



Vacuum measurements of materials and coatings for GWD beampipes

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OUTLINE

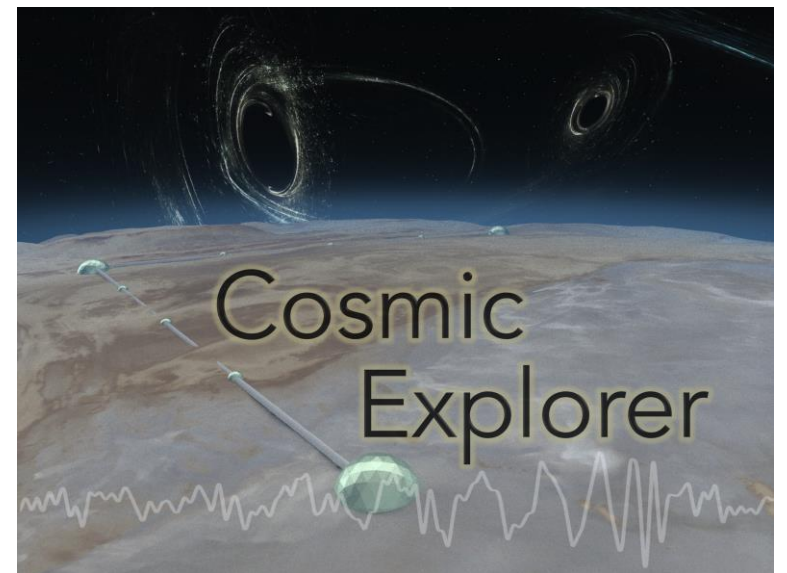
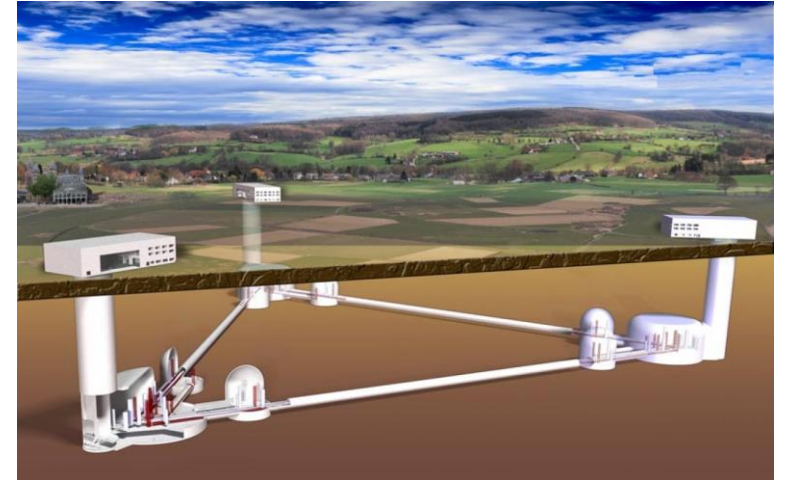


- ❖ INTRODUCTION
 - ✓ Cost reduction guidelines

- ❖ MILD STEEL
 - ✓ Samples
 - ✓ Water outgassing
 - ✓ Hydrogen content
 - ✓ Hydrogen outgassing
 - ✓ Total outgassing

- ❖ SILICON COATING
 - ✓ Samples
 - ✓ Water outgassing
 - ✓ Hydrogen content
 - ✓ Hydrogen outgassing

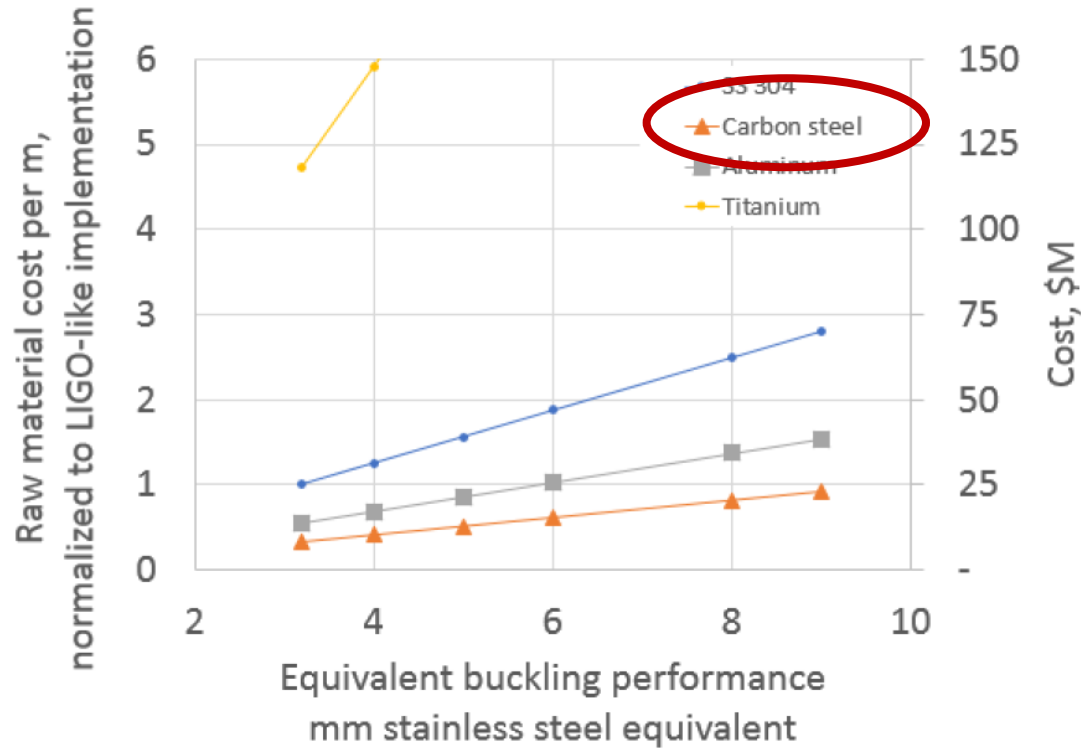
- ❖ CONCLUSIONS



Cost reduction guidelines

Beamtube material

Bake-out



Lower bake-out temperatures for longer durations

Beamtube coatings with low water vapor binding energy:

magnetite Fe_3O_4
silicon

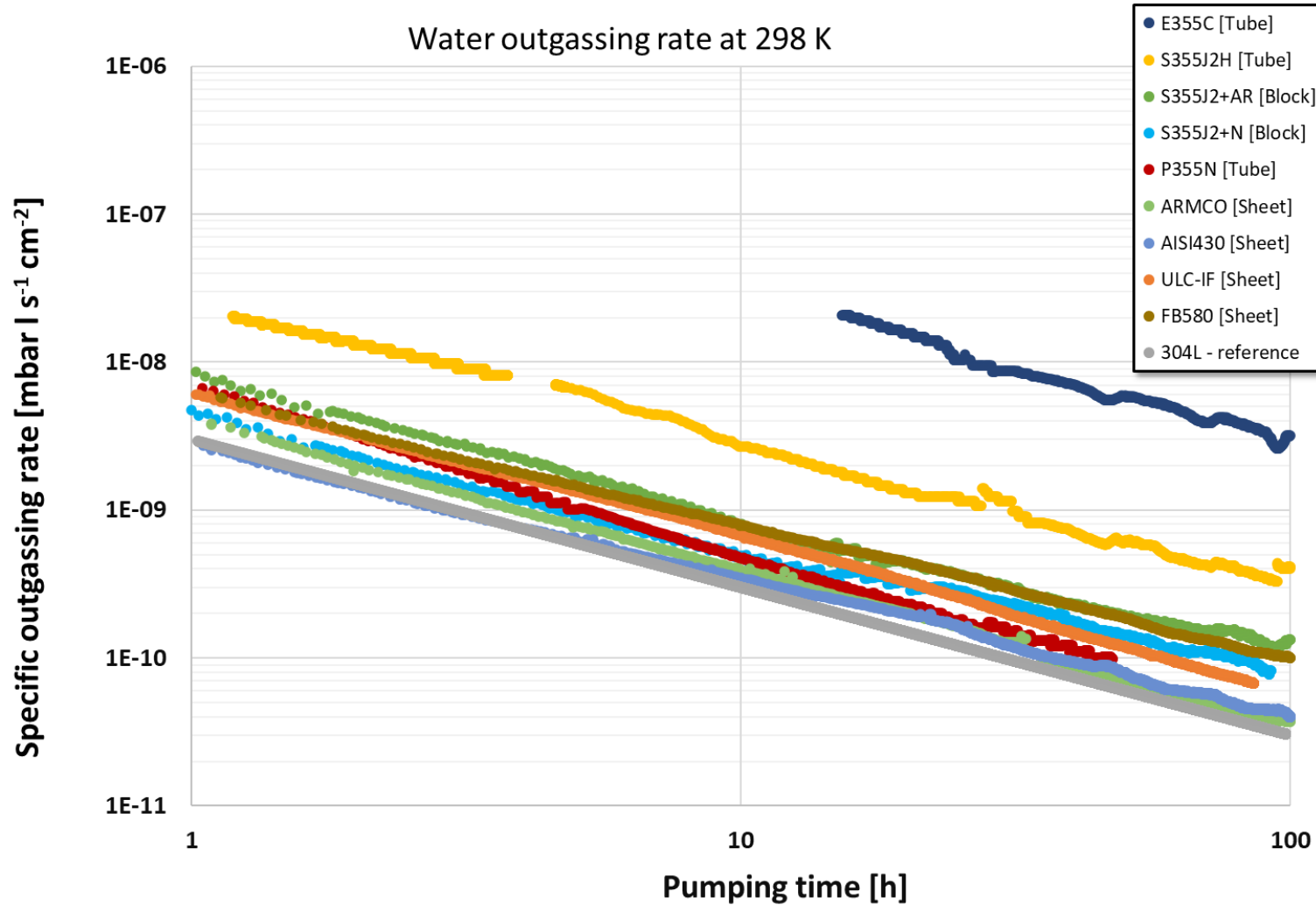
Mild Steel

Materials & Methods

| Class | Grade | Shape |
|--------------------|------------|-------|
| Ferritic/pearlitic | P355 | Tube |
| | E355 | Tube |
| | S355J2H | Tube |
| | S355J2+N | Block |
| | S355J2+AR | Block |
| Ferritic/bainitic | FB580 | Sheet |
| Ferritic | ARMCO | Sheet |
| | ULC-IF | Sheet |
| Ferritic (SS) | AISI430 BA | Sheet |

| Method | Result |
|----------------|--|
| TDS | H content |
| Pumpdown | H ₂ O outgassing |
| Coupled method | H ₂ , CH ₄ , CO & CO ₂ outgassing |
| Binding energy | H ₂ O binding energy |

Mild steel: Water outgassing

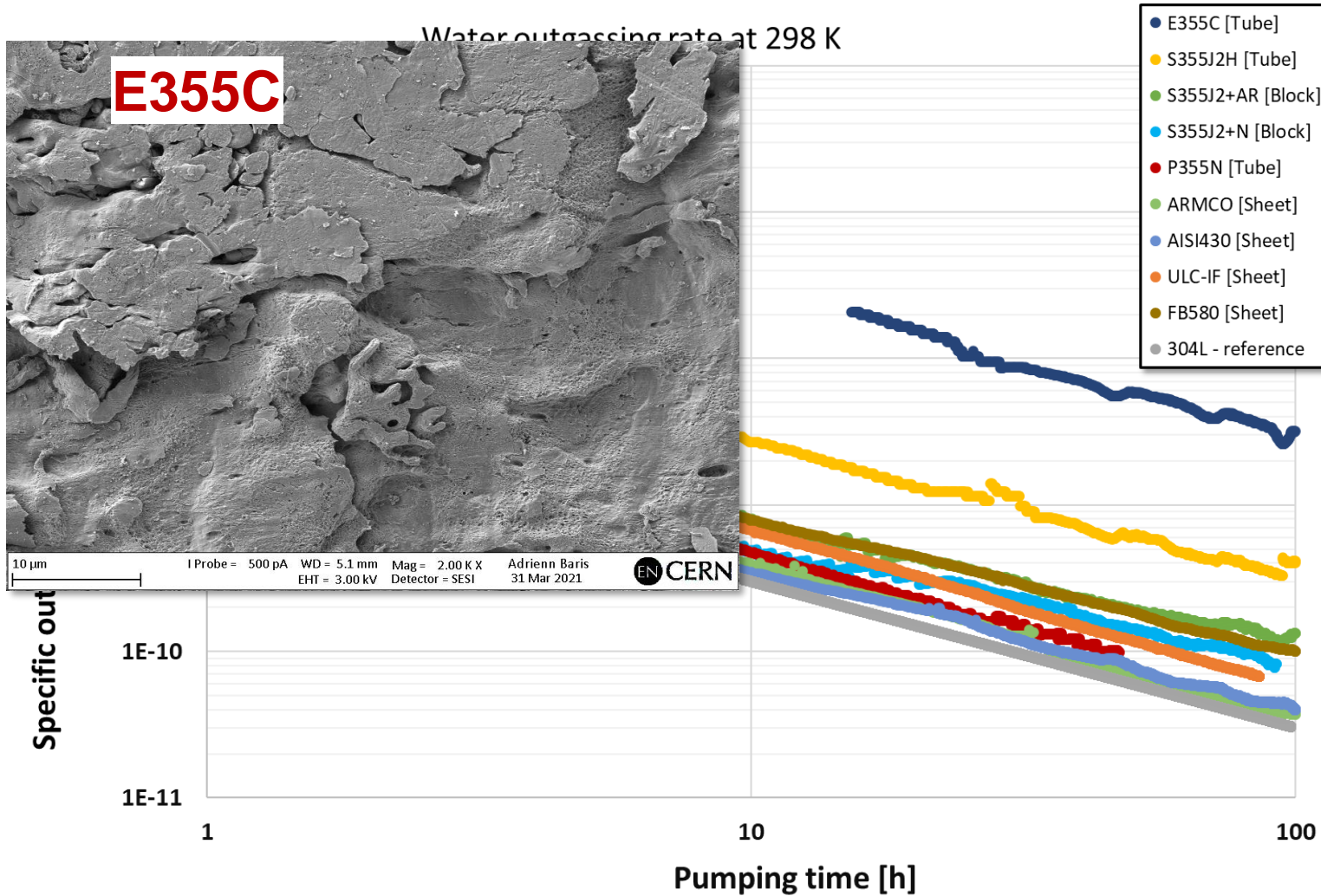


| Sample | Q_{10h} [mbar l s ⁻¹ cm ⁻²] |
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| E355C | $3.0 \cdot 10^{-8**}$ |
| S355J2H | $2.7 \cdot 10^{-9}$ |
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| ARMCO | $3.9 \cdot 10^{-10}$ |
| AISI430 BA | $3.5 \cdot 10^{-10}$ |
| 304L | $3.0 \cdot 10^{-10[1]}$ |

Data contribution by A. Michet & N. Thaus

1 Chiggiato P., Outgassing properties of vacuum materials for particle accelerators. arXiv. 2020. <https://doi.org/10.48550/arXiv.2006.07124>

Mild steel: Water outgassing

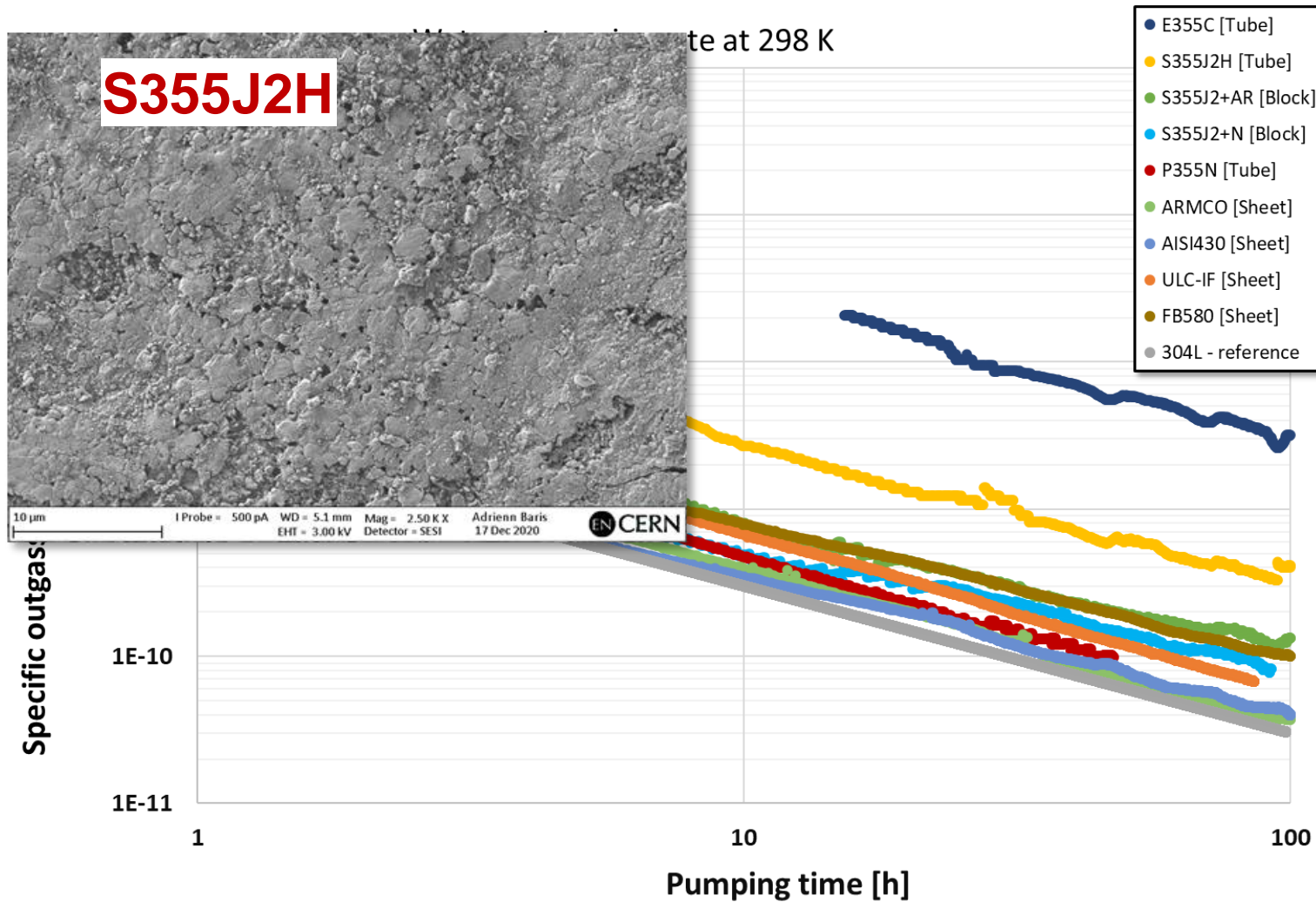


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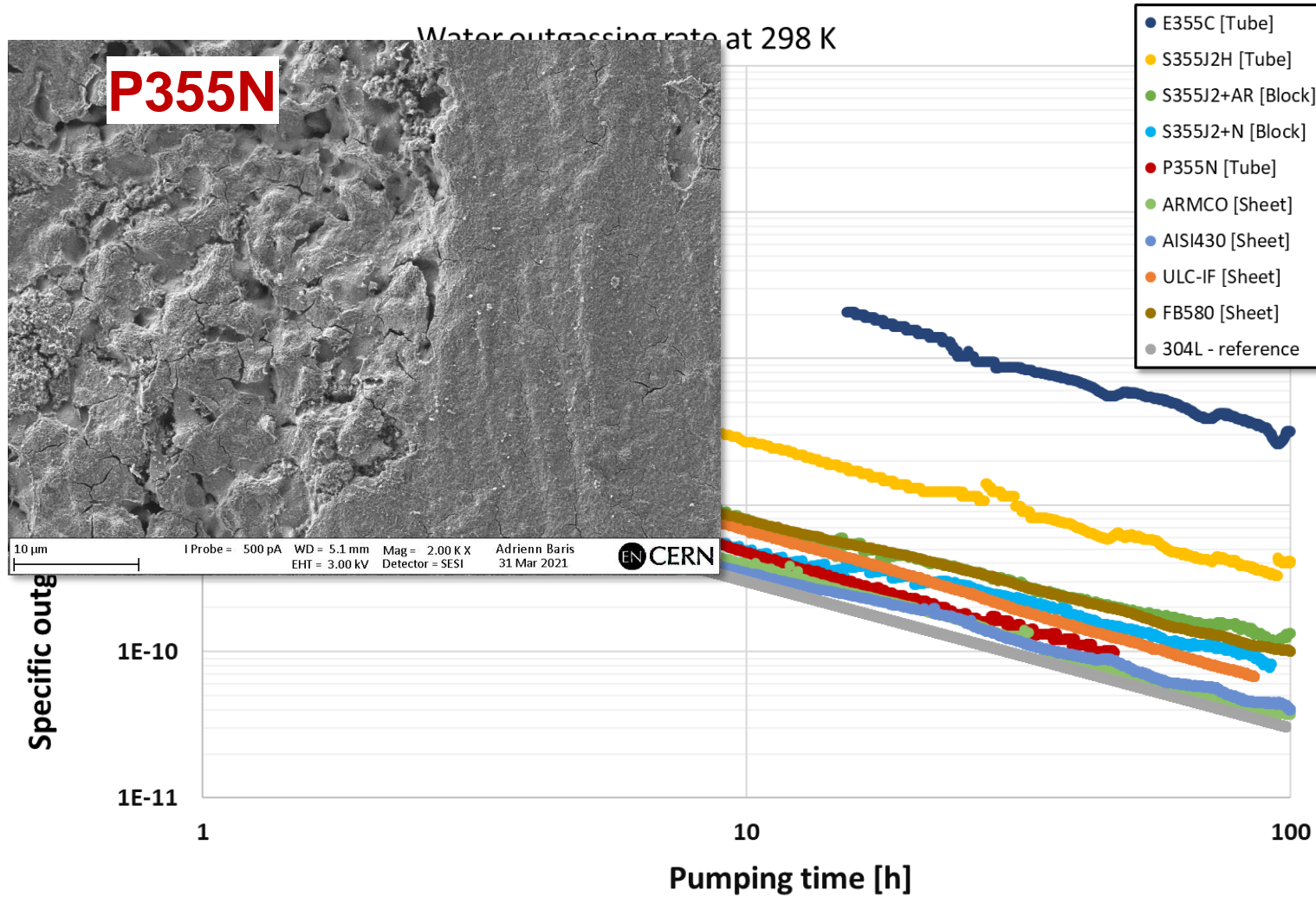


