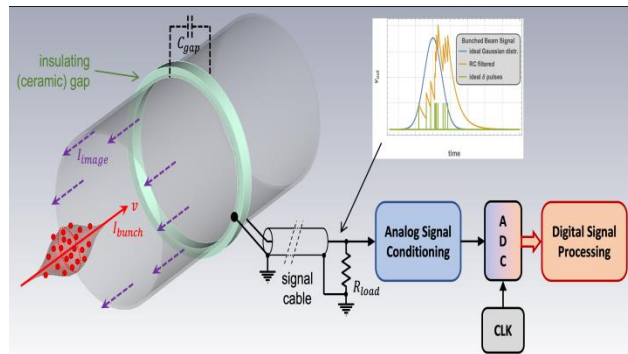
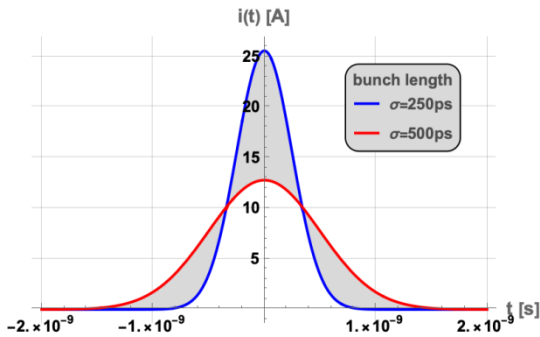
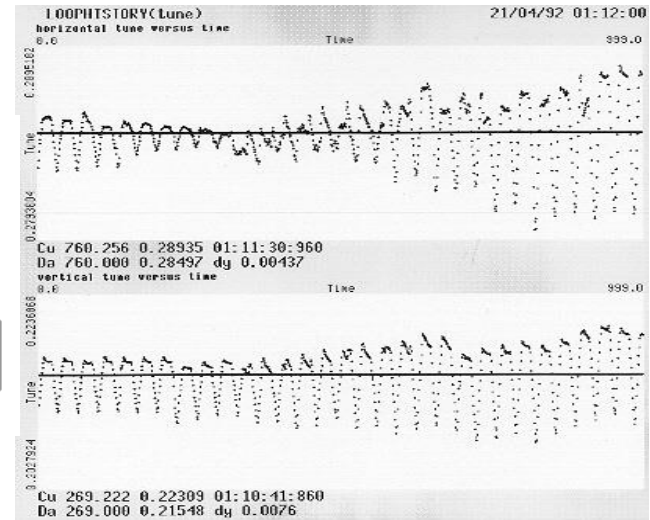
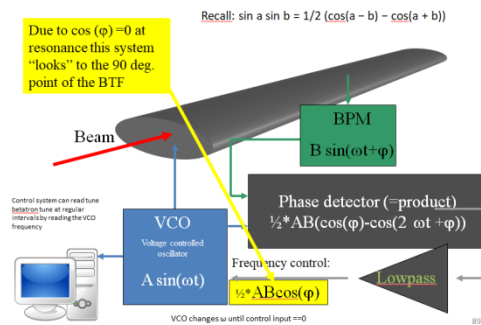
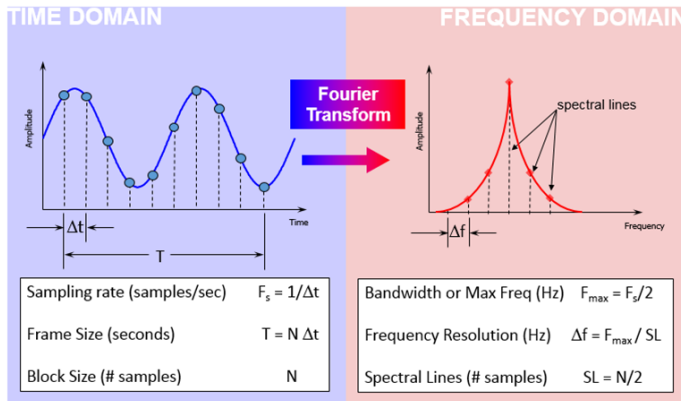


Time & Frequency Domain Signals & Measurements

H.Schmickler, ex-CERN



With slides from:

M.Gasior, R.Jones, M.Wendt (CERN)

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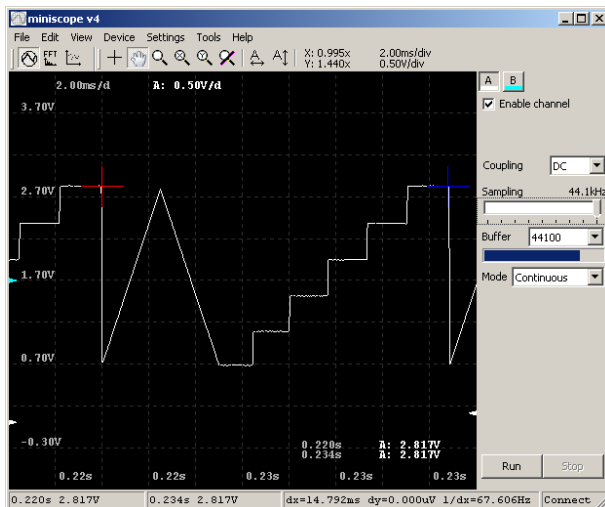
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Part I

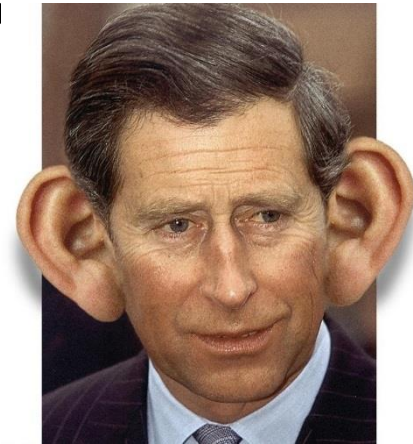
- Introduction: What Is time domain and frequency domain?
- Fourier synthesis and Fourier transform
- Time domain sampling of electrical signals (→ ADCs)
- Bunch signals in time and frequency domain
 - a) single bunch single pass
 - b) single bunch multi pass (circular accelerator)
 - c) multi bunch multi pass (circular accelerator)
- Oscillations within the bunch (head-tail oscillations)
→ advanced course

- Fourier transform of time sampled signals
 - a) basics
 - b) aliasing
 - c) windowing
- Methods to improve the frequency resolution
 - a) interpolation
 - b) fitting (the NAFF algorithm)
 - c) influence of signal to noise ratio
 - d) special case: no spectral leakage + IQ sampling
- Analysis of non stationary signals/spectra:
 - STFT (:= Short time Fourier transform) (Gabor transform)
also called: Sliding FFT, Spectrogram
 - multi-BPM combined signal analysis
 - PLL tune tracking
 - **wavelet analysis** (if time permits, not really relevant for accelerators, but really cool stuff)

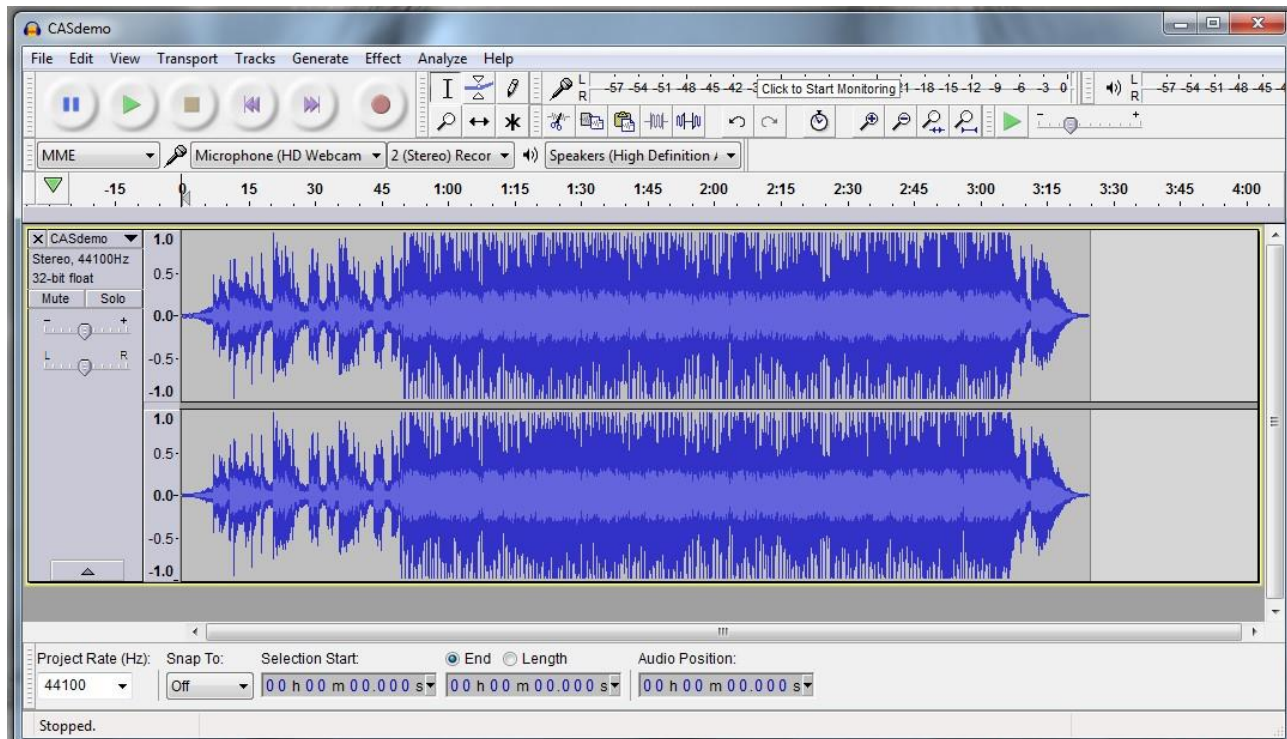
- At first: everything happens in time domain, i.e. we exist in a 4D world, where 3D objects change or move as a function of time.
- And we have our own sensors, which can watch this time evolution: eyes \rightarrow bandwidth limit: 1 Hz
- For faster or slow processes we develop instruments to capture events and look at them: oscilloscopes, stroboscopes, cameras...



- But we have another sensor: ears



- What is this?





- Once we perceive the material in frequency domain (our brain does this for us), we can better understand the material.

Non matter whether we describe a phenomenon in time domain or in frequency domain, we describe the same physical reality. But the proper choice of description improves our understanding!

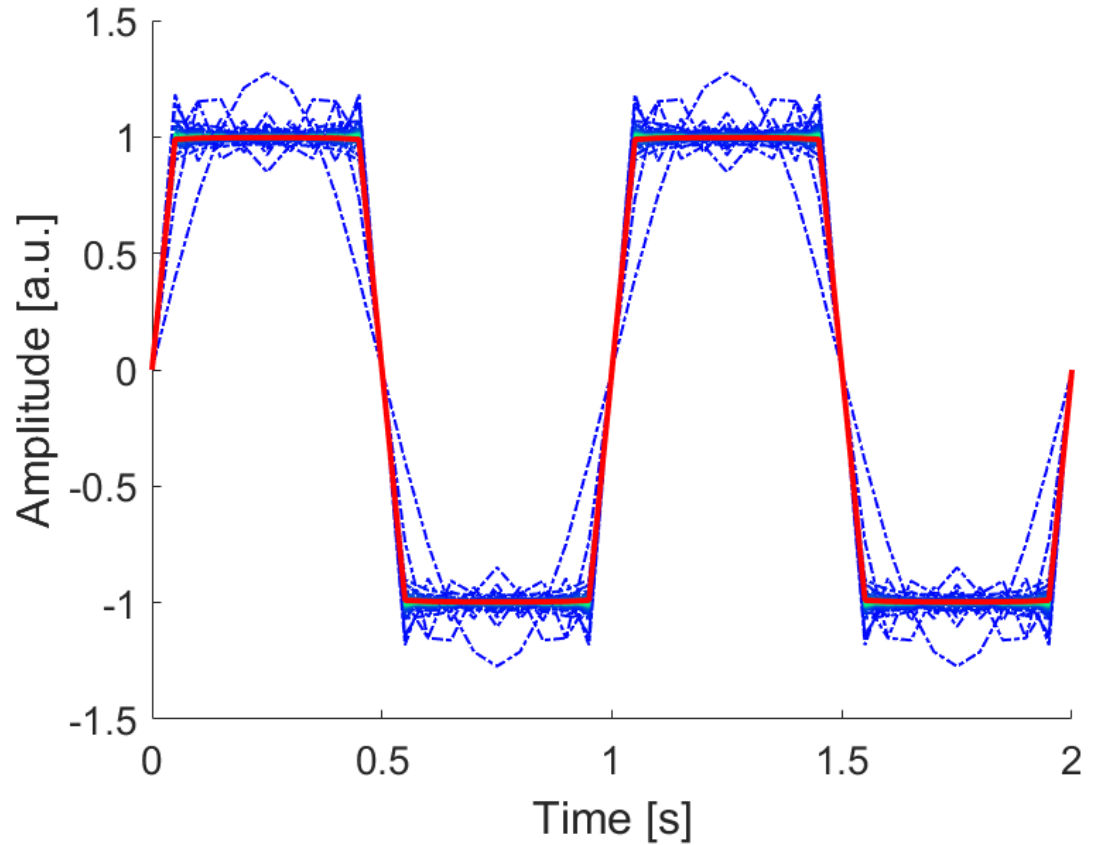
- Had crazy idea (1807):
 - **Any** periodic function can be rewritten as a weighted sum of **Sines** and **Cosines** of different frequencies.
- Don't believe it?
 - Neither did Lagrange, Laplace, Poisson and other big wigs
 - Not translated into English until 1878!
- But it's true!
 - called **Fourier Series**
 - Possibly the greatest tool used in Engineering



A **periodic** function $f(x)$ can be expressed as a series of harmonics, weighted by Fourier coefficients c_n

$$f(x) = \sum_{n=-\infty}^{n=+\infty} c_n e^{-2i\pi\frac{n}{T}x}$$

$$c_n = \frac{1}{T} \int_{-\frac{T}{2}}^{+\frac{T}{2}} f(x) e^{-2i\pi\frac{n}{T}x} dx$$



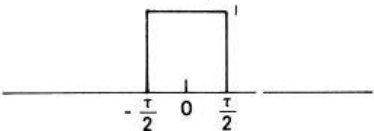
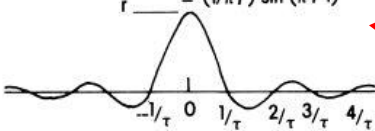
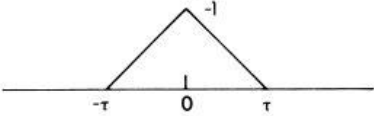
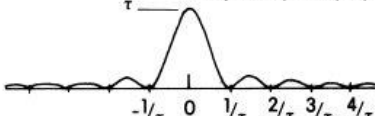
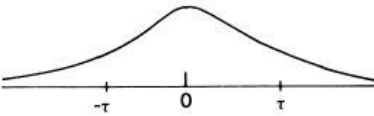
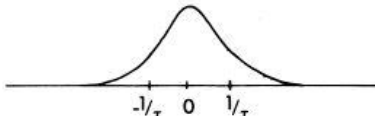
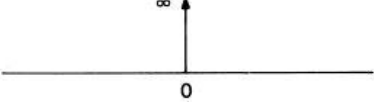
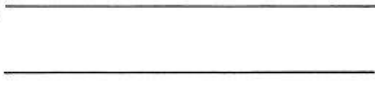
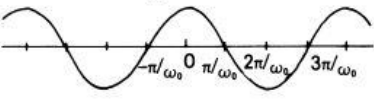
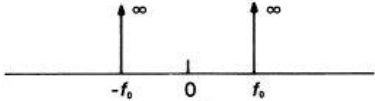
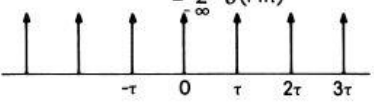
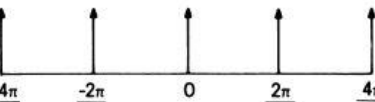
Fourier Transforms (FT)

Time Duration		
Finite	Infinite	
Discrete FT (DFT) $X(k) = \sum_{n=0}^{N-1} x(n)e^{-j\omega_k n}$ $k = 0, 1, \dots, N-1$	Discrete Time FT (DTFT) $X(\omega) = \sum_{n=-\infty}^{+\infty} x(n)e^{-j\omega n}$ $\omega \in (-\pi, +\pi)$	discr. time n
Fourier Series (FS) $X(k) = \int_0^P x(t)e^{-j\omega_k t} dt$ $k = -\infty, \dots, +\infty$	Fourier Transform (FT) $X(\omega) = \int_{-\infty}^{+\infty} x(t)e^{-j\omega t} dt$ $\omega \in (-\infty, +\infty)$	cont. time t
discrete freq. k	continuous freq. ω	

Note: $e^{ik} = \cos k + i \sin k$ $i = \sqrt{-1}$

There is also the term FFT := Fast Fourier Transform
 This is nothing else than a DFT with $N=2^m$; useful to speed up the computation

Fourier Transform Pairs

Time Function	Frequency Function
Boxcar $G(t) = \begin{cases} 1, & t < \tau/2 \\ 0, & t > \tau/2 \end{cases}$ 	Sinc $S(f) = \tau \operatorname{sinc}(f\tau)$ $\tau \operatorname{sinc}(f\tau) = (1/\pi f) \sin(\pi f \tau)$ 
Triangle $G(t) = \begin{cases} 1- t /\tau, & t < \tau \\ 0, & t > \tau \end{cases}$ 	Sinc² $S(f) = \tau \operatorname{sinc}^2(f\tau)$ $= (1/\pi^2 f^2 \tau) \sin^2(\pi f \tau)$ 
Gaussian $G(t) = e^{-1/2 t^2}$ 	Gaussian $S(f) = \tau(2\pi)^{1/2} e^{-(\pi f \tau)^2}$ 
Impulse $G(t) = \delta(t)$ $= 0, \quad t \neq 0$ 	DC Shift $S(f) = 1$ 
Sinusoid $G(t) = \cos \omega_0 t$ 	Single Freq. $S(f) = 1/2 (\delta(f+f_0) + \delta(f-f_0))$ 
Comb. $G(t) = \operatorname{comb}(t)$ $= \sum_{-\infty}^{\infty} \delta(t-n\tau)$ 	Comb. $S(f) = \sum_{-\infty}^{\infty} \delta(f-n/\tau)$ 

Will use this when we come to "windowing"

Gaussian gives a Gaussian!

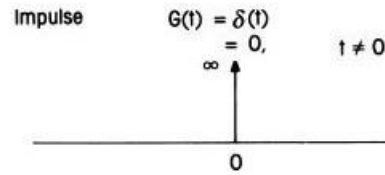
Somewhat surprising!

Not surprising

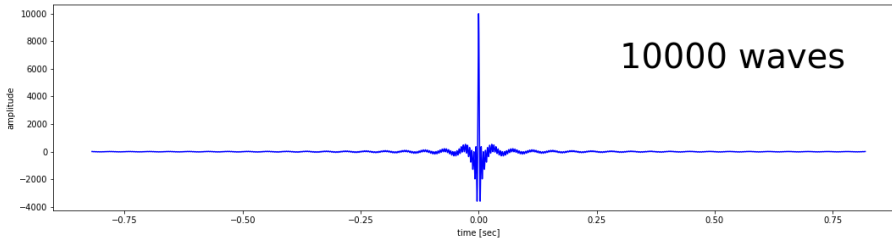
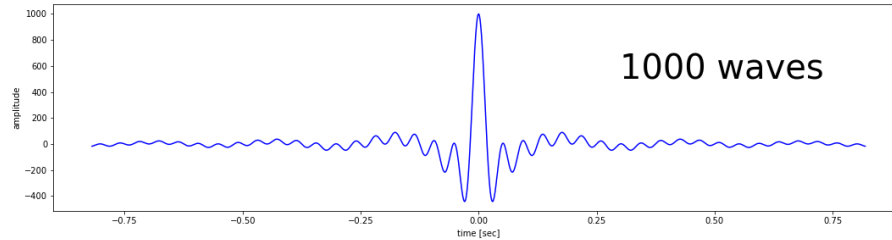
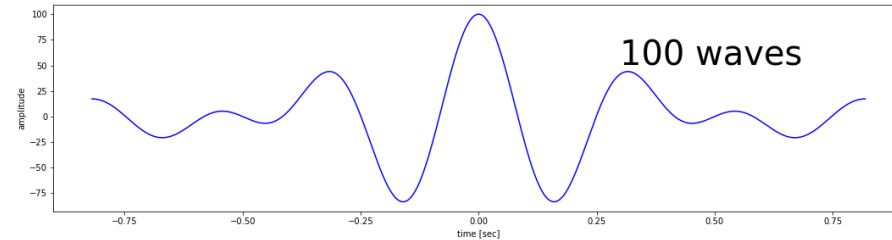
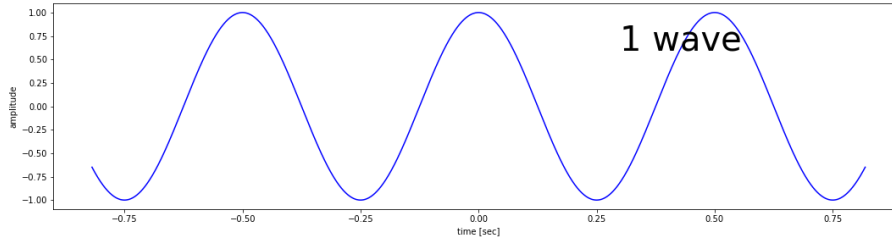
Remember this when we will treat bunches!

Image taken from https://wiki.seg.org/wiki/Dictionary:Fourier_transform

Time pulse = infinite spectrum of sin-waves



DC Shift $S(f) = 1$

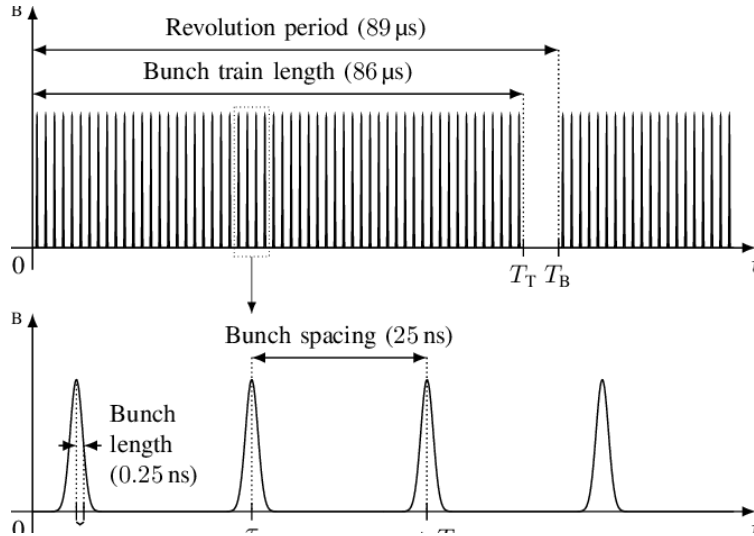



A pulse at $t=0$ corresponds to an overlap of an infinite number of sin-waves with all possible frequencies of infinite length!

In the example at left a base wave is generated and then new waves are added each time with a 1% higher frequency.

Nice example to show that a correct mathematical model not necessarily corresponds to reality!
Imagine an electrical pulse of a generator:
The waves generated should already have existed before the generator was built!
So "infinity" is not always "infinity"

Now we need some definitions in order to treat particle bunches



In real accelerators not all available RF-buckets are filled with particle bunches.

- a gap must be left for the injection/extraction kickers
- Physics experiments can impose a minimum bunch distance, which is larger than one RF period (i.e. LHC)

Revolution frequency: $\omega_{\text{rev}} = 2\pi f_{\text{rev}}$

RF frequency: $\omega_{\text{RF}} = 2\pi f_{\text{RF}} = h^* \omega_{\text{rev}}$ (h=harmonic number)

Bunch Repetition frequency: $\omega_{\text{rep}} = 2\pi f_{\text{rep}} = \omega_{\text{RF}} / n$ (n= number of RF buckets between bunches)
($f_{\text{rep}} = 1/\text{bunch spacing}$)

Nominal LHC Filling Scheme

"Standard Filling Schemes for Various LHC Operation Modes", R. Bailey and P. Collier, [LHC-Project-note-323](#).

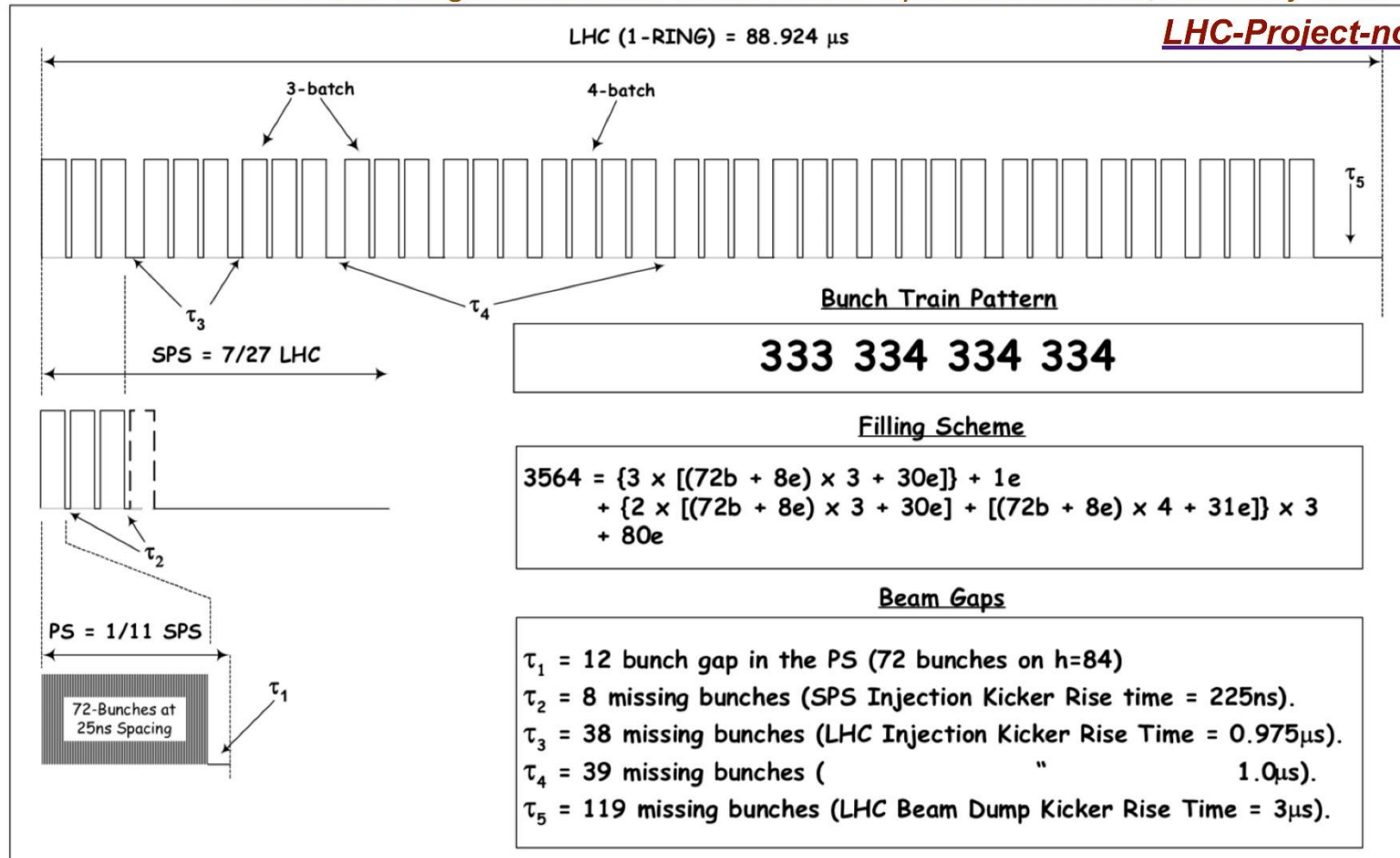


Figure 1: Schematic of the Bunch Disposition around an LHC Ring for the 25ns Filling Scheme

Understanding beam signals in time and frequency domain

We start with:

Single bunch single pass

- Time and frequency domain description
- Measurement of bunch length in time domain
 - Sampling electrical signals with ADCs
- Measurement of bunch length in frequency domain

