

TECHNOLOGY OF COMPONENTS USED FOR HELIUM REFRIGERATION

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THE OIL LUBRICATED SCREW COMPRESSOR



THE OIL LUBRICATED SCREW COMPRESSOR

How does it work ?

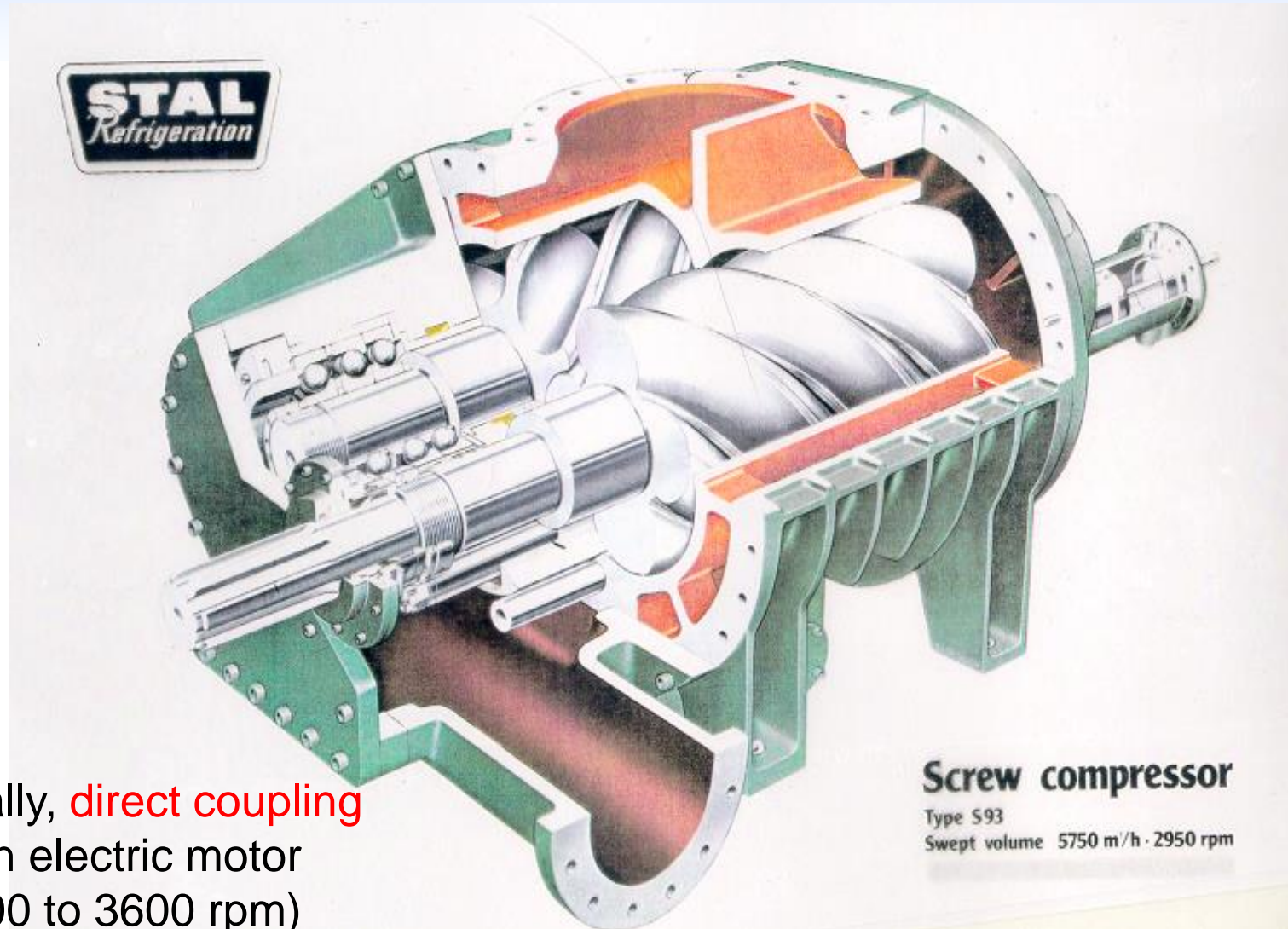
Why does it need oil ?

HISTORY

The basic idea can be found in a German patent, number 4121, applied by Heinrich Krigar, on 24th March **1878** !

- 1934 Lysholm patent (SRM), first machine
- 1940 **Dry compression**, timing gears, high rpm, high noise level, low CR
- 1950 **Oil injection**, still timing gears, lower rpm, lower noise level, higher CR,
- 1957 Oil injection, **no more gears** lower rpm, lower noise level, higher CR,
- 1960 **Symmetrical** rotor profiles, **capacity** control
- 1980 **Asymmetrical** rotor profiles, higher efficiency, quieter operation

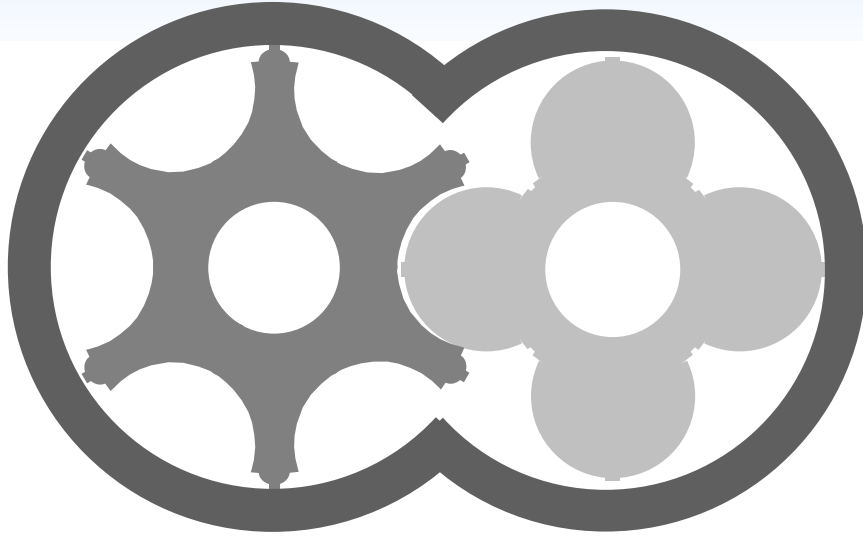
A SCREW COMPRESSOR



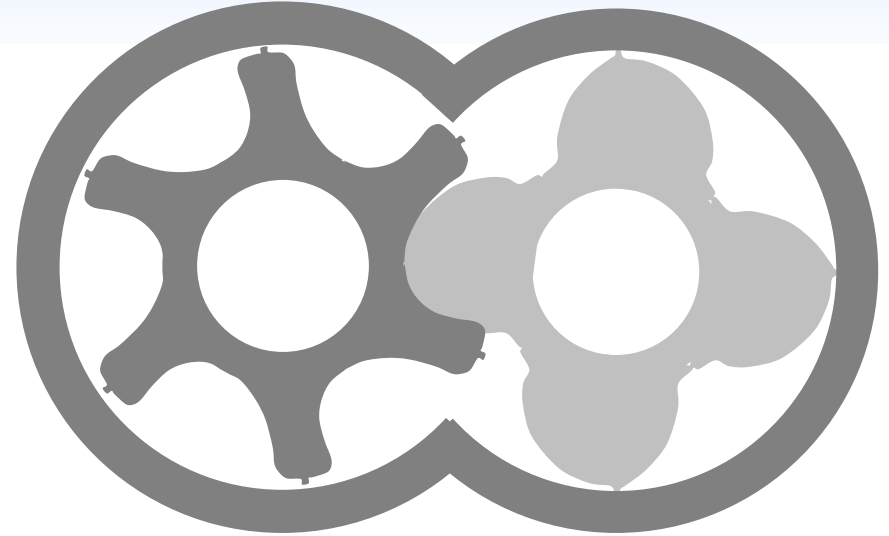
Generally, **direct coupling**
to an electric motor
(3000 to 3600 rpm)

ROTOR PROFILES

SYMETRICAL



ASSYMETRICAL



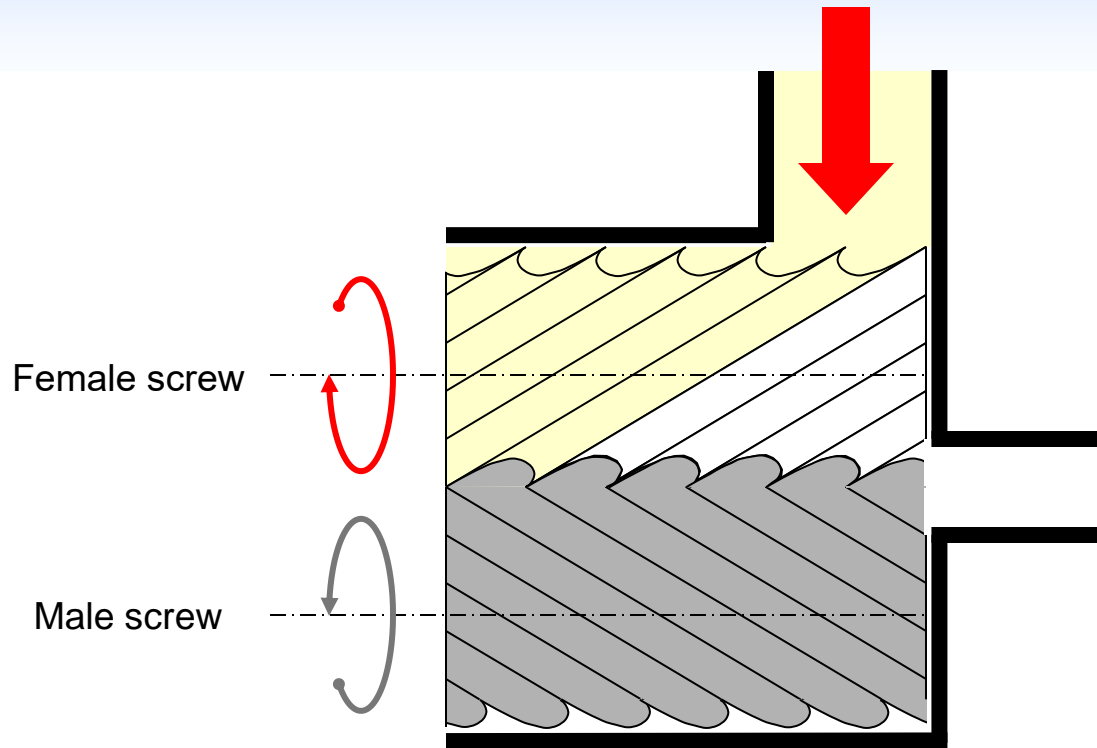
SCREWS



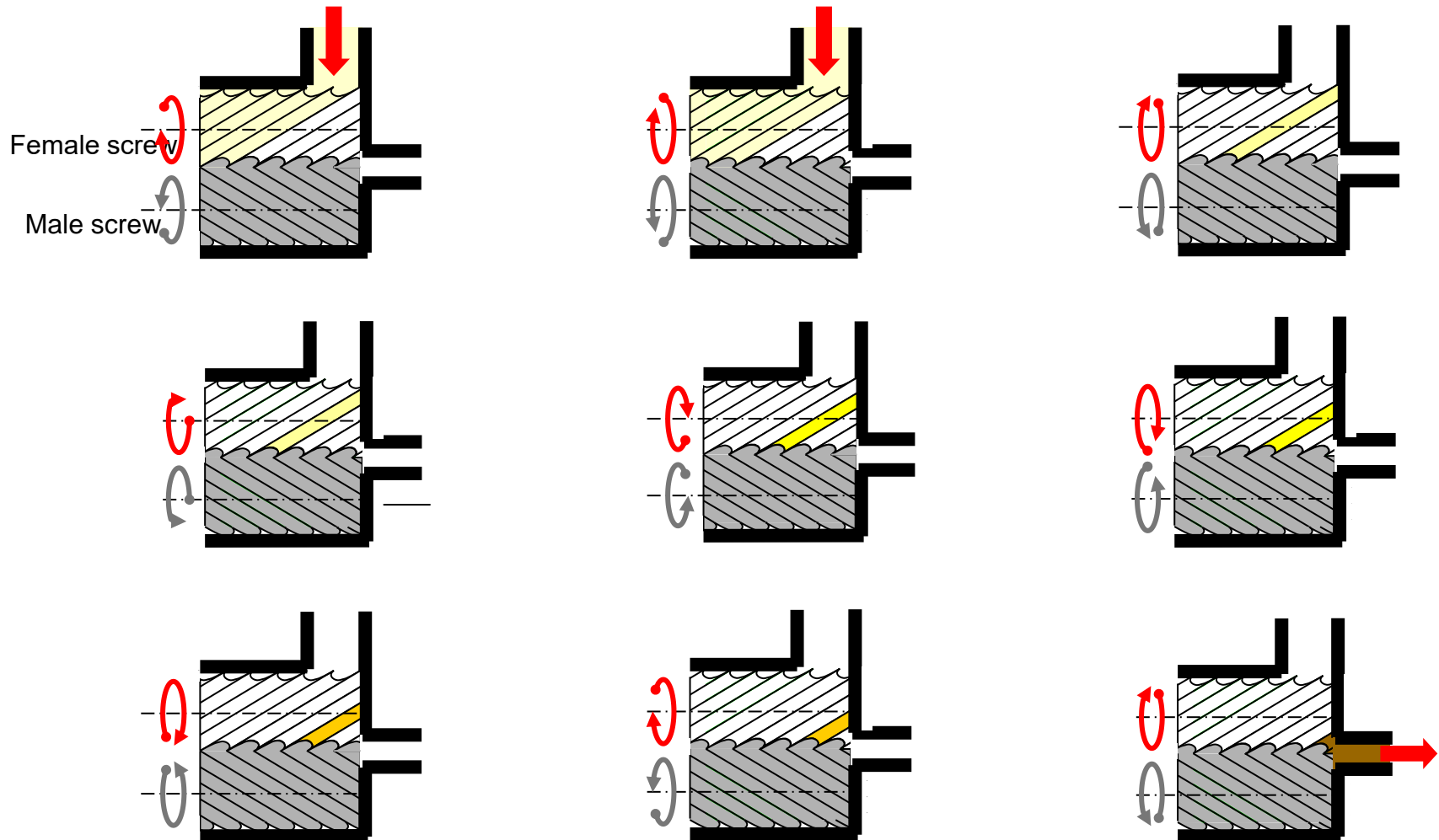
Screw
machining



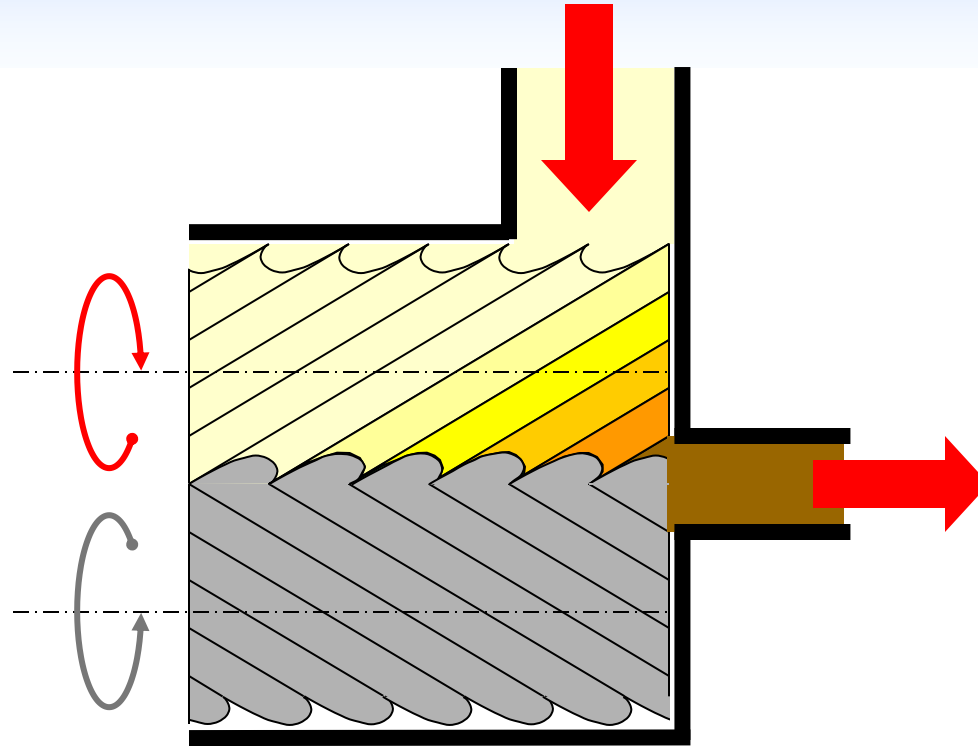
OPERATION



OPERATION



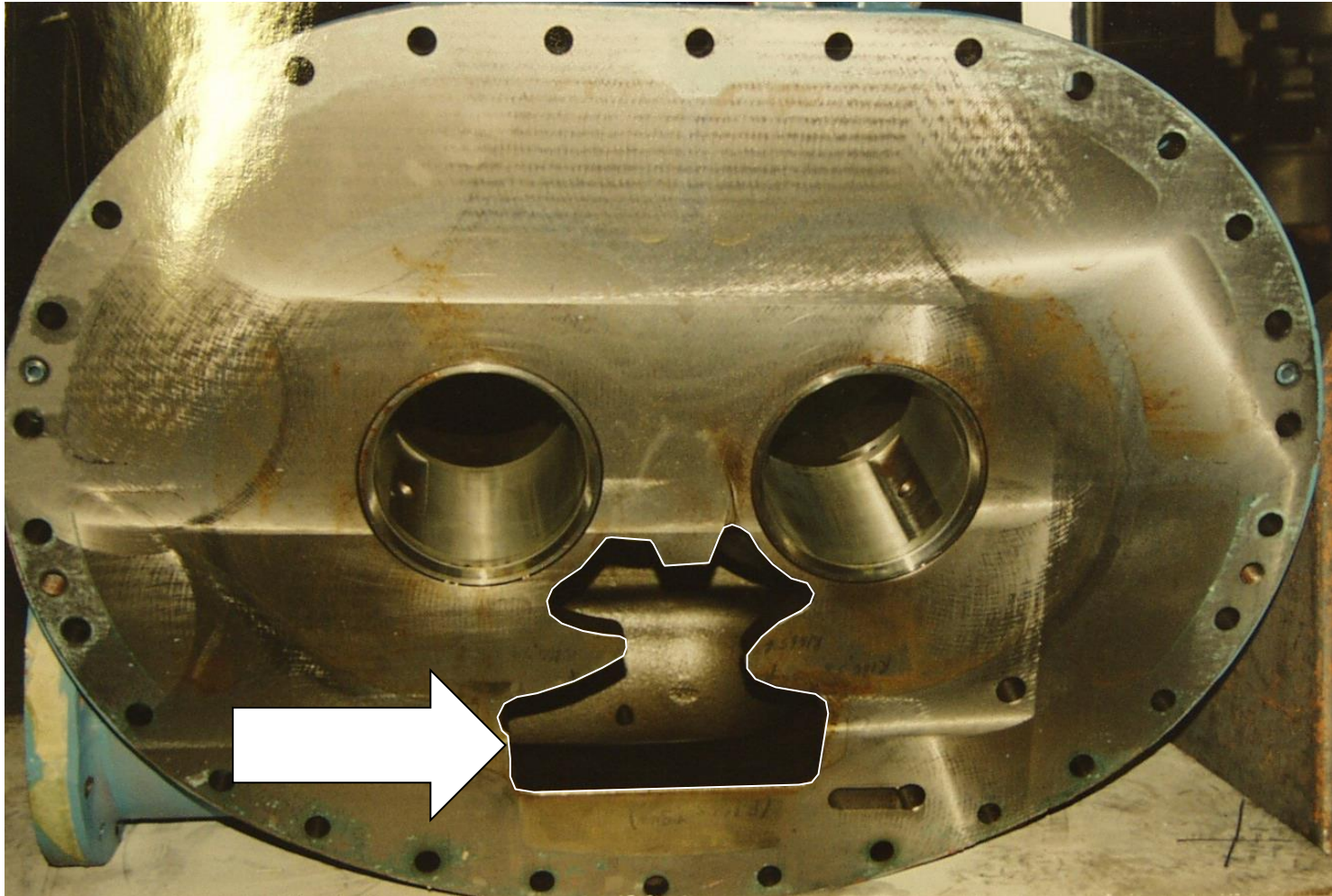
OPERATION



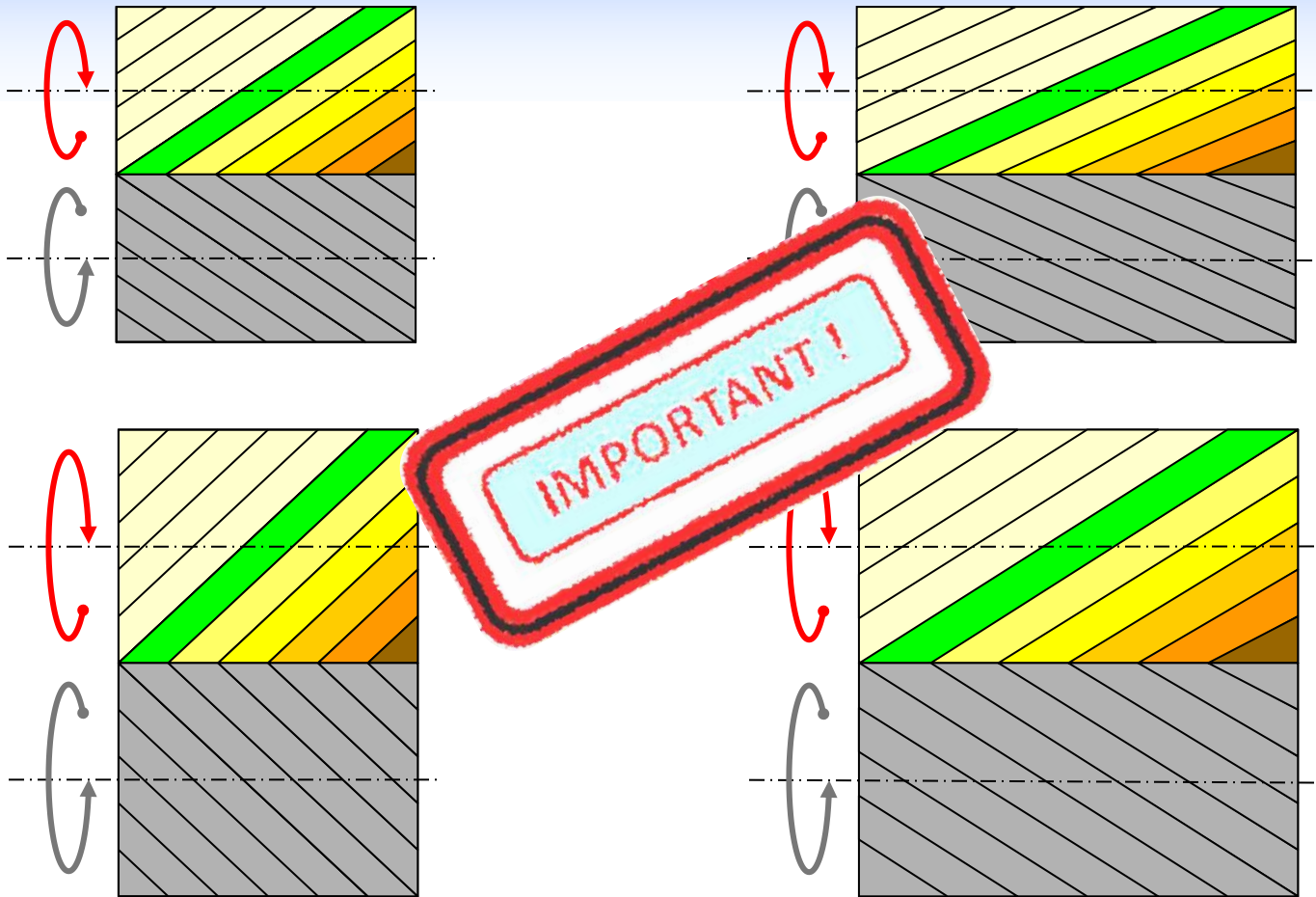
LET'S PLAY WITH THE MODEL !



THE DISCHARGE PORT



VOLUME FLOW



The volume flow of a screw compressor varies:

- according to the **length** of the screw,
- according to the **diameter** of the screw.

THE OIL LUBRICATED SCREW COMPRESSOR

How does it work ?

Why does it need oil ?

THE ADIABATIC COMPRESSION OF HELIUM

$$\frac{T_{\text{dis}}}{T_{\text{suc}}} = \left(\frac{P_{\text{dis}}}{P_{\text{suc}}} \right)^{\frac{\gamma - 1}{\gamma}}$$

For helium, REFPROP
returns : $\gamma = 1,6747$

Example : compression of helium, from 1.05, 300 K, up to 15 bar

$$T_{\text{dis}} = 300 \times \left(\frac{15}{1,05} \right)^{\frac{1,6747 - 1}{1,6747}} = 876 \text{ K !} \quad \text{or } 603 \text{ } ^\circ\text{C}$$

Obviously, the adiabatic
compression of helium is
too difficult !

THE DUTY OF OIL

Oil is injected **during** the compression phase.

It is **finely dispersed**.

Its contact area with helium is **very large**.

It absorbs, by **fast** heat exchange with helium, the **major part** of the **compression heat**.

It improves leak tightness between the rotors.

Accessorially, it lubricates the compressor.

HOW MUCH OIL IS NECESSARY ?

To cool 1 g/s of helium from 864 K to 300 K, one needs to withdraw :

$$(876 - 300) \times \overset{\text{Cp of helium}}{\downarrow} 5.2 = 2995 \text{ W}$$

If one wants to reduce the increase of temperature, a part of the 2930 W has to be absorbed.

