fedchak)
    - CERN

**Description:** Four Steel samples were analyzed as listed below.

**Results:**

<u>Sample Identification:</u>	<u>Hydrogen</u>
	<u>ppm</u>
A36 Steel # 1	0.5
A36 Steel # 2	0.5
304L Blank	3.6
316L Blank	1.9

Method: Vacuum hot extraction - ASTM E 146-83

H<sub>2</sub> concentration A36 mild vs 304L stainless steel using vacuum hot-extraction testing method

Low intrinsic hydrogen in mild steel verified

# Silica coatings-Silane decomposition

- CVD process.
- Silane precursor  $\text{SiH}_4$
- Proprietary process.
- CERN reports hydrogen uptake in the strips.
- Does improve outgassing but at what cost/benefit?
- Layer probably too thick (JRF).
- Dust and particulates.
- Practical on huge beamtube sections?



Above: Test strips ( mild steel and SST) coated with silica. Below: A36 steel test chamber was also coated. The chamber is at now at NIST.



Strips being prepared for Silane CVD coating

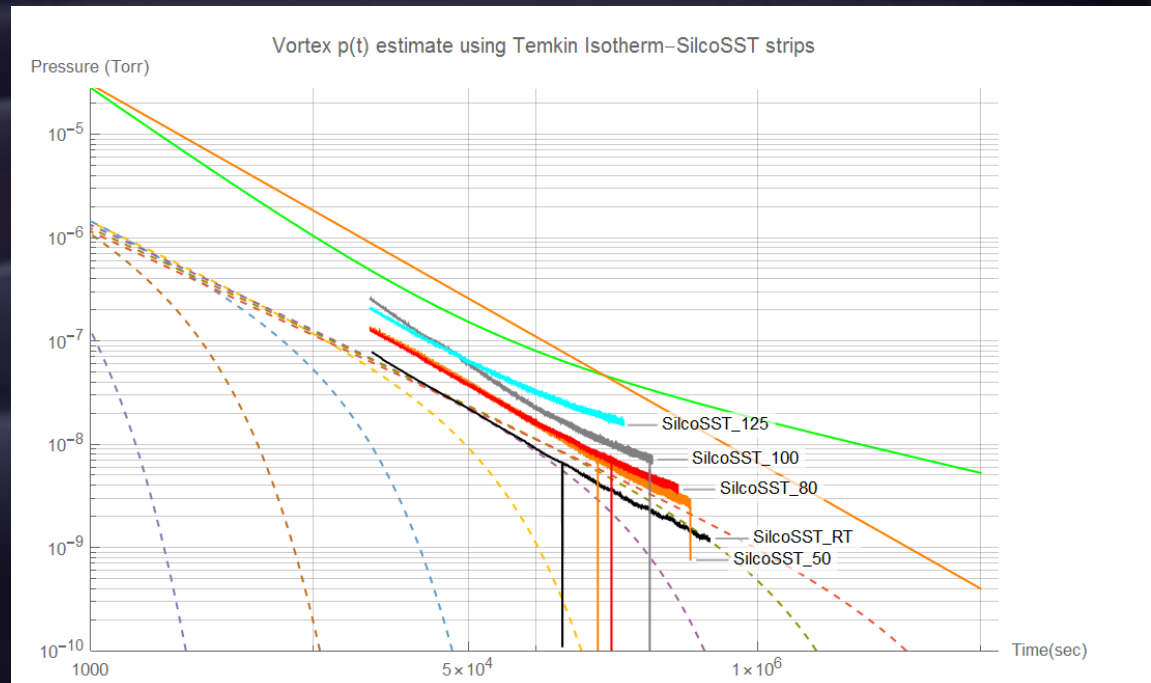
Si-based coating reduces outgassing  $\leq 10x$ .  
Helpful but CVD process too complex for this application

# Thermal outgassing: Temkin Isotherm model $E_0=10.6$ kcal/mol, $E_1=25$ kcal/mol . CIT benchtop system

- Temkin Isotherm.
- $T=300$ K.
- Dashed lines are  $p(t)$  at various energies.
- Green, Orange lines are Li/Dylla\* models for SST pumpdown, show  $1/t$  behavior.
- Still looks like stainless?
- Possible explanation in Y2000 patent?

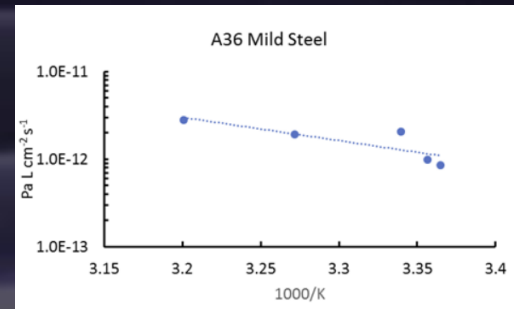
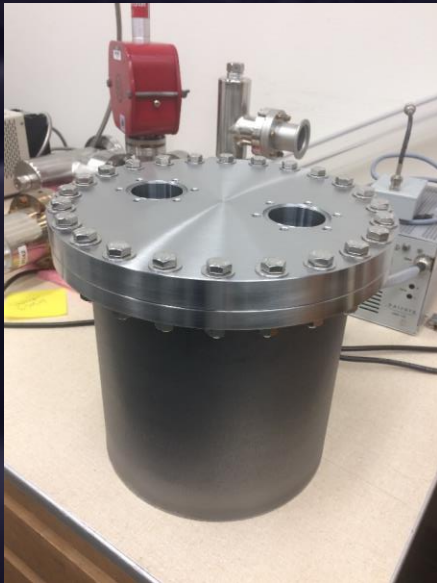