Time domain

$$f(t) = A_0 \exp\left(-\frac{t^2}{2\sigma_t^2}\right)$$

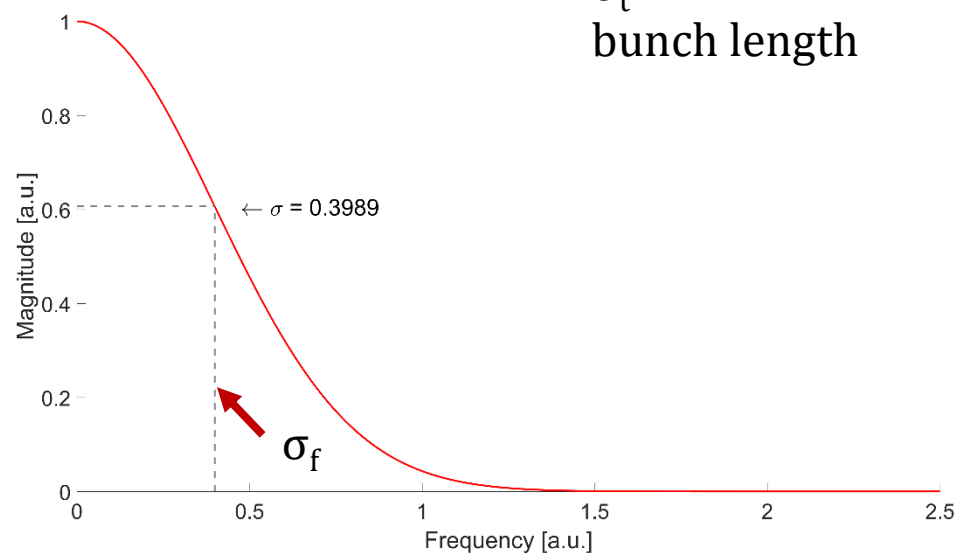
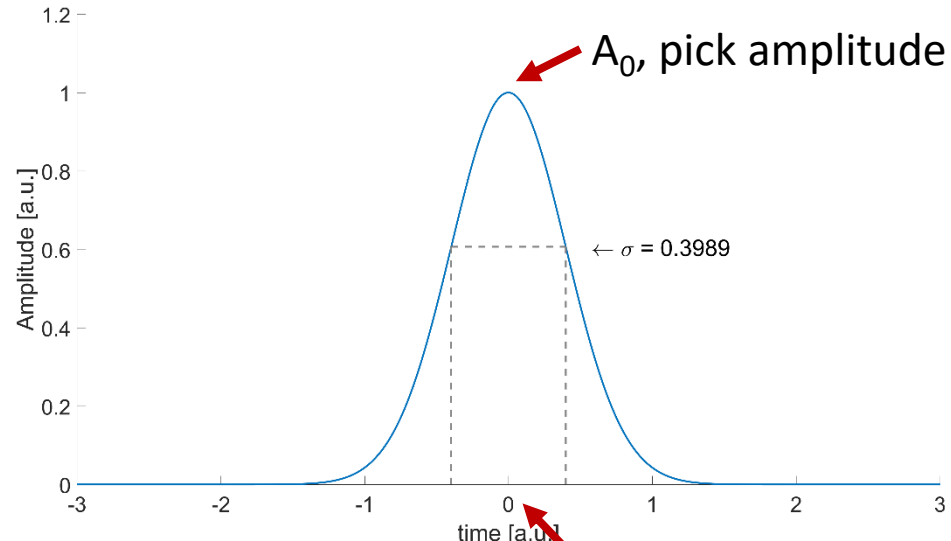
$$area = \int_{-\infty}^{+\infty} f(t) dt = \sqrt{2\pi} A_0 \sigma_t$$

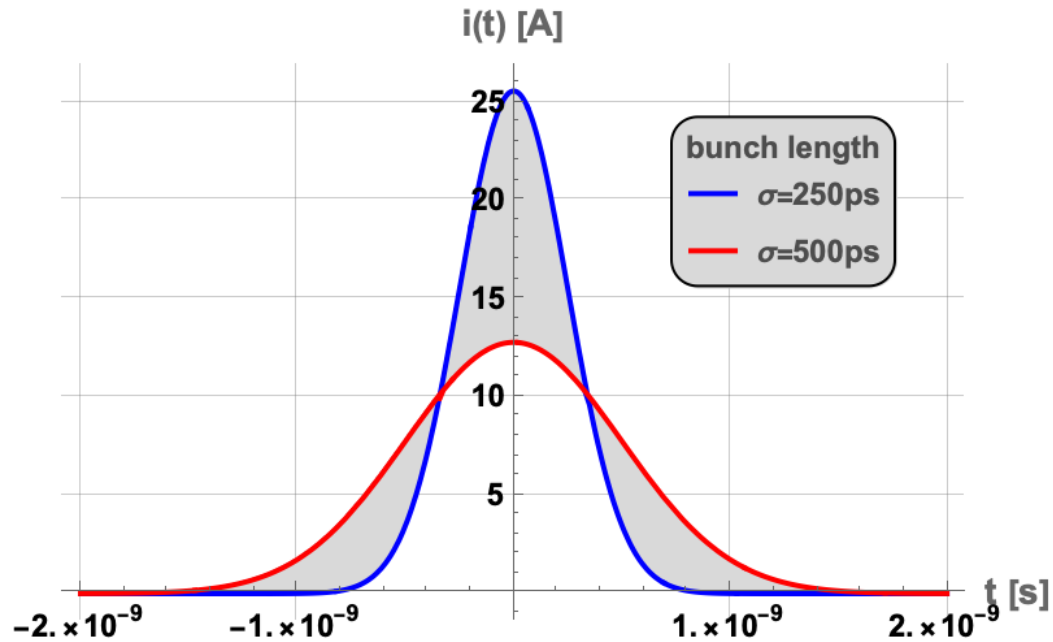
Frequency domain

$$F(k) = \frac{A_0}{\sqrt{2\pi}\sigma_f} \exp\left(-\frac{k^2}{2\sigma_f^2}\right)$$

$$\sigma_f = \frac{1}{2\pi\sigma_t}$$

$$F(0) = area = \frac{A_0}{\sqrt{2\pi}\sigma_f} = \sqrt{2\pi} A_0 \sigma_t$$





In many cases the description of the longitudinal bunch signal as “Gaussian” is adequate and sufficient. Depending on the study, more sophisticated descriptions are needed (next slide).

Typical bunch length for circular (high energy accelerators):

Protons: ~ 50 ns...0.5 ns (LHC) electrons: 1ns ... ~ 10 ps (LEP)

time-domain

$$i_{Gauss}(t) = \frac{zeN}{\sqrt{2\pi}\sigma_t} e^{-\frac{t^2}{2\sigma_t^2}}$$

$$i_{\cos^2}(t) = \begin{cases} \frac{zeN}{t_b} \left(1 + \cos \frac{2\pi t}{t_b}\right), & -t_b/2 < t < t_b/2 \\ 0, & \text{elsewhere} \end{cases}$$

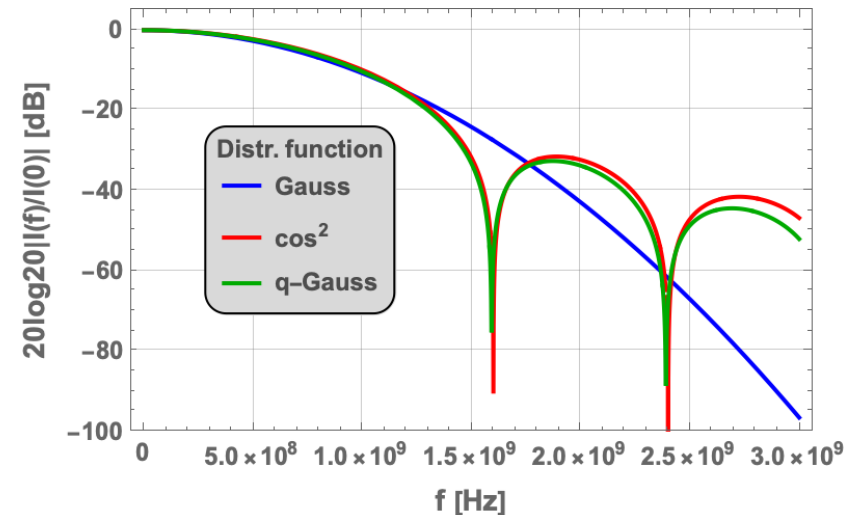
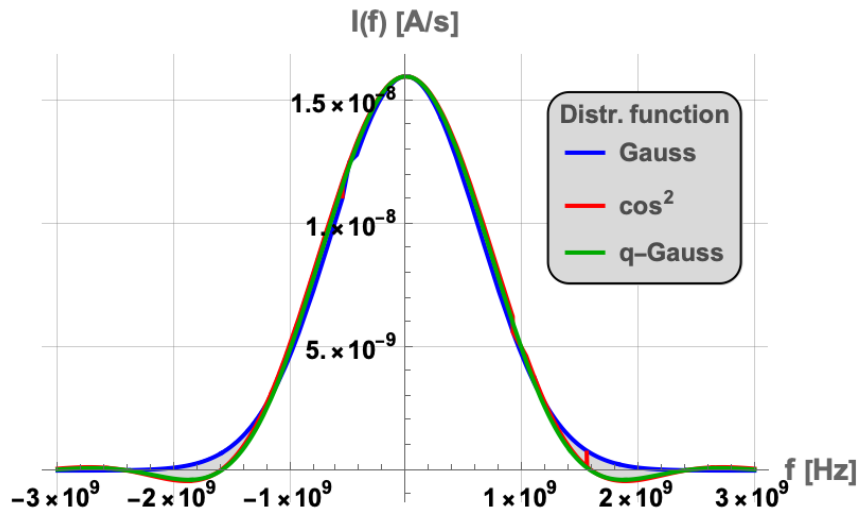
$$i_{q-Gauss}(t) = \frac{zeN \sqrt{1-q} \left(1 + \frac{(q-1)t^2}{2\beta_t^2}\right)^{\frac{1}{1-q}}}{\sqrt{2\pi}\beta_t \Gamma\left(1 + \frac{1}{1-q}\right)}, \quad q < 1$$

$$I_{q-Gauss}(f) = \frac{zeN(1-q) \left(\frac{1-q}{2}\right)^{\left|\frac{1}{2} - \frac{q}{1-q}\right|/2} J_{\frac{1}{1-q} + \frac{1}{2}} \left(2\pi f \beta_t \sqrt{\frac{2}{1-q}}\right) \Gamma\left(\frac{1}{1-q} + \frac{3}{2}\right)}{2f^{\frac{1}{1-q} + \frac{1}{2}} \pi^{\frac{1}{1-q} + \frac{1}{2}} \beta_t^{\frac{1}{1-q} + \frac{1}{2}}}$$

frequency-domain

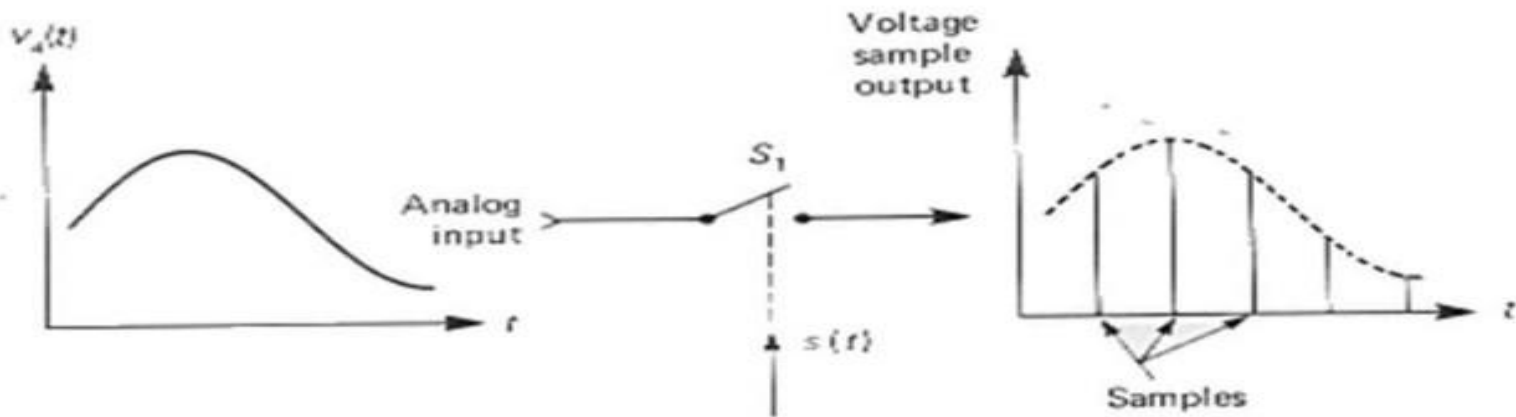
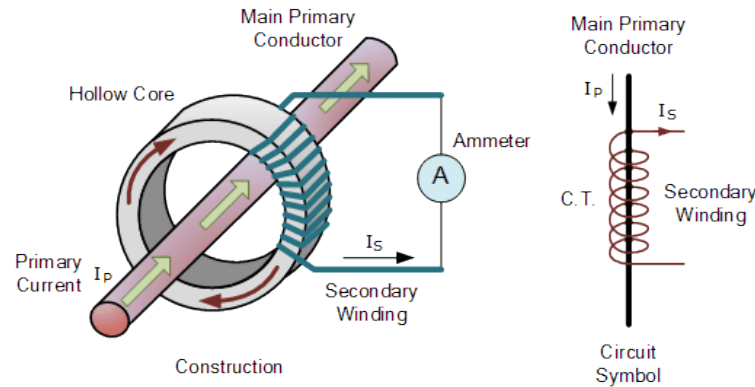
$$I_{Gauss}(f) = zeN e^{-2(\pi f \sigma_t)^2}$$

$$I_{\cos^2}(f) = \frac{zeN \sin \pi f t_b}{\pi f t_b [1 - (f t_b)^2]}$$



Time domain measurement of single bunch

- Sampling (=measurement) of an electrical signal in regular time intervals. The electrical signal is obtained from a monitor, which is sensitive to the particle intensity.



A few slides on Analog-digital conversion

Quantization error

- Here we consider only an ideal quantization of a continuous signal (no sampling). Quantized signal is an approximation of the input signal; their difference is the quantization noise.

- Used quantities:

- A – input signal amplitude
- n – number of bits
- q – one bit amplitude:

$$q = \frac{2A}{2^n}$$

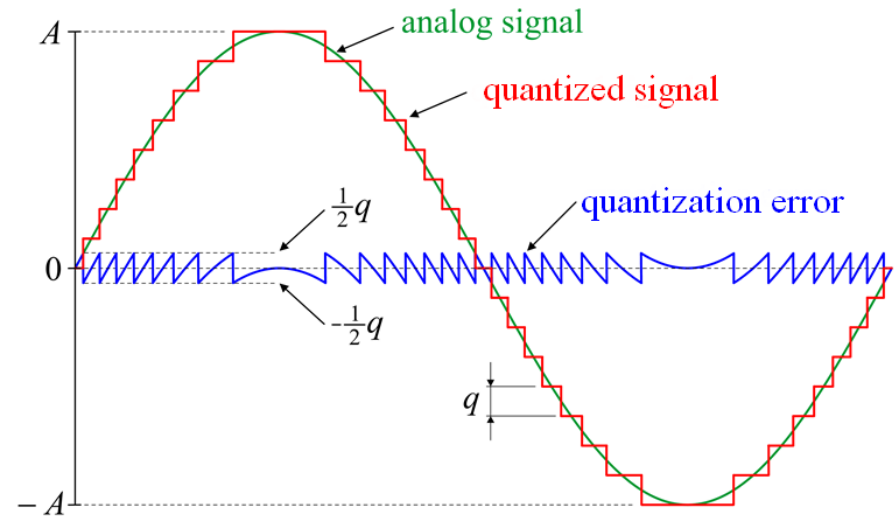
- Max quantization error: $e_m = \frac{\pm q}{2}$

- RMS amplitude of the input signal: $A_{RMS} = \frac{A}{\sqrt{2}}$

- Quantisation error RMS amplitude: $e_{RMS} = \frac{1}{\sqrt{12}} q \cong 0.289 q$

- Signal to Noise Ratio: $SNR = \frac{A_{RMS}}{e_{RMS}} = \frac{\sqrt{6}}{2} 2^n$ $SNR \text{ [dB]} = 20 \log_{10} \frac{\sqrt{6}}{2} 2^n \cong 1.76 + 6.02 n$

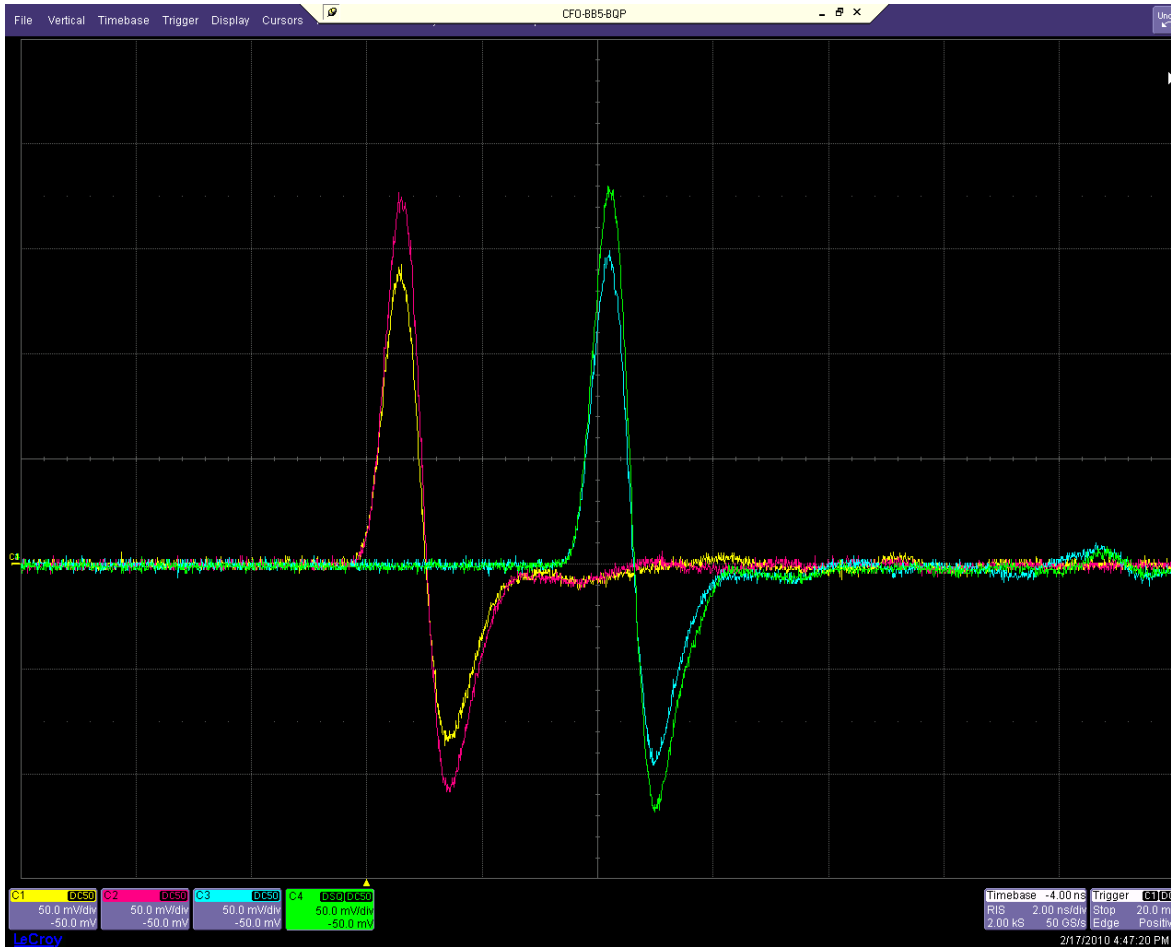
- Effective Number of Bits: $ENOB = \frac{SNR \text{ [dB]} - 1.76}{6.02}$



ADC's: Further considerations

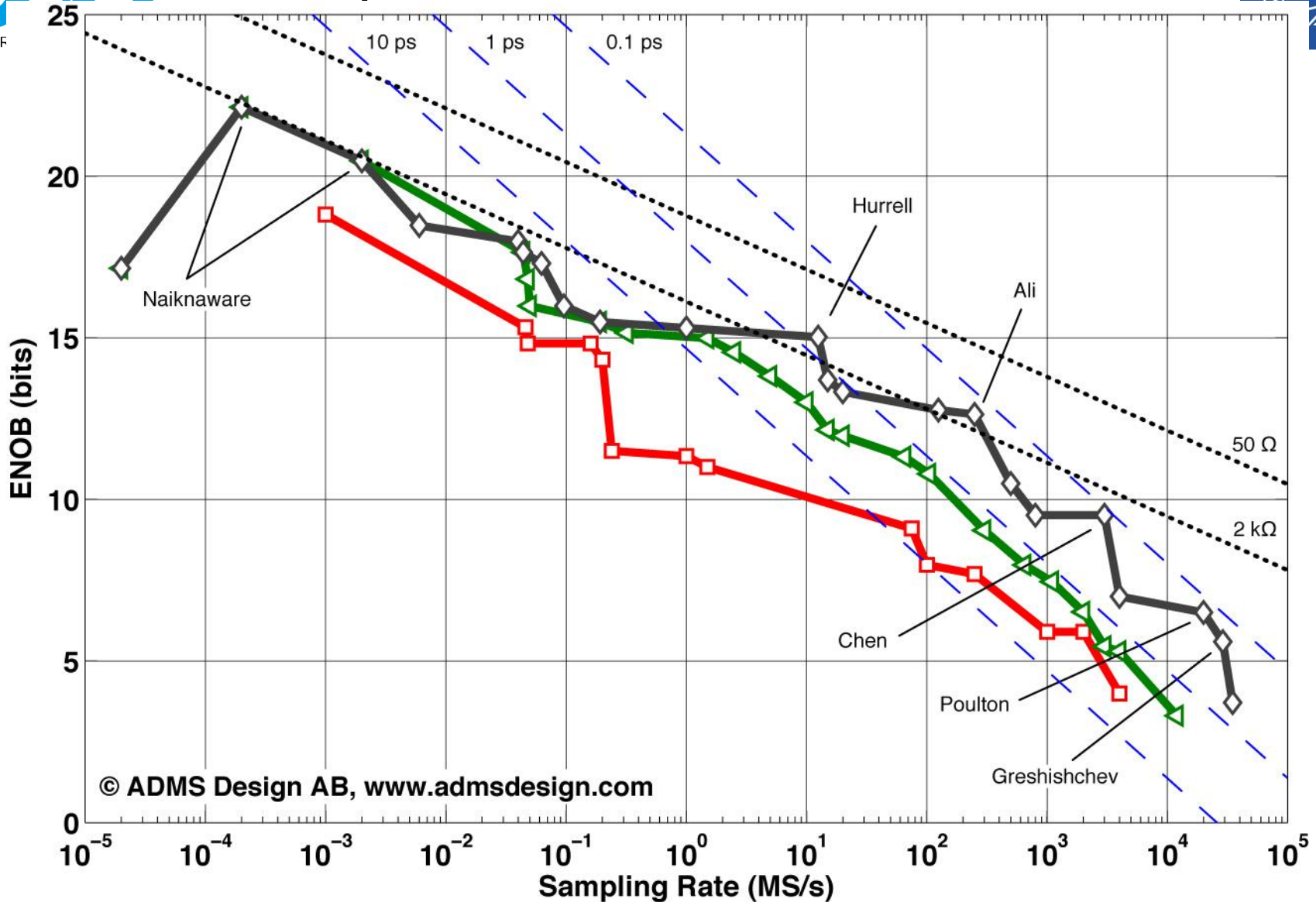
- Simple case: digitization of continuous signals
- Beam signals are different:
 - usually short pulses
 - shape of pulses changes due to beam dynamics
 - good idea is to “look” at these signals with analogue means (analogue oscilloscopes) before using digitized information and/or use filtering
- Criteria/buzzwords to design an ADC system:
 - required resolution → number of bits
 - required bandwidth → sampling frequency
 - stability/synchronicity of ADC clock → clock jitter
 - signal level → use full scale of ADC
 - noise contribution: shielding, low impedance signals (low thermal noise)

Sampling a pulse



- 50 mV/div, 2 ns/div
- SPS beam
- 2 pairs of 10 mm button electrodes
- Signals already “filtered” by quite long cables

ADC performance chart from 2018!



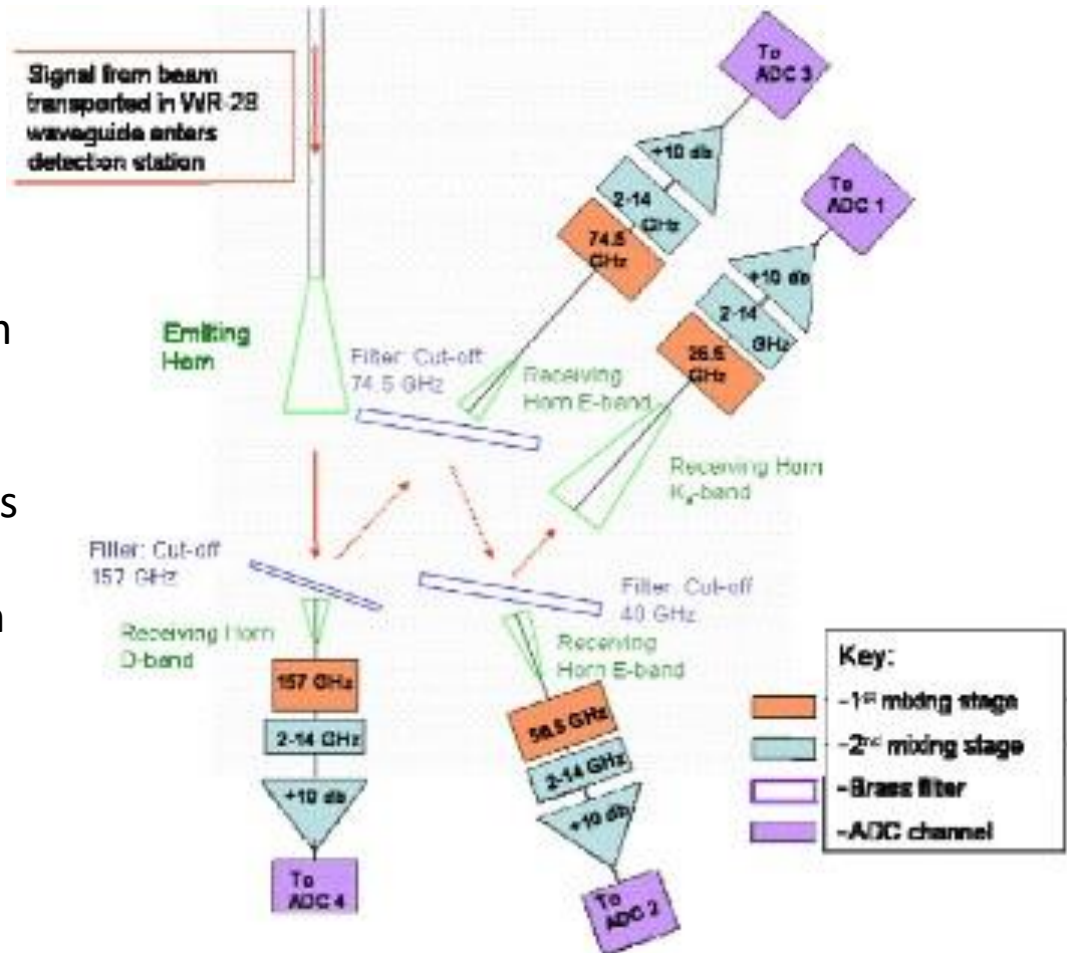
© ADMS Design AB, www.admsdesign.com

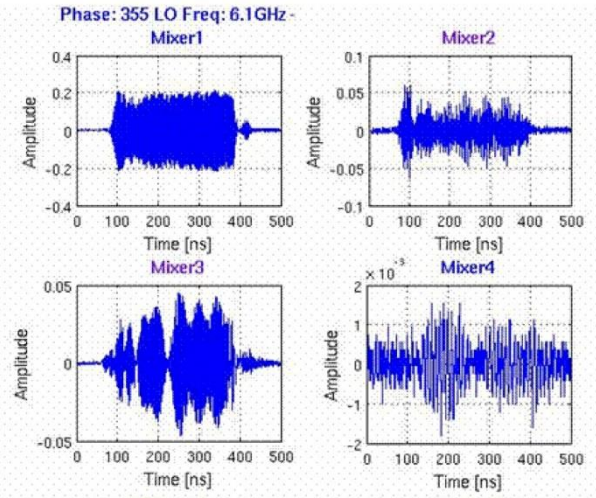
Nice example from R&D work in CTF3 (CERN)
 A.Dabrowski et al., Proc of PAC07, FRPMS045

Primary signal is EM wave of beam extracted through a thin window

Subdivision into 4 frequency bands

Measurement of rms amplitude in the 4 bands





Time domain measurements of 4 bands

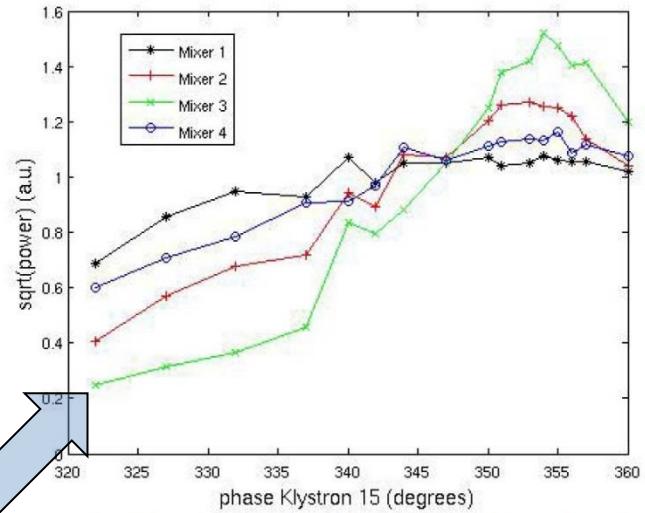
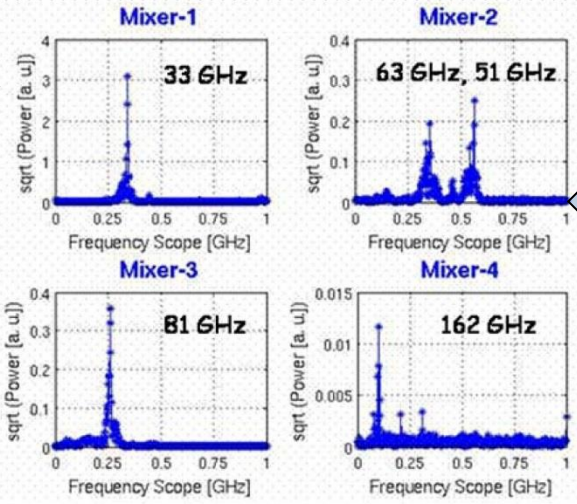


Figure 5: Signal amplitudes from the 4 selected frequencies as a function of the phase in Klystron 15.