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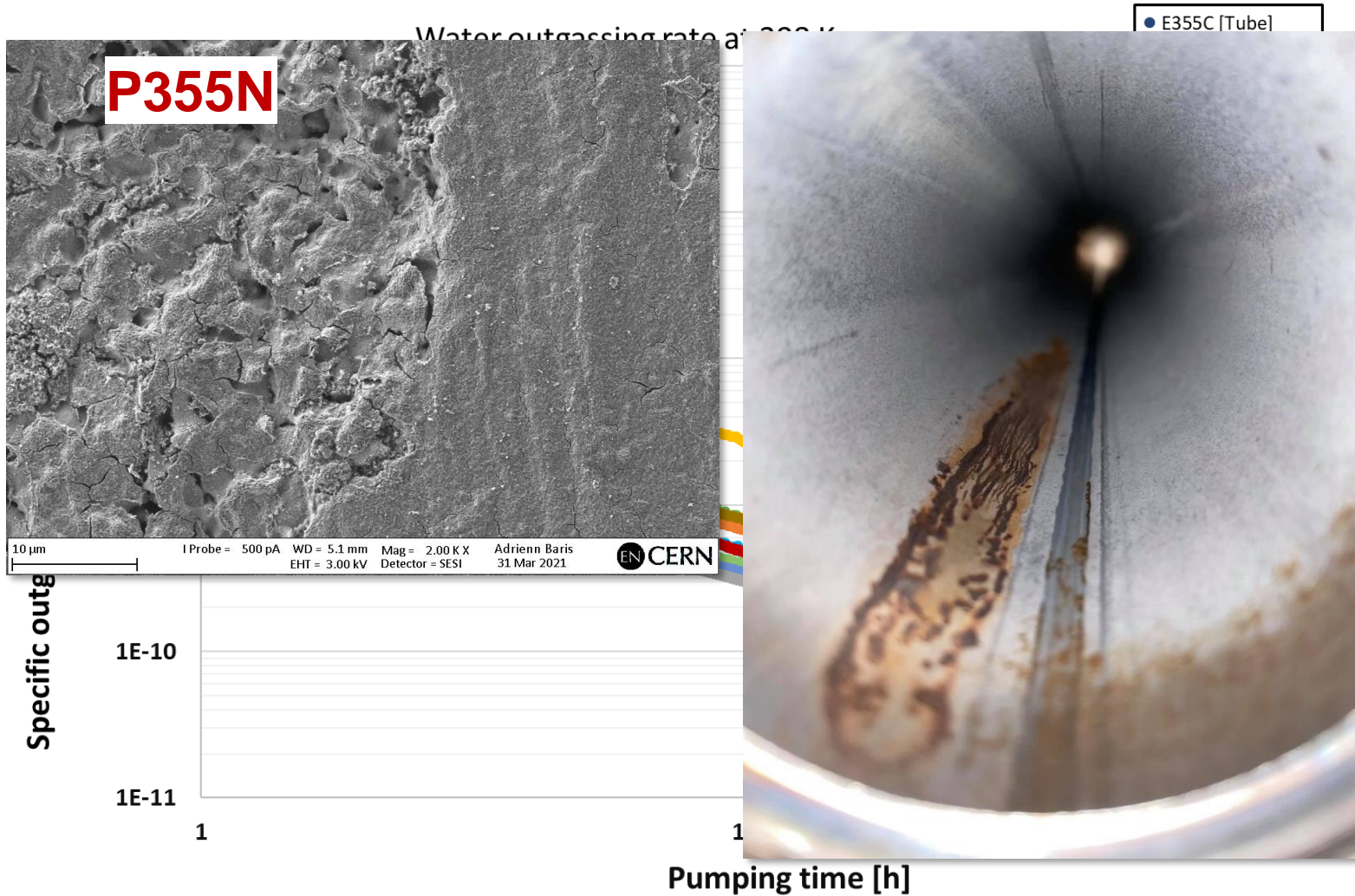


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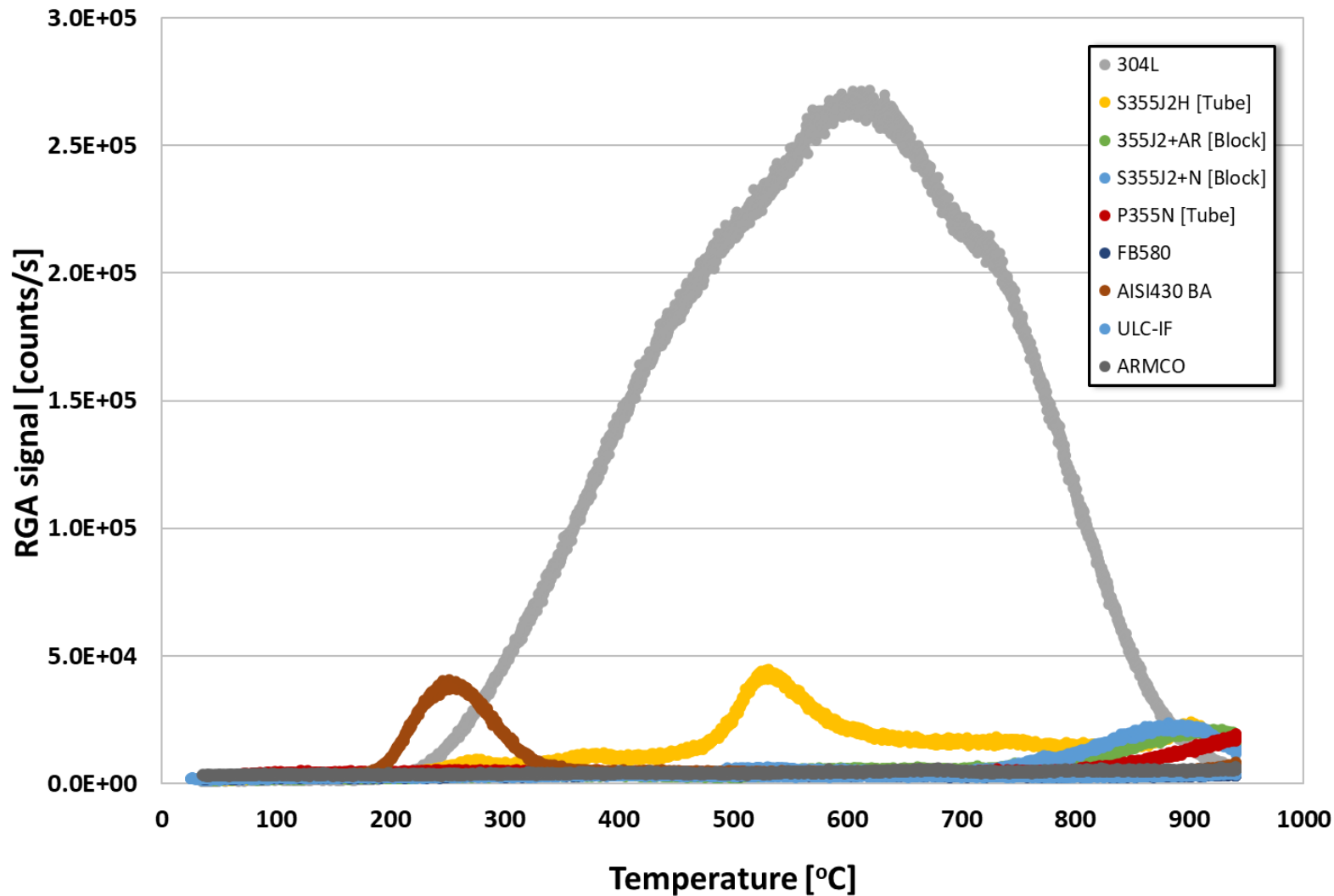


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Mild steel: Thermal desorption

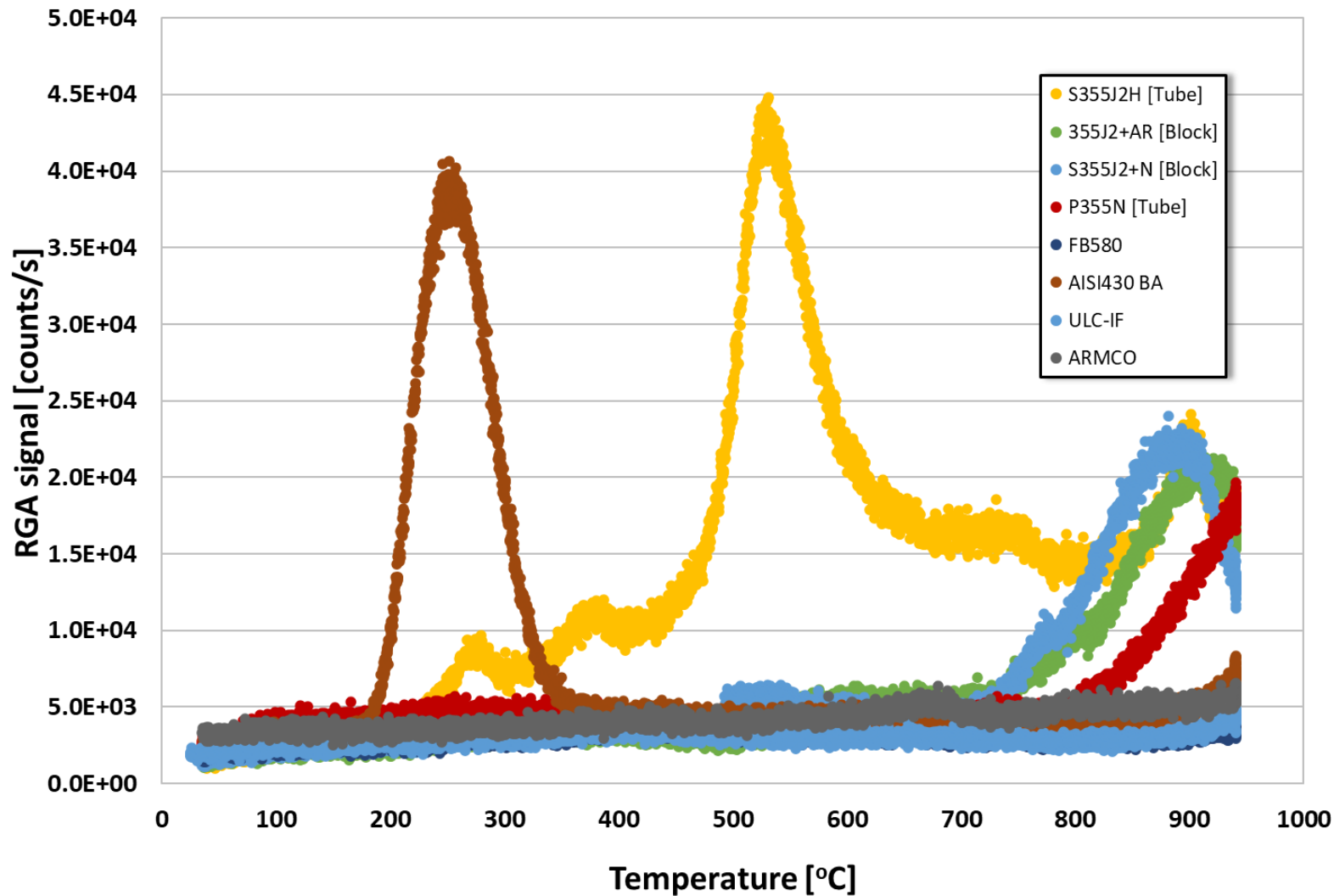


| Sample | Released H ₂ [ppm at.] | Thickness [mm] |
|------------|-----------------------------------|----------------|
| 304L | 80 | 3 |
| S355J2H | 7.8 | 4 |
| S355J2+AR | 2.0 | 3 |
| S355J2+N | 1.6 | 3 |
| P355N | 1.0 | 3.5 |
| FB580 | 2.8 | 2.1 |
| AISI430 BA | 8.3 | 2 |
| ULC-IF | 3.7 | 0.69 |
| ARMCO | 1.2 | 2 |

Data contribution by A. Michet

*Quantities of released hydrogen are calculated up to 850°C

Mild steel: Thermal desorption

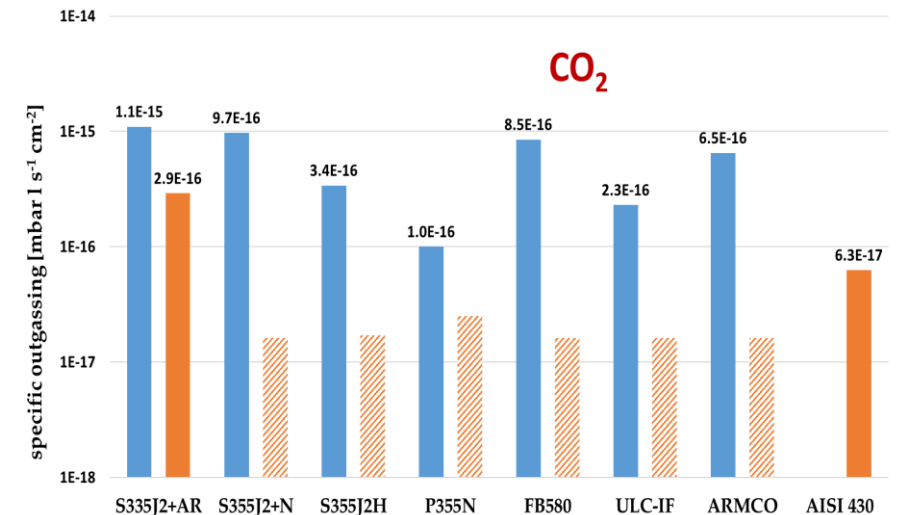
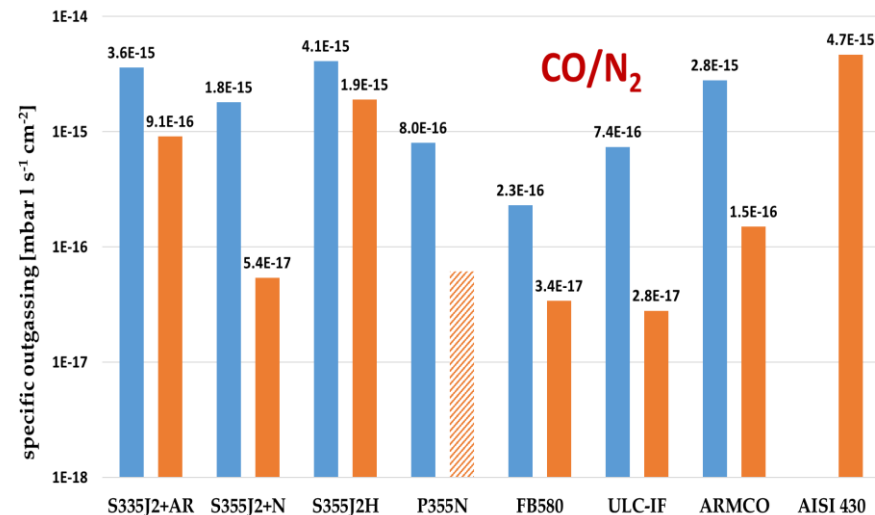
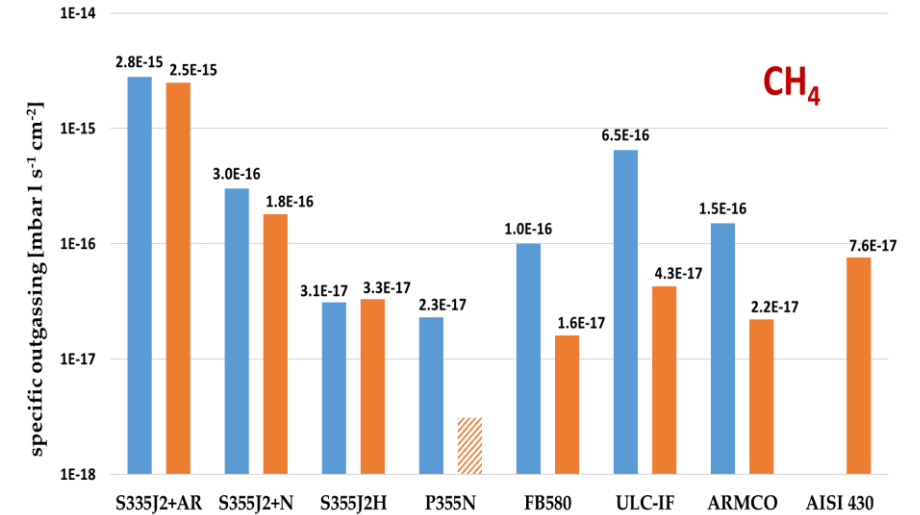
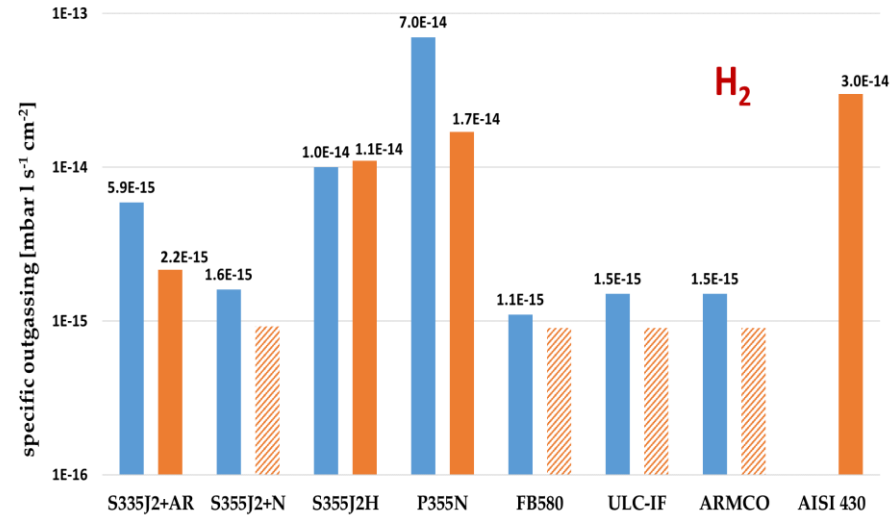
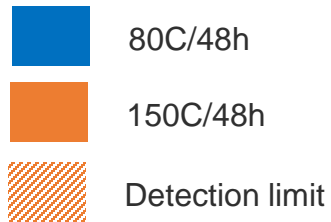