Let 's aim at 80°C (353 K) : we shall remove 2720 W.

If oil, the Cp of which is 1,95 J/g, is injected at 45 °C, we have to mix :

$$2720/1,95 \times (353 - 318) = \mathbf{40 \text{ grams of oil per gram of helium !}}$$

An oil lubricated screw compressor for helium is mainly an **oil pump** !

But the oil versus helium **volume flow** ratio is **8.6 %**.

ISOTHERMAL EFFECTIVENESS OF SCREW COMPRESSORS

$$\frac{\text{isothermal compression power}}{\text{actual compression power (at motor terminal)}} = 0.45 \text{ to } 0.58$$

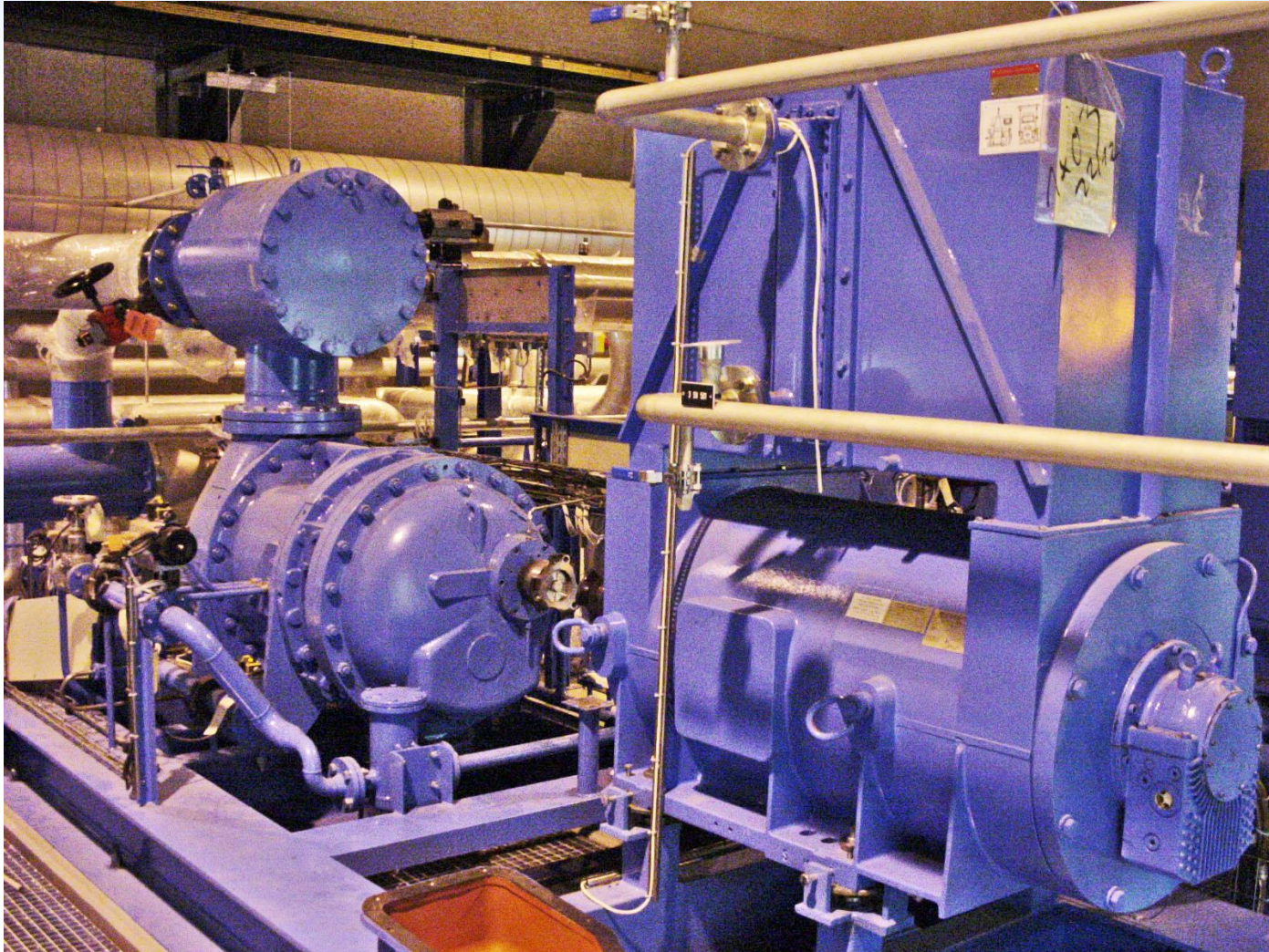
WHERE DOES ENERGY GO?

Assuming that all the energy is released through oil and helium coolers.

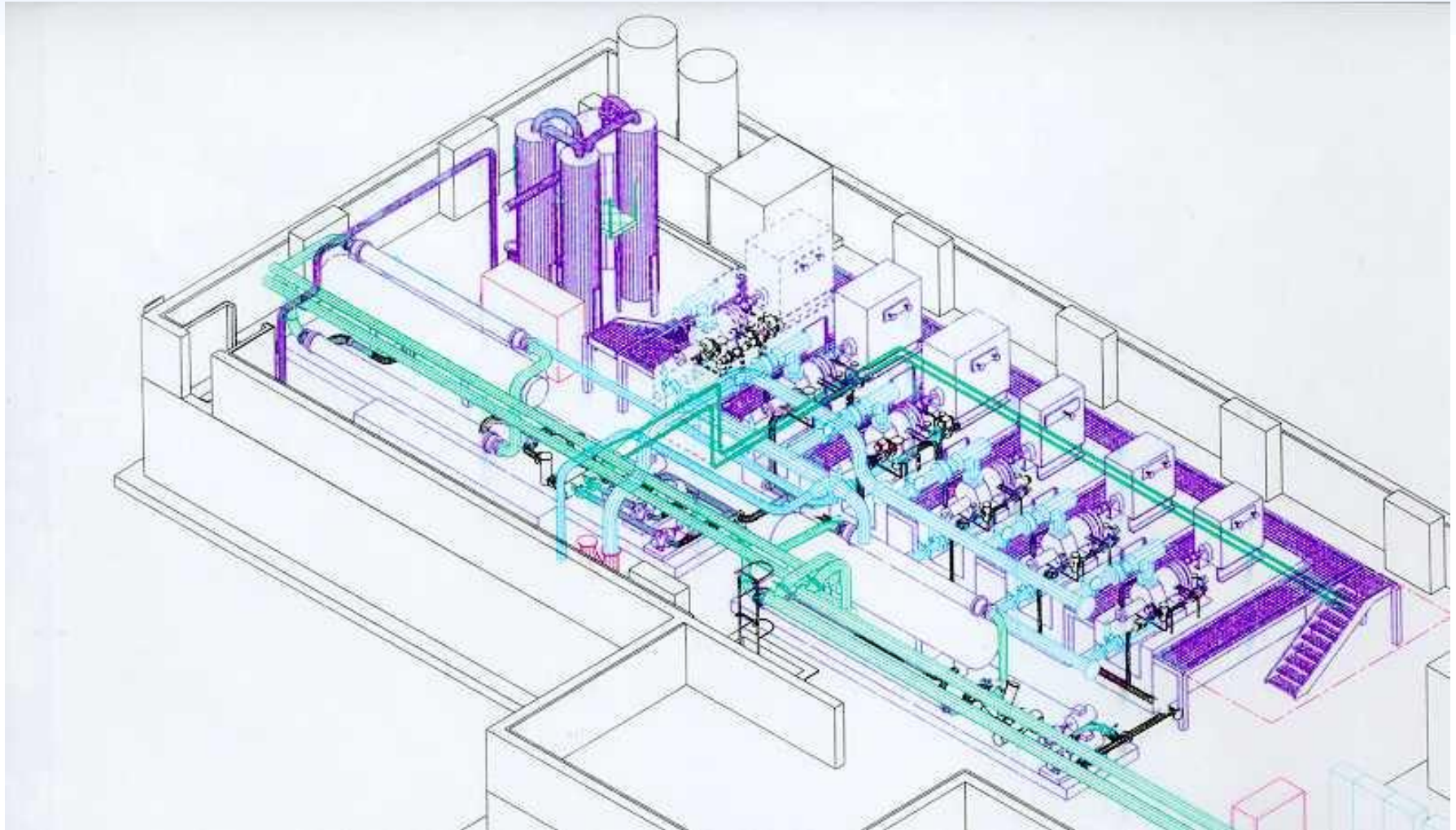
Mass flow	(g/s)	100,00	
Suction pressure	(bar)	1,05	
Suction temperature	(°C)	20,00	
Discharge pressure	(bar)	14,00	
Shaft power	(kW)	284,00	
Oil injection temperature	(°C)	45,00	
Compressor discharge temperature	(°C)	80,00	
Oil cooler power	(kW)	245,96	0,87
He cooler power	(kW)	25,96	0,09

About 10 to 15 % of the energy is released in the ambient.

COMPRESSOR AND MOTOR



A LARGE COMPRESSION STATION



LHC COMPRESSION STATION



THE OIL REMOVAL SYSTEM

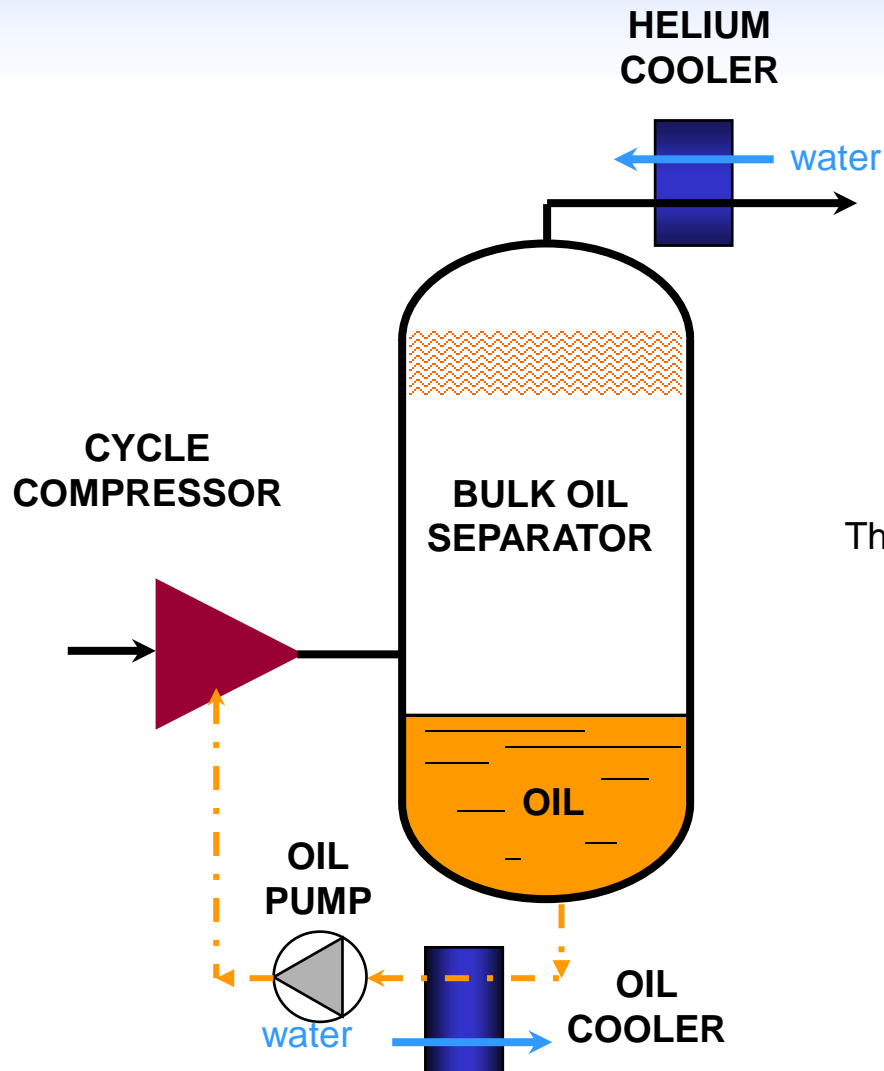
OIL IN HELIUM AT THE DISCHARGE SIDE OF A SCREW COMPRESSOR

A big quantity of liquid

A lot of aerosols

A little bit of vapour

BULK OIL SEPARATOR



There is also an horizontal version of such a bulk oil separator

OIL IN HELIUM AT THE DISCHARGE SIDE OF THE BULK OIL SEPARATOR

A LOT OF AEROSOLS

A LITTLE BIT OF VAPOUR

AEROSOL SEPARATION

PROCESS : COALESCENCE

Agglomerate small particles

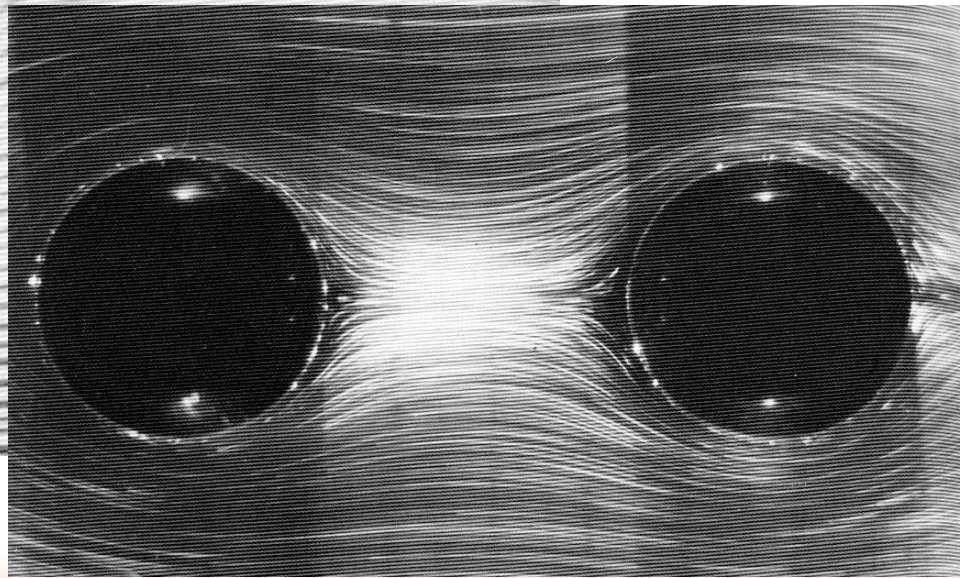
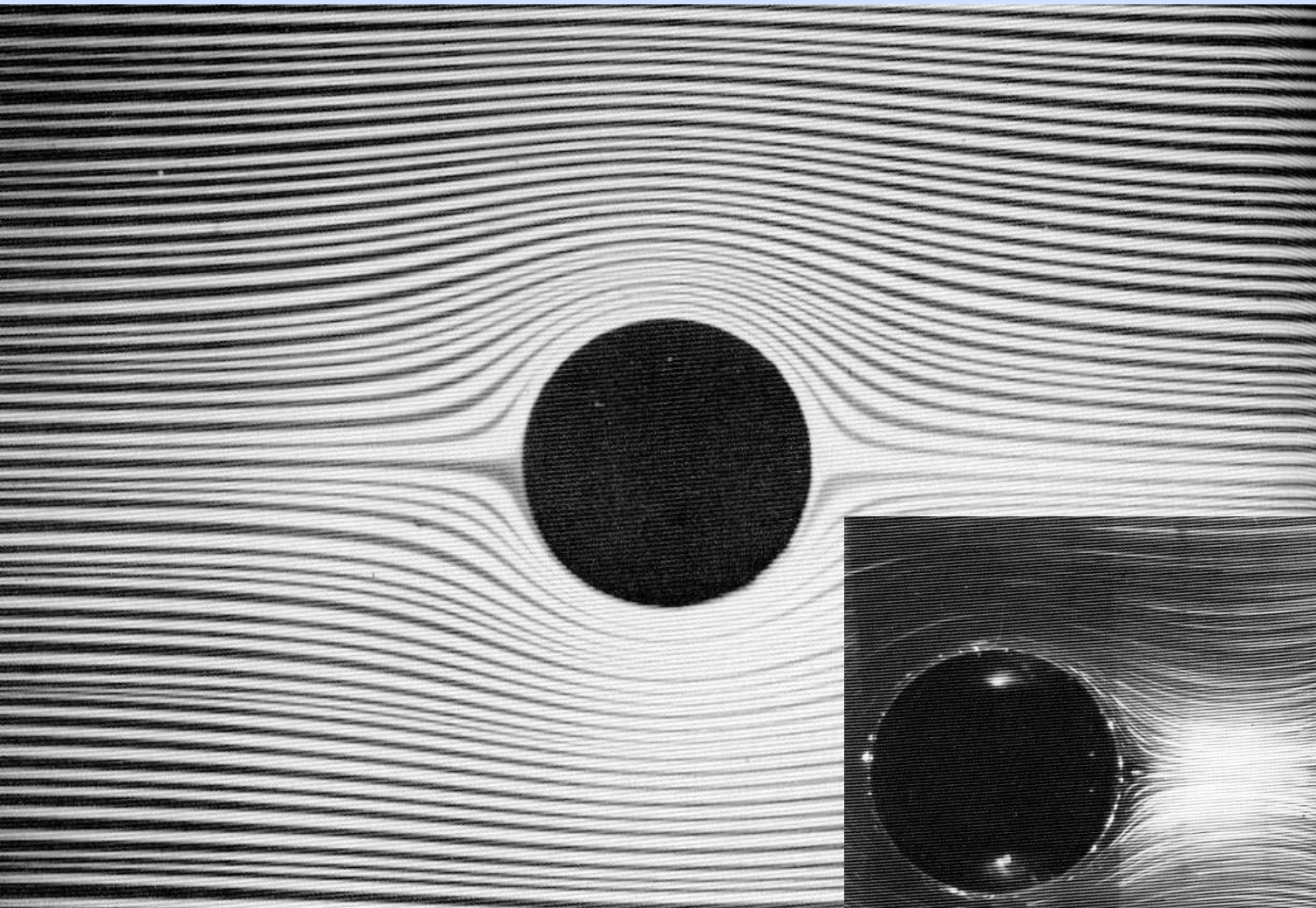
into **bigger ones**

in order they can be easily separated by **gravity**.

No effect on vapour

Obviously!

FLOW PATTERN



INERTIAL IMPACTION

LARGE PARTICLES ($> 3 \mu\text{m}$)

FIBRE

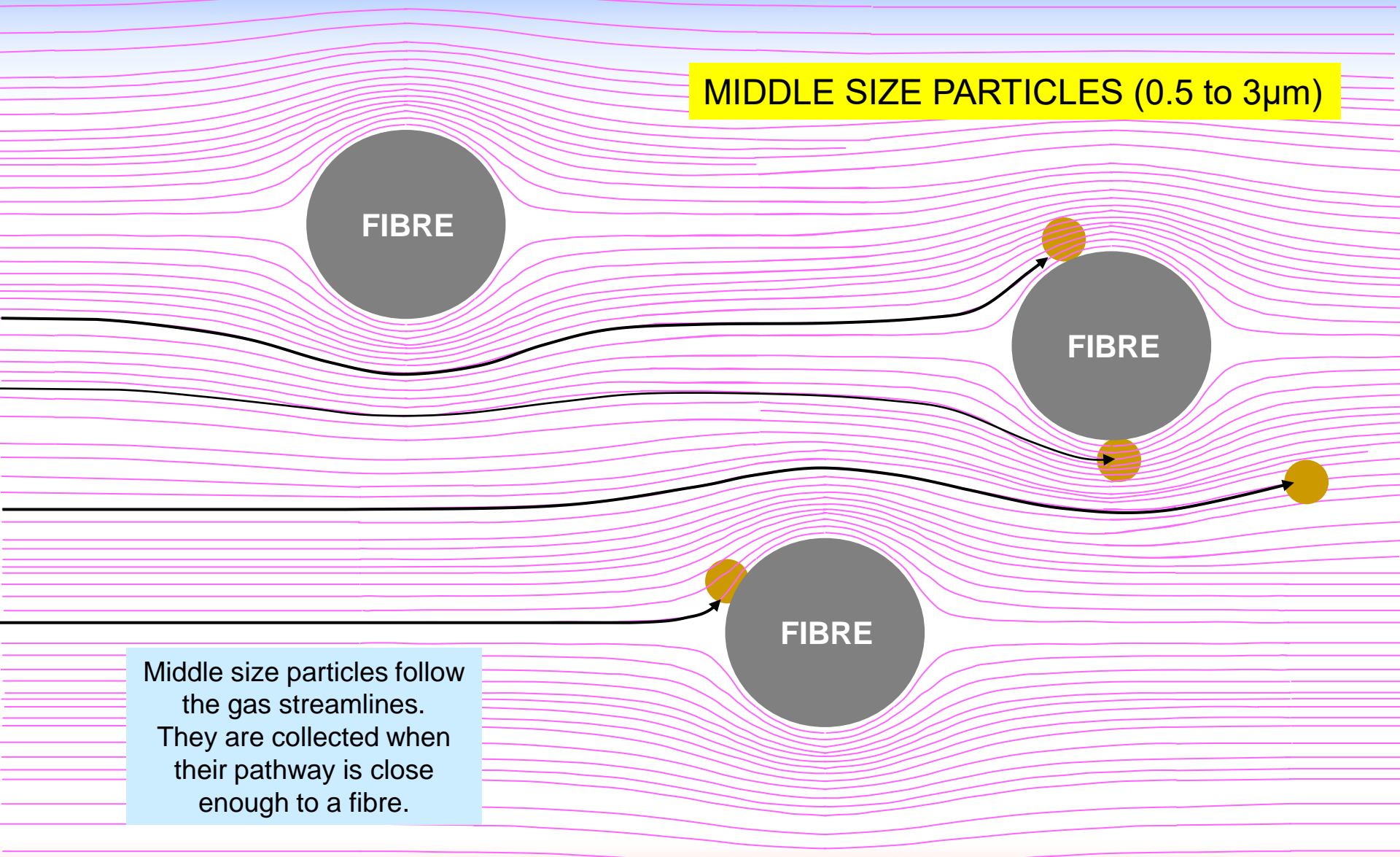
FIBRE

FIBRE

Large particles have too high a momentum to permit them to follow the gas streamlines. They **collide** with fibres.

DIRECT INTERCEPTION

MIDDLE SIZE PARTICLES (0.5 to 3 μ m)



FIBRE

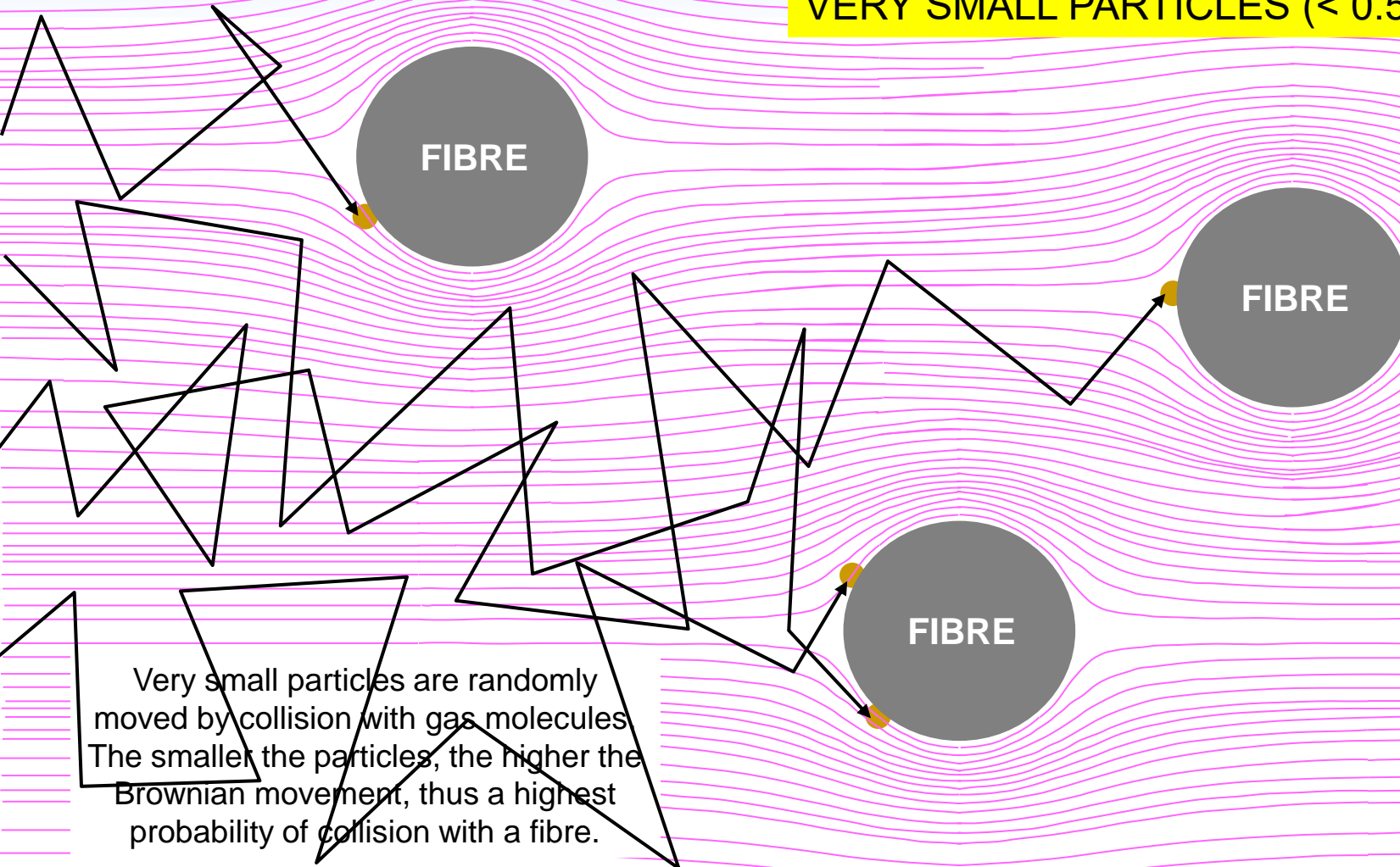
FIBRE

FIBRE

Middle size particles follow the gas streamlines. They are collected when their pathway is close enough to a fibre.

