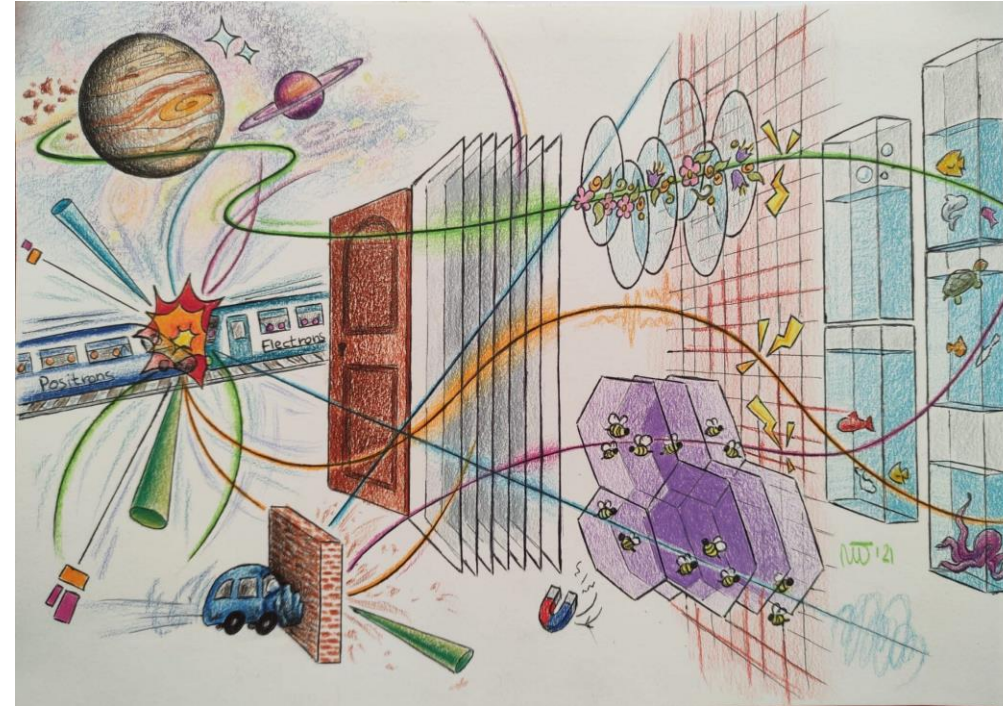


# Tracking particle in space and time

## New trends in silicon sensors design



**N. Cartiglia**  
**INFN Torino,**

# Silicon life in 2010

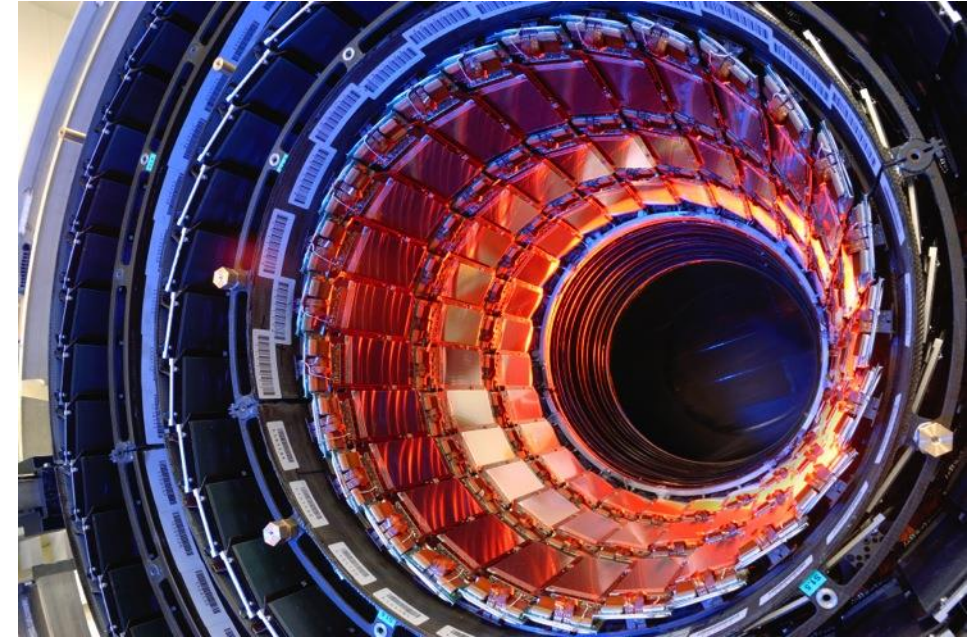
## Very mature silicon systems, very large silicon trackers

Millions of channels, very reliable, very radiation hard

### Two simple facts in 2010:

1. Silicon sensors are not suitable timing detectors
2. Silicon sensors cannot be used efficiently to detect 1-5 keV XRay

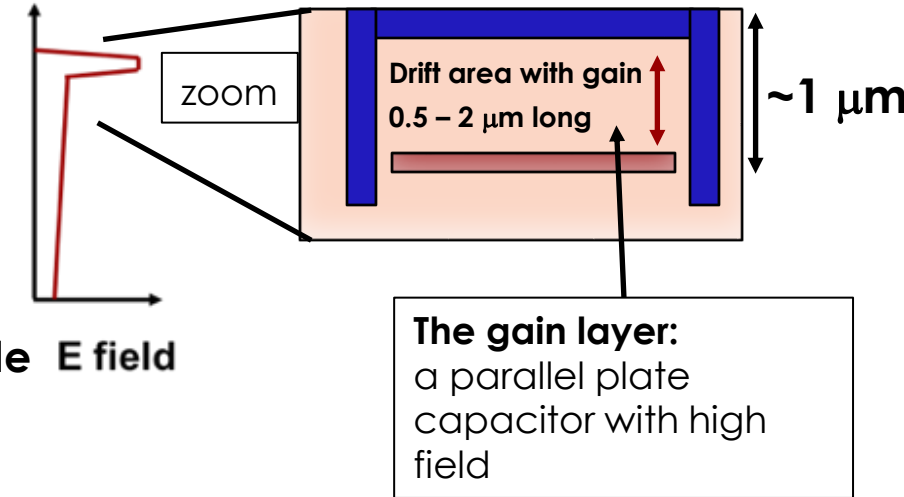
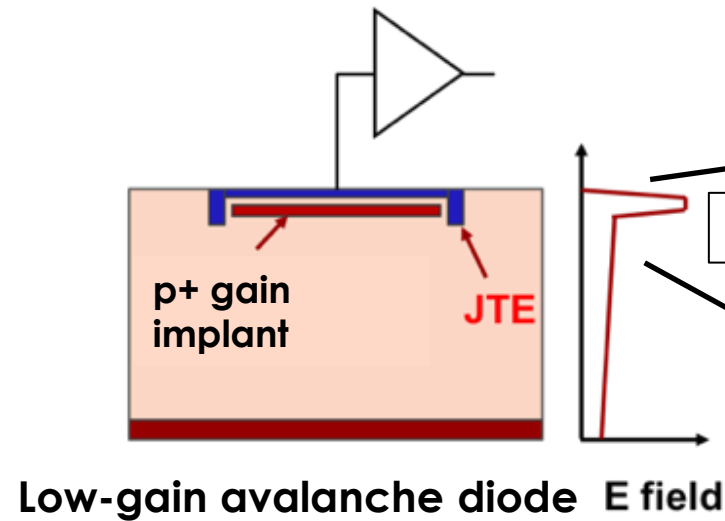
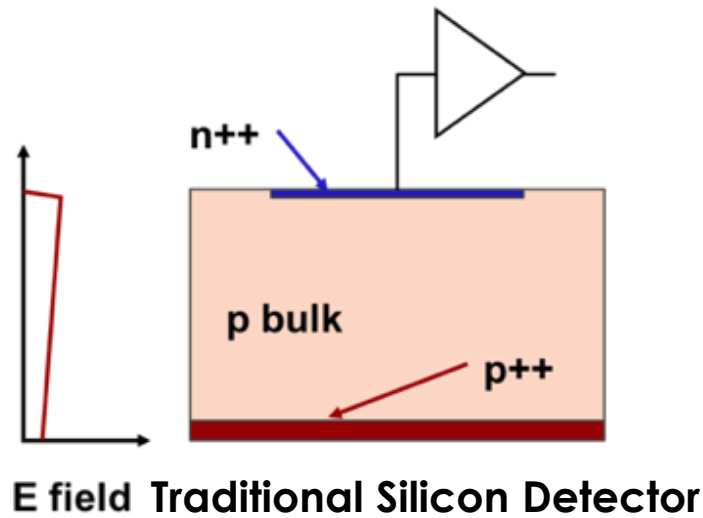
**One nagging problem:** radiation damage causes charge trapping, reducing the signal in heavily irradiated sensors.



**Solution:** add moderate gain, just enough to compensate for charge trapping  
“to control and optimize the charge multiplication effect, **in order to fully recover the collection efficiency of heavily irradiated silicon detectors**” [1]

[1] G.Pellegrini,et al., **Technology developments and first measurements of Low Gain Avalanche Detectors (LGAD) for high energy physics applications**, Nucl. Inst. Meth. A 765 (2014) 12.

# First design innovation: low gain avalanche diode (LGAD)

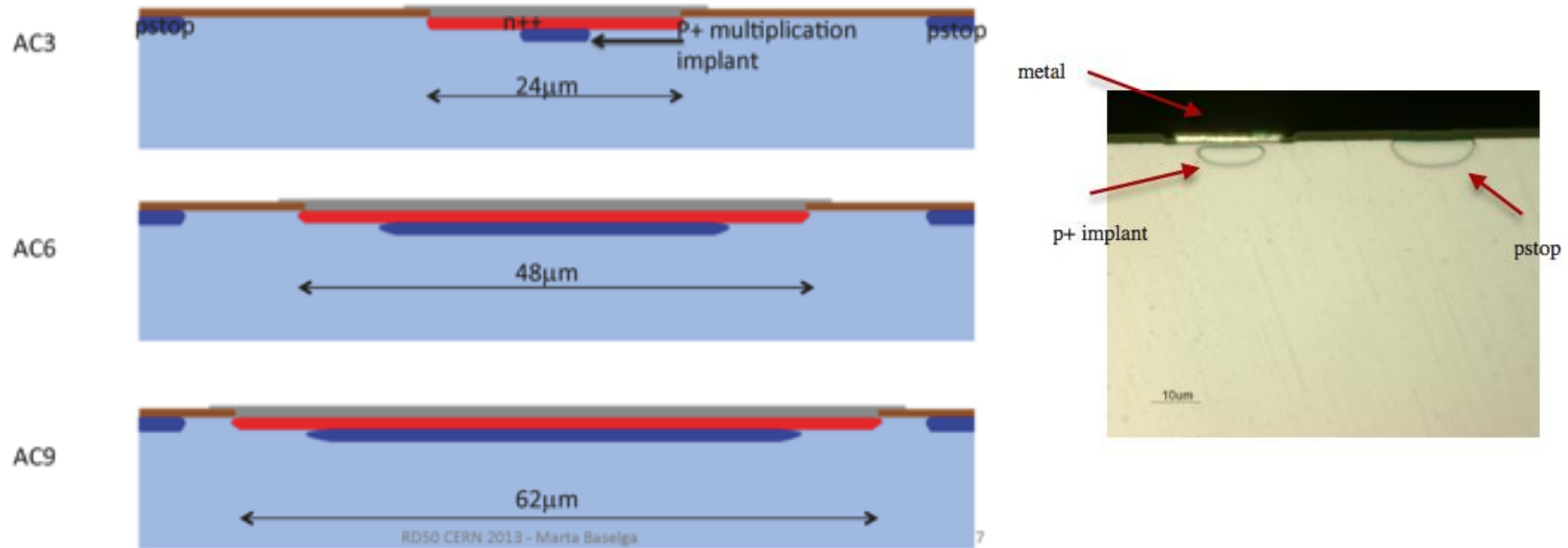


- In LGAD, a moderately p-doped implant creates a volume of high field, where charge multiplication happens.
- **This “extra charge” was supposed to compensate for charge trapping in irradiated silicon sensors**

# LGADs Pads, Pixels and Strips

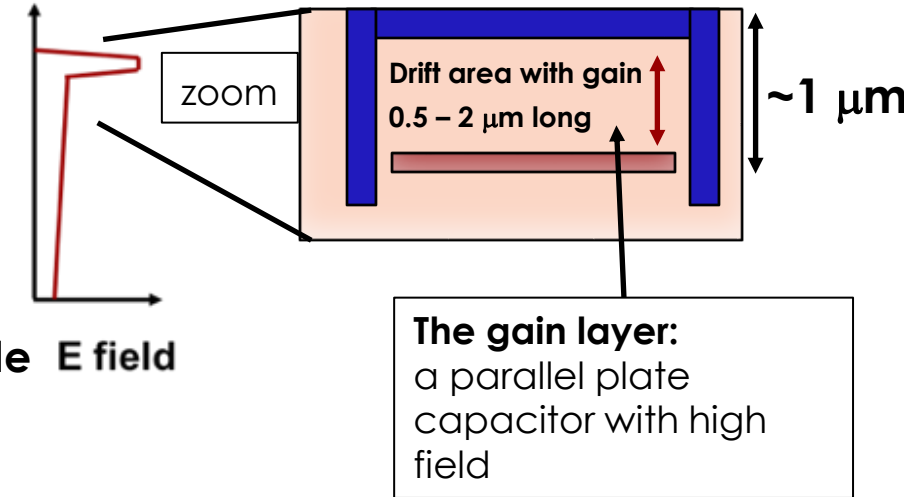
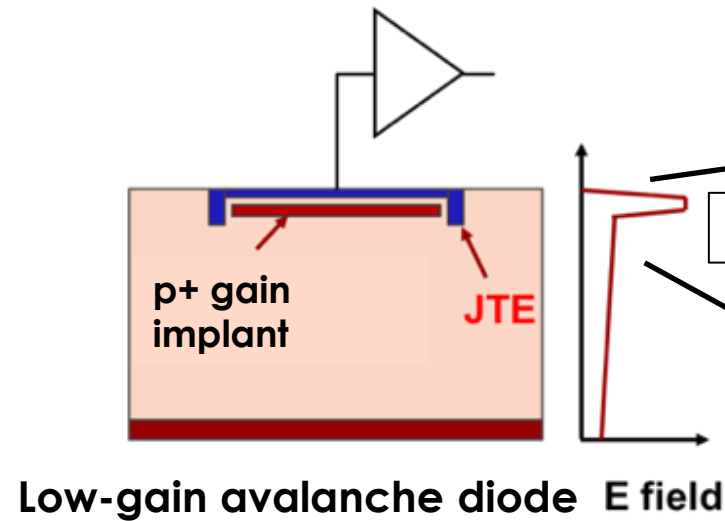
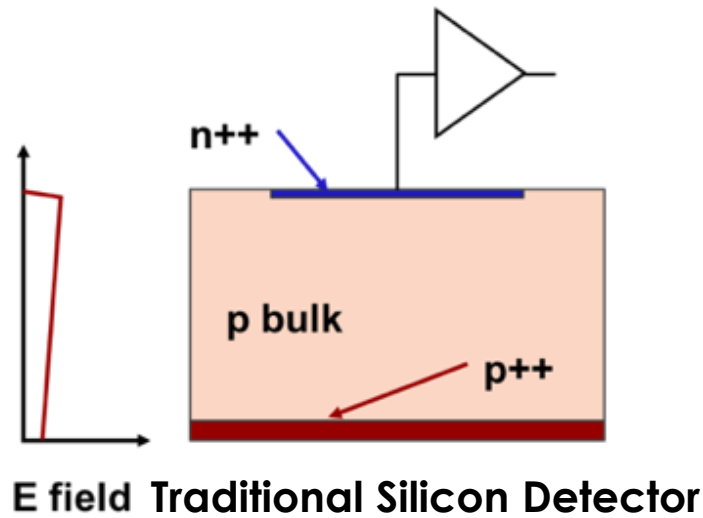
The LGAD approach can be used in any silicon structure,

This is an example of LGAD strips



**LGAD strips are considered in space application, as they allow to have longer strips while keeping constant the ratio Charge/Capacitance**

# First design innovation: low gain avalanche diode (LGAD)



- It turned out that the LGAD design does not solve the charge-trapping problem as the LGAD mechanism does not work well in high radiation environments (above  $2\text{-}3\text{E}15$  1-MeV  $n_{eq}/\text{cm}^2$ )

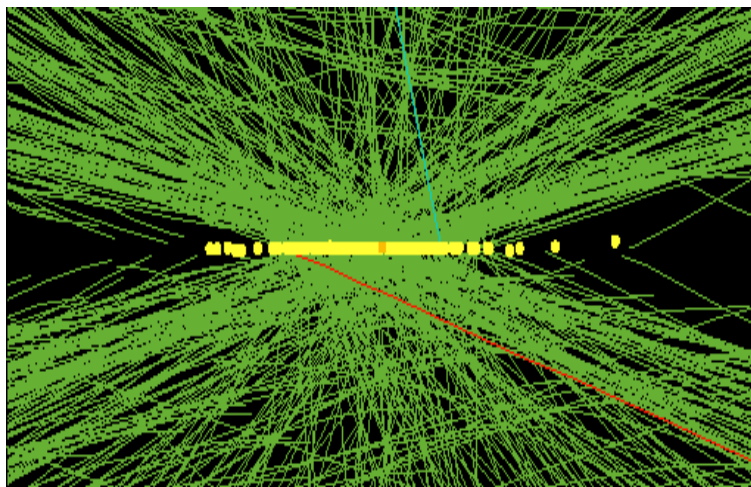
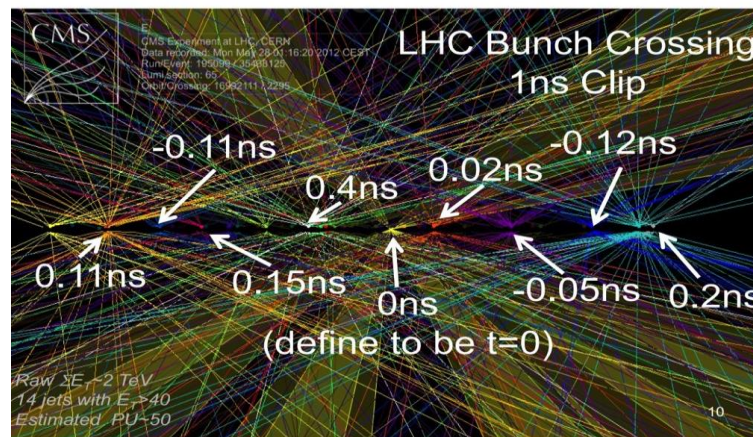
In the meantime, other challenges were becoming important....

# Scattering density in the HL-LHC upgrade



## LHC situation:

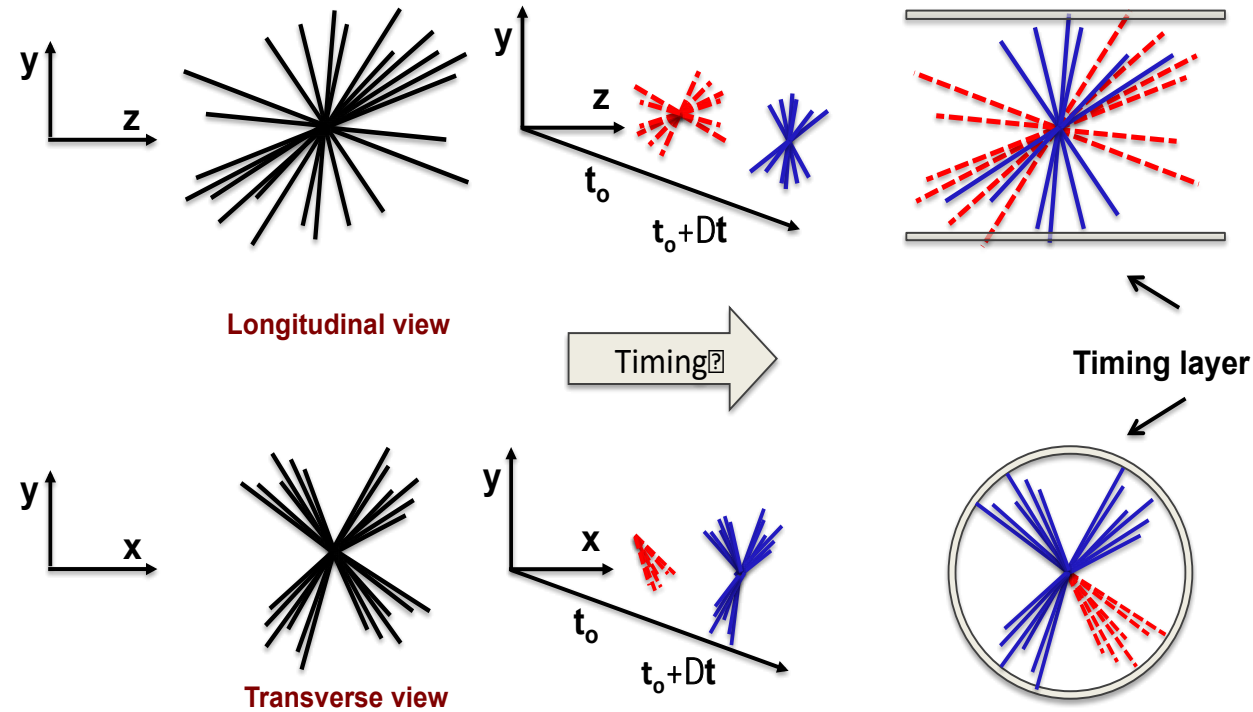
the collisions are separated in space and time



## HL-LHC situation:

the collisions are so dense that they overlap in space and time.  
This leads to error in the reconstruction of the event

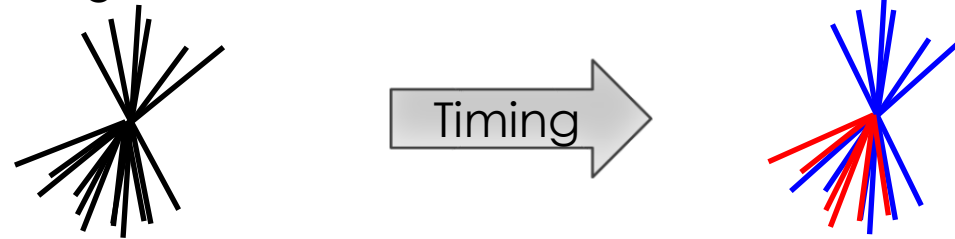
# New concept: Tracking in 4Dimension



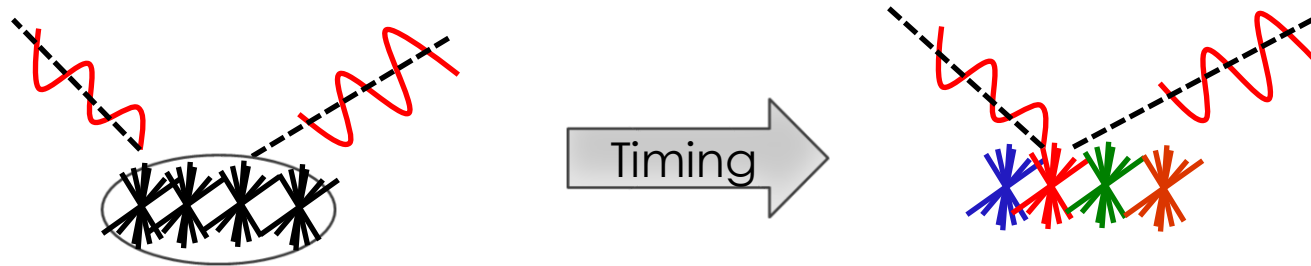
**The introduction of timing allows separating collisions that happen in the same location**

# Timing in the event reconstruction - II

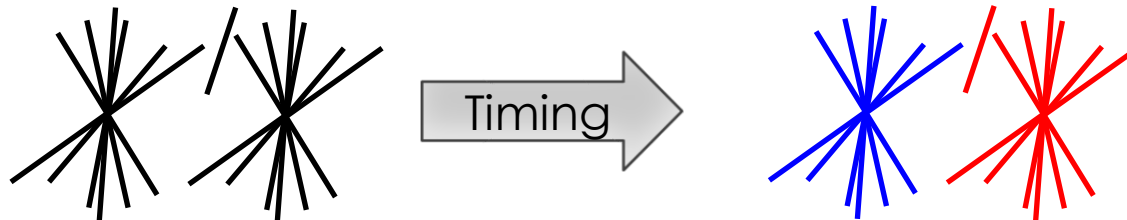
**Missing Et:** consider overlapping vertexes, one with missing Et: Timing allows obtaining at HL-LHC the same resolution on missing Et that we have now



**H  $\rightarrow$   $\gamma\gamma$ :** The timing of the  $\gamma\gamma$  allows to select an area (1 cm) where the vertex is located. The vertex timing allows to select the correct vertex within this area



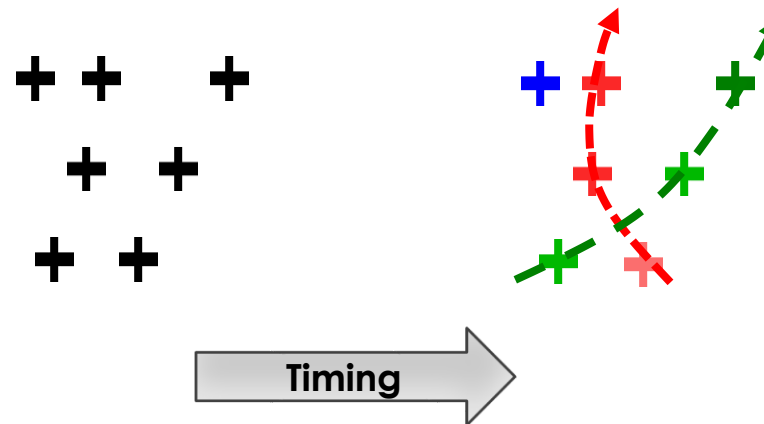
**Displaced vertexes:** The timing of the displaced track and that of each vertex allow identifying the correct vertex





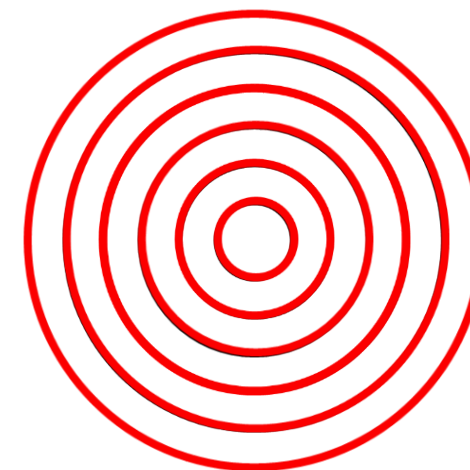
# Timing layers and 4D tracking

By “**4D tracking**” we mean the process of assigning a space and a time coordinate to a hit.



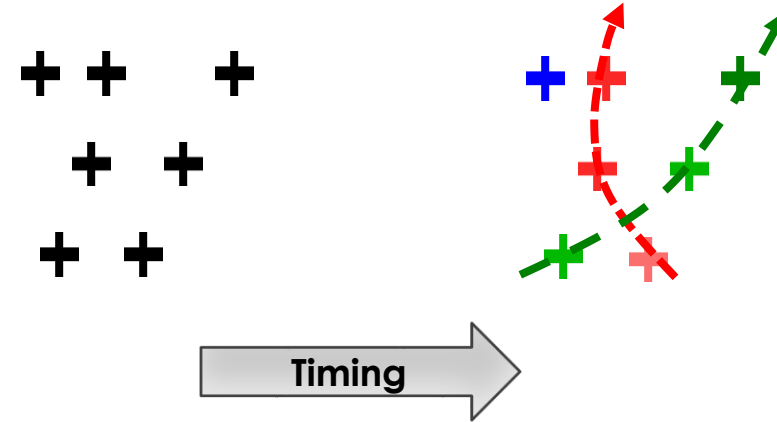
**Timing can be available at different levels of the event reconstruction:**

- 1) Timing in a single point (timing layer ATLAS,CMS)
- 2) Timing at some points along the track
- 3) Timing at each point along the track



# Timing layers and 4D tracking

By “**4D tracking**” we mean the process of assigning a space and a time coordinate to a hit.