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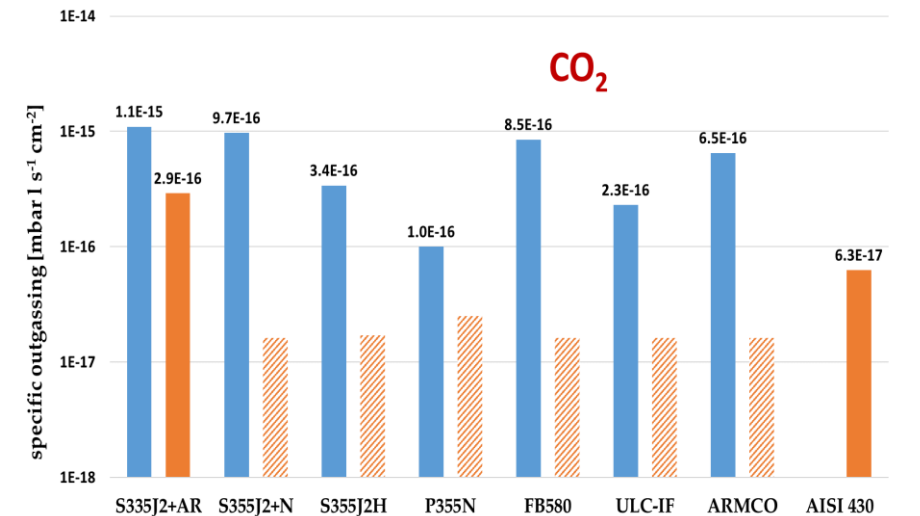
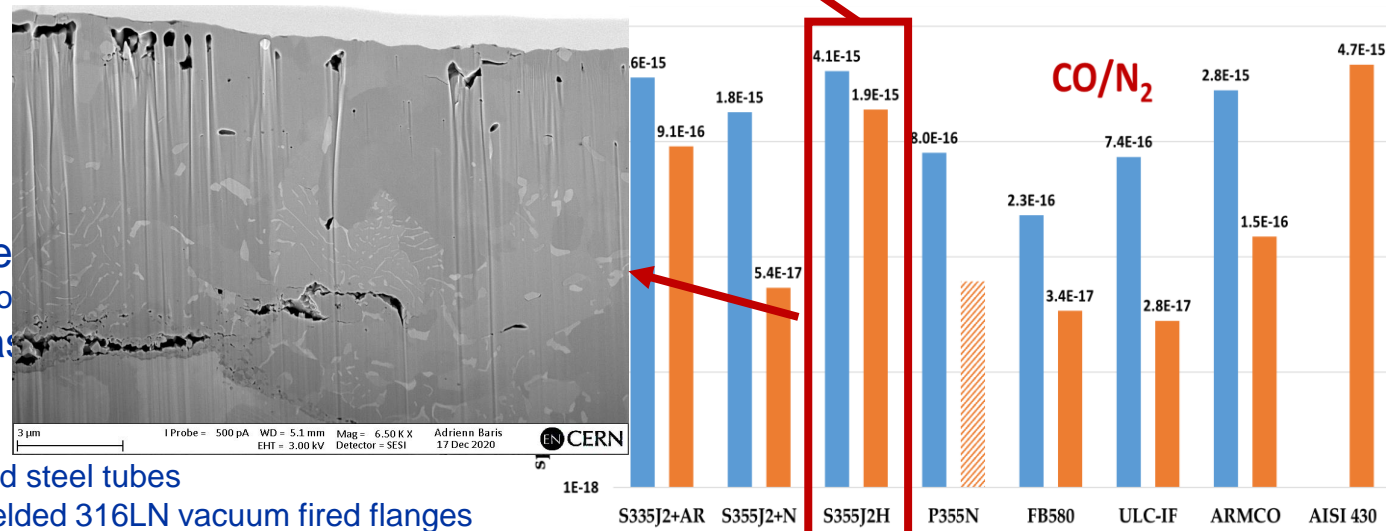
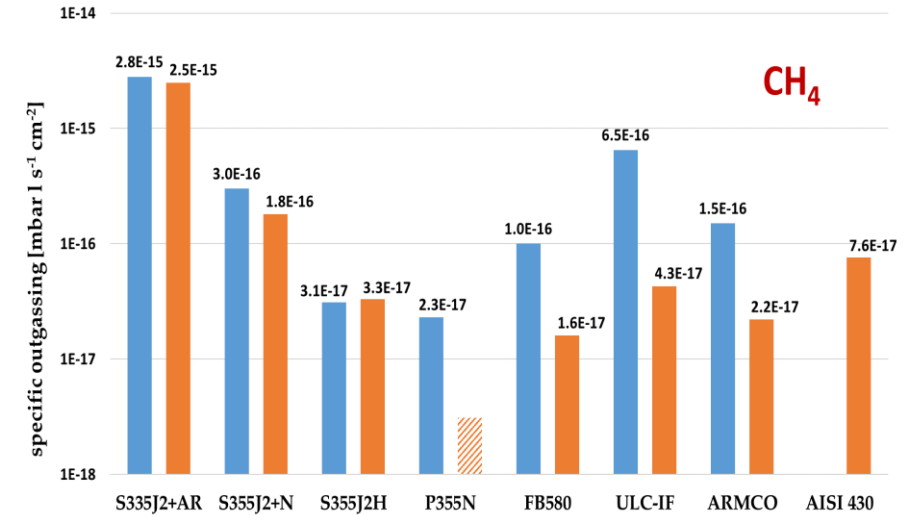
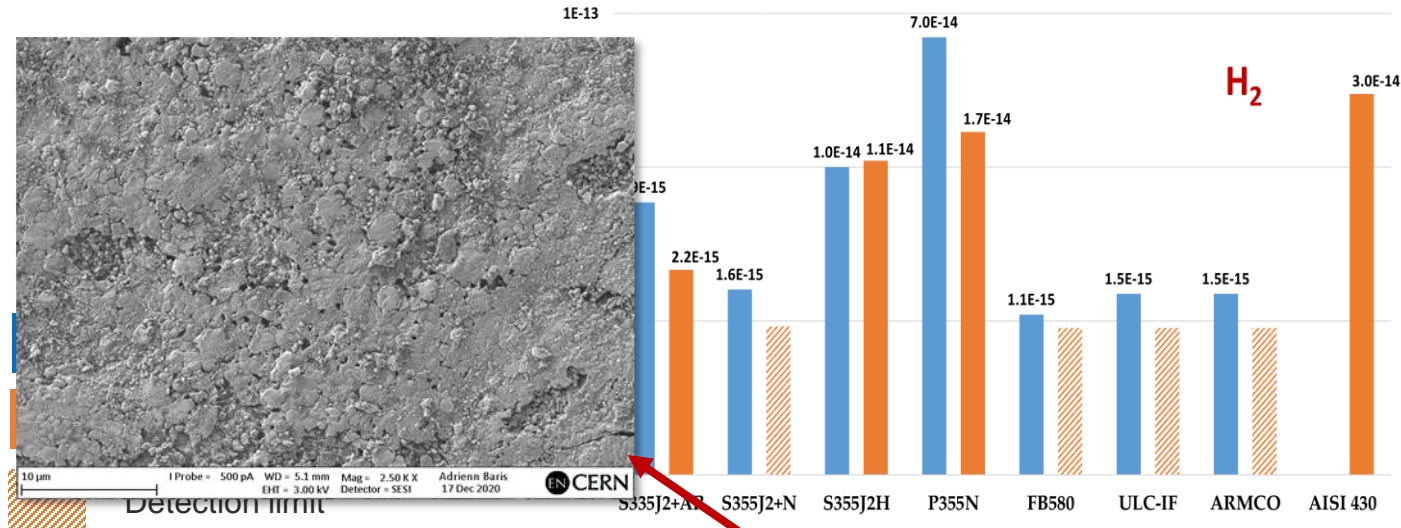
*Quantities of released hydrogen are calculated up to 850°C

Outgassing – coupled method



- Detection limit**
 50% of background
Measurement error
 40%
Mild steel vacuum chamber
 - Mild steel tubes
 - Welded 316LN vacuum fired flanges

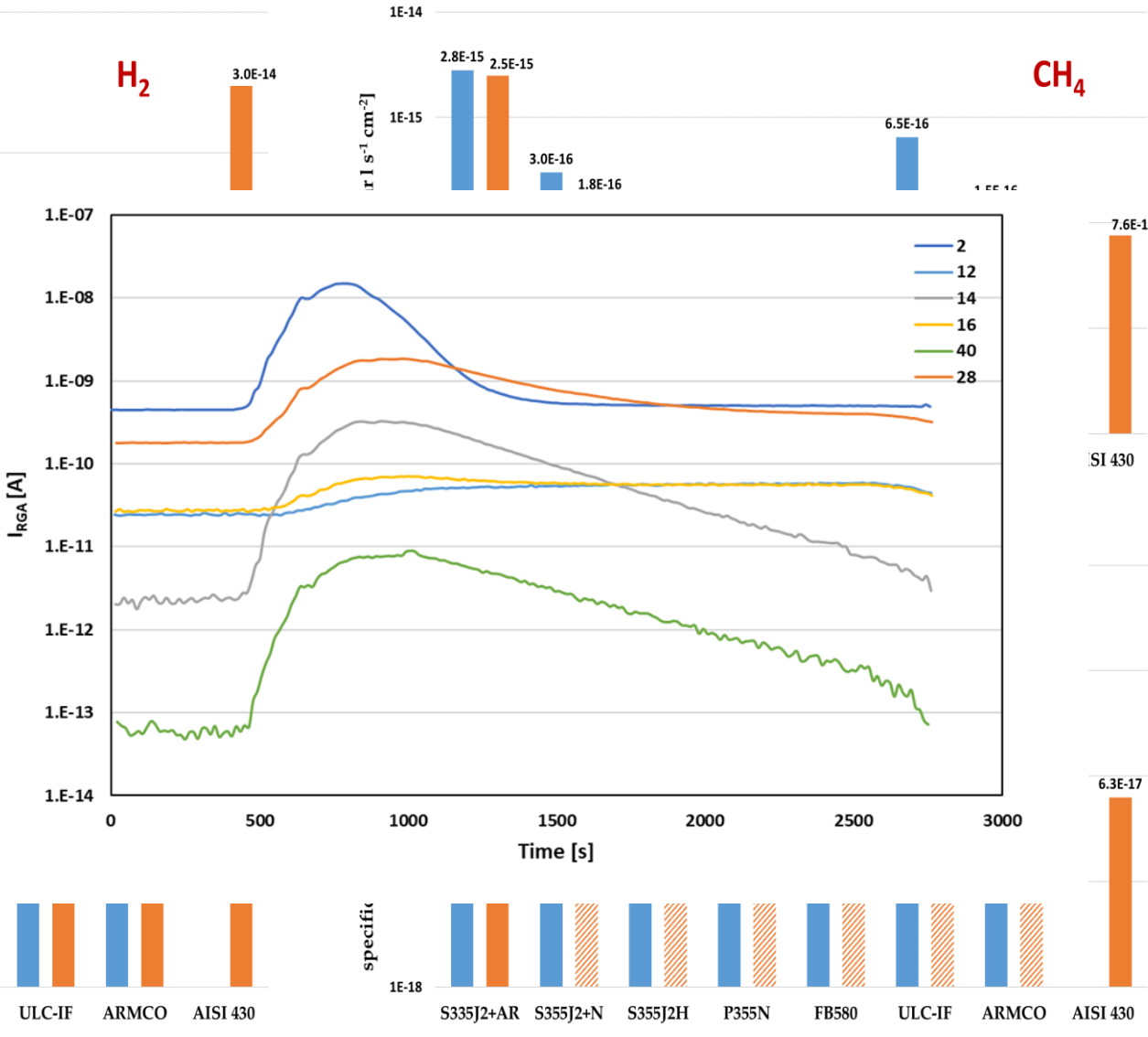
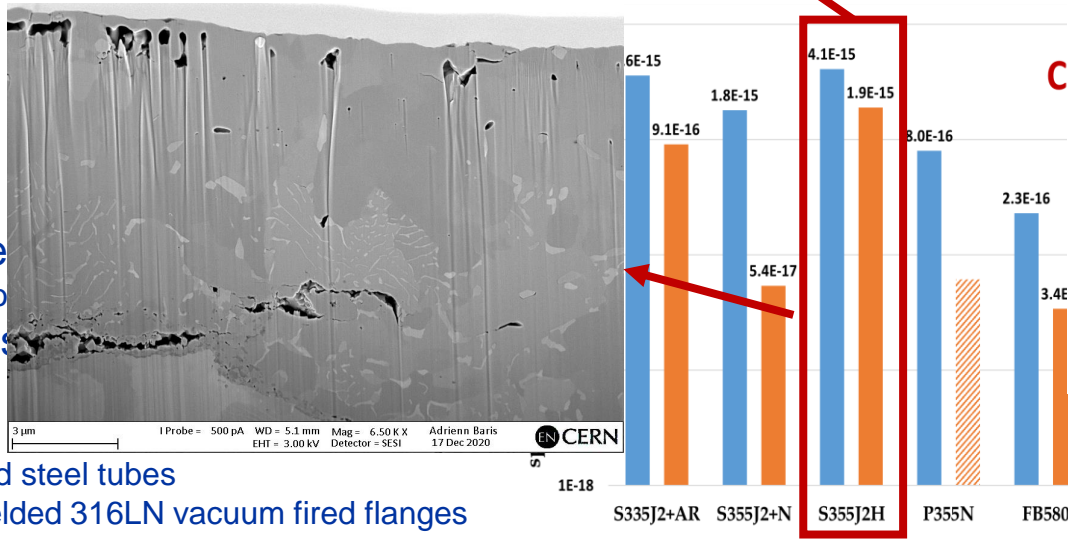
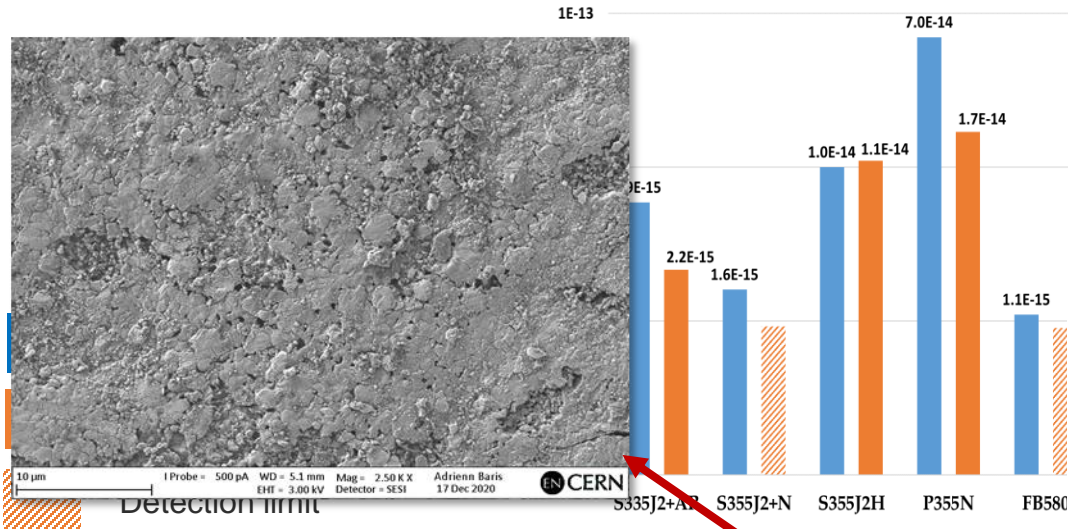
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Meas
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Mild

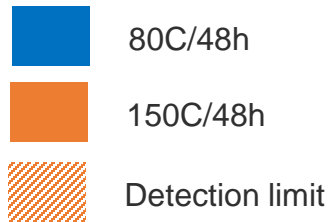
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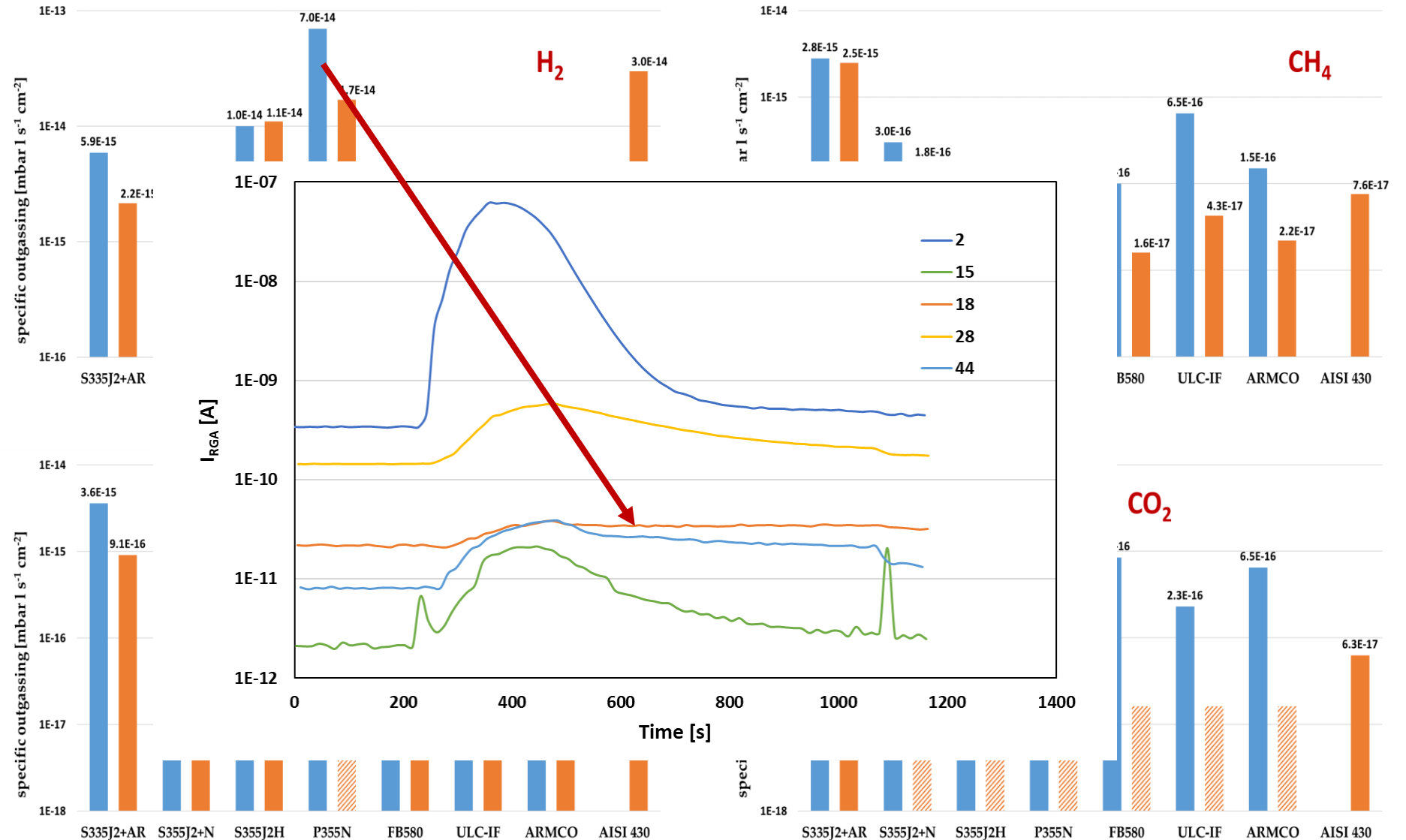