BROWNIAN MOVEMENT

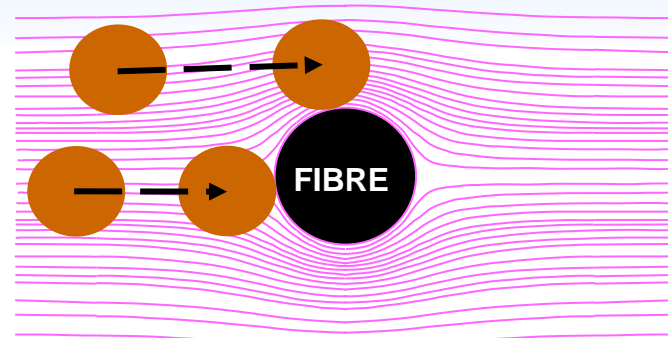
VERY SMALL PARTICLES ($< 0.5 \mu\text{m}$)



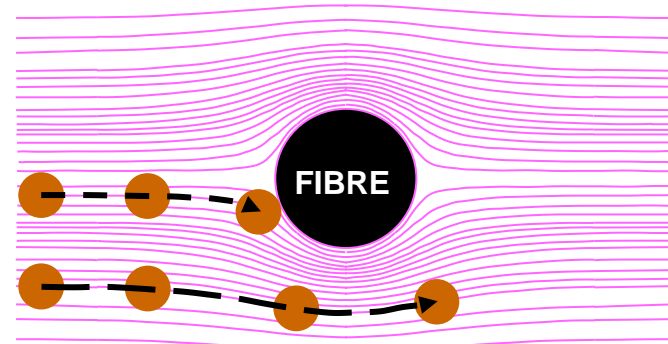
Very small particles are randomly moved by collision with gas molecules. The smaller the particles, the higher the Brownian movement, thus a highest probability of collision with a fibre.

AEROSOL CAPTURE PROCESS

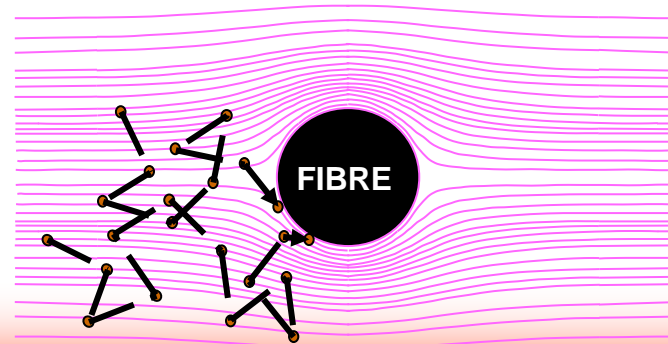
INERTIAL IMPACTION



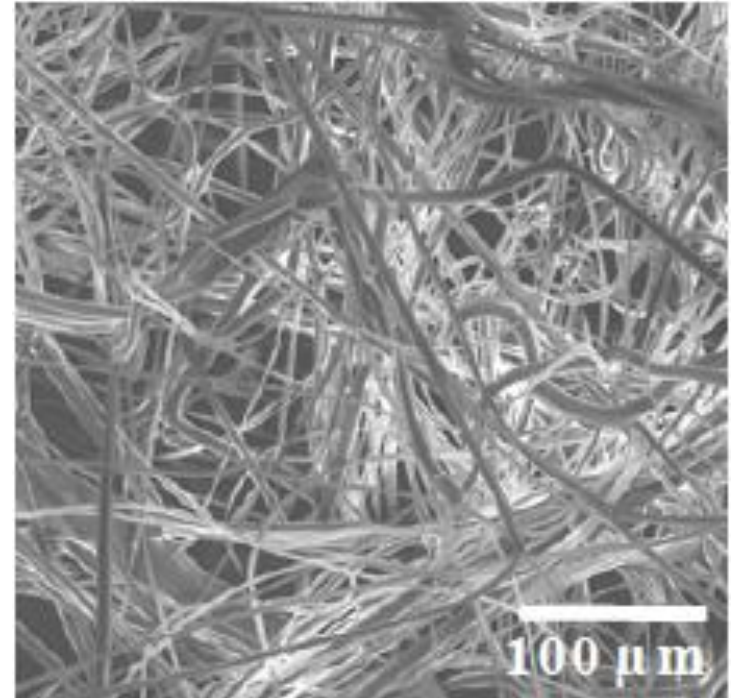
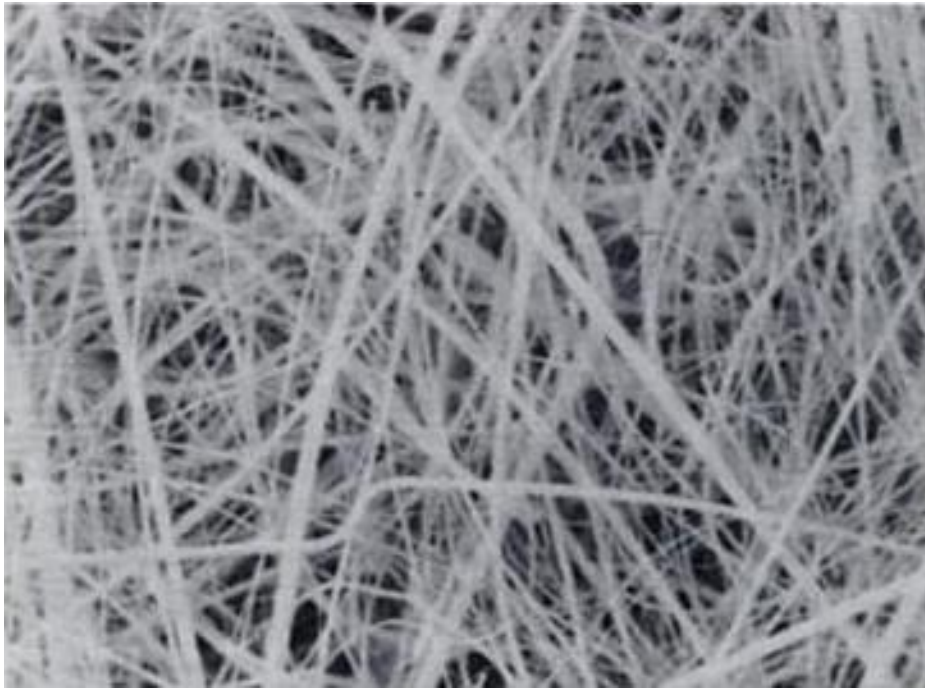
DIRECT INTERCEPTION



BROWNIAN MOVEMENT



FILTERING MEDIA



SURPRISING BEHAVIOUR !

It is not obvious to have an idea of the behaviour of an oil aerosol !

Oil in helium at 20 bar, 80 °C

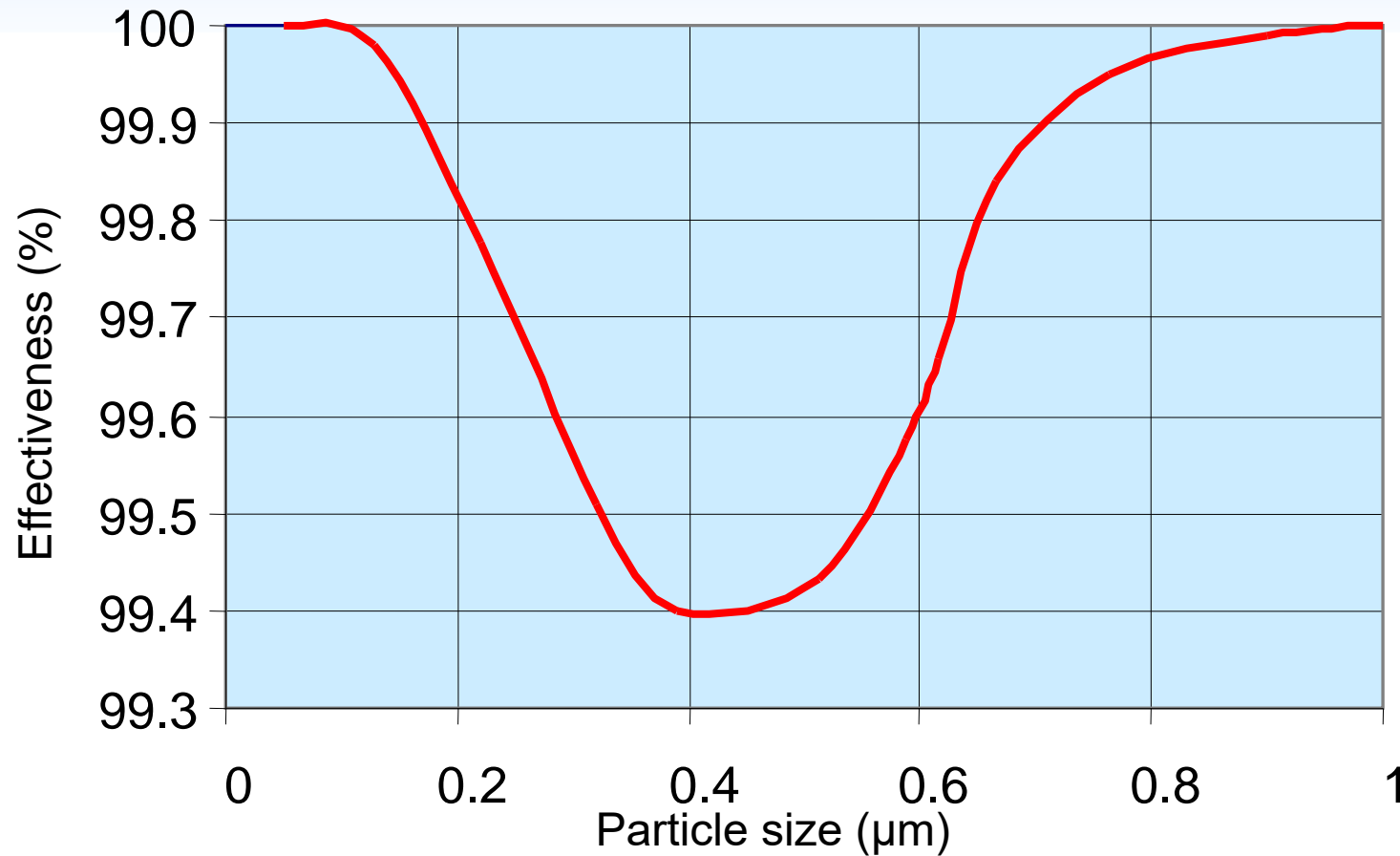
Droplet diameter	(μm)	0.016	0.12	0.91
Falling velocity	(mm/s)	0.01	0.1	1.0

Thumb rule : velocity in mm/s = diameter in μm

The result of this calculation for very small diameters is certainly affected by Brownian movement of helium molecules...

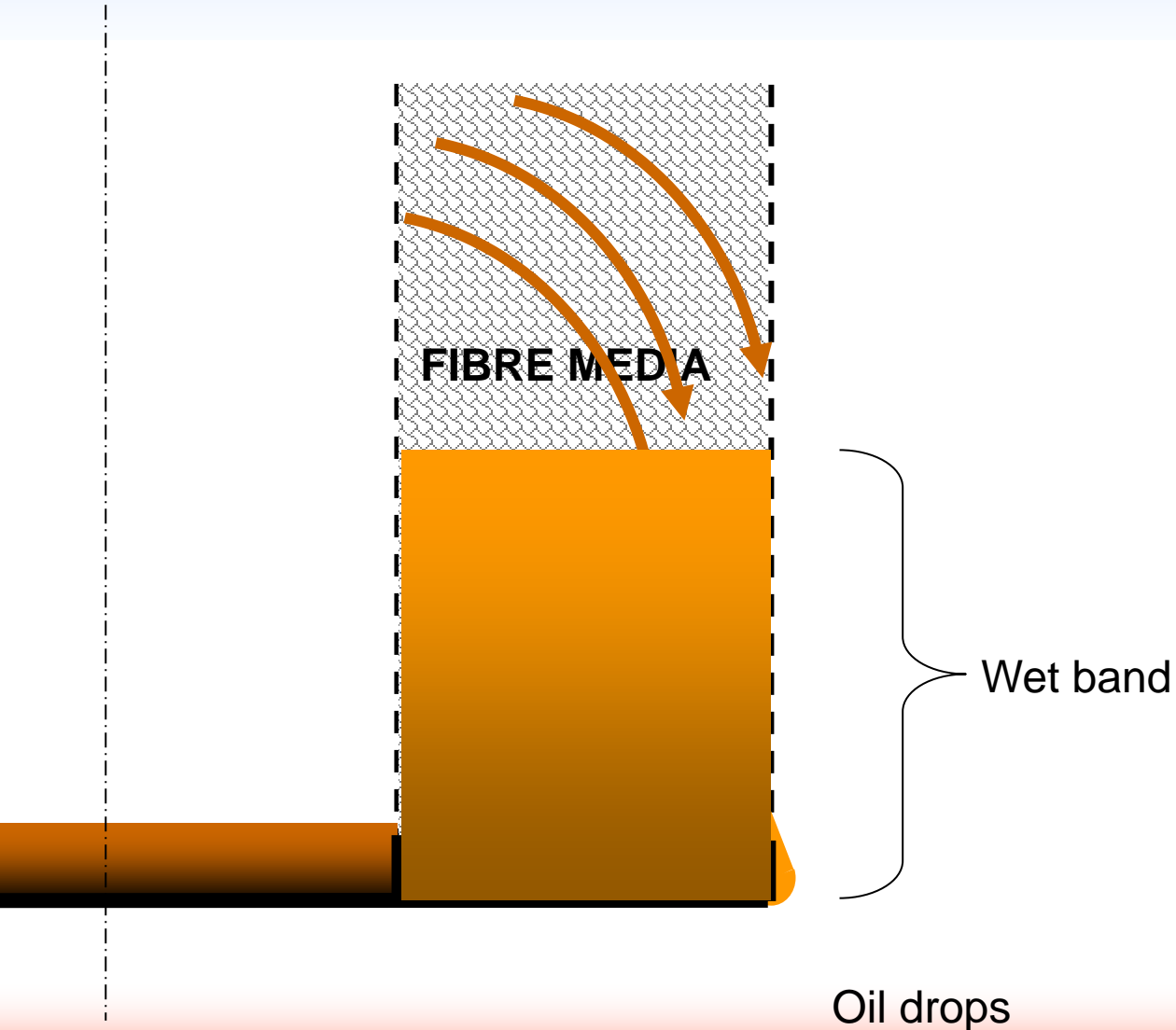
EFFECTIVENESS OF A COALESCER

VERSUS PARTICLE SIZE



Provided that the cartridge sizing is correct !

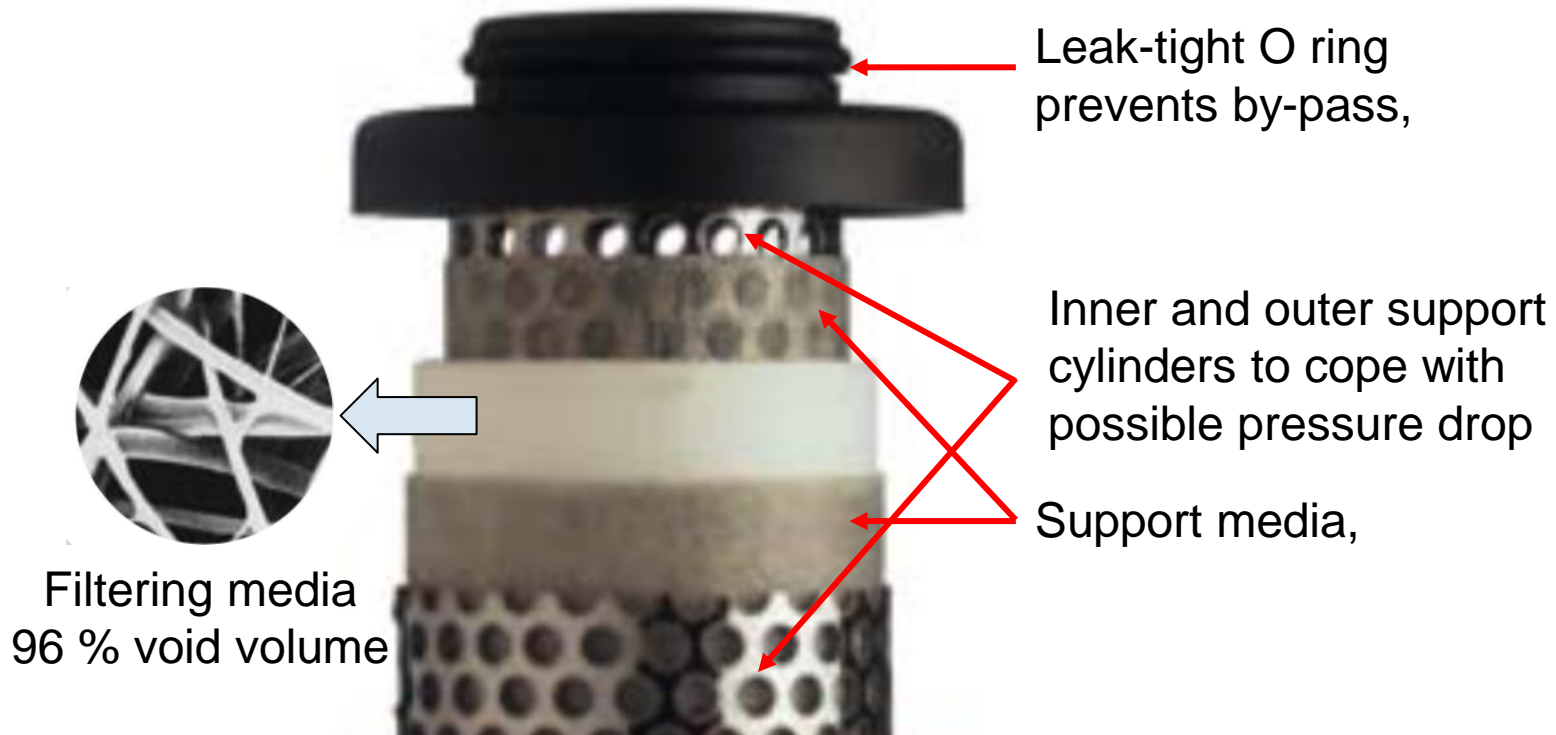
CARTRIDGE CROSS SECTION



Oil drops



A SMALL CARTRIDGE



Domnick Hunter

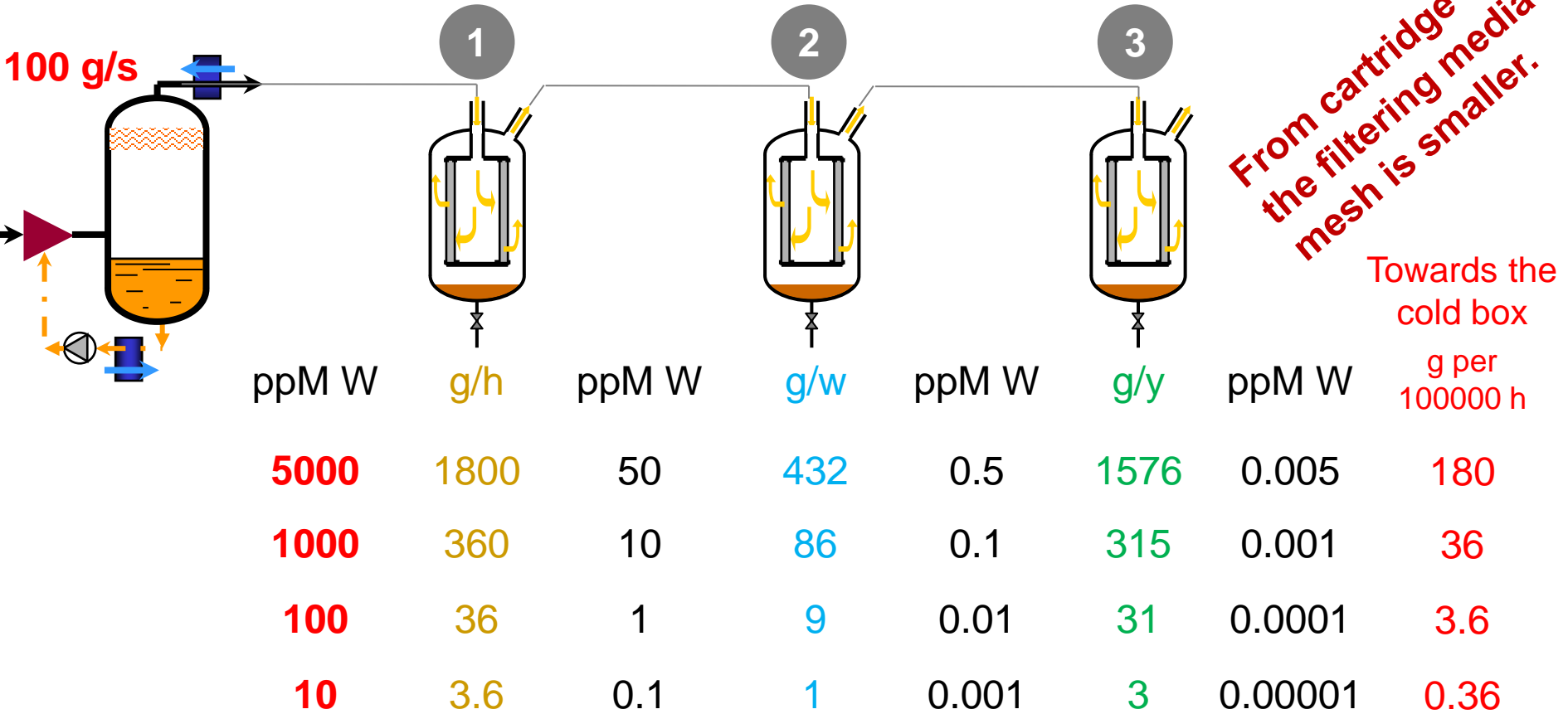
A LARGE CARTRIDGE

Media is stuffed into a metal cage.



HOW TO REACH AN ACCEPTABLE OIL CONCENTRATION ?

Assuming that the effectiveness of one stage of coalescer is 99 %, how many stages are to be implemented ?



TRAPPING OF OIL VAPOUR

PROCESS : ADSORPTION
AT ROOM TEMPERATURE
WITH **ACTIVATED CHARCOAL**

NOT EFFICIENT FOR AEROSOLS

Obviously!

SELECTION OF THE OIL

Viscosity : only for **mechanical** reasons (depends only on the compressor operation).

Vapour pressure : must be **low** ($<10^{-6}$ mbar at 25 °C), in order to reduce oil vapour entrainment.

OIL TREATMENT

IMPURITIES TO ELIMINATE :

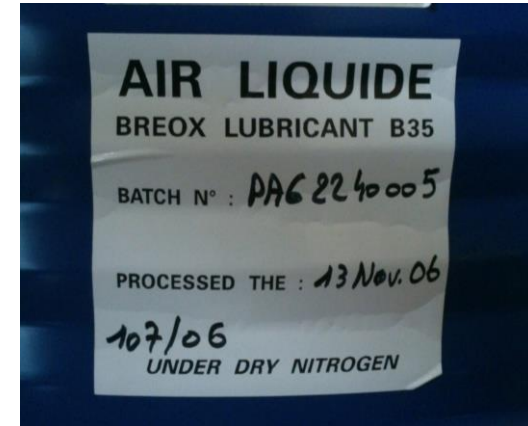
Air : related to the fabrication process

Water : oil is very hygroscopic

The high vapour pressure molecules.

METHOD :

Heating under vacuum.



Fill in and top up with processed oil !