FFT of down-converted signals

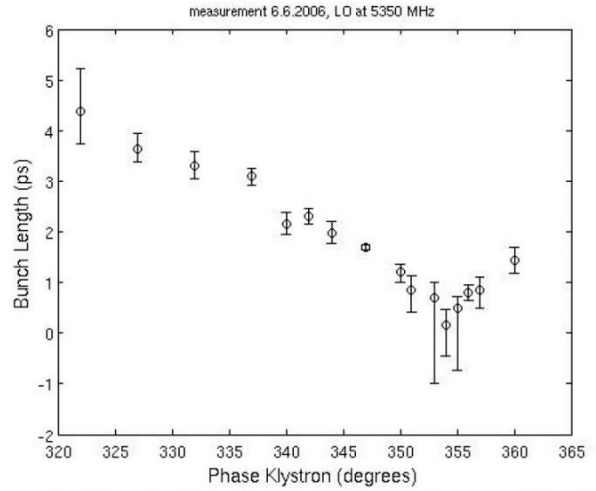


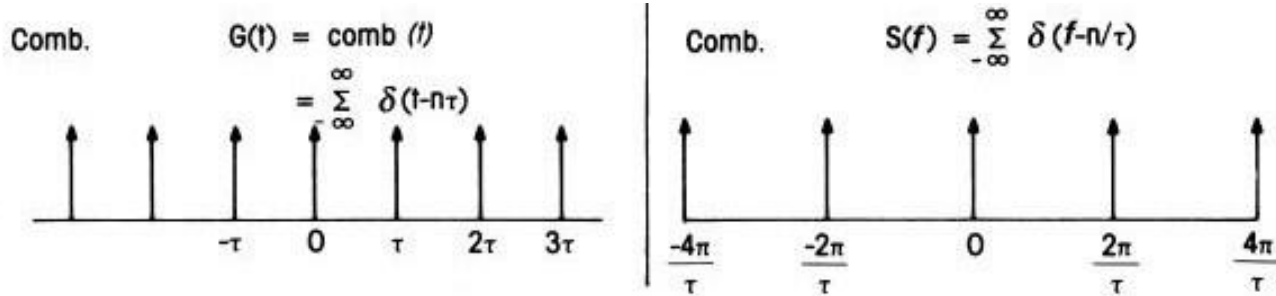
Figure 6: Bunch length measurements as a function of the phase of Klystron 15

fit

After these introductory remarks we shall look at signals produced in an accelerator and understand them:

1. Single bunch single passage: Already done
2. Single bunch - multi pass
3. Multi bunch – multi pass...will be a bit mind boggling, but still very relevant!

Remember:



Time domain

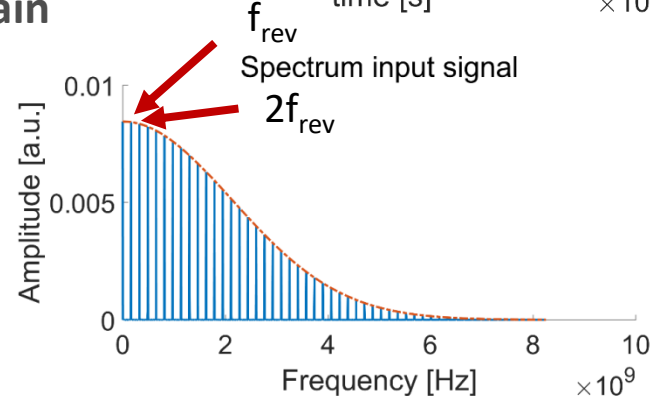
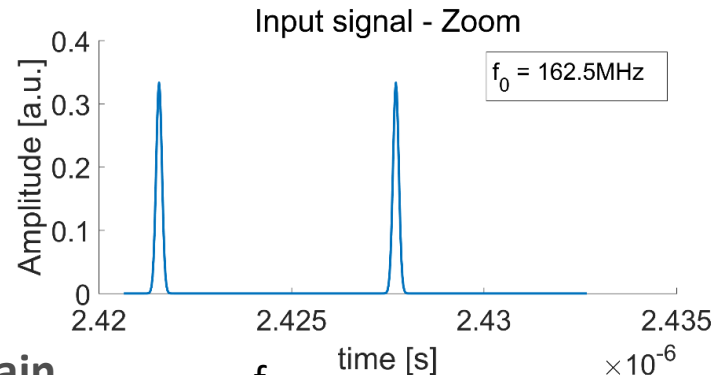
$$f(t) = \sum_{n=1}^N A_0 \exp\left(-\frac{(t - nT)^2}{2\sigma_t^2}\right)$$

$$area = \int_{-\infty}^{+\infty} f(t) dt = N \times \sqrt{2\pi} A_0 \sigma_t$$

Frequency domain

$$F(k) = \sum_{i=1}^N F_c(ik_0) \exp\left(-\frac{(k - ik_0)^2}{2\sigma_f^2}\right),$$

$$\sigma_f = \frac{1}{2\pi\sigma_t}$$

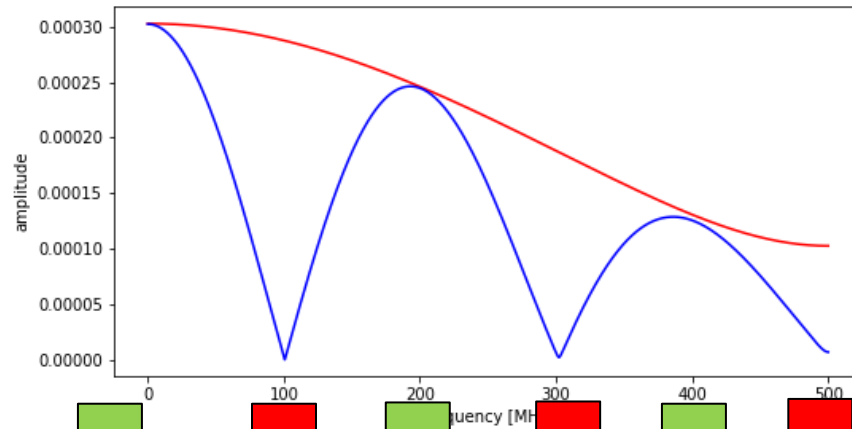
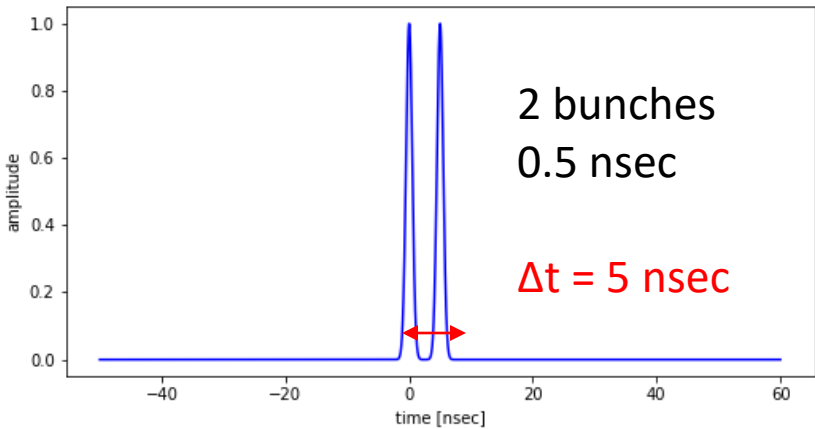
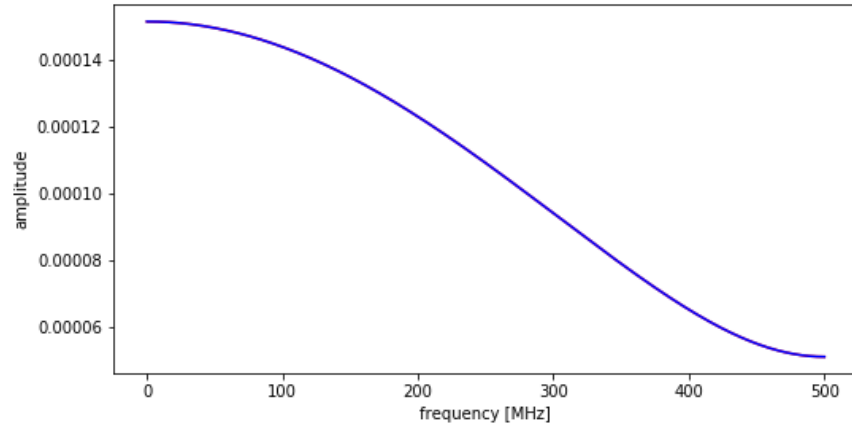
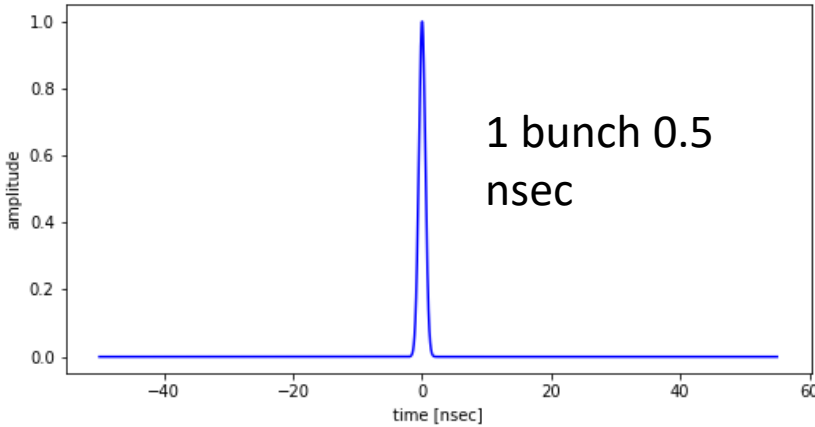


- The continuous spectrum of a single bunch passage becomes a line spectrum.
- The line spacing is $f_{\text{rev}} = 1/T_{\text{rev}}$. (T_{rev} = revolution time)
- The amplitude envelope of the line spectrum is the “old” single pass frequency domain envelope of the single bunch.

- Why?
 - short answer: **Do the Fourier transform!**
 - long answer:
Understand in more detail 2,3,4...N consecutive bunch passages in time and frequency domain (next slides)

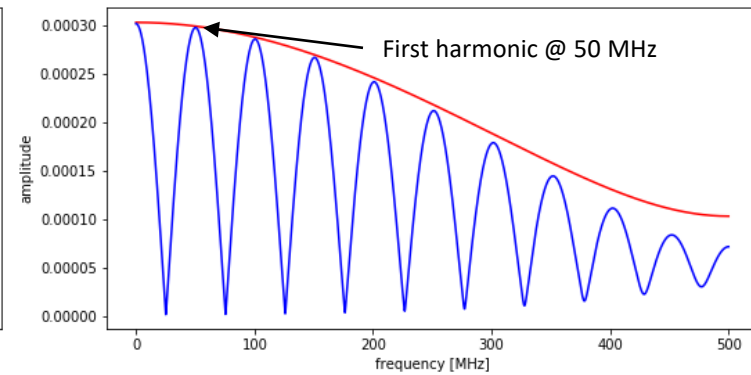
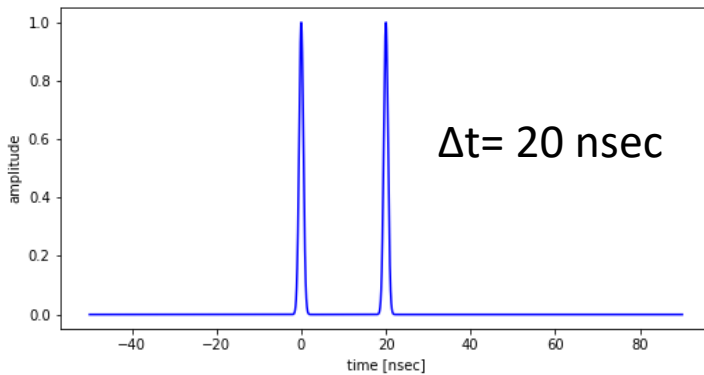
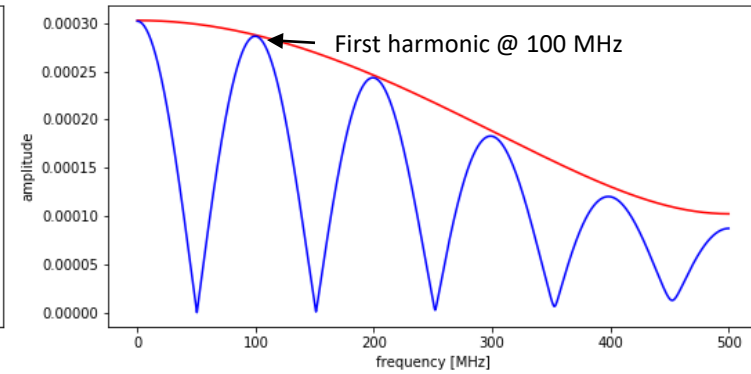
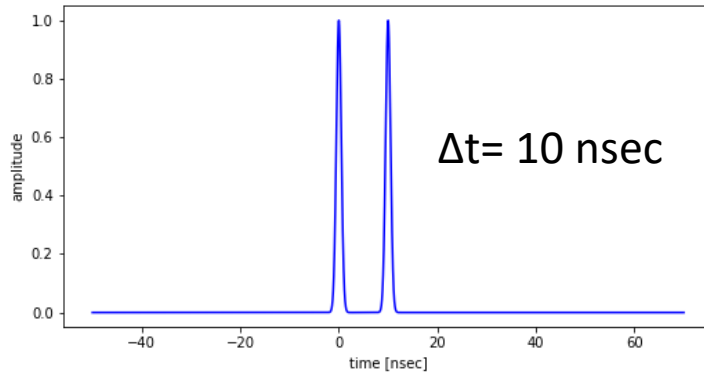
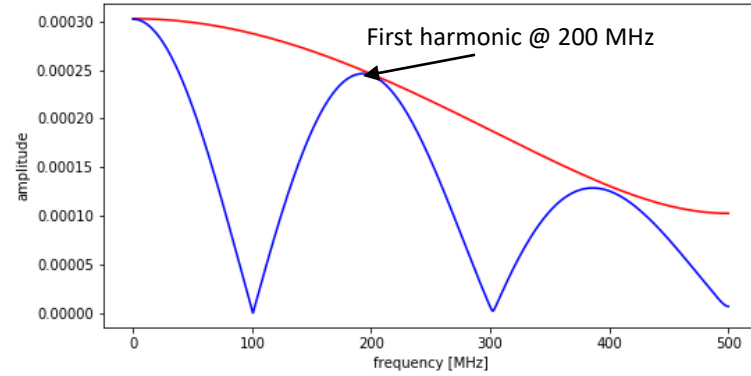
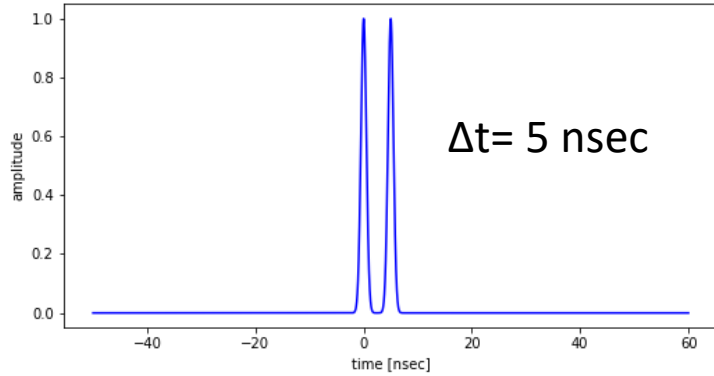


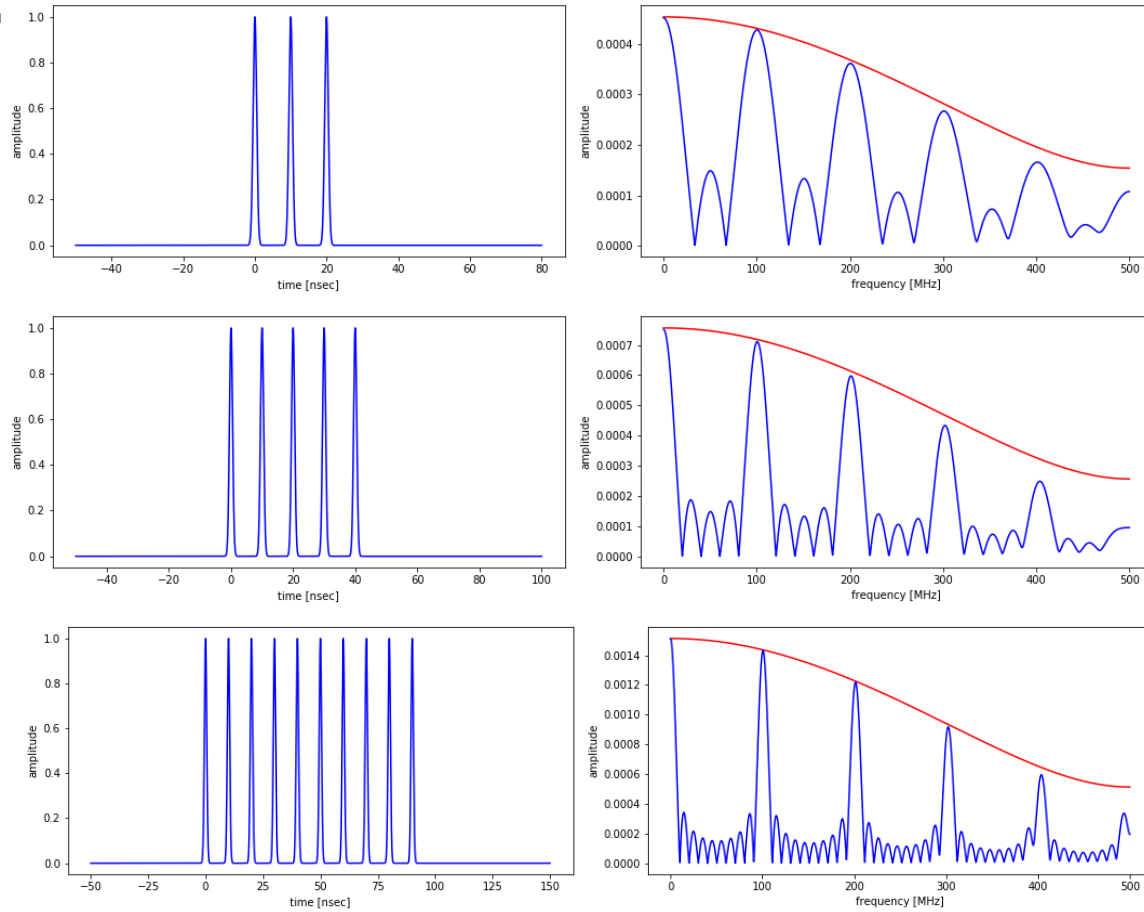
Bunch pattern simulations (1/4)



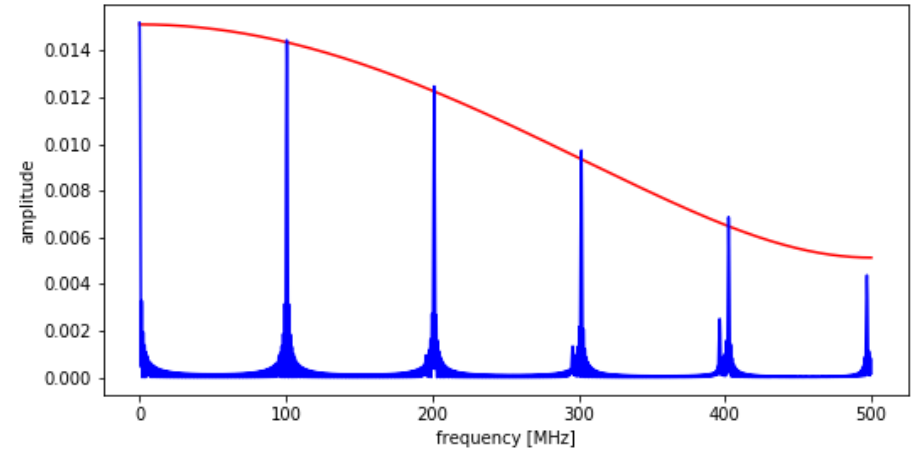
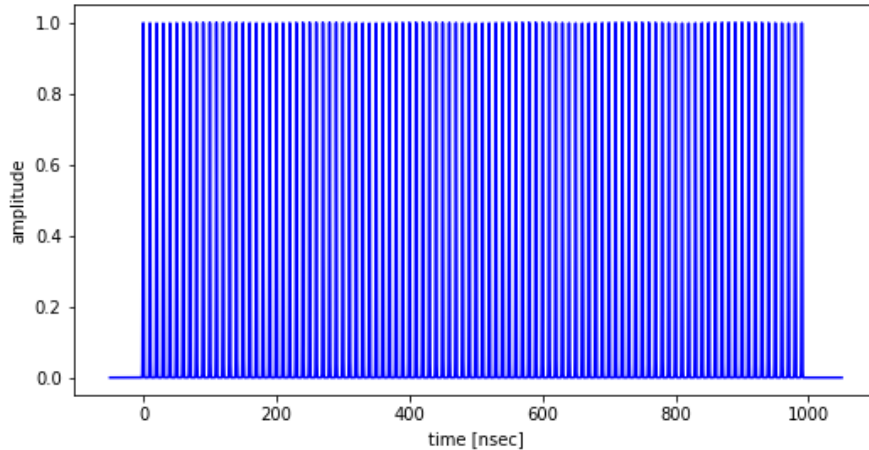
- Frequencies in this range make a constructive interference (no phase difference)
- Frequencies in this range cancel each other (180° phase difference)
- Other frequencies intermediate summation/cancelation

Bunch pattern simulations (2/4)





From top to bottom:
 3, 5, 10 bunches (0.5nsec long, $\Delta t = 10$ nsec)



- 100 equidistant bunches ($\Delta t = 10$ nsec)
- Resulting spectrum is a line spectrum with the fundamental line given by the inverse of the bunch distance

- **Circular accelerator**

→ Beam signal periodic with **revolution frequency**: ω_{rev}

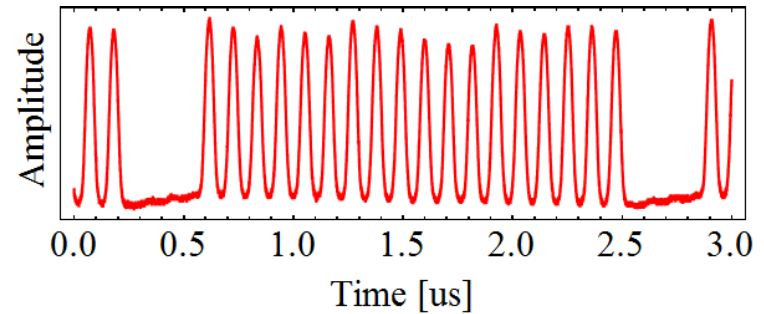
→ **Spectral components at:**

$$\omega = n\omega_{\text{rev}}$$

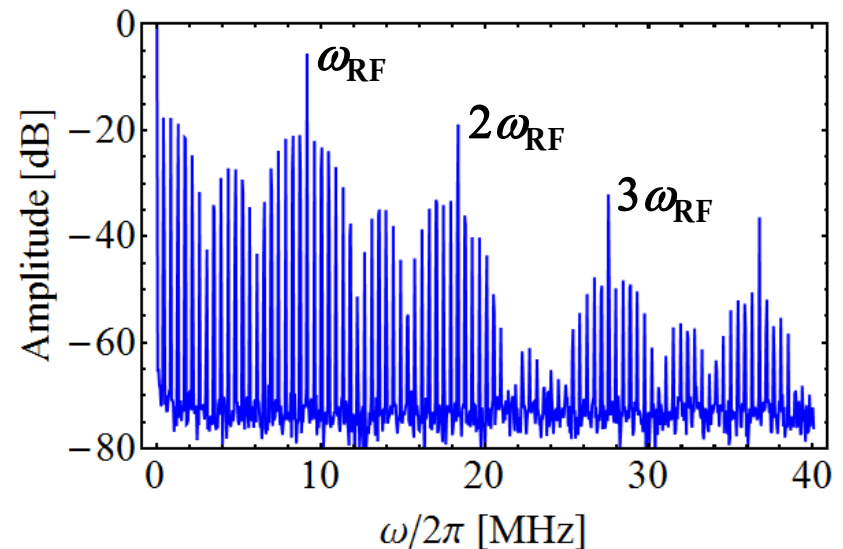
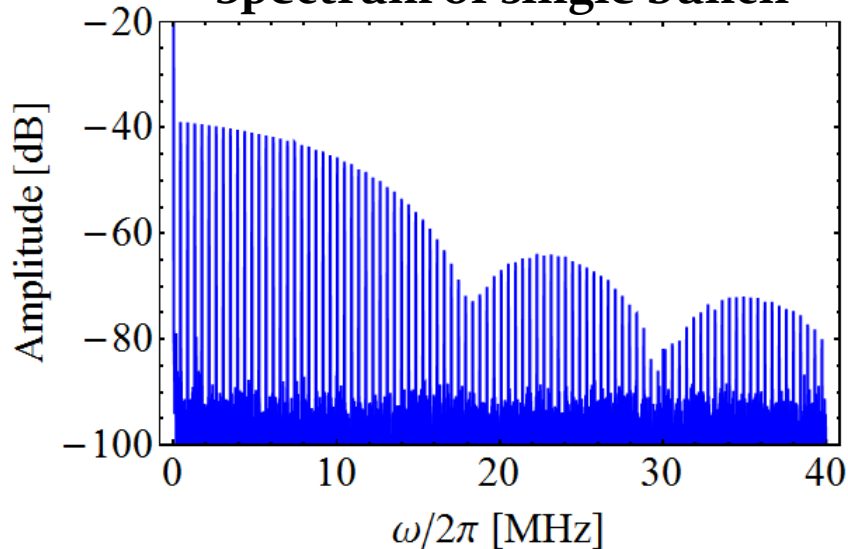
Bunch not Gaussian.