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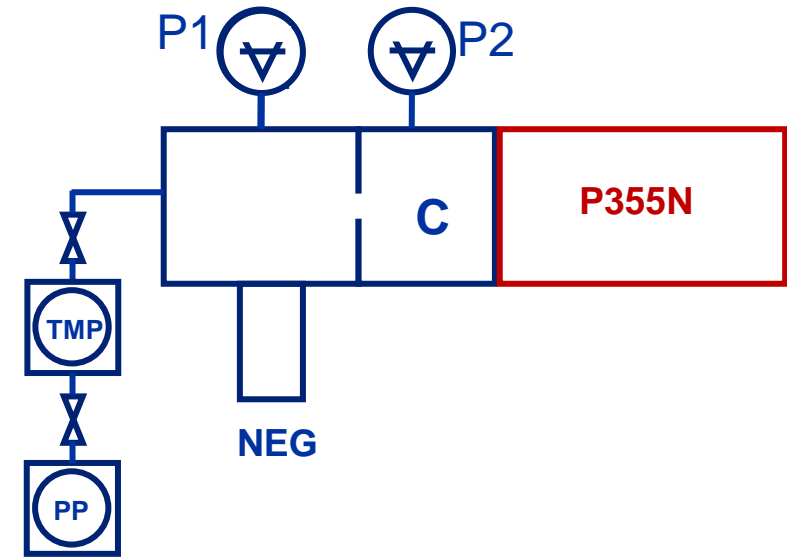
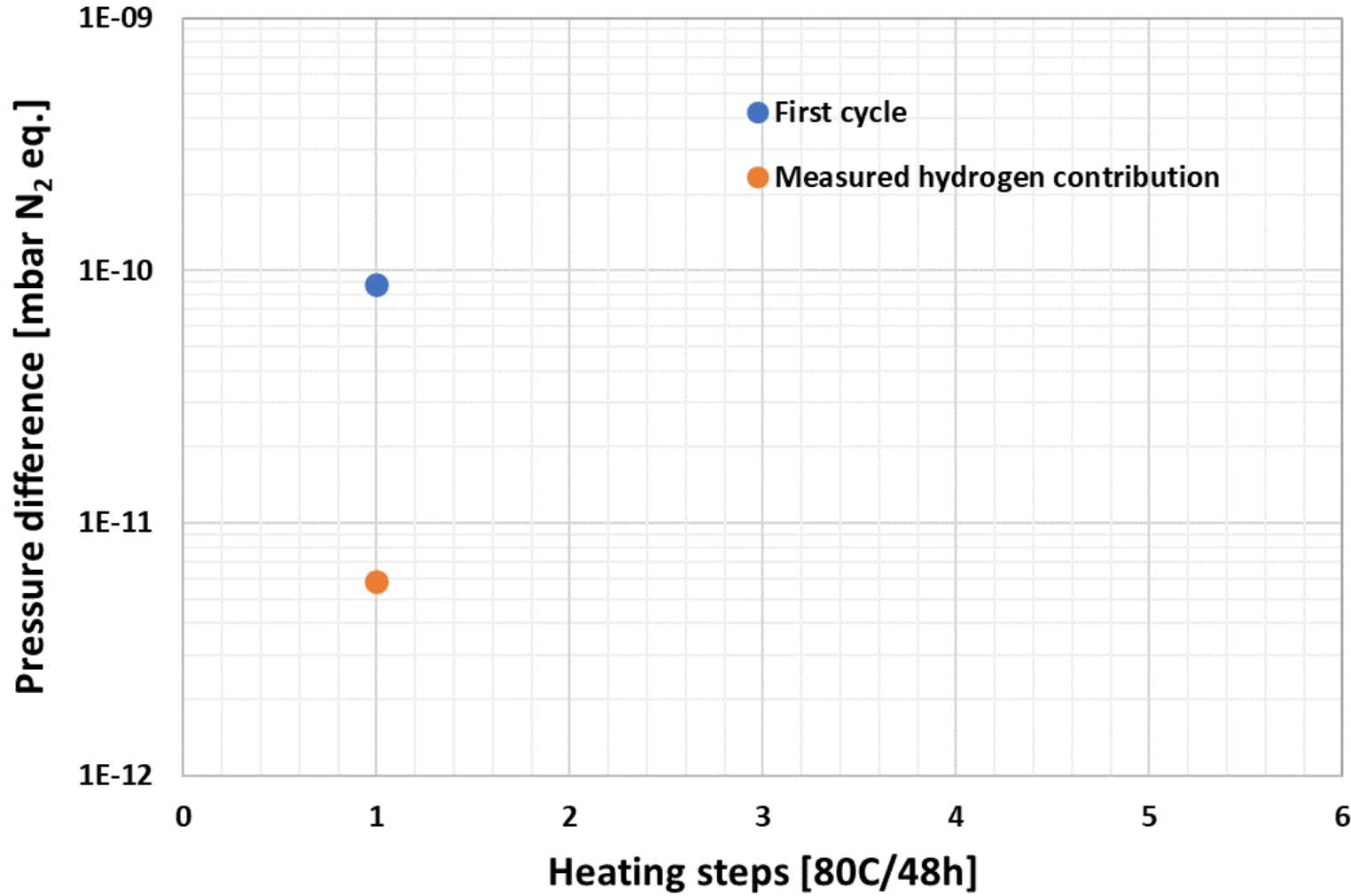
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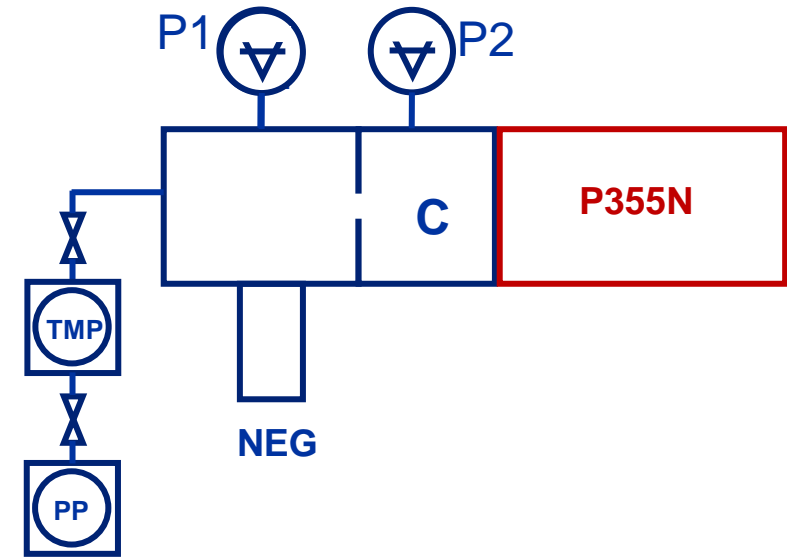
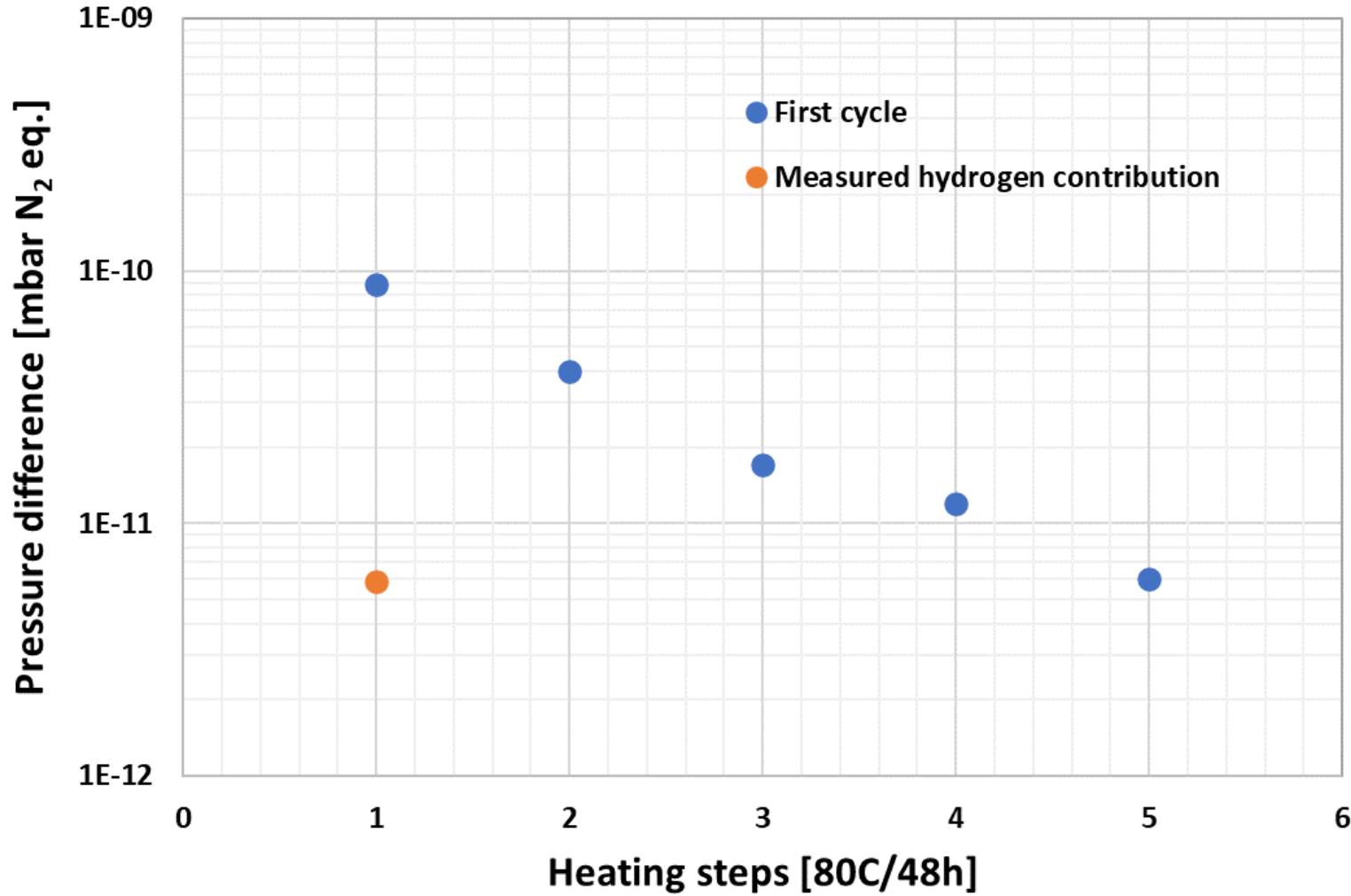


Ultimate pressure – P355N



- ❖ Throughput system: \varnothing 10 mm orifice – Surface area P355N chamber = 6333 cm²
- ❖ Background pressure removed
- ❖ The hydrogen outgassing rate of an as-received chamber after heating 80°C for 48 hours is $7 \cdot 10^{-14}$ mbar l s⁻¹ cm⁻². The outgassing rates of the other gasses (CH₄, CO/N₂ and CO₂) are at least 10x lower

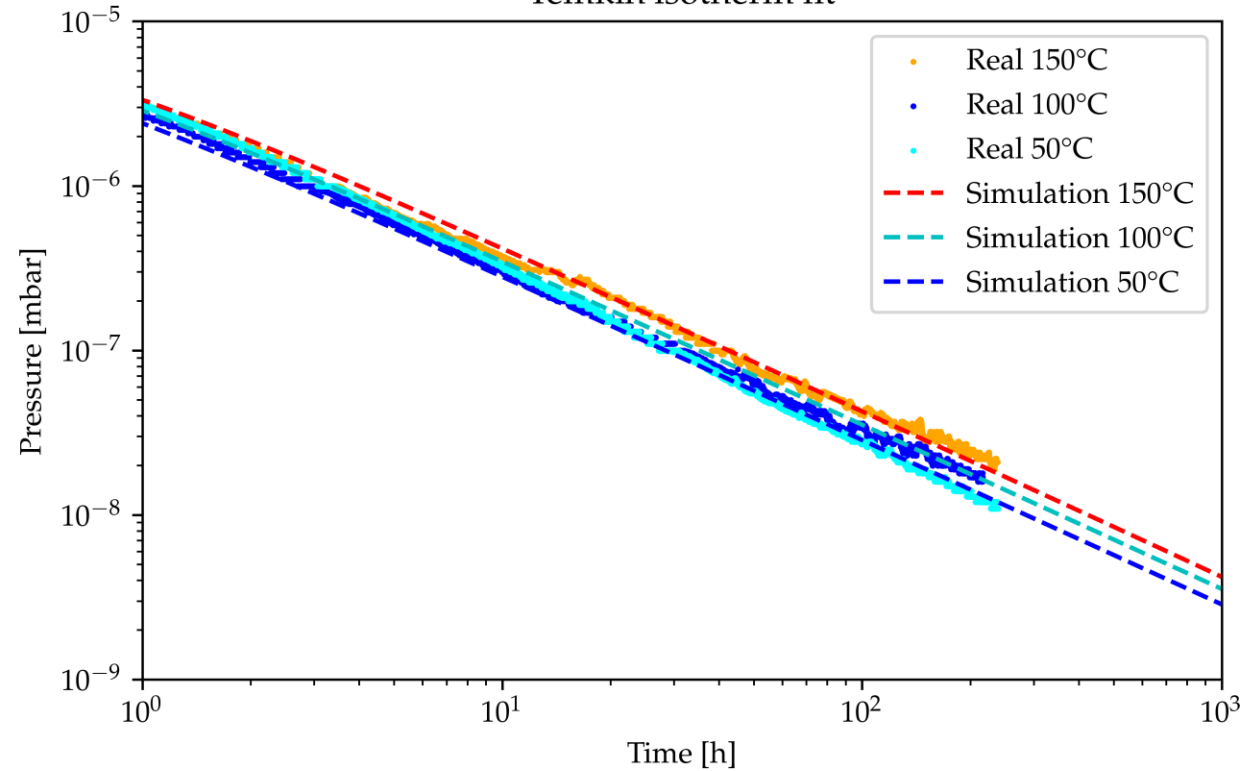
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Water binding energy – P355N

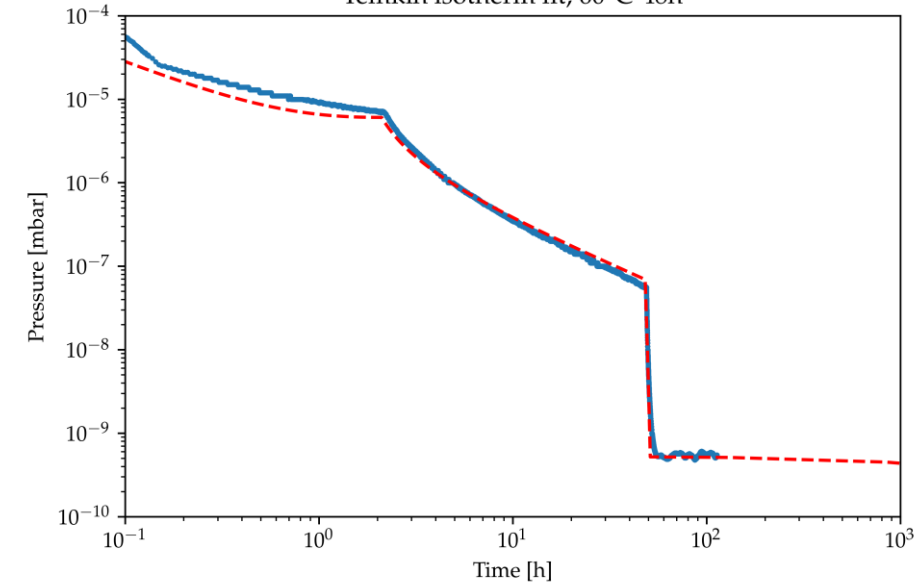
Temkin isotherm fit



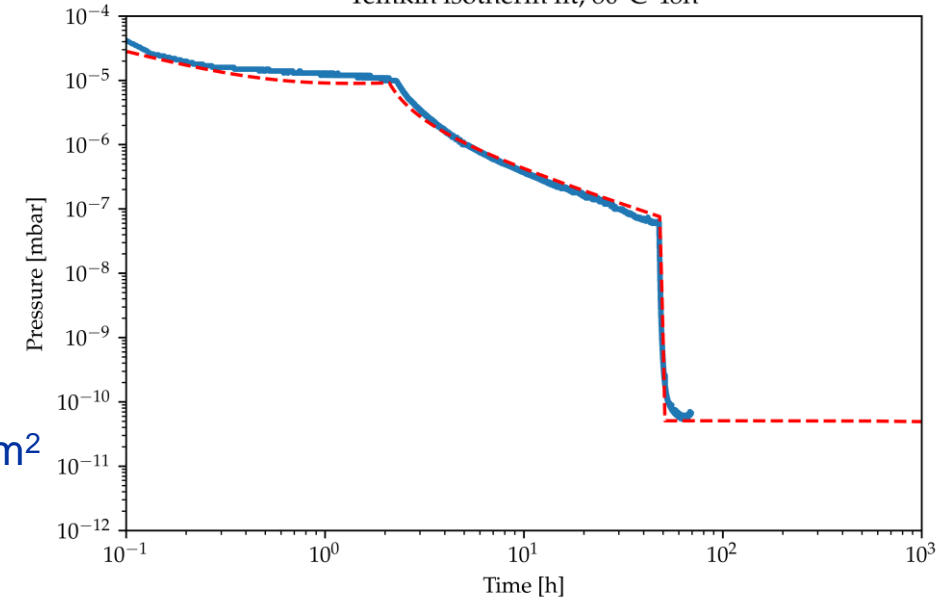
n_m
 E_0, E_1



Temkin isotherm fit, 60°C-48h



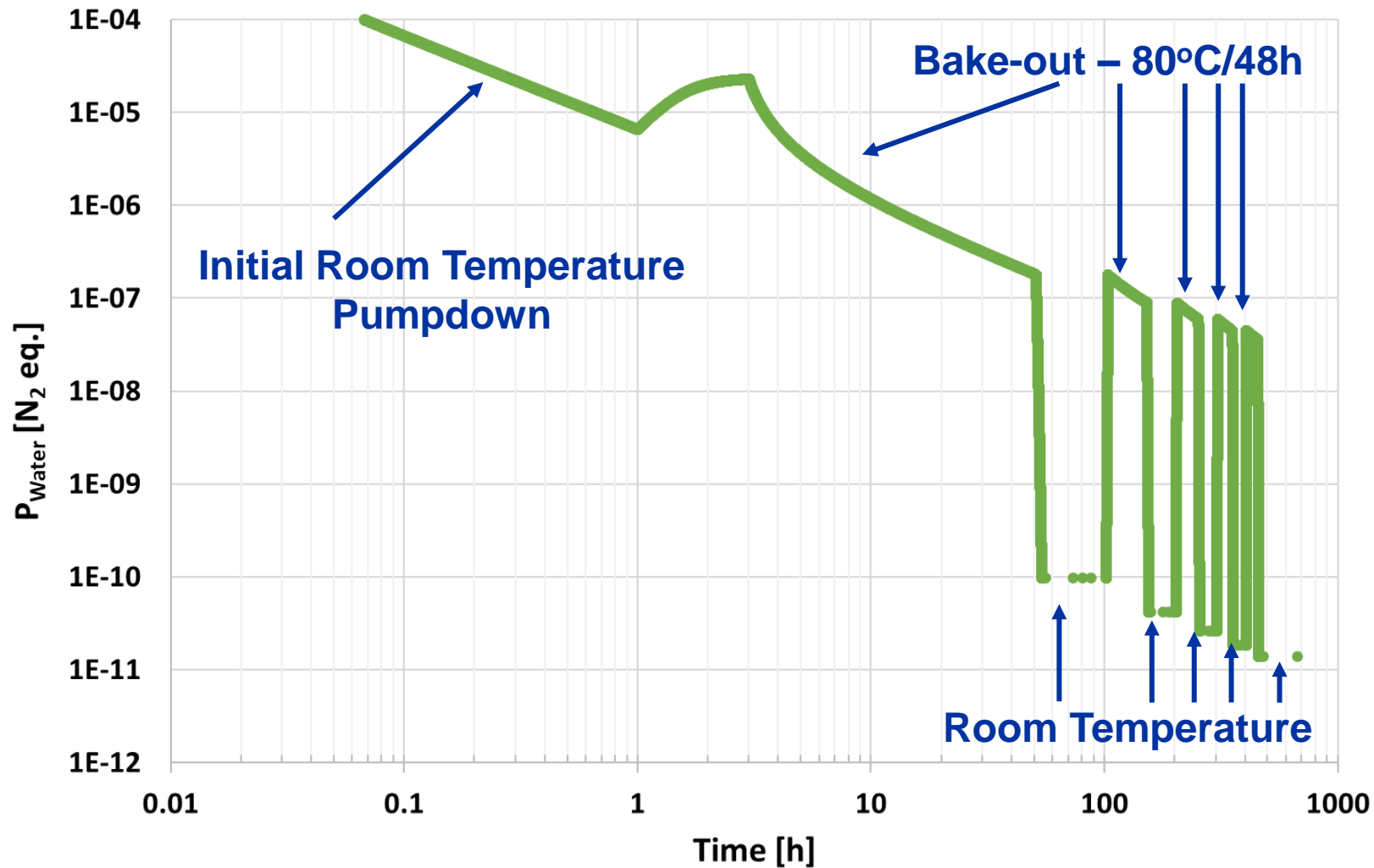
Temkin isotherm fit, 80°C-48h



n_m : number of sites (molecules) per unit of surface
 E_0 : Binding energy at Theta = 0 (zero coverage)
 E_1 : Binding energy at Theta = 1 (maximum coverage)

