



Tests on radiation hardness of 3D-trench silicon sensors

F. Borgato, M. Boscardin, D. Brundu, A. Cardini, G.M. Cossu, G.-F. Dalla Betta, <u>M. Garau</u>, L. La Delfa, A. Lampis, A. Lai, A. Loi, M. Obertino, S. Ronchin, G. Simi, S. Vecchi







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3D-trench silicon pixel sensors fo HEP experiments



To cope with the **very high instantaneous luminosity** in the current HEP experiments, detectors are required to have very good <u>spatial resolution</u>, <u>time resolution</u> and high <u>radiation hardness</u> **at the same time**!

e. g. LHCb VELO requirements for Upgrade II:

- Radiation hardness $10^{16} 10^{17}$ 1 MeV n_{eq}/cm²
- $\sigma_t \approx 50 \text{ ps per hit}, \mathcal{O}(20 ps) \text{ per track}$
- $\sigma_s \approx 10 \ \mu m$

3D sensors are a very promising option to satisfy these requirements



Optimization of the electrodes geometry for timing

5 columns 3D trench Weighting field (1/cm) 2.000e+03 1.667e+03 1.333e+03 1.000e+03 6.667e+02 3.333e+02 0.000e+00 $i = q \vec{E}_w \cdot \vec{v}_d$ Electric field (V/cm) 1.000e+05 8.333e+04 6.667e+04 5.000e+04 3.333e+04 1.667e+04 TCAD simulation, $V_{\text{bias}} = -150V$

Electric and weighting field maps much more uniform in the trench geometry

Simulated charge collection curves

for MIPs uniformly crossing a pixel

over its active area

Faster and more uniform charge collection time in the 3D trench geometry



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- Two batches of TimeSPOT sensors were produced in 2019 and 2021 at Fondazione Bruno Kessler (FBK, Trento, Italy)
- Several devices designed and fabricated (single and double pixels, 10 pixel-strips, various pixel matrices, etc.)

- 55x55 μm² pixels
- 40 µm long n++ trench placed between continuous p++ trenches used for the bias
- 150 µm active thickness
- Collection electrode 135 µm deep



3D-trench sensors characterization

- Different test structures characterized: single pixels, pixel-strips (10 or 30 pixels)
- Single-channel custom-made Front-End Electronics boards featuring a two-stage <u>transimpedence amplifier</u> made with fast SiGe BJTs





- In this talk I will focus on **highly irradiated TimeSPOT sensors** characterization, comparing the results with those obtained for non-irradiated sensors
- Laboratory and beam tests characterizations

Laboratory setup with ⁹⁰Sr source



⁹⁰Sr β ⁻ radioactive source, emitting electrons with energy in the range (0.5-2.2) MeV





Iulatio

The **multiple scattering** in silicon at these energies is an important effect

- This setup with the ⁹⁰Sr source allows to 0 measure only an **upper limit** of the **time resolution** - about twice that one measured at the test beam
- However, it allows to make preliminary tests in **laboratory** and to compare different test structures performance

Highly irradiated TimeSPOT sensors

- Irradiation of TimeSPOT sensors (1st and 2nd batch) with neutrons in the TRIGA Mark II reactor of Institut Jožef Stefan in Ljubljana (Slovenia)
- Up to a fluence of $2.5 \cdot 10^{16} 1 \text{ MeV } n_{eq}/\text{cm}^2$ (max irradiation fluence of the VELO Upgrade 2 detector $6 \cdot 10^{16} 1 \text{ MeV } n_{eq}/\text{cm}^2$ without modules replacement every year)
- It is necessary to operate irradiated sensors at low temperature to reduce the leakage current
- Preliminary characterizations in the laboratory

⁹⁰Sr source setup inside a **climatic chamber** to cool down the irradiated sensors and reduce, in this way, the leakage current





Laboratory characterization of irradiated TimeSPOT sensors



IV curves (single-pixels)

Leakage current increases with the irradiation fluence



Events rate VS bias voltage (pixel-strips)

Trigger at fixed threshold, slightly above the noise, and **events count** in a 30s time interval.