**Timing can be available at different levels of the event reconstruction:**

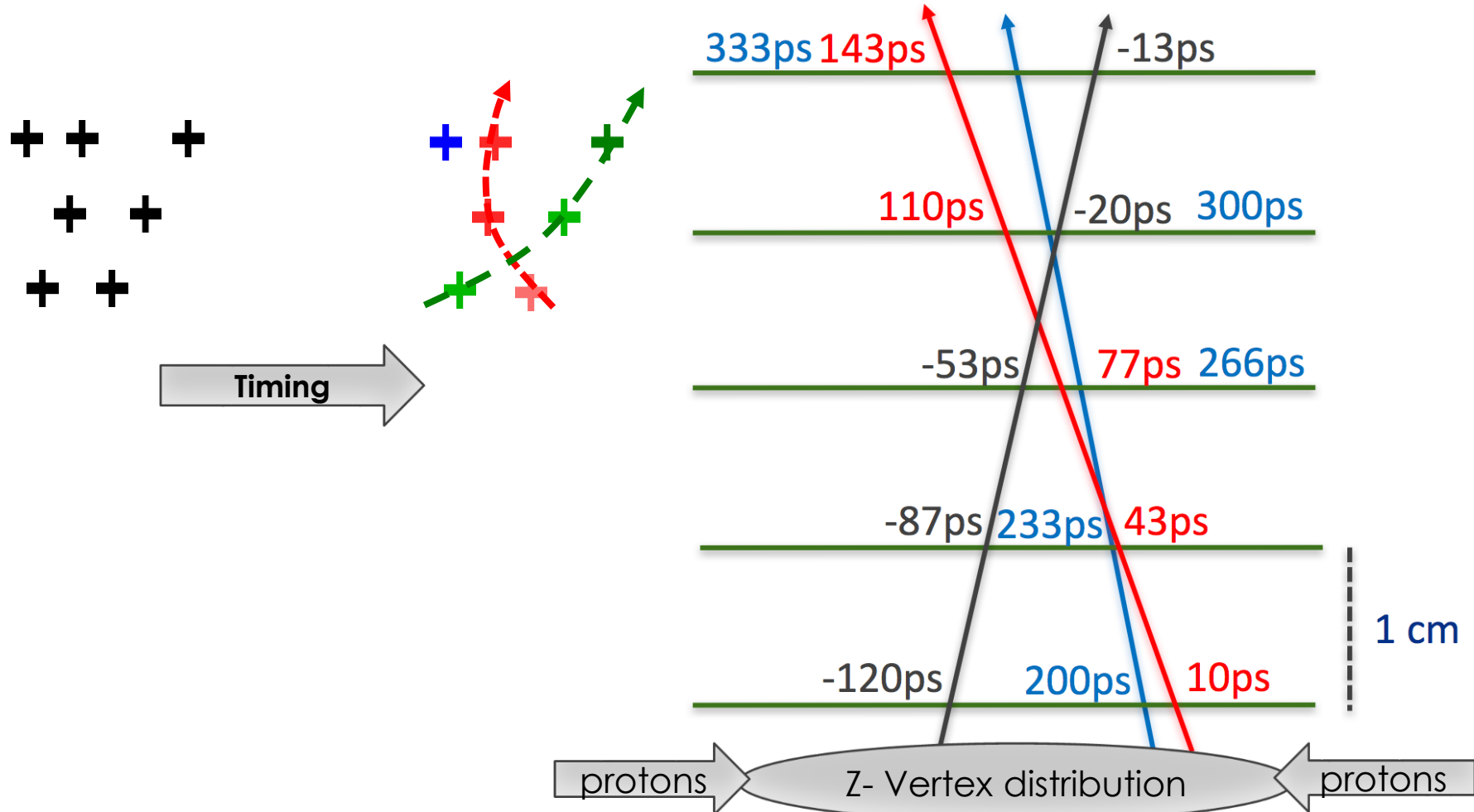
- 1) Timing in a single point (timing layer ATLAS,CMS)
- 2) Timing at some points along the track
- 3) Timing at each point along the track



**More timing coordinates yields to more performing systems, but require a much more complex read-out system.**  
**Some projects will be perfectly fine with having a limited set of timing points**

# 4D tracking: Timing at each point

- Massive simplification of pattern recognition, new tracking algorithms will be faster even in very dense environments
- Use only “time compatible points”



# Systems designed for accurate timing



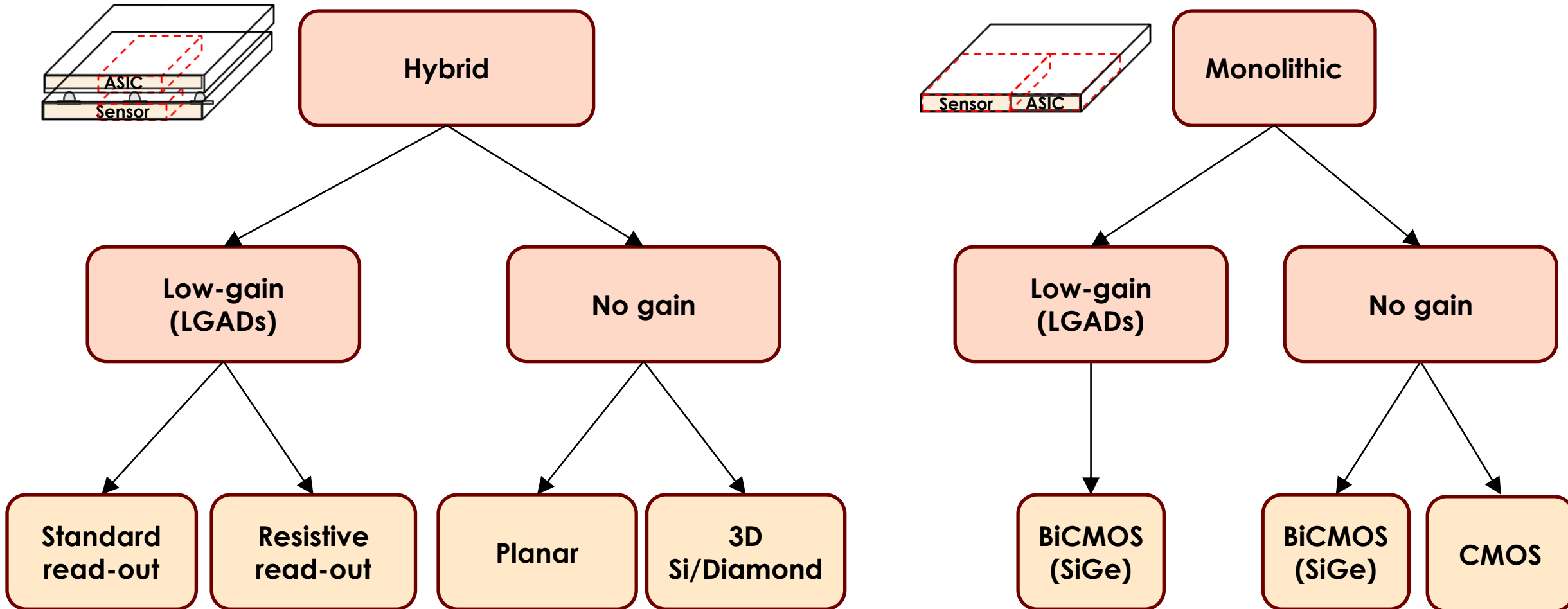
In a large detector system, good temporal resolution has many parts:

1. **The sensor**
2. **The design of the ASIC:**
  - Technology (process, BW..)
  - Money
  - Power available
2. **Detector design:**
  - Cabling, module quality, noise rejection
  - quality of power supply etc
3. **Infrastructure:**
  - Clock distribution
  - Cooling
  - Data transfer

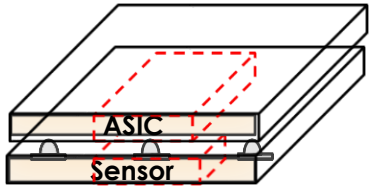
**A detector for timing needs very strong R&Ds in many additional aspects**  
(these challenges are now faced by the ATLAS and CMS timing layers)

# Tracking in 4-dimensions

The present R&Ds in position-sensitive timing detectors is very diverse



# The LGAD R&D



Hybrid

Low-gain  
(LGADs)

Standard  
read-out

Resistive  
read-out

In the past 10 years, the developments of LGAD have reached a very mature phase. LGAD are now used in ATLAS and CMS, and considered in many future experiments.

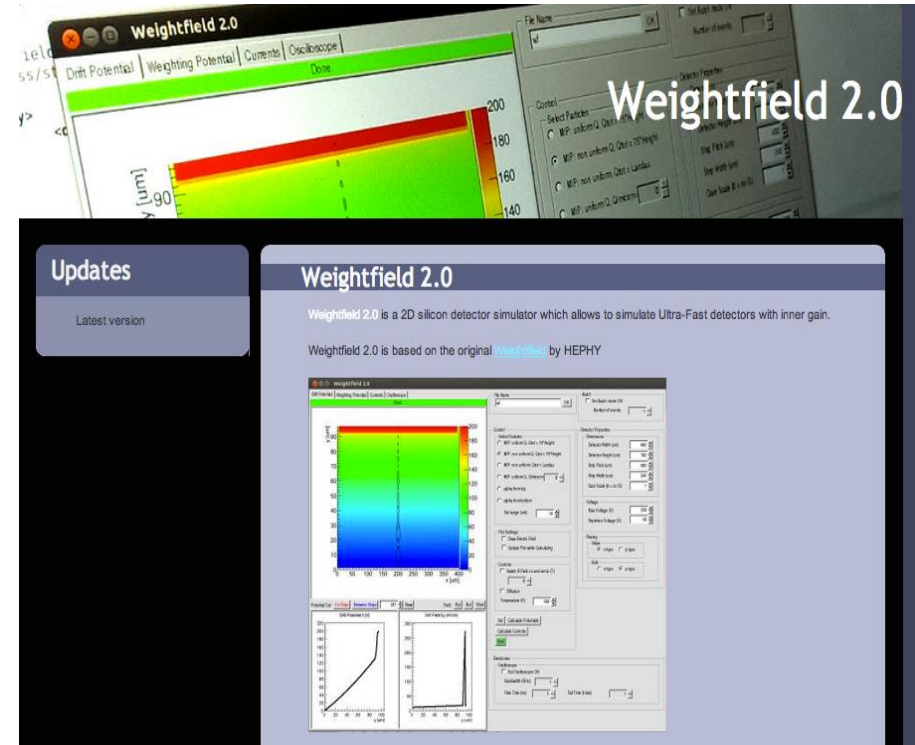
# Key tool: WF2 sensor simulation

The design of pico-second front-end electronics needs to know what type of current signals the front end will receive.

For this reason, we designed a simulator able to simulate the current pulse generated by silicon sensors accurately

## It includes:

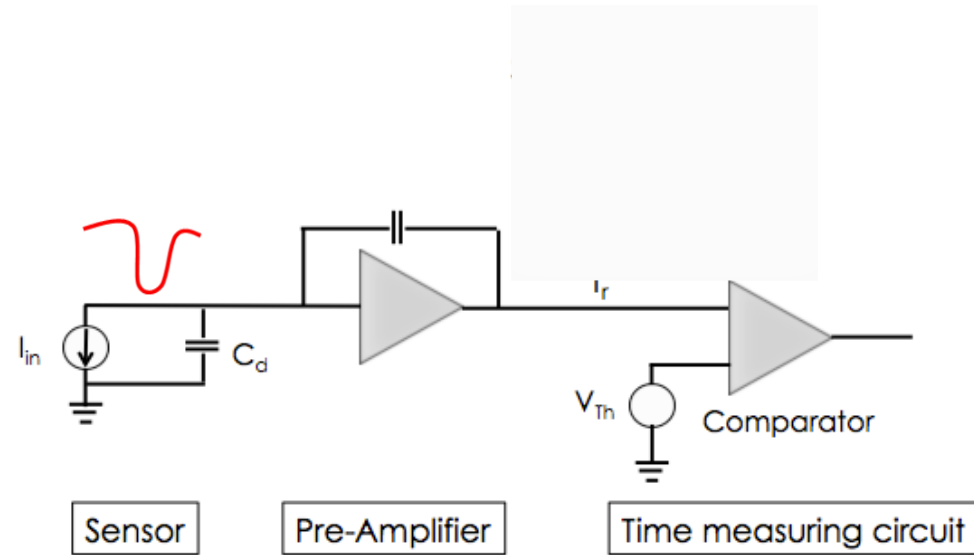
- Custom Geometry
- Calculation of drift field and weighting field
- Currents signal via Ramo's Theorem
- Gain
- Diffusion
- Temperature effect
- Non-uniform deposition
- Electronics



WeightField2, Available at  
<http://personalpages.to.infn.it/~cartigli/weightfield2>

# Silicon time-tagging detector

- Sensors produce a current pulse
- The read-out measures the time of arrival



**Sensors and read-out are two parts of a single object, sometimes even on the same substrate (monolithic option).**

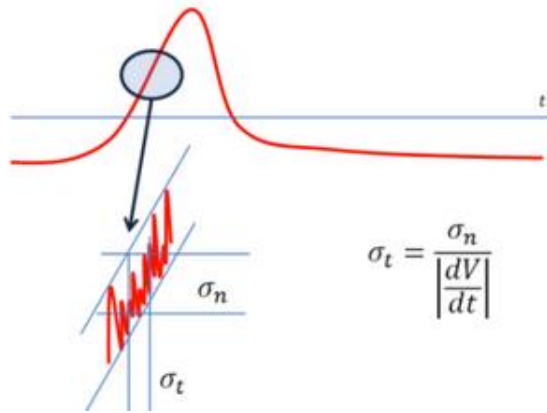
Sensors and electronics succeed (or eventually fail) together

In “timing circuits”, things can go wrong very rapidly (quote stolen from a chip designer)  
=> this is not a simple evolution of what we know how to do.

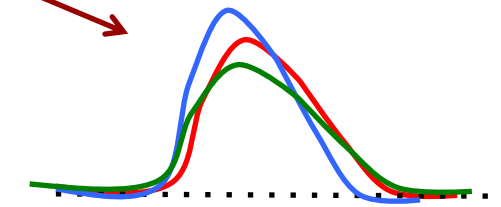
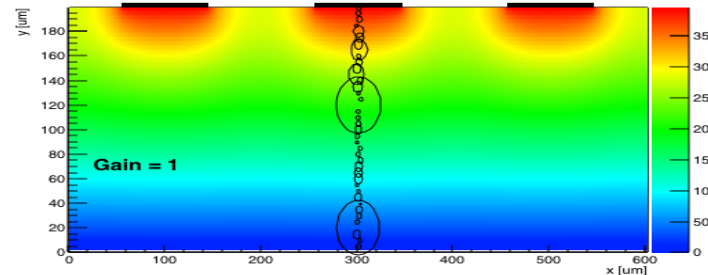
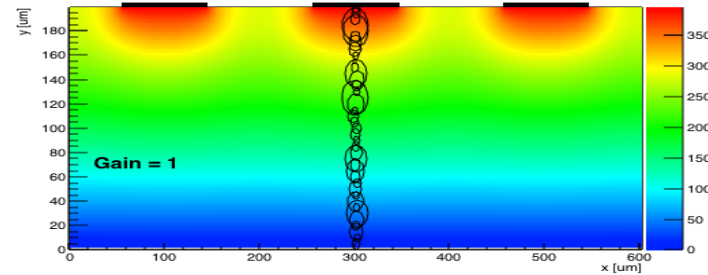


# Time resolution

$$\sigma_t^2 = \left( \frac{\text{Noise}}{dV/dt} \right)^2 + (\Delta \text{ionization})^2 + (\Delta \text{geometry})^2$$

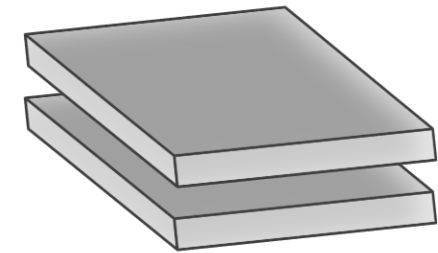


“Jitter” term



Signal shape is determined by  
Ramo's Theorem

$$i \mu q v E_w$$



**Amplitude variation** ==> corrected offline  
(time walk)

**Non-homogeneous energy deposition**  
==> signal change variation. Cannot be  
corrected, =minimized by design

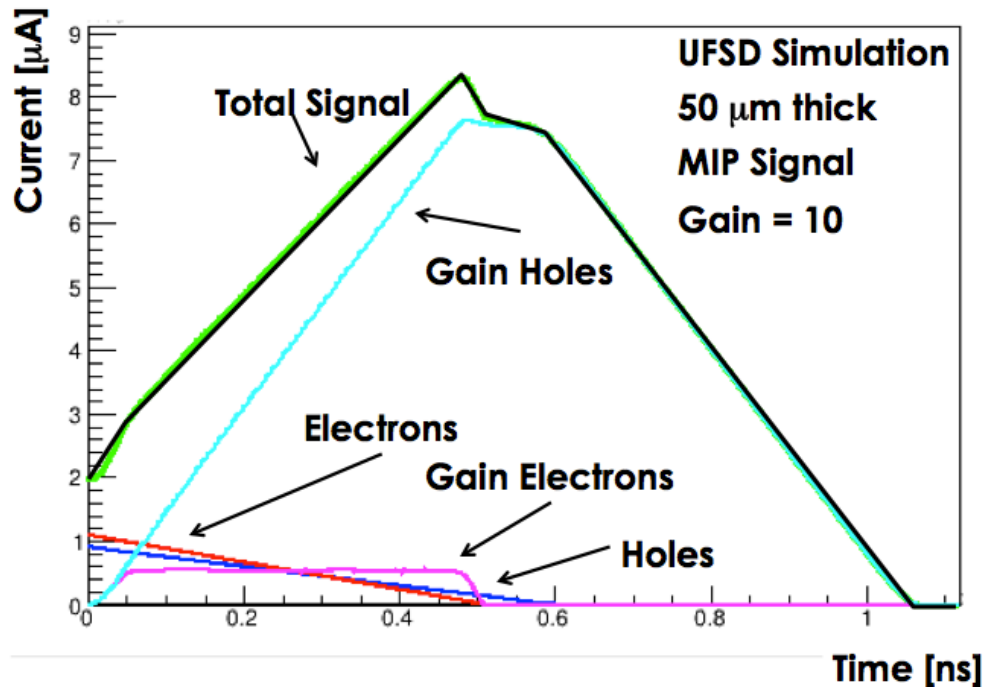
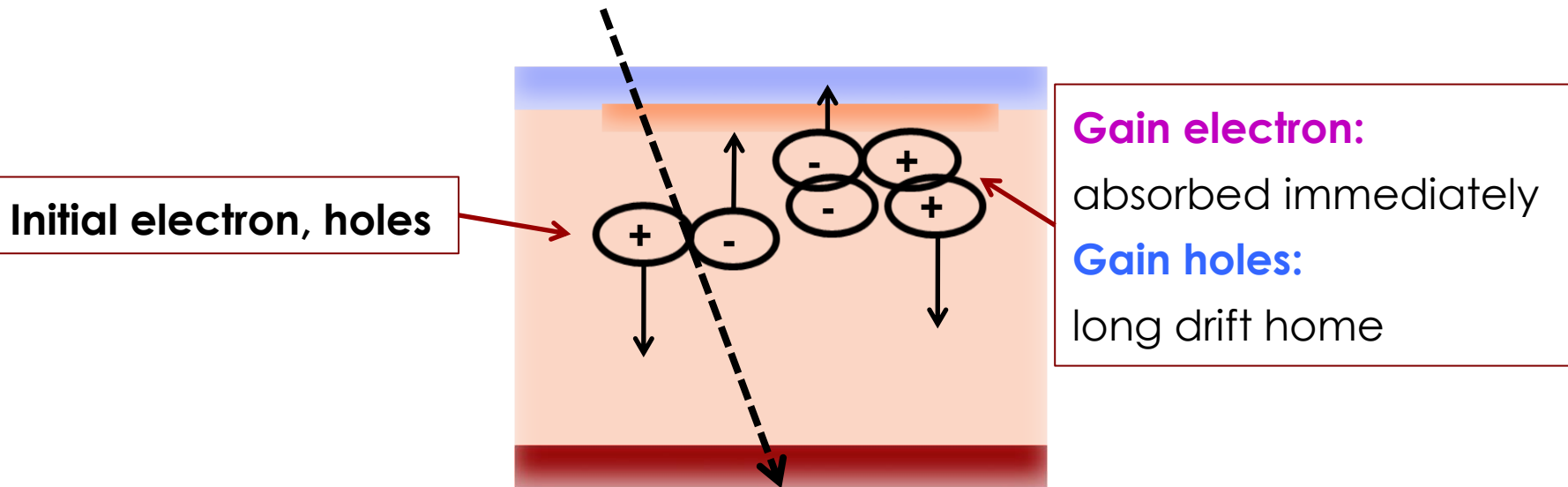
**Saturated drift velocity v**  
everywhere in the sensor volume  
**Uniform weighting field E<sub>w</sub>**

**==> Needs parallel plate geometry**

**Small noise** ==> choice of electronic  
technology

**Large dV/dt** ==> use sensors with  
internal gain

# Minimize jitter: LGADs have large signals!



Electrons multiply and produce additional electrons and holes.

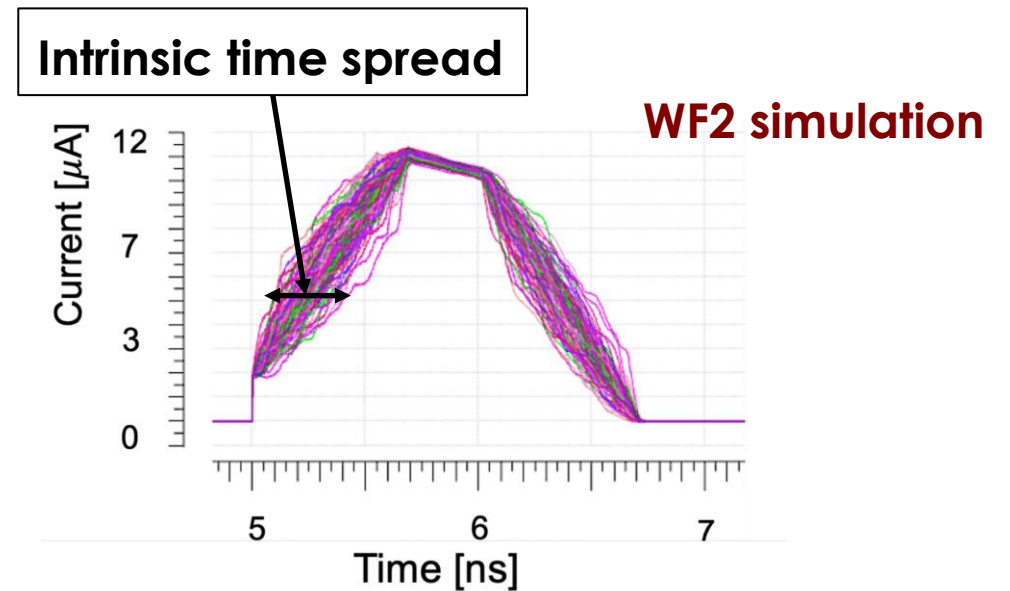
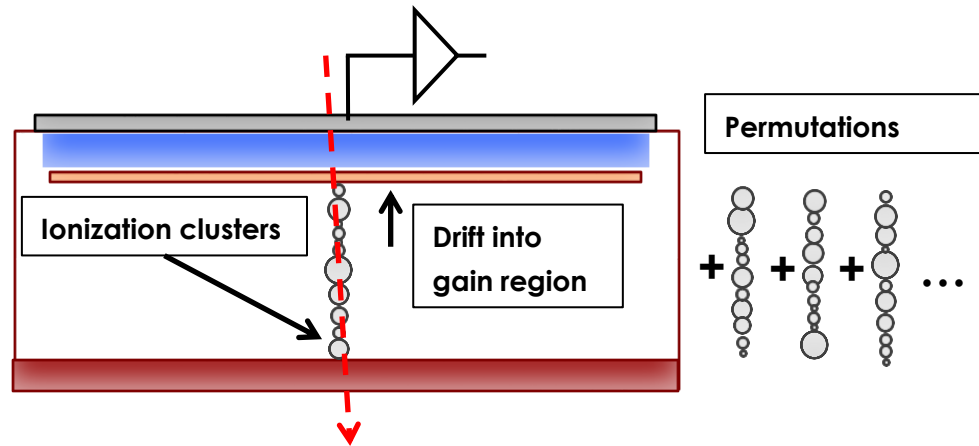
- Gain electrons have almost no effect
- Gain holes dominate the signal

➔ No holes multiplications

# Intrinsic LGAD time resolution

Why LGAD have an “intrinsic” time resolution?

**It is a combinatorial problem:** how many different ways are there to produce a given amplitude summing up individual ionization clusters (imagine there is 1 cluster every 1 micron) ?



50 microns thick ==> 50! Permutations...

10 microns thick ==> 10! Permutation

**The thinner the sensor, the smaller the intrinsic time resolution**

# Sensor geometry: how to minimize its contribution to $\sigma_t^2$

Signal shape is determined by Ramo's Theorem:

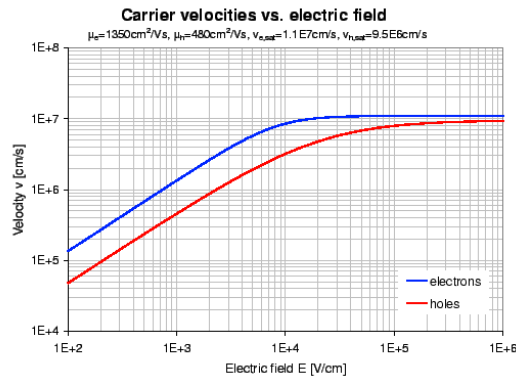
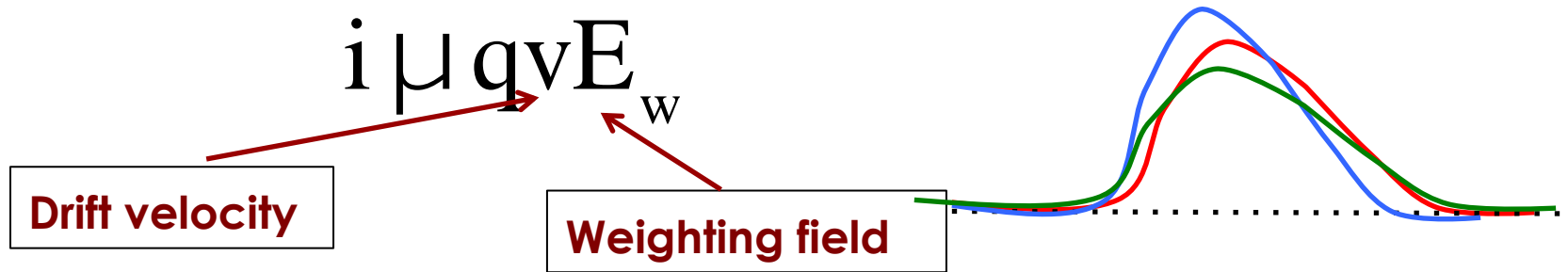
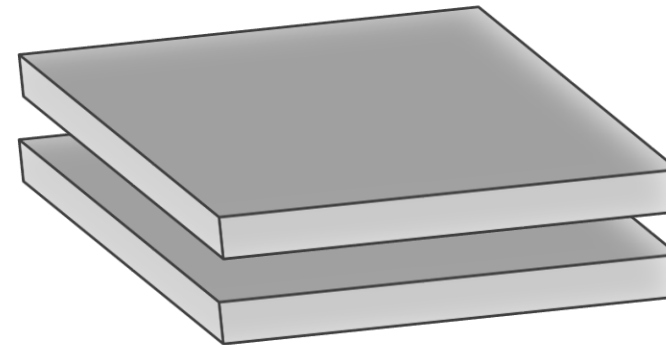


Figure: Electron and hole velocities vs. the electric field strength in silicon.



**The key to good timing is the uniformity of signals:**

Drift velocity and Weighting field need to be as uniform as possible

**Basic rule: parallel plate geometry**

# What is the signal of one e/h pair?

(Simplified model for pad detectors)

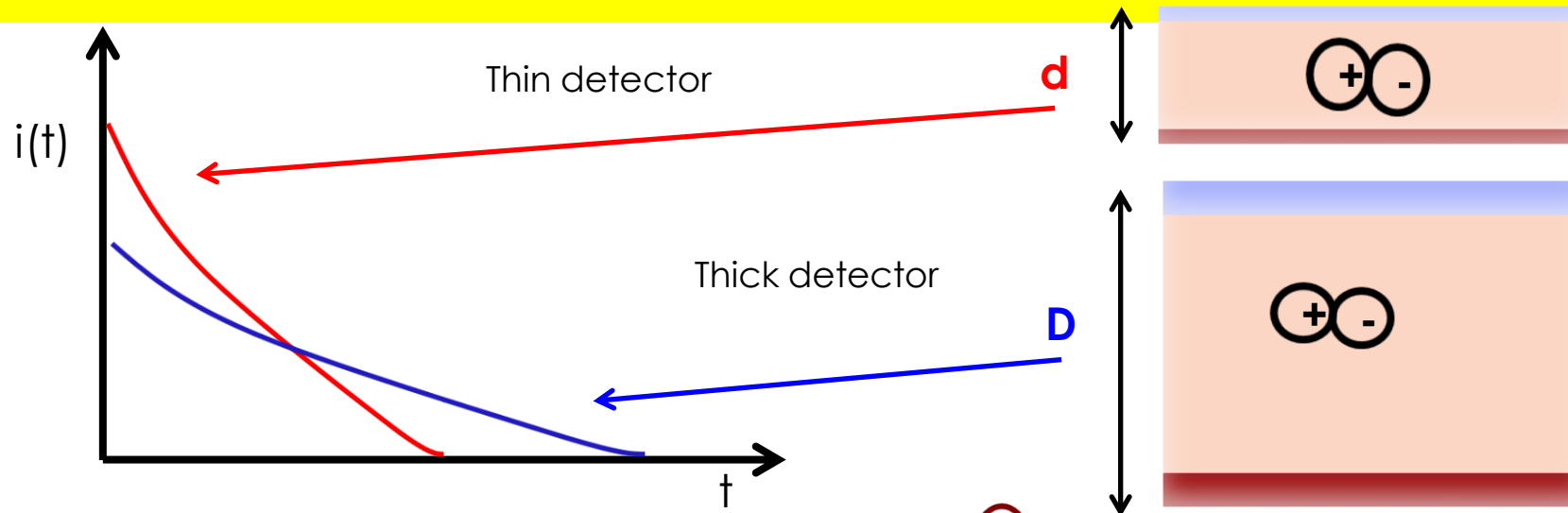


Let's consider **one single electron-hole pair**.