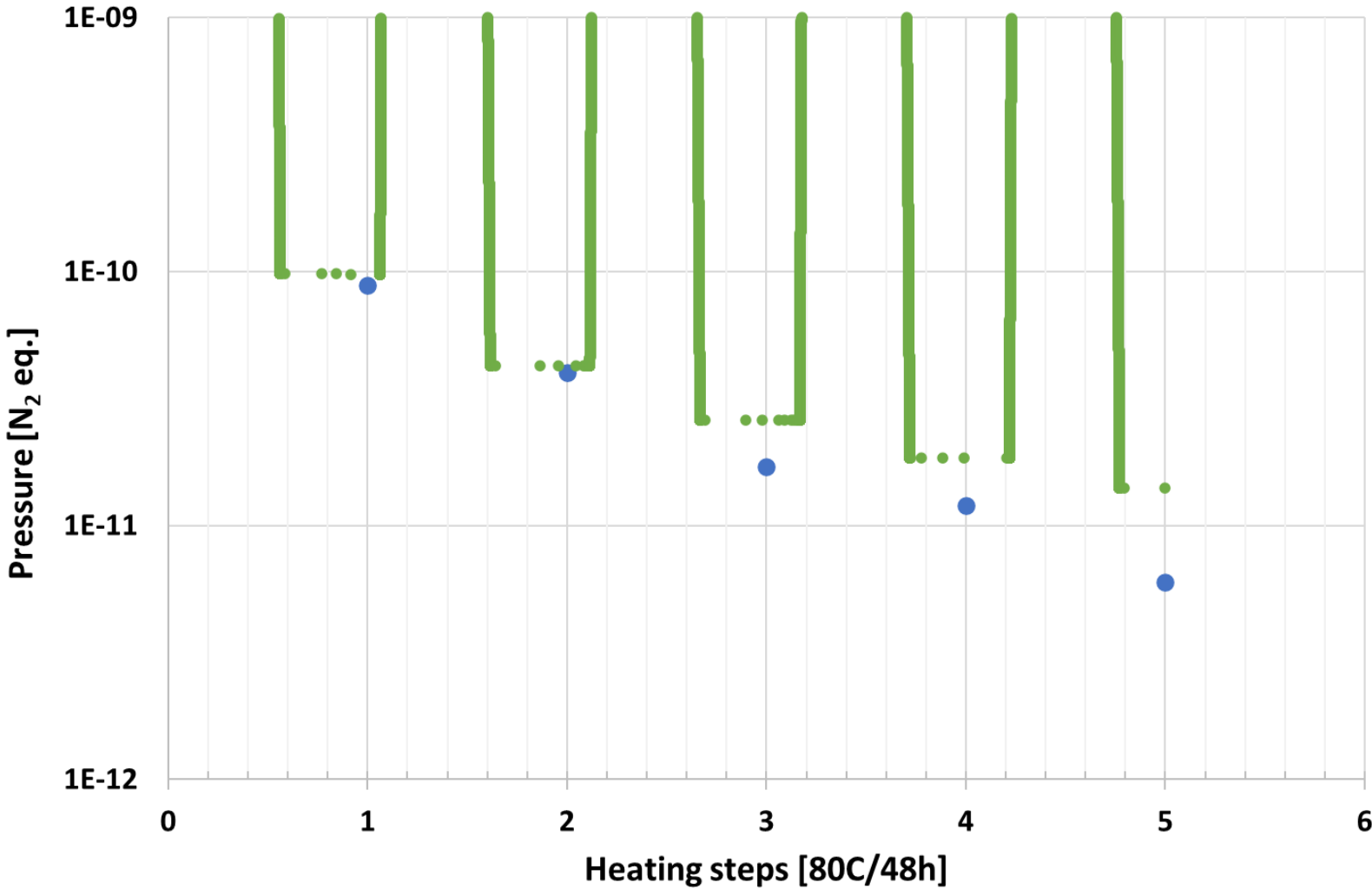
$4.5 \cdot 10^{20}$ molecules/cm²
 1.5 eV
 0.32 eV

Ultimate pressure – P355N



- ❖ Simulation of water pressure with 5 heating steps at 80°C for 48 hours
- ❖ The number of available sites has been kept constant

Ultimate pressure – P355N



Pressure ($P_2 - P_1$) nitrogen eq. in function of heating steps at 80°C for 48 hours

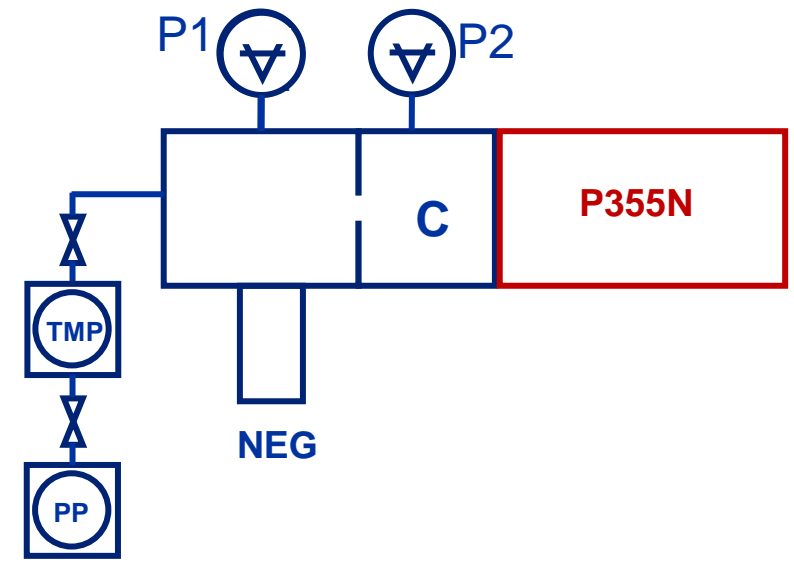
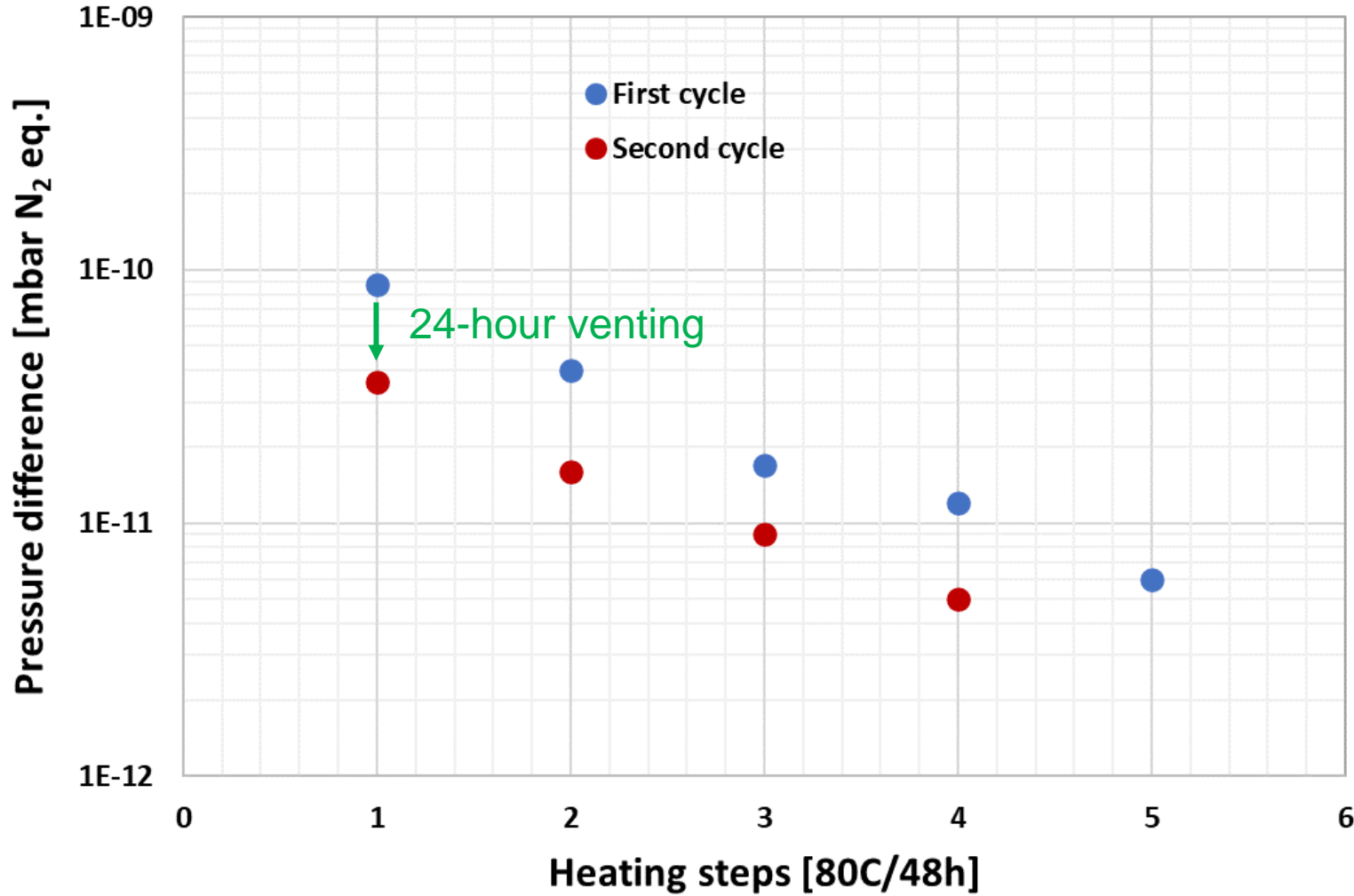
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Discrepancy between measurement and simulation due to:

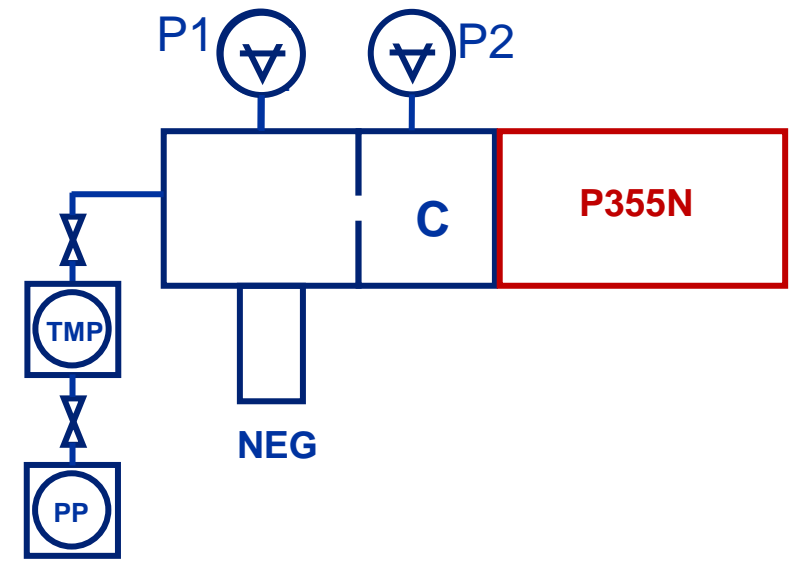
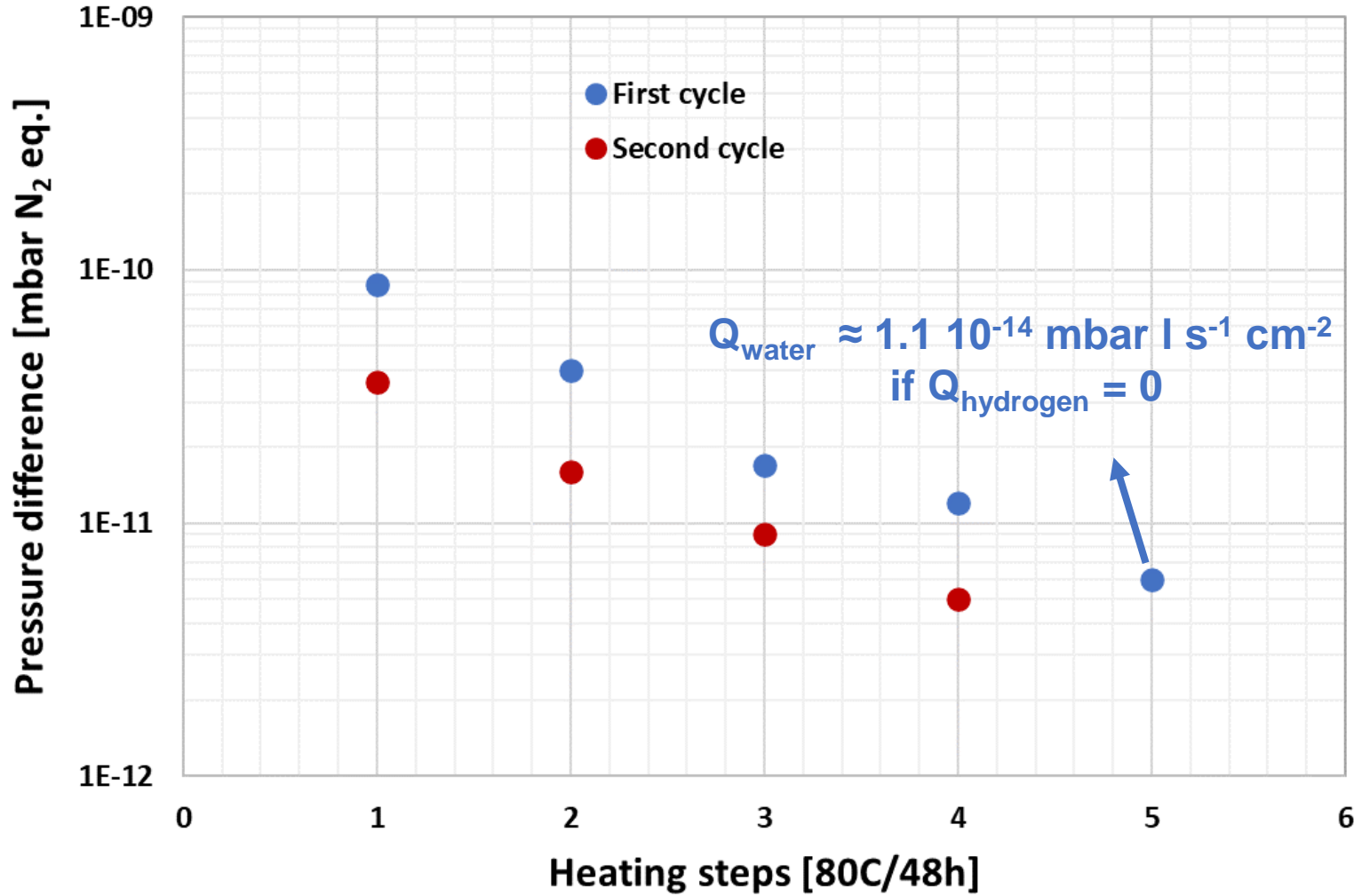
-Number of available sites \neq constant ?

Ultimate pressure – P355N



- ❖ Throughput system: \varnothing 10 mm orifice – Surface area P355N chamber = 6333 cm²
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- ❖ Pressure drop after 24-hour venting

Ultimate pressure – P355N



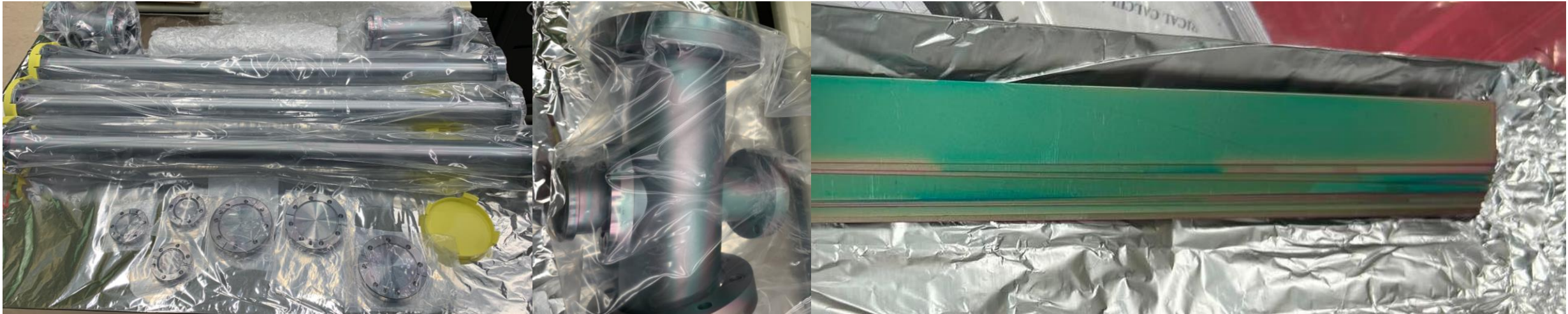
- ❖ Throughput system: \varnothing 10 mm orifice – Surface area P355N chamber = 6333 cm²
- ❖ Background pressure removed
- ❖ Pressure drop after 24-hour venting
- ❖ Hydrogen outgassing after 12 repeated heating steps 80C/48h:

$7 \cdot 10^{-16} \text{ mbar l s}^{-1} \text{ cm}^{-2}$

Silicon coating

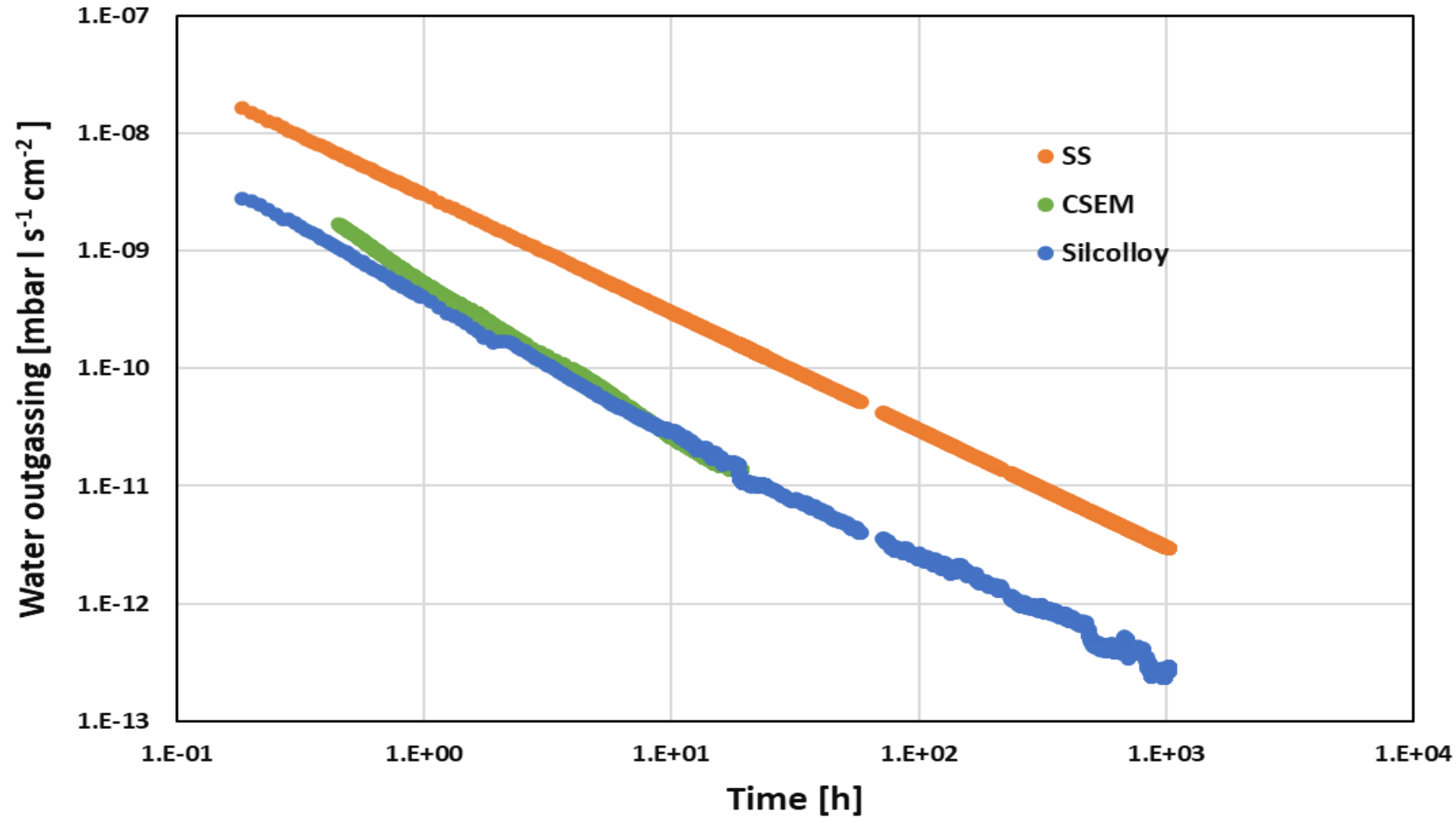
aSi:H coating by CVD

- ❖ Thermal enhanced CVD (Silcolloy by SilcoTek)
- ❖ Temperature during coating $\approx 400^{\circ}\text{C}$
- ❖ Coating thickness $\approx 890\text{ nm}$
- ❖ Substrate: 304L – 2 mm – VF* components
304L – 1 mm – VF* plates
- ❖ Plasma enhanced CVD (CSEM)
- ❖ Temperature during coating $\approx 180^{\circ}\text{C}$
- ❖ Coating thickness $\approx 200\text{ nm}$ **(to be confirmed)**
- ❖ Substrate: 304L – 0.5 mm – VF* plates