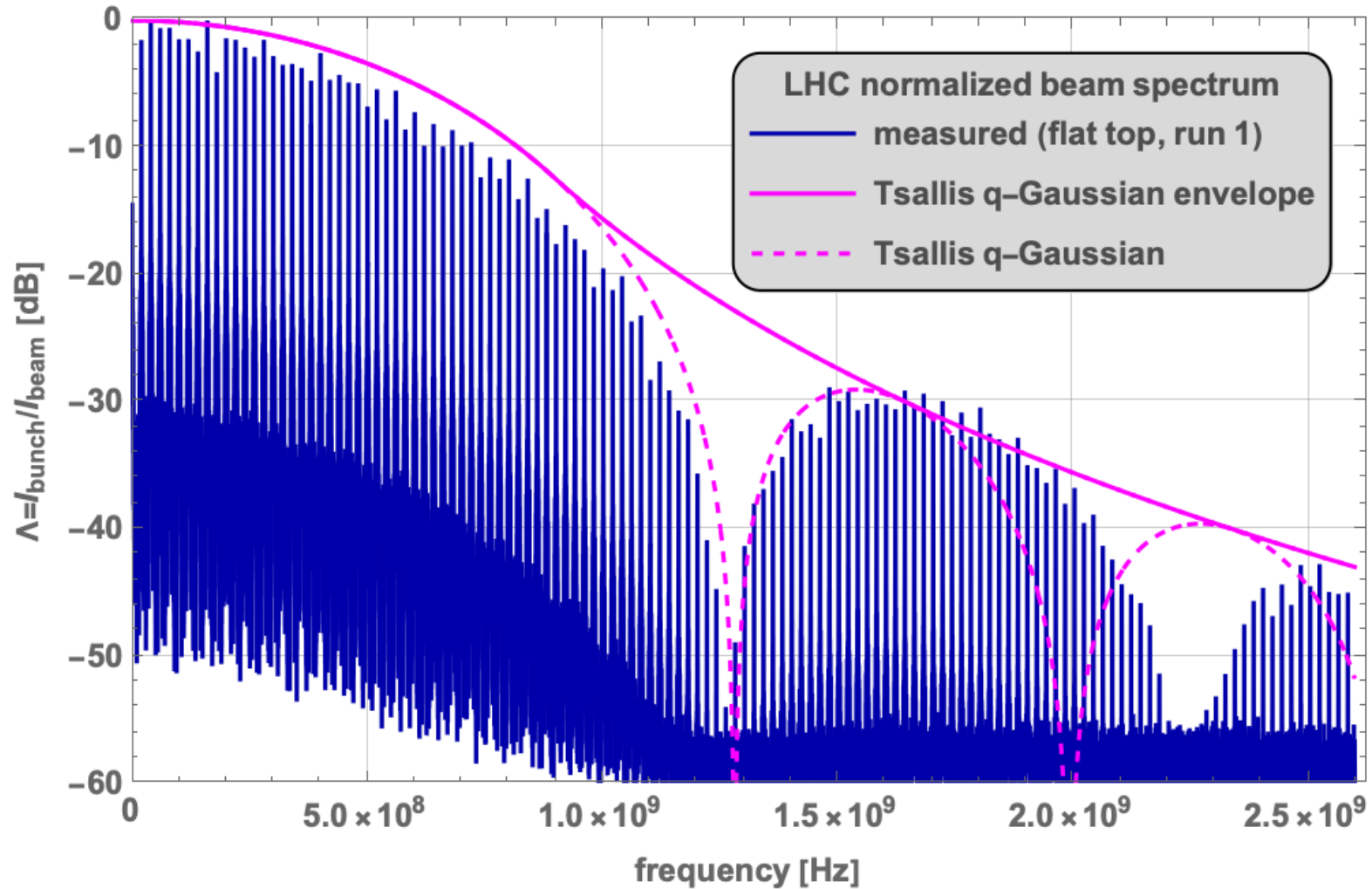
Somewhat between triangular and parabolic

Multi-bunch beam



Spectrum of single bunch

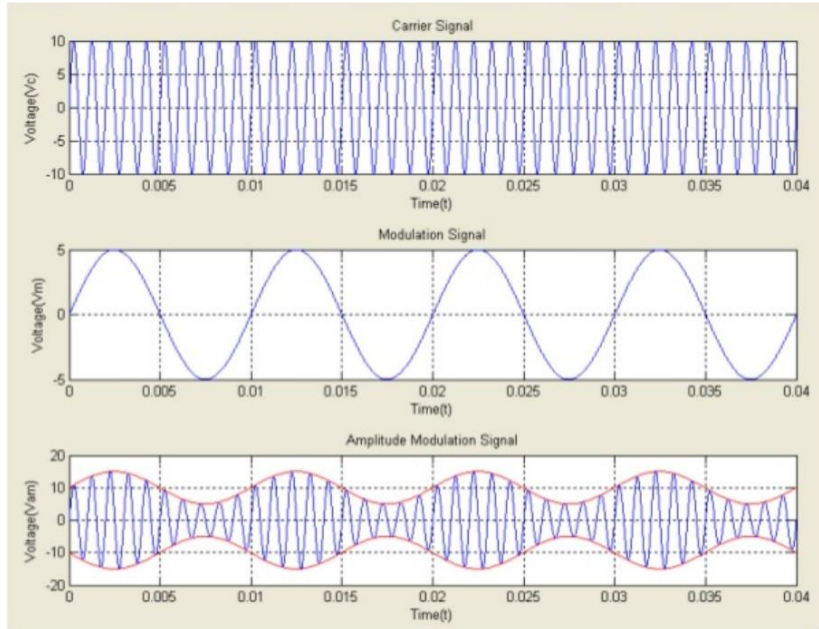




And if this was not enough:

amplitude modulation of bunch signals

Any amplitude modulation in time domain leads to sidebands in frequency domain



Using trigonometric identity:

$$(\sin a)(\sin b) = 1/2 [\cos(a-b) - \cos(a+b)]$$

$$v = V_c \sin 2\pi f_c t$$

$$+ \frac{m}{2} V_c \cos 2\pi(f_c - f_m)t$$

$$- \frac{m}{2} V_c \cos 2\pi(f_c + f_m)t$$

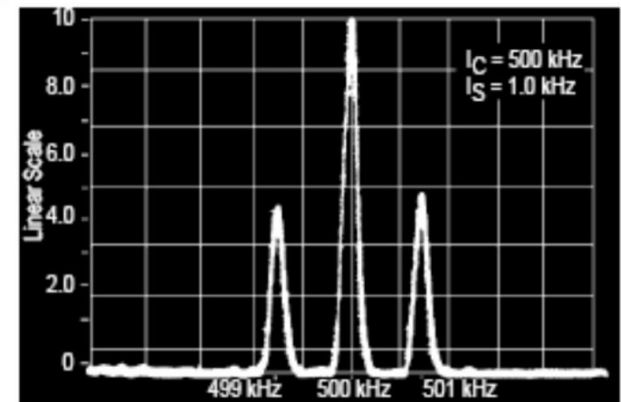
$$v_{AM} = V_c \sin 2\pi f_c t + \frac{V_m}{2} \cos 2\pi(f_c - f_m)t - \frac{V_m}{2} \cos 2\pi(f_c + f_m)t$$

Carrier LSB USB

$$v = V_{env} \sin 2\pi f_c t$$

$$= V_c (1 + m \sin 2\pi f_m t) \bullet \sin 2\pi f_c t$$

m = modulation index 0...1 ($V_{env} = V_c$)



Relevant example of amplitude modulation:
stimulated betatron oscillation(or: tune measurement)

this means an amplitude modulation of the intensity signal by transverse excursions

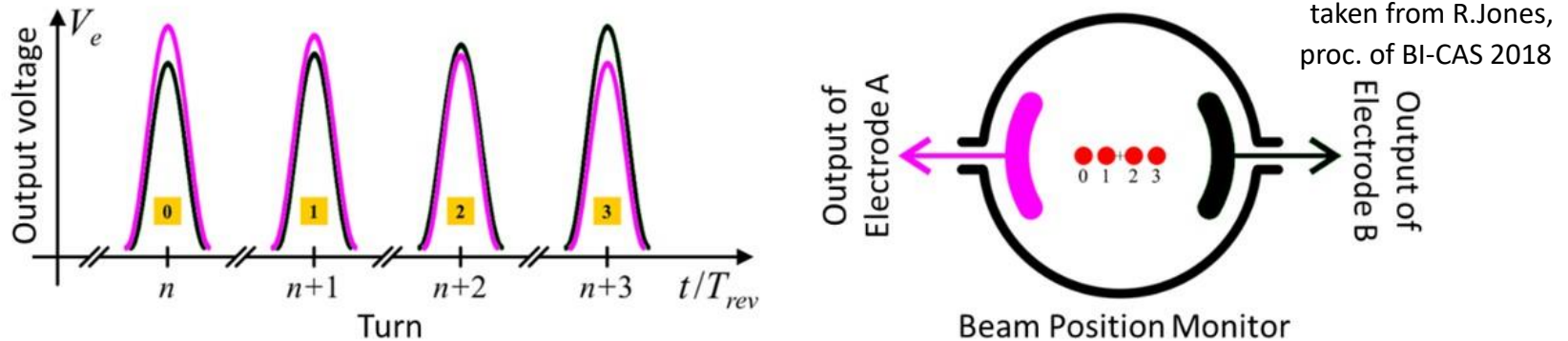
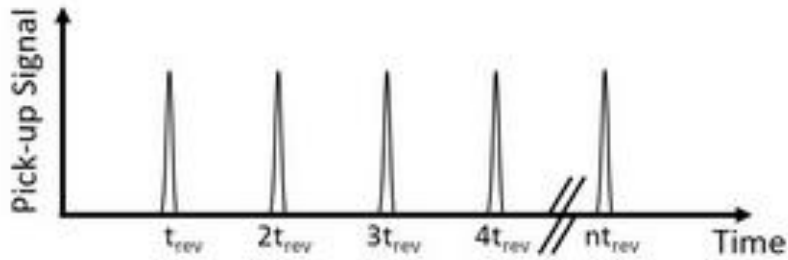


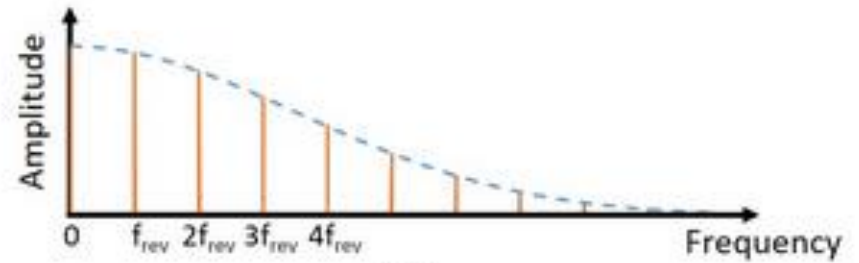
Fig. 4: Detecting oscillations using a beam position monitor. The oscillation information is superimposed as a small modulation on a large intensity signal.

Beam centre of charge makes small betatron oscillation around the closed orbit
(- stimulated by an exciter or by a beam instability)

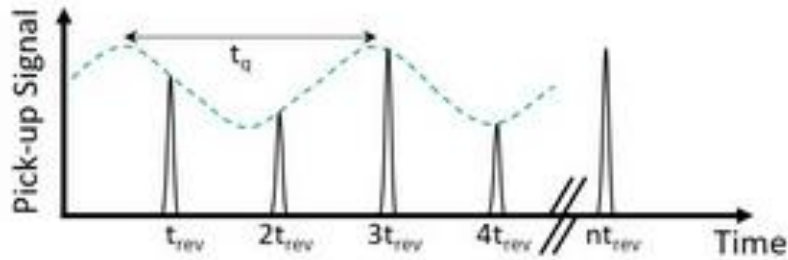
Depending on the proximity to an EM sensor the measured signal amplitude varies.



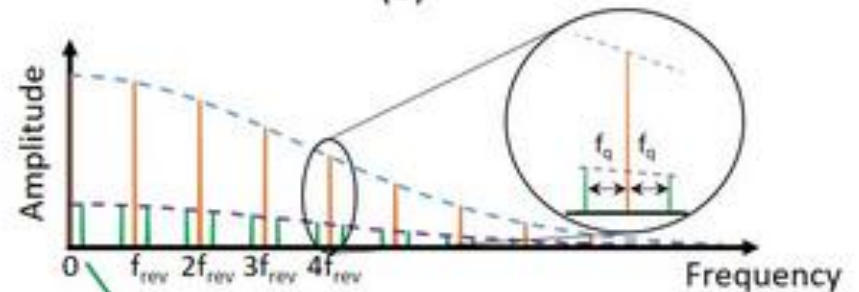
(a)



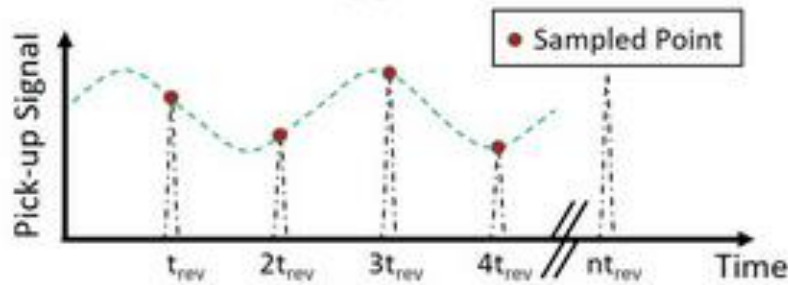
(b)



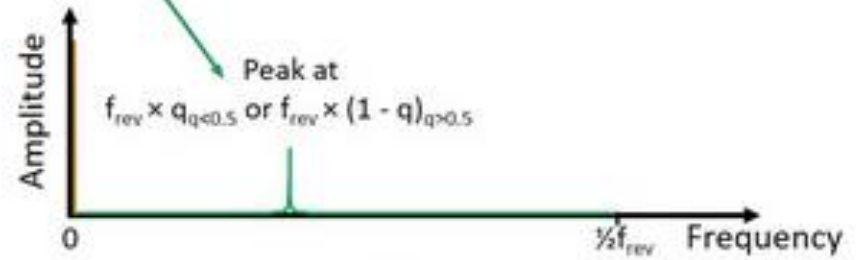
(c)



(d)



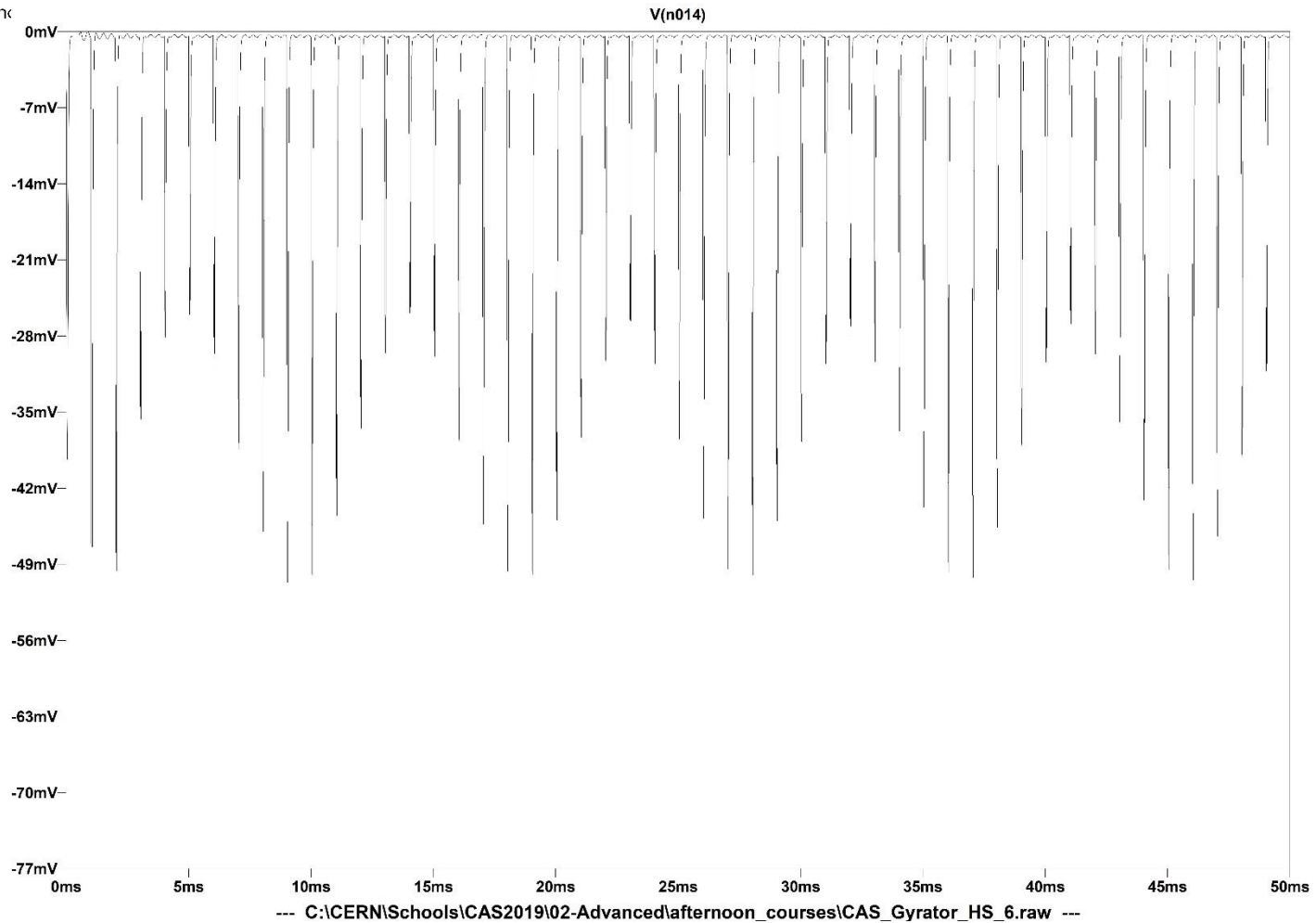
(e)



(f)

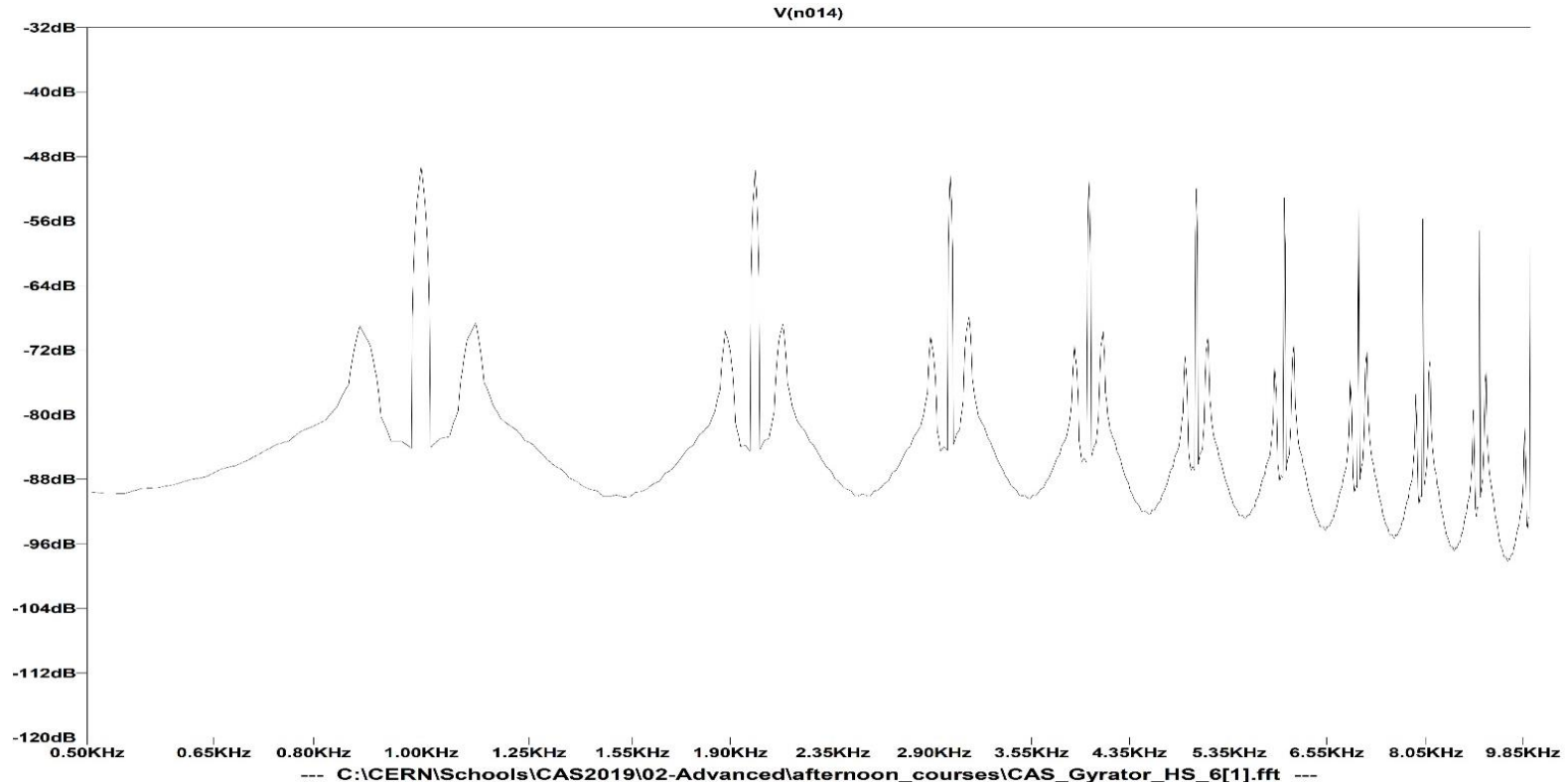
circumference of the accelerator. (a & b) continuous measurement without betatron oscillation; (c & d) continuous measurement undergoing betatron oscillation (50% modulation); (e & f) sampled once per revolution.

A measured signal as example



Time domain signal of one beam sensor during a betatron oscillation of the beam (visible as amplitude modulation)

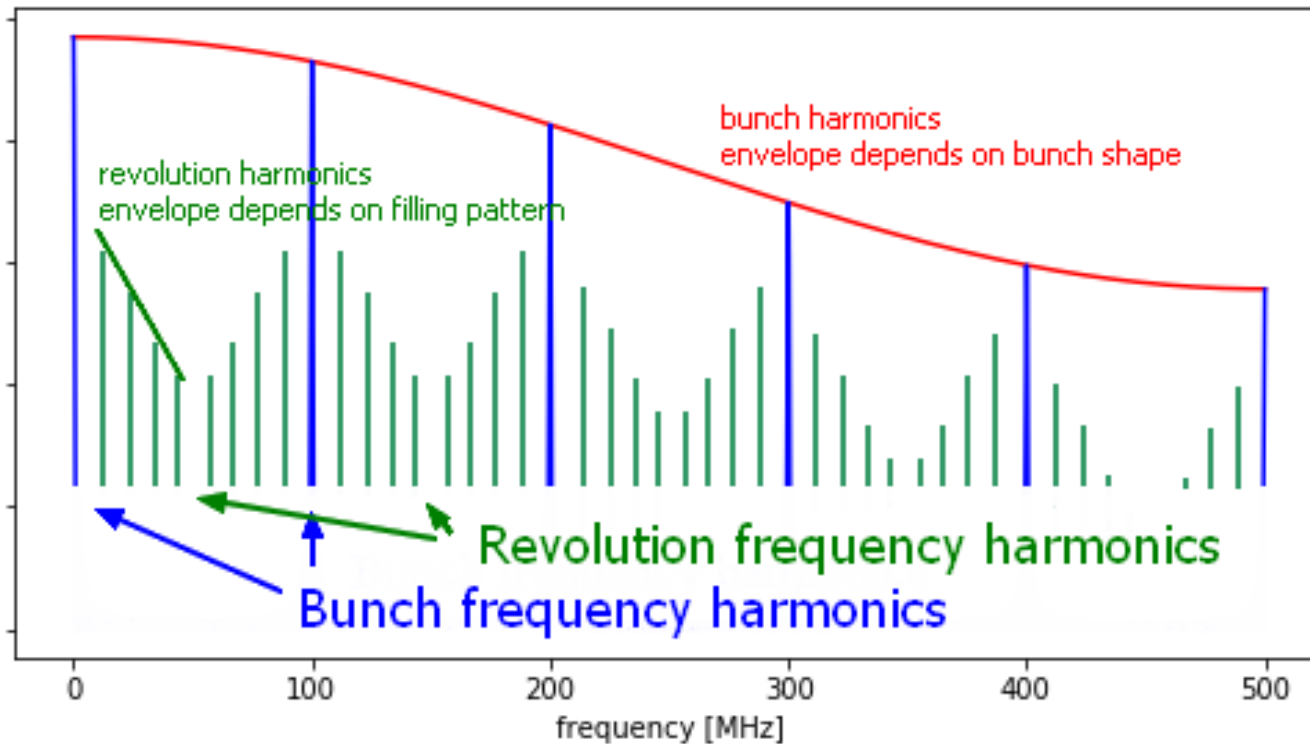
The same in frequency domain



As expected revolution lines (attention log. X-axis!) with betatron side bands.

One bunch/several bunches?

- In the case of more than one bunch (N) in the accelerator (**assume equal intensities filled at equal distances!**) one cannot distinguish between
 - an accelerator with **1 bunch** and a revolution time of t_{rev}
 - an accelerator with **N bunches** and a revolution time of t_{rev} / N **!**

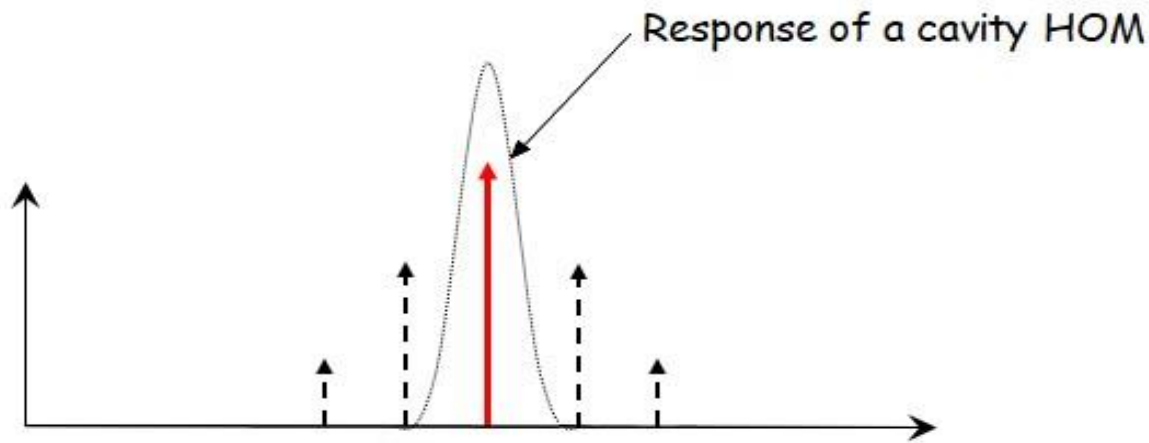


Multi-bunch multi-pass

- If one has **N bunches** of equal intensity circulating in an accelerator with T_{rev} and those bunches only move coherently without any phase difference, then this is undistinguishable from an accelerator with T_{rev}/N as revolution time and **one bunch** in this accelerator
- In reality the oscillations of individual bunches are not correlated and in consequence the time domain and frequency domain signals get really mind-boggling.
- The study of these oscillations is important in case of multi-bunch instabilities or in case of the design of transverse active feedback systems

Why do we worry about this?

- The additional bunches will create additional spectral lines in frequency domain. Depending on the number of bunches the spacing between these lines can become so narrow, such that overlap of the beam spectral lines with the resonance of structures around the beam pipe (HOM modes of cavities for example) can excite the beam to oscillations.
- This can lead to beam blow up or even particle losses.



Multi-bunch Multi-pass Mode Analysis



Let us consider M bunches equally spaced around the ring

The bunches do in general **not oscillate coherently**. Instead of following the oscillations of every bunch individually, we describe the motion of every bunch as the **weighted sum of eigenmodes** of oscillations, the so called **multi-bunch modes**.