The integral of the current is equal to the electric charge,  $q$ :

$$\int_0^{\infty} [i_{e_l}(t) + i_h(t)] dt = q$$

However, **the shape of the signal depends on the thickness  $d$** :  
Thinner detectors have a higher slew rate

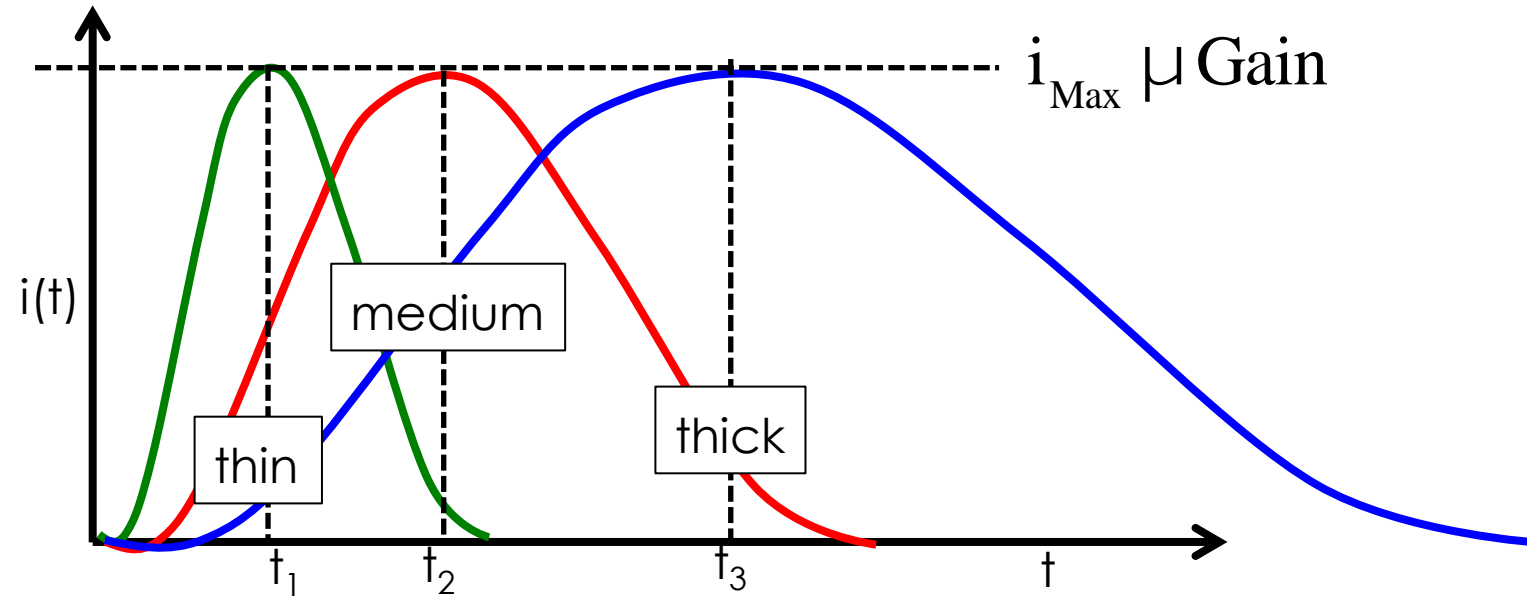


→ One e/h pair generates a higher current in thin detectors

$$i \propto qv \left( \frac{1}{d} \right) \leftarrow \text{Weighting field}$$

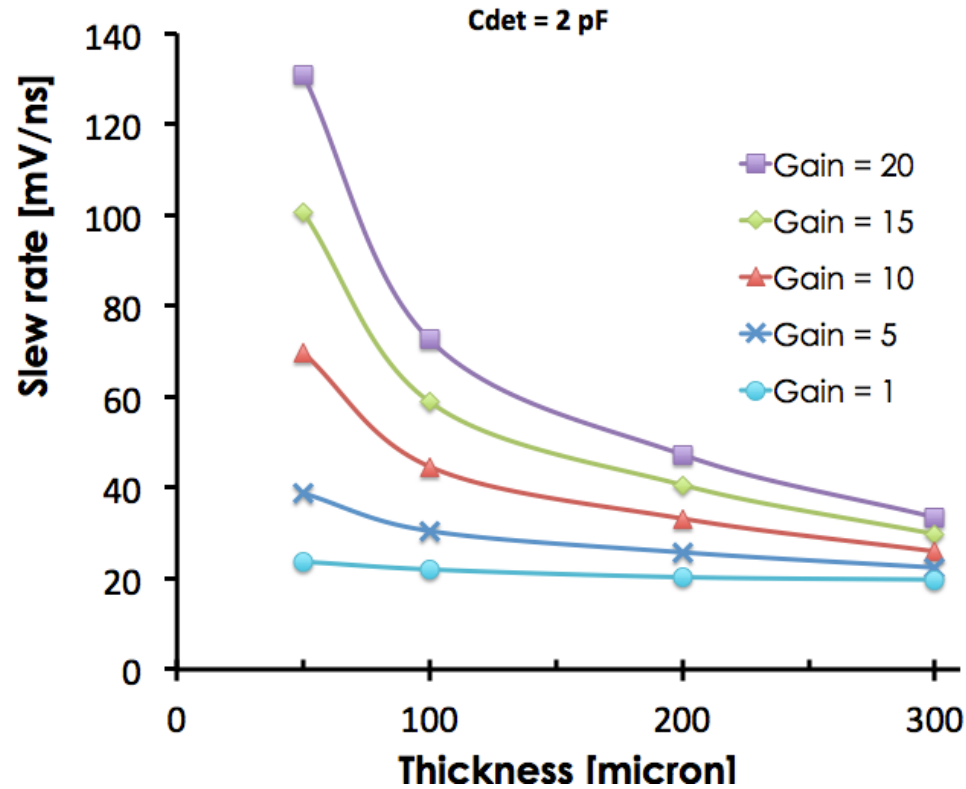
# Slew rate $dV/dt$

$$\frac{dV}{dt} \propto \frac{G}{d}$$



The rise time depends only on the sensor thickness  $\sim 1/d$

# Slew rate vs sensor thickness



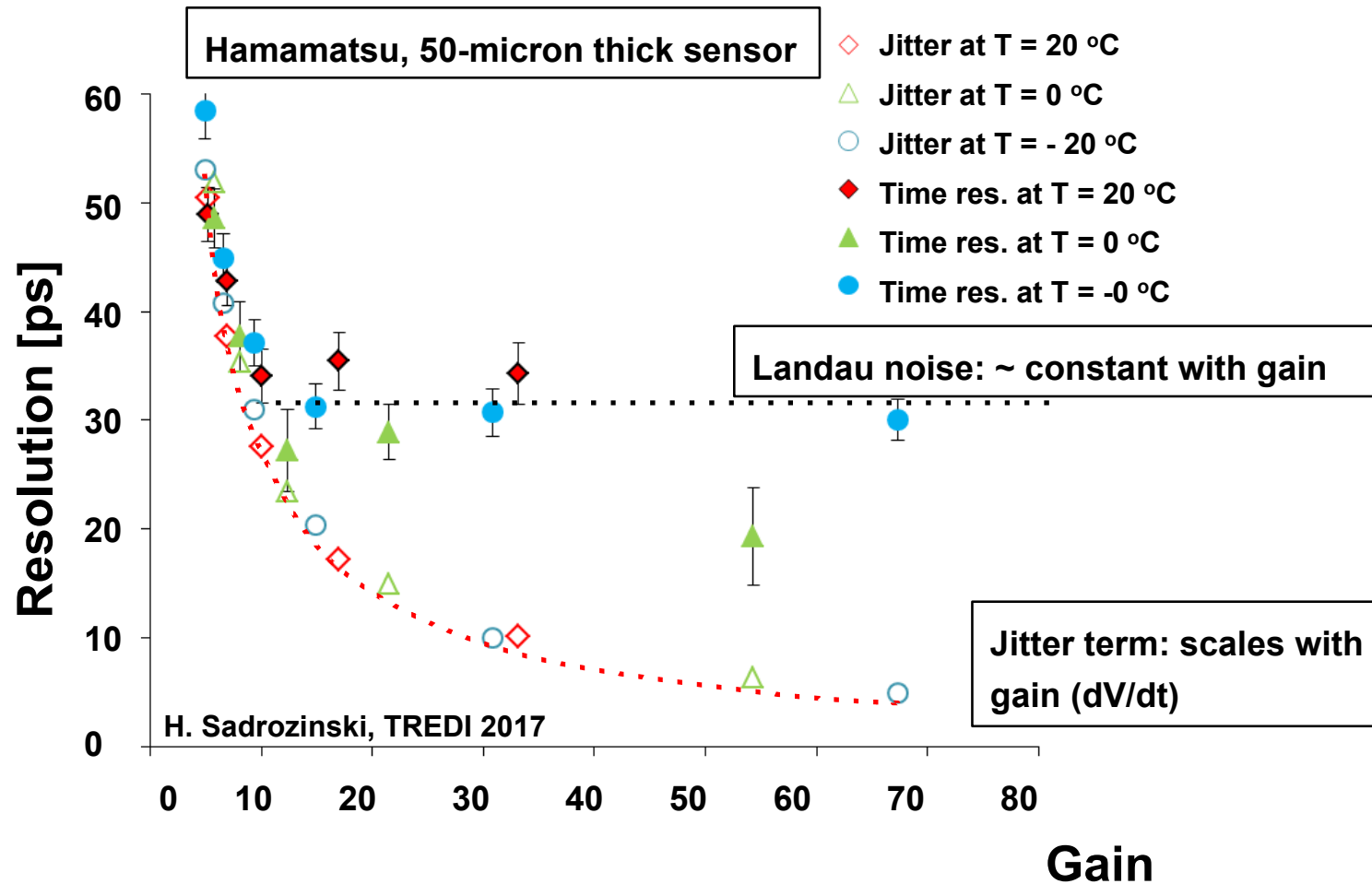
← 300 micron:  
~ 2-3 improvement  
with gain = 20

**Significant improvements in time resolution require thin detectors**

# An example of LGAD Hamamatsu's time resolution

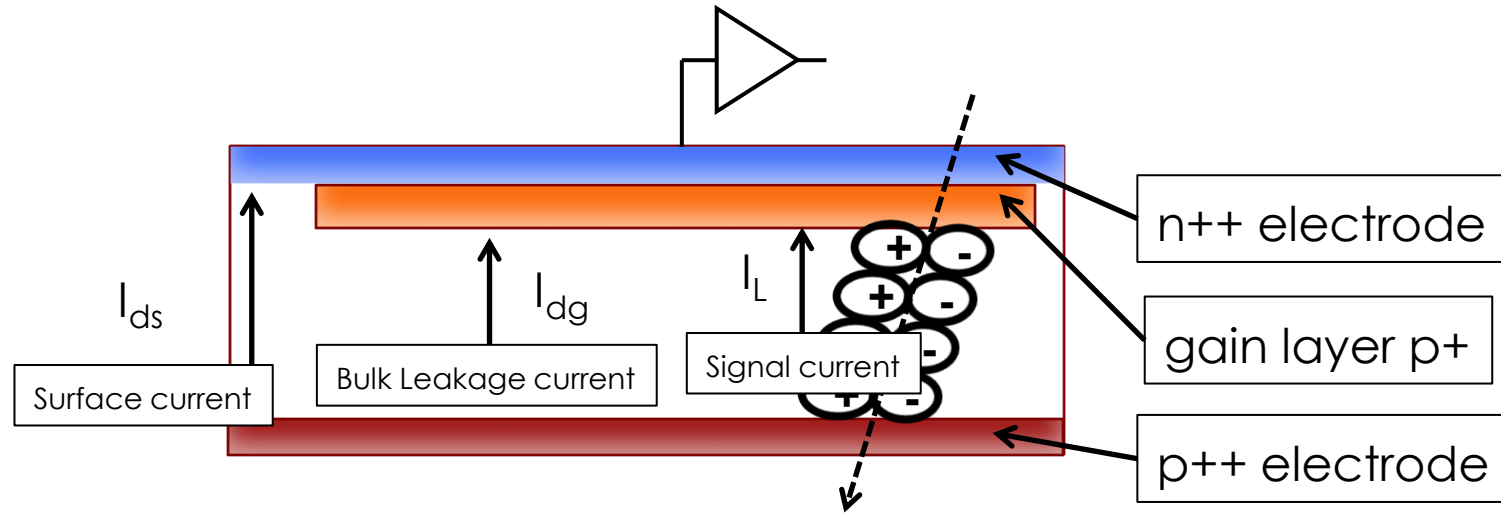


UFSD from Hamamatsu: 30 ps time resolution,  
Value of gain  $\sim 20$





# Why low gain? Shot noise in LGAD - APD



$$i_{Shot}^2 = 2eI_{Det} = 2e \left( \frac{e}{e} I_{Surface} + (I_{Bulk} + I_{Signal}) M^2 F \right)$$

$$F = Mk + \frac{x}{2} - \frac{1}{M} (1 - k)$$

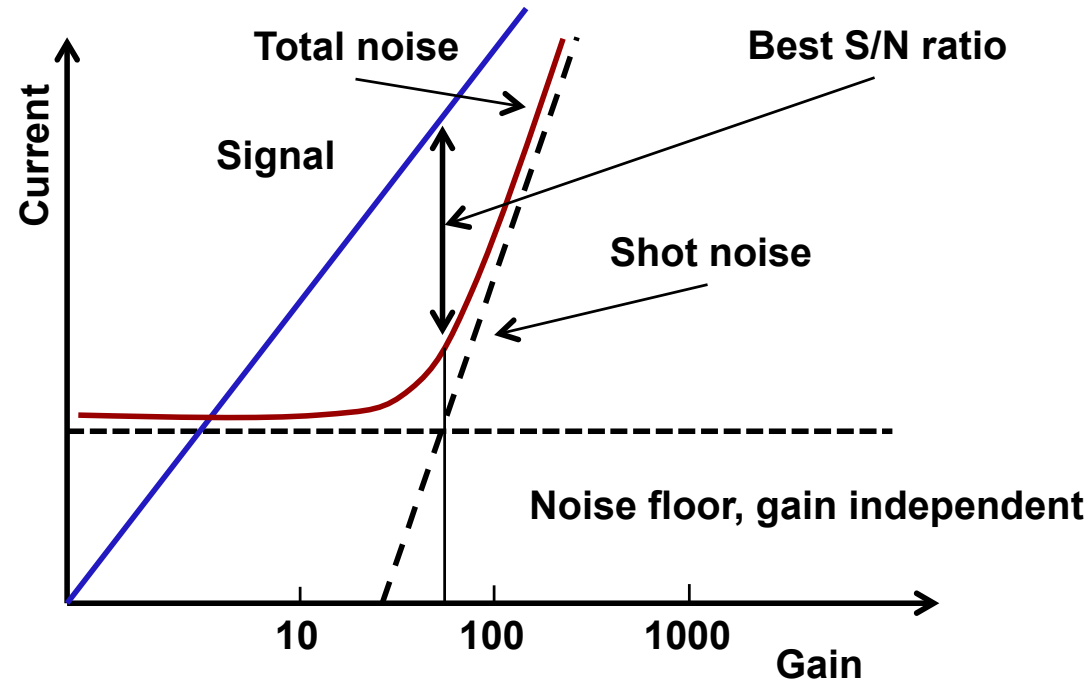
$$F \sim M^x$$

$k = e/h$  ionization rate  
 $x =$  excess noise index  
 $M =$  gain

Correction factor to the standard Shot noise, due to the noise of the multiplication mechanism

$$F = \frac{\langle M^2 \rangle}{\langle M \rangle^2} \quad \text{D} \quad \langle M^2 \rangle = \langle M \rangle^2 F$$

# Noise increase as a function of gain



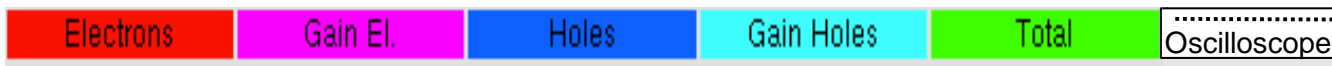
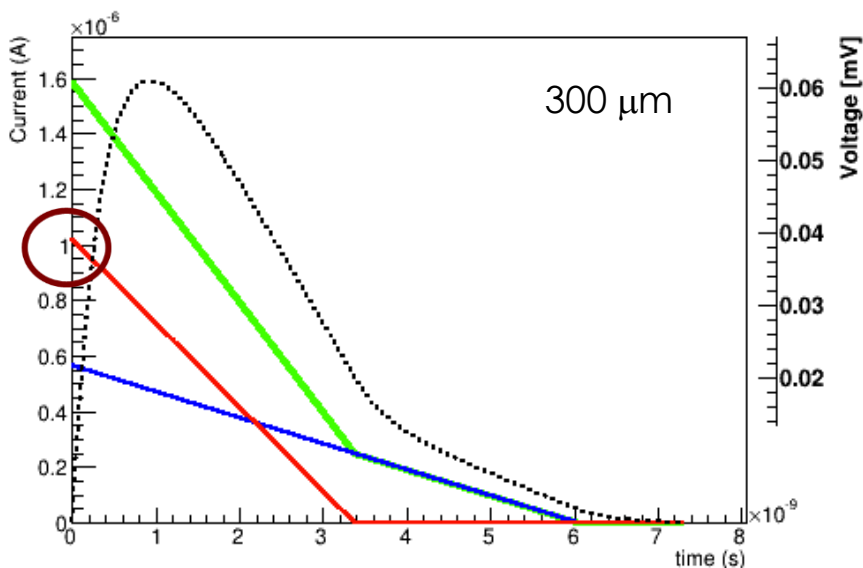
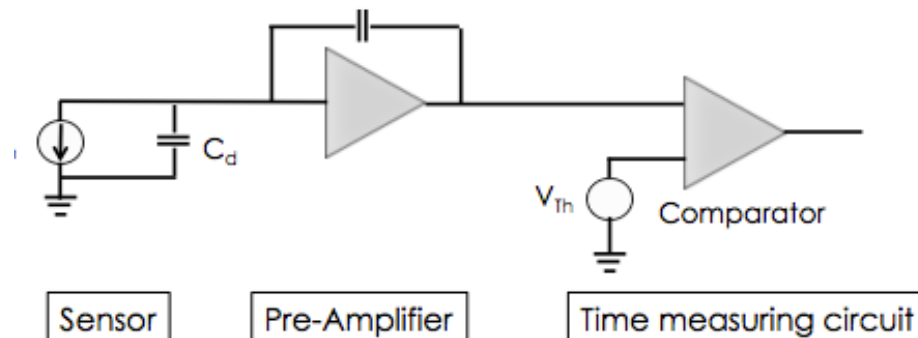
**Goal:**

**The noise from silicon current should stay below that of the electronics**

# Electronics

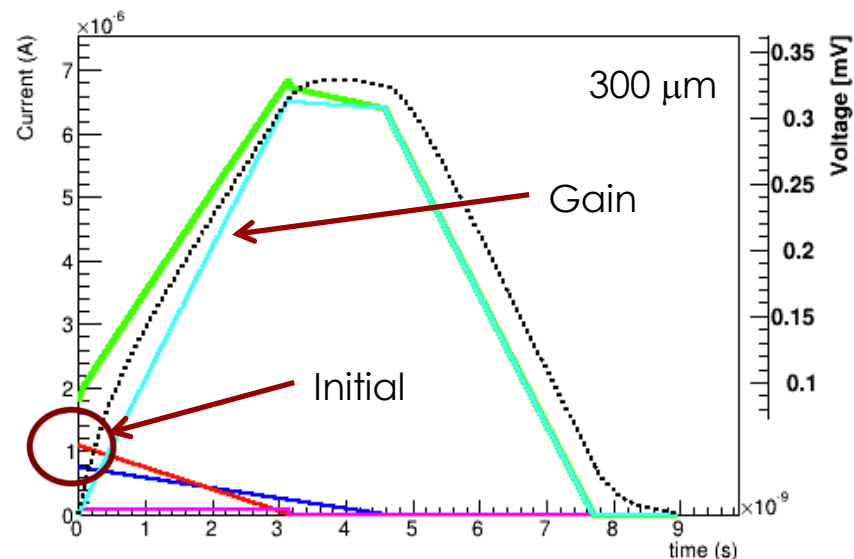
To fully exploit UFSDs, dedicated electronics needs to be designed.

**The signal from UFSDs is different from that of traditional sensors**



**Pads with no gain**

Charges generated uniquely by the incident particle

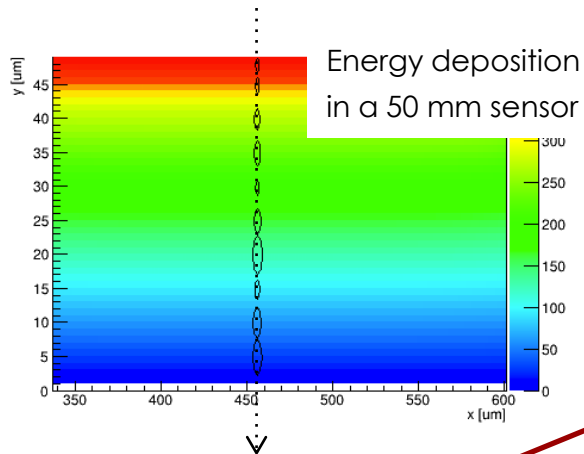


**Pads with gain**

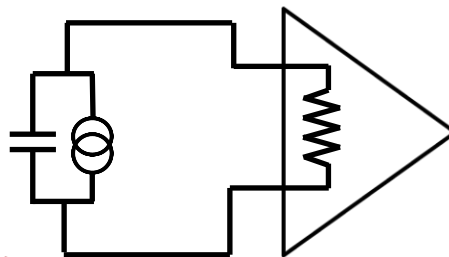
Current due to gain holes creates a longer and higher signal

Simulated Weightfield2

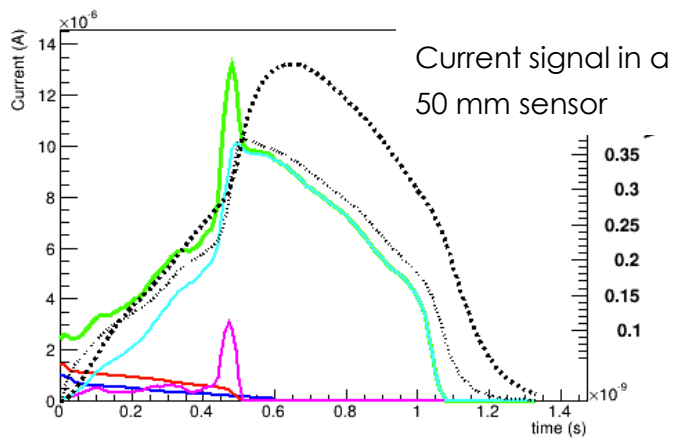
# Electronics: What is the best pre-amp choice?



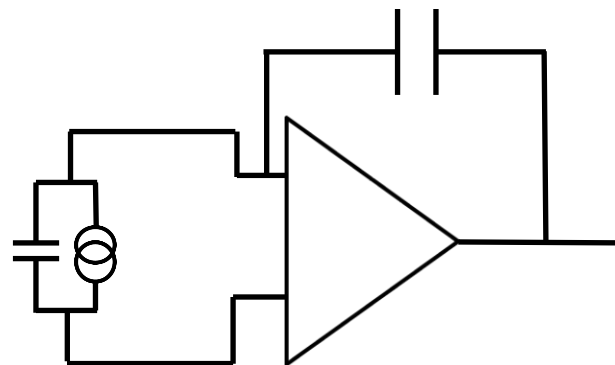
## Current Amplifier



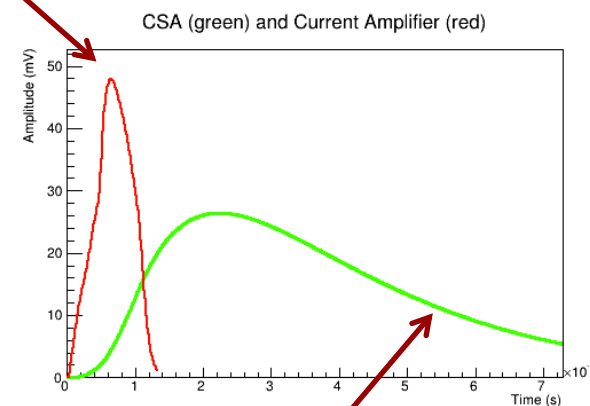
- Fast slew rate
- Higher noise
- Sensitive to Landau bumps



## Charge Sensitive Amplifier



- Slower slew rate
- Quieter
- Integration helps the signal smoothing



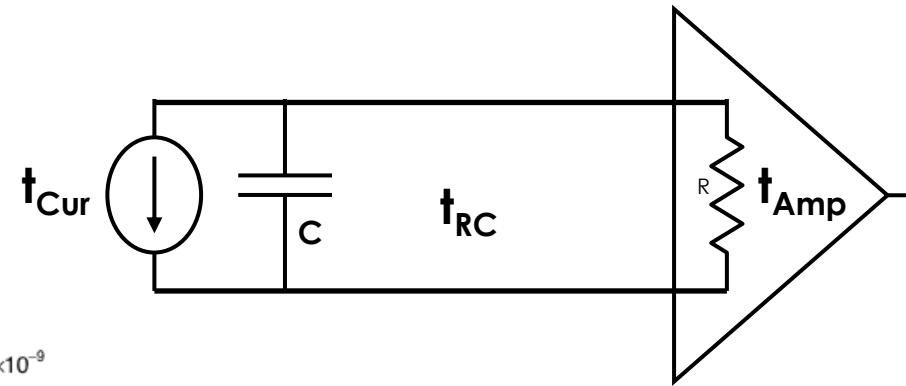
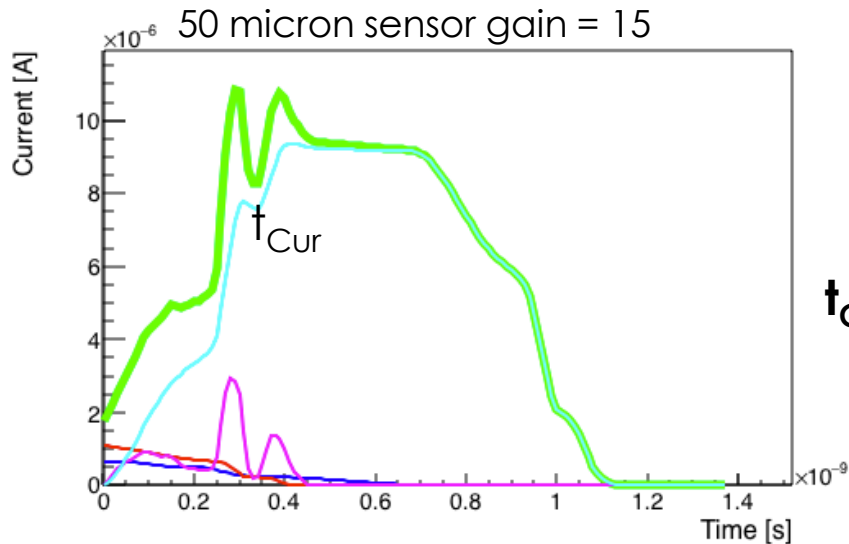
# The players: signal, noise and slope

Signal  $dV/dt$

Landau Noise

Shot Noise

Electronic Noise



Electrons Gain El. Holes Gain Holes Total

The current rise time ( $t_{Cur}$ )

The RC circuit ( $t_{RC}$ )

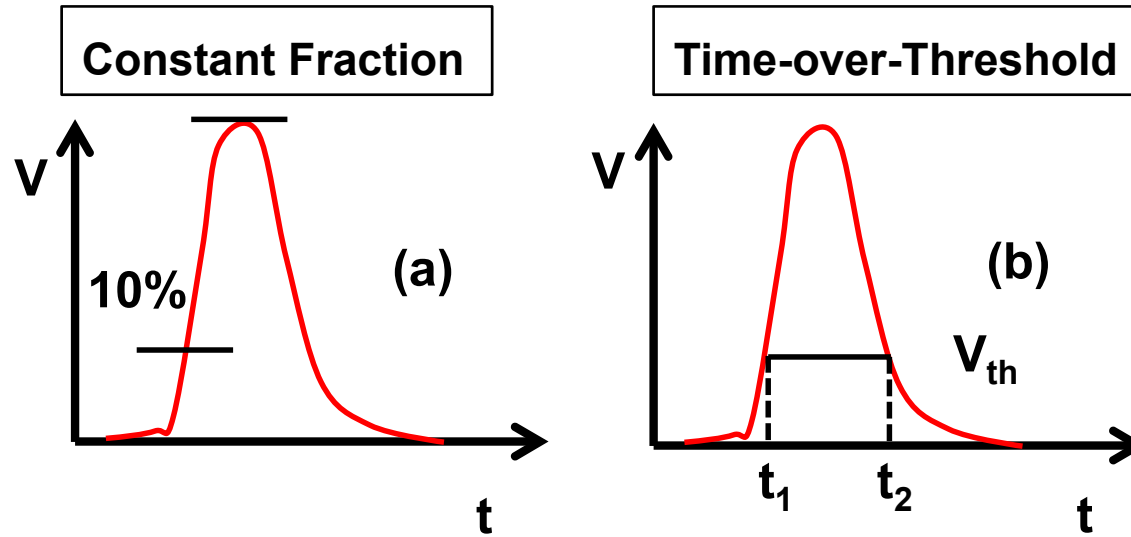
Amplifier rise time ( $t_{Amp}$ )

There are 3 quantities determining the rise time after the amplifier:

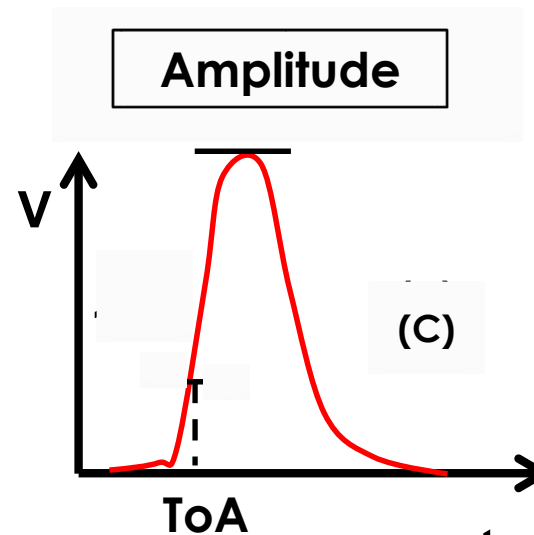
1. The signal rise time ( $t_{Cur}$ )
2. The RC circuit formed by the detector capacitance and the amplifier input impedance ( $t_{RC}$ )
3. The amplifier rise time ( $t_{Amp}$ )

# Time walk corrections

On paper both seem feasible, in practice **ToT is much easier to implement**



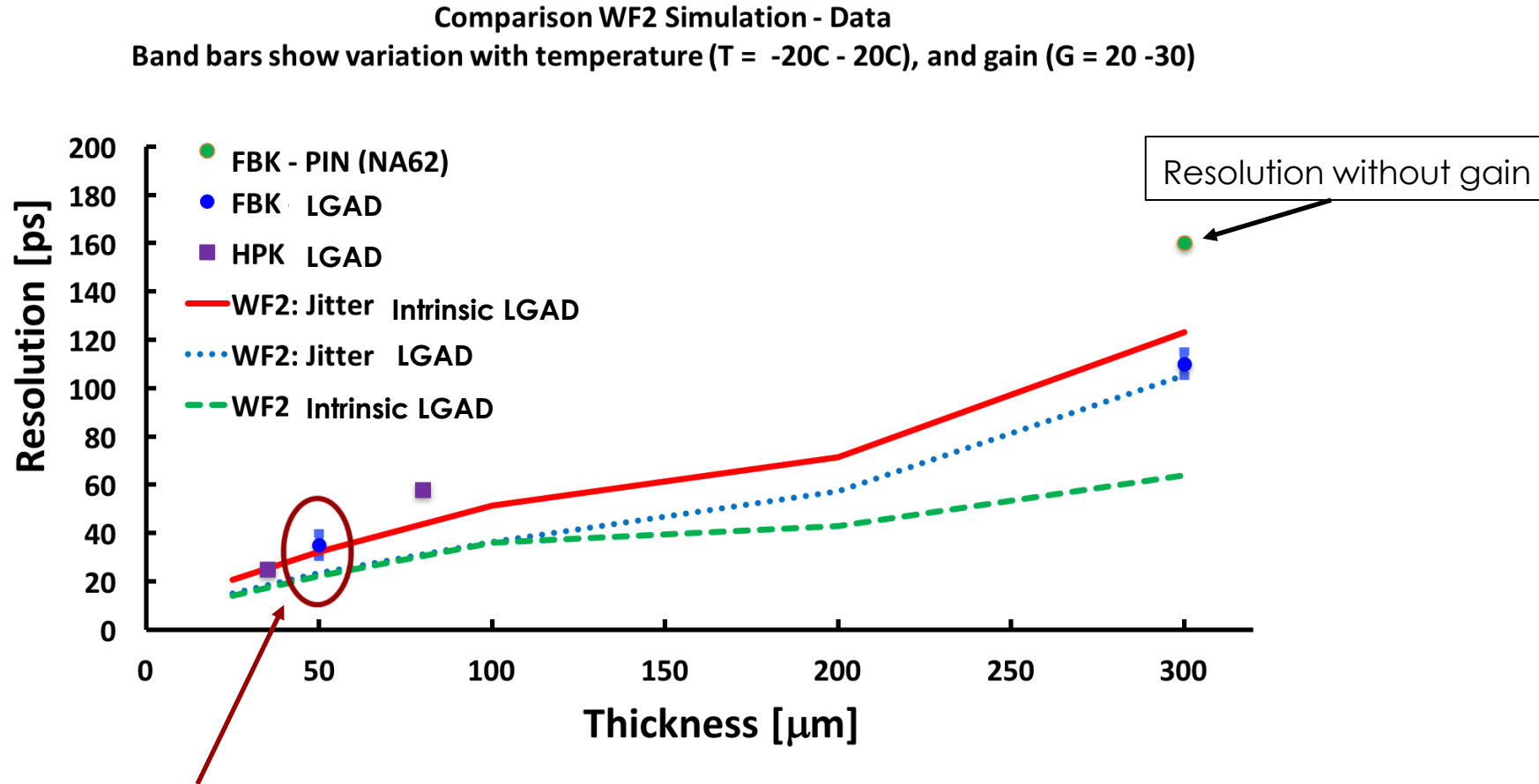
My favorite: **ToA and Amplitude**  
 → The tail of the signal is prone to large changes due to charge trapping



What is the influence of the sensor on the level of the CFD or of  $V_{th}$ ?