*VF: Vacuum fired

Silcolloy vs CSEM: Pumpdown



Silcolloy:

$$Q_{10h} = 2.5 \cdot 10^{-11} \text{ mbar l s}^{-1} \text{ cm}^{-2}$$

CSEM:

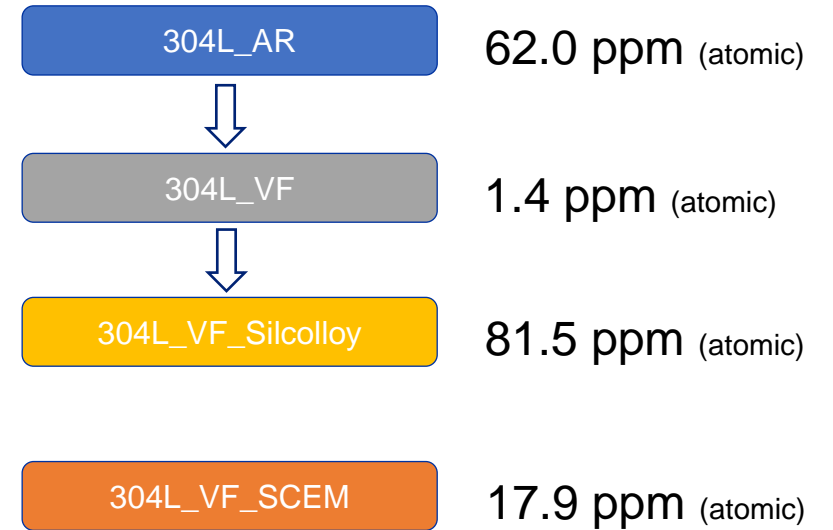
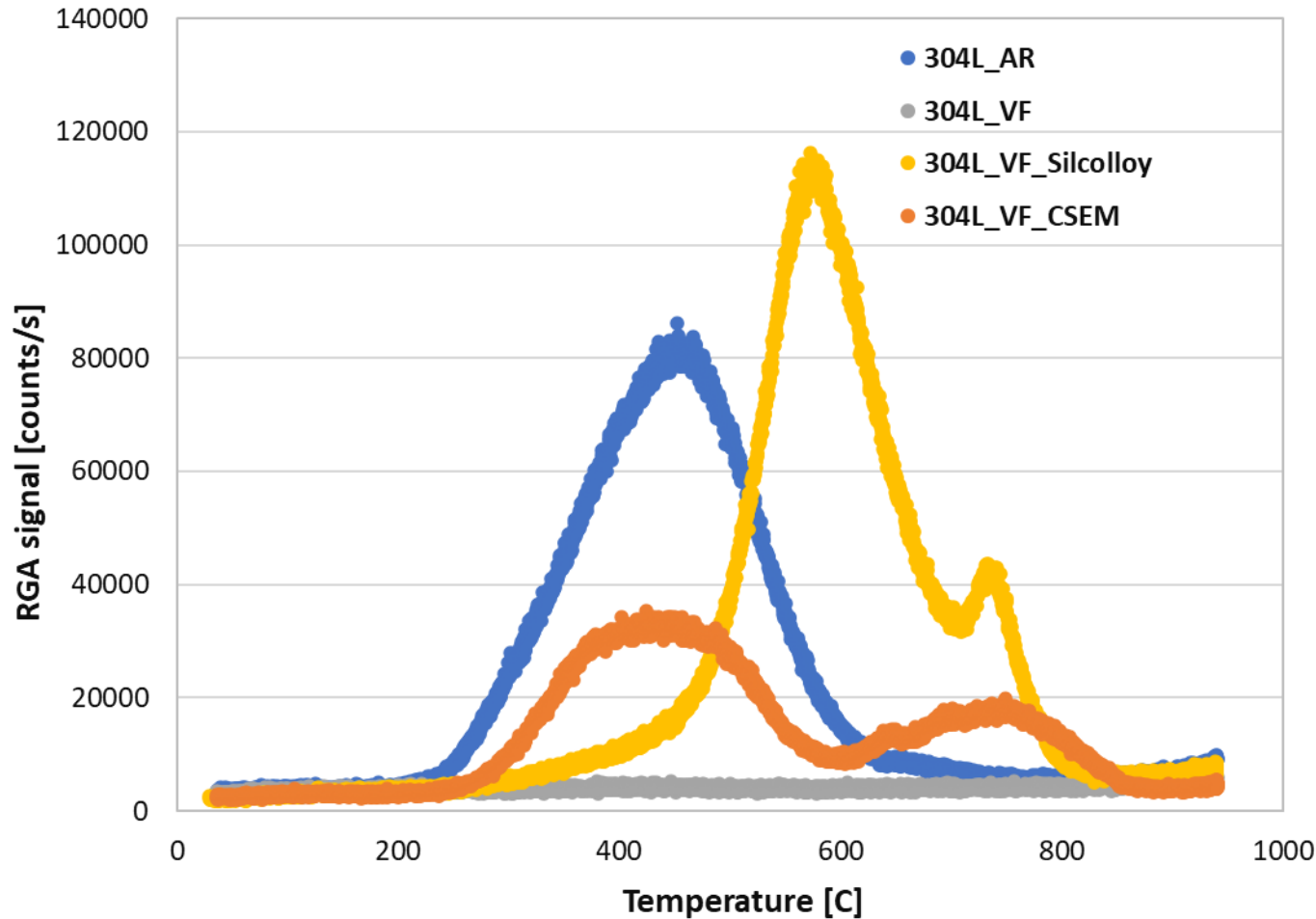
$$Q_{10h} = 2.6 \cdot 10^{-11} \text{ mbar l s}^{-1} \text{ cm}^{-2}$$

SS:

$$Q_{10h} = 3 \cdot 10^{-10} \text{ mbar l s}^{-1} \text{ cm}^{-2}$$

Silcolloy vs CSEM: TDS

Mass 2



AR : As Received

VF : Vacuum Fired (950C/2h)

Silcolloy coating

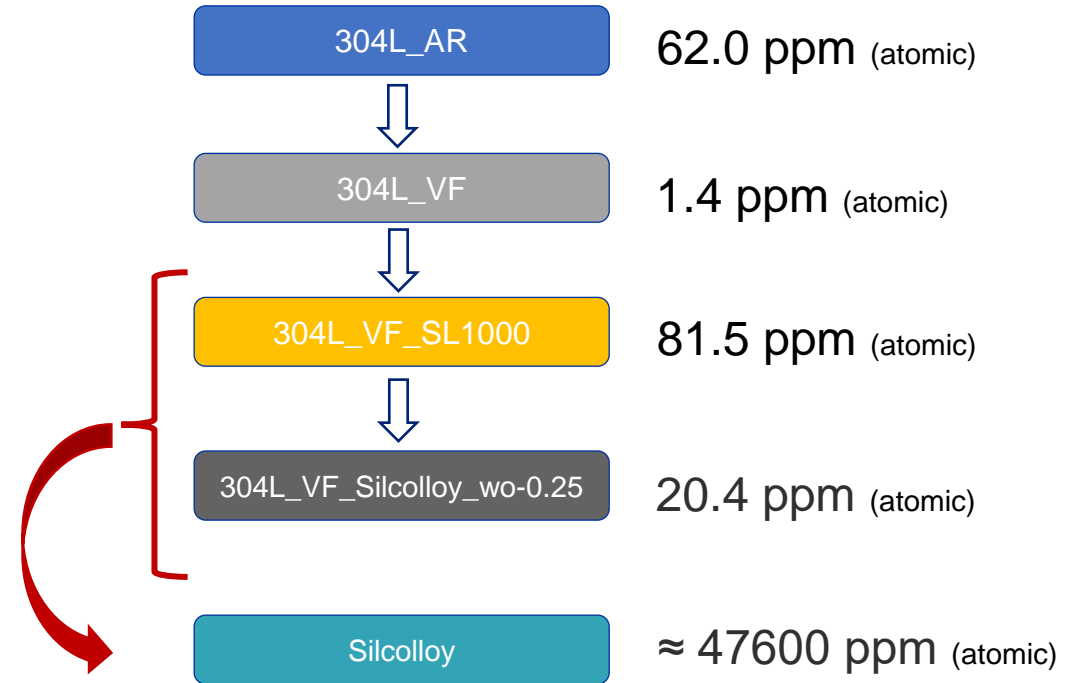
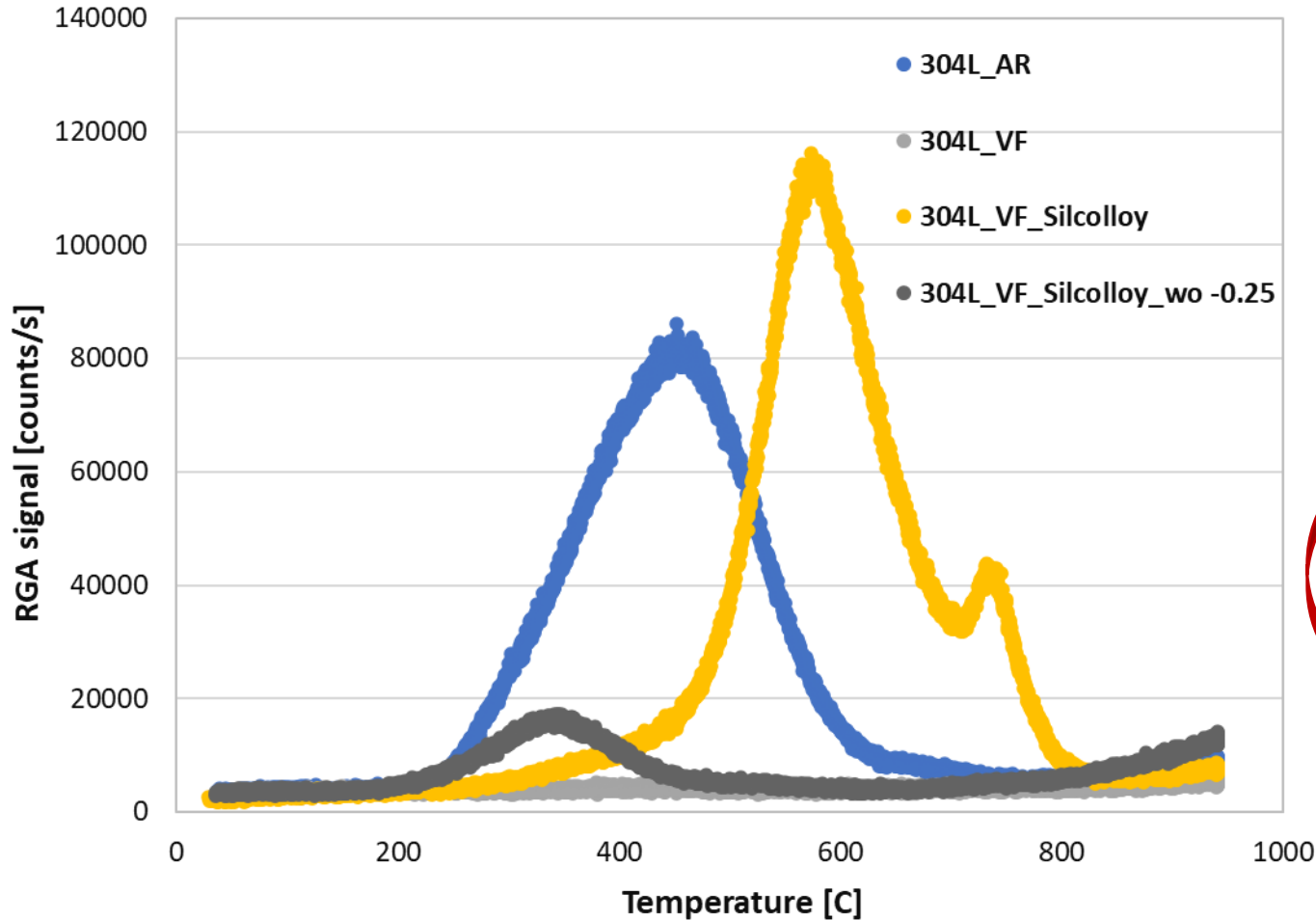
CSEM

Thermal enhanced CVD

Plasma enhanced CVD

Silcolloy: TDS

Mass 2



AR : As Received

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Silcolloy coating

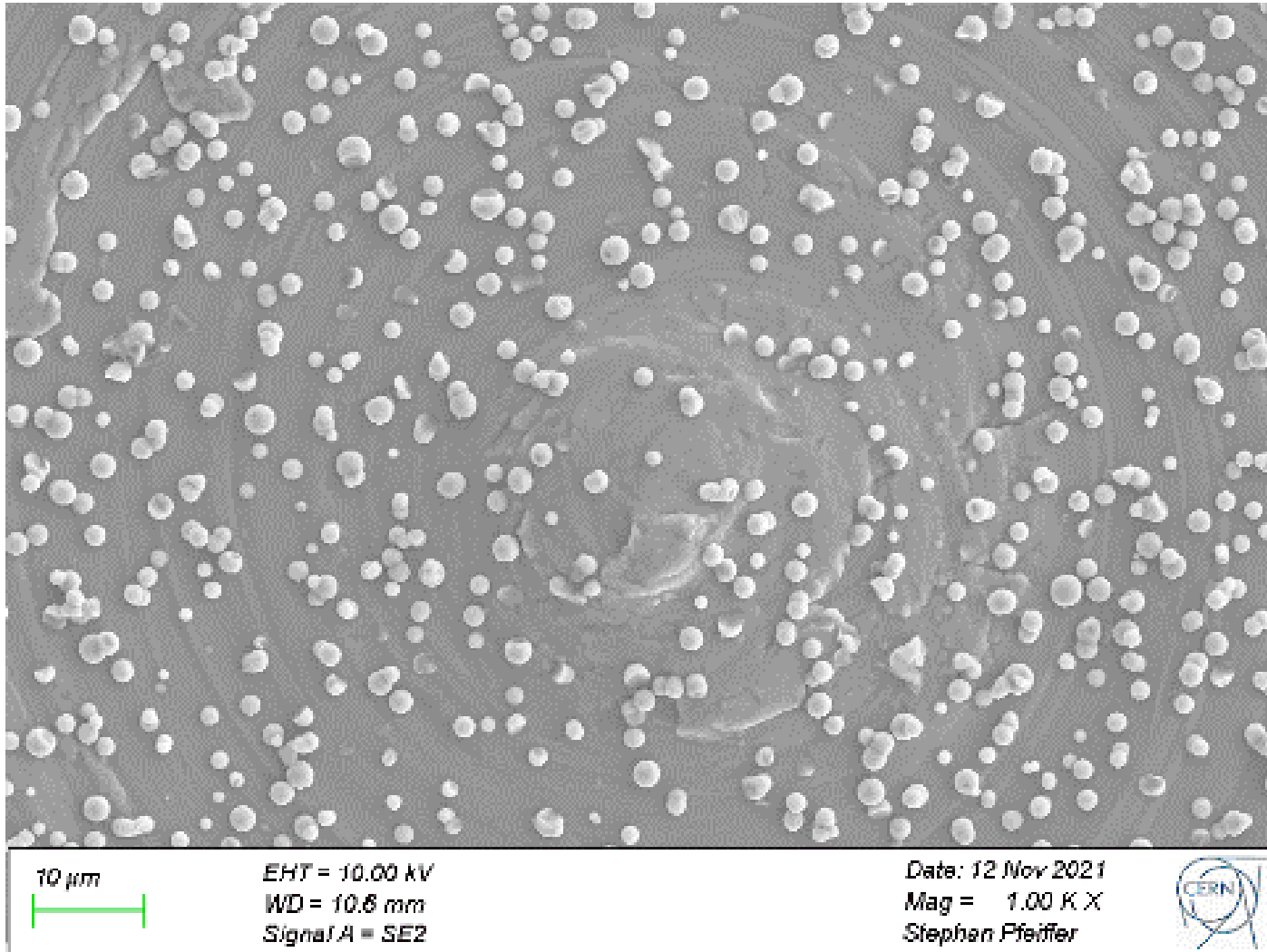
wo-0.25 : 0.25 mm removed mechanically

Silcolloy: Hydrogen outgassing

| Temperature | Mass | 2 | 15 | 28 | 44 |
|-------------|------|----------------------|----------------------|----------------------|----------------------|
| 80°C | | $7.1 \cdot 10^{-15}$ | $3.4 \cdot 10^{-17}$ | $1.6 \cdot 10^{-16}$ | $2.6 \cdot 10^{-17}$ |
| 150°C | | $1.6 \cdot 10^{-14}$ | $4.0 \cdot 10^{-17}$ | $1.2 \cdot 10^{-16}$ | $3.2 \cdot 10^{-17}$ |
| 200°C | | $1.5 \cdot 10^{-14}$ | $2.0 \cdot 10^{-17}$ | $9.9 \cdot 10^{-17}$ | $3.9 \cdot 10^{-17}$ |

- Outgassing rates units: $\text{mbarl s}^{-1} \text{cm}^{-2}$
- Duration of heating: 48h
- CSEM samples: measurements ongoing

Silcolloy: SEM



- ❖ Spherical particle growth
- ❖ Diameter ranging from 1 to 3 μm
- ❖ Unacceptable for the operation of a gravitational wave detector

Conclusions – mild steel

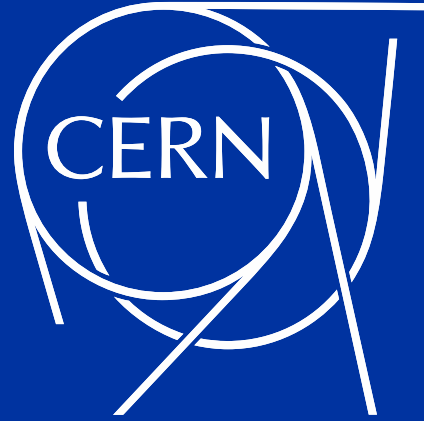
- The residual water outgassing rate from mild steels were found to be similar or higher (up to 2 orders of magnitude) than that of stainless steel. This large range of water outgassing rates can be attributed to the surface morphology.
- The hydrogen content of mild steel is comparable to those found in vacuum fired stainless steel resulting in low hydrogen outgassing rates.
- Long duration bake-out at 80°C could be used to achieve the pressures required in the next generation of gravitational wave detectors. The effect of such a bake-out on mild steel needs further investigation.
- Simulations of bake-out/pumpdown cycles are now possible. The data has been fitted according to the Temkin isotherm to determine the interval of water binding energies.