First indication that it is necessary to increase the bias voltage (few tens of volts) applied to irradiated sensors to recover the performance before irradiation – because of the depletion voltage increase

Test beam of irradiated sensors

Test beam made in May 2022 at CERN SPS/H8 beamline, 180 GeV/c positive pions beam

- **DUT outside the trigger** and can be rotated
- Piezoelectric stages to precisely align the two 3D structures with beam, all mounted in a RF-shielded box
- Dry ice, allows to keep the irradiated sensor under test in the range of temperature (-40,-20)°C, monitoring with a PT100 sensor
- **2 MCP-PMTs** as time reference of the setup with a measured accuracy of **3-4 ps**
- DAQ with an 8 GHz bandwidth 20 GSa/s oscilloscope
- Time resolution and efficiency measurements







Waveforms analysis

For each sensor's waveform – in both laboratory and test beam data analysis:

- Signal baseline (red-dashed line) is evaluated on an event-by-event basis
- The signal amplitude A is measured (w.r.t. to the event baseline)
- Signal time of arrival evaluated with a costant fraction algorithm, the *Reference method*: subtract each waveform from a delayed (by about half of the signal rise time) copy of itself, then on the resulting signal we trigger at X/2 height



-200



Single pixel – amplitude distributions



- Very good performance of the non-irradiated sensor even at low V_{bias}
- A slightly larger bias voltage is required to recover the signal amplitude for irradiated sensors indication of good functioning also after high radiation fluence exposition

Irradiated single pixels – time resolution



Two Gaussian fit of the time distribution to include late signals contributions + a constant modelling the background

 $\sigma_{\rm eff}$ is the standard deviation of the mixture distribution of the two Gaussians

$$(\sigma_t^{\text{eff}})^2 = f_1(\sigma_1^2 + \mu_1^2) + (1 - f_1) \cdot (\sigma_2^2 + \mu_2^2) - \mu^2$$

where f_1 is the fraction of the Gaussian core and μ is defined as

$$\mu = f_1 \mu_1 + (1 - f_1) \cdot \mu_2$$

Irradiated single pixels – time resolution

Results obtained with a constant fraction based algorithm - *Reference* method



- Excellent time resolution measured also on irradiated single pixels
- Slightly better results on irradiated sensors w.r.t. non-irradiated one (also in laboratory measurements)

Possible explanations:

- At lower temperatures the timing performance improves (transistor gain) – verified by measuring the non-irradiated pixel performance at low temperature
- 2) The FEE boards have a slightly different gain

First time resolution measurements of irradiated TimeSPOT sensors have shown an excellent time resolution up to a fluence of $2.5 \cdot 10^{16}$ 1 MeV n_{eq} / cm²



- Trenches (5 µm wide) are non-active volumes, channeled particles will not be detected
- Tilt the sensors with respect to normal incidence should allow to recover geometrical efficiency
- Trigger on one pixel (55 μm x 55 μm, on piezos) centered on a triple strip (165 μm x 550 μm, DUT) and counting the fraction of signals seen in the triple strip (on a single FE channel)
- Rotate the DUT around the trench direction



Geometrical efficiency measurement method:

Time distribution of the triple-strip signals w.r.t. the time reference



- Fit of the **peak** + the **background**
- The events under the peak are the events seen by the triple-strip
- The flat background corresponds to undetected particles
- The *seen* events are calculated by subtracting the background events from the total histogram events



Efficiency VS bias voltage at perpendicular beam incidence (0°)

- Non-irradiated sensor already efficient at -20 V •
- $1 \cdot 10^{16}$ 1 MeV n_{eq} / cm² triple strip shows an about 30% ٠ smaller efficiency at -20 V w.r.t. the non-irradiated one
- Irradiated sensor efficiency recovery by increasing the bias ٠ voltage







Efficiency VS beam incidence angle

Compatible results obtained for the **nonirradiated** and the $2.5 \cdot 10^{16} 1 \text{ MeV } n_{eq} / \text{ cm}^2$ sensors by increasing the bias voltage of the second by only 30 V w.r.t. the non-irradiated

Almost fully efficient at 20°

 $\varepsilon = 99.1 \pm 1.2 \%$ $\varepsilon = 98.7 \pm 1.1 \%$

This result, together with the timing measurements, proves for the first time the **good performance of TimeSPOT sensors** also when they are exposed to **high radiation fluences**