Each **multi-bunch mode** is characterized by a bunch-to-bunch phase difference of:

$$\Delta\Phi = m \frac{2\pi}{M} \quad m = \text{multi-bunch mode number } (0, 1, \dots, M-1)$$

Each multi-bunch eigenmode is characterized by a set of frequencies:

$$\omega = p M \omega_{rev} \pm (m + \nu) \omega_{rev}$$

Where:

p is an integer number $-\infty < p < \infty$; $p=0$:= baseband

ω_{rev} is the **revolution frequency**

$M\omega_{rev} = \omega_{rep}$ is the **bunch repetition frequency**,

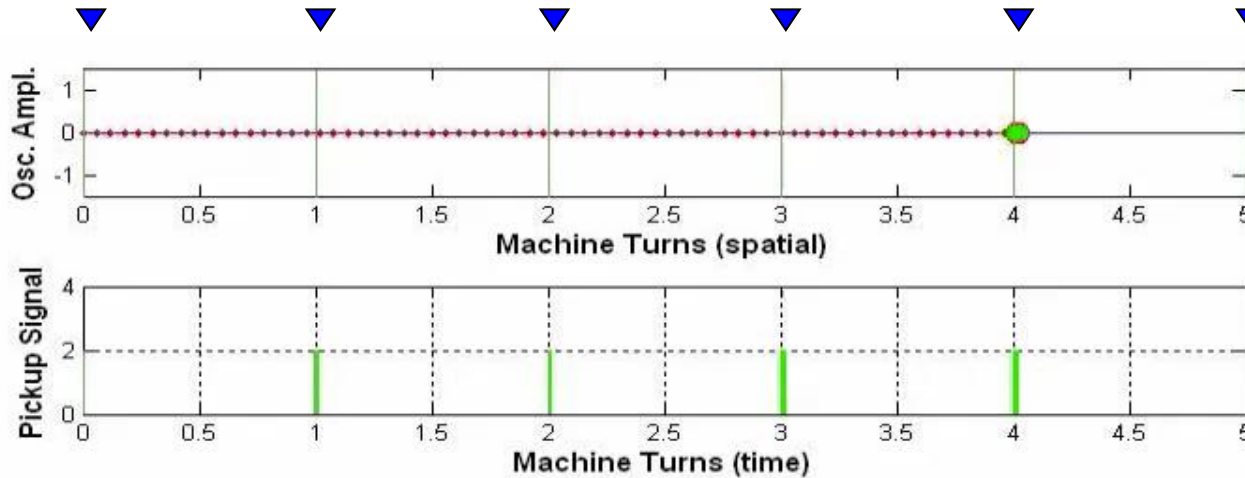
ν is the **tune**, i.e. the **eigenfrequency of transverse or long. oscillations**

Hard to understand like this...needs some graphics

Multi-bunch modes: single stable bunch

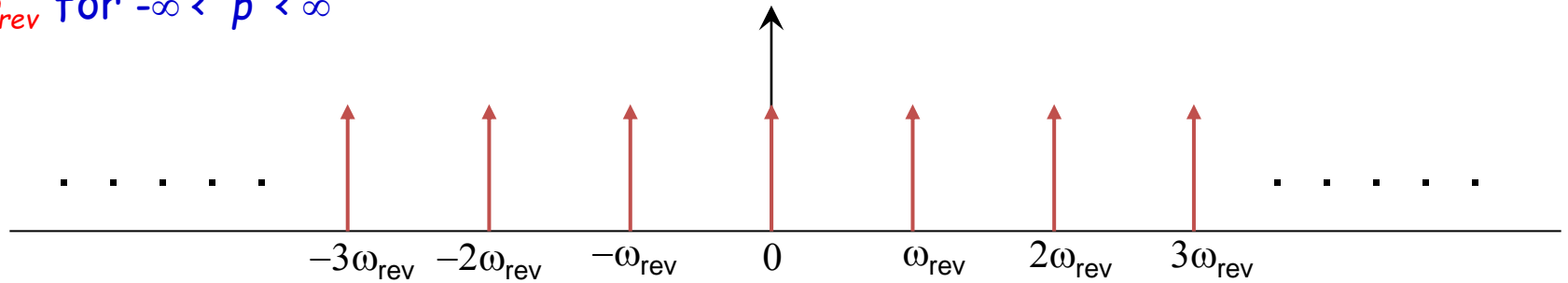
transverse. One single stable bunch

Pickup position

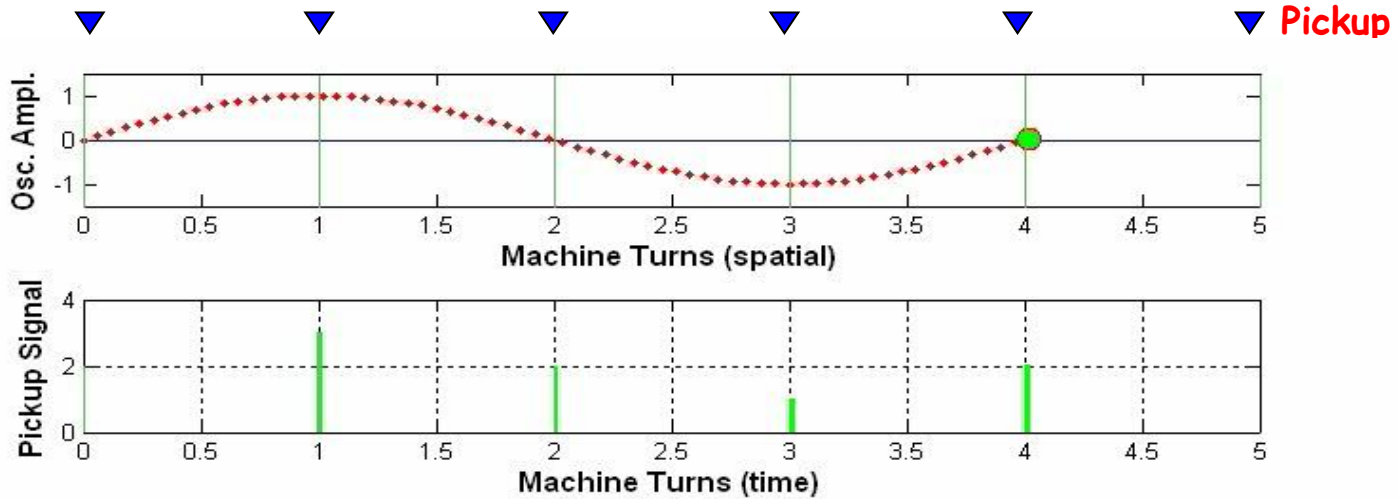


Every time the bunch passes through the pickup (\blacktriangledown) placed at coordinate 0, a pulse with constant amplitude is generated. If we think it as a Dirac impulse, the spectrum of the pickup signal is a repetition of frequency lines at multiple of the revolution frequency:

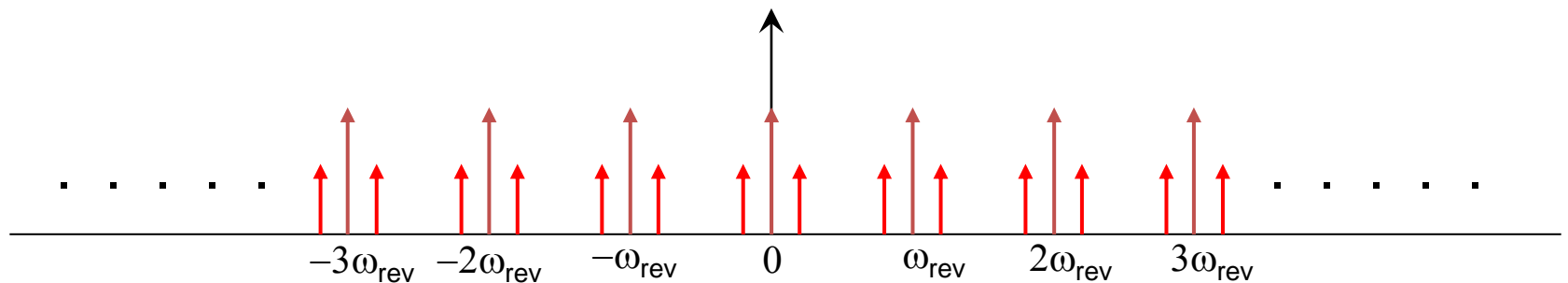
$p\omega_{rev}$ for $-\infty < p < \infty$



One single unstable bunch oscillating at the tune frequency $\nu\omega_0$: for simplicity we consider a vertical tune $\nu < 1$, ex. $\nu = 0.25$. $M = 1 \rightarrow$ only mode #0 exists

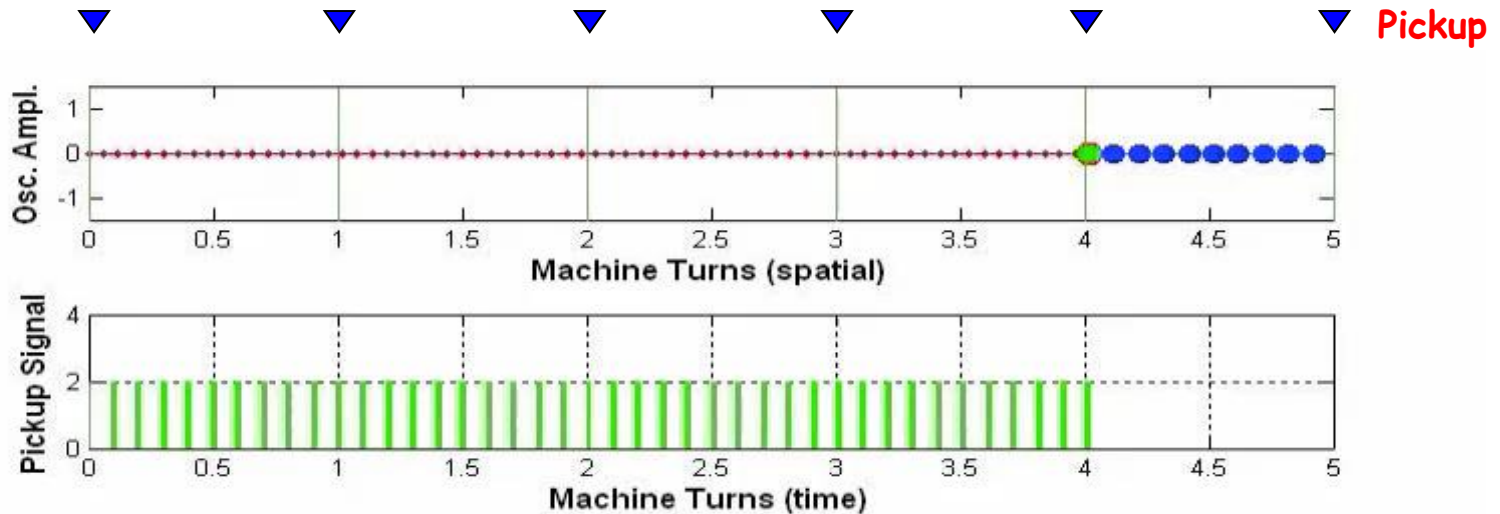


The pickup signal is a sequence of pulses modulated in amplitude with frequency $\nu\omega_0$
 Two sidebands at $\pm\nu\omega_0$ appear at each of the revolution harmonics

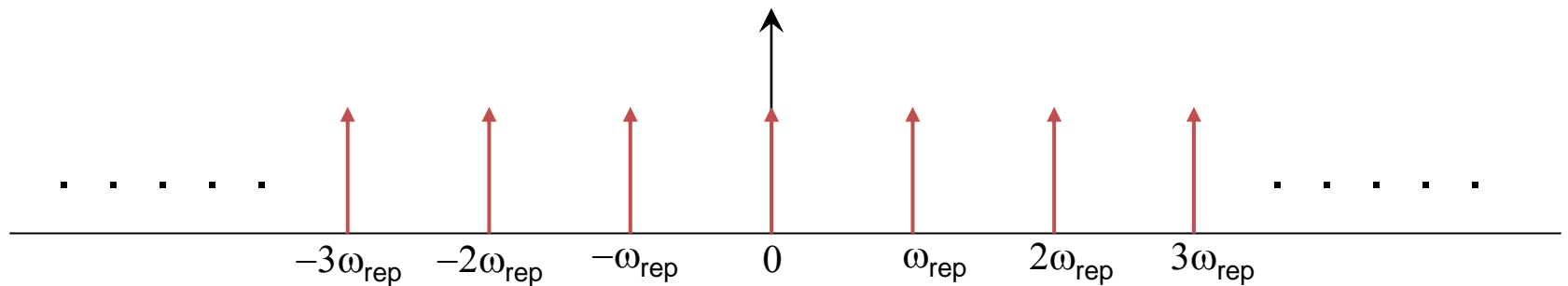


Multi-bunch modes: 10 stable bunches

Ten identical equally-spaced stable bunches ($M = 10$)



The spectrum is a repetition of frequency lines at multiples of the bunch repetition frequency:
 $\omega_{\text{rep}} = 10 \omega_{\text{rev}}$ (bunch repetition frequency)



Multi-bunch modes: 10 unstable bunches ($m=0$)

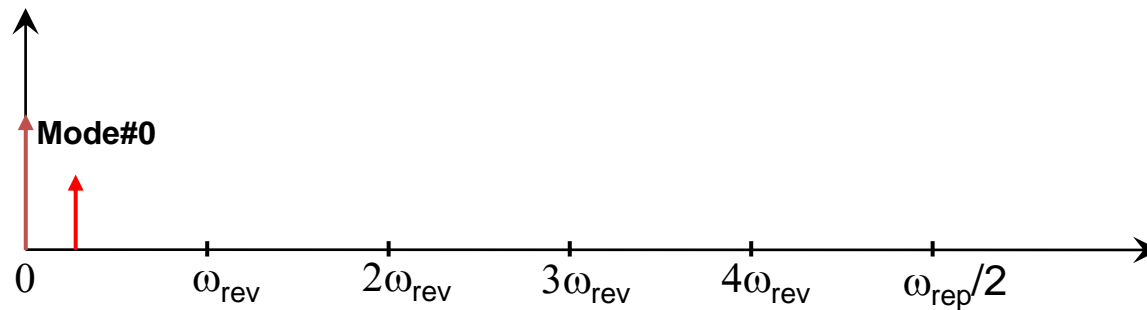
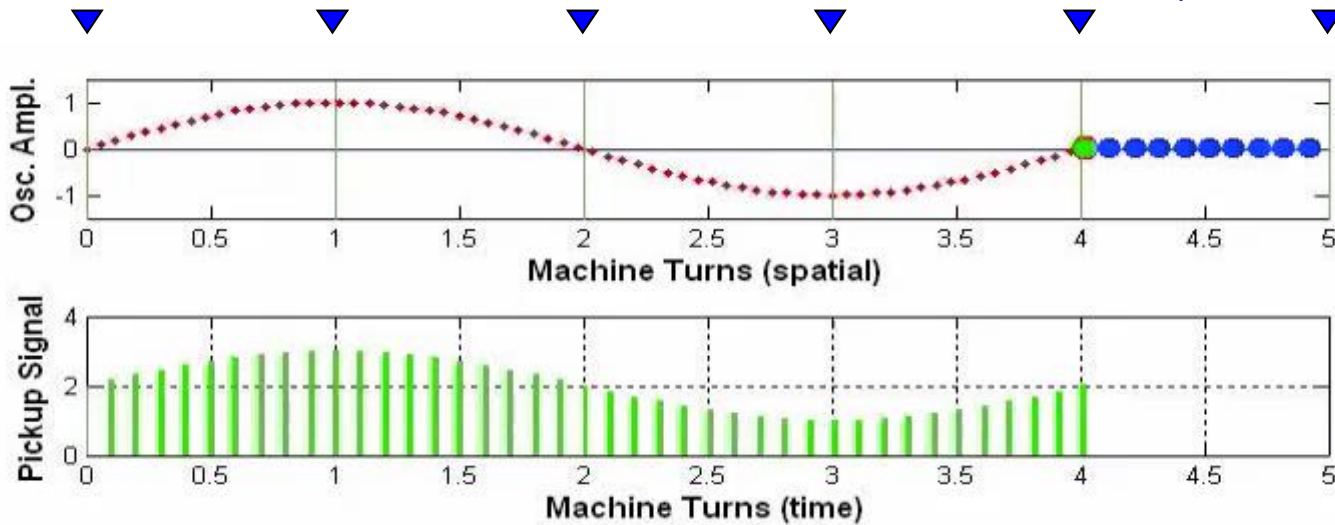
Ten identical equally-spaced unstable bunches oscillating at the tune frequency $\nu\omega_0$ ($\nu = 0.25$)

$M = 10 \rightarrow$ there are 10 possible modes of oscillation

$$\Delta\Phi = m \frac{2\pi}{M} \quad m = 0, 1, \dots, M-1$$

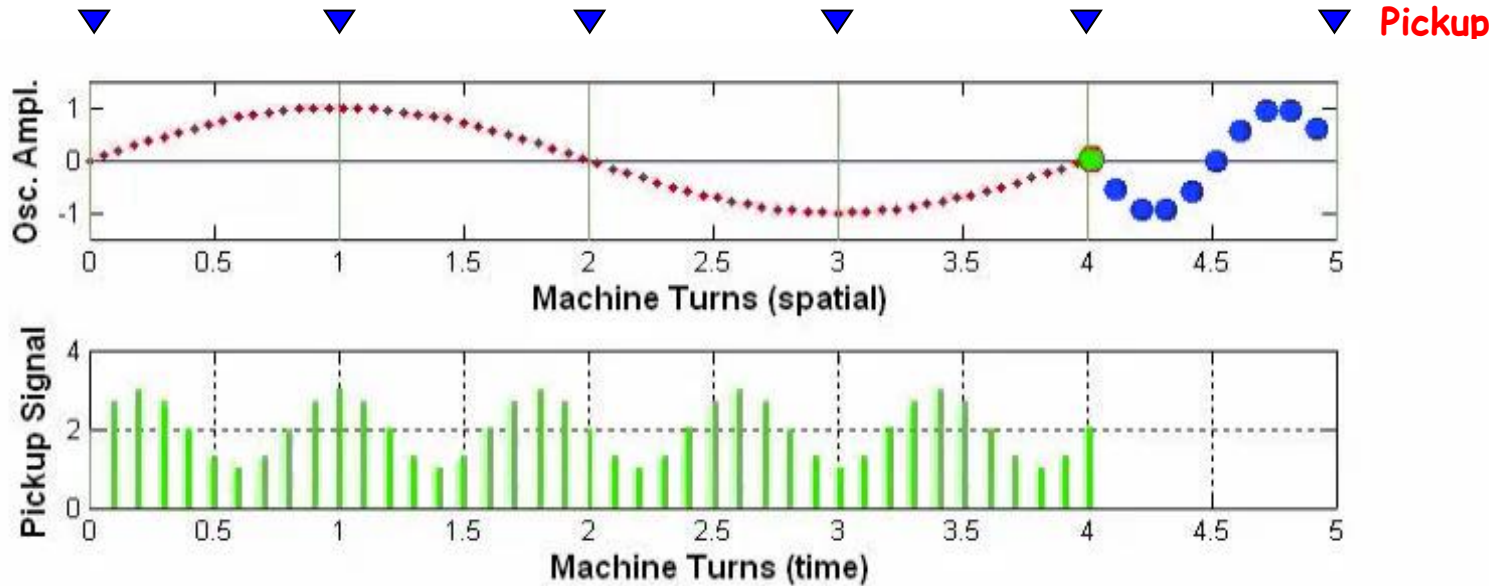
Ex.: mode #0 ($m = 0$) $\Delta\Phi=0$ all bunches oscillate with the same phase

Pickup

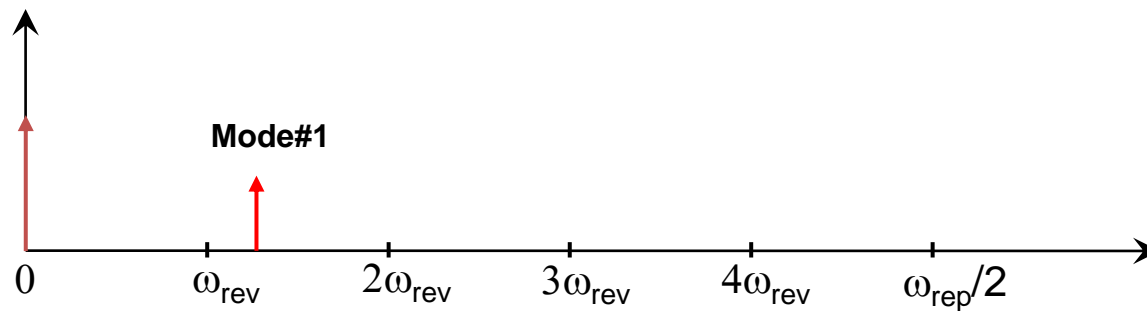


Multi-bunch modes: 10 unstable bunches ($m=1$)

Ex.: mode #1 ($m = 1$) $\Delta\Phi = 2\pi/10$ ($\nu = 0.25$)

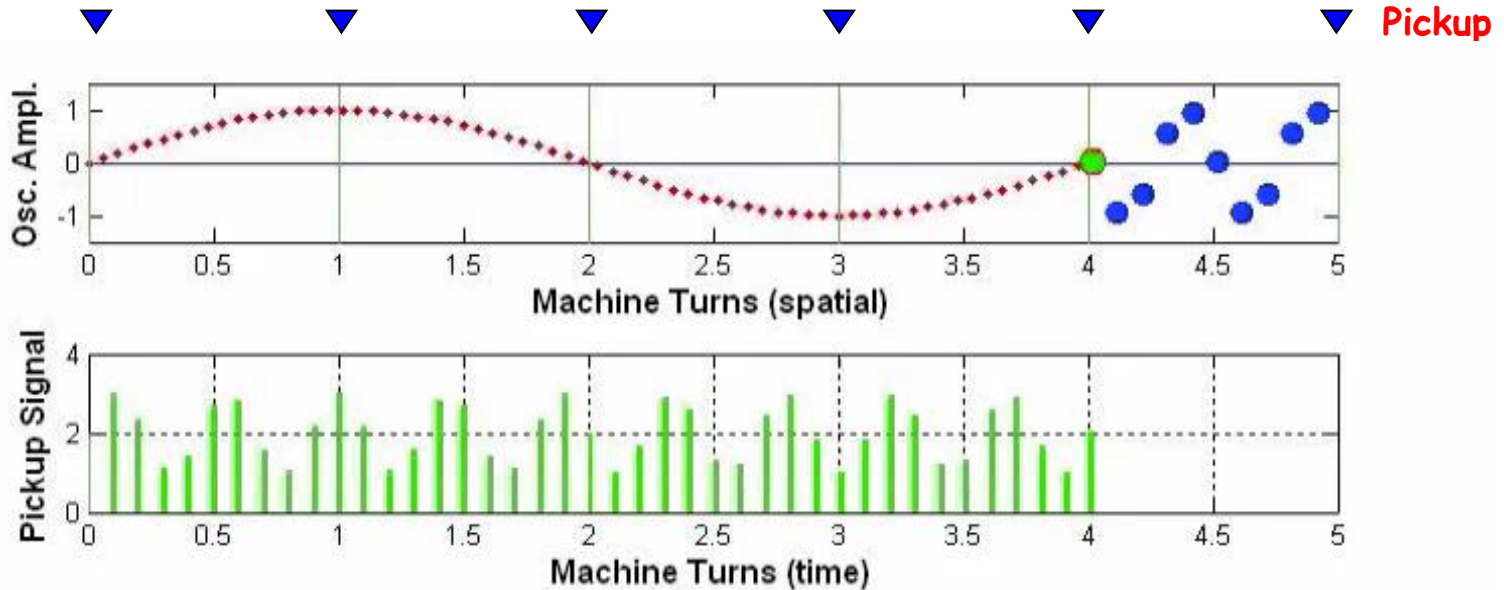


$$\omega = p\omega_{\text{rep}} \pm (\nu+1)\omega_{\text{rev}} \quad -\infty < p < \infty$$

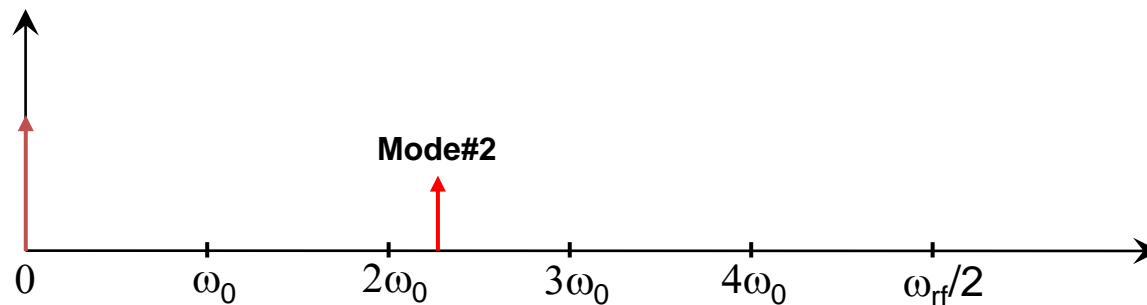


Multi-bunch modes: 10 unstable bunches ($m=2$)

Ex.: mode #2 ($m = 2$) $\Delta\Phi = 4\pi/10$ ($\nu = 0.25$)

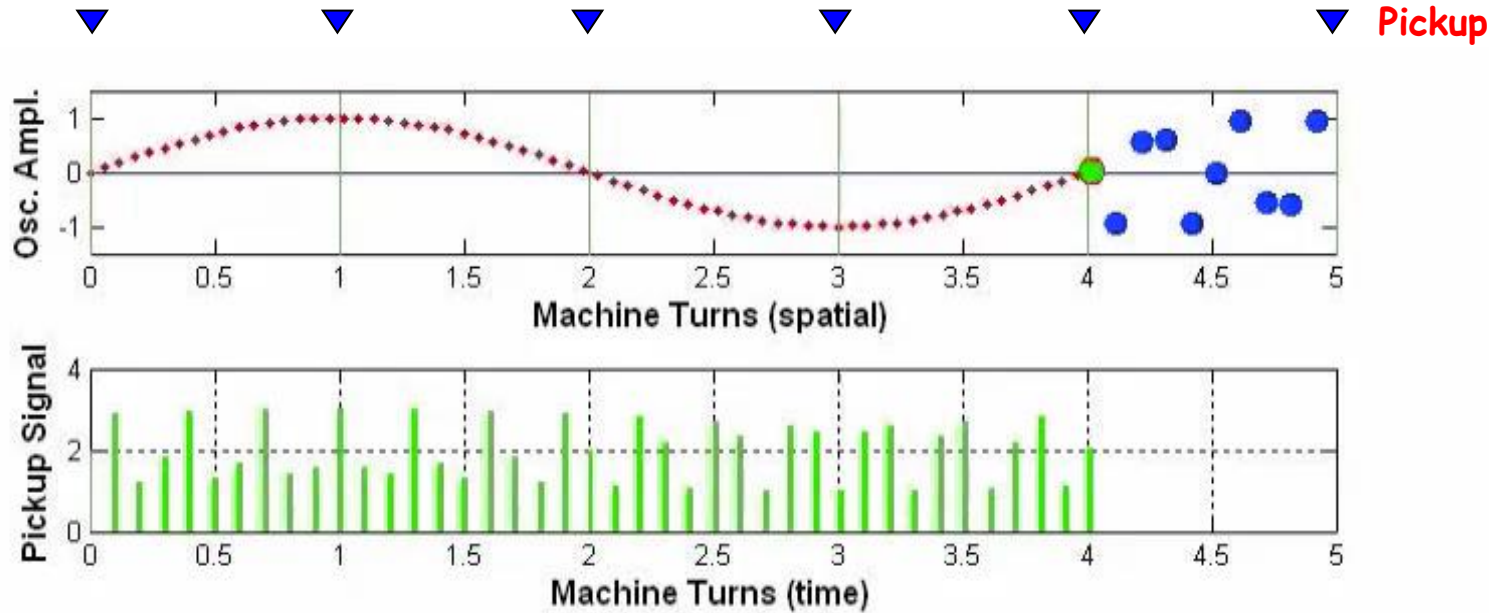


$$\omega = p\omega_{\text{rep}} \pm (\nu+2)\omega_{\text{rev}} \quad -\infty < p < \infty$$

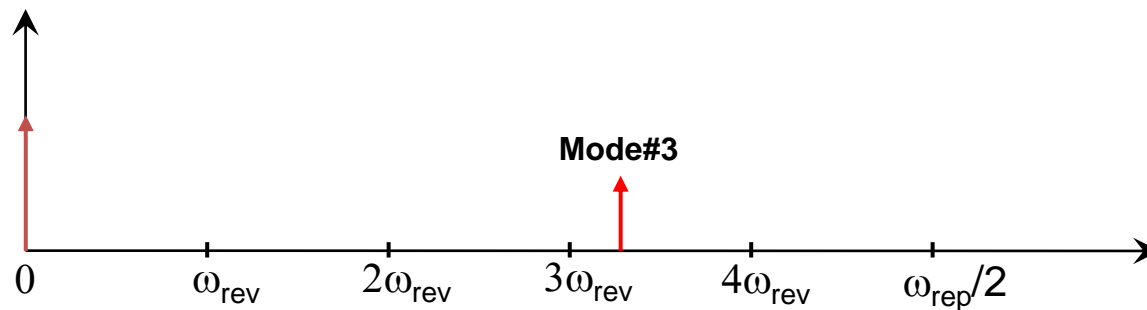


Multi-bunch modes: 10 unstable bunches ($m=3$)

Ex.: mode #3 ($m = 3$) $\Delta\Phi = 6\pi/10$ ($\nu = 0.25$)