# LGAD temporal resolution vs sensor thickness

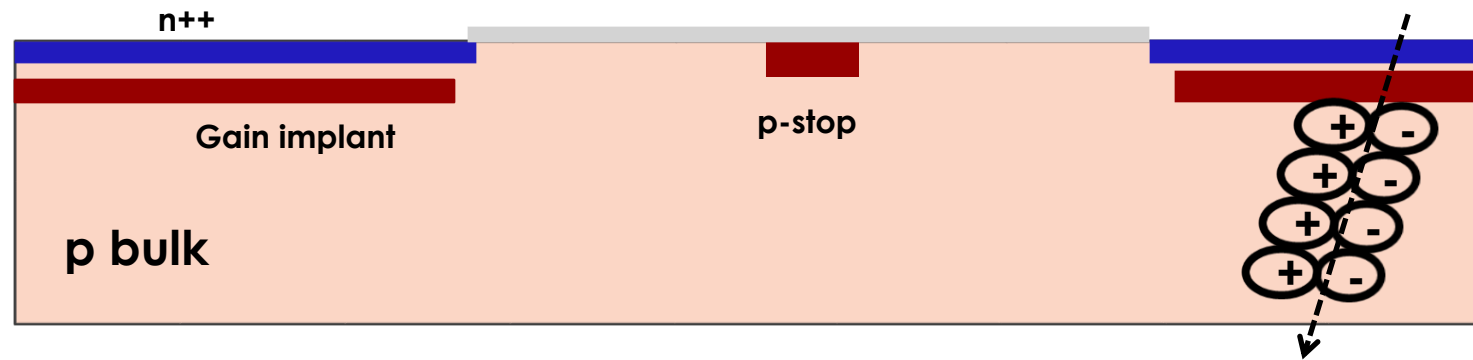
**Note: LGADs have an intrinsic resolution that depends on the thickness**



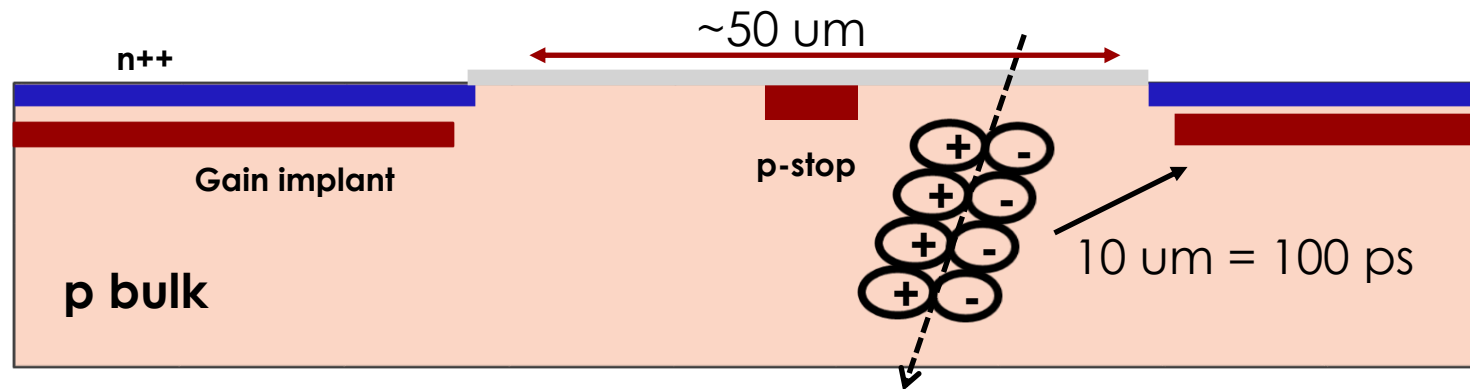
**Both CMS and ATLAS have opted for 50 μm thick LGAD,  
(intrinsic time resolution of about 30 ps)**

# Signals from inter-pad region

Particles hitting a pad create charges underneath the timing layer: no delay between the passage of the particle and the start of multiplication



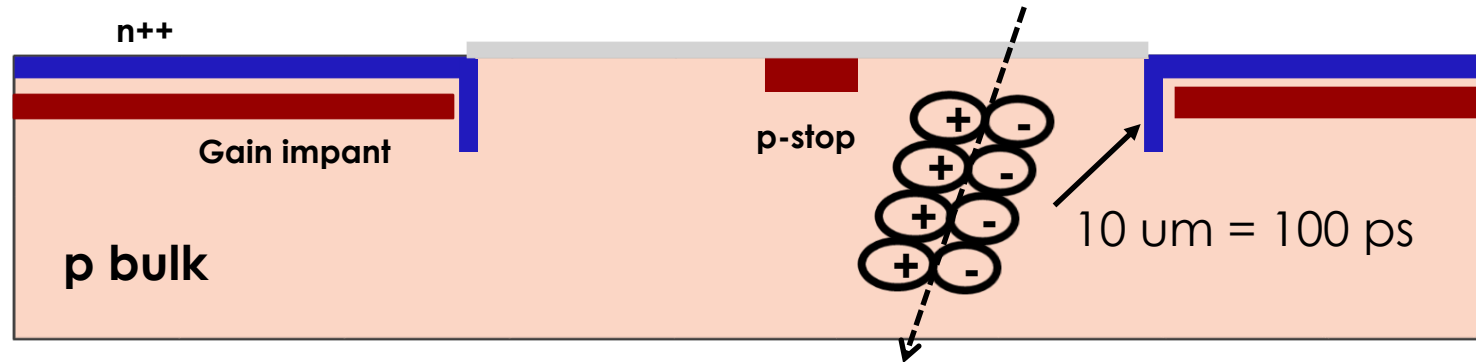
Particles hitting between pads create charges far from the multiplication layers: they generate late signals





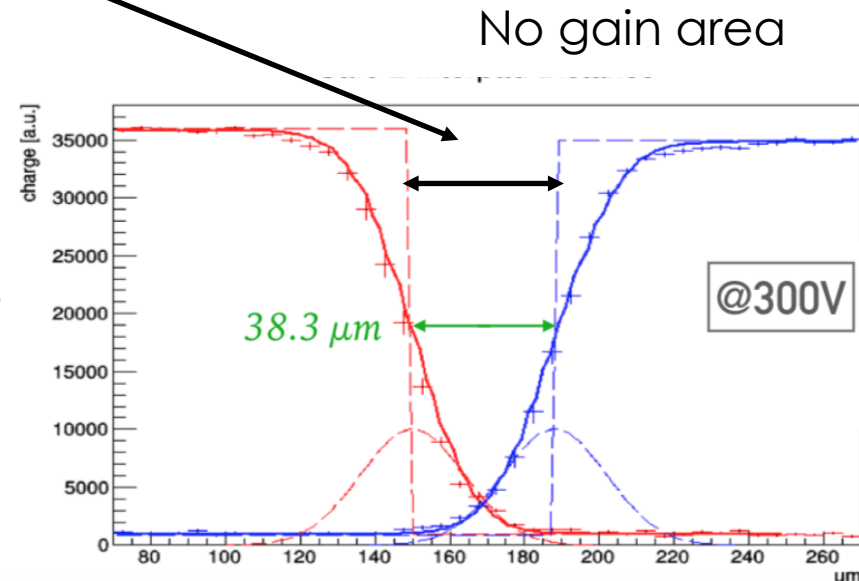
# Signals from inter-pad region

Solution: add a deep n implant to collect the charges in the interpad

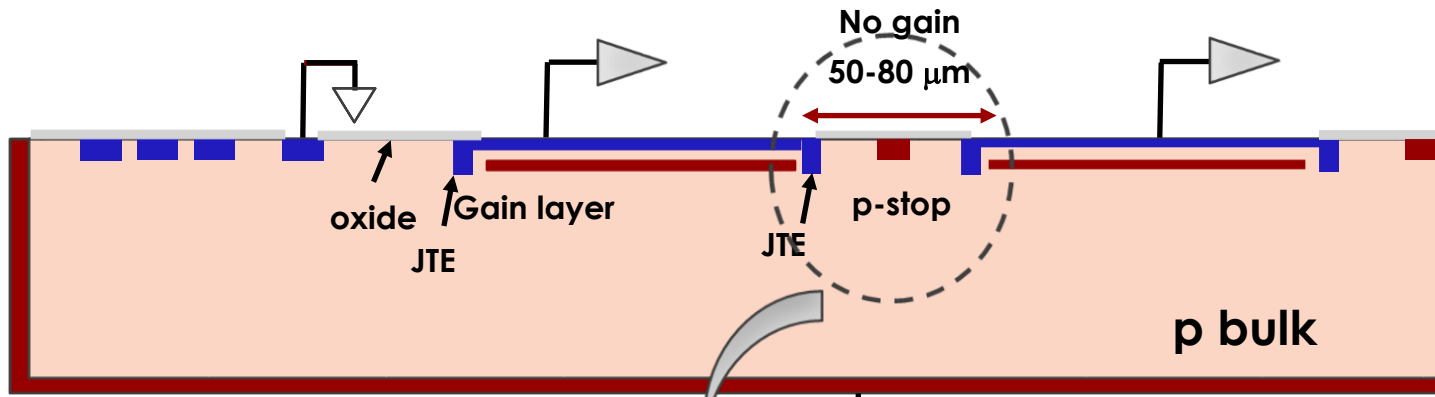


Deep implants collect the charge carriers preventing their multiplications:

- signals that are “out of time” are not multiplied
- Setting a threshold high enough allows to be blind to the interpad signals

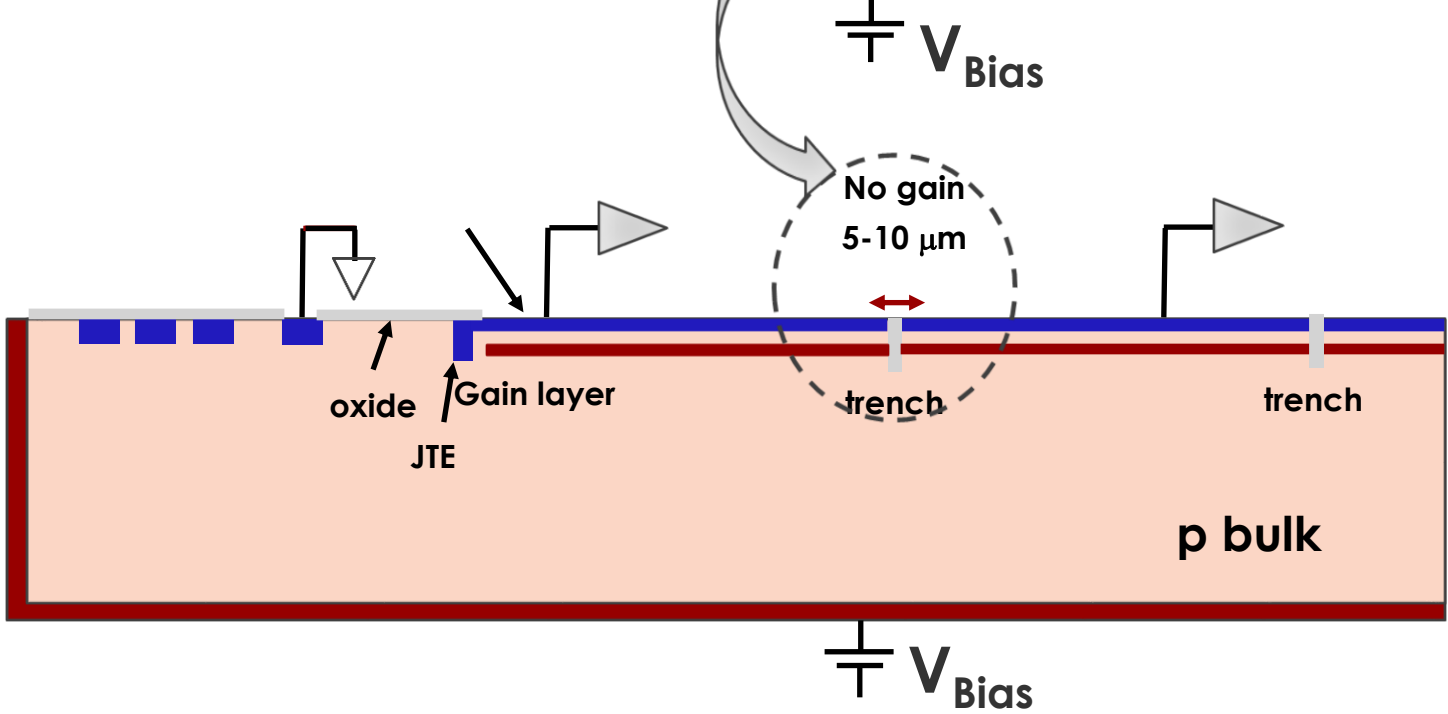


# LGAD Trench Isolated: enabling small UFSD pixels



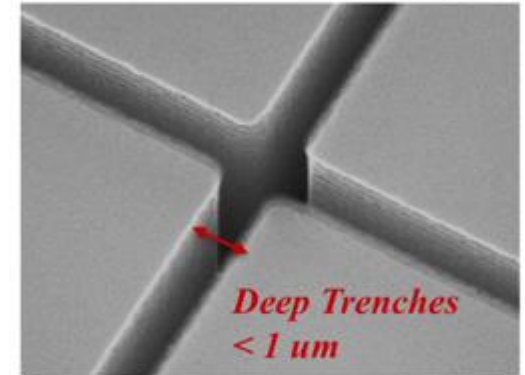
No-gain region ~ 50-80  $\mu\text{m}$   
 → cannot use for small pixels

**Solution: use trenches for pad isolation**  
 → No-gain region ~ 0 – 10  $\mu\text{m}$



## RD50-TI production

Interpad design	Interpad distance [ $\mu\text{m}$ ]
V1_1TR	$2.7 \pm 0.2$
V2_1TR	$6.5 \pm 0.2$
V3_1TR	$7.9 \pm 0.1$
V4_1TR	$10.6 \pm 0.2$
V2_2TR	$8.9 \pm 0.2$
V3_2TR	$10.3 \pm 0.1$



→ The R&D to achieve small pixels is clear

# Irradiation effects in LGADs

---



## **Irradiation causes 3 main effects:**

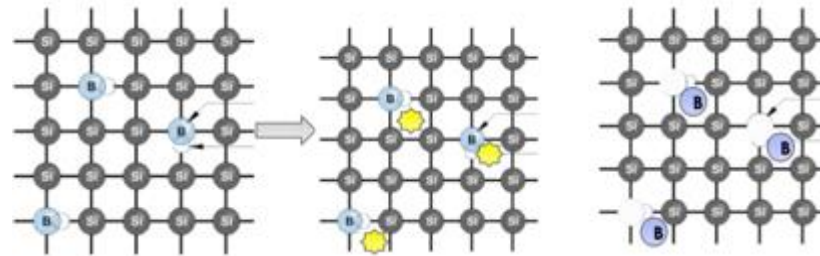
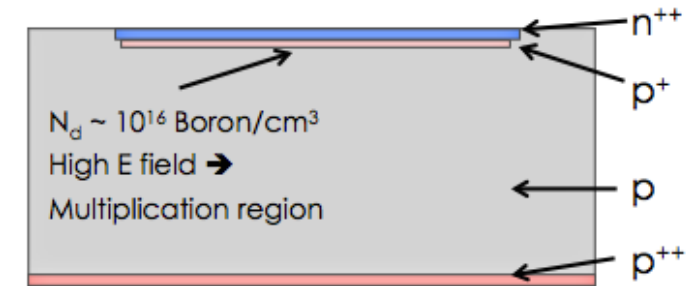
- Decrease of charge collection efficiency due to trapping
- Doping creation/removal
- Increased leakage current, shot noise

We need to design a detector that is able to survive large fluences,  
up to  $\sim 5E15 - 1E16 n_{eq}/cm^2$

# Acceptor removal

**Unfortunate fact:** irradiation de-activate p-doping removing Boron from the reticle

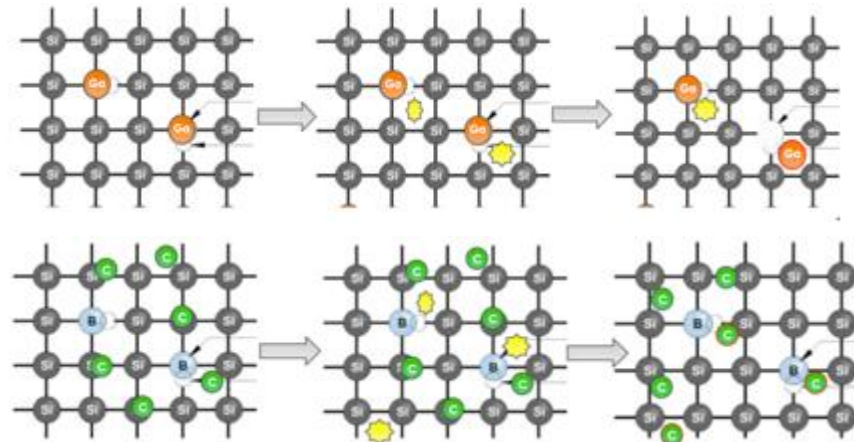
$$N(\emptyset) = N(0) * e^{-c\emptyset}$$



## Boron

Radiation creates interstitial defects that inactivate the Boron:  $Si_i + B_s \rightarrow Si_s + B_i$

Two possible solutions: 1) use Gallium, 2) Add Carbon



## Gallium

From literature, Gallium has a lower possibility to become interstitial

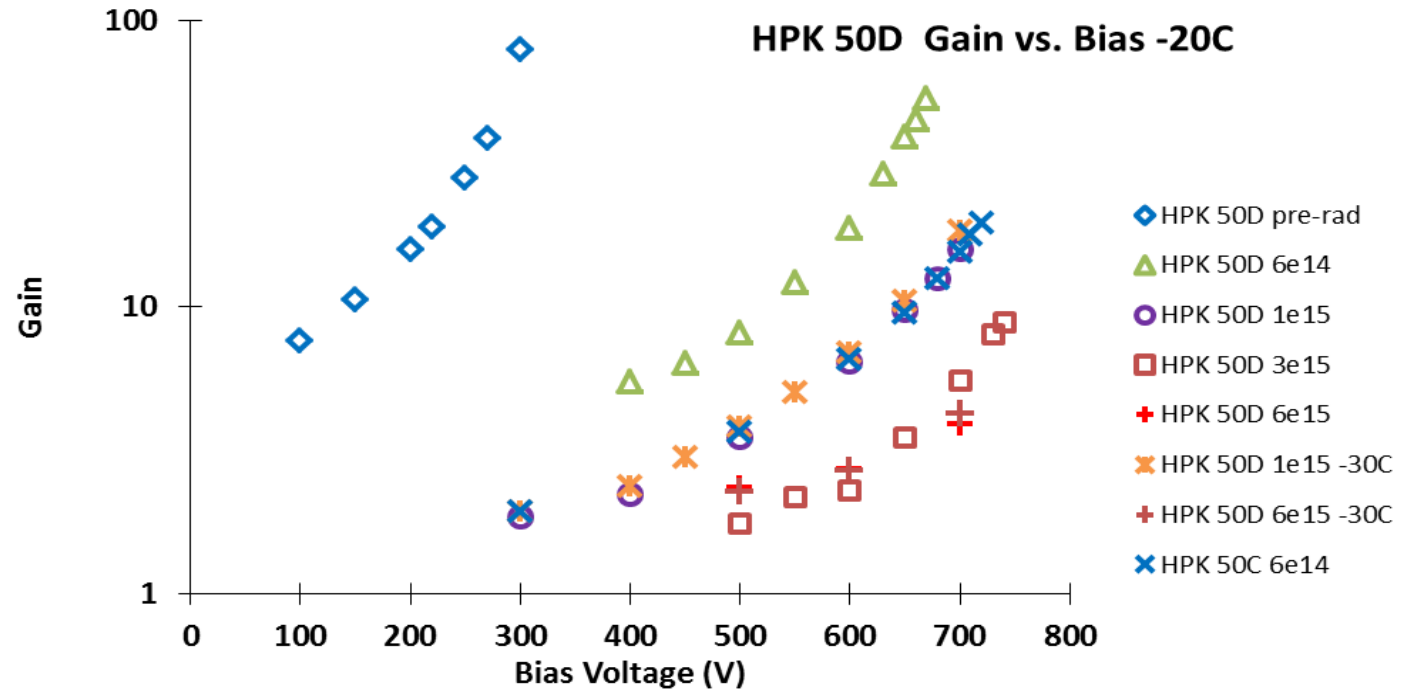
## Carbon

Interstitial defects filled with Carbon instead of with Boron and Gallium

# Effect of acceptor removal

$$N(\phi) = N(0) * e^{-c\phi}$$

Acceptor removal,  
Gain layer deactivation



To some extent, the gain layer disappearance might be compensated by increasing the bias voltage

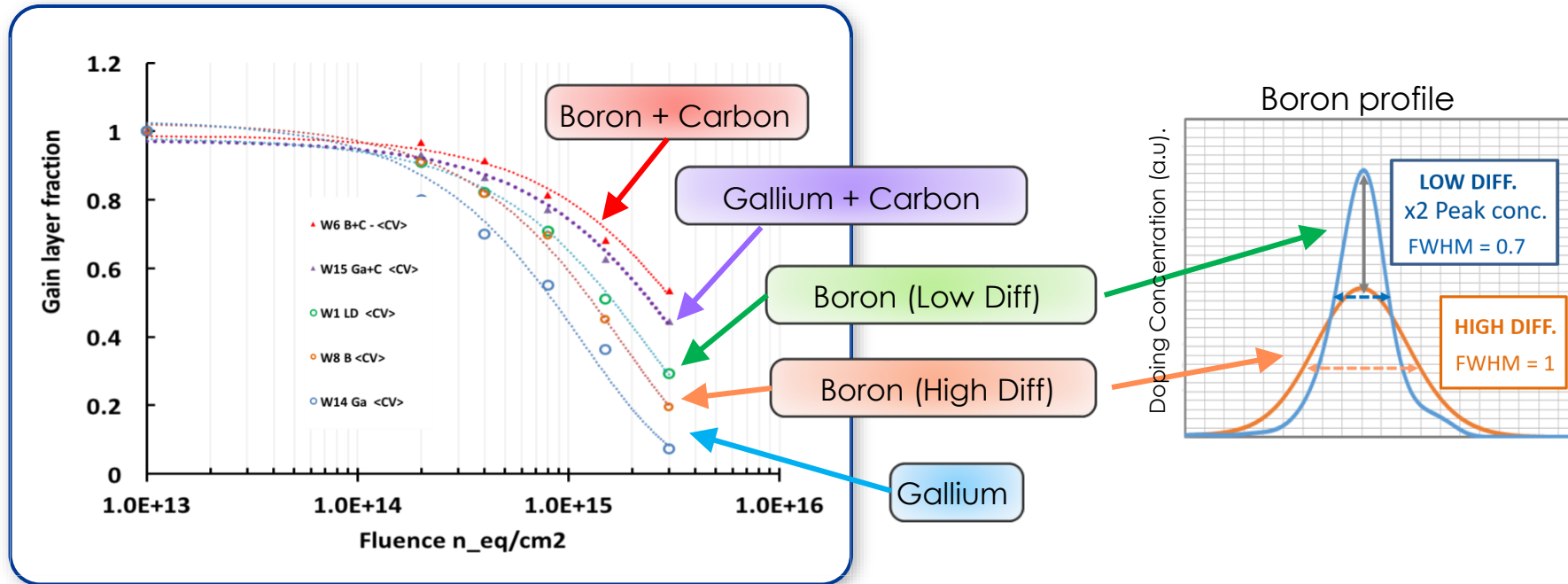
# LGAD radiation hardness improvement

## Defect Engineering of the gain implant

- **Carbon** co-implantation mitigates the gain loss after irradiation
- Replacing Boron by **Gallium** did not improve the radiation hardness

## Modification of the gain implant profile

- Narrower **Boron doping profiles** with high concentration peak (Low Thermal Diffusion) are less prone to be inactivated



# Summary so far...

---



- Low gain was introduced to compensate charge trapping
- Low gain is a key technological innovation to reach good temporal resolution with silicon detectors
- Low gain in thin silicon sensors allows reaching a temporal precision of about 30 ps (50 micron thick sensors)
- The radiation resistance of LGAD is achieved by designing a gain implant that is less sensitive to acceptor removal.
- Silicon detectors with good timing capability have been widely adopted in future experiments.
- 4D tracking is possible ONLY if sensors and electronics are designed together.

# Summary so far...

---



- Low gain was introduced to compensate charge trapping
- Low gain is a key technological innovation to reach good temporal resolution with silicon detectors
- Low gain in thin silicon sensors allows reaching a temporal precision of about 30 ps (50 micron thick sensors)
- The radiation resistance of LGAD is achieved by designing a gain implant that is less sensitive to acceptor removal.
- Silicon detectors with good timing capability have been widely adopted in future experiments.
- 4D tracking is possible ONLY if sensors and electronics are designed together.

**Can we achieved 4D tracking, i.e. 4D information in each layer of the tracker?**

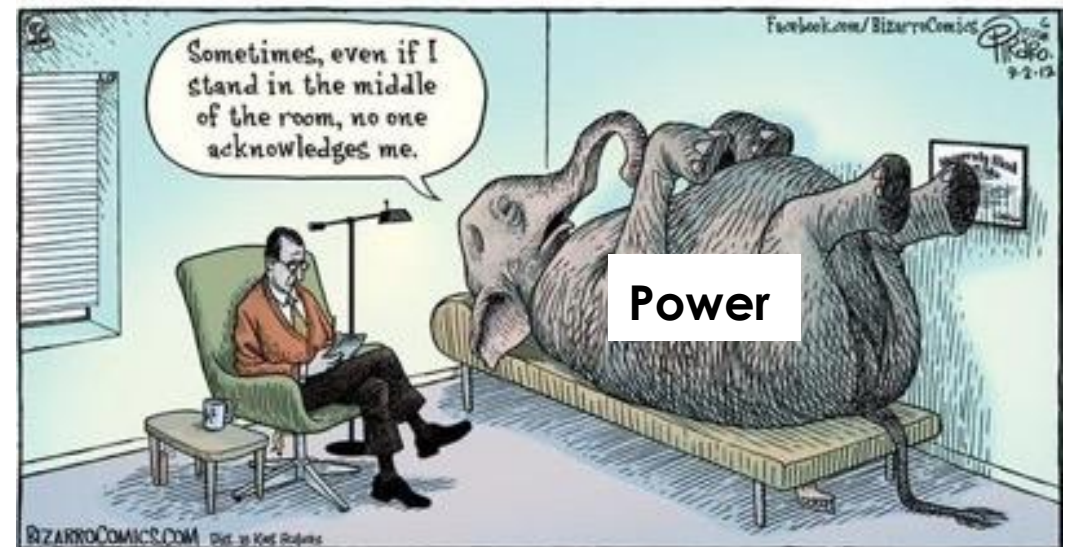


# Interplay of power, pixel size, and electronics

- The LGAD mechanism provides large signals, a fundamental component for achieving high temporal resolution.
- However: when using small pixels, the power requirement/cm<sup>2</sup> is too high

## Power will determine:

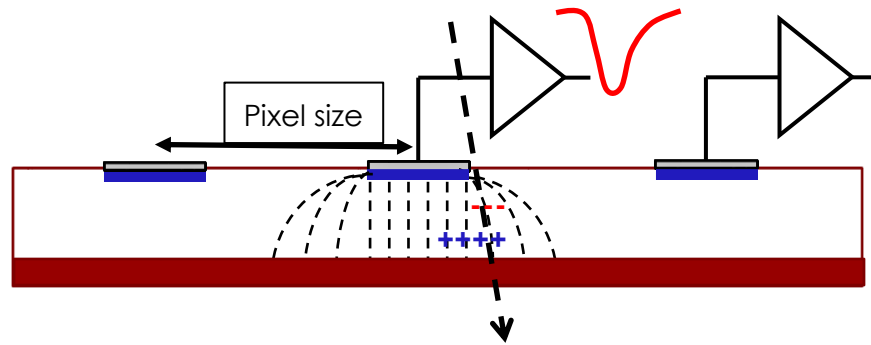
- The architecture of 4D tracking detectors
  - how many layers will be 4D and how many will be 3D
- The pixel size and the temporal precisions.