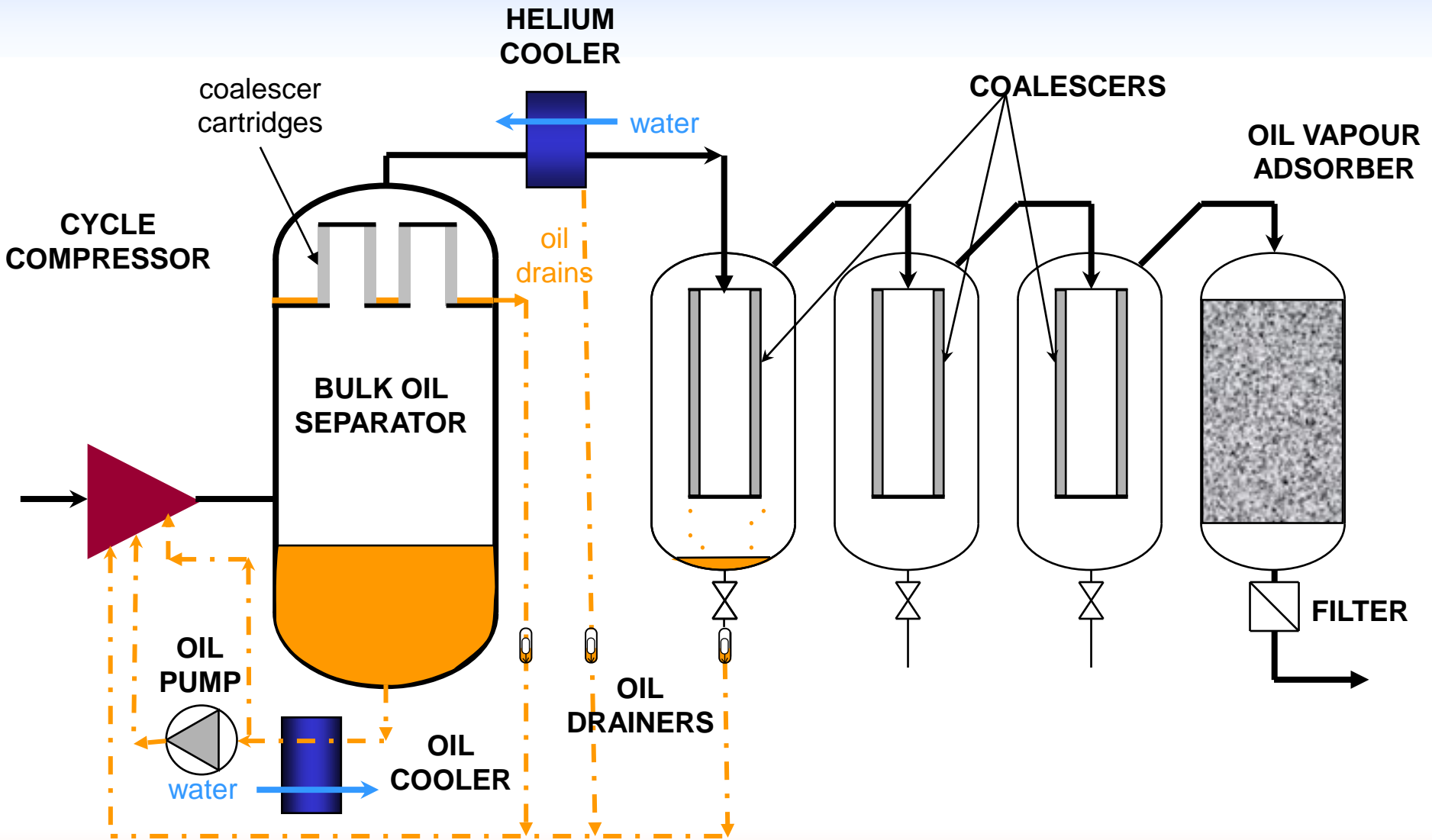
PRECAUTIONS RELATED TO BREOX OIL

Avoid any contact with skin or mucous membranes.

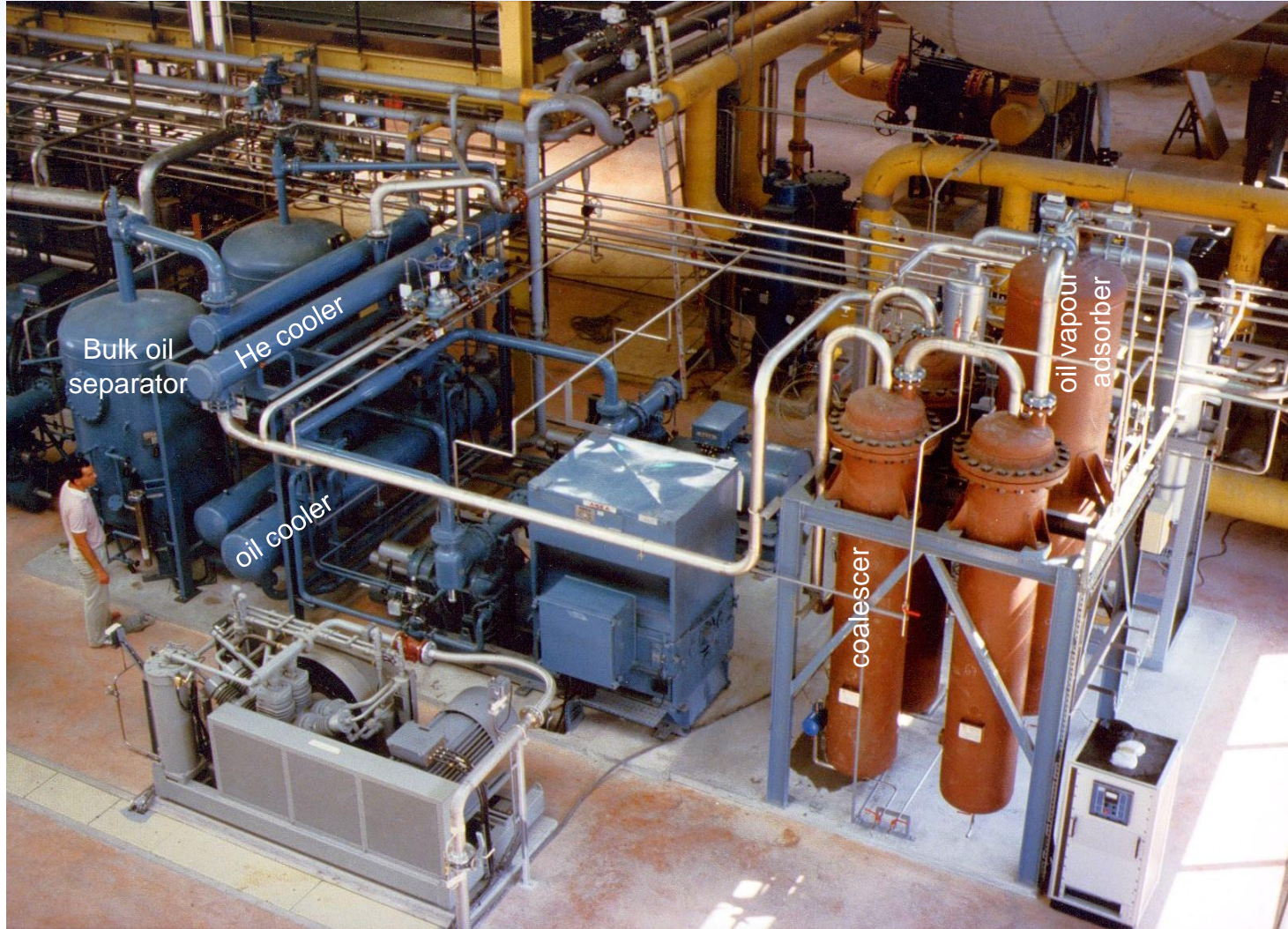
Oil deteriorates paint.

Use **only** Viton seals.

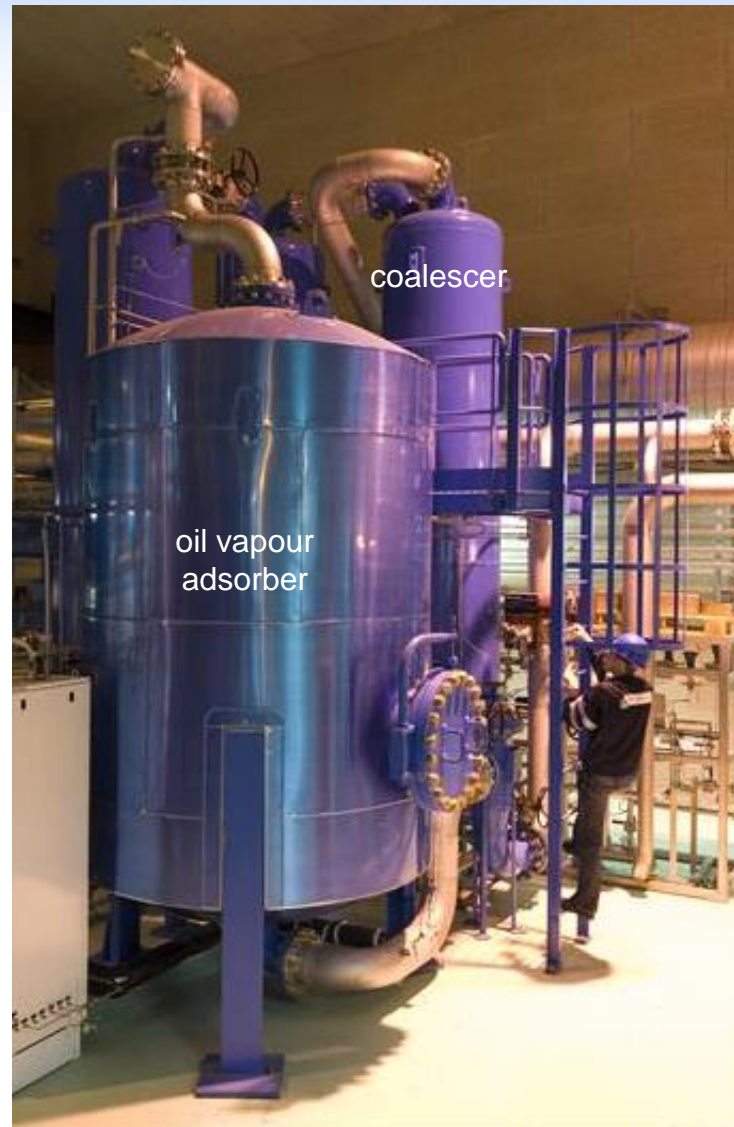
OIL SEPARATION SYSTEM



TORE SUPRA OIL REMOVAL SYSTEM



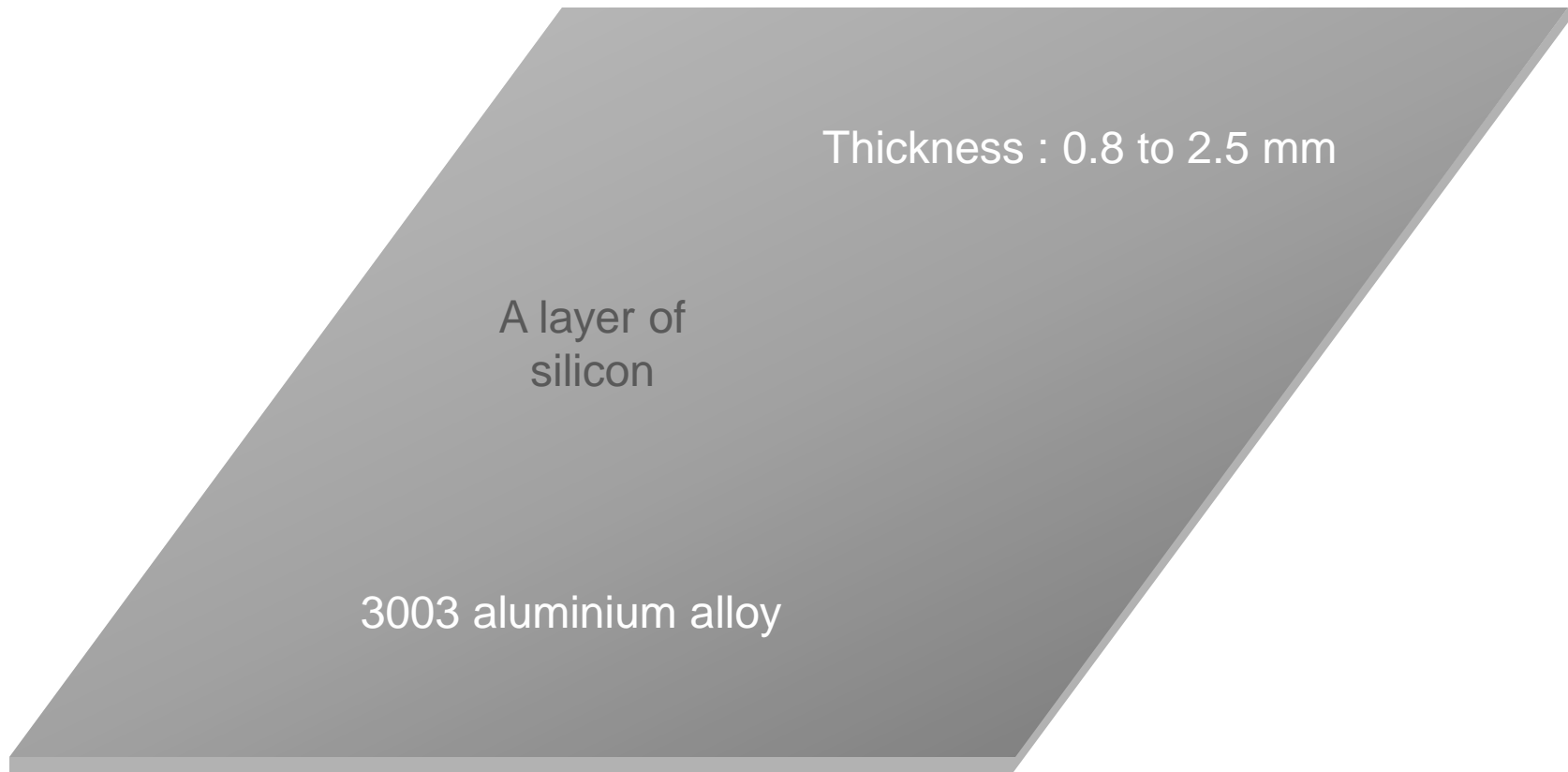
FINAL OIL REMOVAL SYSTEM OF LHC



THE BRASED PLATE AND FIN HEAT EXCHANGERS

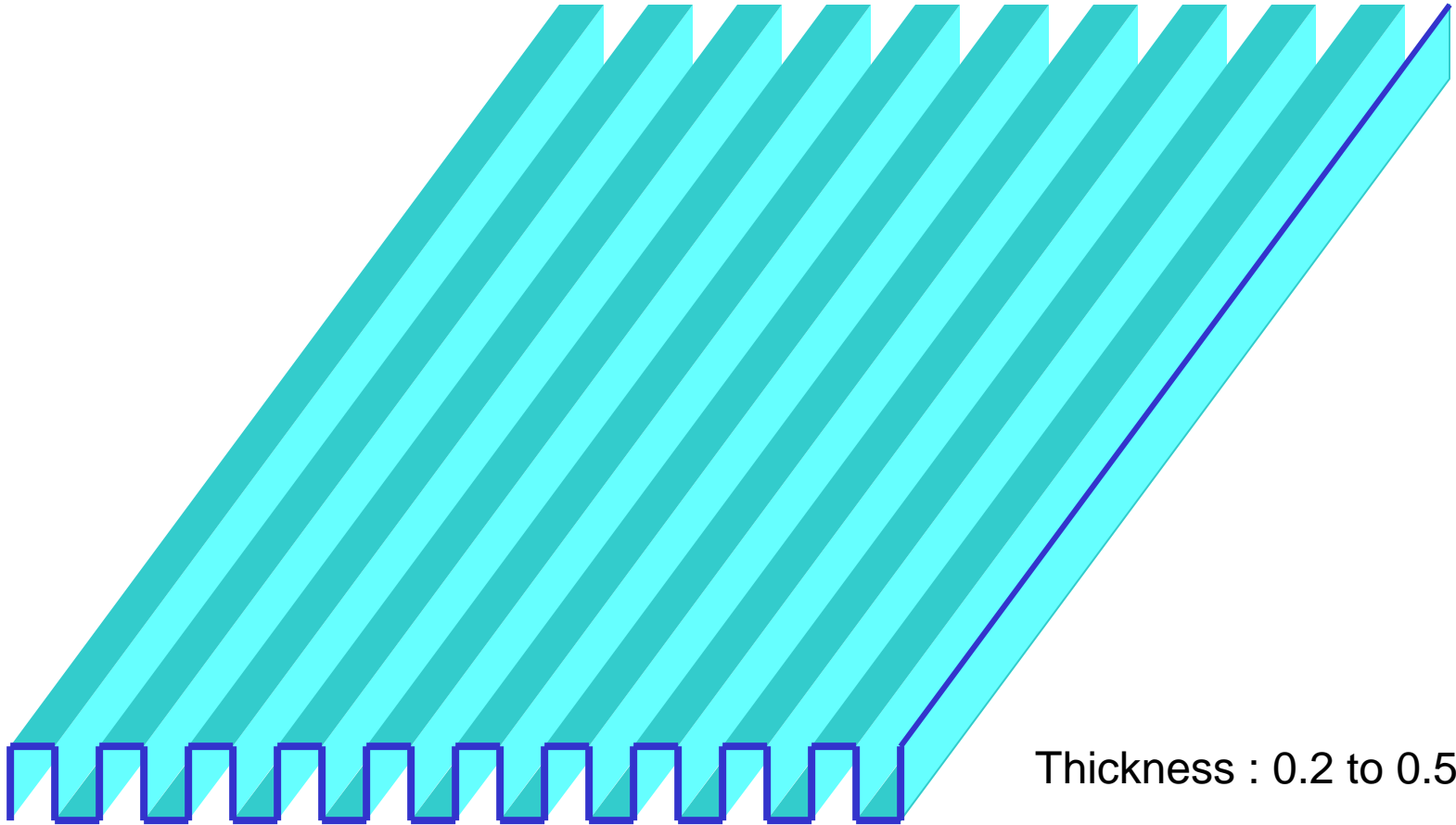
THE BASIC ELEMENTS OF A PLATE AND FIN HEAT EXCHANGER

1. THE PARTING SHEET



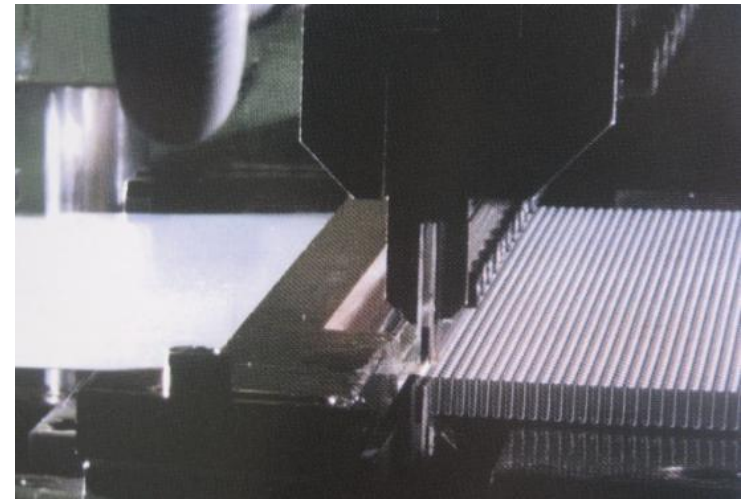
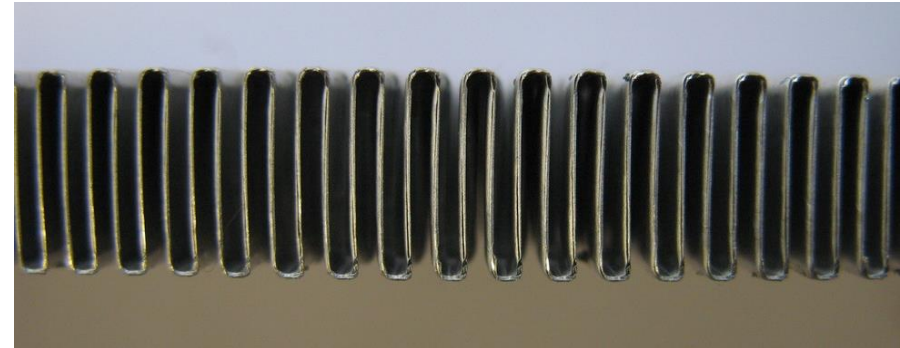
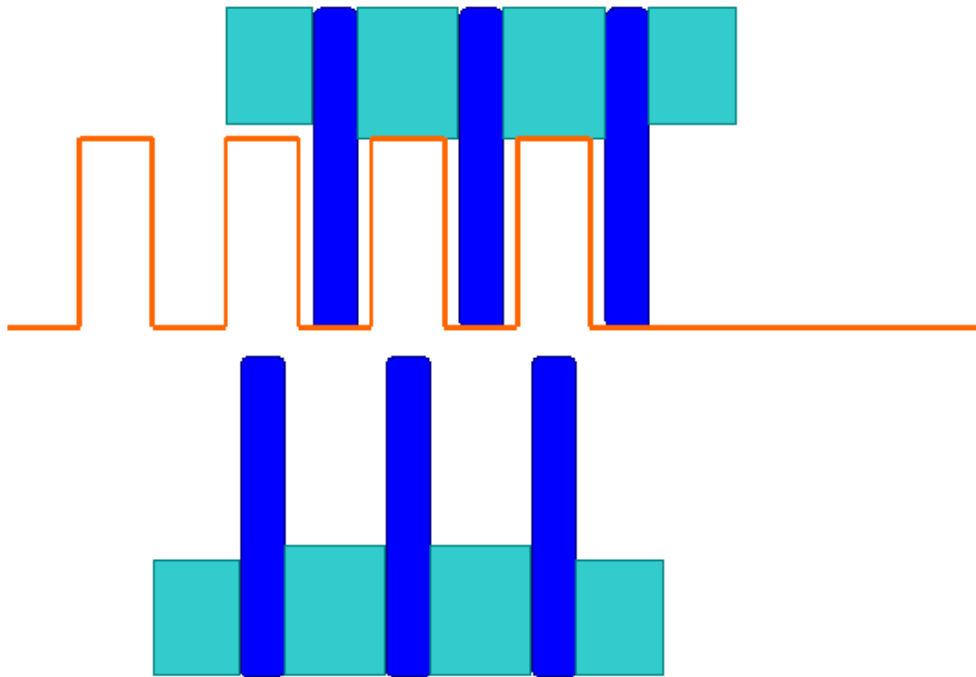
THE BASIC ELEMENTS

THE FINS

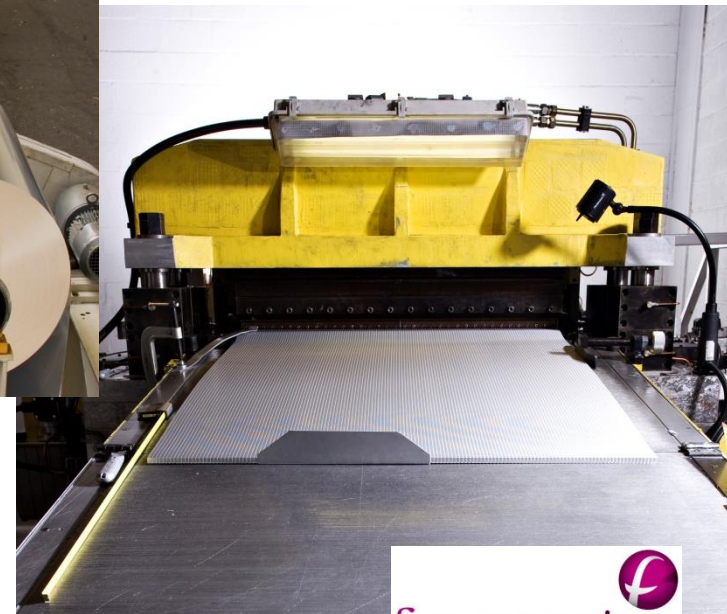
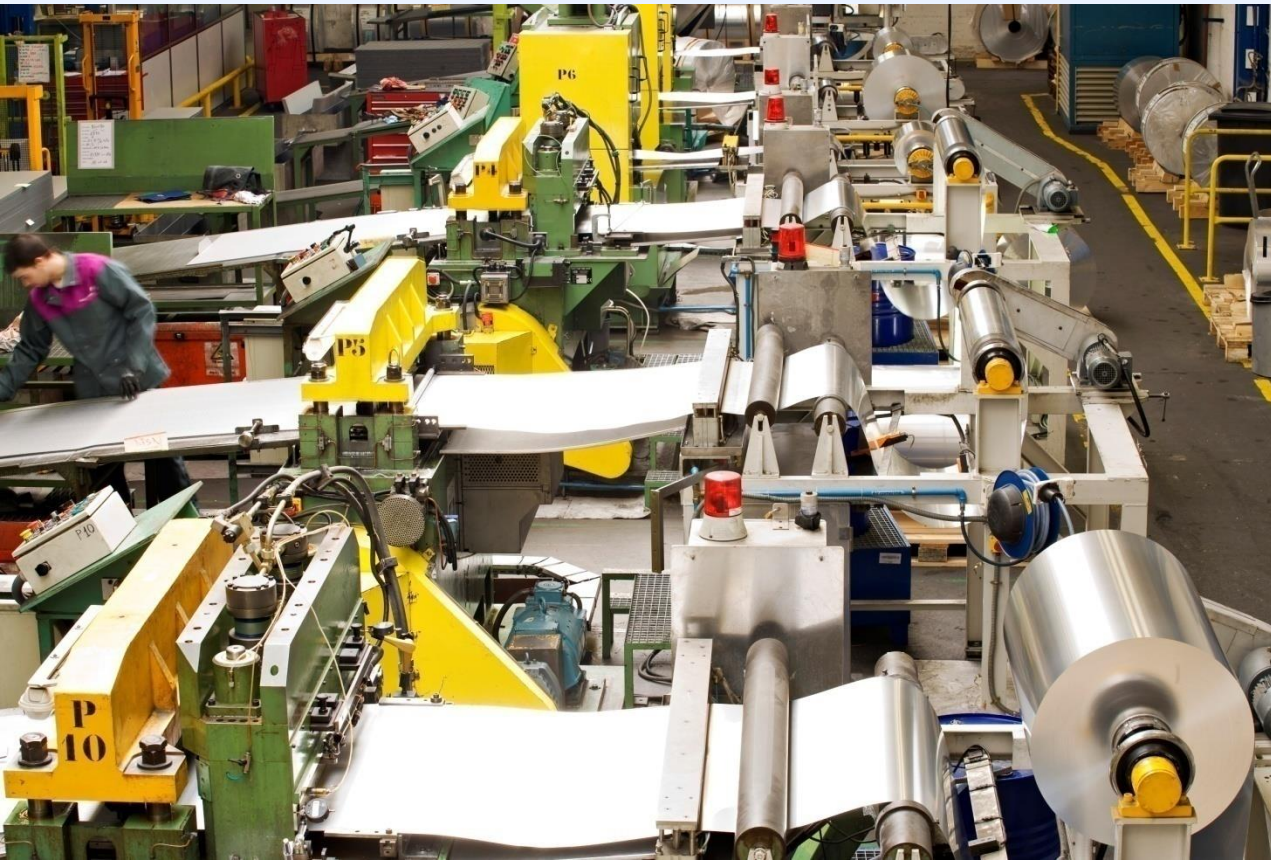