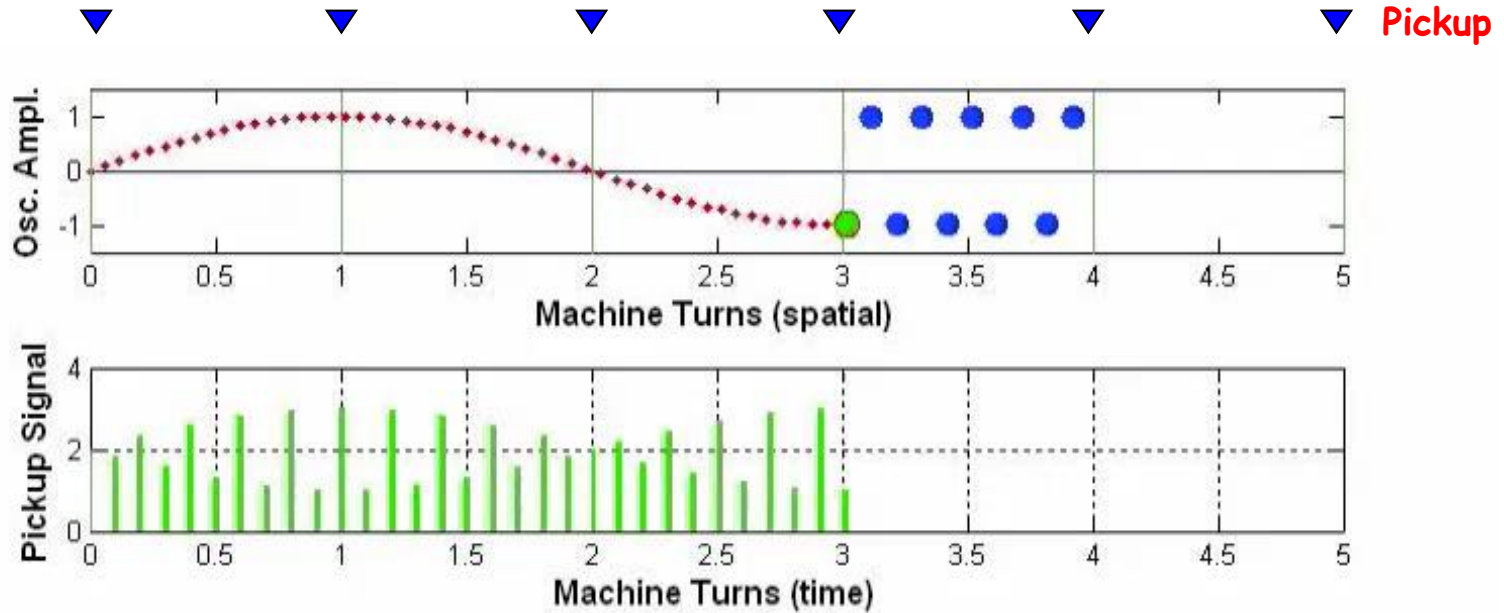


$$\omega = p\omega_{\text{rep}} \pm (\nu+3)\omega_{\text{rev}} \quad -\infty < p < \infty$$

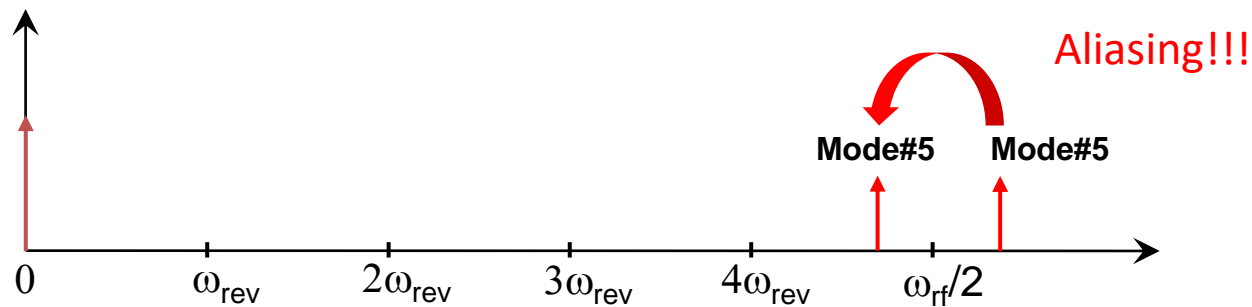


Multi-bunch modes: 10 unstable bunches ($m=5$)

Ex.: mode #5 ($m = 5$) $\Delta\Phi = \pi$ ($\nu = 0.25$)

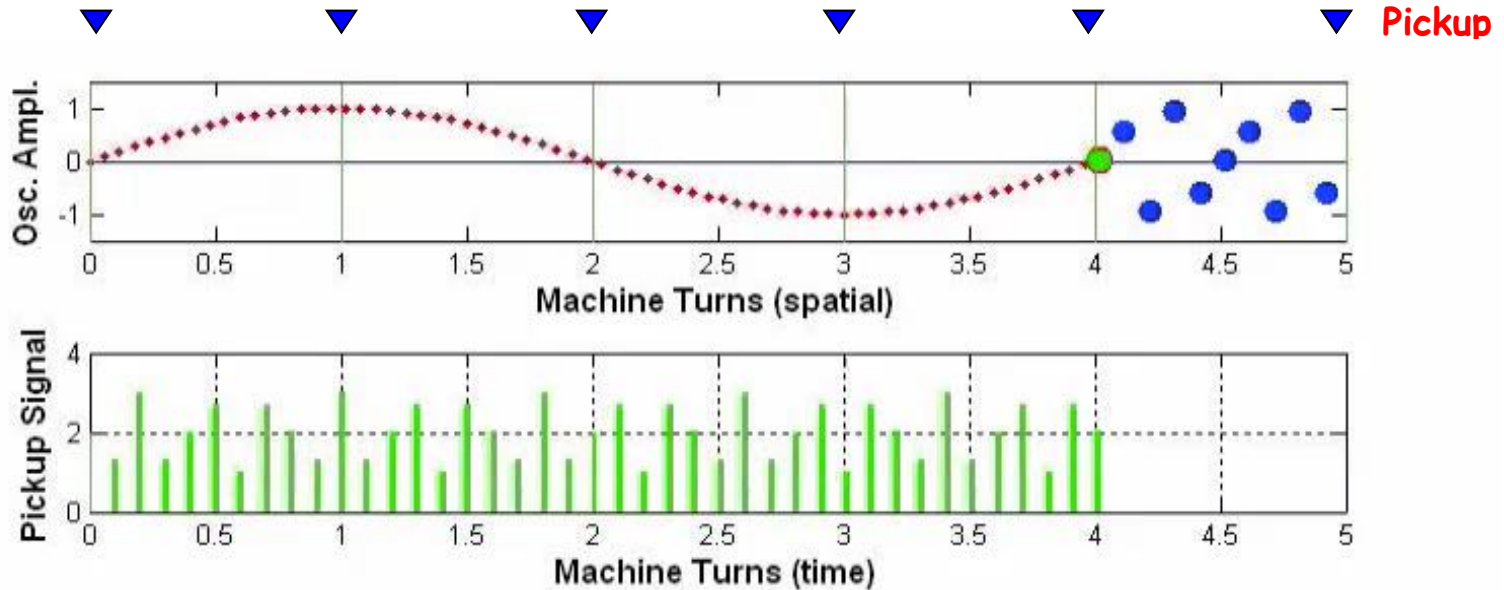


$$\omega = p\omega_{\text{rep}} \pm (\nu+5)\omega_{\text{rev}} \quad -\infty < p < \infty$$

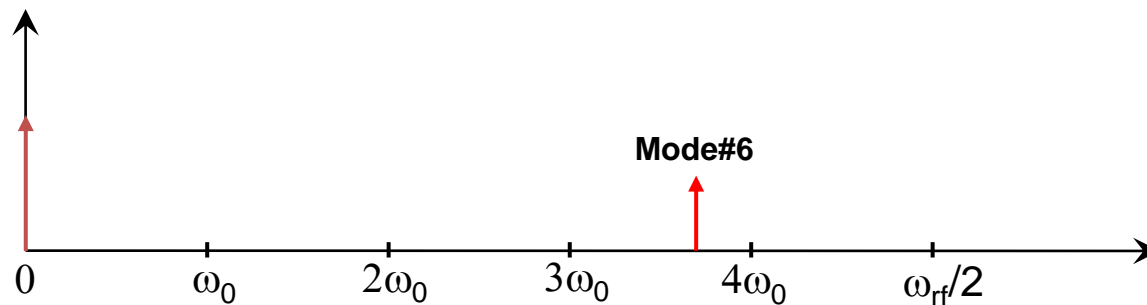


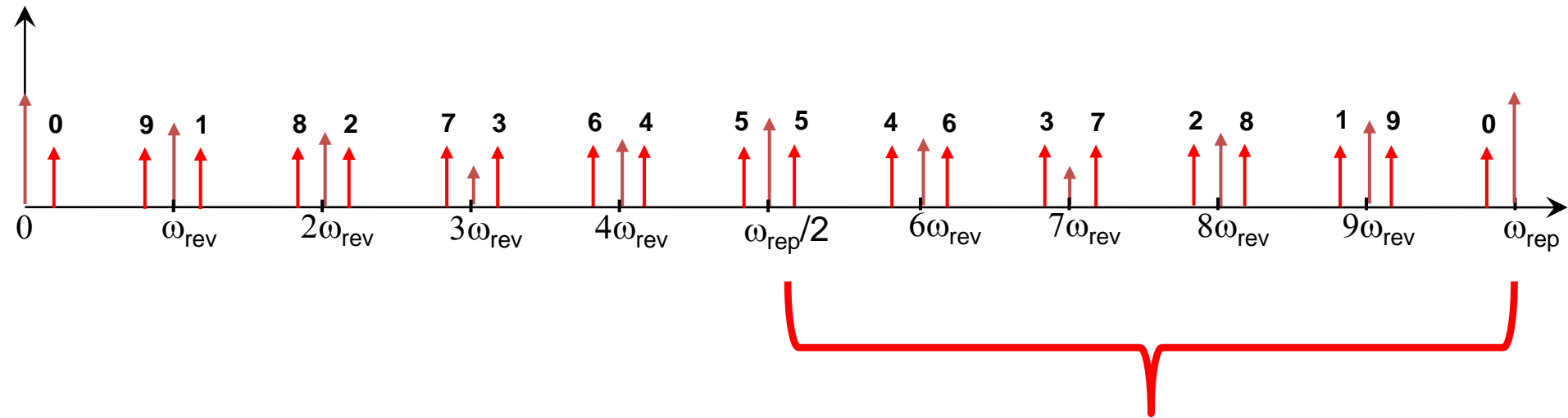
Multi-bunch modes: 10 unstable bunches ($m=6$)

Ex.: mode #6 ($m = 6$) $\Delta\Phi = 12\pi/10$ ($\nu = 0.25$)



$$\omega = p\omega_{rf} \pm (\nu+6)\omega_0 \quad -\infty < p < \infty$$





Lower sidebands of first revolution harmonics

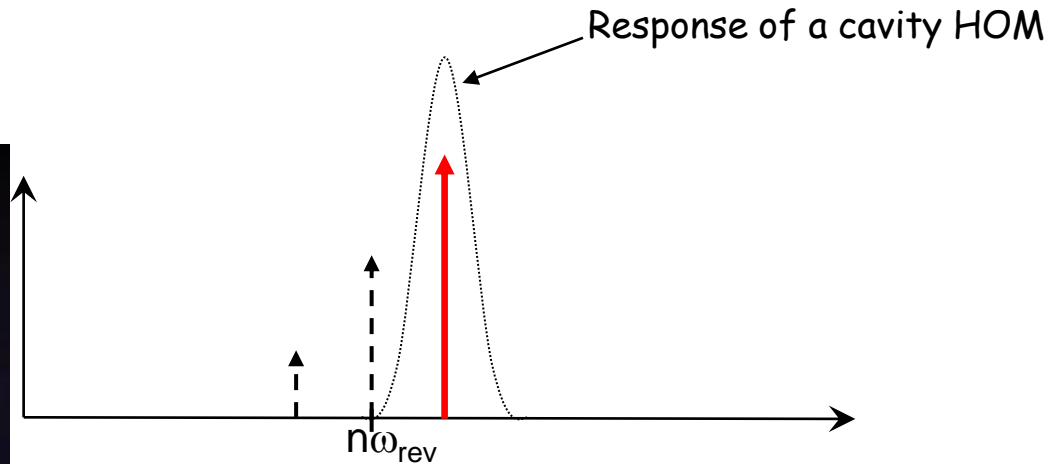
$$\omega = p M \omega_{rev} \pm (m + q) \omega_{rev}$$

If the bunches have **not the same charge**, i.e. the buckets are not equally filled (uneven filling), the spectrum has frequency **components also at the revolution harmonics** (multiples of ω_{rev}). The amplitude of each revolution harmonic depends on the filling pattern of one machine turn

One multi-bunch mode can become unstable if one of its sidebands overlaps, for example, with the frequency response of a cavity high order mode (HOM). The HOM couples with the sideband giving rise to a **coupled-bunch instability**, with consequent increase of the sideband amplitude



Synchrotron Radiation Monitor showing the transverse beam shape



Effects of coupled-bunch instabilities:

- ☹️ increase of the transverse beam dimensions
- ☹️ increase of the effective emittance
- ☹️ beam loss and max current limitation
- 😊 increase of lifetime due to decreased Touschek scattering (dilution of particles)

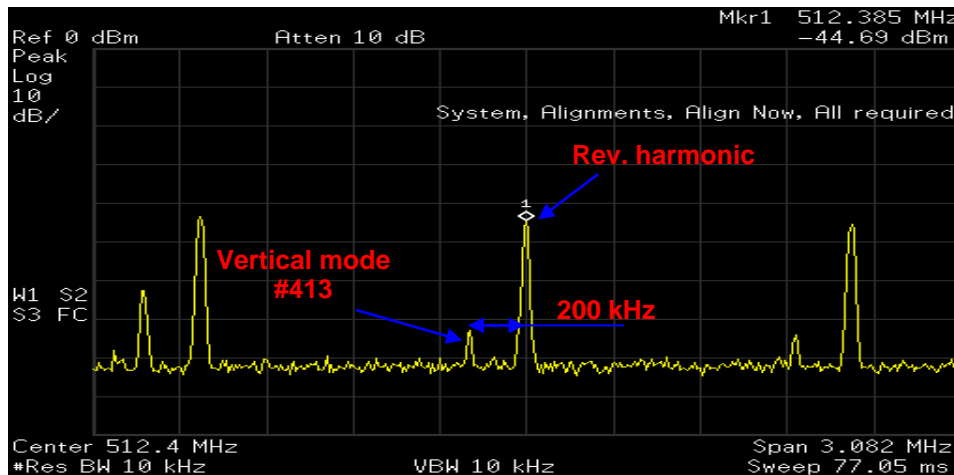
Real example of multi-bunch modes

ELETTRA Synchrotron: $f_{rf}=499.654$ MHz, bunch spacing ≈ 2 ns, 432 bunches, $f_0 = 1.15$ MHz

$v_{hor} = 12.30$ (fractional tune frequency = 345 kHz), $v_{vert} = 8.17$ (fractional tune frequency = 200 kHz)

$v_{long} = 0.0076$ (8.8 kHz)

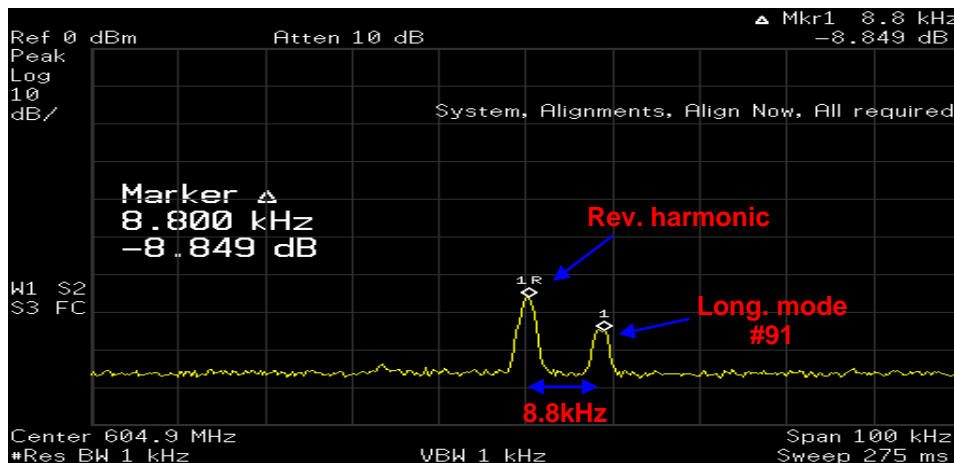
$$\omega = pM\omega_0 \pm (m+v)\omega_0$$



Spectral line at 512.185 MHz

Lower sideband of $2f_{rf}$, 200 kHz apart from the 443rd revolution harmonic

→ vertical mode #413



Spectral line at 604.914 MHz

Upper sideband of f_{rf} , 8.8 kHz apart from the 523rd revolution harmonic

→ longitudinal mode #91

Part II



- Fourier transform of time sampled signals
 - a) recap of basics
 - b) aliasing → limitation of usable bandwidth to 50% of sampling frequency
 - c) windowing

- Methods to improve the frequency resolution
 - a) interpolation
 - b) fitting (ex: NAFF algorithm)
 - c) influence of signal to noise ratio

- Analysis of non stationary signals/spectra:
 - STFT (:= Short time Fourier transform) (Gabor transform)
also called: Sliding FFT, Spectrogram
 - multi-BPM combined signal analysis
 - PLL tune tracking
 - **wavelet analysis** (if time permits, not really relevant for accelerators, but really cool stuff)

- Discrete Fourier Transform basics

In general:

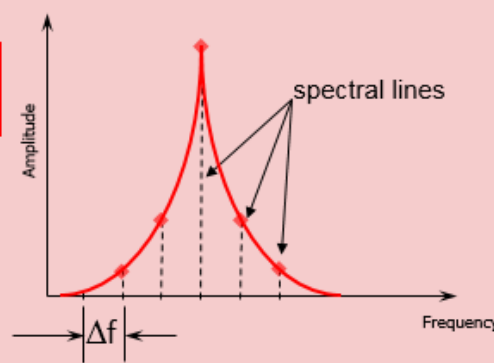
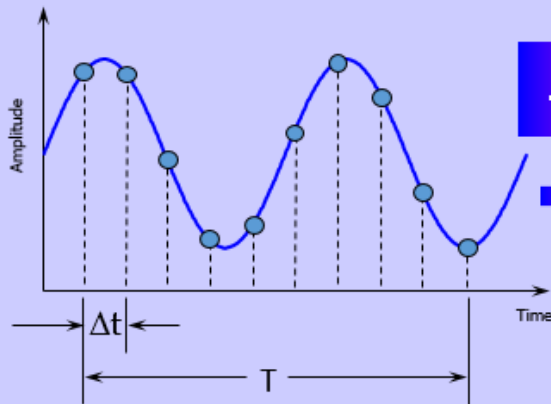
We use DFTs of **N equidistant time sampled signals**;

A FFT (Fast Fourier transform) is a DFT with $N = 2^k$

Time Duration		
Finite	Infinite	
Discrete FT (DFT) $X(k) = \sum_{n=0}^{N-1} x(n)e^{-j\omega_k n}$ $k = 0, 1, \dots, N-1$	Discrete Time FT (DTFT) $X(\omega) = \sum_{n=-\infty}^{+\infty} x(n)e^{-j\omega n}$ $\omega \in (-\pi, +\pi)$	discr. time n
Fourier Series (FS) $X(k) = \int_0^P x(t)e^{-j\omega_k t} dt$ $k = -\infty, \dots, +\infty$	Fourier Transform (FT) $X(\omega) = \int_{-\infty}^{+\infty} x(t)e^{-j\omega t} dt$ $\omega \in (-\infty, +\infty)$	cont. time t
discrete freq. k	continuous freq. ω	

TIME DOMAIN

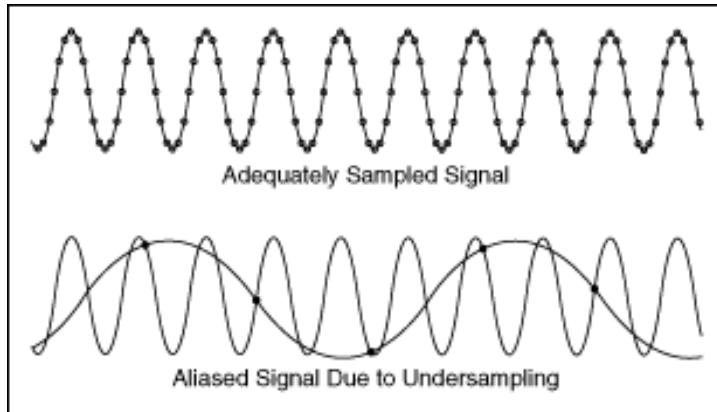
FREQUENCY DOMAIN



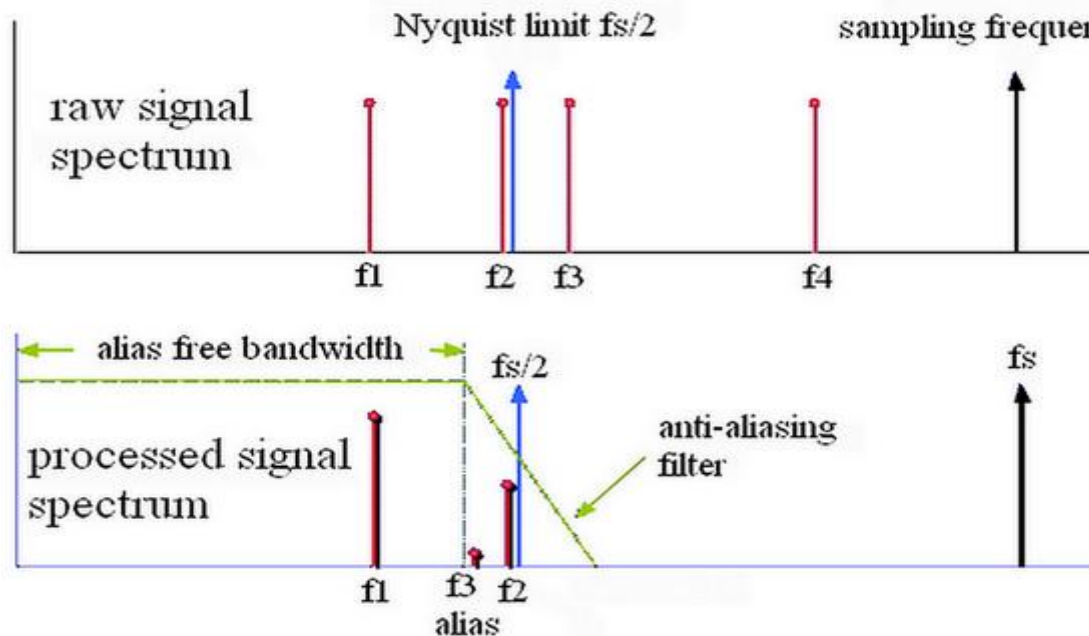
Sampling rate (samples/sec)	$F_s = 1/\Delta t$
Frame Size (seconds)	$T = N \Delta t$
Block Size (# samples)	N

Bandwidth or Max Freq (Hz)	$F_{\max} = F_s/2$
Frequency Resolution (Hz)	$\Delta f = F_{\max} / SL$
Spectral Lines (# samples)	$SL = N/2$

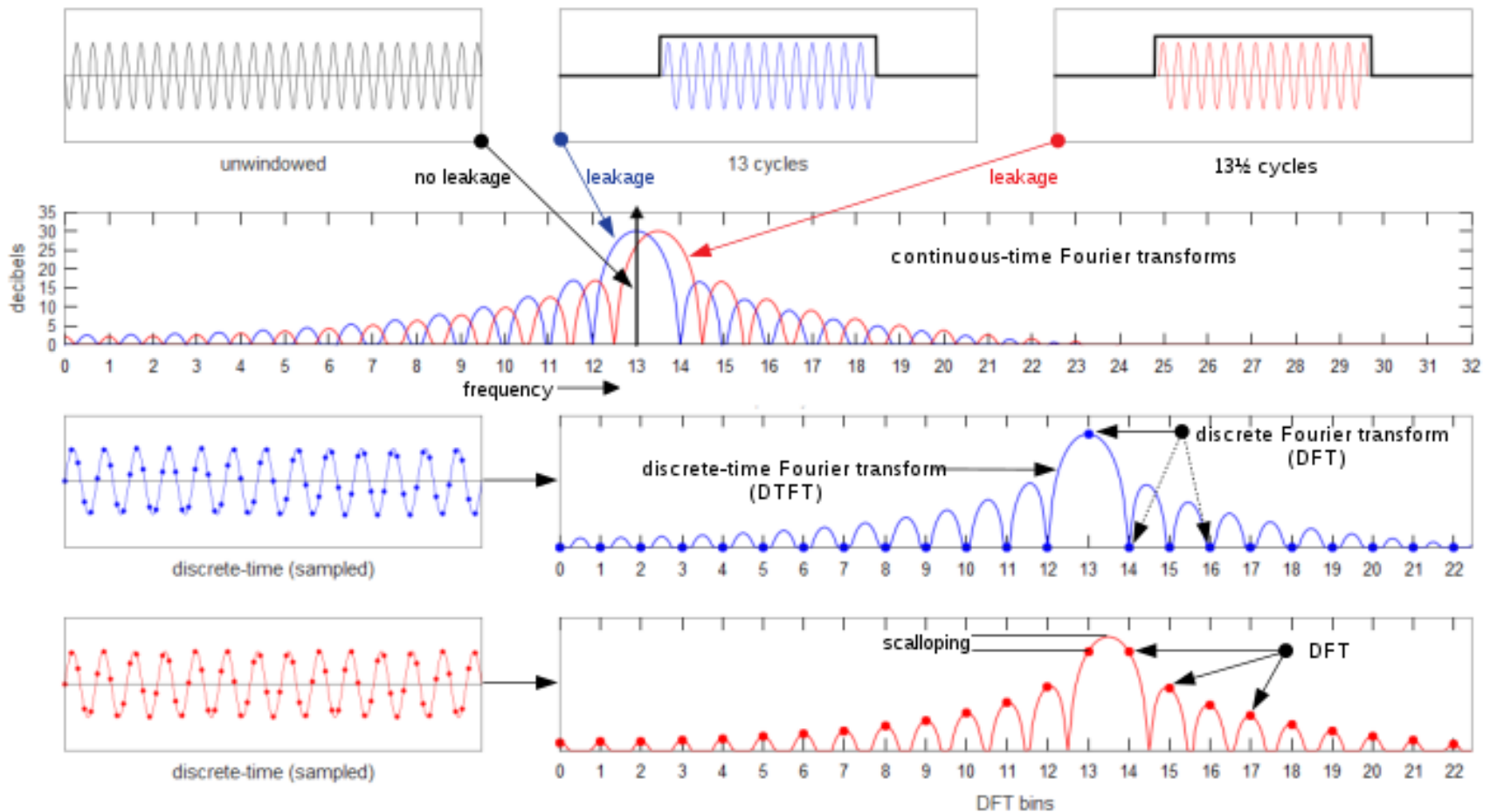
Aliasing



- Periodic signals, which are sampled with at least 2 samples per period, can be unambiguously reconstructed from the frequency spectrum. (Nyquist-Shannon Theorem)
- In other words, with a DFT one only obtains useful information up to half the sampling frequency.
- **Antialiasing filters** need to be inserted upstream of the sampling in order to suppress unwanted higher spectral information.



Spectral leakage caused by windowing

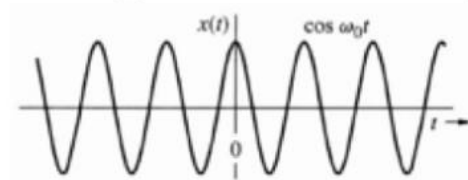


By measuring a continuous signal only over a **finite length**, we apply a “**data window**” to signal, which leads to spectral artefacts in frequency domain.

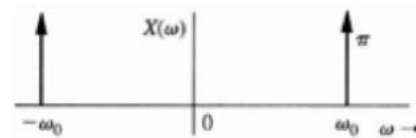
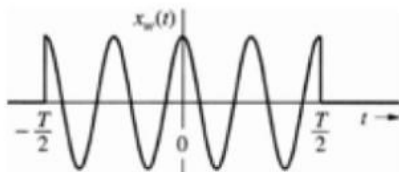
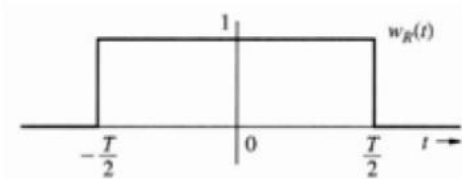
Windowing = Convolution of continuous signal with window function

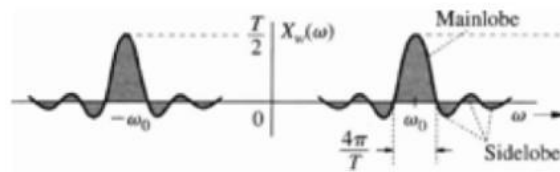
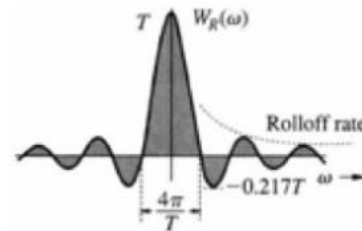
- Recall: The Fourier transform of a product in time domain is the convolution of the individual Fourier transforms in Frequency domain

◆ Extracting a segment of a signal in time is the same as multiplying the signal with a rectangular window:



X





Spectral spreading

Energy spread out from ω_0 to width of $2\pi/T$ – reduced spectral resolution.