# Spatial resolution: single and multi pixels read-out

## Single pixel

where the charge is collected in one pixel

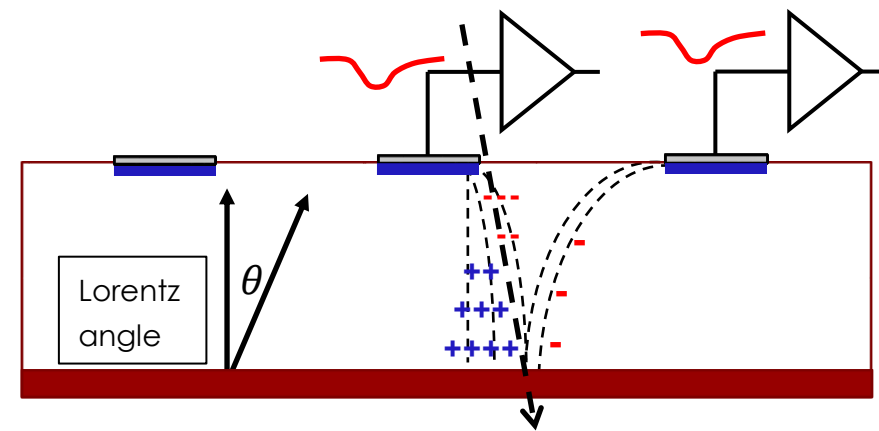


$$\sigma_x = k \frac{\text{pitch}}{\sqrt{12}}, k \sim 0.5 - 1$$

- $\sigma_x$  depend on the pixel size  
pixel = 100  $\mu\text{m}$   $\rightarrow$   $\sigma_x = 20 \mu\text{m}$

## Multi pixels

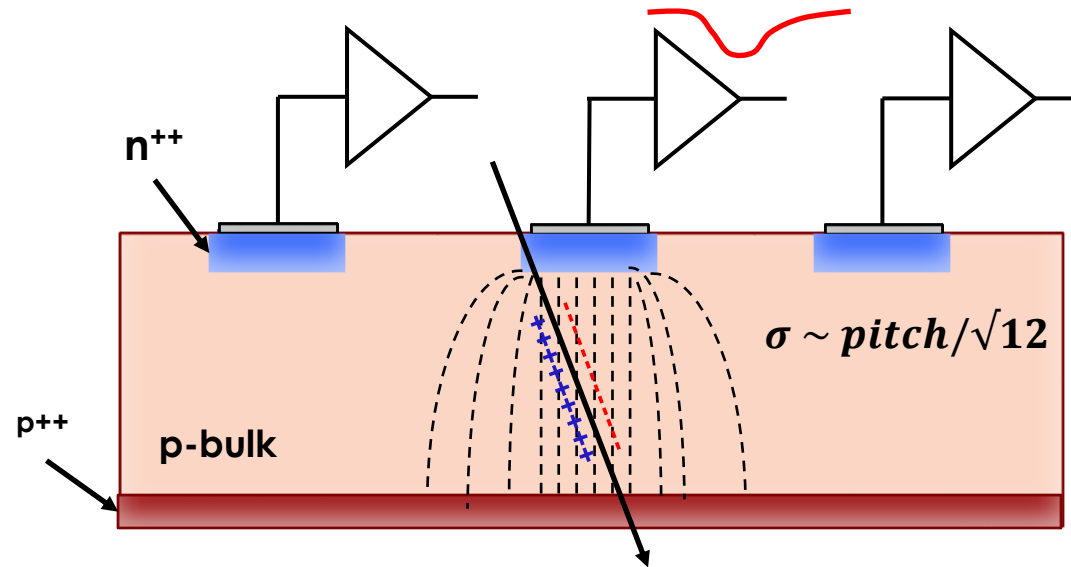
where the charge is collected in a few pixels



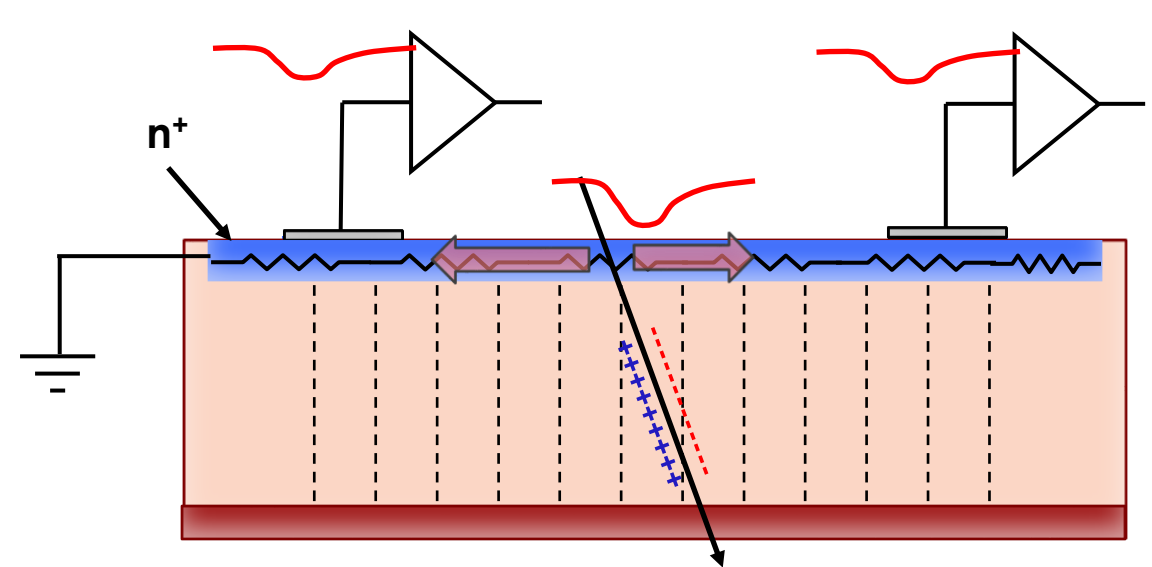
$$x_i = \frac{A_i x_i}{\sum_1^2 A_l x_l}$$

- $\sigma_x \ll$  pixel size
- Sensors have to be thick to maintain efficiency
- Need B field (or floating electrodes) to spread the signal

# Second design innovation: resistive read-out



**Silicon detector with standard read-out**

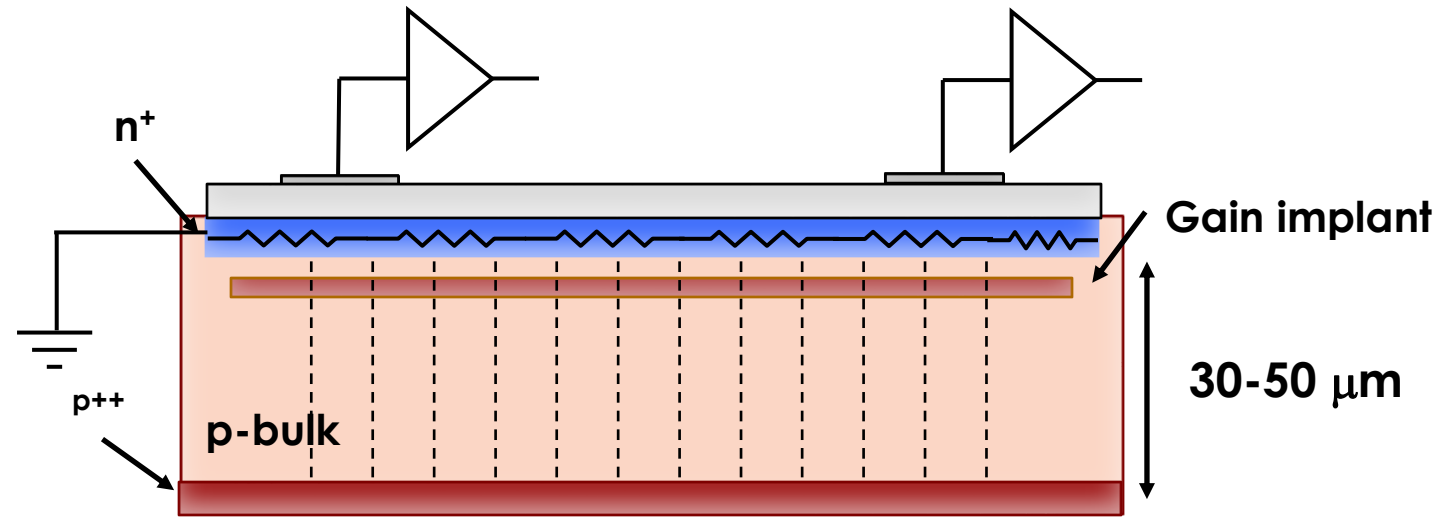


**Silicon detector with resistive read-out**

- In resistive read-out, instead of many p-n diodes, there is a single diode.
- The n-doped implant is resistive and acts as a signal divider
- Very uniform Electric and Weighing fields

**Signal sharing is the key ingredient to excellent spatial resolution**

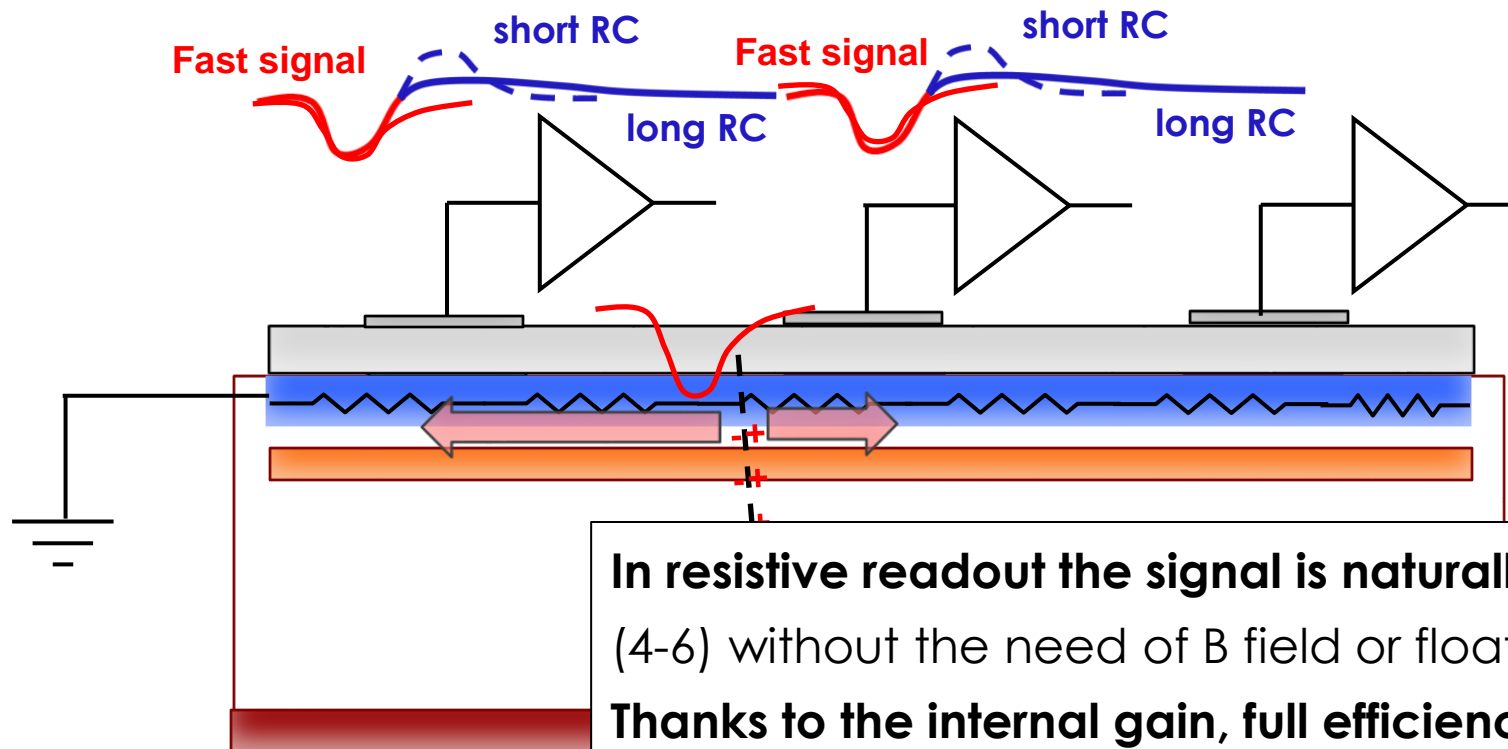
# Resistive Silicon Detector (RSD)



**Resistive Silicon Detectors**  
combine low-gain and resistive read-out

# Signal formation and sharing in RSD

- The signal is formed on the n+ electrode ==> no signal on the AC pads
- The AC pads offer the smallest impedance to ground for the fast signal
- The signal discharges to ground



**In resistive readout the signal is naturally shared among pads (4-6) without the need of B field or floating pads**

**Thanks to the internal gain, full efficiency even with sharing**

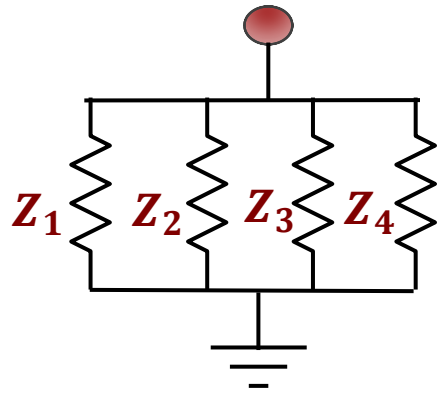
**Results presented here are from the FBK RSD1 production**

(INFN grant "giovani" RSD, PI M. Mandurrino)

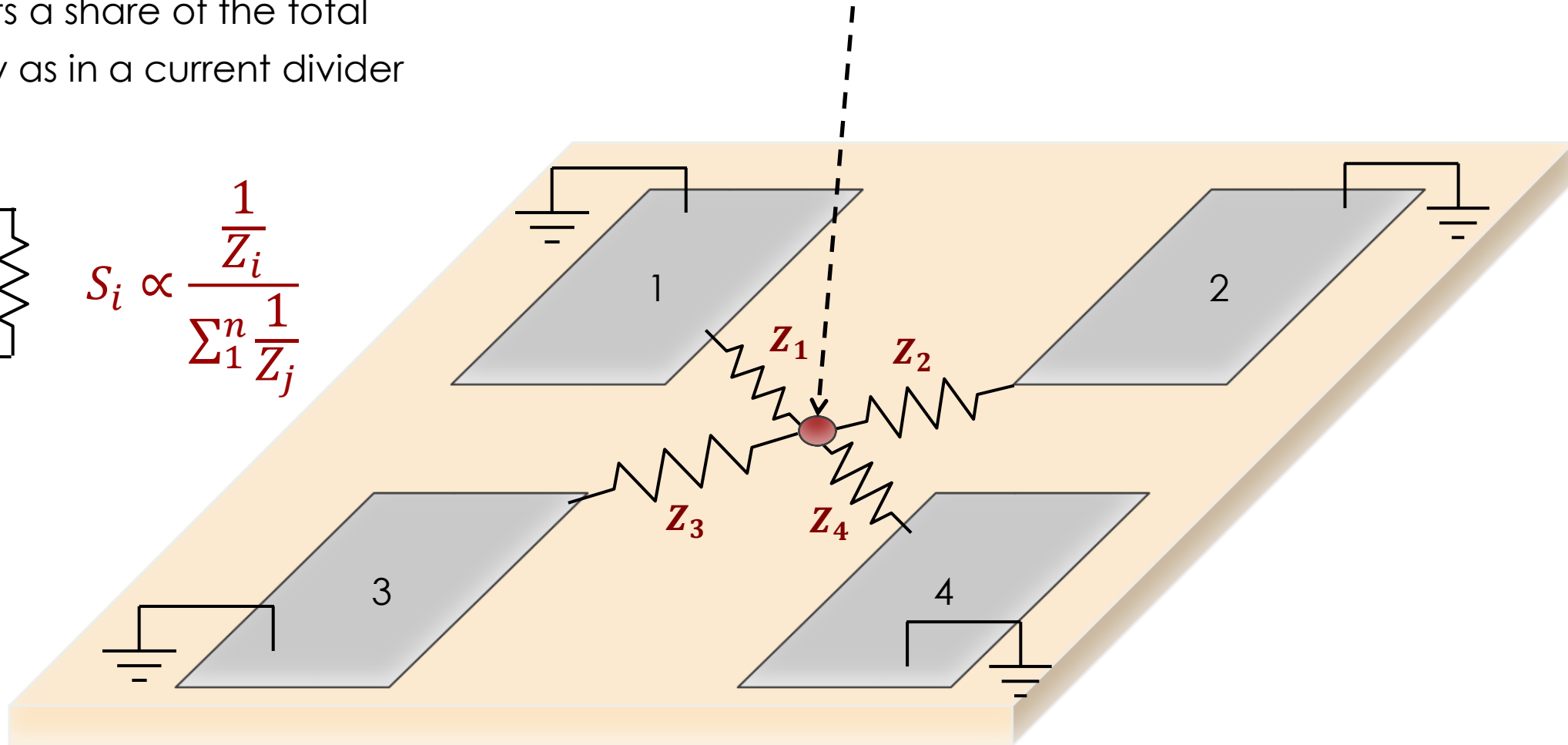
# Charge sharing in RSD

The signal sees several impedances in parallel, and it is split according to Ohm's law.

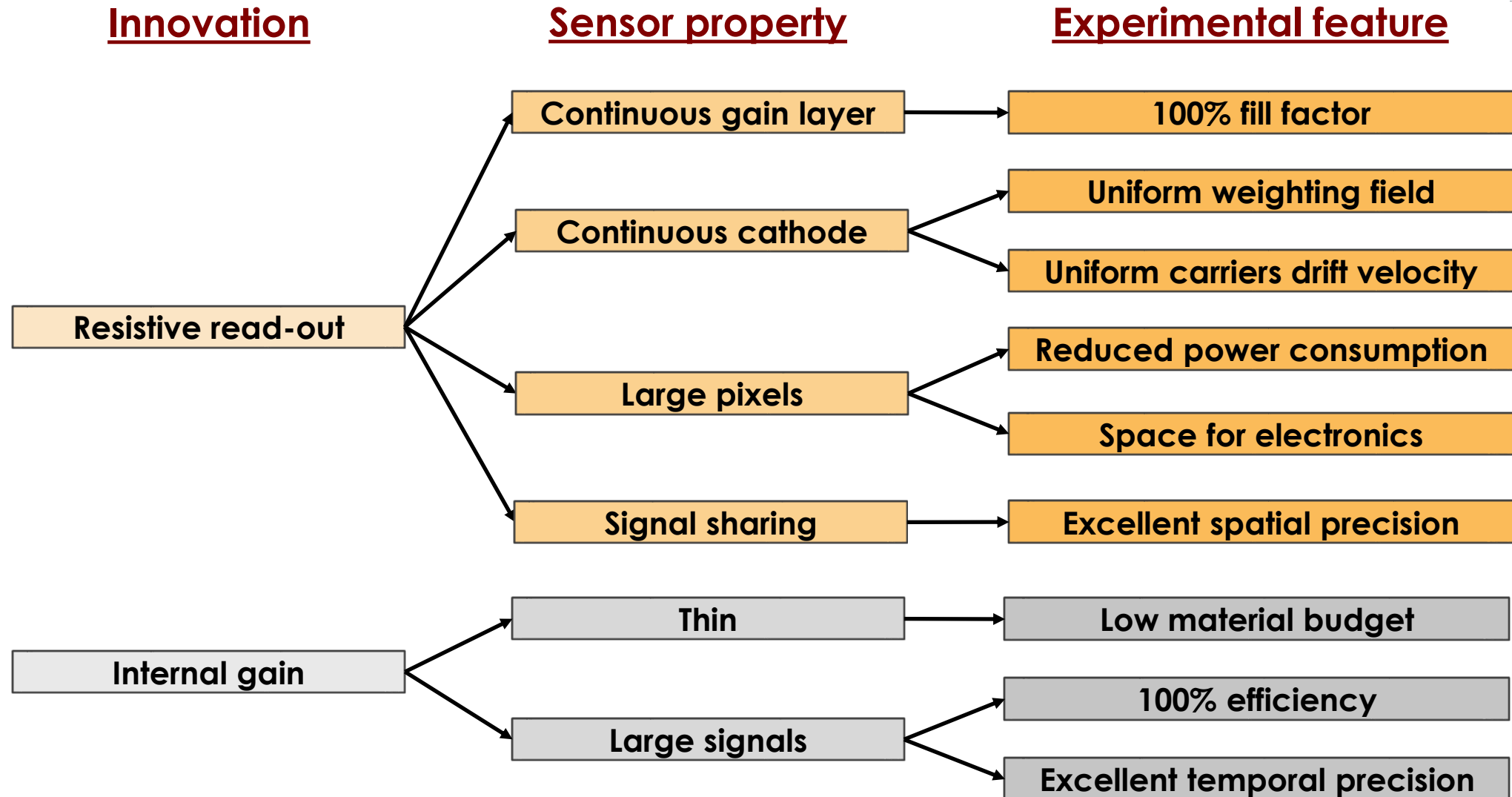
Each pad gets a share of the total signal, exactly as in a current divider



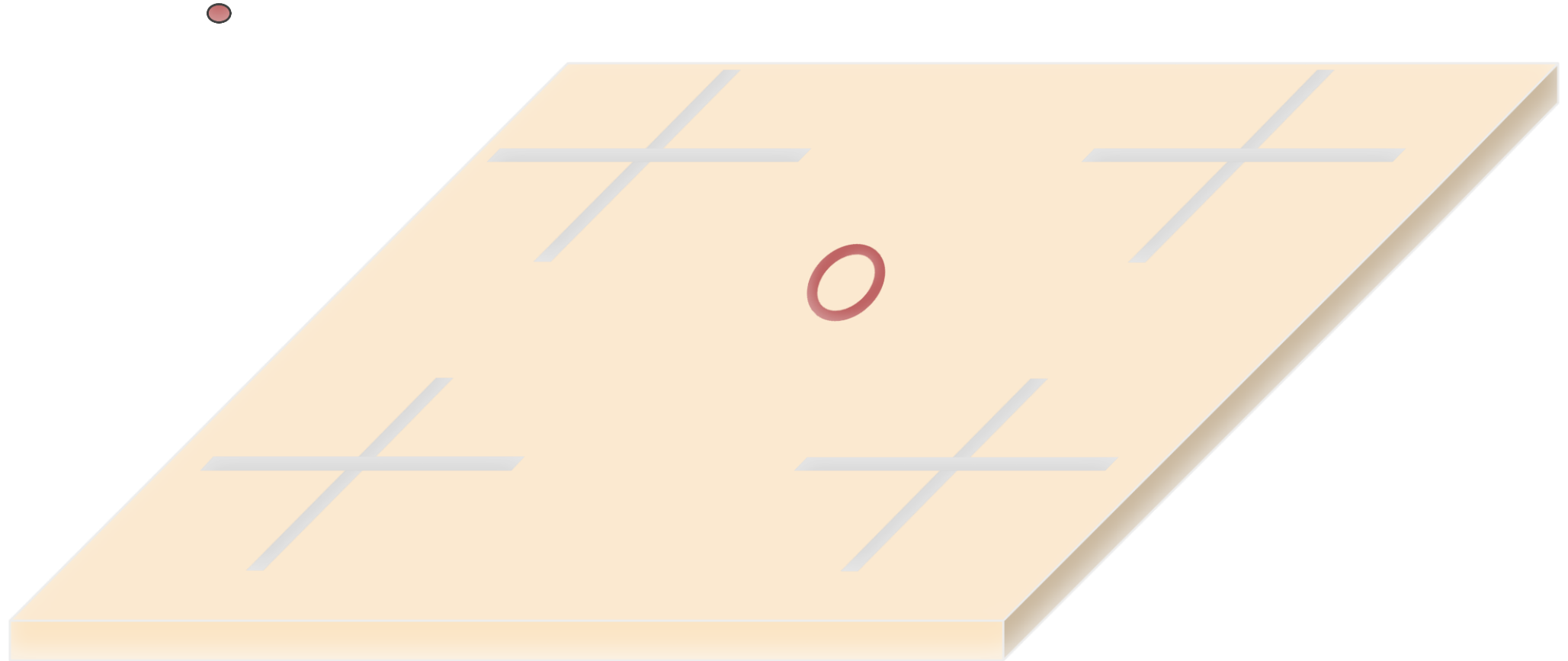
$$S_i \propto \frac{1}{Z_i} \frac{1}{\sum_{j=1}^n \frac{1}{Z_j}}$$



# Why are RSDs well-suited for 4D tracking?

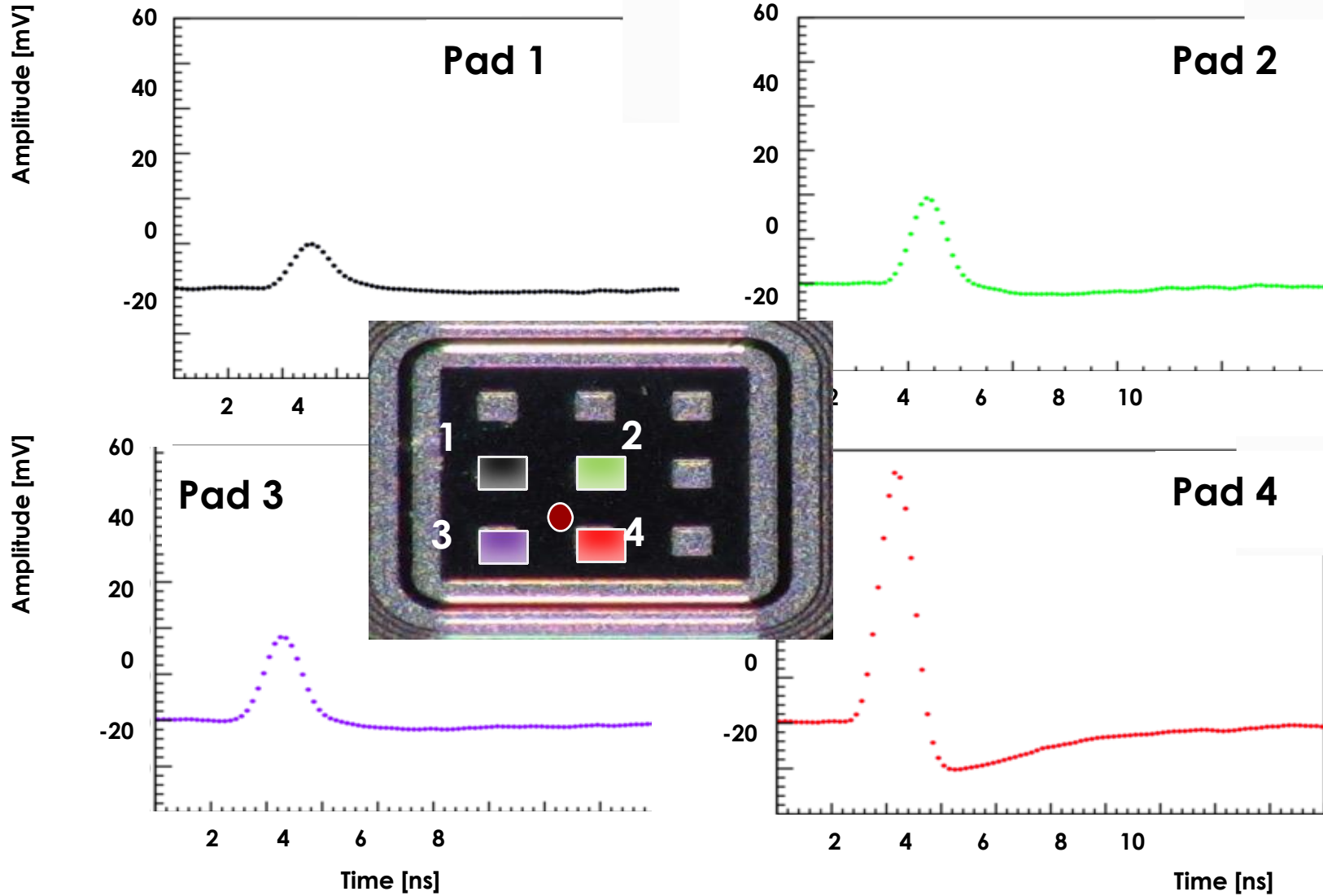


# RSD principle of operation in motion





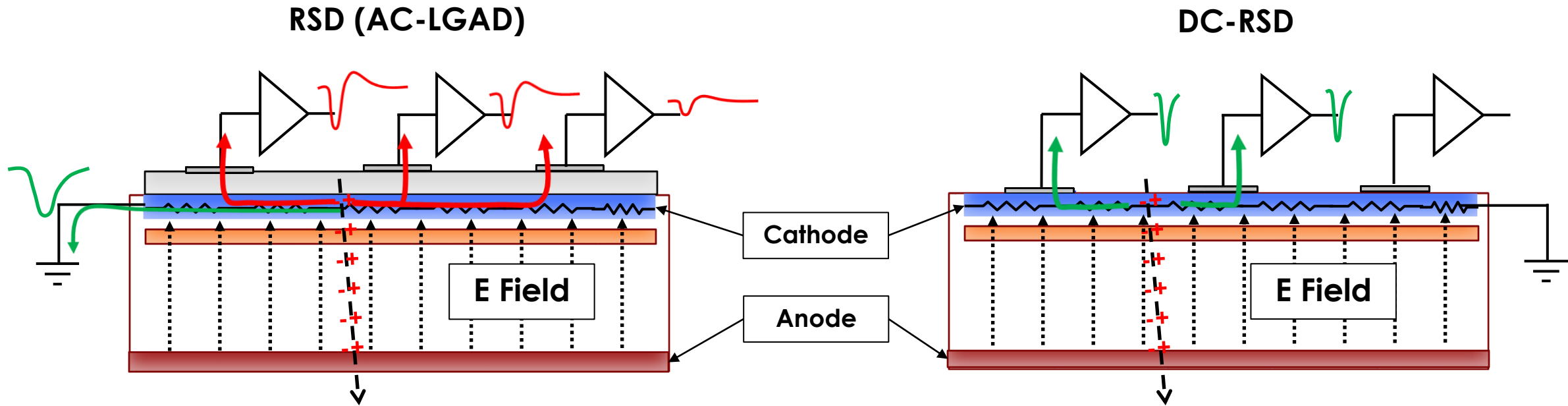
# Example of signal sharing



50-mm thick RSD,  
Gain ~ 20

The laser is shot at the position of the red dot: the signal is seen in 4 pads

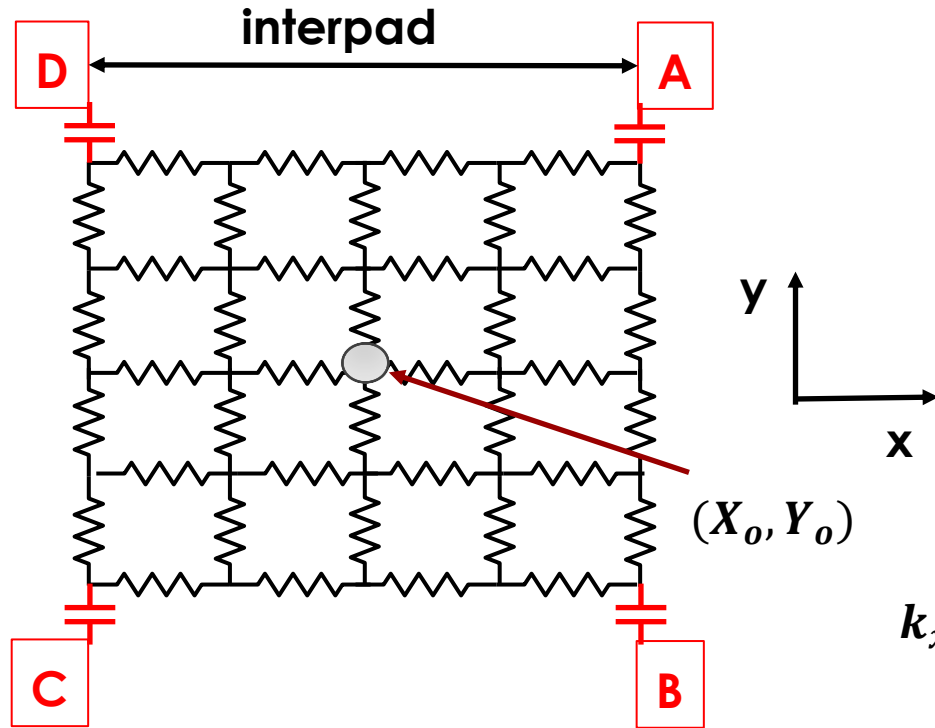
# Present RSD research paths



This design has been manufactured in several productions by FBK, BNL, and HPK

This design is presently under development by FBK  
The main advantage of the DC-RSD design is the ability to control the signal spread

# RSD as a Discretized Positioning Circuit



$$X = X_o + k_x \left( \frac{Q_A + Q_B - Q_C - Q_D}{Q_A + Q_B + Q_C + Q_D} \right)$$

$$Y = Y_o + k_y \left( \frac{Q_A + Q_D - Q_B - Q_C}{Q_A + Q_B + Q_C + Q_D} \right)$$

$$k_x = \frac{\text{interpad}}{2} * \frac{\alpha_x}{\left( \frac{Q_A + Q_D - Q_B - Q_C}{Q_A + Q_B + Q_C + Q_D} \right)_{x=X_o + \frac{\text{Interpad}}{2}, y=Y_o}}$$

RSD is a hybrid resistors/capacitors DPC circuit

The reconstruction method uses only the signals in the 4 pads to reconstruct the hit position

➔ no need for an analytical sharing law.