Vortex thermal outgassing system at CIT



\* Minxu Li and H. F. Dylla , Journal of Vacuum Science & Technology A 12, 1772 (1994)

# Outgassing tests at NIST

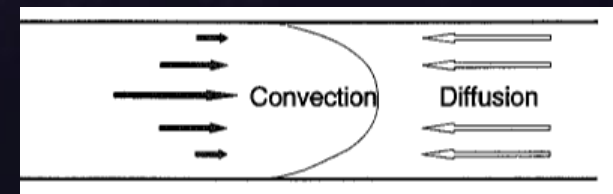
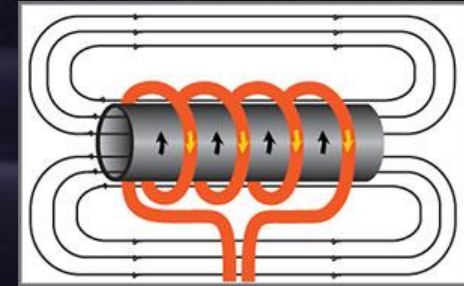


Mild-steel vacuum test chamber made from A36 mild steel. H<sub>2</sub> outgassing measured by NIST using spinning rotor gauge. Technique described in J. Fedchak, *JVST B* **39**, 024201 (2021).

Invited talk J. Fedchak 3/28 @ 09:00

# Traveling Bakeout System?

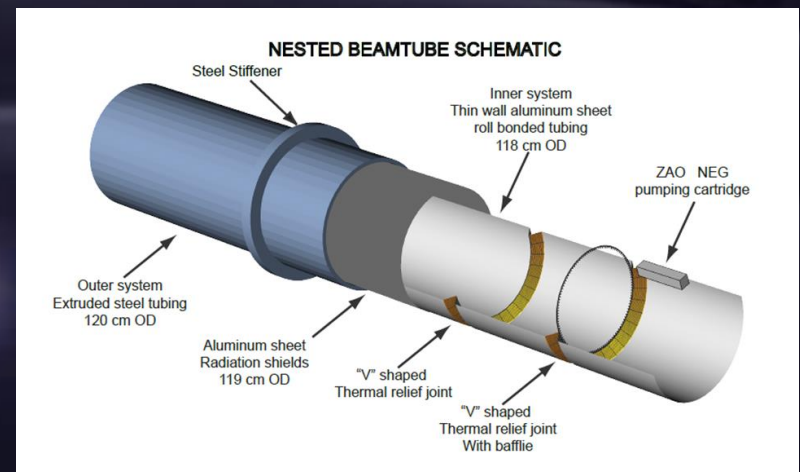
- Thought experiment
  - Heat pipe with traveling heater while flowing ultra-dry gas to prevent recontamination
  - Temperature and flow rates?
  - How to heat the pipe.
  - Practicality?
- RF Induction heating (the easy part)
  - Eddy current and magnetic hysteresis loss.
  - Works best on magnetic materials.
  - 10-30 kHz for pipe.
  - Turn-key for pipeline heating.
  - Purge with ultra-dry (< ppb) air.
  - Low conductance so vacuum ineffective.
- Now the hard part....
  - Back-contamination with water vapor.
  - Balance flow rate out with diffusion back in.
  - Common technique in semiconductor gas systems.
  - Flow rate may be unmanageable. Throttle ?.
  - Active research. Model and scale tests.



# Nested System

- **Complex but has several unique features**

- Steel outer pipe (thickness TBD) with thin (1/2 mm) aluminum inner pipe (could also be thin steel).
- Modest vacuum ( $10^{-4}$  Torr) in annular gap.
- Thin inner liner resistively heated to bake (same as LIGO).
- Aluminum is excellent vacuum material. Reflectivity at  $1\mu$ ?
- Spiral formed and cold welded (new technology).
- Gap vacuum: Thermal insulation, crush of inner tube, allows some leaks in inner liner.
- Complex thermal/electrical isolation, valves need to be developed, unique feedthroughs and ports, manage 2x CTE mismatch between inner and outer systems.
- Updated design (May 2022) both tubes are steel.
- ZAO Getter pumps-require feedthroughs to heat. Water speed?
- Hide ZAO getter behind baffle.



Proposed by R. Weiss

# Summary

- Tasks started
  - Mild steel outgassing characterization.
  - Hydrogen content A36 steel.
  - Pipe mill inquiries and tube mfg. details.
  - Silica coatings prepared, tested.
  - Tube travelling heater/bake funded.
  - LTREX experiments underway.
  - Ultra-dry air benchtop tests started (Vortex).
  - Coaxial alternate system conceptual design.
  - Back-diffusion modelling.
- Tasks needing effort
  - **Welding and joining methods-dissimilar metal.**
  - **Alternate coatings.**
  - **Gate valve(s)-design details.**
  - **Coaxial system-design details.**