Conclusions – aSi:H

- The water outgassing rate is about one order of magnitude lower than standard stainless steel
- The coating contains a huge quantity of hydrogen, and the coating process recharges the stainless-steel substrate
- The outgassing rate for hydrogen is in the lower 10^{-14} mbar l s⁻¹ cm⁻² range. An anomalous increase is measured when increasing the bake-out temperature from 80°C to 150°C
- Spherical particle growth on the surface should be avoided during the coating process

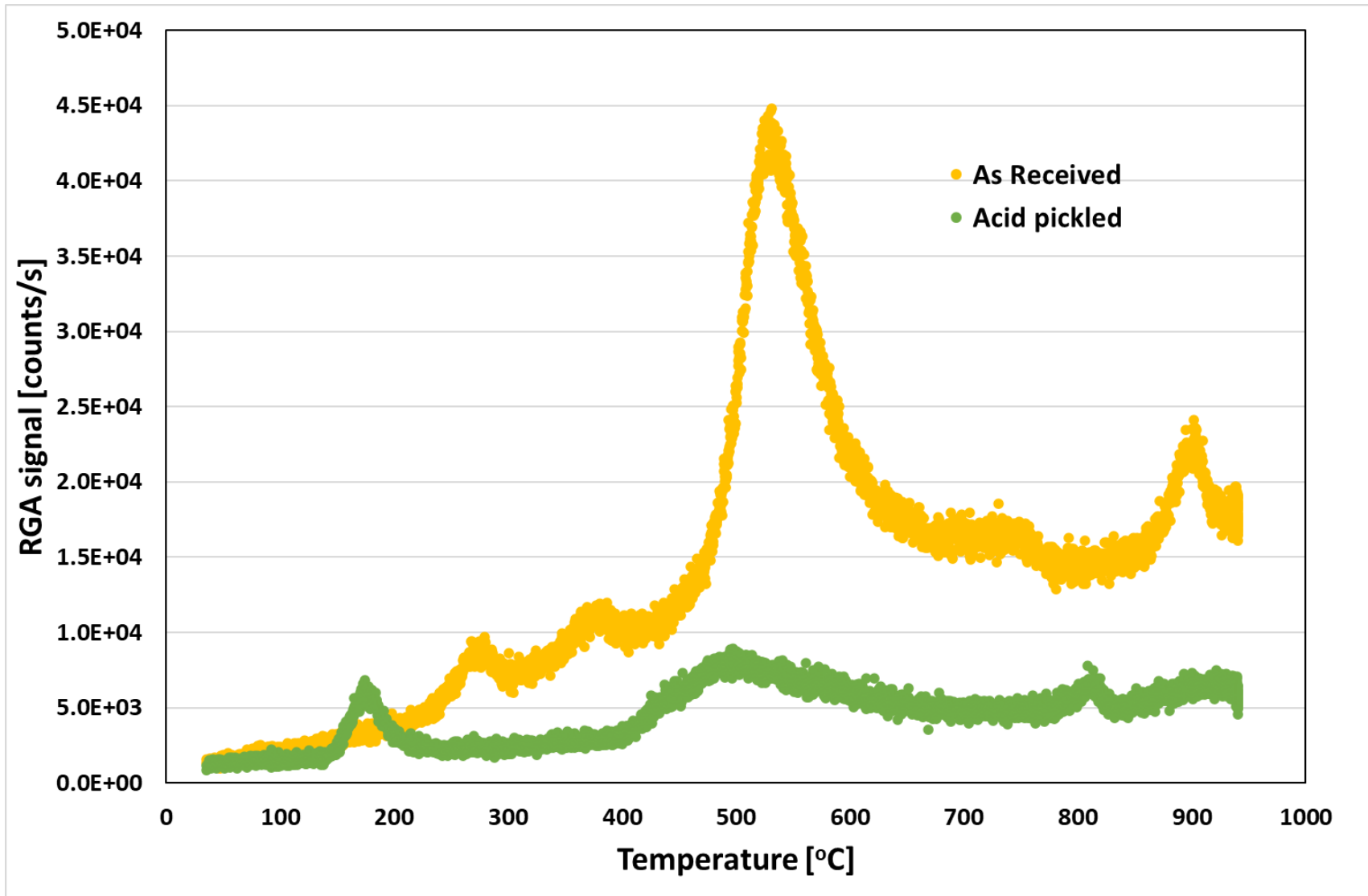
Conclusions

- From a point of view of achievable pressures mild steel is a valid candidate for the manufacturing of the GWD beampipe at a lower cost than the current baseline
- Other important aspects of mild steel must be investigated: long term corrosion resistance, weldability, cleaning methods,...
- The low 80°C bake-out of mild steel would reduce the cost of materials, energy and insulation
- In the present state of development, despite a reduction of a factor 10 in water outgassing rate, the tested hydrogenated amorphous silicon coating will not avoid the need for a bake-out of the beampipe of future GWD.
- The upsizing this coating technology to future GWD is a technological challenge.



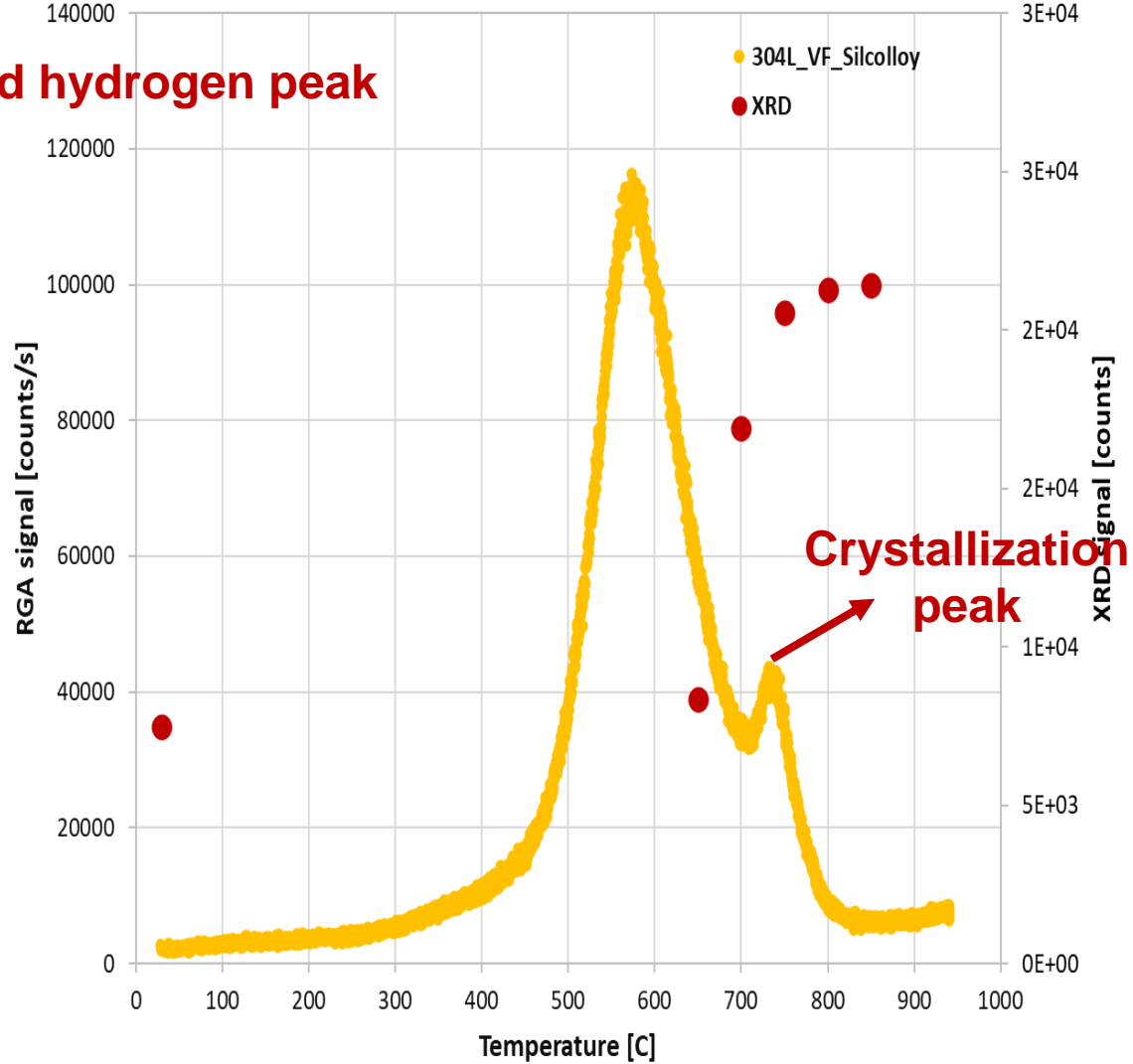
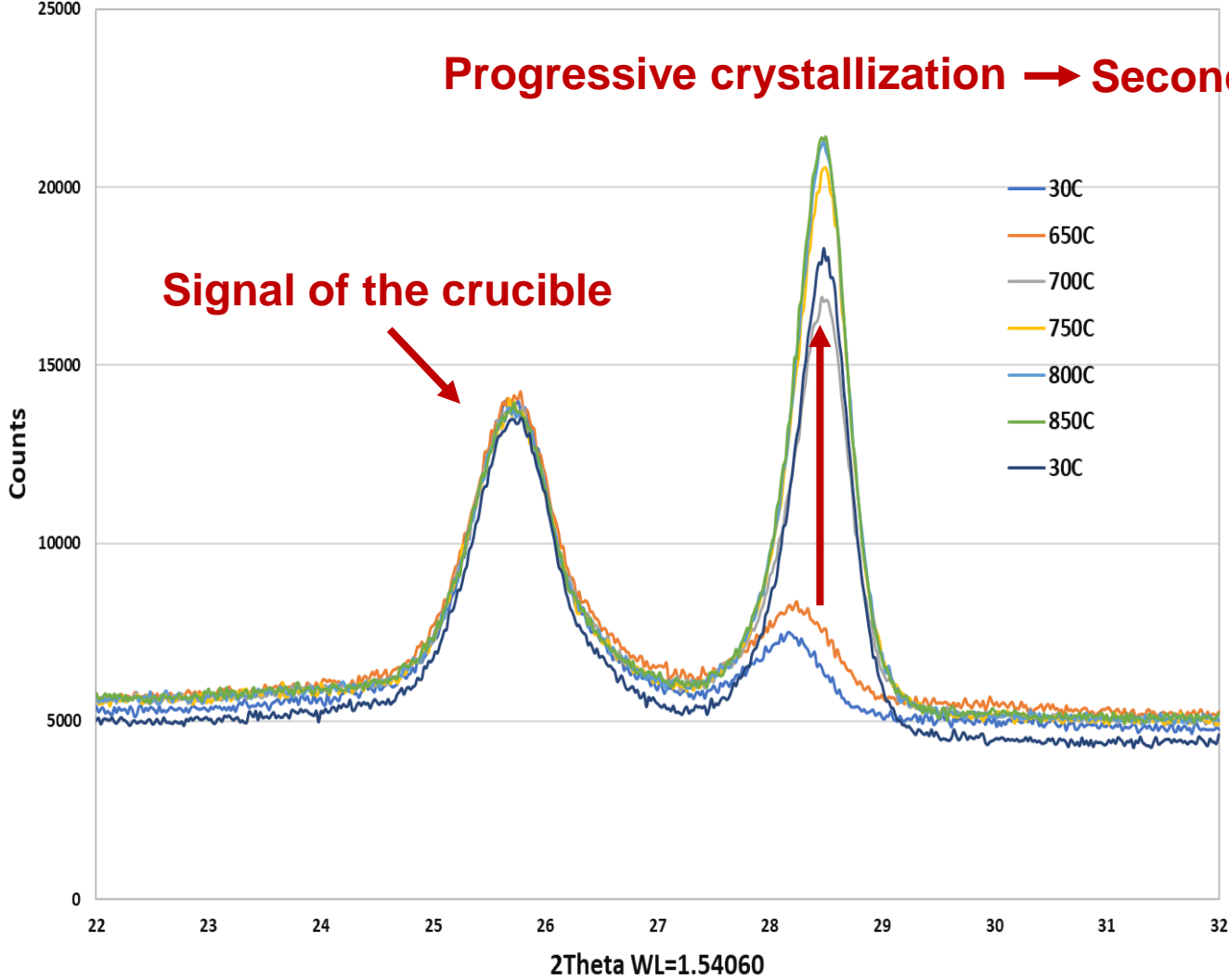
Thank you for your attention

S355J2H: Thermal desorption measurement



Removal of oxide layer by HCl acid pickling

Silcolloy: XRD



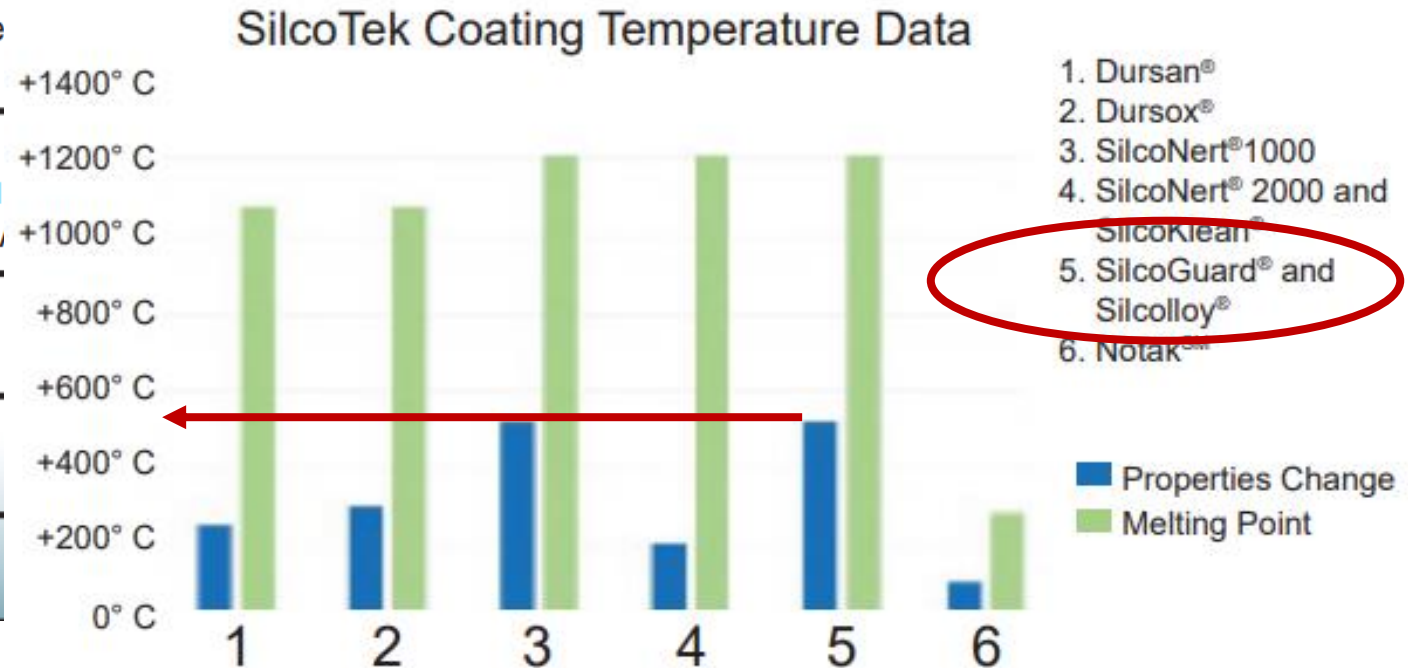
Silcolloy: aSi:H coating by CVD

Silcolloy® Properties

| | |
|---------------------------------|--|
| Coating Structure: | Hydrogenated amorphous |
| Deposition Process: | Thermal chemical vapor |
| Maximum Temperature:* | Advertised properties Melting: 1410° C |
| Substrate: | Compatibility: Size: Typical Geometry: |
| Typical Thickness: | 180 - 800 nm |
| Hydrophobicity (contact angle): | ≥40° |
| Allowable pH Exposure: | 0 - 8 |

HIGH-TEMPERATURE STABLE

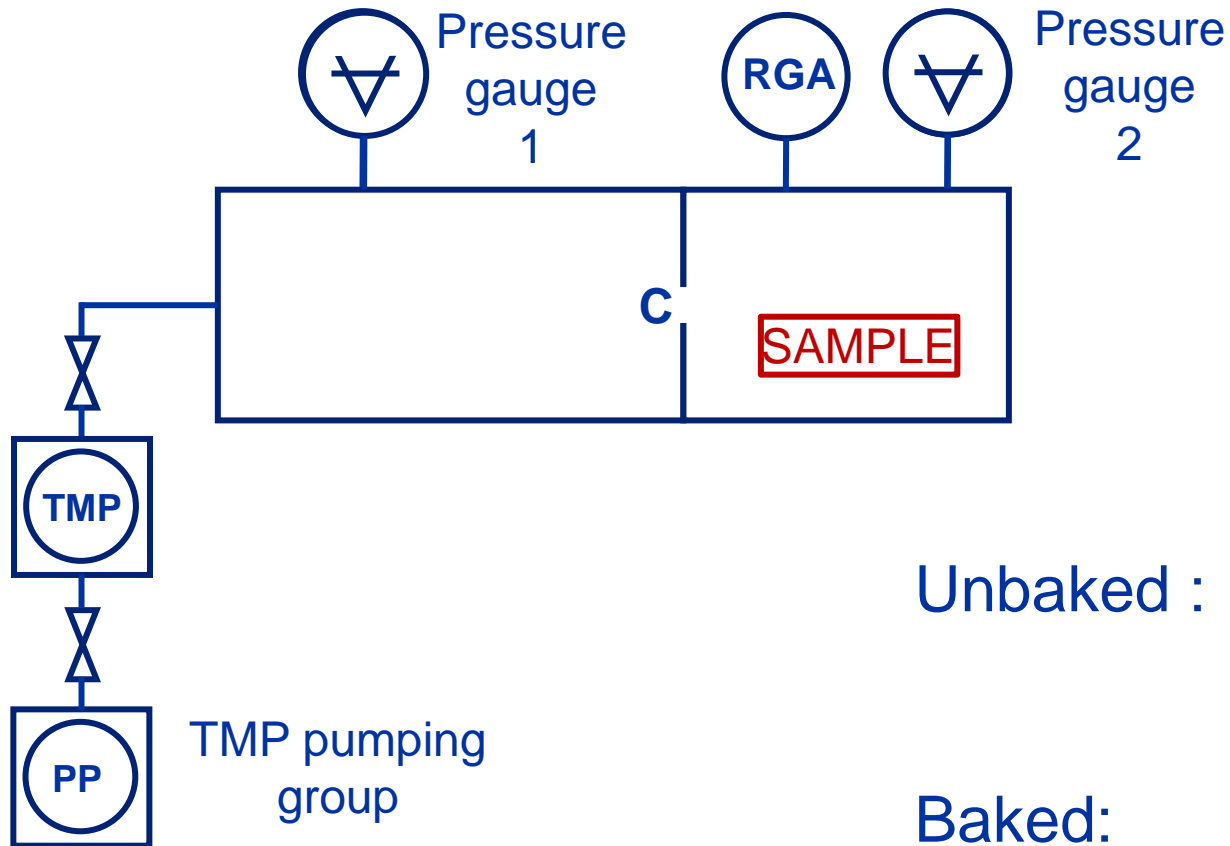
The Silcolloy process provides coatings inert at temperatures up to 1410°C, allowing high temperature analytical or general barrier applications.