Thickness : 0.2 to 0.5 mm

FIN MACHINING



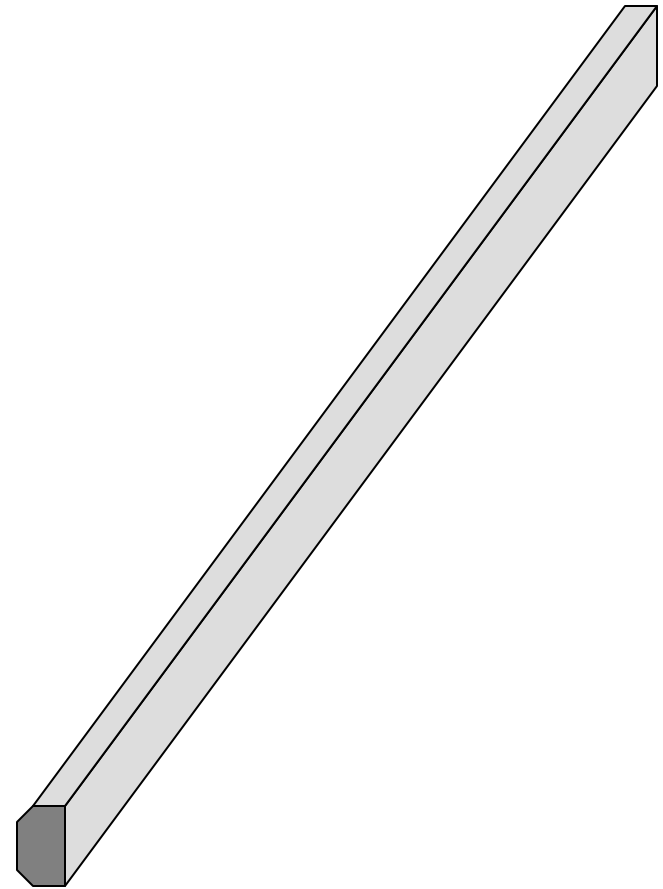
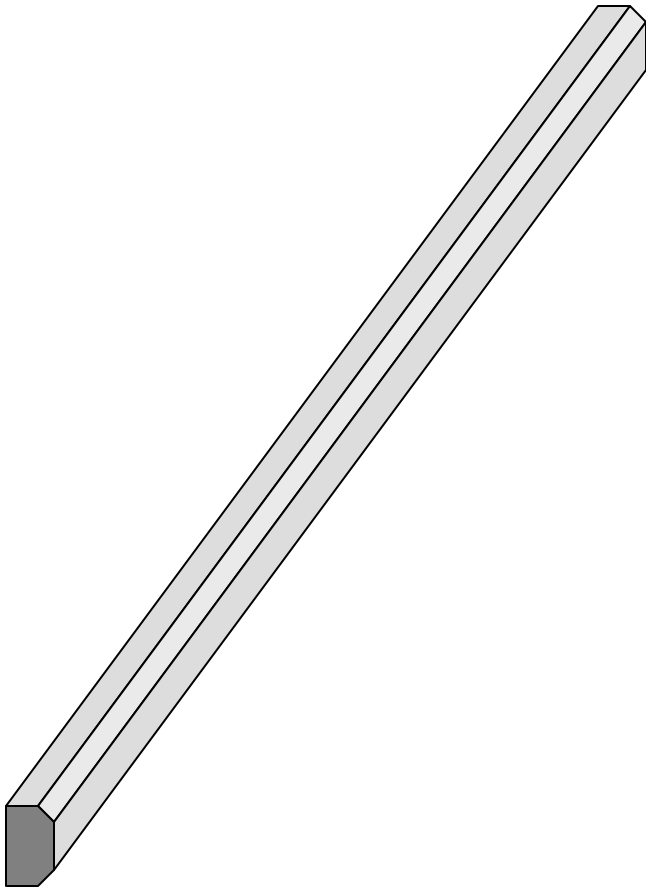
FIN MACHINING



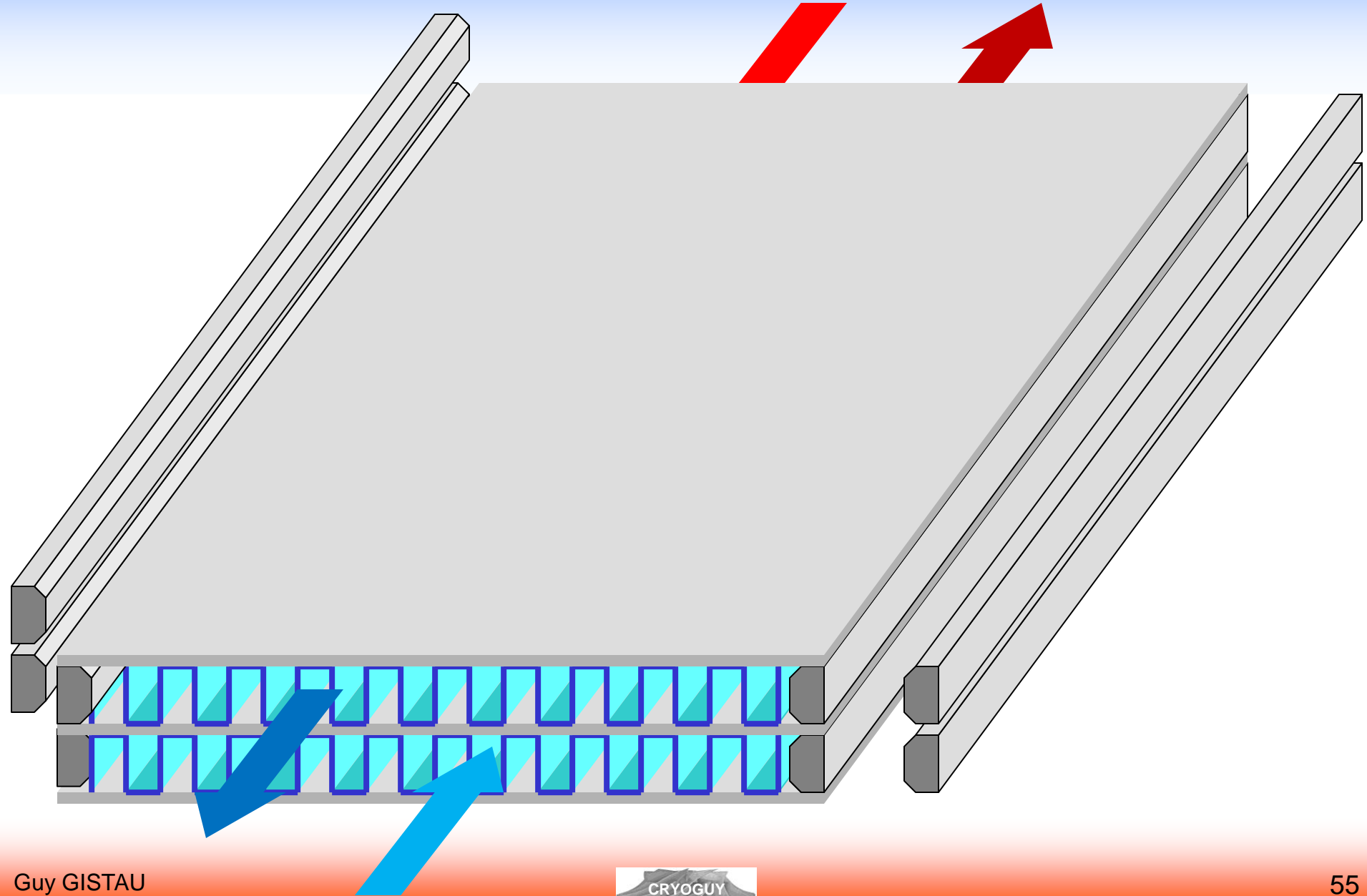
fives cryogenie 

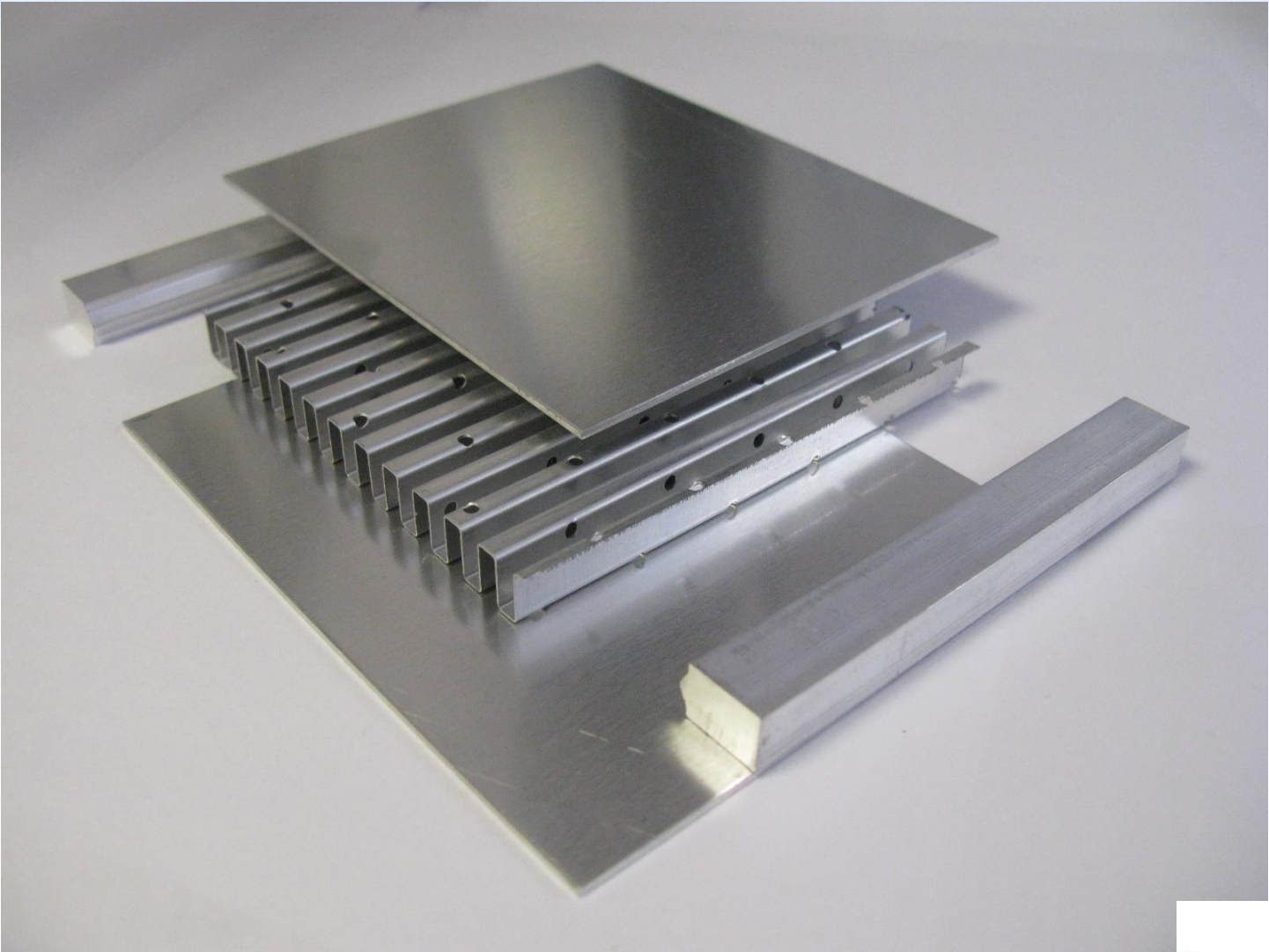
THE BASIC ELEMENTS

THE SIDE BARS



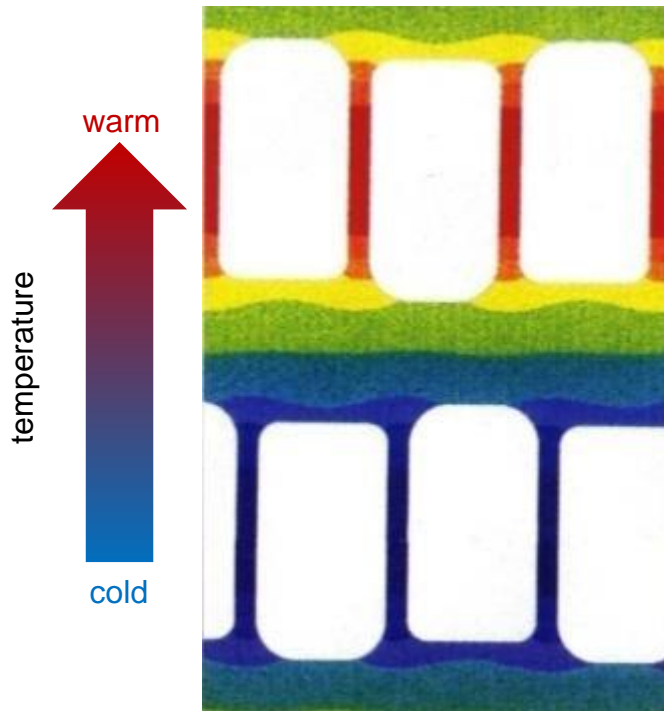
THE CONSTRUCTION





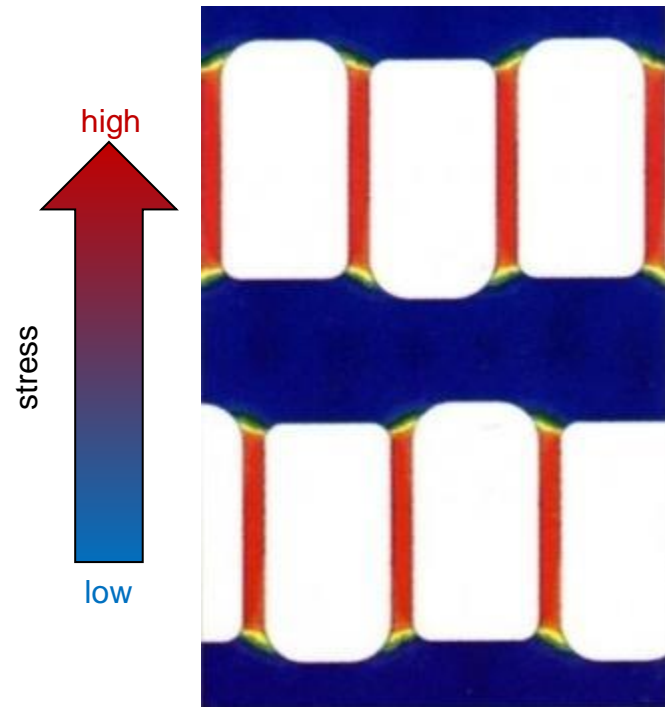
DUTIES OF THE FINS

Transfer heat



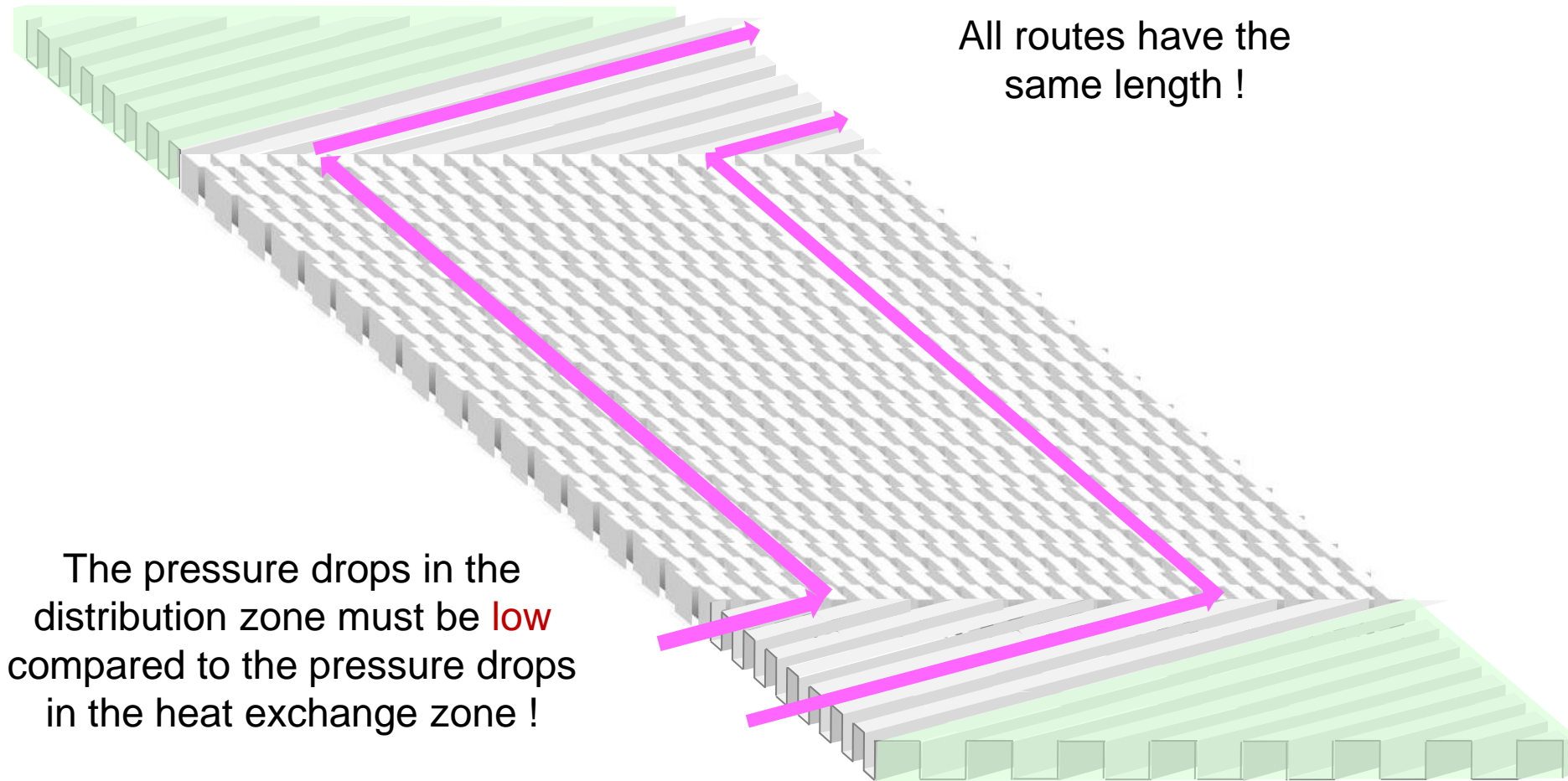
Isotherms of heat transfer from warm passage to cold passage

Withstand the pressure



Mechanical stresses under the effect of internal pressure

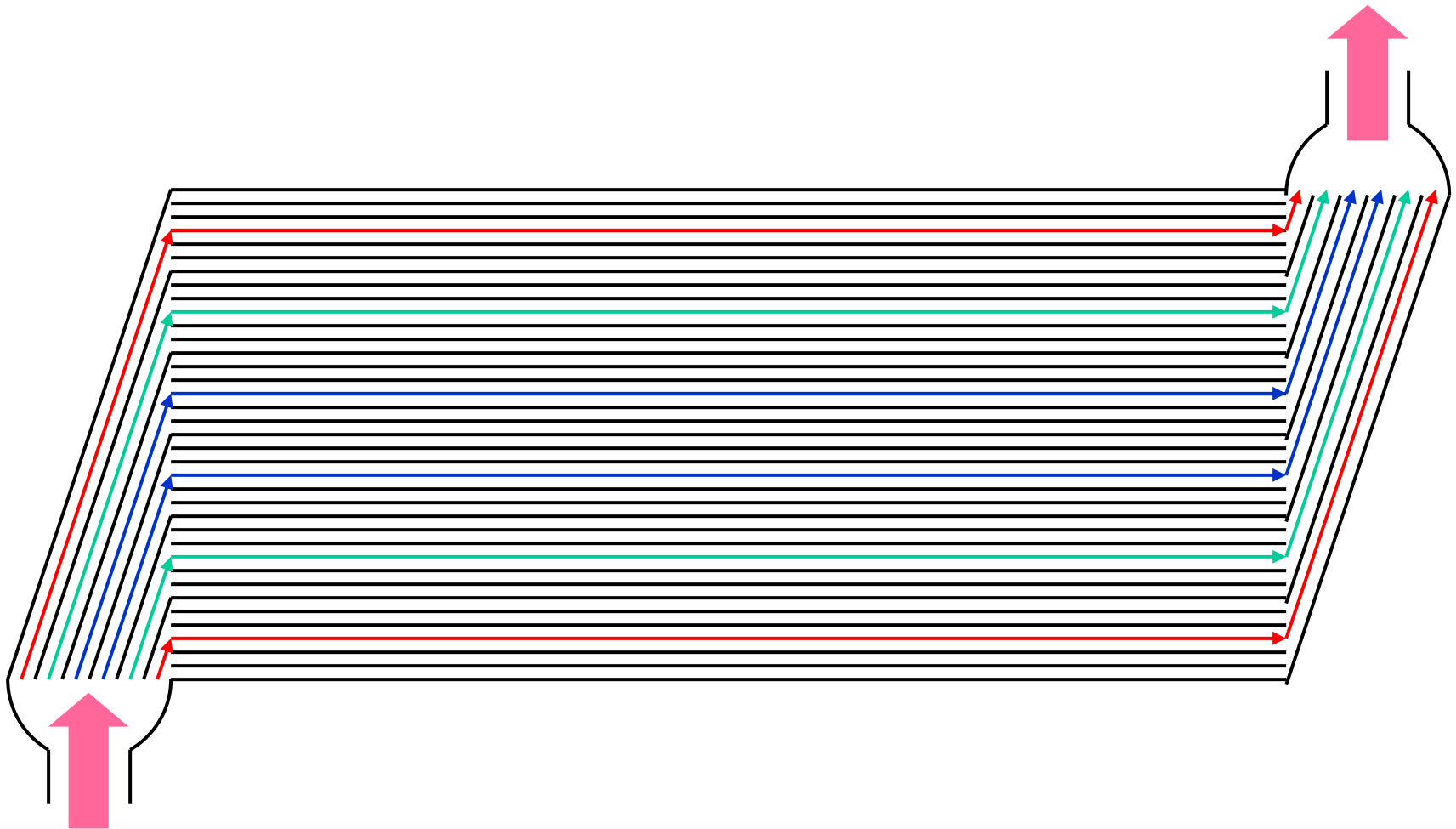
HOW TO EVENLY DISTRIBUTE THE FLUIDS THROUGH THE FINS ?



All routes have the same length !

The pressure drops in the distribution zone must be **low** compared to the pressure drops in the heat exchange zone !

BALANCING THE GAS DISTRIBUTION (1)



PILING UP !



BEFORE BRAZING



Five Cryo



BRAZING PROCESS

The parting sheets have been **covered** with a brazing alloy (silicon).

Fins and parting sheets are **perfectly cleaned**

Fins and parting sheets are **pressed** together

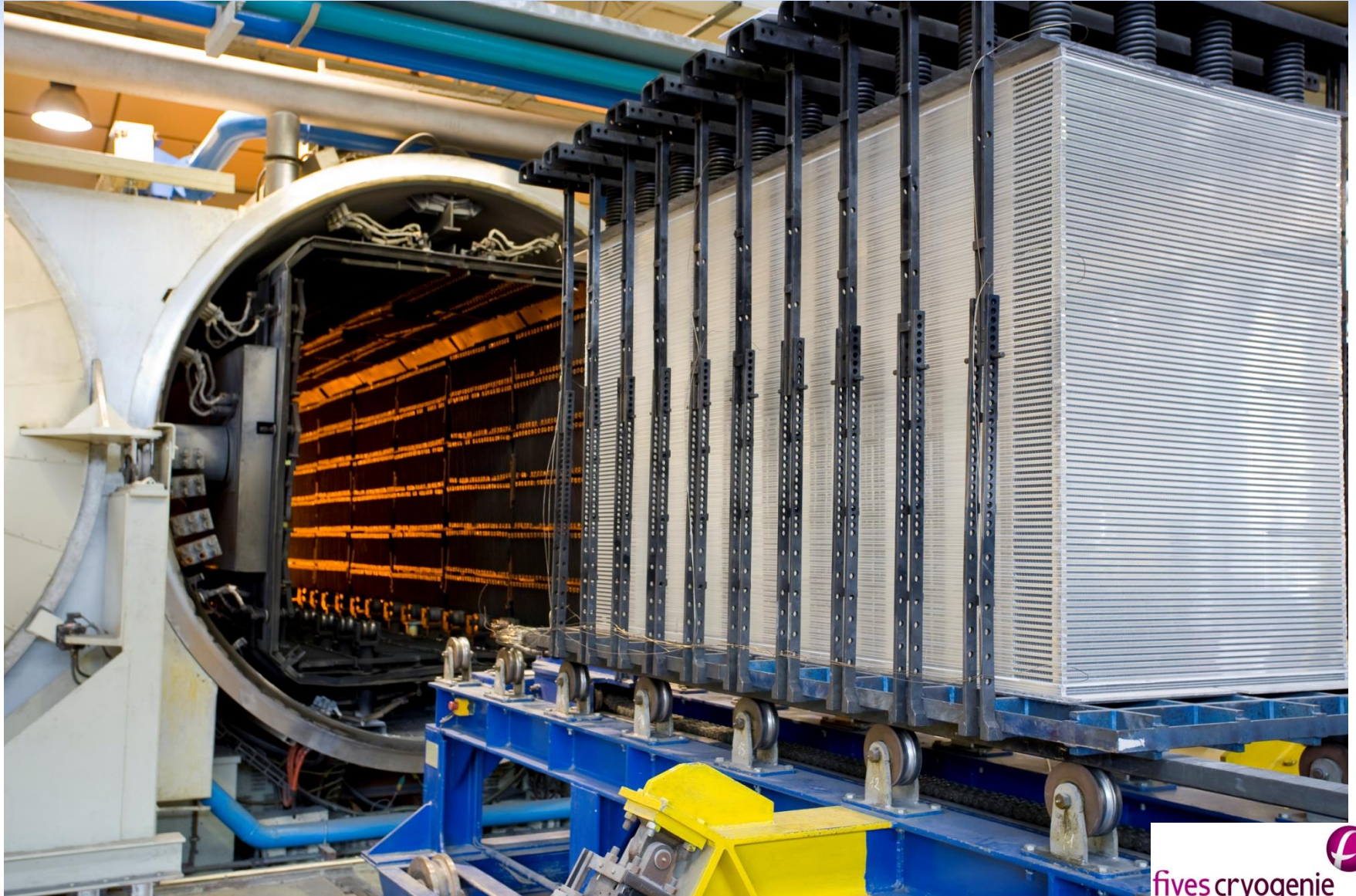
The core is inserted into a **vacuum** furnace heated at **620°C**.