➔  $k_{x,y}$  = imbalance parameter along x or y

- Maximum value of the charge imbalance within the pixel
- Needs to be determined experimentally for each geometry

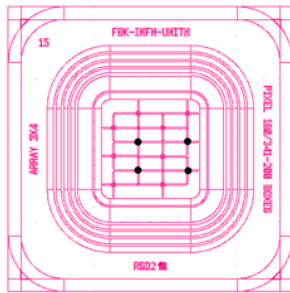
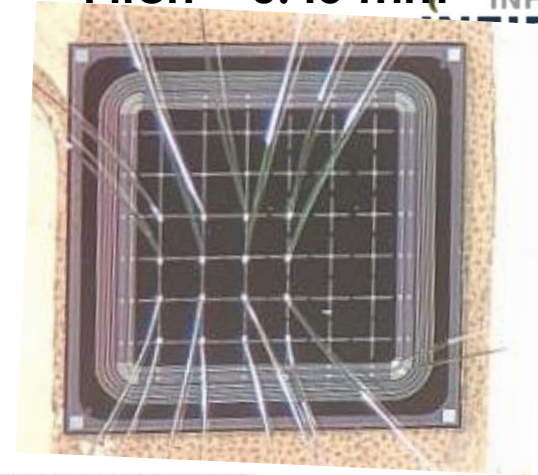
# RSD2 sensors with cross-shaped electrodes



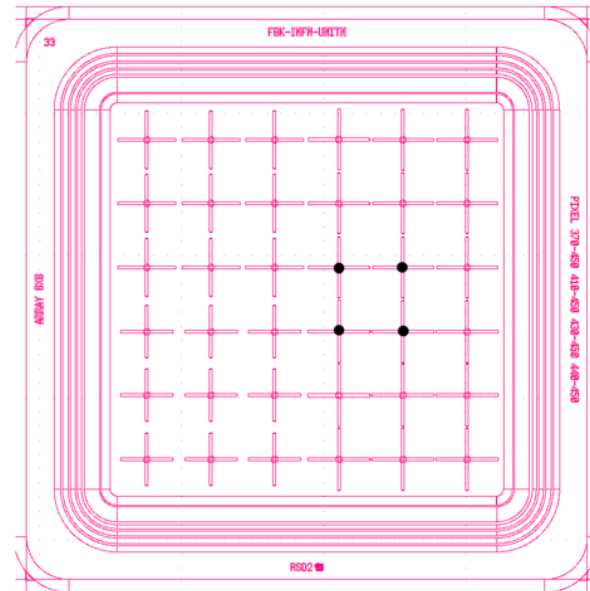
Sensor production at Fondazione Bruno Kessler

Several geometries are explored in RSD2, for example cross with different pitch and arm length: 200, 340, 450, and 1300  $\mu\text{m}$

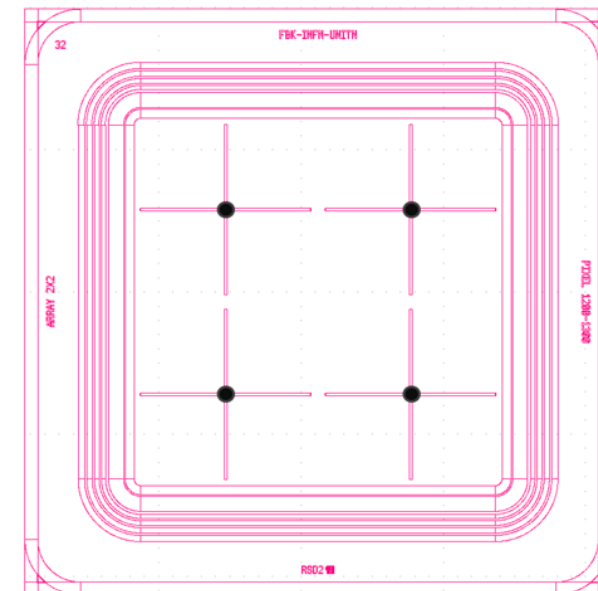
Pitch = 0.45 mm



(A)  
200 x 340  $\mu\text{m}^2$

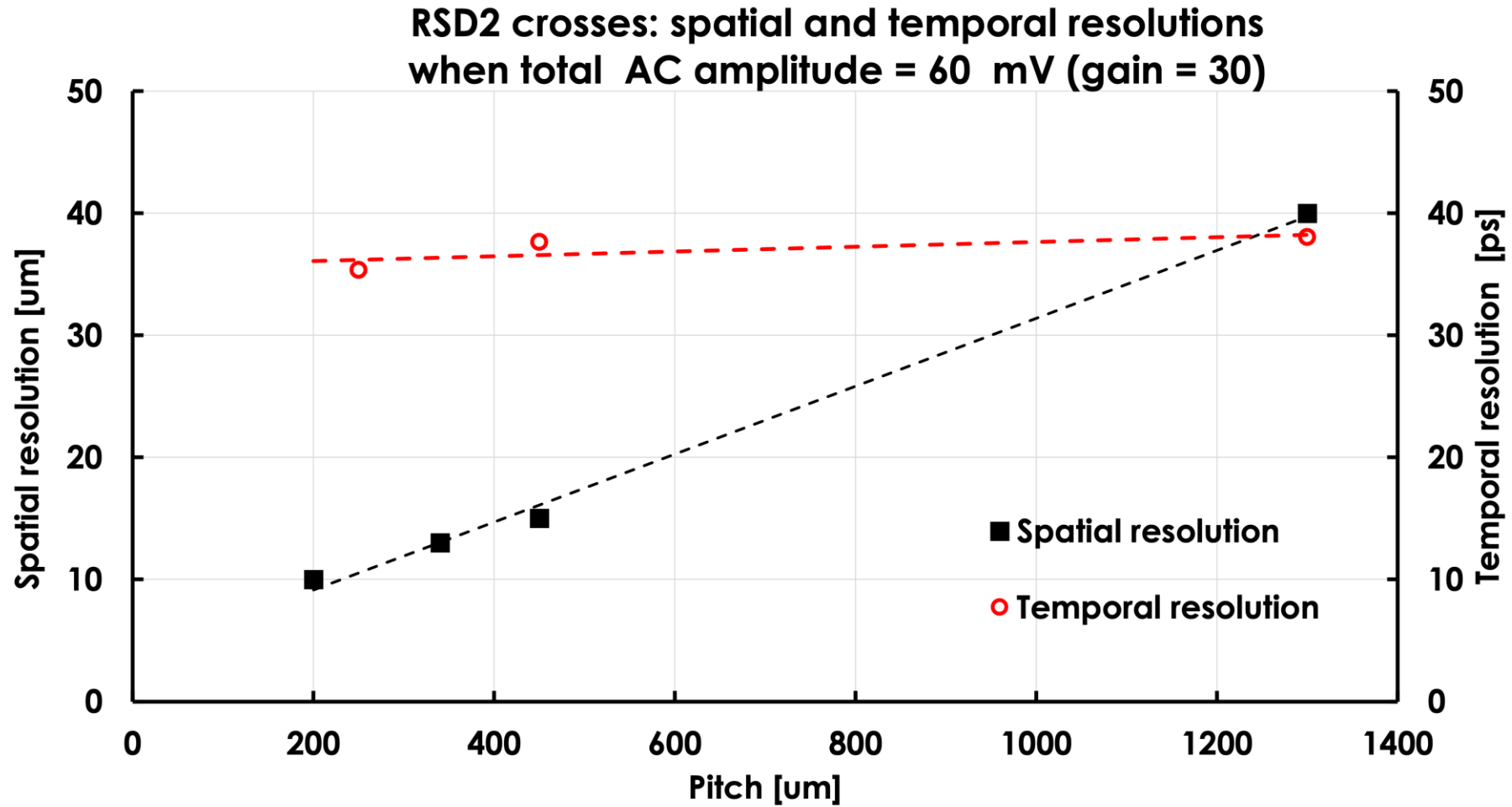


(B)  
Pitch = 450  $\mu\text{m}$



(C)  
Pitch = 1300  $\mu\text{m}$

# FBK-RSD2 performance summary



# Limiting the signal spread to a single cell

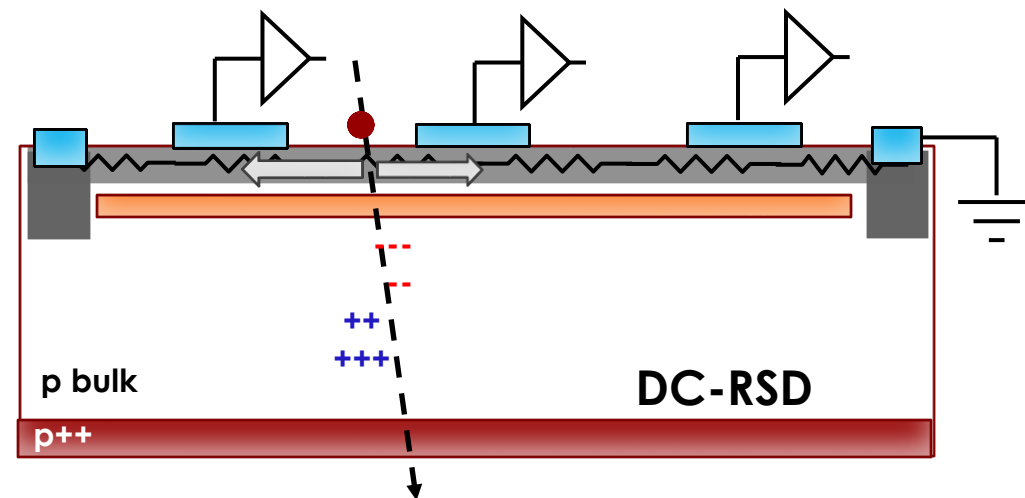
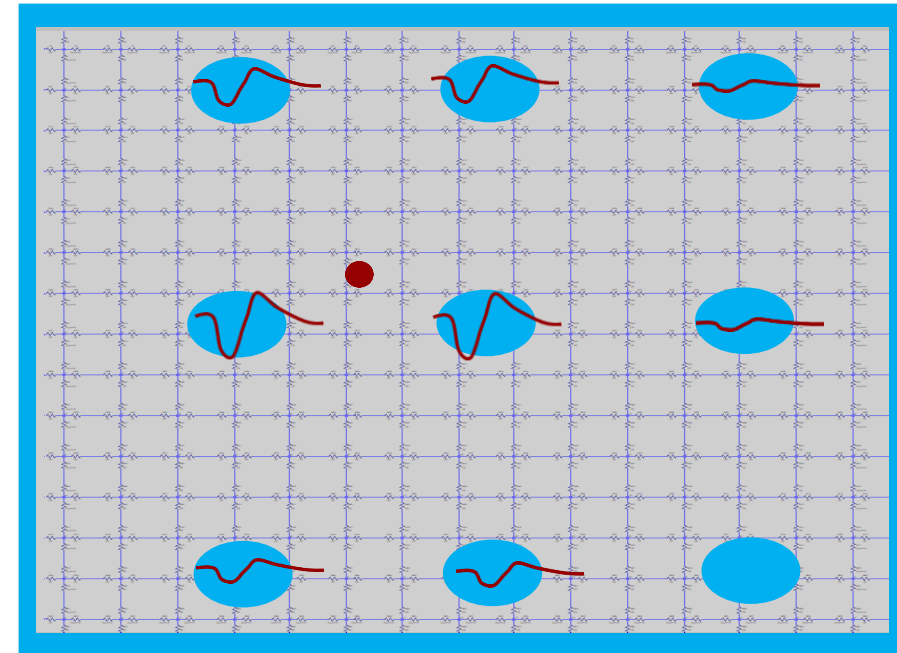
Top view

## Problem:

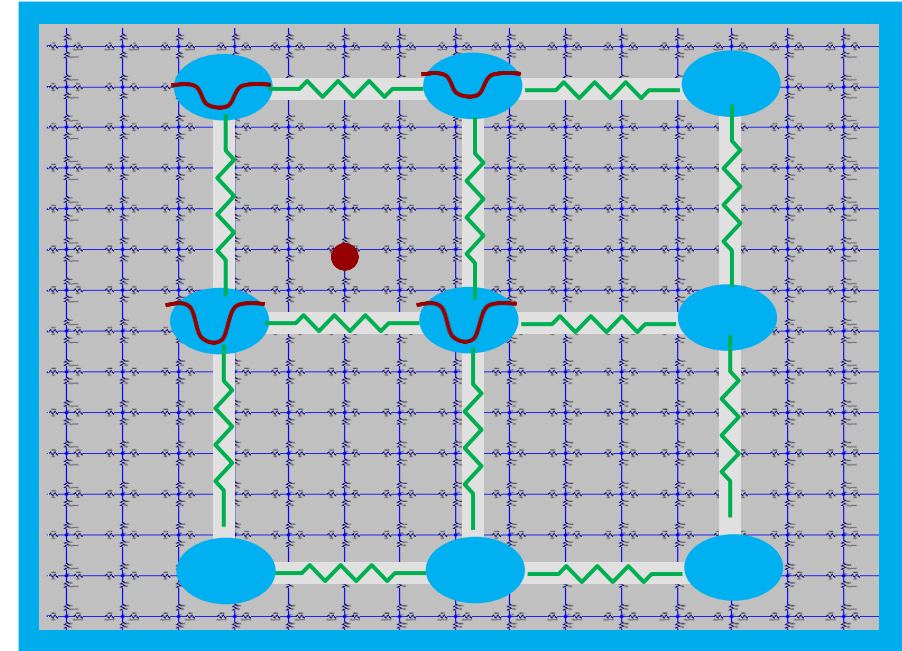
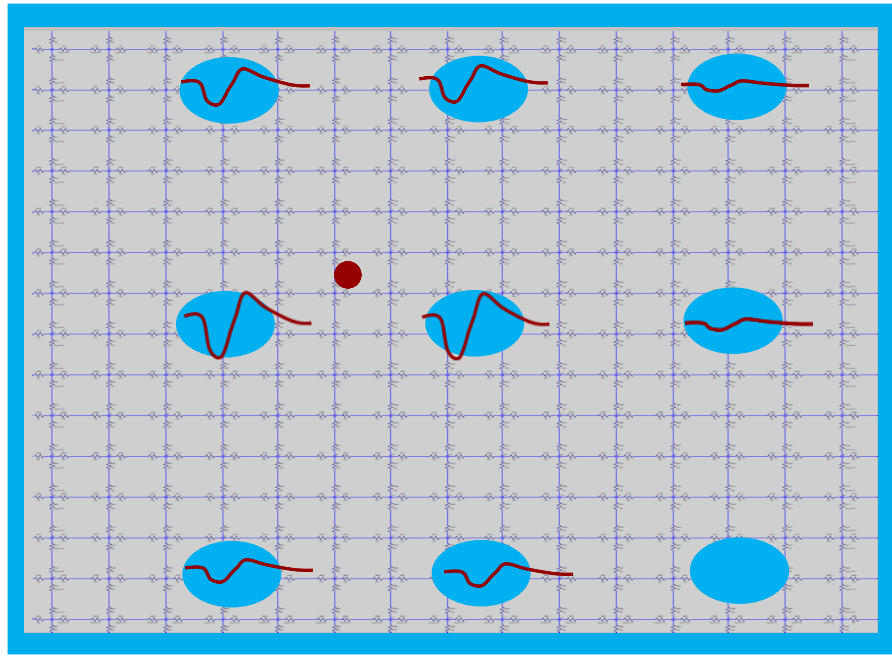
we have been too successful in charge sharing.

In our measurements, the signal is shared on too many electrodes.

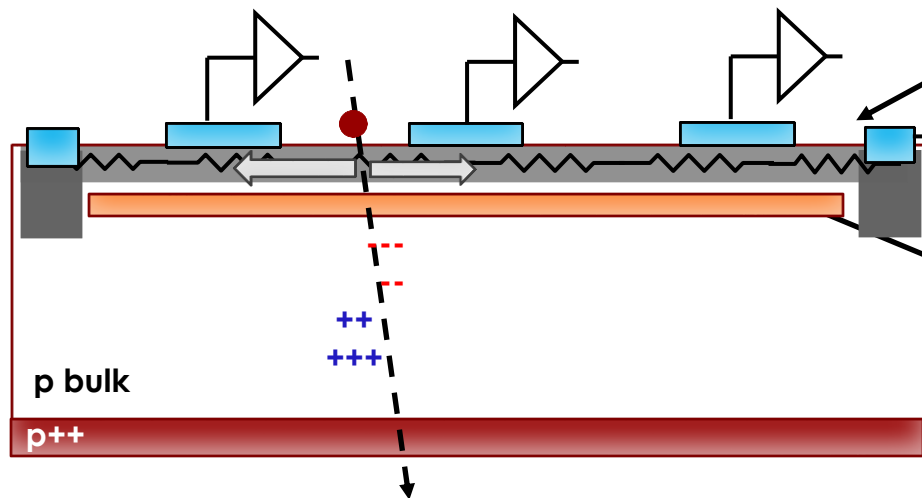
**If the signal is shared on too many electrodes, the signal-to-noise ratio is degraded**



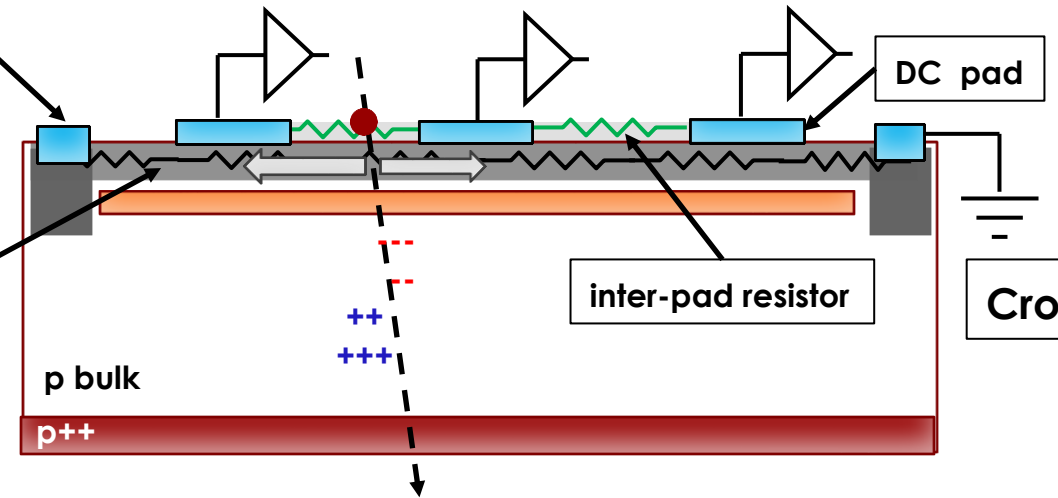
# Adding resistors in between electrodes



Top view



DC-RSD



Crosscut

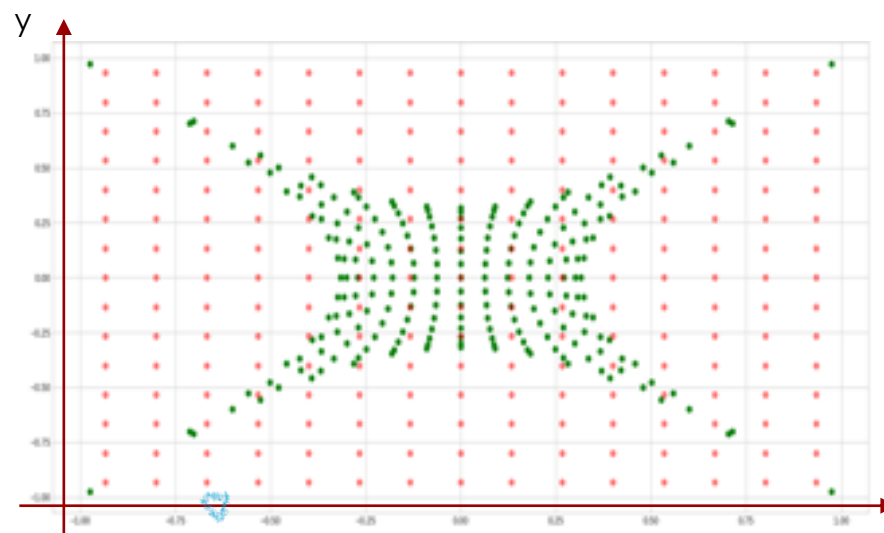
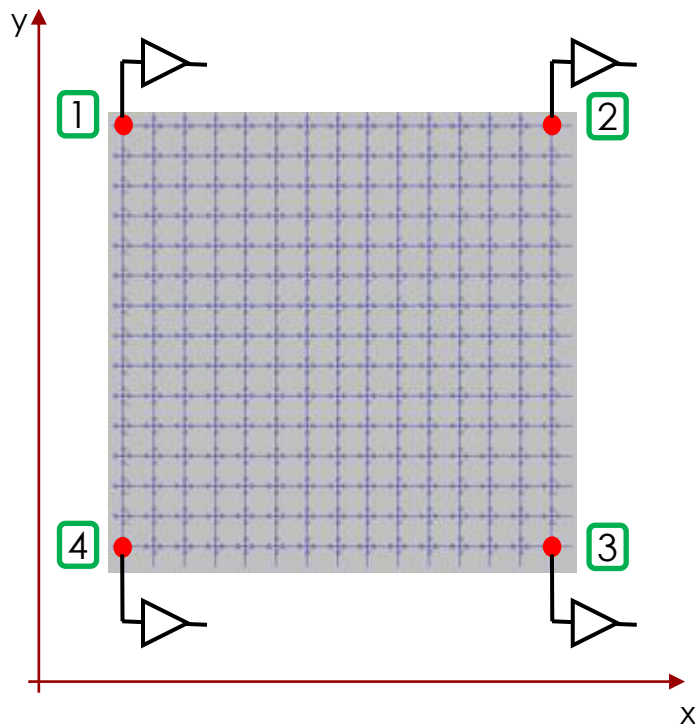
DC-RSD

# Position Reconstruction: DC-RSD

Position distortion is typical of resistive devices and well documented in the literature.

$$x_i = x_{center} + k_x \frac{pitch}{2} * \frac{Q_3 + Q_4 - (Q_1 + Q_2)}{Q_{tot}}$$

$$y_i = y_{center} + k_y \frac{pitch}{2} * \frac{Q_1 + Q_3 - (Q_2 + Q_4)}{Q_{tot}}$$



Red  
original points

Green  
reconstructed points

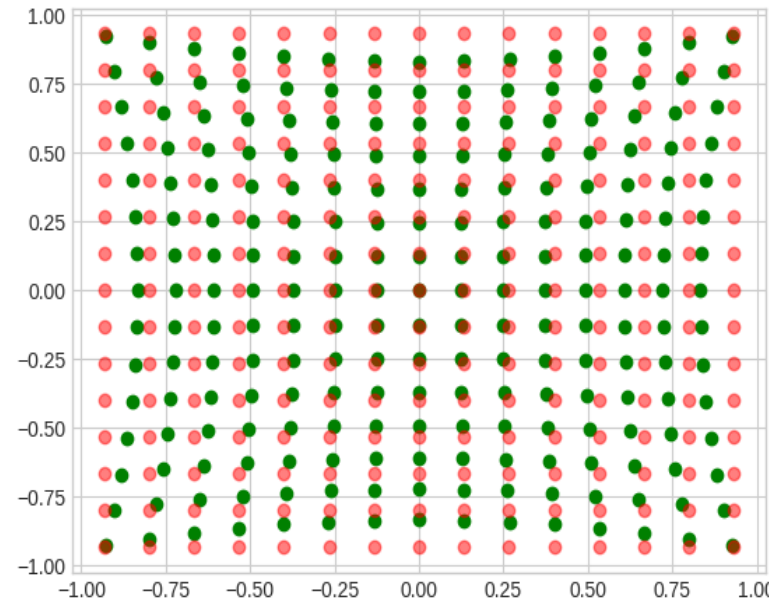
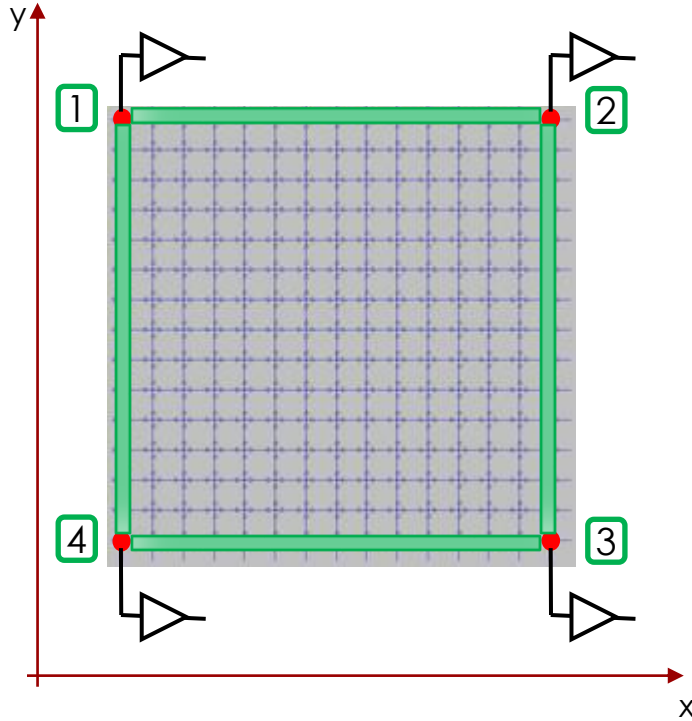
**This is an extreme case, chosen to illustrate the problem**



# Position Reconstruction: DC-RSD with resistive strip

$$x_i = x_{center} + k_x \frac{pitch}{2} * \frac{Q_3 + Q_4 - (Q_1 + Q_2)}{Q_{tot}}$$

$$y_i = y_{center} + k_y \frac{pitch}{2} * \frac{Q_1 + Q_3 - (Q_2 + Q_4)}{Q_{tot}}$$



Red  
original points

Green  
reconstructed  
points

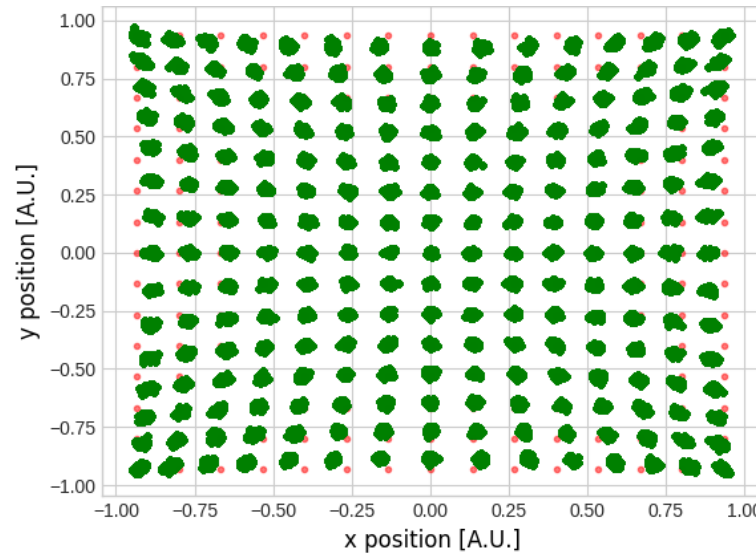
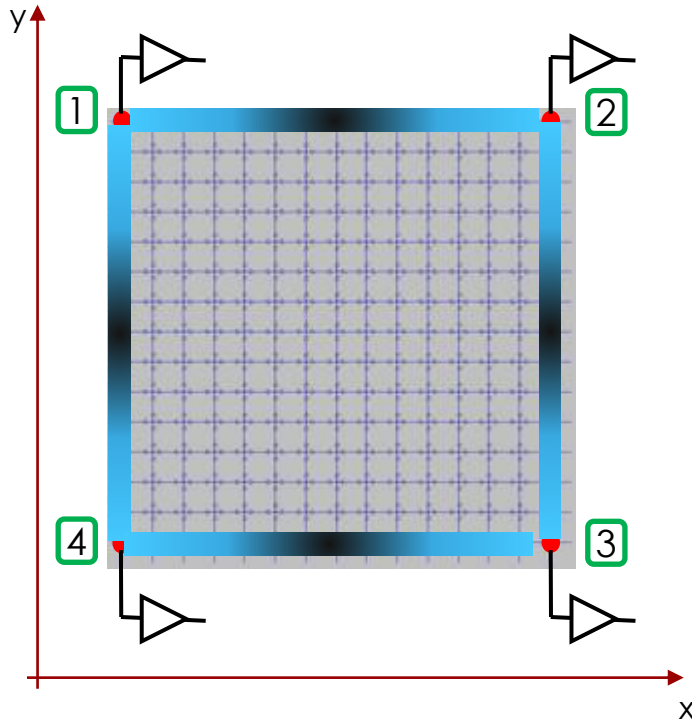
The distortion in the reconstruction can be strongly reduced by adding resistive strips connecting the electrodes.

**Proposed in:** *On the dynamic two-dimensional charge diffusion of the interpolating readout structure employed in the MicroCAT detector*, Wagner et al., NIM A, (2002).