Conclusions

- Characterization of highly irradiated TimeSPOT silicon sensors both in the laboratory and at the test beam
- Excellent timing performance of irradiated sensors, compatible with those of non-irradiated sensors, showing a time resolution of 10-12 ps at -100V
- Efficiency of irradiated sensors compatible to non-irradiated one, by slightly increasing the bias voltage. At 20° beam incidence angle about 99% efficiency
- Radiation tolerance limit not reached yet
- Tests on the Timespot1 ASIC are ongoing (see <u>A. Loi talk</u>)



Additional material

Time resolution contributions

At a first order simplified analysis, the time resolution of a system sensor + read-out electronics is

$$\sigma_t = \sqrt{\sigma_{tw}^2 + \sigma_{dr}^2 + \sigma_{un}^2 + \sigma_{ej}^2 + \sigma_{TDC}^2}$$

 ϕ_w : signal amplitude fluctuation event by event \rightarrow time-walk jitter \rightarrow constant fraction discriminator

 σ_{ar} : delta rays \rightarrow signal amplitude and shape variations \longrightarrow negligible in a 3D sensor

 σ_{un} : <u>non-uniformities</u> in the charge collecting field and carrier velocities \rightarrow different signal shape

 σ_{ej} : <u>noise of the preamplifier</u> used to readout the sensor

 σ_{CDC} : <u>digital resolution</u> of the electronics used to measure the signal \longrightarrow adequate TDC

For a 3D sensor
$$\sigma_t \cong \sqrt{\sigma_{un}^2}$$



Laboratory setup with ⁹⁰Sr source (2)



The **MCP-PMT** is used both to:

- \circ $\$ have an accurate time reference
- select more energetic electrons →

Cherenkov threshold in the 5.5 mm thick quartz input window $E_{th} \sim 0.7 \ MeV$

The multiple scattering in silicon at these energies is an important effect to be taken into account -> **simulation**

Geant4 simulation





Beam at CERN SPS/H8 beamline where we made TimeSPOT beam tests in 2021 and 2022

Laboratory setup with ⁹⁰Sr source



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The **multiple scattering** in silicon at these energies is an important effect to be taken into account and it is a critical aspect of this setup



For electrons 0.5-2 MeV a large amount of charge deposited outside the pixel \Rightarrow lower deposit \Rightarrow higher time jitter $\left(\sigma_{ej} \approx \frac{t_r}{S/N}\right)$

This setup with the ⁹⁰Sr source allows to measure only an upper limit of the time resolution (about twice), <u>but</u> it allows to make preliminary tests in laboratory and to compare different test structures performance

Not-irradiated sensors characterization with ⁹⁰Sr setup



This setup with the ⁹⁰Sr source allows to measure only an **upper limit** of the **time resolution** (about twice), <u>but</u> it allows to make **preliminary tests** in **laboratory** and to compare different test structures performance

Laboratory characterization of irradiated TimeSPOT sensors



Two Gaussian fit of the time distribution to include late signals contributions + a constant modelling the background

 \rightarrow mixture distribution with std dev σ_{eff}

Apparently better result at -25 V, probably due to the rejection of small signals by the trigger coincidence condition \rightarrow following test beam results confirm this hypotesis

Waveforms analysis

For each sensor's waveform – in both laboratory and test beam data analysis:

- Signal baseline (red-dashed line) is evaluated on an event-by-event basis
- The **signal amplitude** A is measured (w.r.t. to the event baseline)
- **Signal time of arrival** evaluated with a costant fraction algorithm:
 - *Reference*: subtract each waveform from a delayed (by about half of the signal rise time) copy of itself, then on the resulting signal we trigger at X/2 height
 - Leading-edge: time at 15 mV signal amplitude, linear interpolation around threshold (time-walk effect is present)
 - LE corrected for the amplitude to suppress the time-walk effect
 - Spline: a classic CFD at 20% with rising edge interpolated with a spline



Test beam of irradiated sensors

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Irradiated single pixels – time resolution

Single pixel time resolution measured with the two constant fraction based algorithms Spline and Reference



Reference method

Efficiency measurement

Counts/(5.7 ps) 10³ Ē seen ε all histogram events 10² 10 F 1 2 t _{3strip} -2 -10 -8 -6 -4 0 4 - < t_{MCP-PMT} > [ns]



Time distribution of the triple-strip signals w.r.t. the time reference