The aluminium alloy/silicon melts at a temperature that is **20°C** lower than the aluminium alloy.

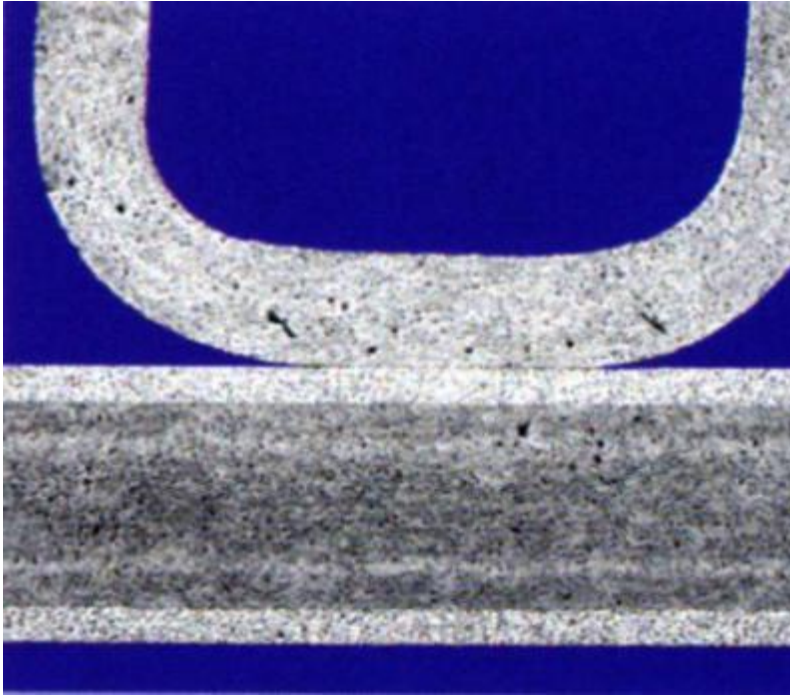
All contact points **braze** together to form a compact block.

The brazing process is **monitored** with thermocouples located inside the core to ensure an even temperature distribution.

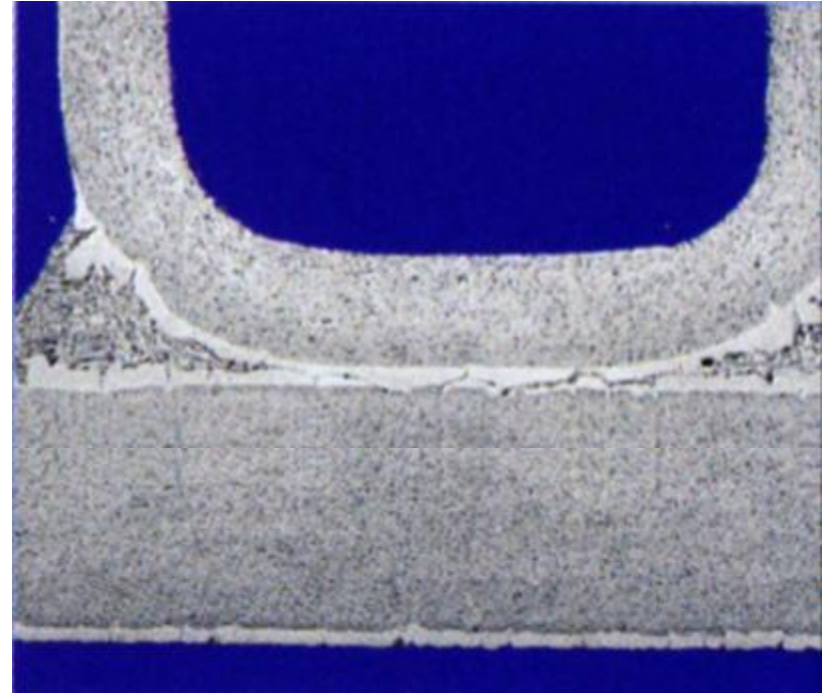
THE VACUUM FURNACE



BRAZING PROCESS



Before brazing



After brazing

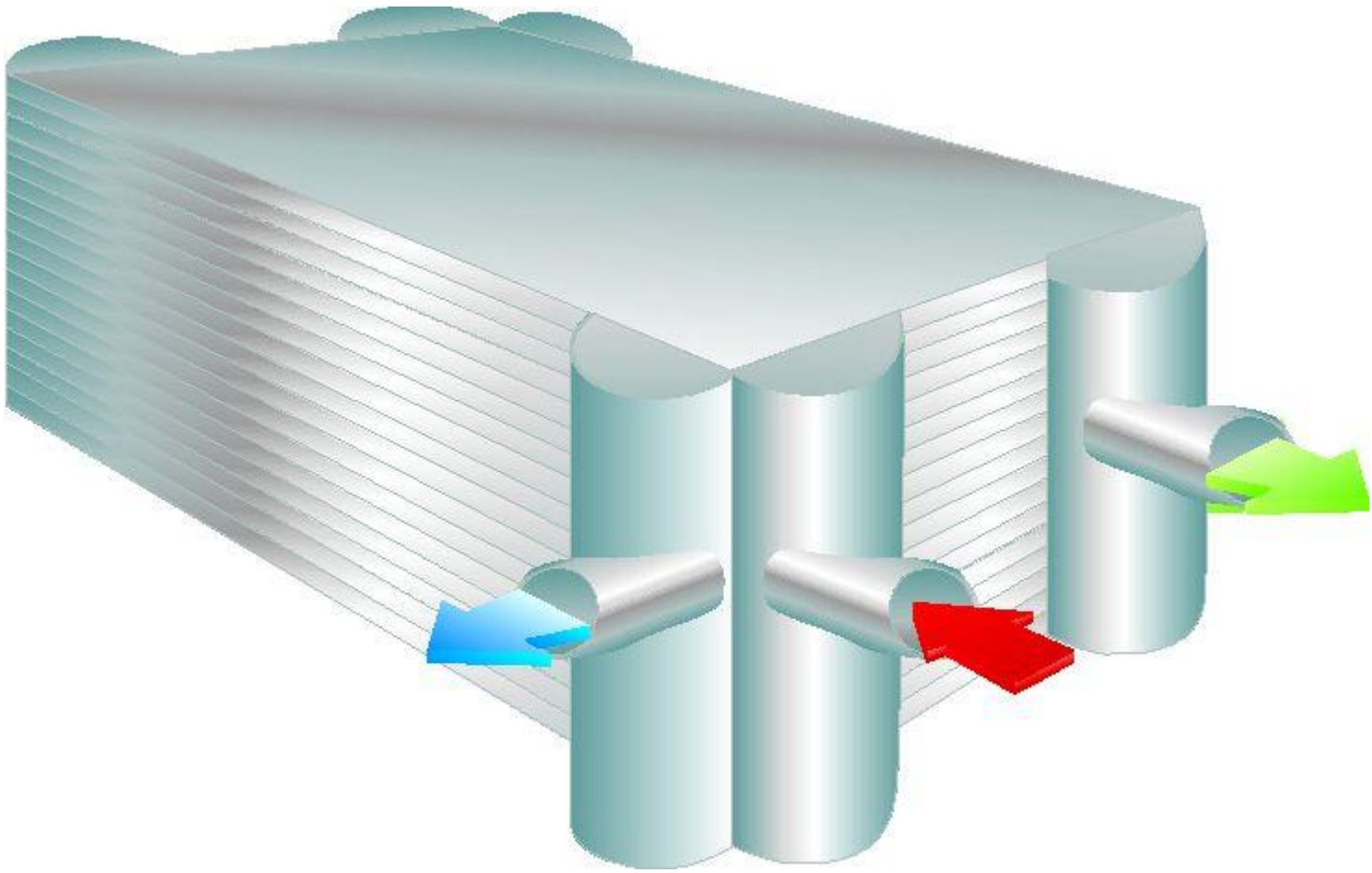
POST-BRAZING MANUFACTURING PROCESS

Welding of headers

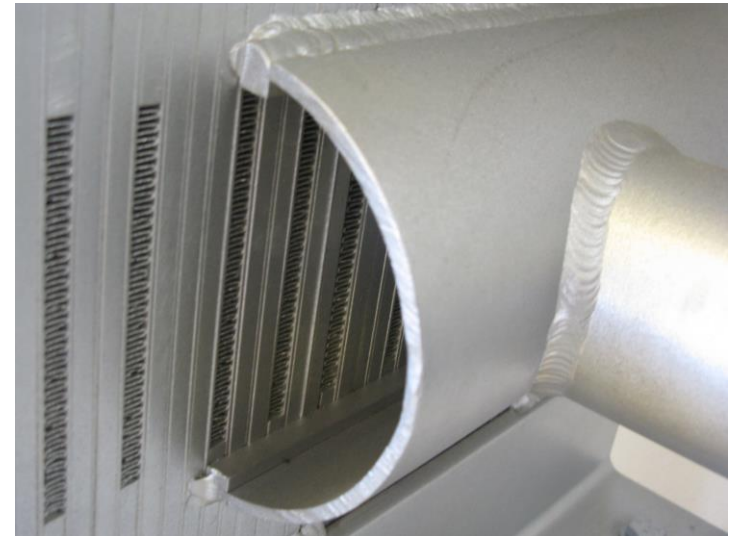
Hydraulic or Pneumatic Strength Test

Helium Leak Testing (Internal and External)

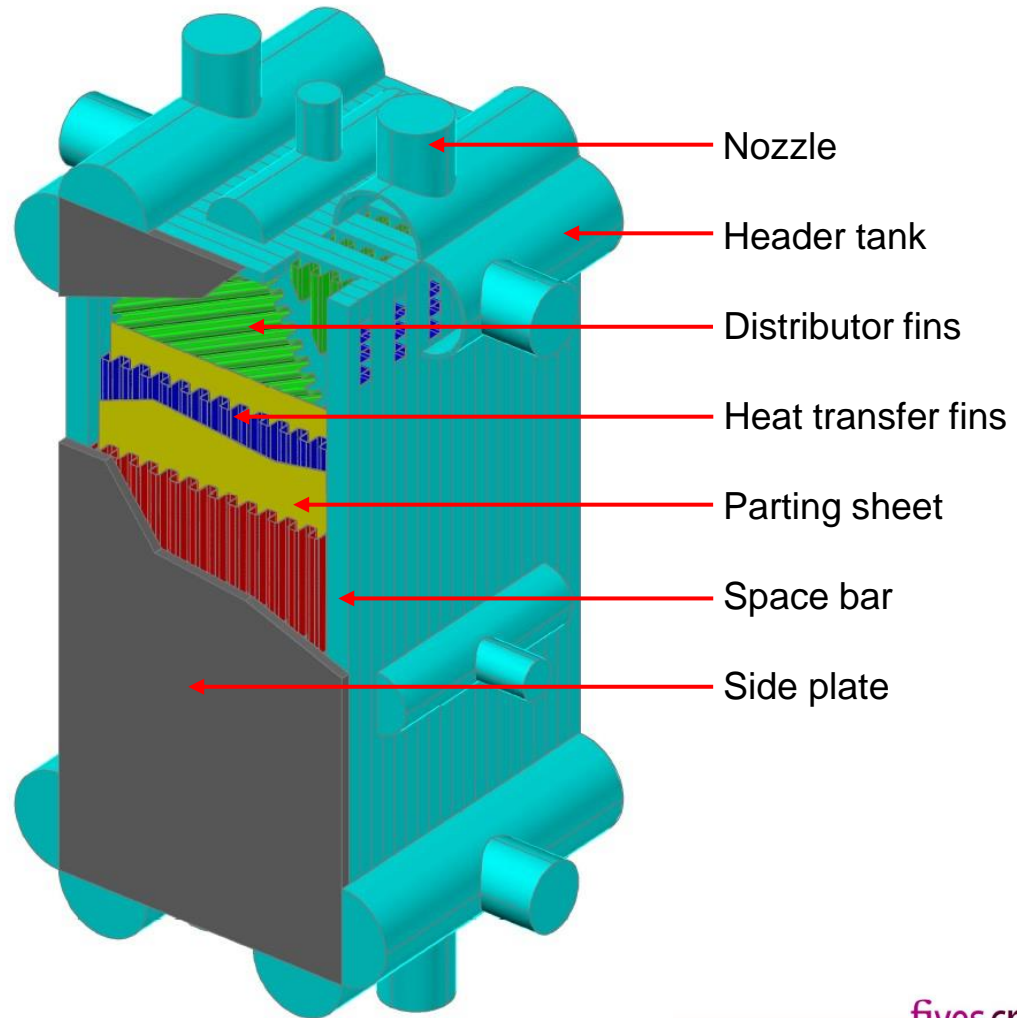
Welding of aluminium to stainless steel transition joints



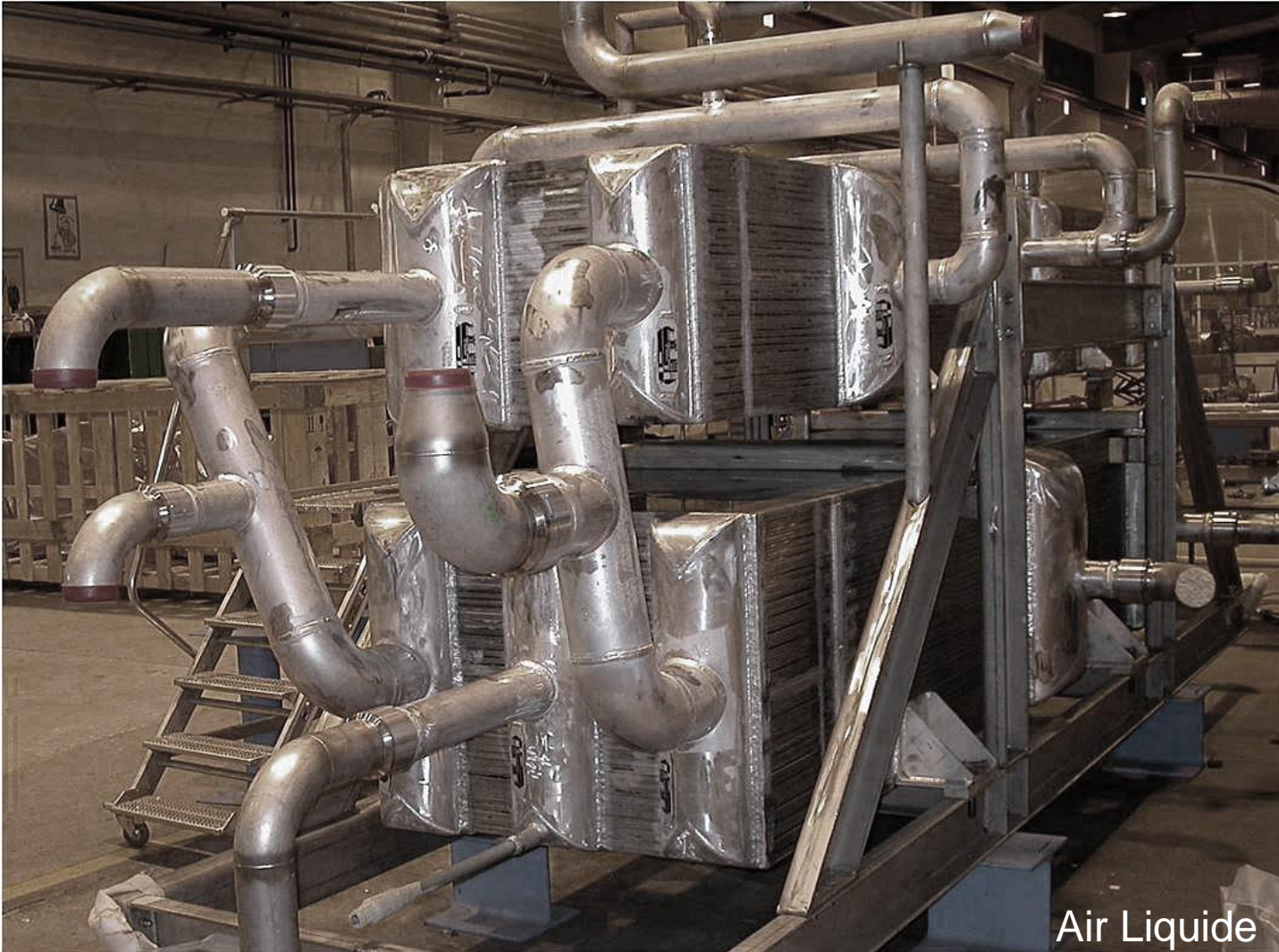
WELDING HEADERS



A HEAT EXCHANGER BLOCK



THE HEAT EXCHANGERS OF A LARGE HELIUM LIQUEFIER



Air Liquide

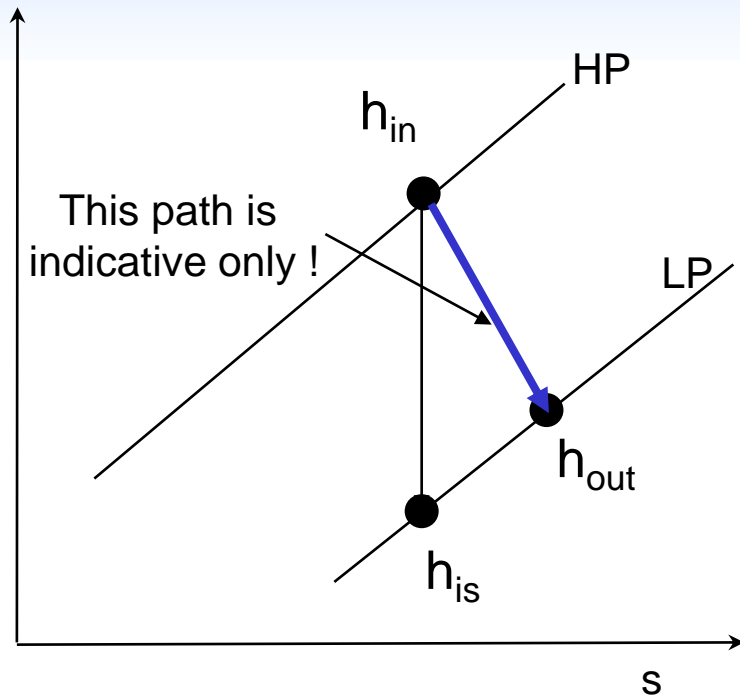
THE CRYOGENIC EXPANSION TURBINE

SPECIFICITIES OF A CRYOGENIC EXPANSION TURBINE

A cryogenic expansion turbine must be considered according to various issues :

- It must rotate at very high speeds (a few thousands rps),
- It is designed for **nominal** (or near to) operation, but it must also operate at **any temperature** between room temperature and the nominal operating temperature.
- It is sensitive to **impurities** that are diluted into the processed gas..

EXPANSION WITH EXTERNAL WORK



Isentropic effectiveness :

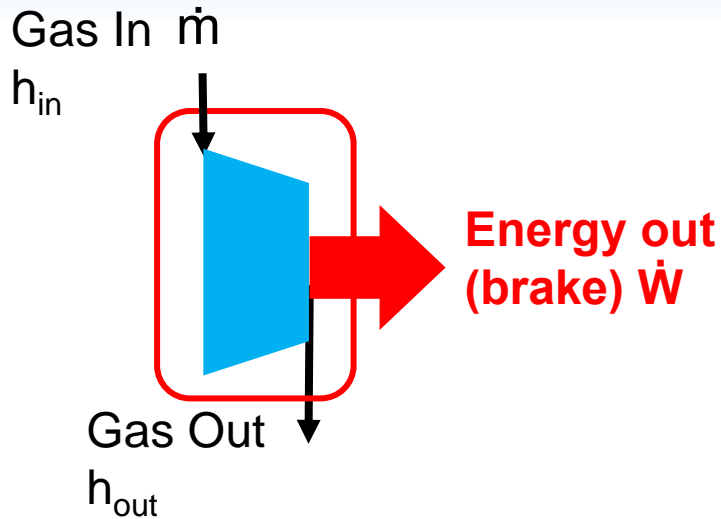
$$\eta_{is} = \frac{h_{in} - h_{out}}{h_{in} - h_{is}}$$

T-s CHART

AN EVERYDAY PRACTICAL TOOL

P (bar)	T (K)	h (J/g)	m (g/s)		Dh real (J/g)	Dh isent (J/g)
TURBINE						
11,00	25,00	142,0154	50,00			
0,75						
1,20	13,74	85,3601		-2832,77	-56,66	-75,54

ENERGY BALANCE



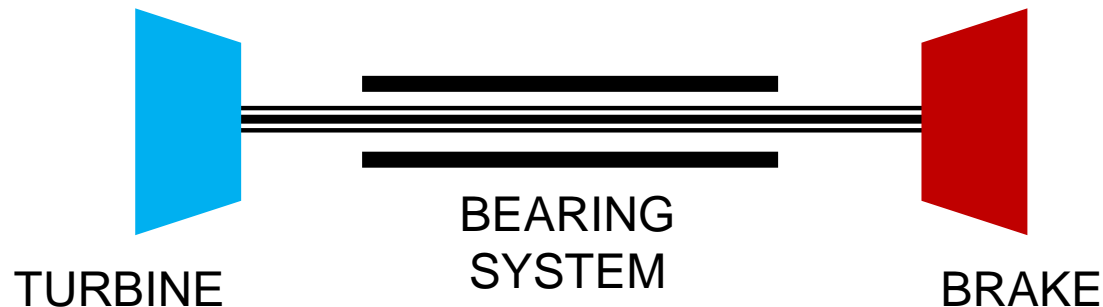
The refrigeration power of a turbine is the power that is **withdrawn from the processed gas**:

$$\dot{W} = \dot{m} \times (h_{in} - h_{out})$$

$$\dot{W} = \eta \times \dot{m} \times (h_{in} - h_{is})$$

Assuming no losses on the bearing system

GENERAL STRUCTURE

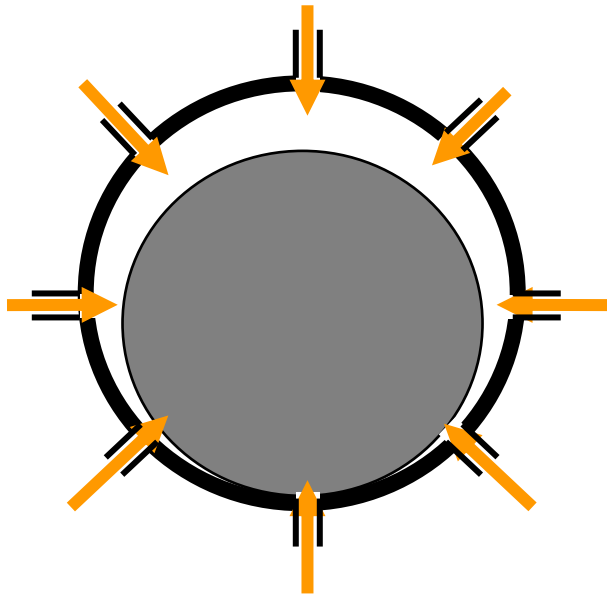


GAS BEARING SYSTEMS

Cryogenic expansion turbine rotate at very high speeds (up to 5000 rps)

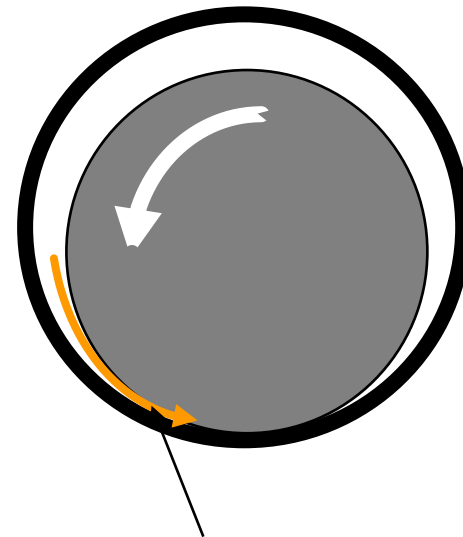
Any contact between shaft and bushing must be avoided !