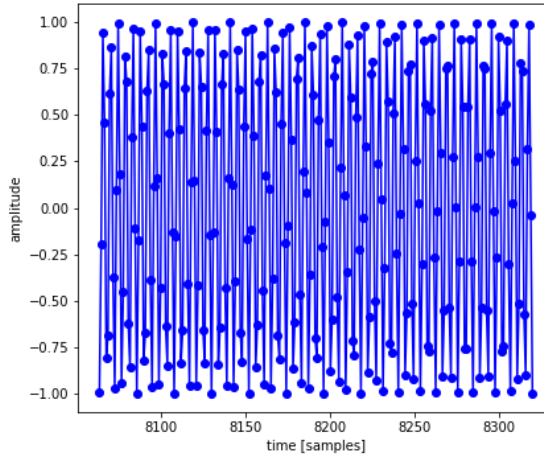
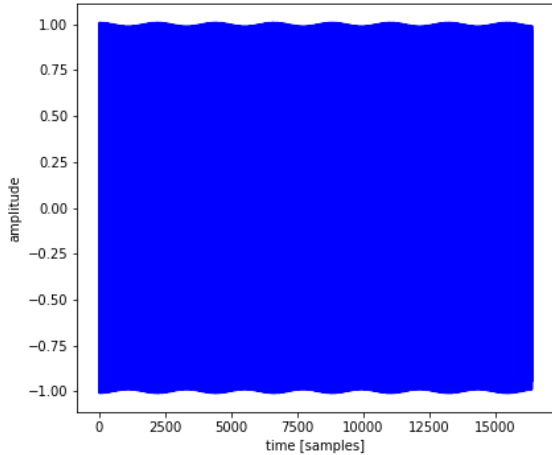
Leakage

Energy leaks out from the mainlobe to the sidelobes.

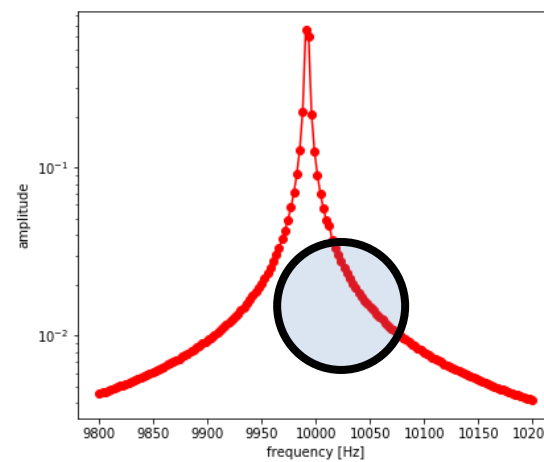
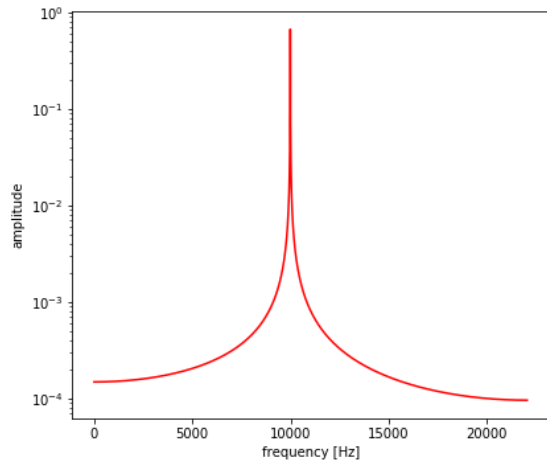
$$\text{signal} = \text{amp1} * \sin(2\pi \omega_1 t) + \text{amp2} * \sin(2\pi \omega_2 t)$$

$$\begin{aligned} \text{amp1} &= 1 \\ \text{amp2} &= 0.01 \end{aligned}$$

$$\begin{aligned} \omega_1 &= 2\pi * 9990 \text{ Hz} \\ \omega_2 &= 2\pi * 10010 \text{ Hz} \end{aligned}$$



FFT



The small signal component is completely masked by the sidelobe of the large signal



ZOOM

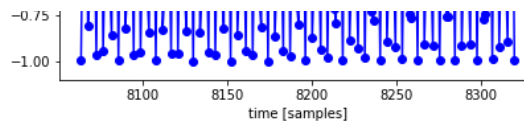
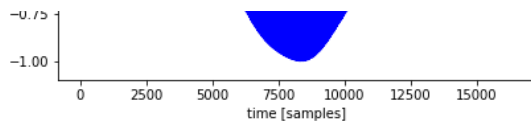
$$\text{signal} = \text{window} * \text{amp1} * \sin(2\pi \omega_1 t) + \text{amp2} * \sin(2\pi \omega_2 t)$$

Blackman-Harris window

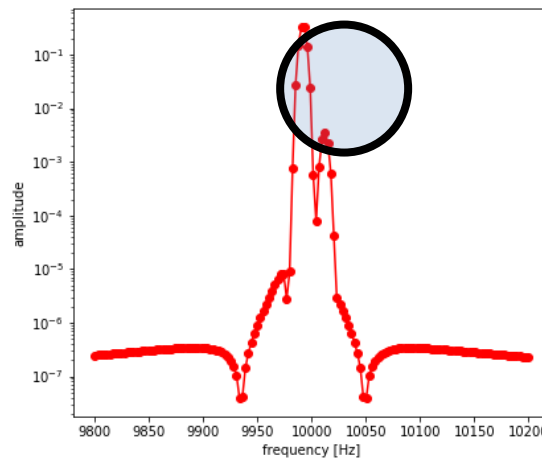
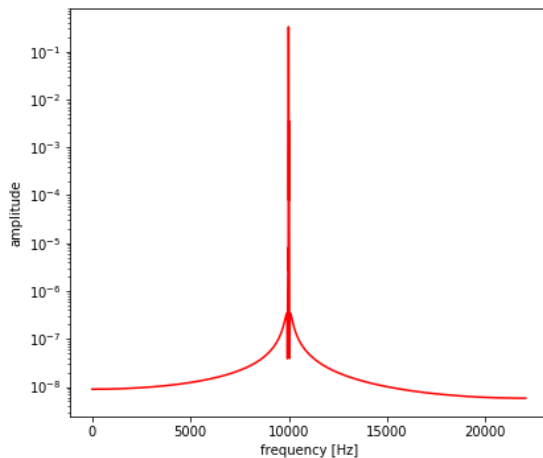
A generalization of the Hamming family, produced by adding more shifted sinc functions, meant to minimize side-lobe levels

$$w[n] = a_0 - a_1 \cos\left(\frac{2\pi n}{N}\right) + a_2 \cos\left(\frac{4\pi n}{N}\right) - a_3 \cos\left(\frac{6\pi n}{N}\right)$$

$$a_0 = 0.35875; \quad a_1 = 0.48829; \quad a_2 = 0.14128; \quad a_3 = 0.01168.$$

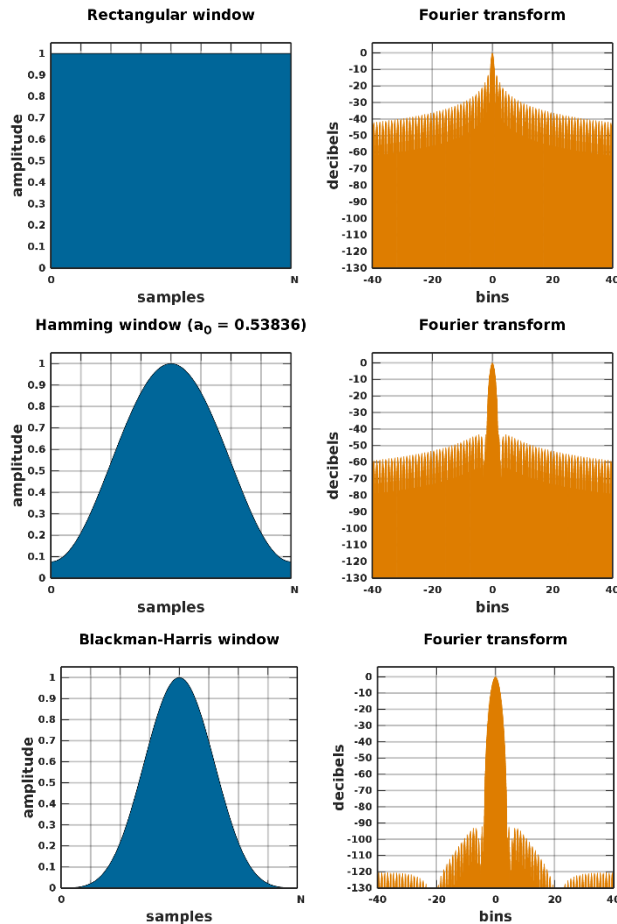


FFT



The small signal component is nicely resolved

- The following link contains many frequently used window functions, their main features and application:
- https://en.wikipedia.org/wiki/Window_function



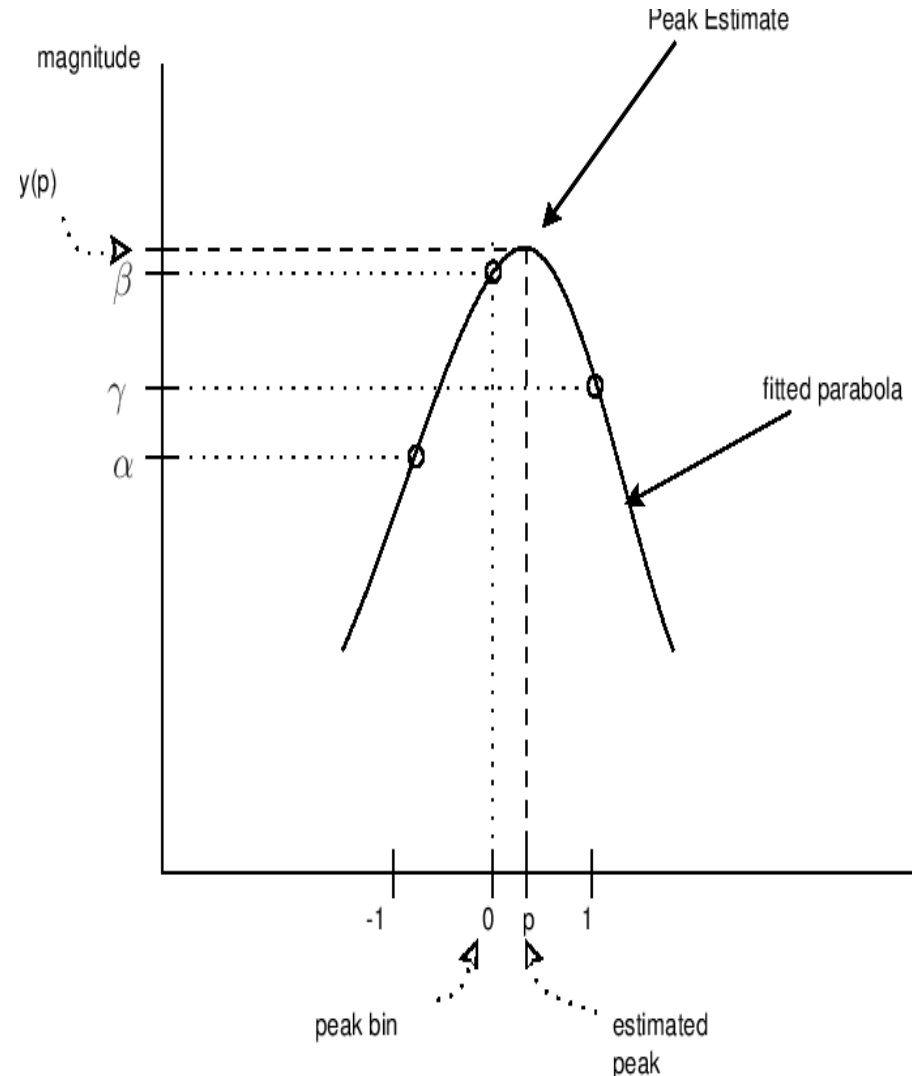
The actual choice of the window depends on:

- The signal composition
- The required dynamic range
- The signal to noise ration

remark: every window except the rectangular window is linked to a loss in amplitude (we multiply many samples with almost “zero”)
 → reduced S/N up to 6 dB

Improving the frequency resolution of a DFT spectrum

- Recall: basic frequency resolution:
 $\Delta f = 2 \cdot f_{\text{samp}} / N_{\text{samp}}$
- We can interpolate between the frequency bin with maximum content and the left and right neighbouring bins
- We limit the discussion to “three point interpolation methods”
- The interpolation function is either:
 - a parabola of the measurements
 (:= parabolic interpolation)
 - a parabola of the log of the measurements
 (:= Gaussian interpolation)
- Can get up to $1/N^2$ resolution



Details: https://mgasior.web.cern.ch/mgasior/pap/FFT_resol_note.pdf



Improving the frequency resolution of a DFT spectrum

Table 1. Efficiency of the parabolic and Gaussian interpolation with different windowing methods. The windows are characterised by main lobe width, highest sidelobe level and sidelobe asymptotic fall-off. The maximum interpolation error is given as a percentage of the spectrum bin spacing Δ_f . The interpolation gain factor G is defined in (19). Some details concerning the windows and the interpolation errors are given in the Appendix.

Window	Main lobe width [bin]	Highest sidelobe [dB]	Sidelobe asymptotic fall-off [dB/oct]	Parabolic interpolation		Gaussian interpolation	
				Error max. [% of Δ_f]	Gain factor G	Error max. [% of Δ_f]	Gain factor G
Rectangular	2	-13.3	6	23.4	2.14	16.7	2.99
Triangular	4	-26.5	12	6.92	7.23	2.08	24.1
Hann	4	-31.5	18	5.28	9.47	1.60	31.2
Hamming	4	-44.0	6	6.80	7.35	1.60	31.2
Blackman	6	-68.2	6	4.66	10.7	0.578	86.5
Blackman-Harris	6.54	-74.4	6	4.18	12.0	0.476	105
Nuttall	8	-98.2	6	3.51	14.2	0.314	159
Blackman-Harris-Nuttall	8	-93.3	18	3.34	15.0	0.314	159
Gaussian $L = 6 \sigma$	6.96	-57.2	6	4.95	10.1	0.240	208
Gaussian $L = 7 \sigma$	10.46	-71.0	6	3.80	13.2	0.0516	970
Gaussian $L = 8 \sigma$	11.41	-87.6	6	2.95	17.0	0.00869	5756

$$\text{Gain factor } G := \frac{\Delta_f}{2 \times \text{Error max.}}$$

from: https://mgasior.web.cern.ch/mgasior/pap/FFT_resol_note.pdf

1. Assume a model function for the data (sample $_{1...N}$) (i.e. in the most simple case a monochromatic sin wave), in general $\text{sample}_i = f(i * \Delta t)$
2. Get frequency and peak (or interpolated peak) from FFT:
 f_{\max} and a_{\max}

3. Minimize:

$$\Sigma = \sum_{i=0}^N (\text{sample}_i)^2 - (a_{\max} * \sin(2\pi f_{\max} * \Delta t))^2$$

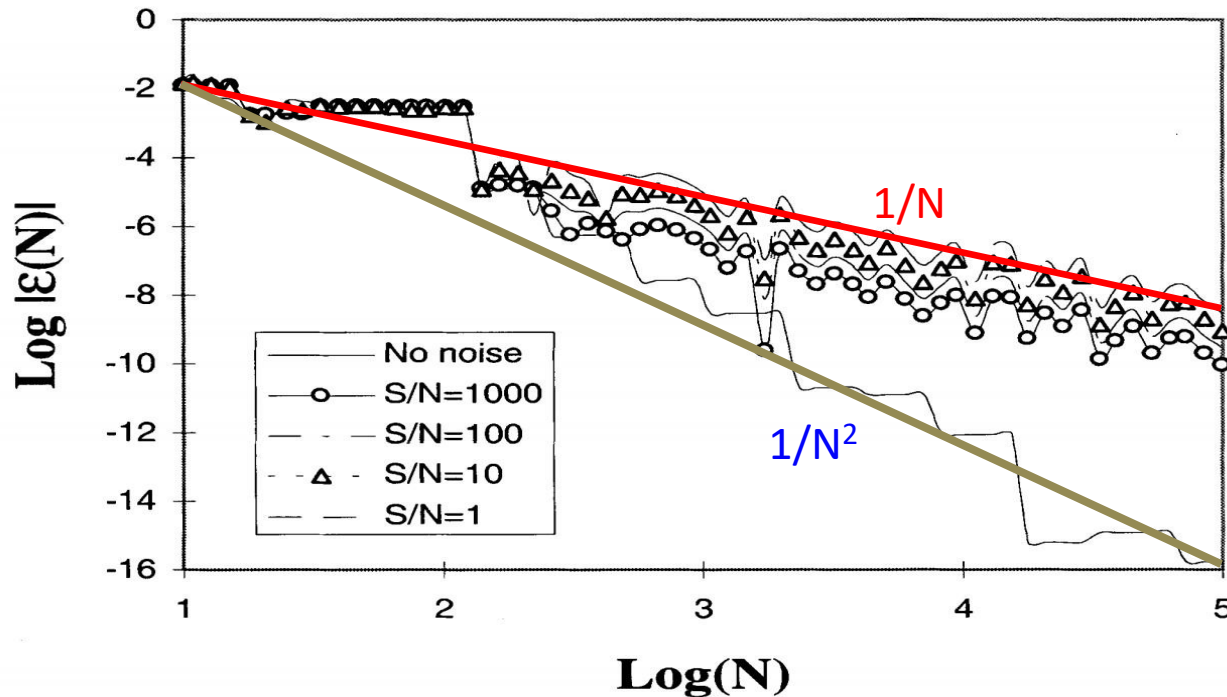
by varying a_{\max} and f_{\max}

(\rightarrow **NAFF algorithm** := Numerical Analysis of Fundamental Frequencies

\rightarrow NAFF algorithm can get up to $1/N^4$ resolution)

4. Very good convergence for **noise free data** (i.e. predominantly in simulations)

A little summary on frequency resolution



Taken from: R. Bartolini et al, Precise Measurement of the Betatron tune, Proceedings of PAC 1995, Vol. 55, pp 247-256

- Frequency measurement error $\epsilon(N)$ as function of $\log(N)$ for different S/N ratios
- Basic FFT resolution proportional to $1/N$
- Plot shows result for interpolation using Hanning window.
- With interpolation and no noise proportional to $1/N^2$
- **Data fitting (NAFF algorithm) also very sensitive to S/N**

1. Introduction and outline

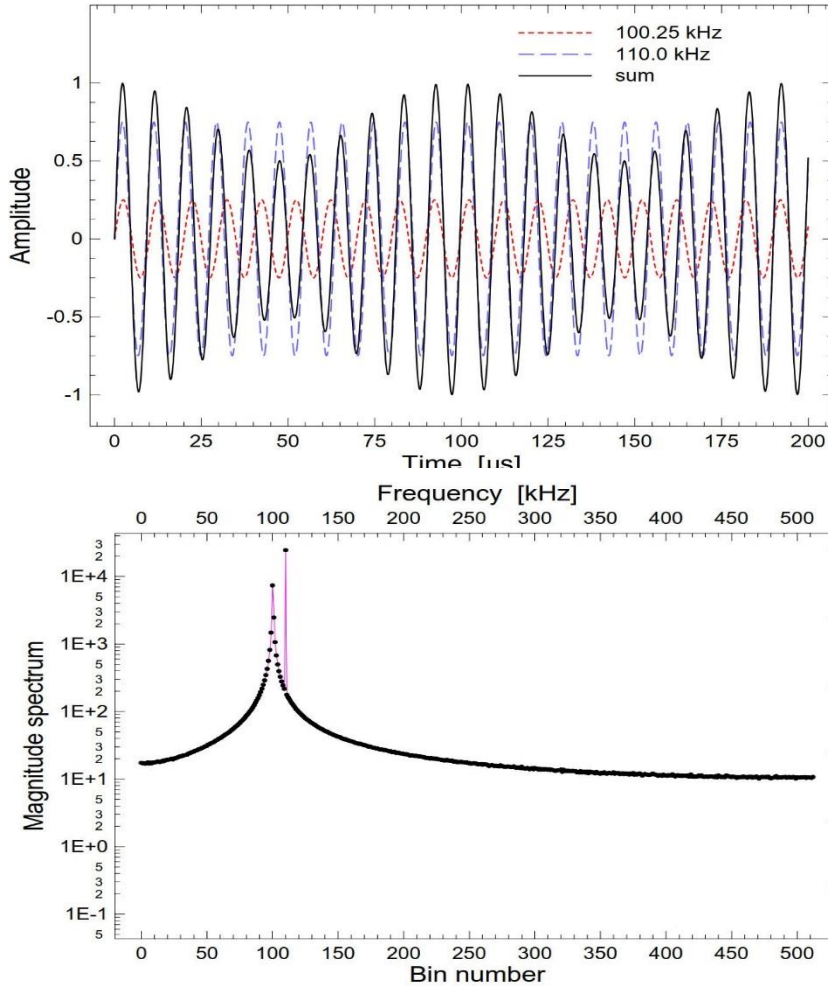


Fig. 1-1. Signal $s(t)$ (black solid line) of unitary amplitude contains two sinusoidal components: the component of interest, $s_{in}(t)$ (red dashed line), whose frequency is to be measured, and an undesirable component, $s_{bg}(t)$ (blue dashed line), considered as a simplified background. Component frequencies are $f_{in}=100.25$ kHz and $f_{bg}=110.0$ kHz, their amplitudes $A_{in}=0.25$ and $A_{bg}=0.75$.

All pictures: M.Gasior

Fig. 1-3. The magnitude spectrum of $N=1024$ samples of the example signal shown in Fig. 1-2. The smaller spectral peak corresponds to the input component and the bigger to the background one. The input component peak is biased by the spectral leakage effect, while the background peak is narrow and biased only by the spectral leakage of the input component. The right vertical axis is scaled in dB with respect to the highest peak.

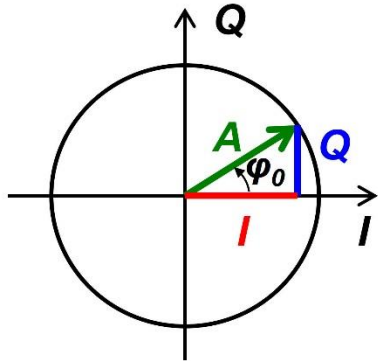
The FFT of the so called background signal has no spectral leakage!!!!

1. In the shown example the following relation holds:

$$\frac{f_{background}}{f_{sampling}} = \frac{110}{1024} = \frac{M}{N} \text{ (ratio of rational numbers)}$$

2. This means that with the 1024 samples **exactly** 110 full periods of the background signals have been measured.
3. The mathematical equivalent is that we have not applied a window function (no truncation), we get as result of the FFT the pure sine wave corresponding to the background frequency.
4. In accelerators we often know the frequency of a signal for which we want to measure the amplitude (=multiple of RF frequency) → we can avoid spectral leakage.
5. Important application of 4: IQ-sampling at 4*f (next slide)

I-Q Sampling



- **Vector representation of sinusoidal signals:**
 - **Phasor rotating counter-clockwise (pos. freq.)**

$$y(t) = A \sin(\omega t + \varphi_0)$$

$$y(t) = \underbrace{A \cos \varphi_0}_{=: I} \sin \omega t + \underbrace{A \sin \varphi_0}_{=: Q} \cos \omega t$$

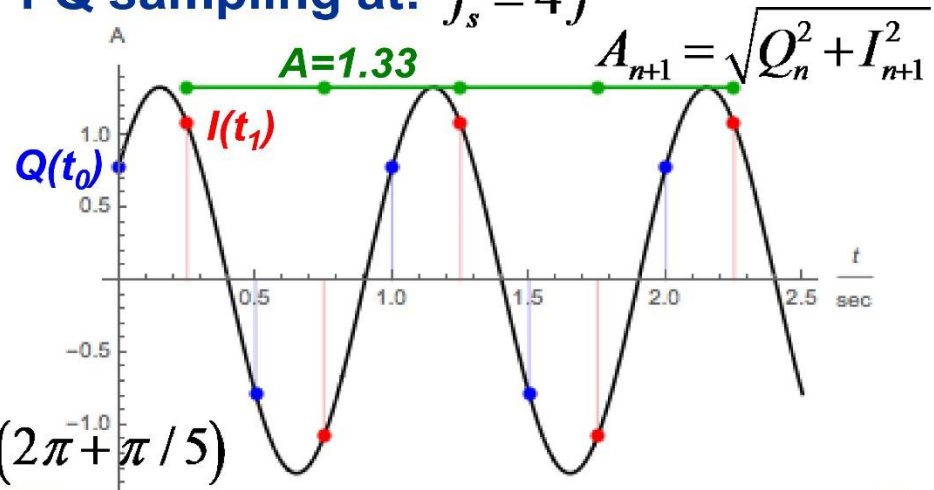
I: in-phase component **Q: quadrature-phase component**

$$y(t) = I \sin \omega t + Q \cos \omega t$$

$$I = A \cos \varphi_0 \quad A = \sqrt{I^2 + Q^2}$$

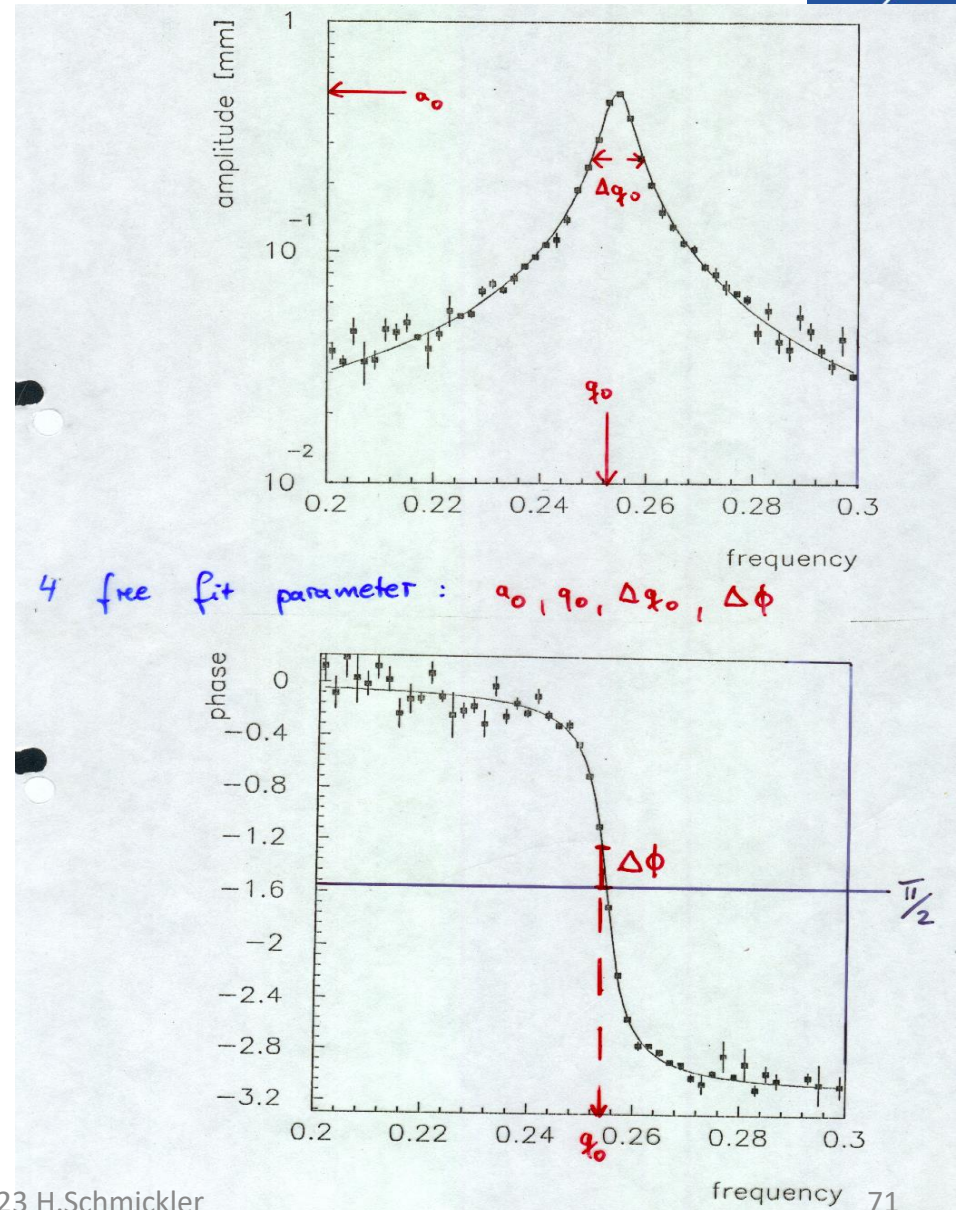
$$Q = A \sin \varphi_0 \quad \varphi_0 = \arctan\left(\frac{Q}{I}\right)$$