# Position Reconstruction: DC-RSD with variable resistive strip

$$x_i = x_{center} + k_x \frac{pitch}{2} * \frac{Q_3 + Q_4 - (Q_1 + Q_2)}{Q_{tot}}$$

$$y_i = y_{center} + k_y \frac{pitch}{2} * \frac{Q_1 + Q_3 - (Q_2 + Q_4)}{Q_{tot}}$$



Red  
original points

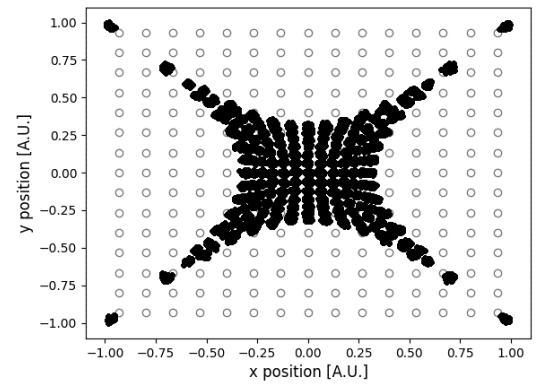
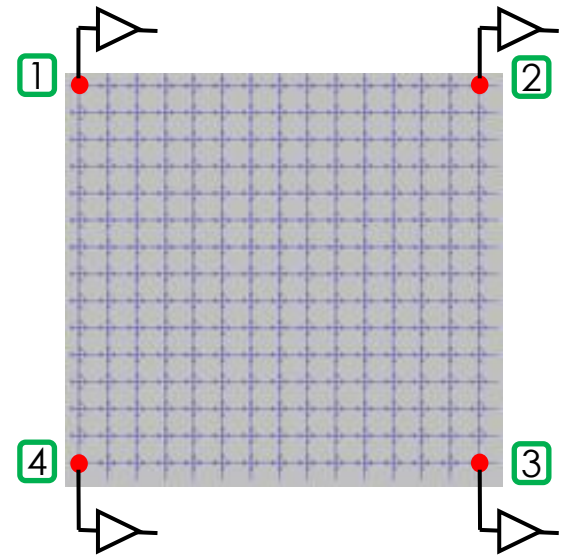
Green  
reconstructed  
points

Variable resistive strips have the potential to almost totally eliminate the distortion in the position reconstruction

# DC-RSD research paths

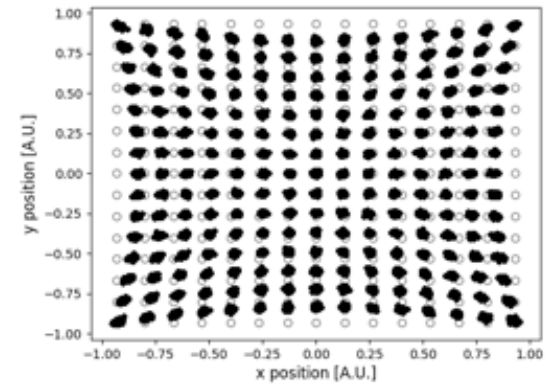
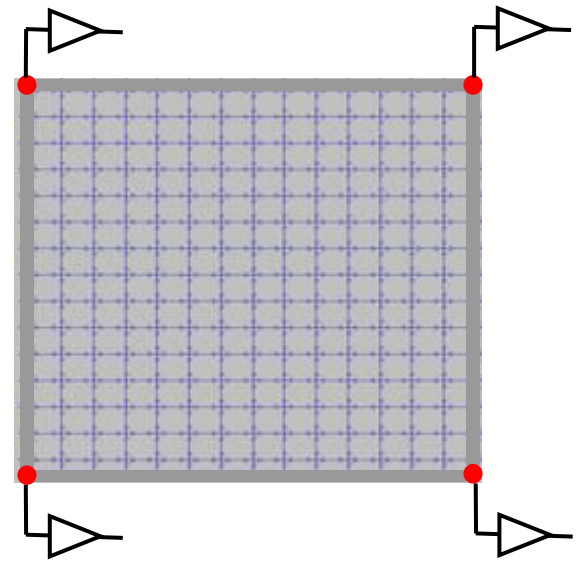


### DC-RSD



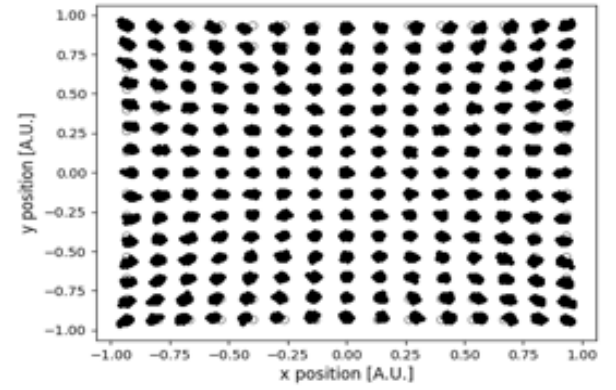
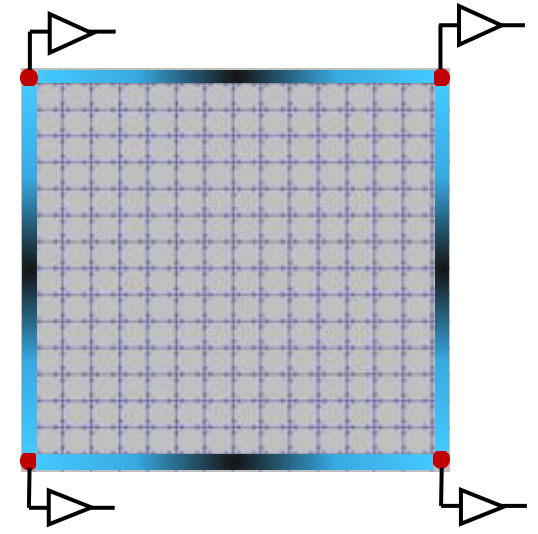
### DC-RSD

#### with resistive strips



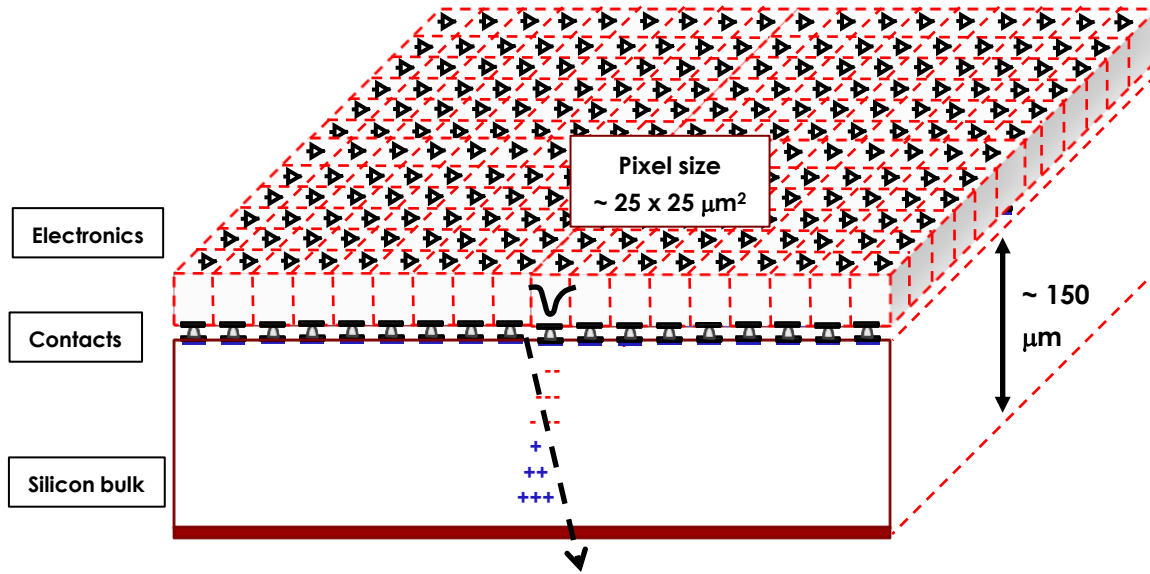
### DC-RSD

#### with variable resistive strips

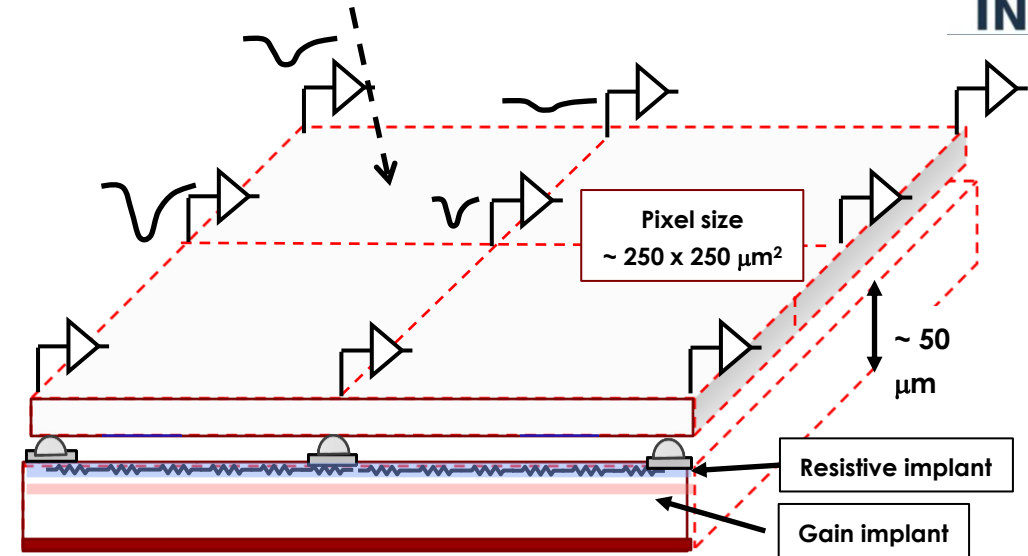


**Empty circles:** original points  
**Filled Circles:** reconstructed points

# Final goal of RSD R&D: a completely new tracker



**Standard Tracker**



**RSD-based tracker**

**The design of a tracker based on RSD is truly innovative:**

- It delivers  $\sim 20$  - $30$  ps temporal resolution
- For the same spatial resolution, the number of pixels is reduced by 50-100
- The electronic circuitry can be easily accommodated
- The power consumption is much lower; it might even be air-cooled ( $\sim 0.1$ - $0.2$  W/cm<sup>2</sup>)
- The sensors can be really thin

# RSD Read-out scheme

## Signal characteristics:

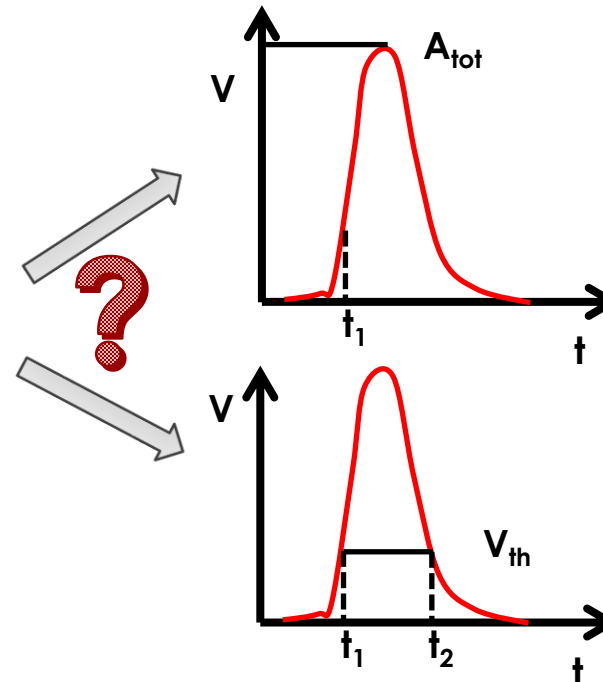
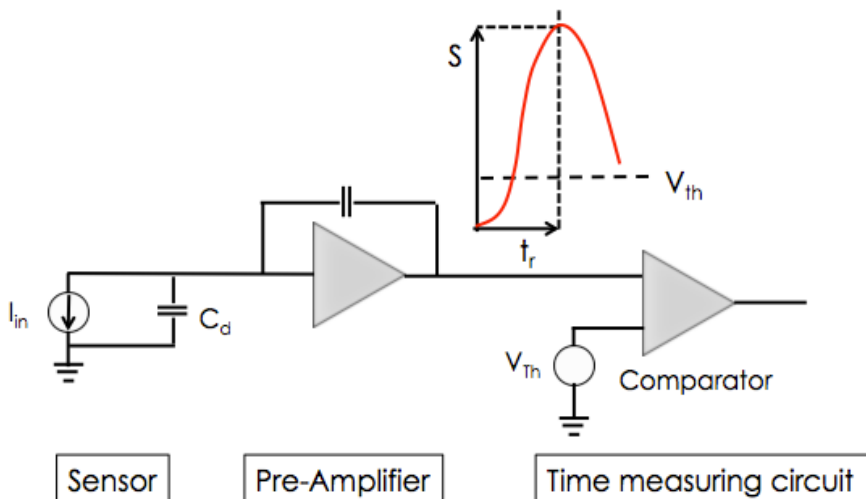
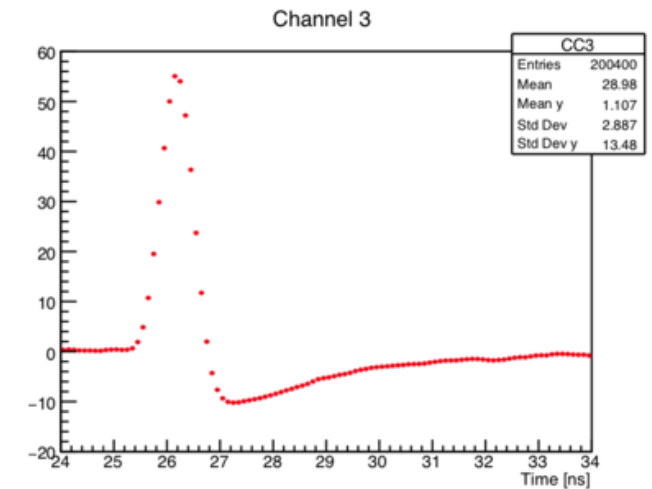
- Short and fast, very similar to standard UFSD

## Read-out characteristics:

- Record signal amplitude with good precision for position
- Timing capabilities: keep the jitter below the Landau floor

$$BW \sim 500 \text{ MHz}, Q_{in} \sim 5 - 10 fC$$

→ A Leading edge discriminator with linear Time-over-Threshold information or/and a DAC for amplitude measurement



## Time of Arrival and Amplitude:

$$t_1, A_{tot}$$

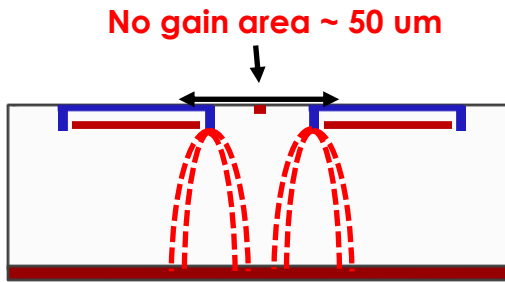
TDC for  $t_1$ ,  
ADC for  $A_{tot}$

## Time over Threshold:

$$ToT = t_2 - t_1$$

Need TDC for  $t_1, t_2$

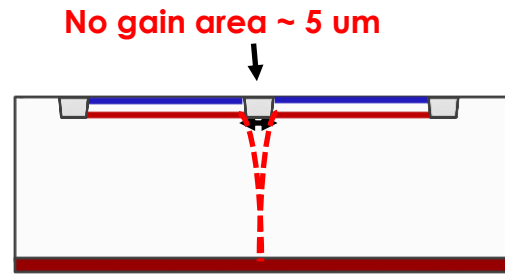
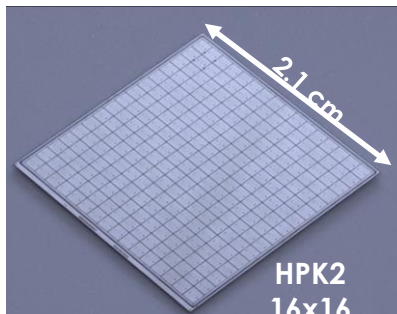
# UFSD Summary: more gaining and more sharing



JTE + p-stop design

## JTE/p-stop UFSD

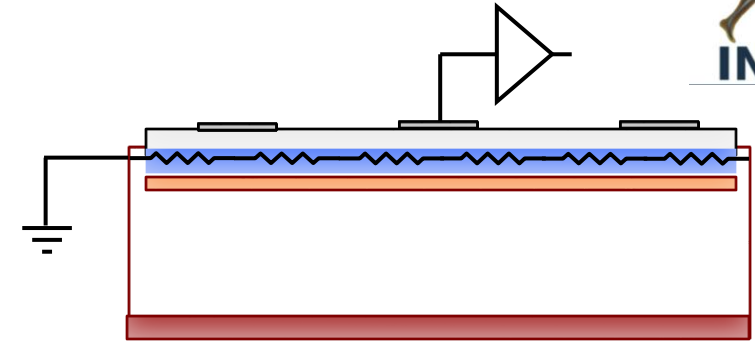
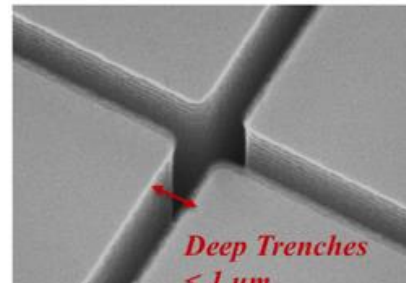
- CMS & ATLAS choice
- Signal in a single pixel
- Not 100% fill factor
- Very well tested
- High Occupancy OK
- Rate ~ 50-100 MHz
- Rad hardness ~ 2-3E15 n/cm2



Trench-isolated design

## UFSD evolution: use trenches

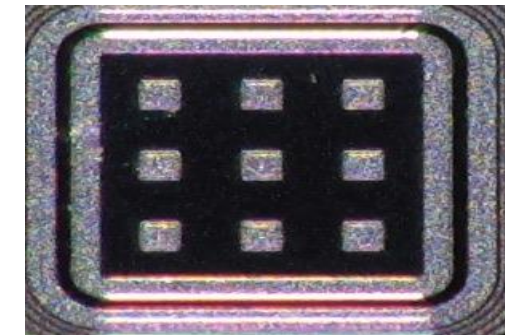
- Signal in a single pixel
- Almost 100% fill factor
- Temporal resolution (50  $\mu\text{m}$ ) : 35-40 ps
- High Occupancy OK
- Rate ~ 50-100 MHz
- Rad hardness: to be studied



RSD -- AC-LGAD

## RSD evolution: resistive readout

- Signal in many pixels
- 100% fill factor
- Excellent position resolution: ~ 5  $\mu\text{m}$  with large pixels
- Temporal resolution (50  $\mu\text{m}$ ) : 35-40 ps
- Rate ~ 10-50 MHz
- Rad hardness: to be studied



# Conclusions

The combination of internal multiplication and built-in charge sharing leads to the design of a new type of silicon tracker.

Resistive read-out && LGAD can be used both in hybrid and monolithic sensors

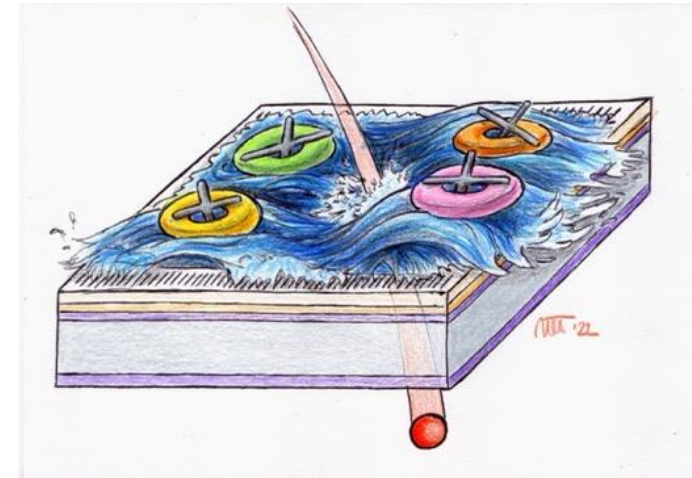
The pixel size can be quite large given the very good spatial resolution. Limitations might be introduced by occupancy.

Spatial resolution depends upon  $\sim 1/\text{gain}$ ,  $\sim 1/\text{pitch}$ , and  $\sim \text{noise}$

The temporal resolution is weakly dependent on the pixel size

Our laboratory measurements yield to (at gain = 30)

- a spatial resolution of about 3% of the pixel size
- a temporal resolution similar (but marginally worse) than that of standard LGADs



# Backup

---





# Spatial resolution in resistive readout

$$\sigma_x^2 = \sigma_{Jitter}^2 + \sigma_{Sensor}^2 + \sigma_{Reconstruction}^2$$

$$\sigma_{Jitter} = \frac{\sigma_{El\_noise}}{\frac{dV}{dx}}$$

## Electronic noise

Assume a geometry with only 2 pads:

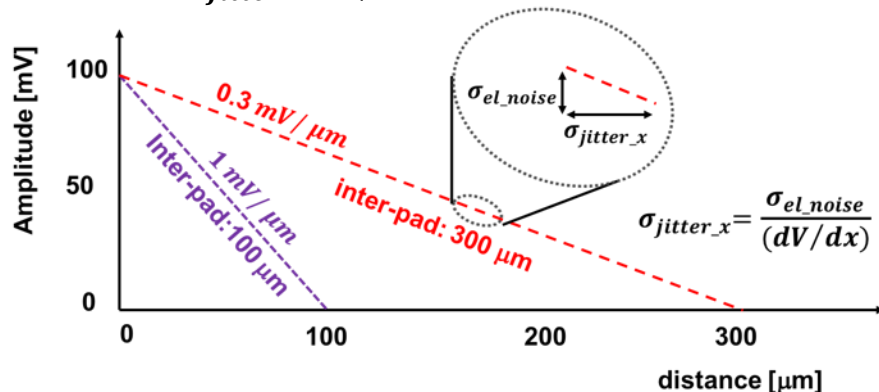
- 100  $\mu\text{m}$  and 300  $\mu\text{m}$  apart
- 100mV signal
- 3 mV electronic noise

**100  $\mu\text{m}$ :** the signal changes by 1 mV/  $\mu\text{m}$

$$\rightarrow \sigma_{Jitter} = 3 \mu\text{m}$$

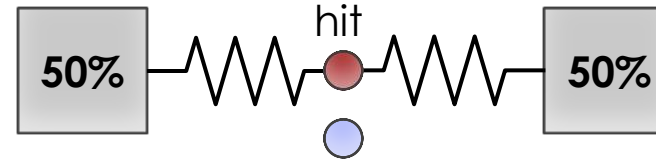
**300  $\mu\text{m}$ :** the signal changes by 3 mV/  $\mu\text{m}$

$$\rightarrow \sigma_{Jitter} = 9 \mu\text{m}$$

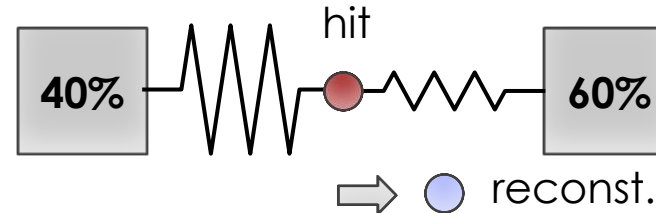


$\sigma_{Sensor}$

## Sensor non-uniformity



For equal resistivity, 50%-50% sharing indicates the hit is in the middle



If the resistivity is not uniform, the reconstruction shifts the point closer to the smaller resistivity

$\sigma_{Reconstruction}$

## Algorithm

$$S_i(\alpha_i, r_i) = \frac{\frac{\alpha_i}{\ln(r_i)}}{\sum_1^n \frac{\alpha_j}{\ln(r_j)}}$$

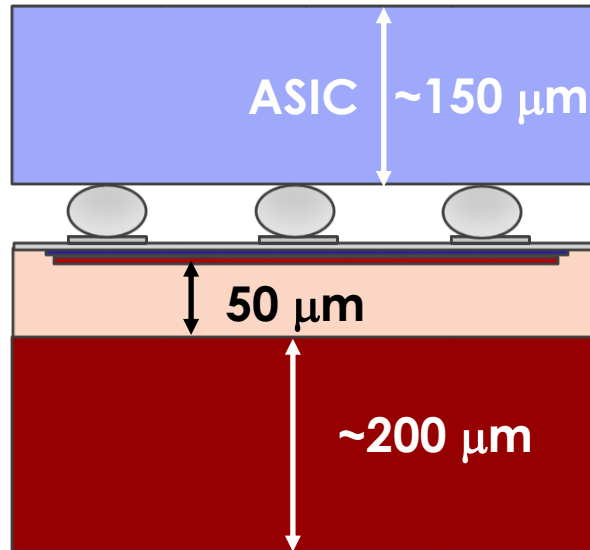
If the predicted sharing is incorrect, the reconstructed position is shifted.

**DPC:** RSD might not be a perfect DPC, yielding to systematic errors.

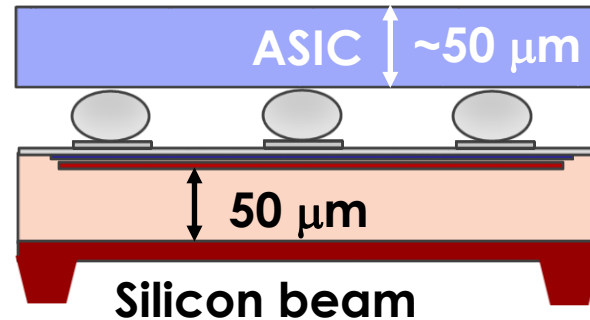
# Reduced material budget

The active thickness of RSD sensor is rather small  $\sim 50 \mu\text{m}$ .

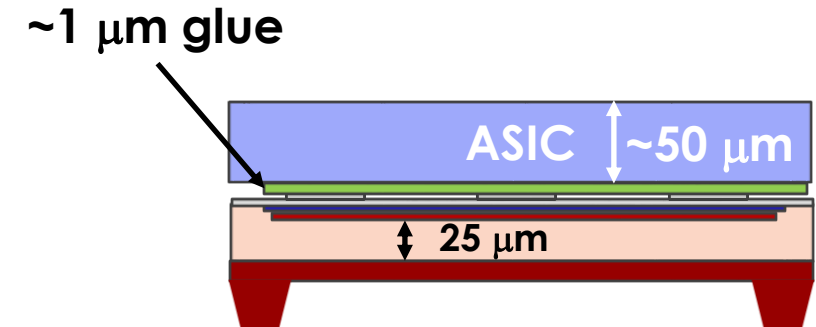
**There is a clear path leading to  $< 100 \mu\text{m}$  material:**



Present design: no material budget optimization

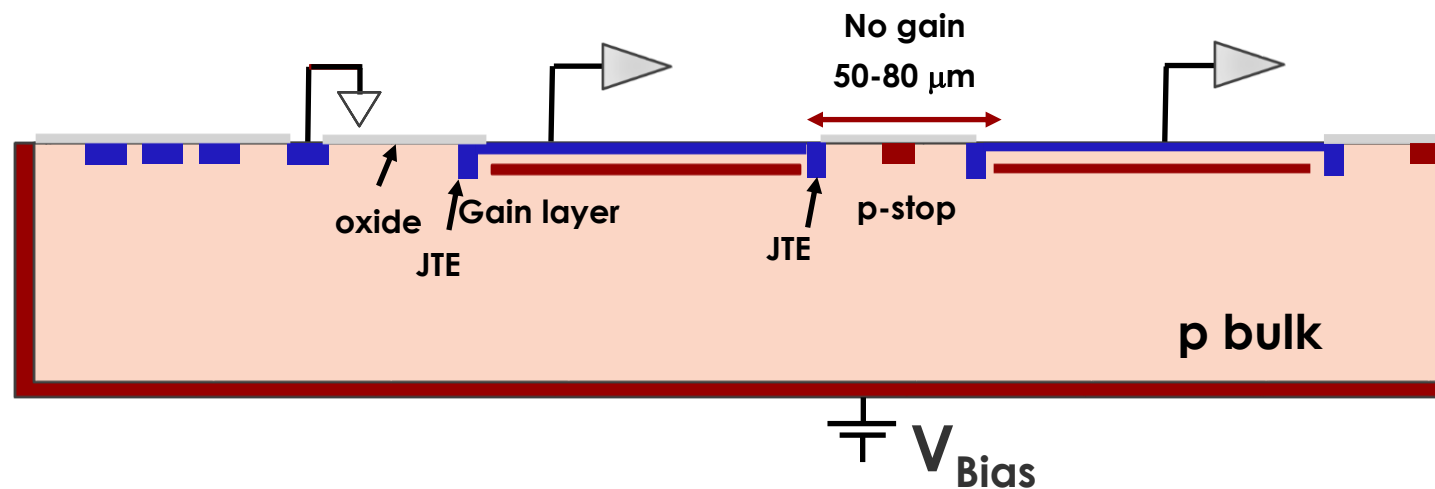


- Thinned handle wafer:  $500 \mu\text{m} \rightarrow 10\text{-}20 \mu\text{m}$



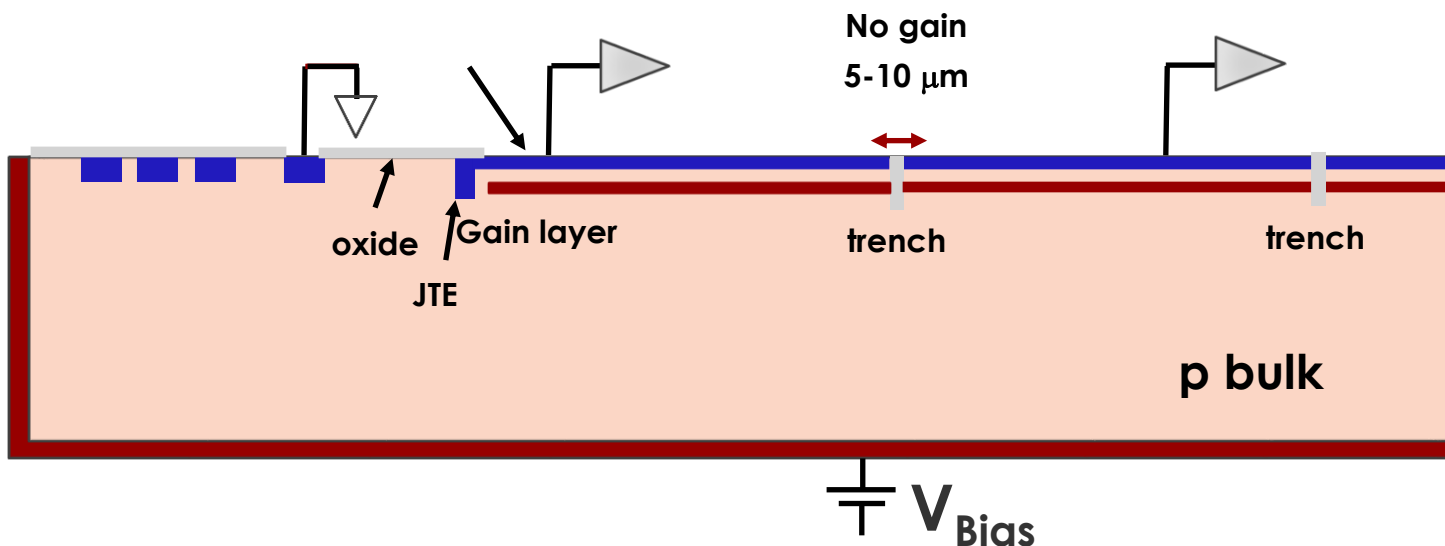
- Thinned handle wafer:  $500 \mu\text{m} \rightarrow 10\text{-}20 \mu\text{m}$
- Thinned active area:  $50 \mu\text{m} \rightarrow 25 \mu\text{m}$   
 $50 \text{ ps} \rightarrow 25 \text{ ps}$