STATIC



injection of helium

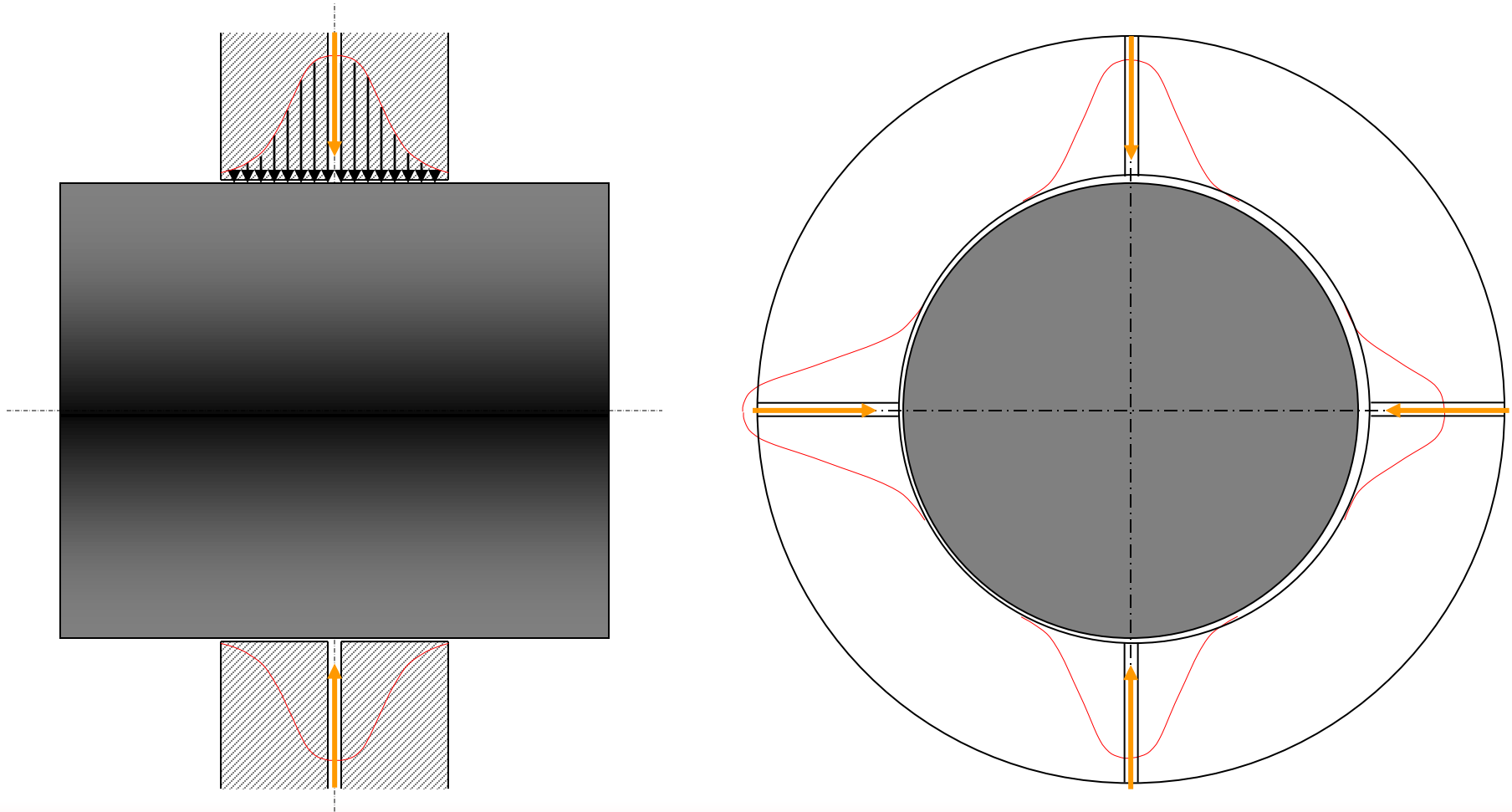
DYNAMIC



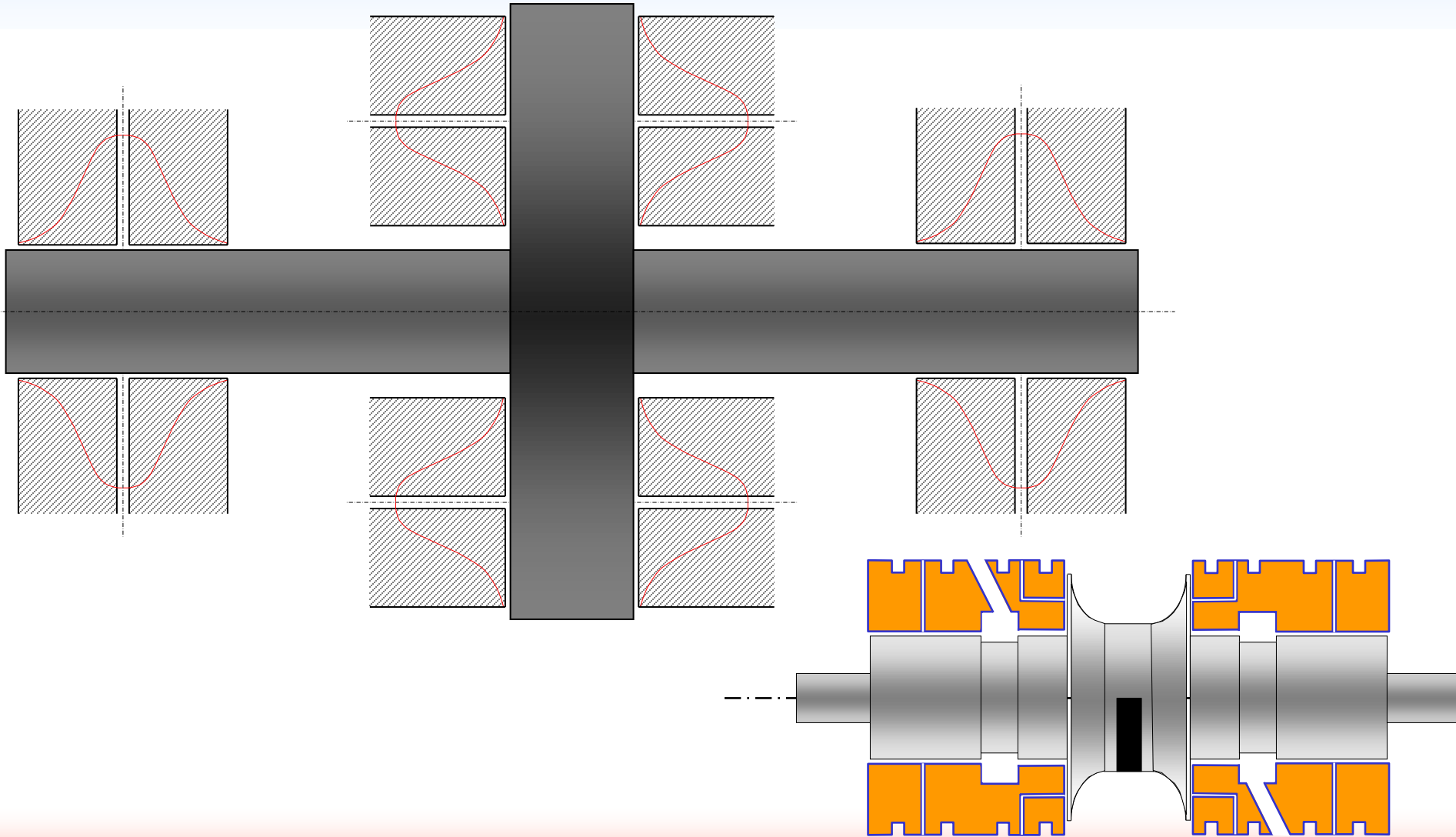
helium is pushed by viscosity

STATIC GAS BEARING

JOURNAL



STATIC GAS BEARING



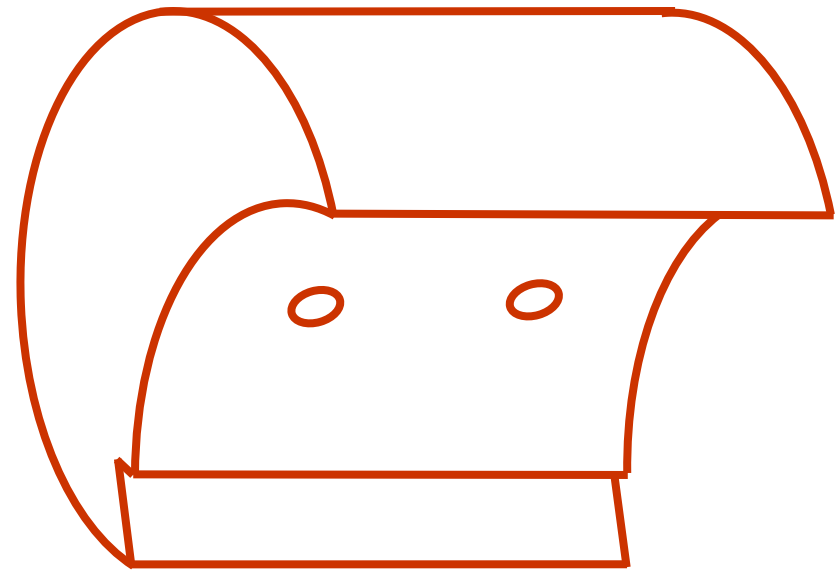
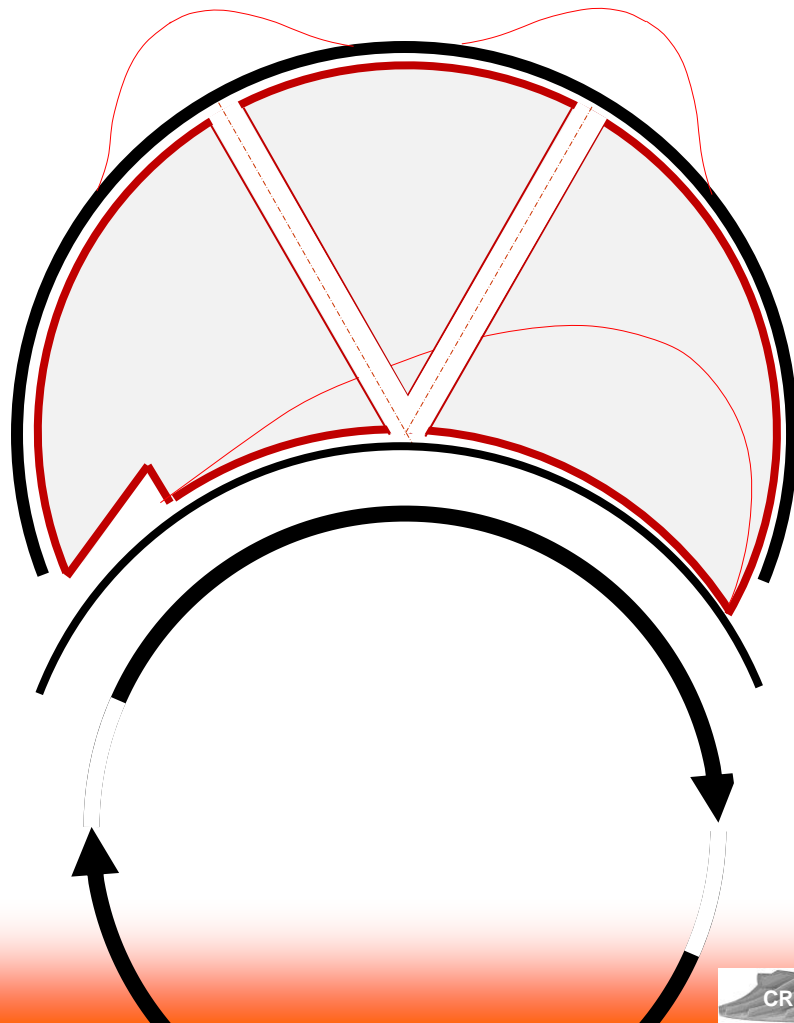
A STATIC GAS BEARING SYSTEM

SHAFT AND BEARING



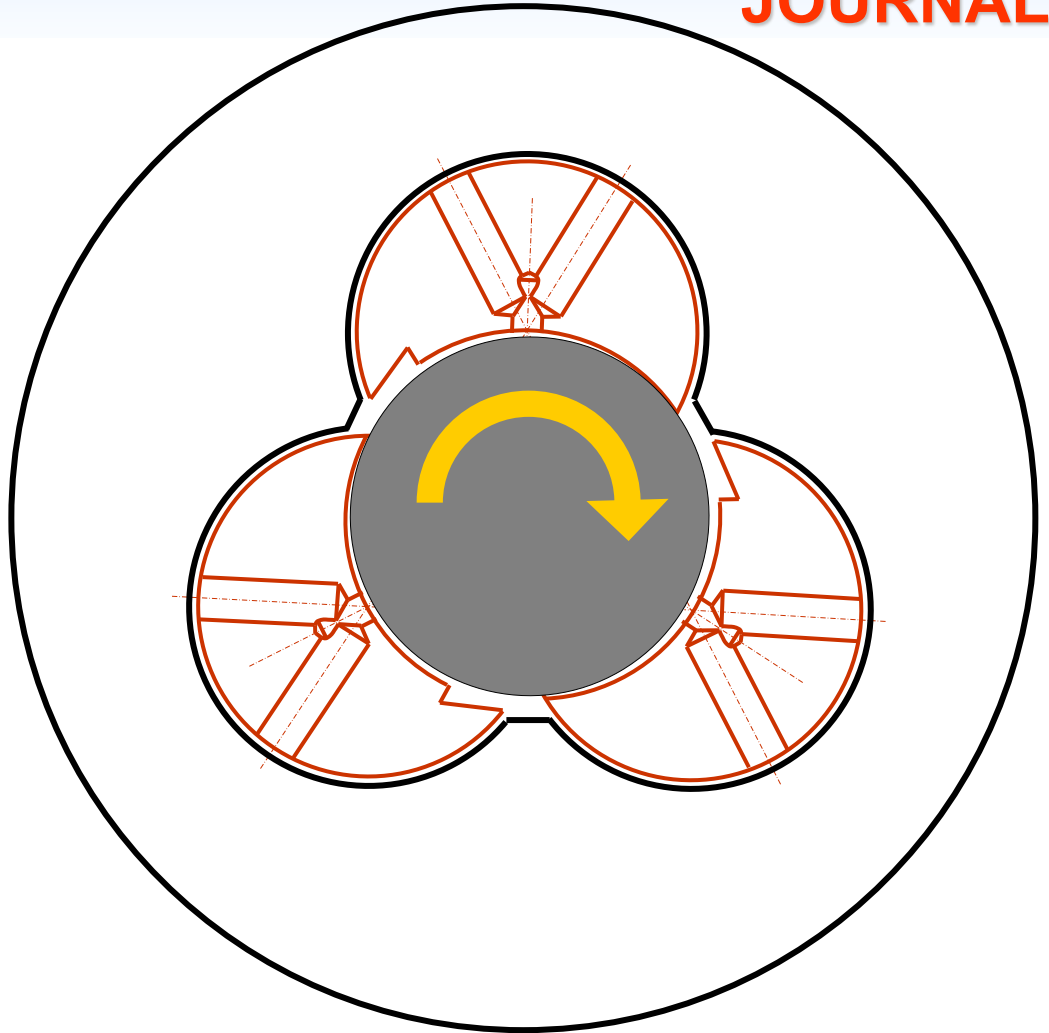
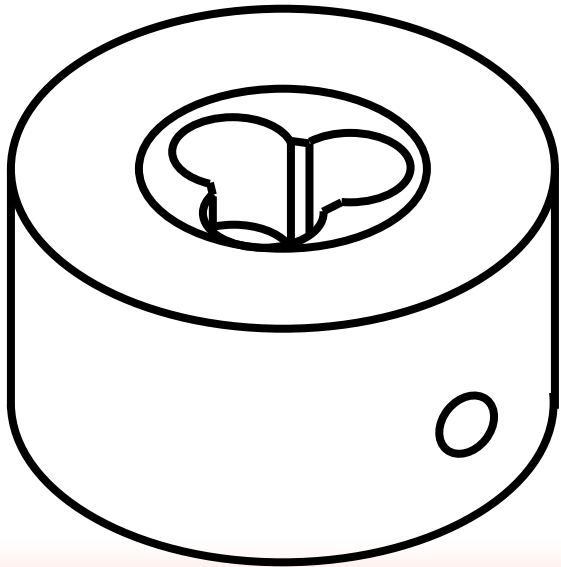
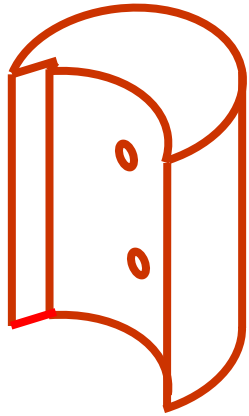
A DYNAMIC GAS BEARING SYSTEM

JOURNAL



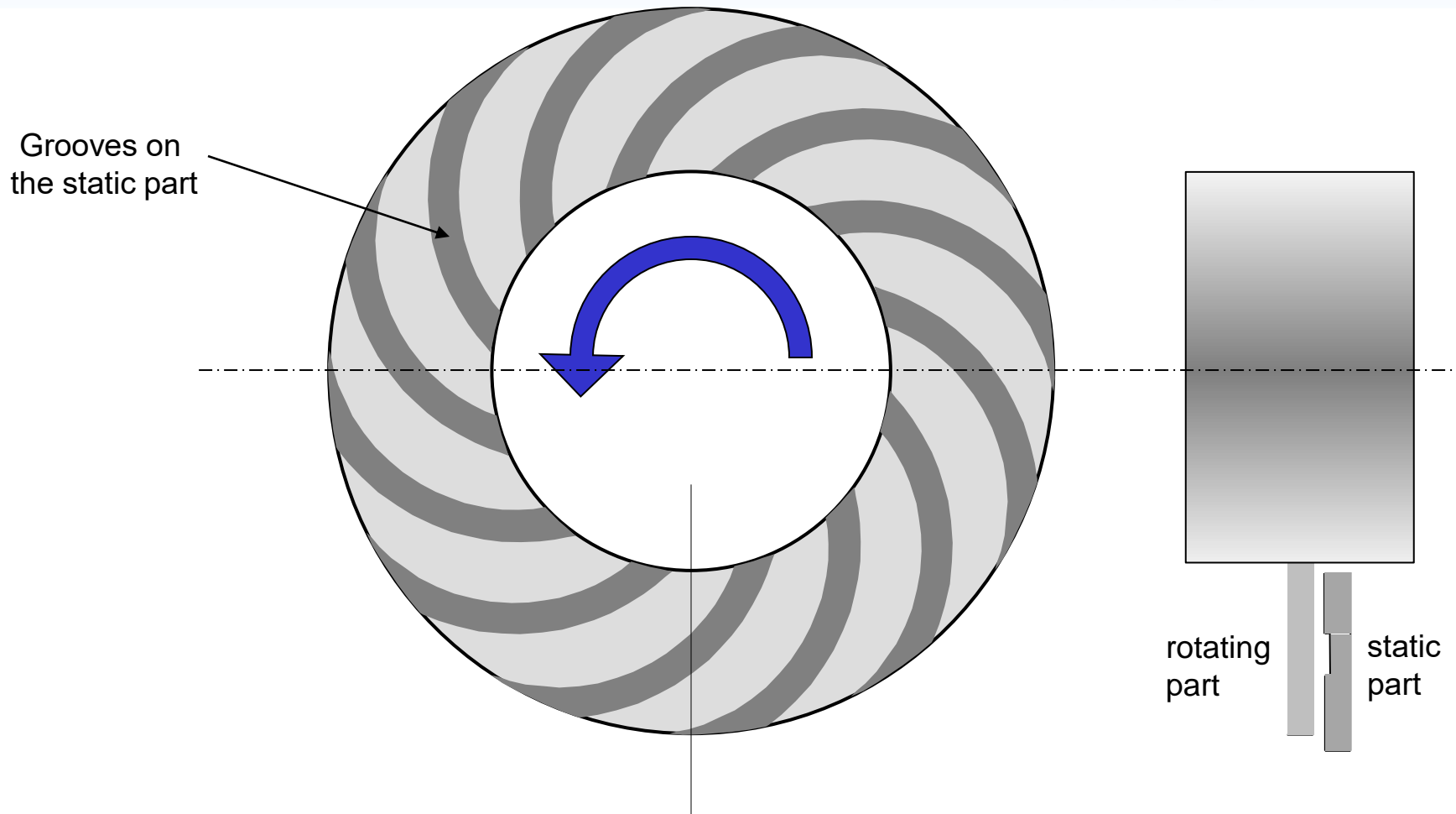
A DYNAMIC GAS BEARING SYSTEM

JOURNAL

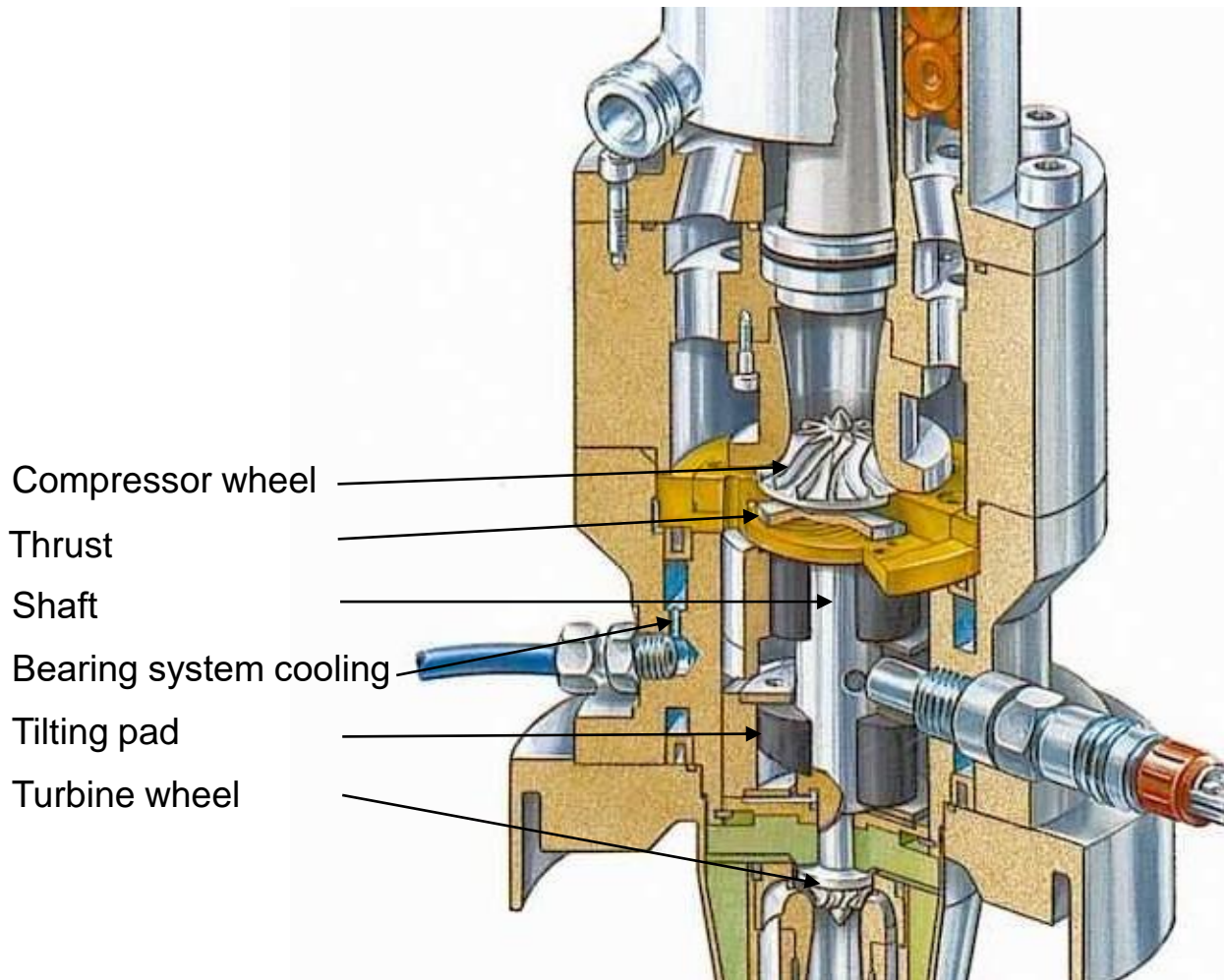


A DYNAMIC GAS BEARING SYSTEM

THRUST



A LINDE DYNAMIC GAS BEARING SYSTEM



TURBINE OPERATING PRINCIPLE

1st step

Conversion of most of the energy of pressure into kinetic energy:

Distributor duty

2nd step

Conversion of most of the kinetic energy into mechanical energy:

Wheel duty

3rd step

Conversion of the remaining kinetic energy into pressure:

Diffuser duty

THE DISTRIBUTOR DUTY

The distributor is a **fixed nozzle**.

1. Energy conservation:
enthalpy is converted into **kinetic energy**.

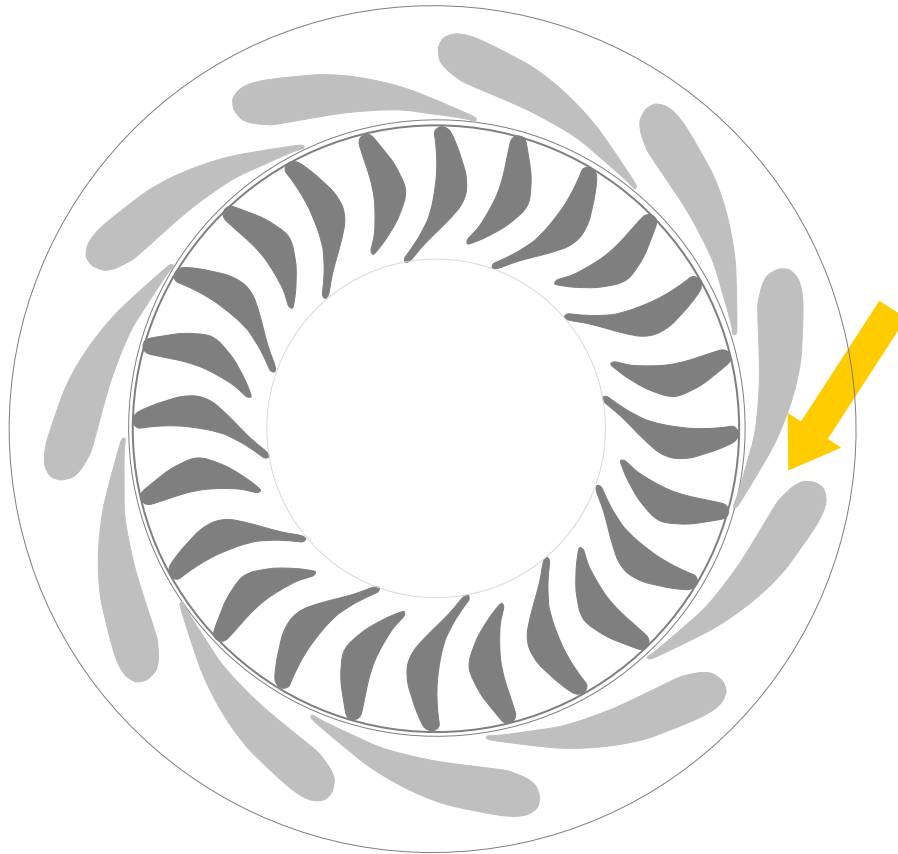
$$\Delta h_{\text{dist}} = \frac{1}{2} (C_{\text{dis}}^2 - C_{\text{in}}^2)$$

Part of expansion **and cooling** is done in the distributor.