* Datasheet from www.silcoTek.com

Material characterization methods

Measurement methods: Throughput



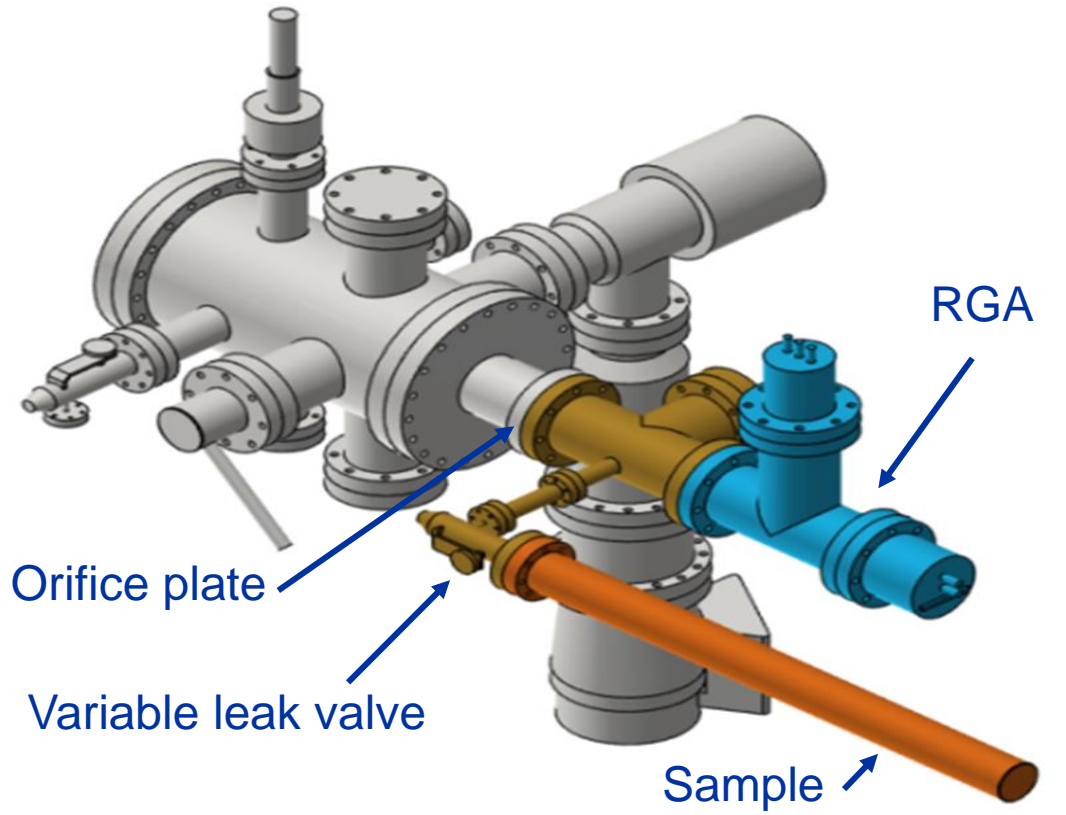
$$Q = \left(\frac{\overbrace{C (P_2 - P_1)}^{\text{Sample \& background}} - \overbrace{C (P_{2bg} - P_{1bg})}^{\text{background}}}{A_{\text{sample}}} \right)$$

Q in mbar l s⁻¹ cm⁻²

Unbaked : outgassing of water – time dependent
Cold cathode ionization gauges

Baked: outgassing of (mainly) hydrogen
hot cathode ionization gauges

Measurement methods: Coupled-method



All system components are baked to temperatures ranging from 200°C to 350°C

Sample and variable leak valve are heated to requested temperature and duration

Prior to cooldown all instrumentation is degassed

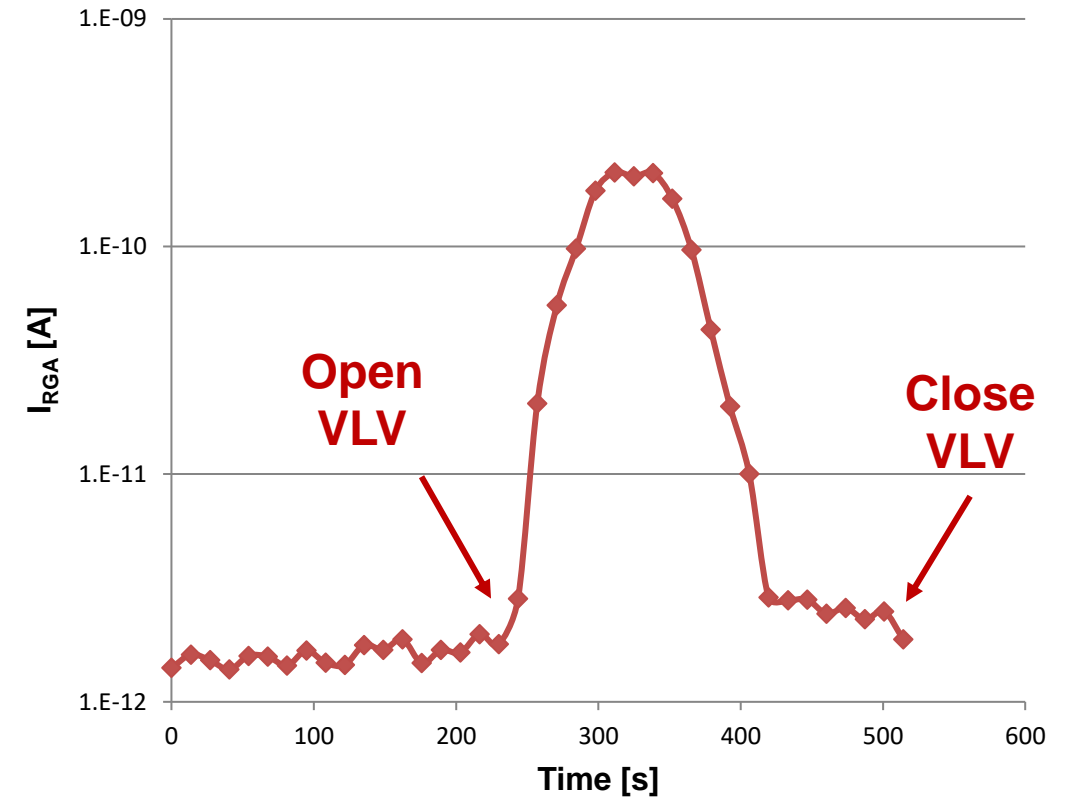
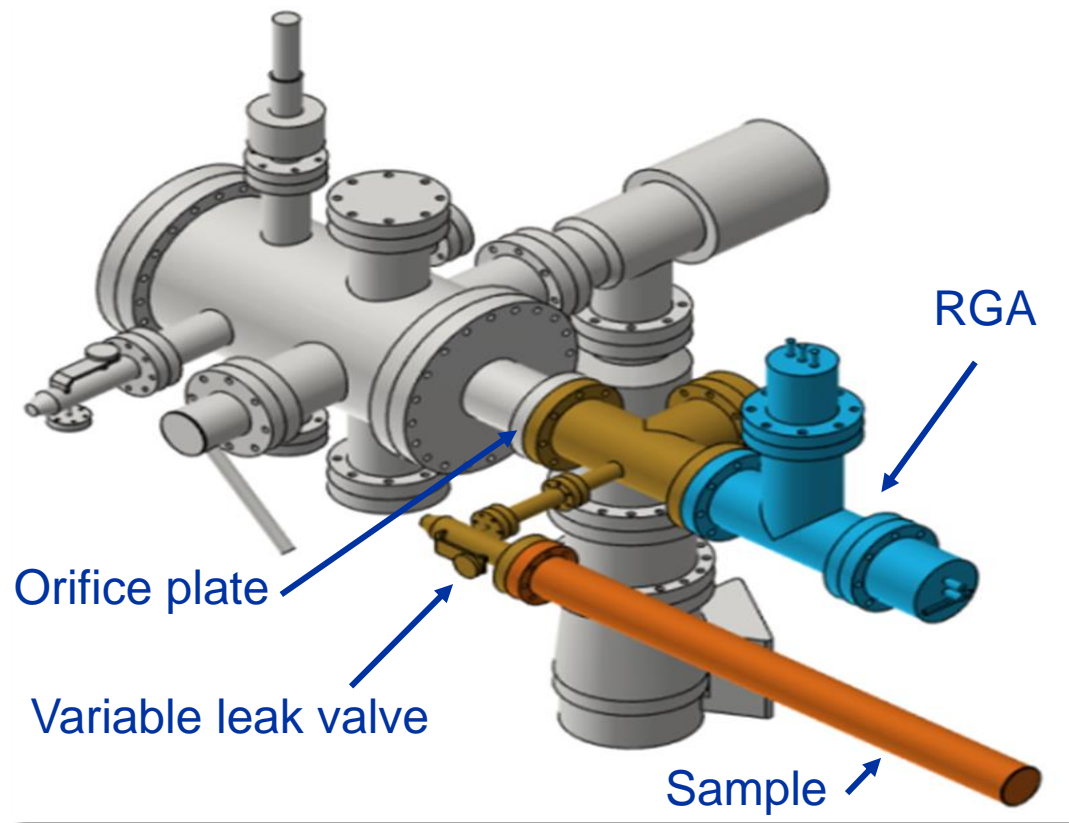
Variable leak valve body has been vacuum fired to minimize contribution

24 hours at room temperature before the start of the first measurement

Not suitable for gasses that can be reabsorbed (water)

RGA has been calibrated to an in-house calibrated hot cathode ionization gauge

Measurement methods: Coupled-method



Measurement methods: Coupled-method

$$Q [\text{mbarl/s}] = \frac{S_c \times \int_{\Delta\tau} I_{RGA} \times \alpha_{RGA} d\tau}{\Delta t_a}$$

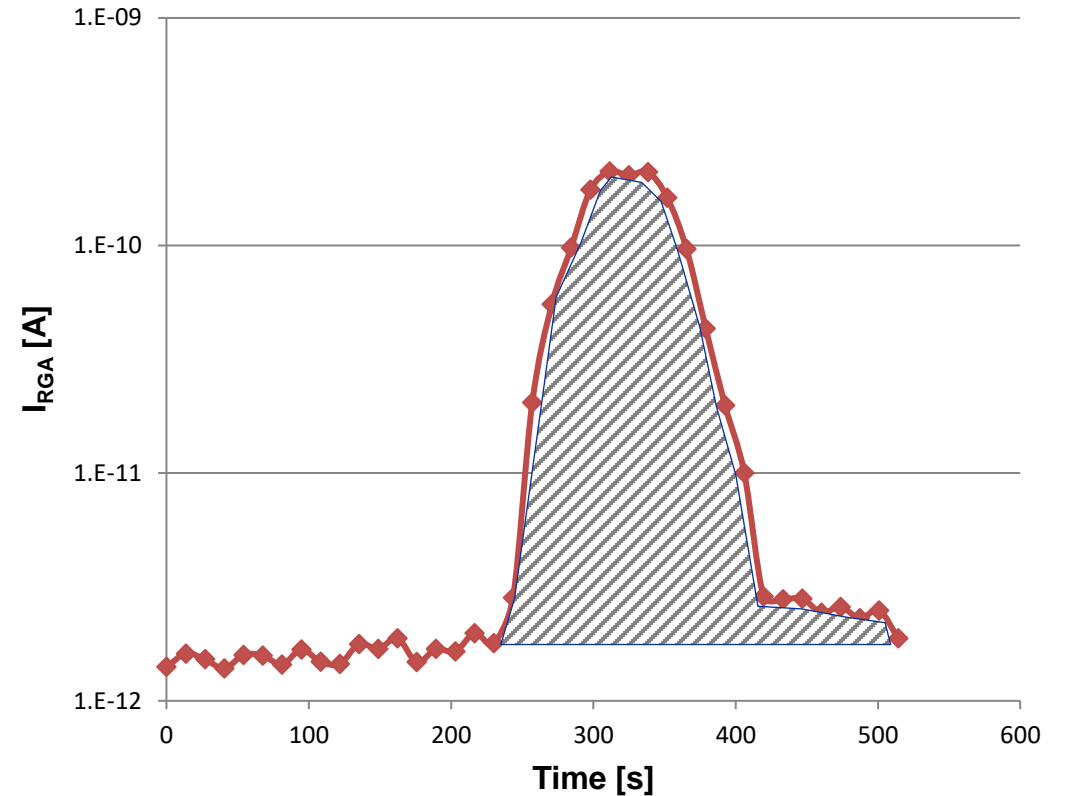
Δt_a : duration of the accumulation [s]

I_{RGA} : current recorded for the gas of interest [A]

S_c : conductance of the orifice for the gas of interest [l/s]

α_{RGA} : calibration factor for the gas of interest [A/mbar]

$\Delta\tau$: duration of the RGA recording [s]



Measurement methods: Coupled-method

$$Q [\text{mbarl/s}] = \frac{S_c \times \int_{\Delta\tau} I_{RGA} \times \alpha_{RGA} d\tau}{\Delta t_a}$$

Δt_a : duration of the accumulation [s]

I_{RGA} : current recorded for the gas of interest [A]

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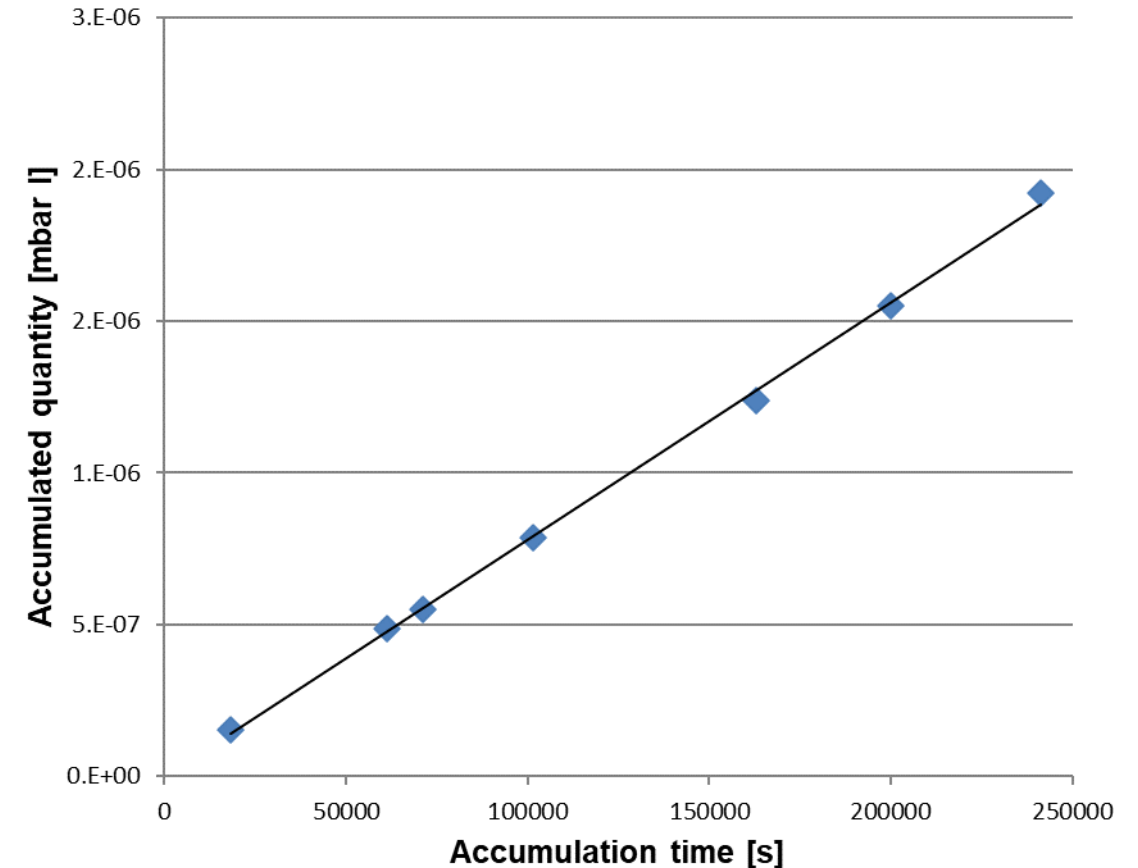
$\Delta\tau$: duration of the RGA recording [s]

Background outgassing rates (hydrogen)

System tubes: $5.3 \cdot 10^{-13}$ mbar l s⁻¹

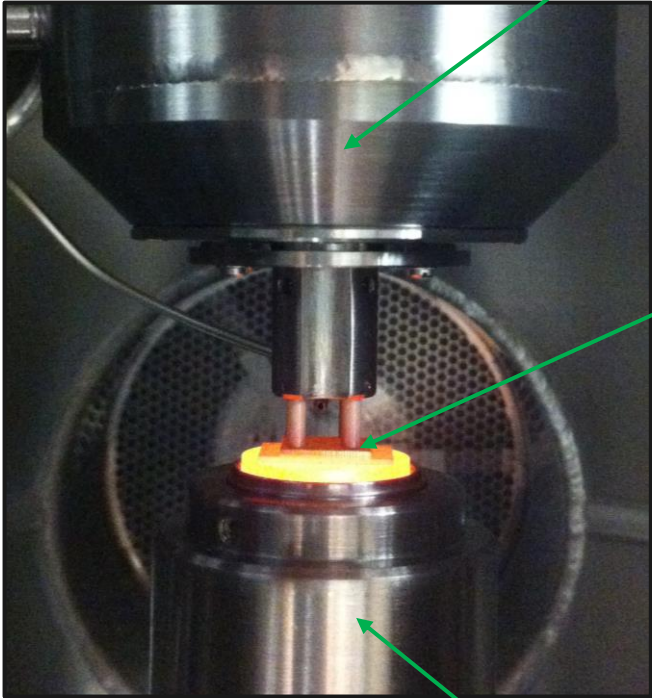
System samples: $7.8 \cdot 10^{-13}$ mbar l s⁻¹

Measurement error: $\pm 40\%$



Measurement methods: Thermal Desorption

Residual Gas Analyser

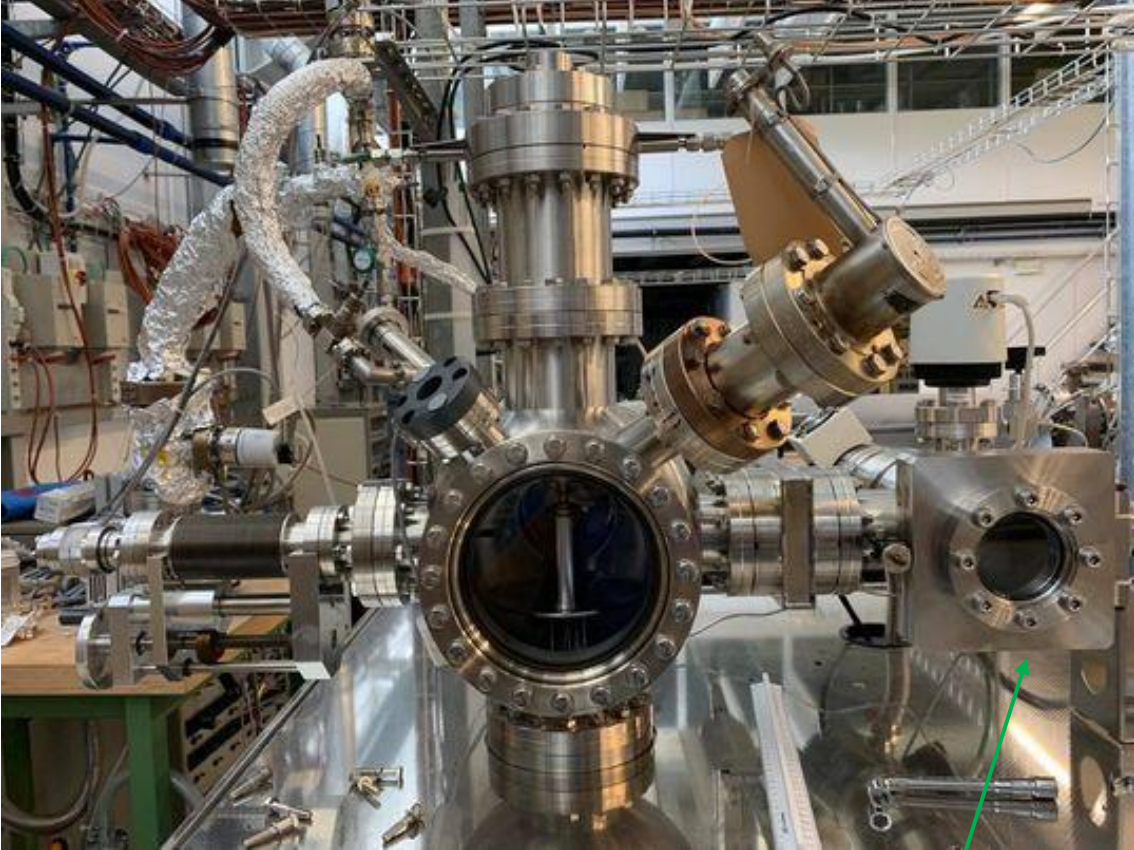


Sample

Heater

Heating rate: 5K/min

Dimensions of sample: 10mm x 10mm x 1mm



Loadlock

Water binding energy