# Towards 100% fill factor: Trench Isolated LGAD



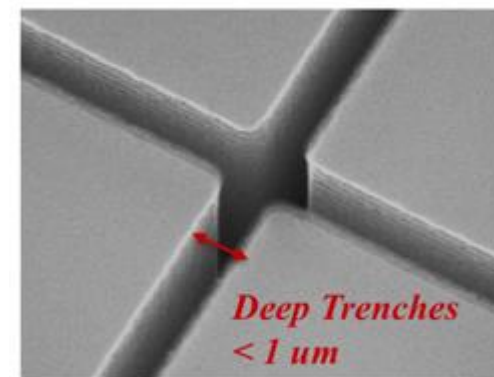
No-gain region ~ 50-80 μm

→ cannot use UFSDs for small pixels

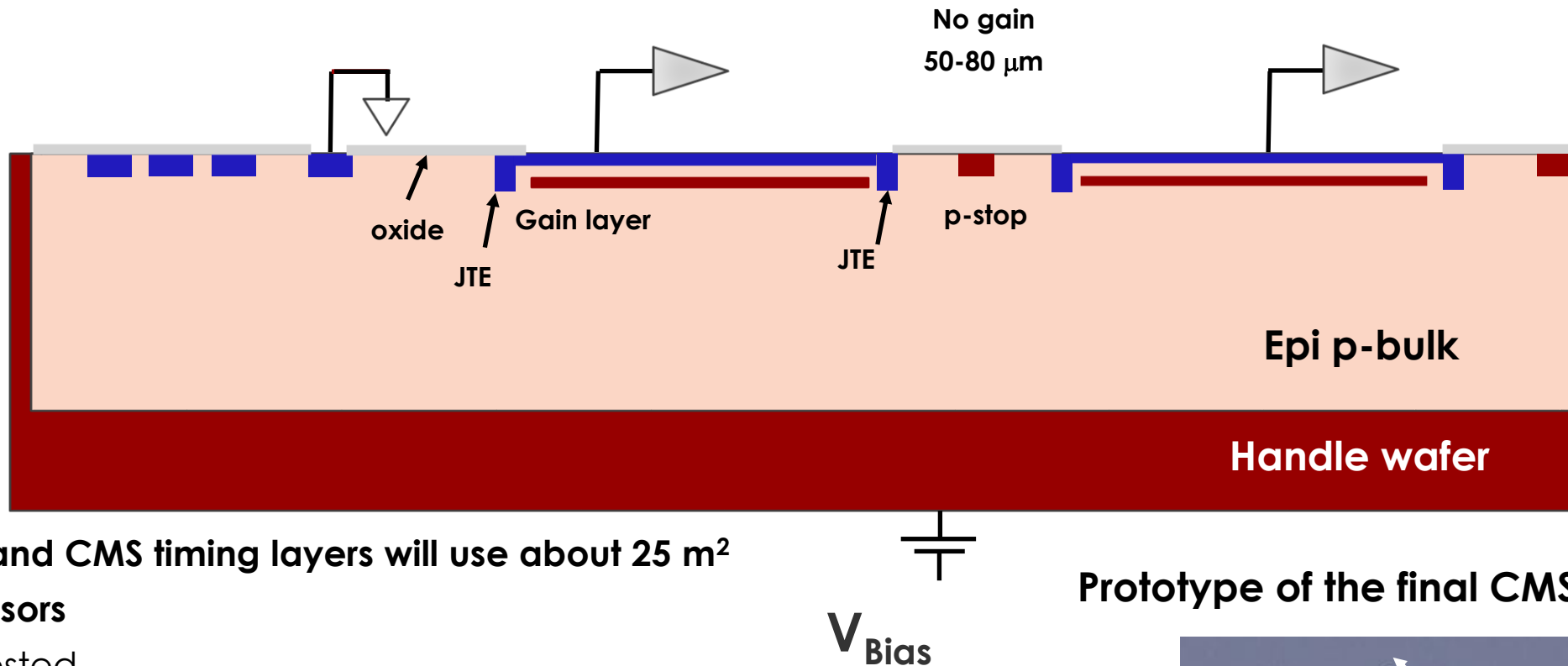


Solution: use trenches for pad isolation

→ No-gain region ~ 5 – 10 μm



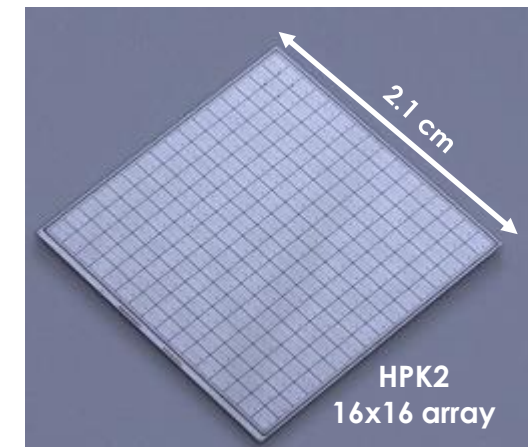
# State-of-the-art: sensors for ATLAS and CMS



- The ATLAS and CMS timing layers will use about 25 m<sup>2</sup> of UFSD sensors

- Very well tested
- Will be used up to  $\sim 2 \text{ E}15 \text{ n}_{eq}/\text{cm}^2$
- Gain  $\sim$  up to 40 when new  $\implies$  up to 20 fC
- Signal duration  $\sim 1 \text{ ns}$
- Low noise
- Rate  $\sim 50\text{-}100 \text{ MHz}$
- Excellent production uniformity

Prototype of the final CMS sensor



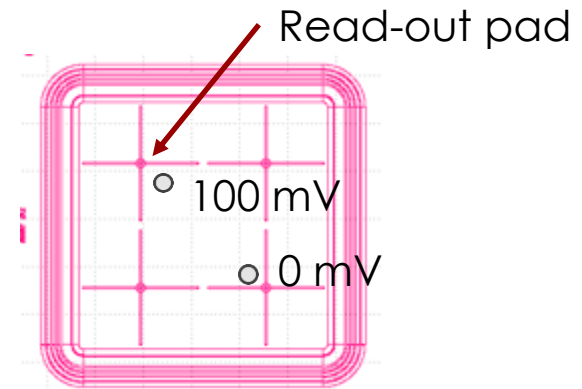
# Spatial resolution: the role of jitter

The main component of the position resolution is the position jitter, defined as:

$$\sigma_{jitter} = \frac{\sigma_{el\_noise}}{\frac{dA}{dx}}$$

Imagine a system with a single read-out pad where a hit generates:

- A signal of 100 mV when shot near a pad
- A signal of 0 mV when shot at the opposite corner
- Noise  $\sim 1$  mV (as in our lab)

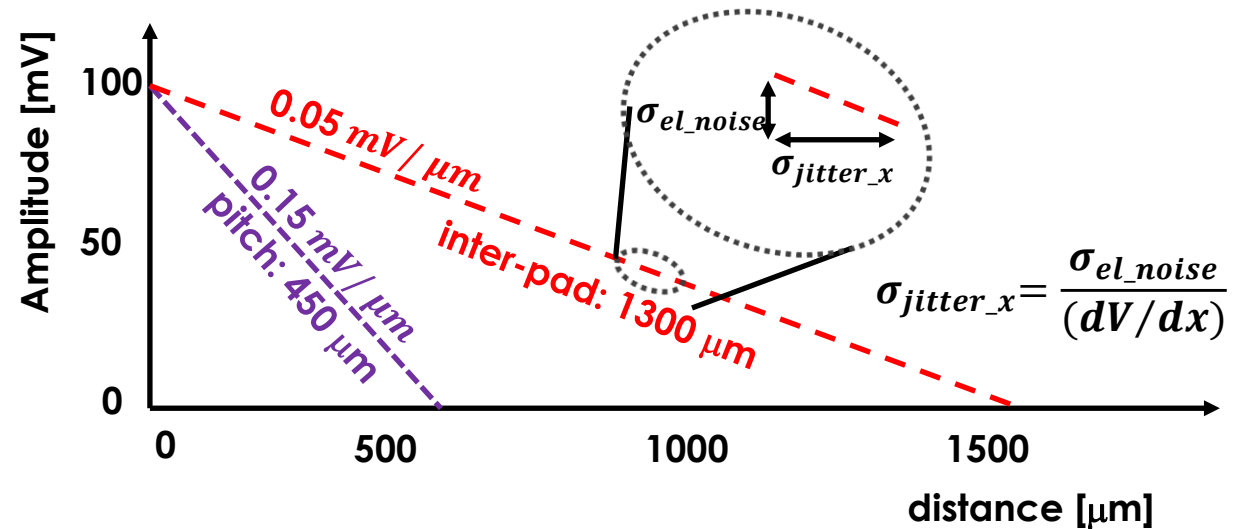


In this simplified system, the signal decreases by:

- Pitch 1300  $\mu\text{m}$ : 0.05 mV/ $\mu\text{m}$
- Pitch 450  $\mu\text{m}$ : 0.15 mV/ $\mu\text{m}$

So, the jitter is:

- Pitch 1300  $\mu\text{m}$ :  $1 \text{ mV} / (0.05 \text{ mV}/\mu\text{m}) = 20 \mu\text{m}$
- Pitch 450  $\mu\text{m}$ :  $2 \text{ mV} / (0.15 \text{ mV}/\mu\text{m}) = 7 \mu\text{m}$



# Irradiation effects

## Irradiation causes 3 main effects:

- Decrease of charge collection efficiency due to trapping
- Doping creation/removal
- Increased leakage current, shot noise

**The main effect in LGAD is “acceptor removal”, i.e., the reduction of the gain implant doping**

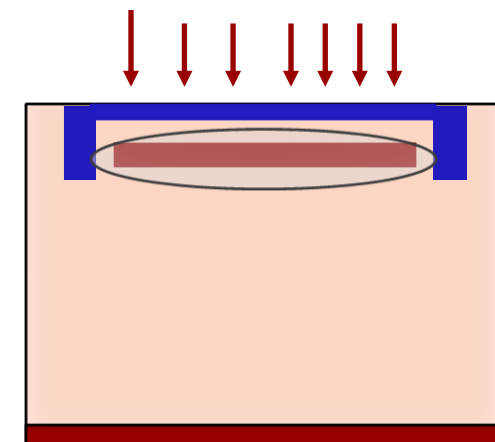
**The electric field due to the gain implant decreases → Compensated with higher bias**

**Main technique to decrease acceptor removal:** carbon implantation in the gain layer

Carbon spoils the properties of silicon sensors.

However, **in the right amount and only on the gain implant, it increases the sensor rad. resistance by a factor of 3**

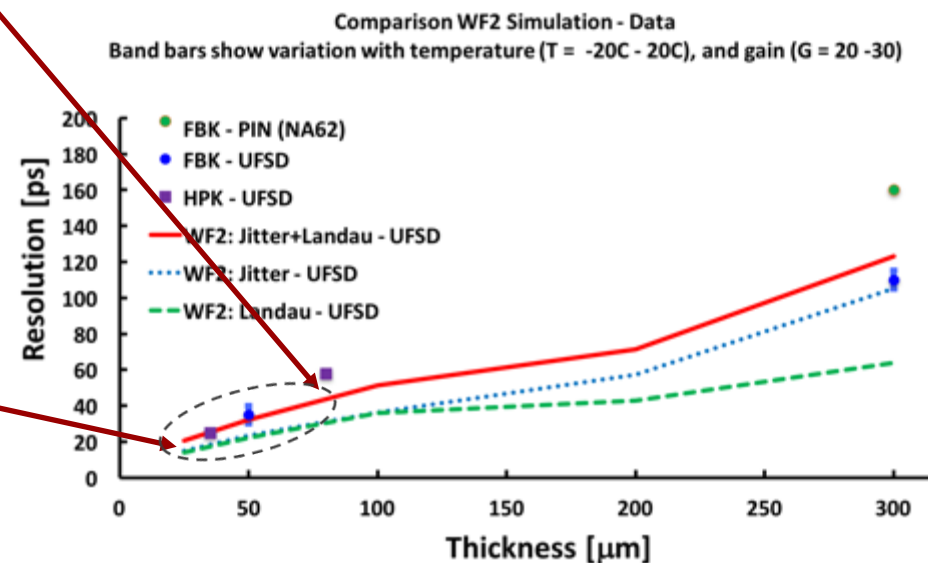
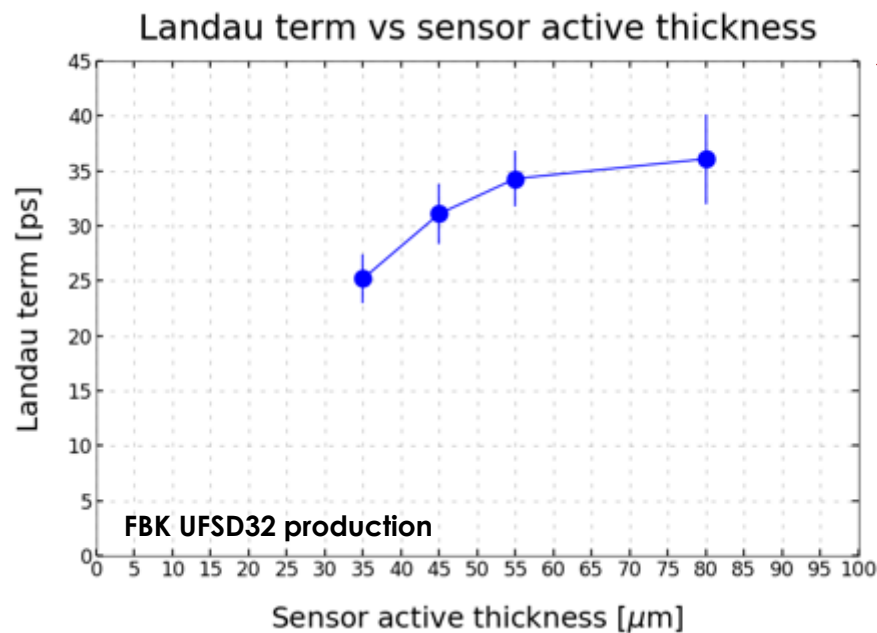
## carbon implantation



# UFSD temporal resolution in thinner sensors

UFSD temporal resolution improves in thinner sensors:  
==> reasonable to expect 10-20 ps for 10-20  $\mu\text{m}$  thick sensors.

**Be aware: very difficult to do timing with small signals... power consumption increases**



# Position reconstruction using charge imbalance



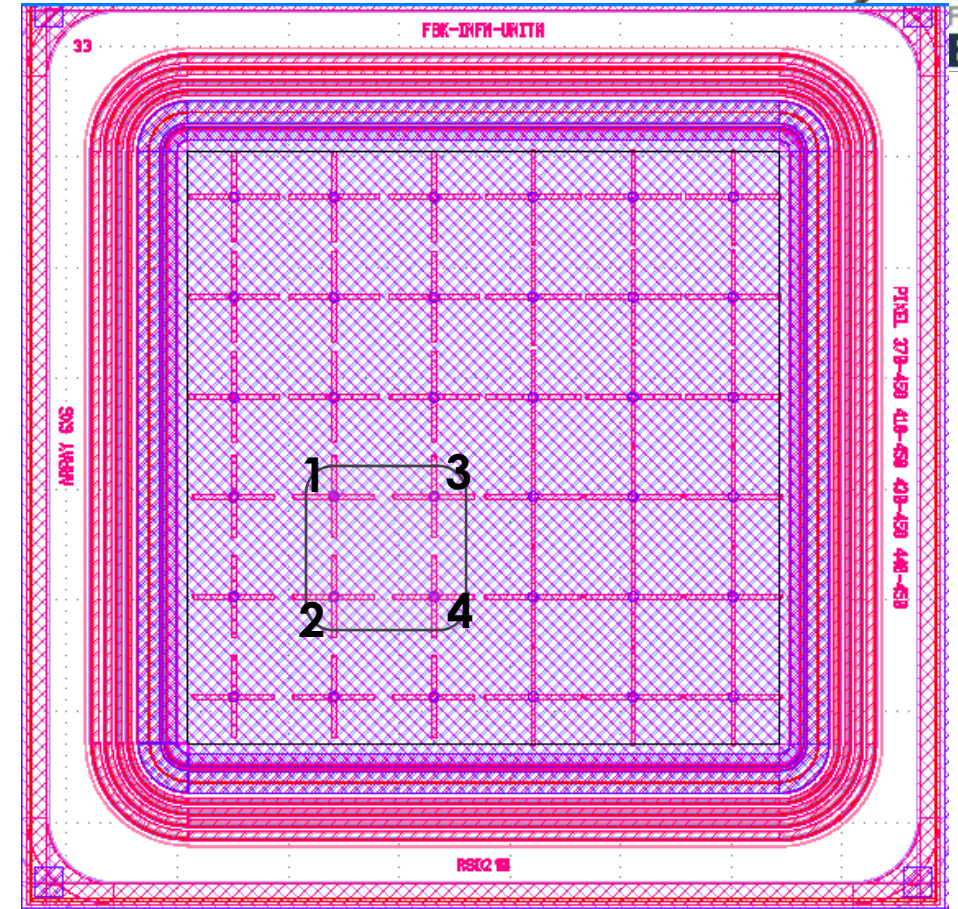
The position is reconstructed using the charge imbalance among the electrodes positioned at the 4 corners

$$x_i = x_{center} + k_x \frac{pitch}{2} * \frac{Q_3 + Q_4 - (Q_1 + Q_2)}{Q_{tot}}$$

$$y_i = y_{center} + k_y \frac{pitch}{2} * \frac{Q_1 + Q_3 - (Q_2 + Q_4)}{Q_{tot}}$$

$$k_x = \frac{Q_{tot}}{Q_3 + Q_4 - (Q_1 + Q_2)} \Big|_{x@edge}$$

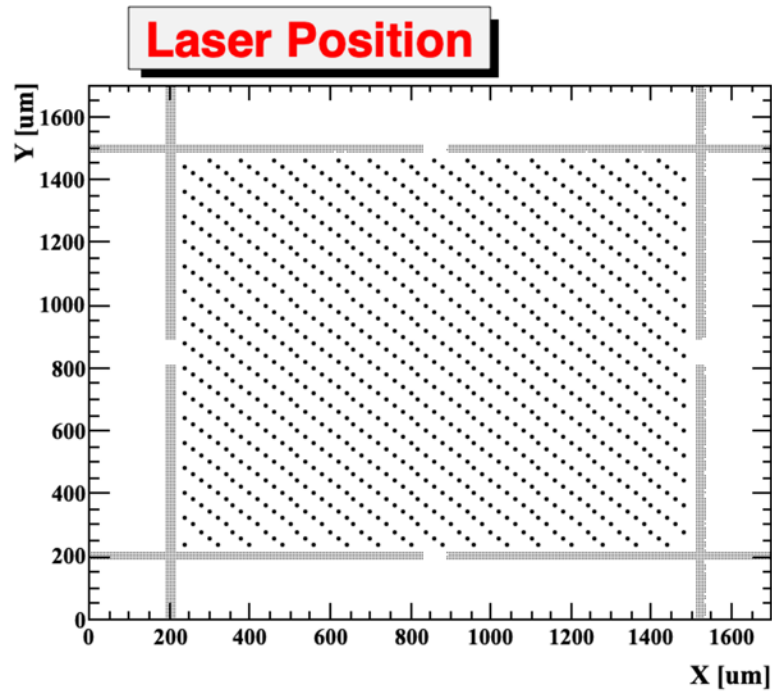
$$k_y = \frac{Q_{tot}}{Q_1 + Q_3 - (Q_2 + Q_4)} \Big|_{y@edge}$$



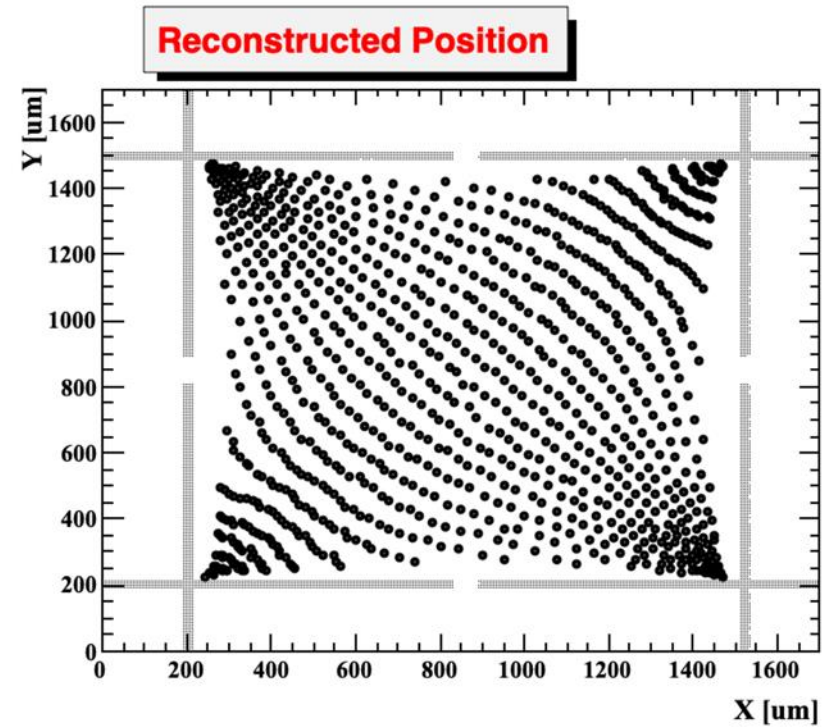


# Evaluate the spatial resolution using laser TCT

Shoot the laser in a grid of points



Reconstruct the hit position with charge imbalance



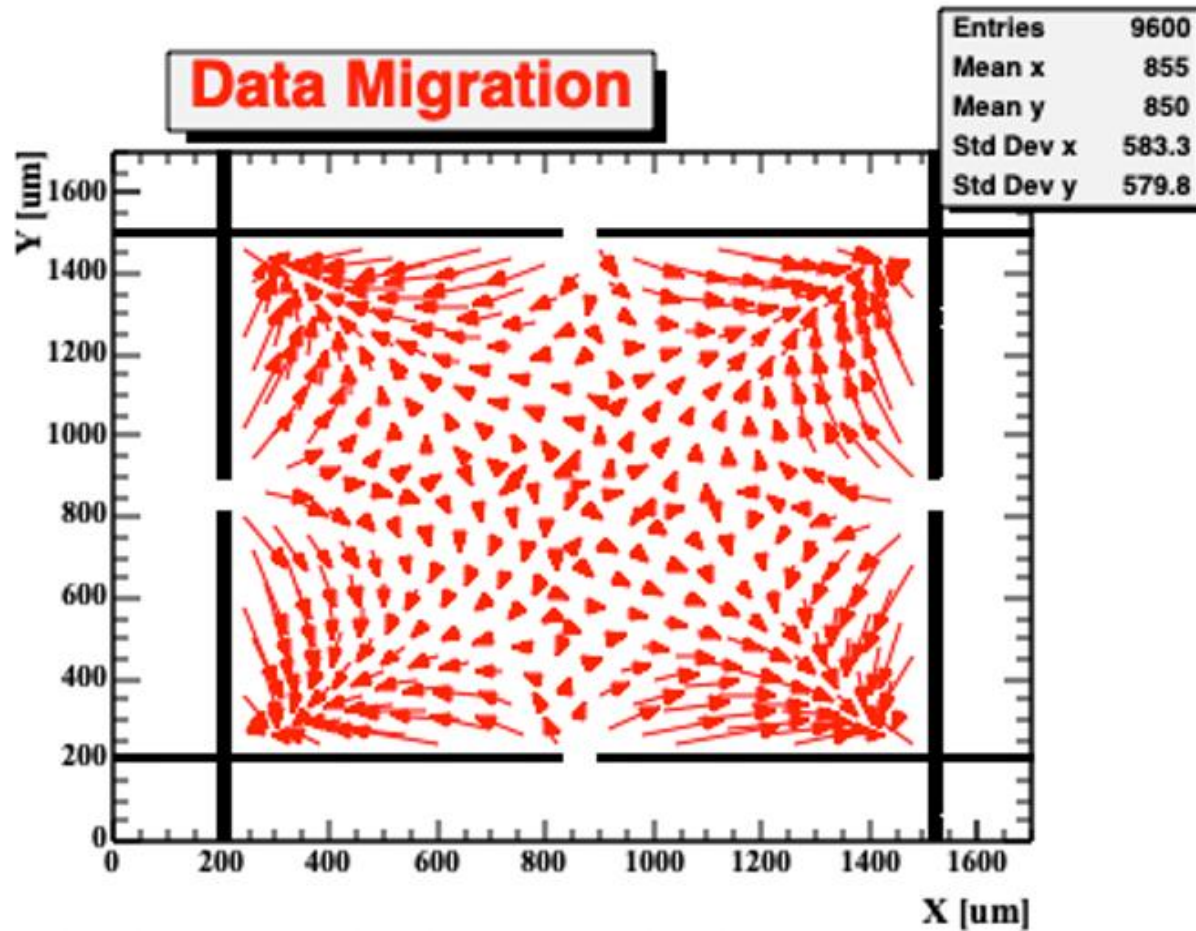
**First take-home result:** even without any additional correction, the cross-shaped electrodes provide a fairly accurate position reconstruction

**Second take-home result:** near the pads, the reconstructed positions are systematically shifted with respect to true positions

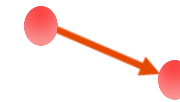
# Correct the reconstructed position

Compute the migration map:

For each laser position, connect the true and reconstructed positions.



Laser Position



Reconstructed position

# RSD2 spatial resolution



RSDs at gain = 30 achieve a spatial resolution of about 2-3% of the pitch size:

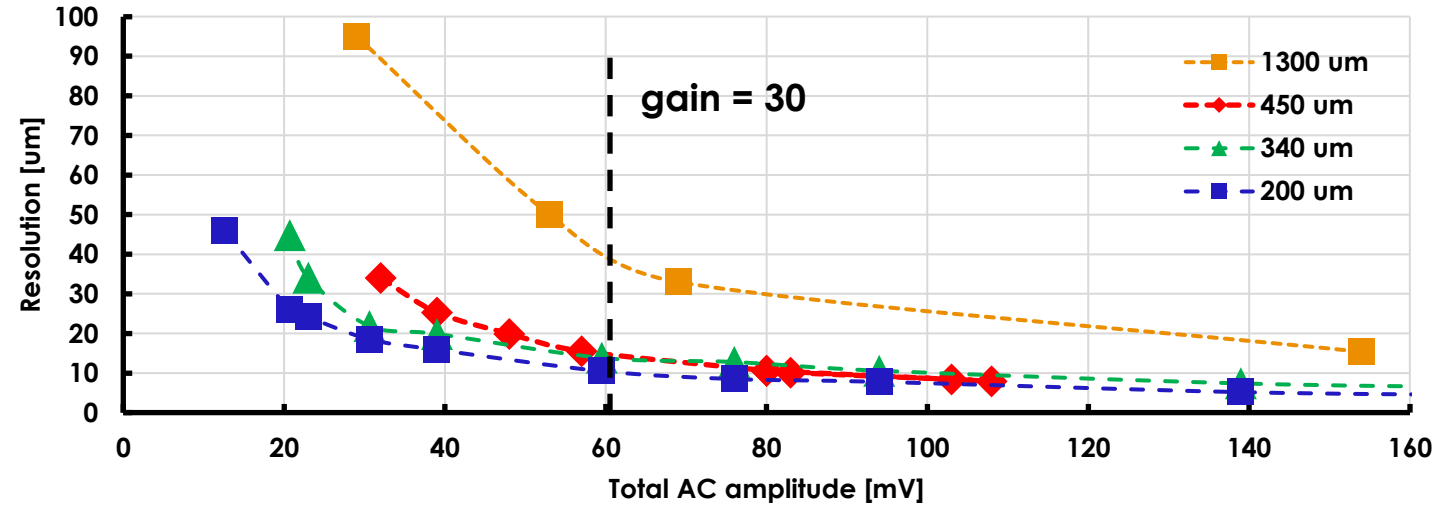
## RSD:

- 1300 x 1300 mm<sup>2</sup>:  $\sigma_x \sim 40 \mu\text{m}$
- 450 x 450 mm<sup>2</sup>:  $\sigma_x \sim 15 \mu\text{m}$

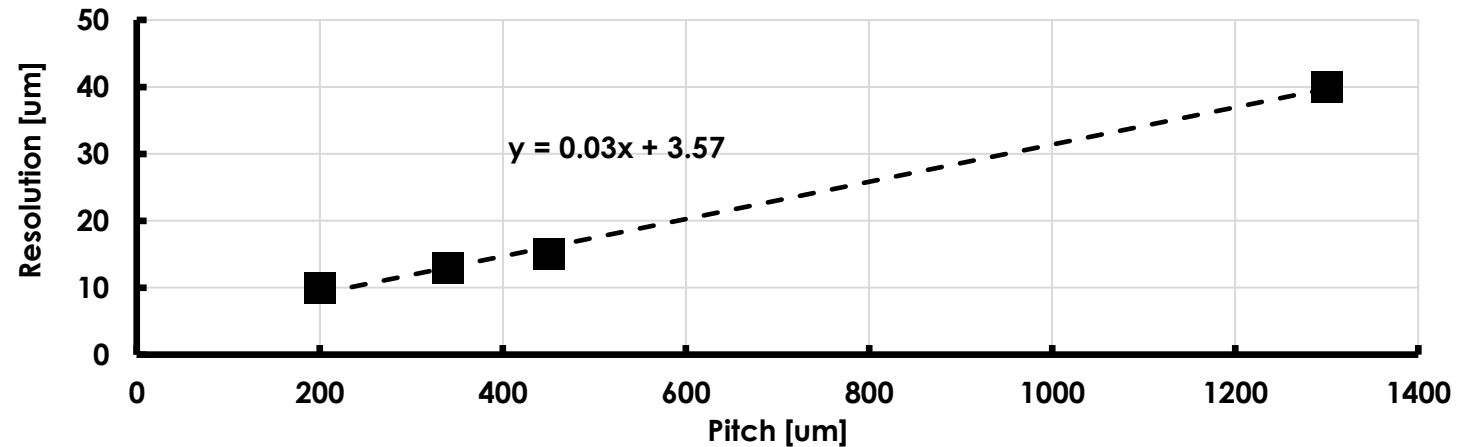
## Traditional standard pixel

- 1300 x 1300 mm<sup>2</sup>:  $\sigma_x \sim 920 \mu\text{m}$
- 450 x 450 mm<sup>2</sup>:  $\sigma_x \sim 320 \mu\text{m}$

RSD2 crosses: spatial resolution for 4 different pitch sizes



RSD2 crosses: spatial resolution when the total AC amplitude = 60 mV



# RSD2 temporal resolution

The **resolution** depends mostly upon the signal size and **weakly on the pixel size**  
RSDs at gain = 30 achieve a temporal jitter of about 20 ps