2. Right **orientation** of the gas velocity
in order to enter correctly into the wheel.

3. **Calibration** of the gas flow by the cross section.

THE DISTRIBUTOR DUTY



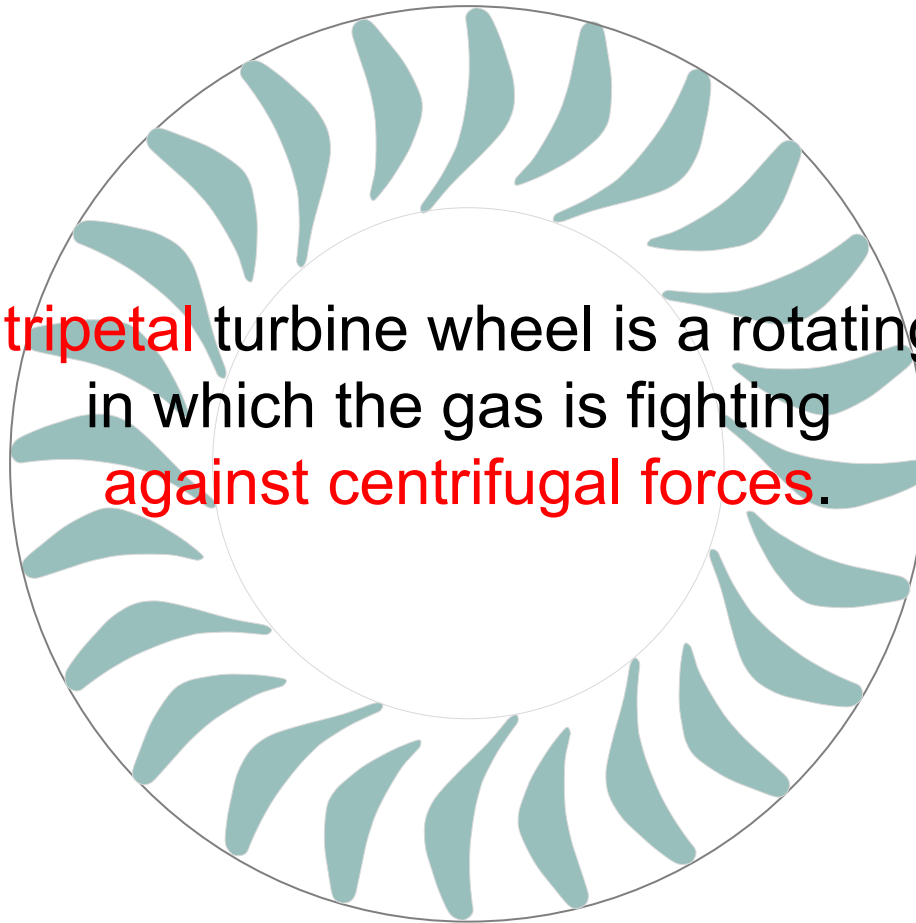
The cross section in which helium flows **reduces** in order to **increase the velocity**.

The distributor gives also a **correct orientation** of the gas velocity.

The cross section in which helium flows **calibrates the gas flow**.

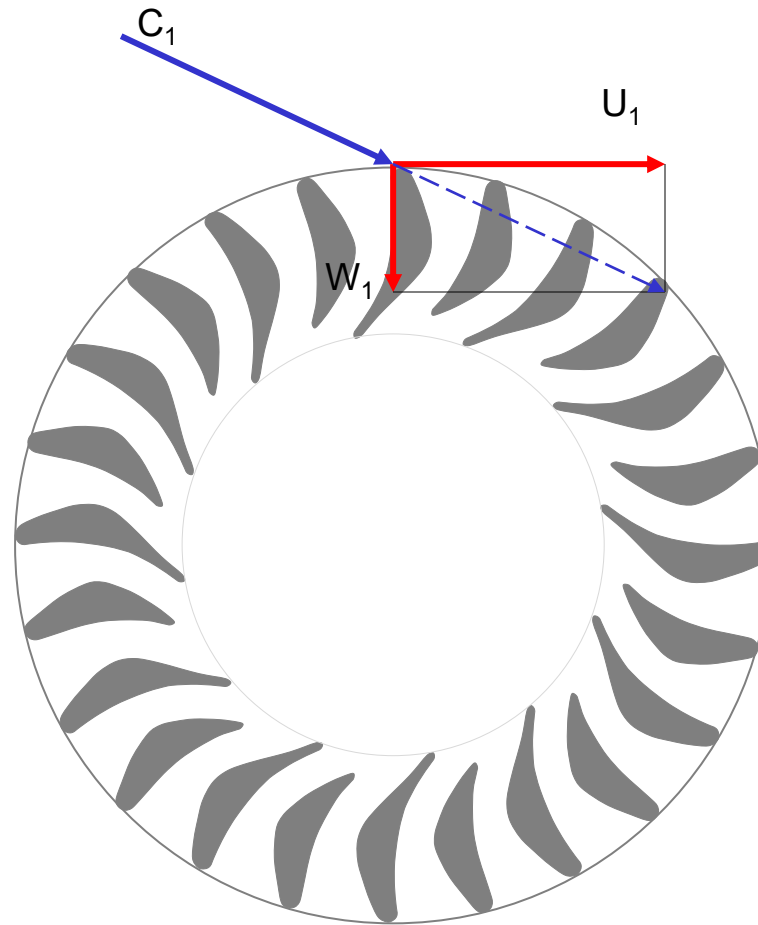
THE TURBINE WHEEL

The **centripetal** turbine wheel is a rotating nozzle in which the gas is fighting **against centrifugal forces**.

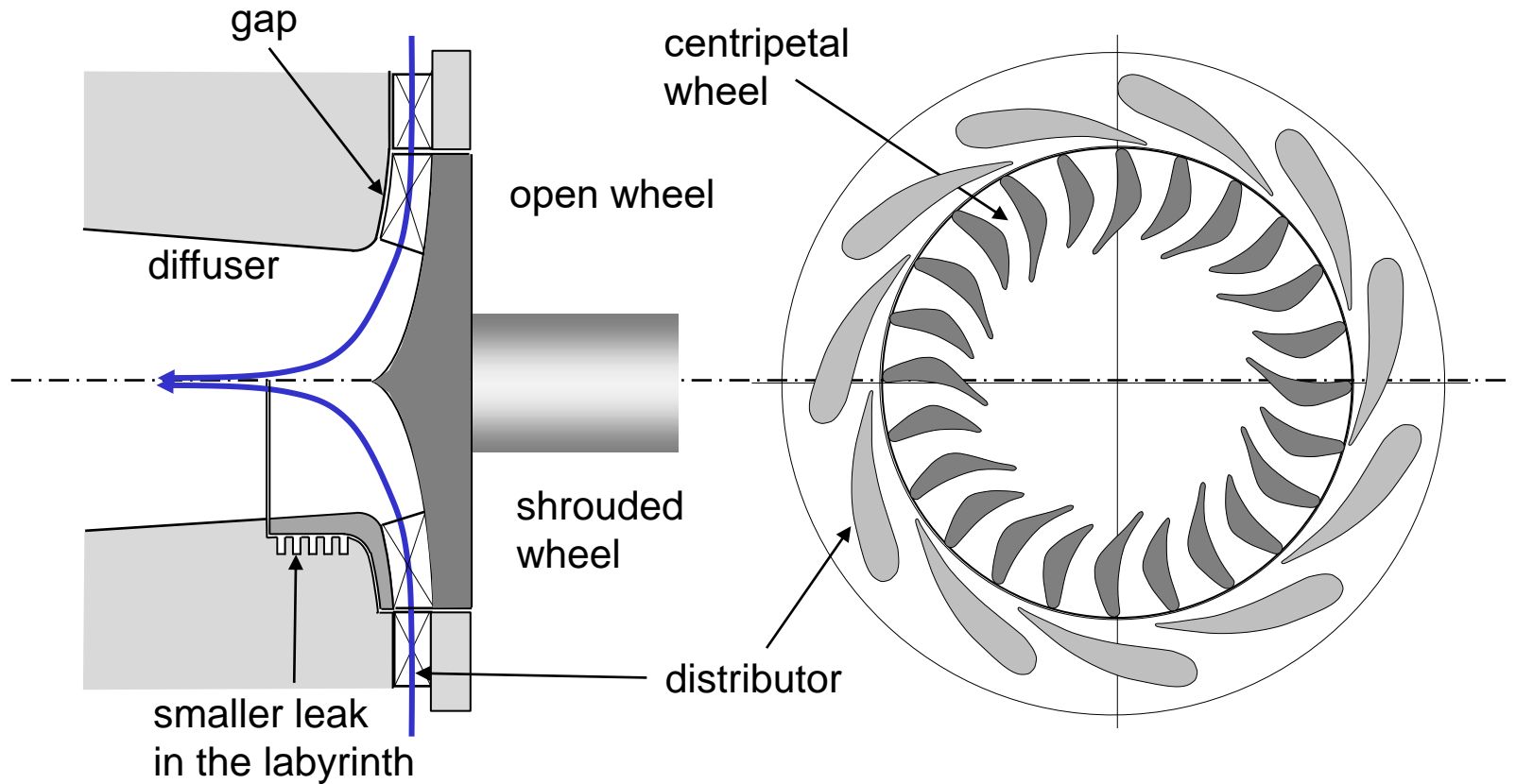


VELOCITY COMPOSITION

RADIAL INLET



TYPES OF WHEELS



SOME TURBINE WHEELS...

radial wheels



radial-axial wheel



radial
shrouded
wheel



THE DIFFUSER

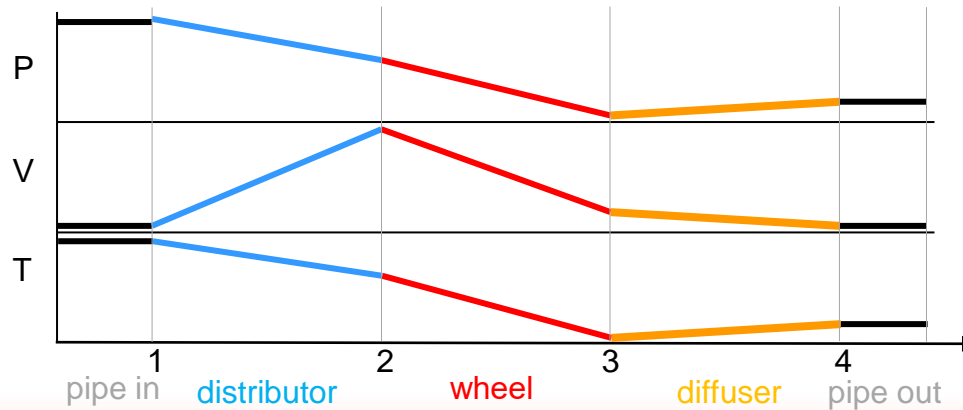
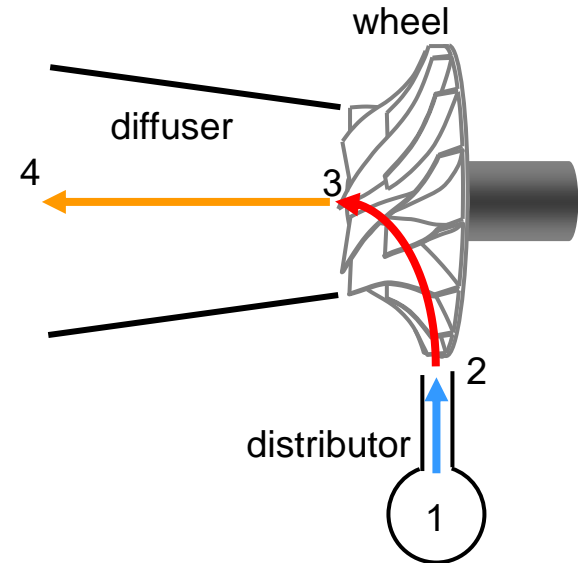
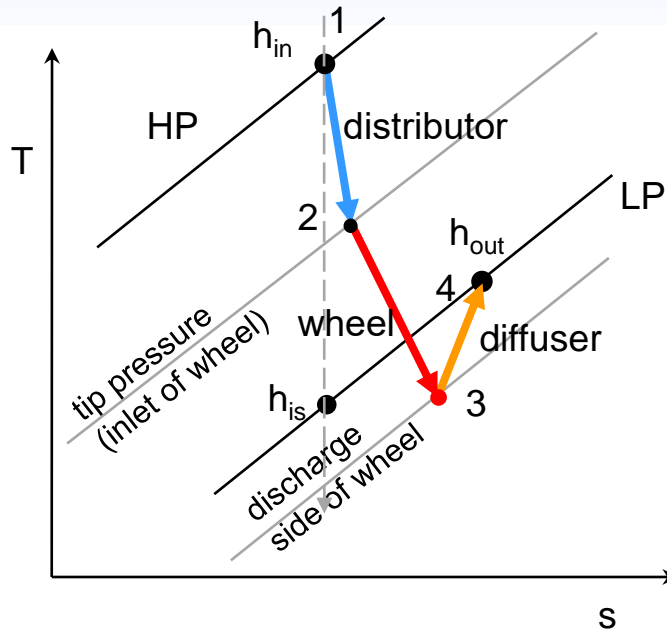
When the gas exits the wheel, its velocity is not zero.

The velocity has to be reduced.

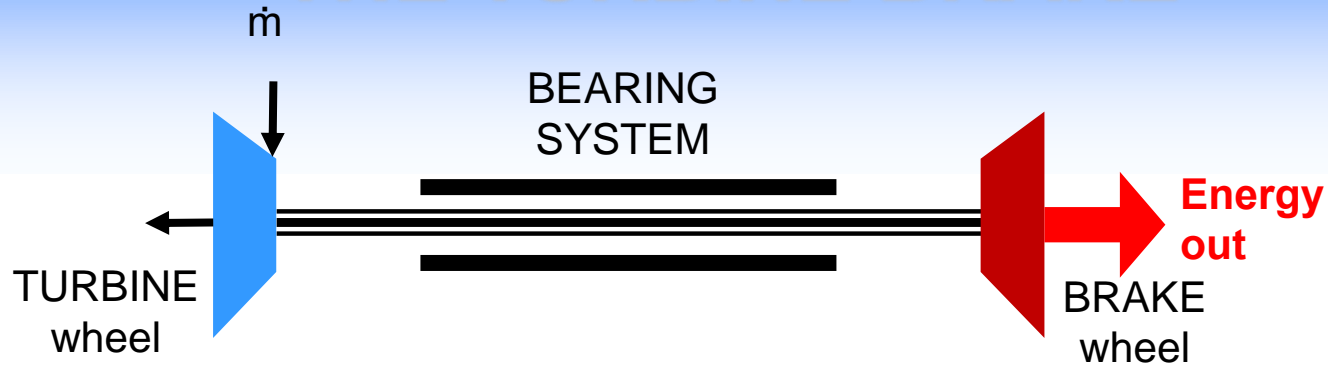
This is done by means of another nozzle : the **diffuser**.

As a consequence, both **pressure** and **temperature** **increase slightly**.

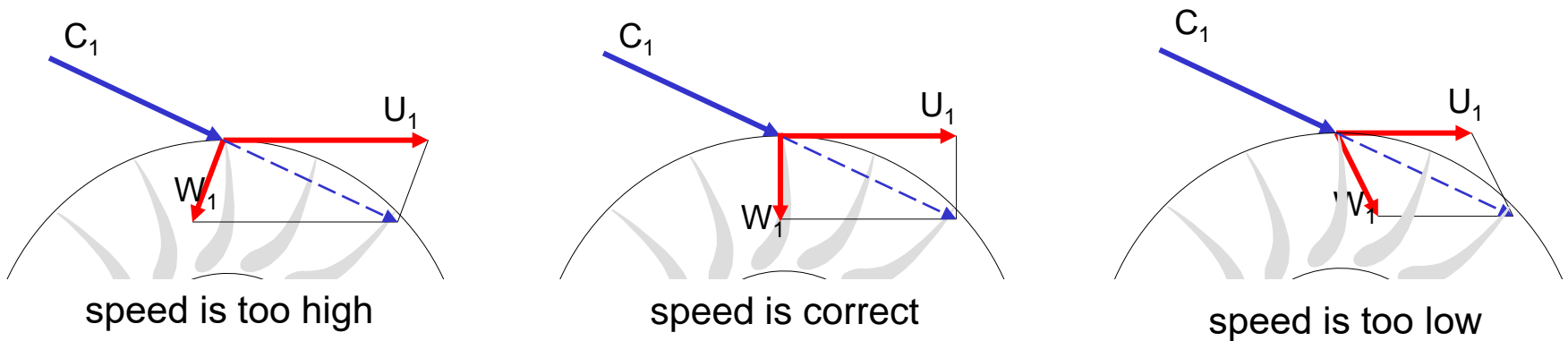
EVOLUTION OF GAS THROUGH THE TURBINE



THE TURBINE BRAKE



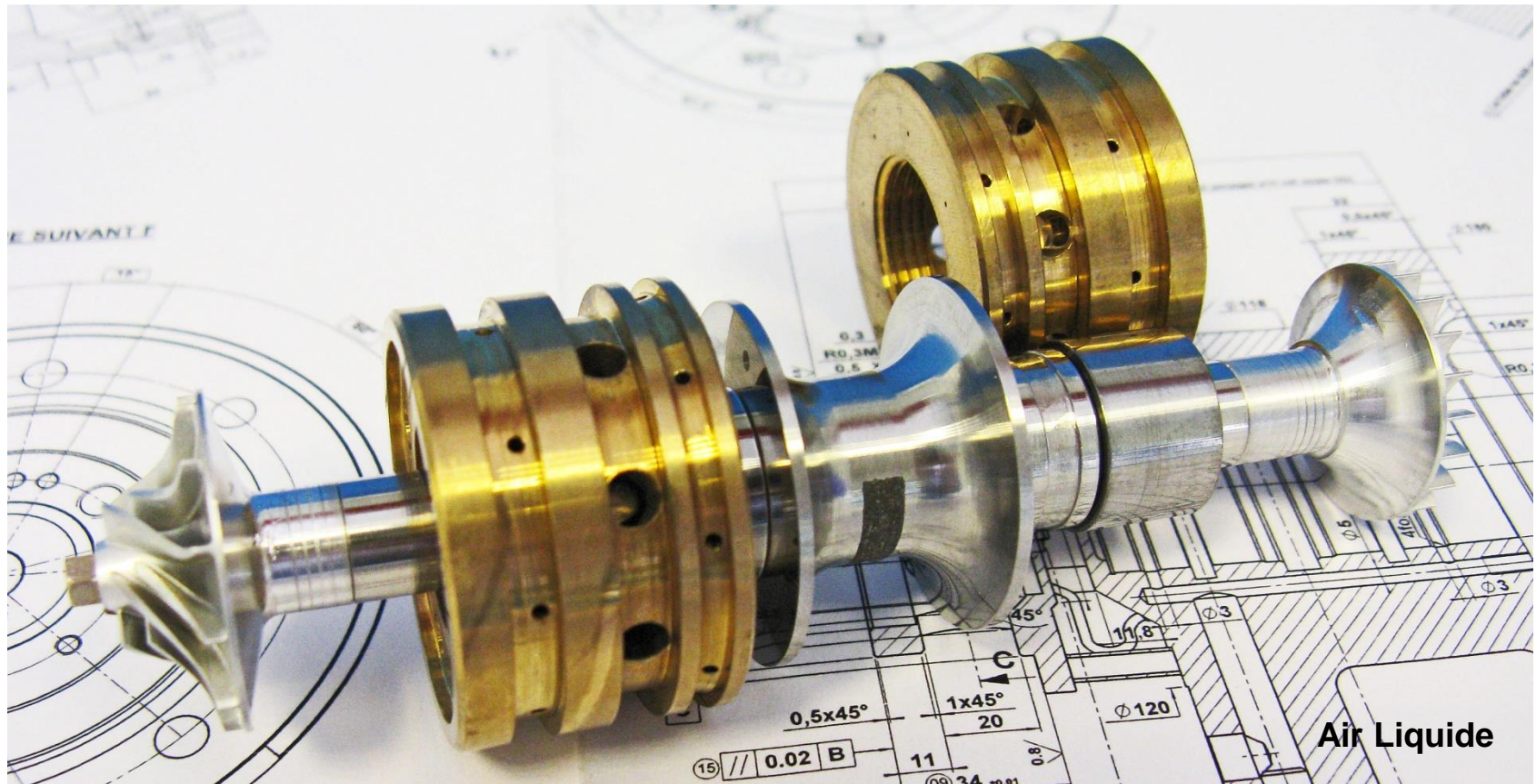
The brake dissipates the power that is extracted by the wheel, but it must fulfil this duty **at the correct rotational speed !**



The main brake technologies are :

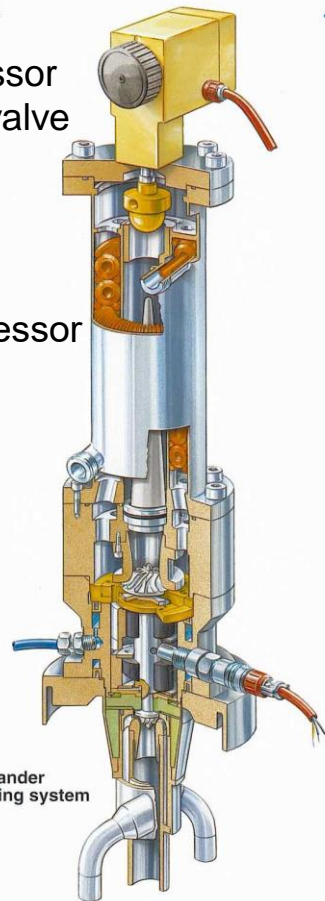
- a centrifugal compressor (most common)
- an eddy current system (for small powers).

SHAFT, BEARINGS AND WHEELS



STRUCTURE OF A TURBINE

A LINDE TURBINE



LINDE KRYOTECHNIK AG
Brake
compressor
control valve

Linde

Brake
compressor
cooler

Cryogenic turboexpander
Self-acting gas bearing system

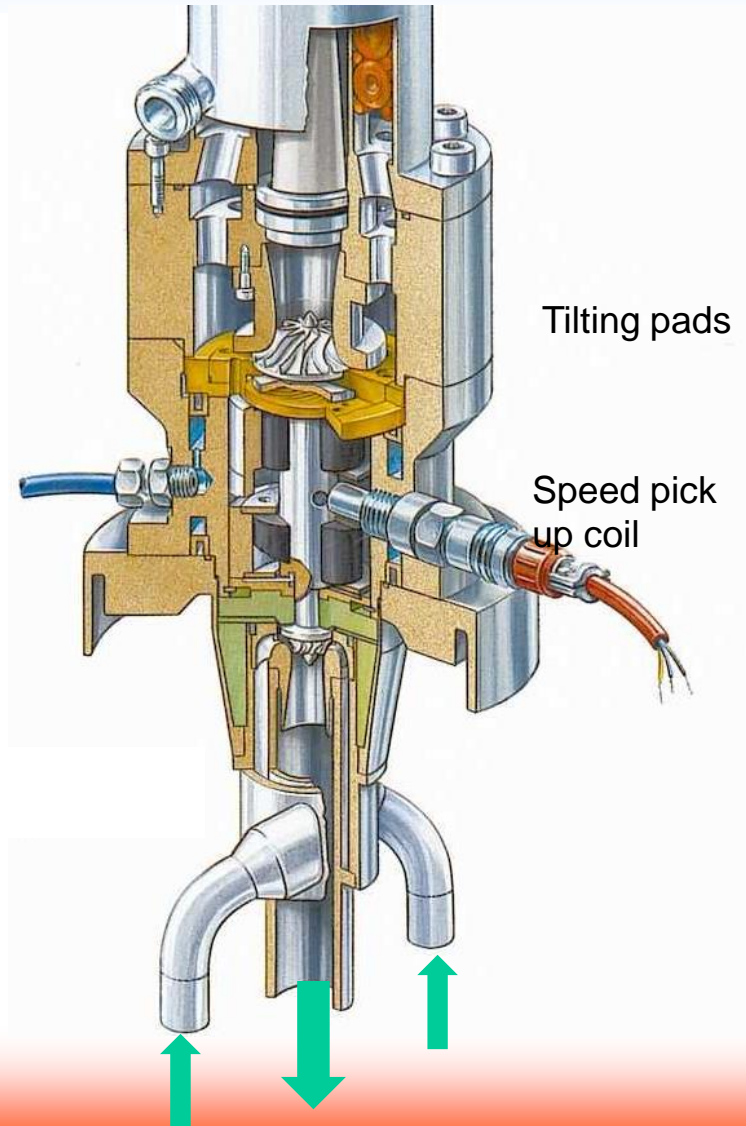
Dynamic gas bearings

Non constant brake compressor pressure

Compressor
wheel

Bearing
cooling
water

Turbine
wheel



Tilting pads

Speed pick
up coil