- **I-Q sampling at: $f_s = 4f$**



$$y(t) = 1.33 \sin(2\pi + \pi/5)$$

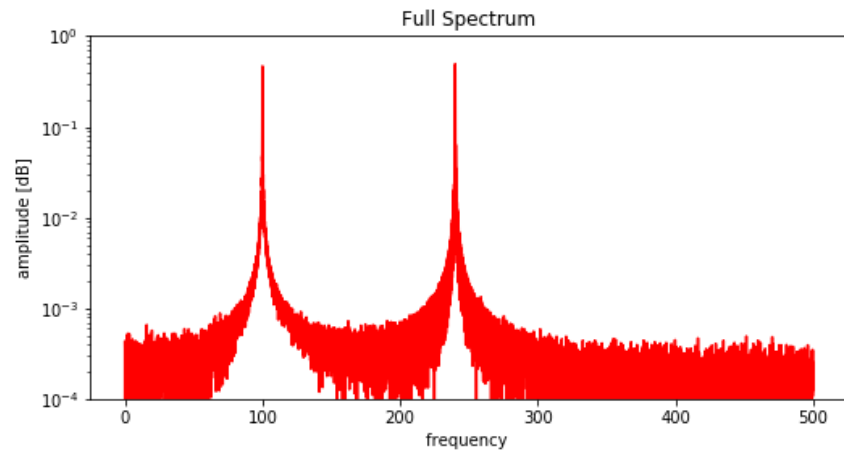
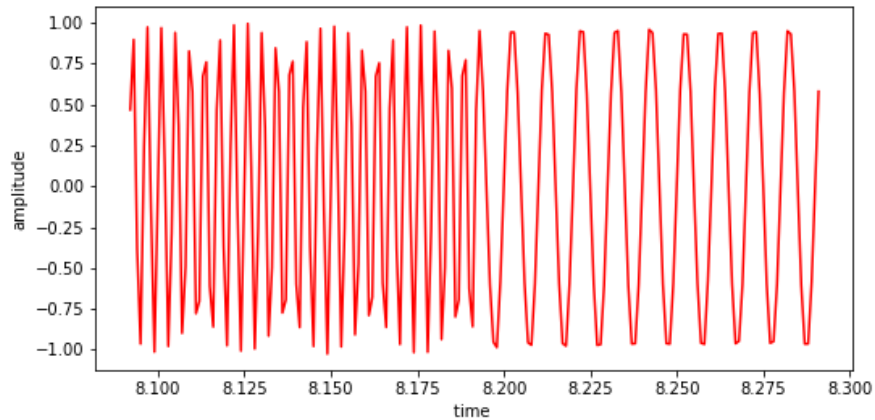
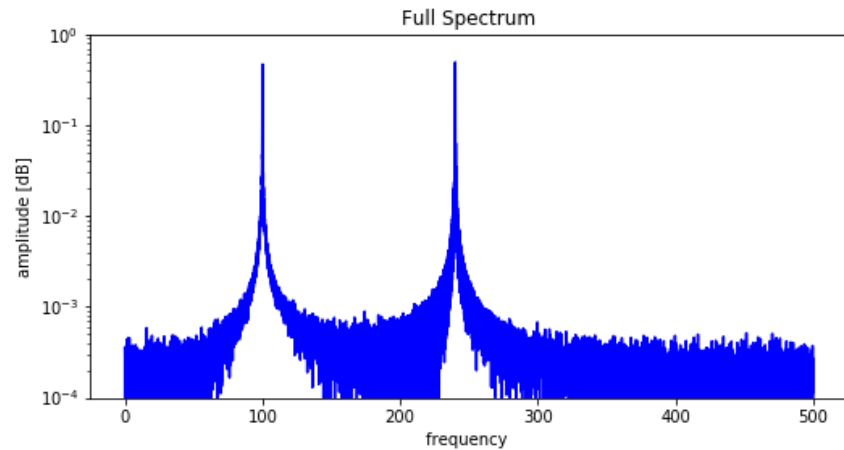
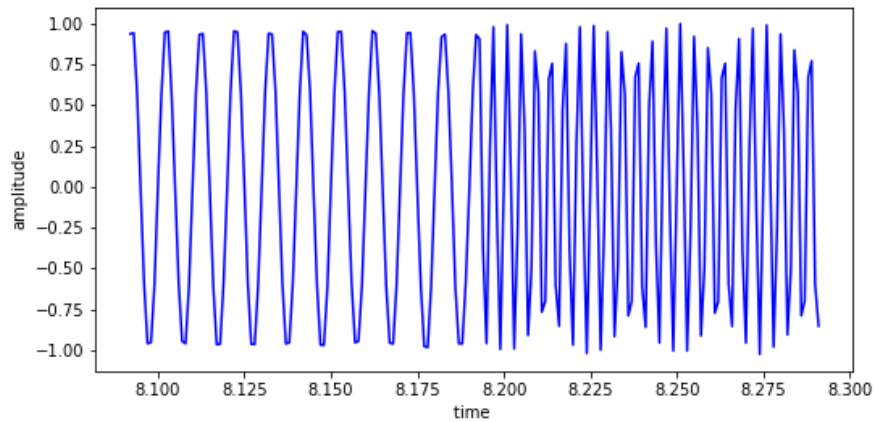
1. Excite beams with a sinusoidal carrier
2. Measure beam response
3. Sweep excitation frequency slowly through beam response



- Stationary Signal
 - Signals with frequency content unchanged in time
 - All frequency components exist at all times
 - ideal situation for Fourier transform (FT)
(orthonormal base functions of Fourier transform are infinitely long, no time information when spectral component happens)
- Non-stationary Signal
 - Frequency composition changes in time
 - need different analysis tools
 - Illustration on the 3 following slides



Example of non-stationary signals



Two stationary signals (single frequency) changing at one point in time.

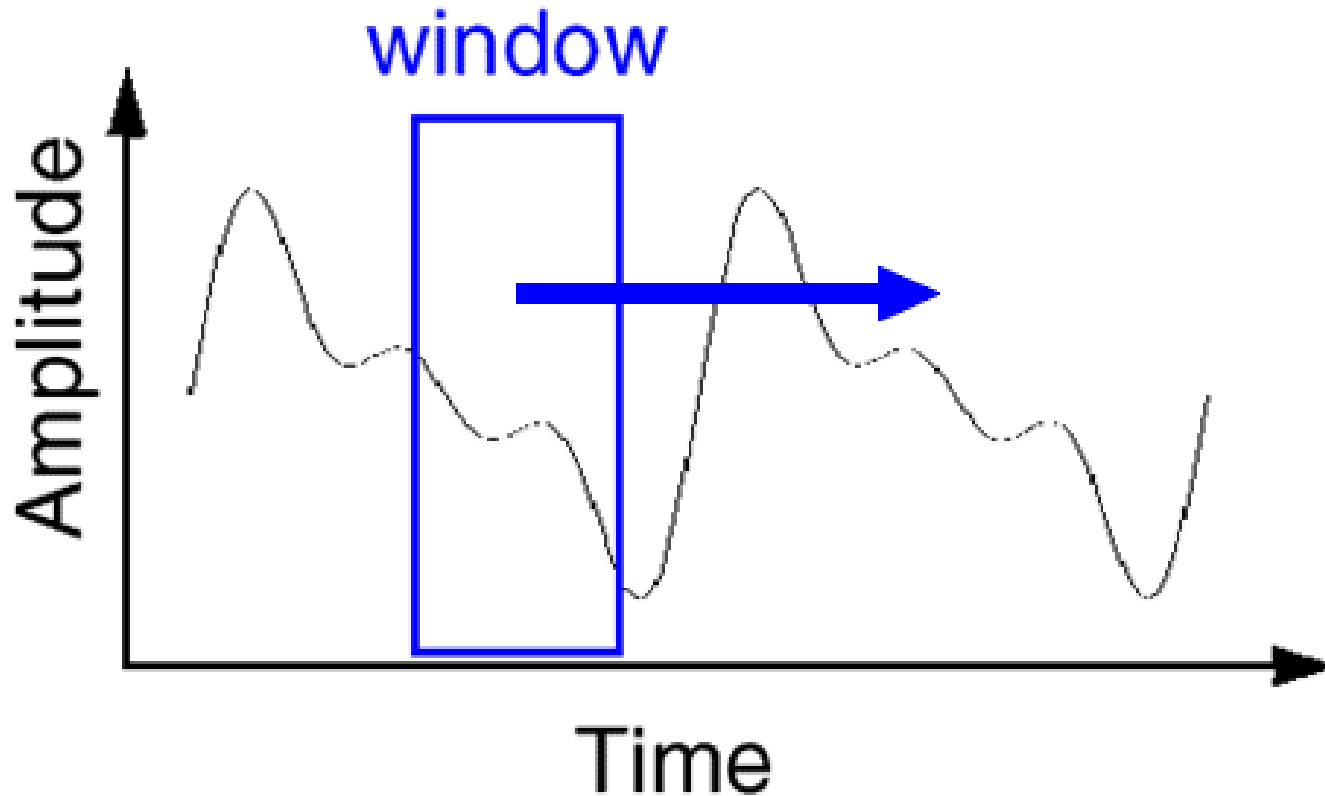
Blue: lower frequency first

Red: higher frequency first.

FT spectra identical; impossible to say which signal was first.

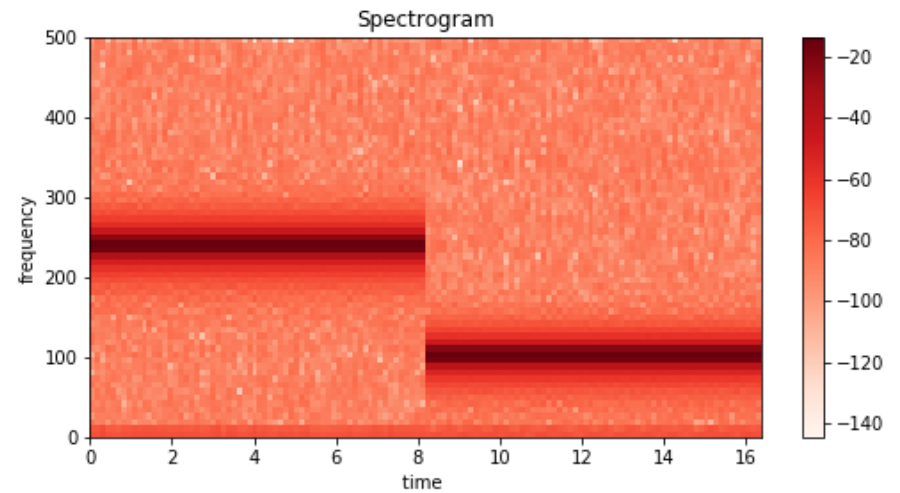
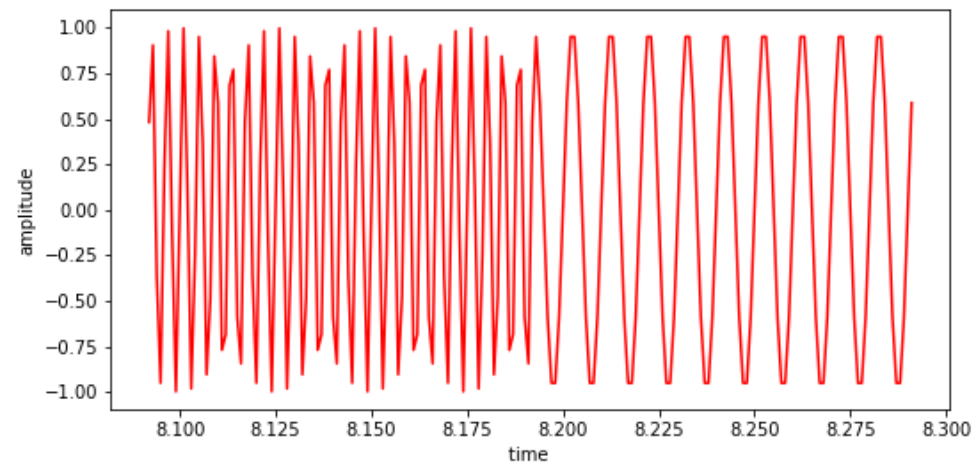
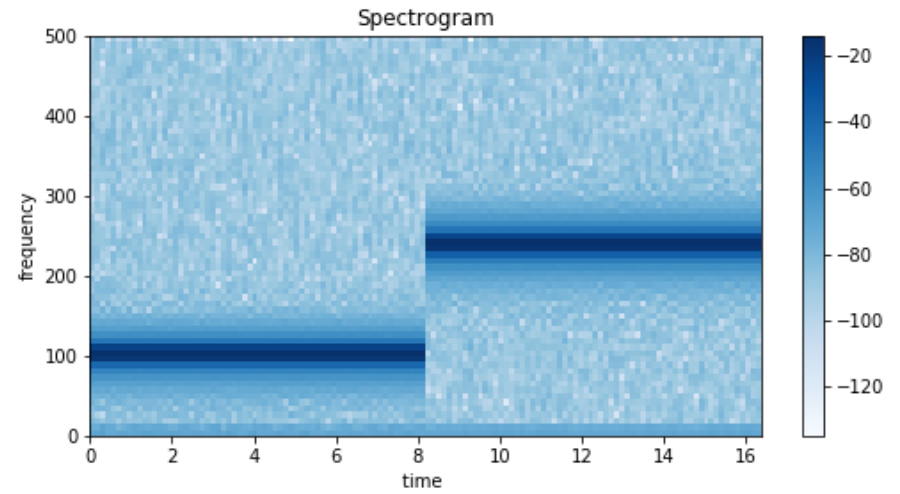
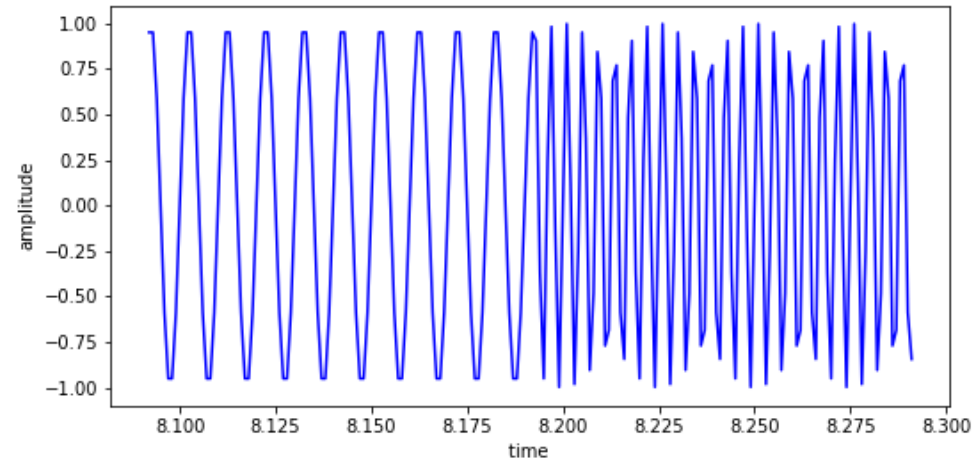
Sliding time window

(and FT each time window advances)

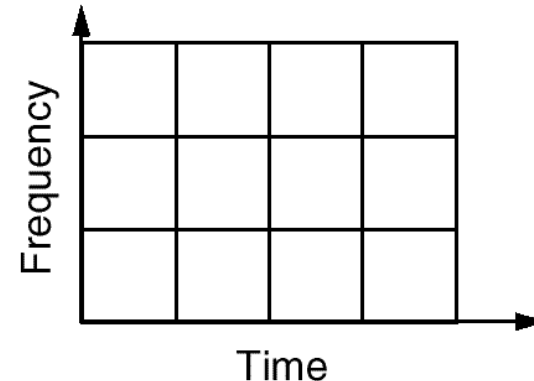
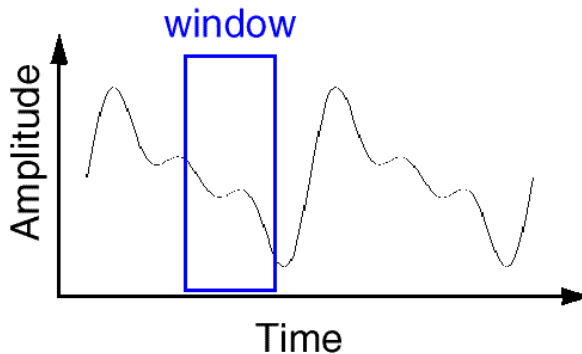


Originally called Short Time Fourier Transform (STFT) or spectrograms

Spectrogram of two consecutive signals at two distinct frequencies

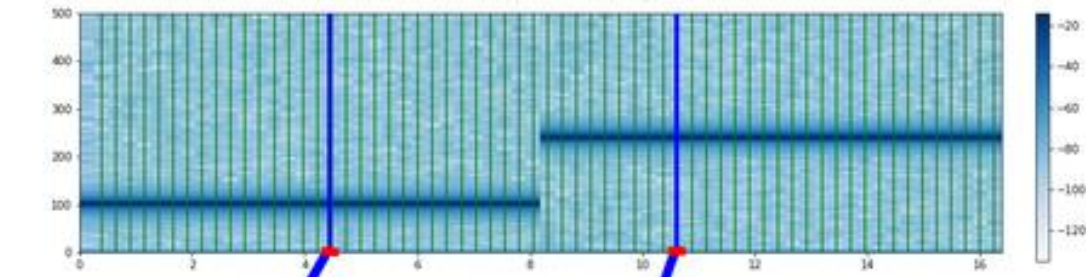


- In order to analyze small section of a signal, Dennis Gabor (1946), developed a technique, based on the FT and using windowing:
Short Time Fourier Transform:= STFT

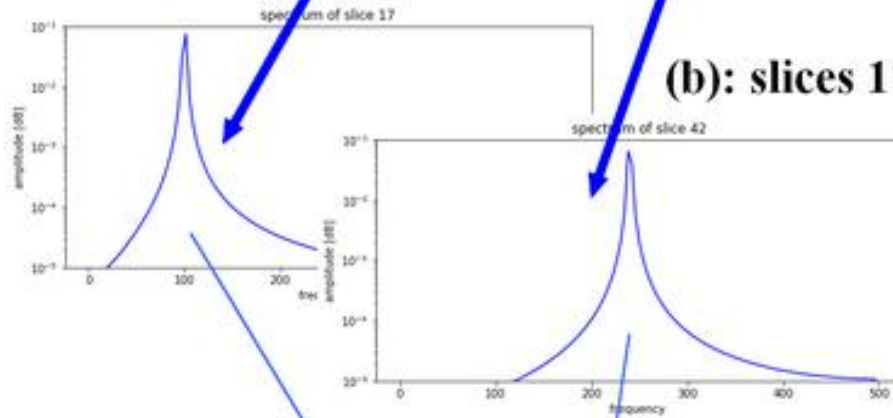


- A compromise between **time-based** and **frequency-based** views of a signal.
- both time and frequency are obtained in **limited precision**.
- The compromise between time and frequency resolution is given by the length of the time window.
- Usually one chooses a fixed length of the observation window during the analysis.

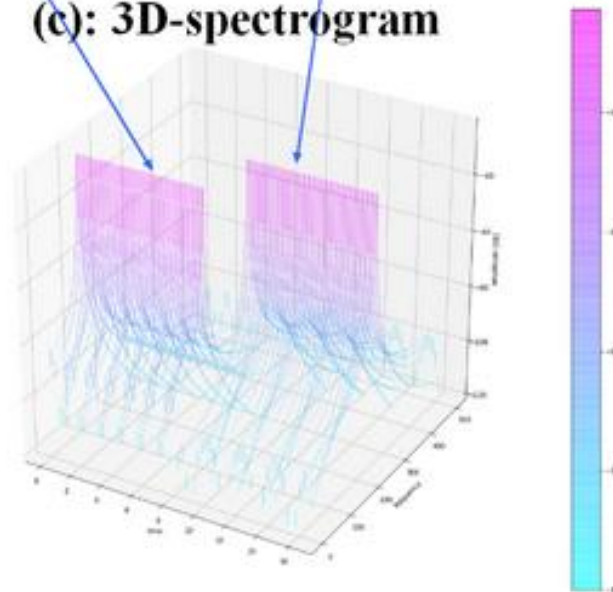
(a): 2D-spectrogram



(b): slices 17 & 42



(c): 3D-spectrogram

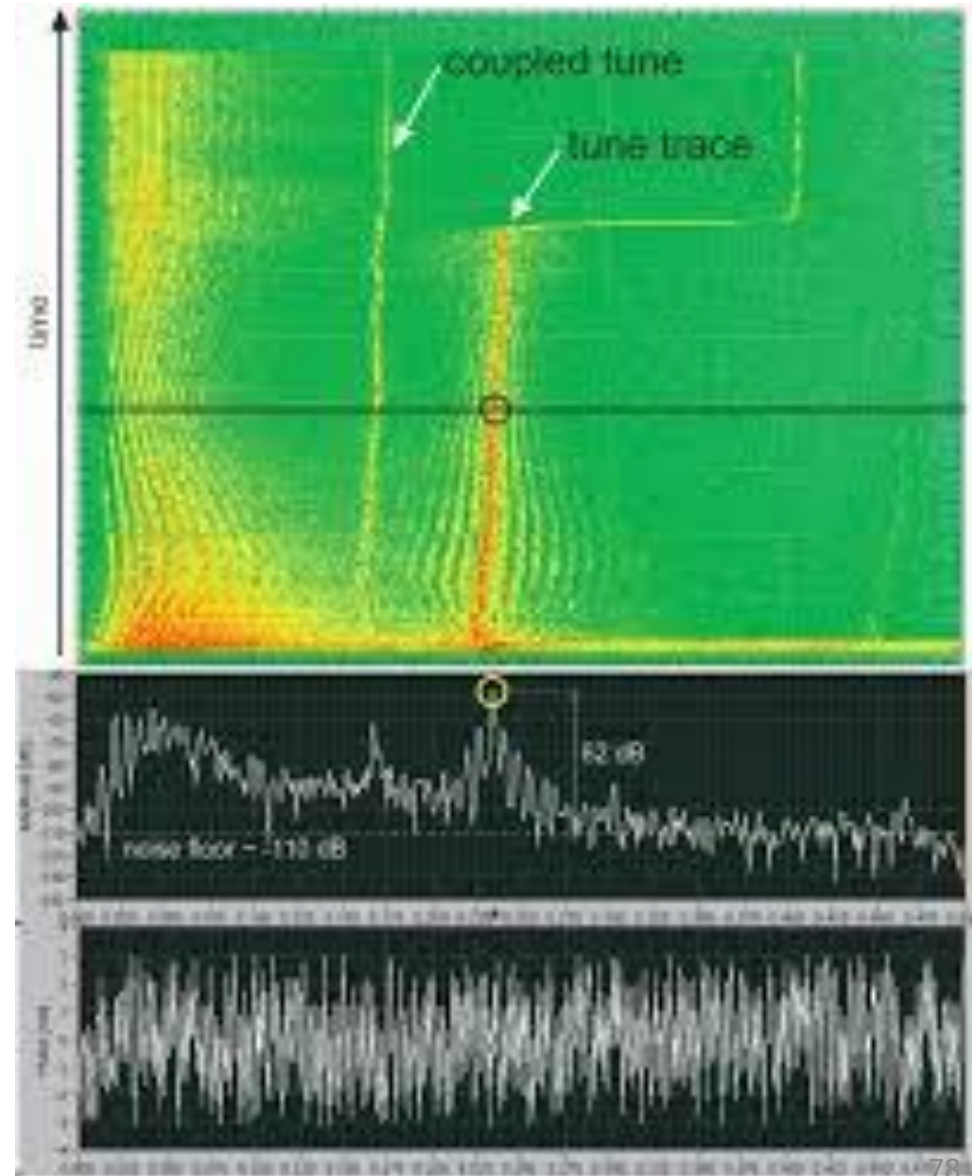


3D view

Not much readable information, but nice for publications 😊

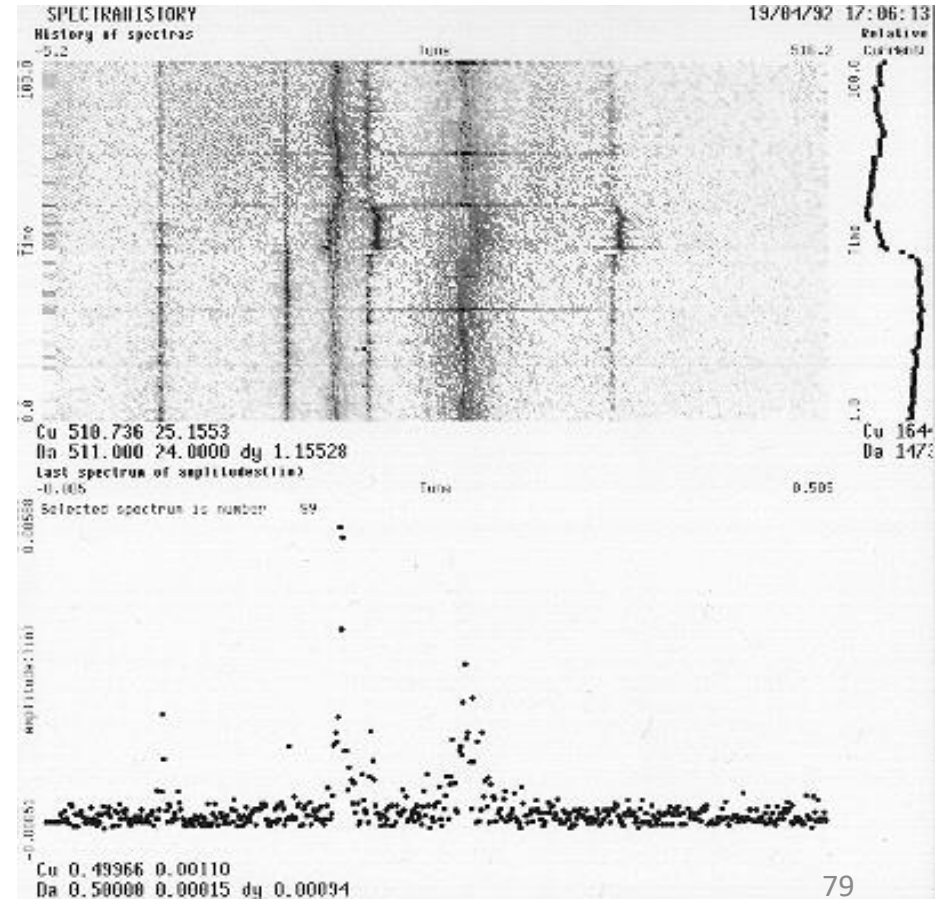
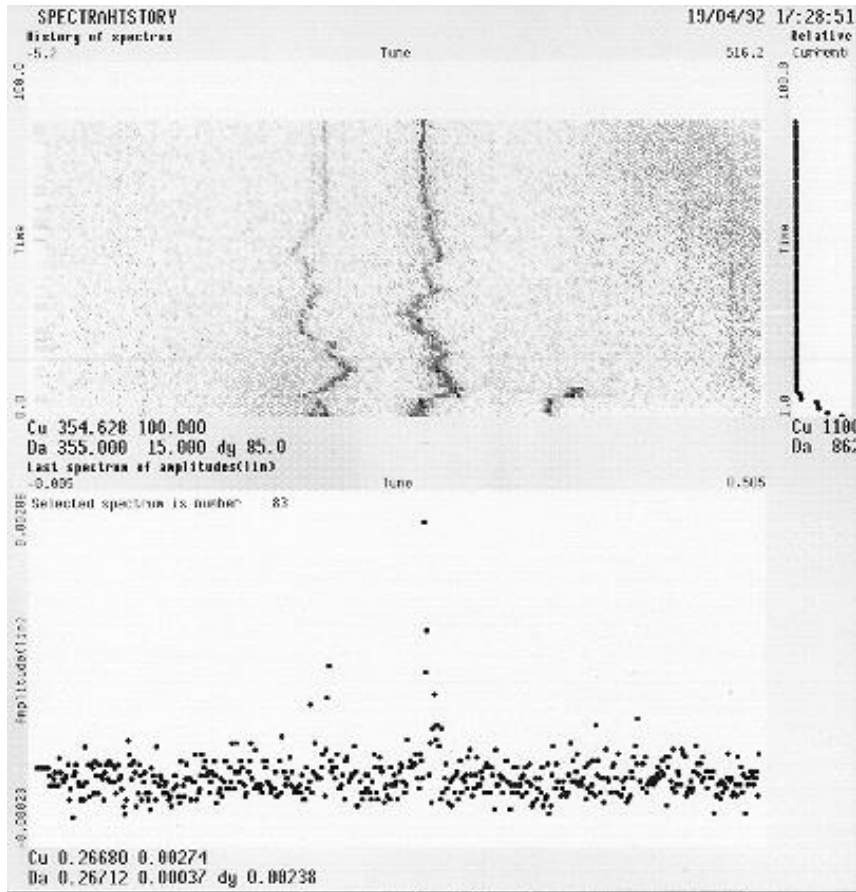
STFT Measurement examples I

- A trace of a transverse tune signal over several seconds during the energy ramp of the CERN SPS proton accelerator.



Even older:

Left: horizontal and vertical tunes during LEP acceleration
 Right: Machine experiment: all 3 tunes and synchro-betatron coupling



Some more cool stuff:



- Sampling in time and space in a circular accelerator + retransform of data as new set of samples only in time, but at a higher sampling frequency.
- Phase locked loop measurements of a single frequency (this way “in the old days” a radio receiver worked); if you still now what this is?
- Wavelet analysis; not really used in accelerators, but used for example to find oilfields!

- P.Zisopoulos et al, Phys. Rev. Acc.&Beams 22, 071002 (2019)

Refined betatron tune measurements by mixing BPM data

Basic idea: Create additional samples per turn by using data from neighbouring BPMs (up to 500 in the LHC) and transforming them from samples in space to samples in time.

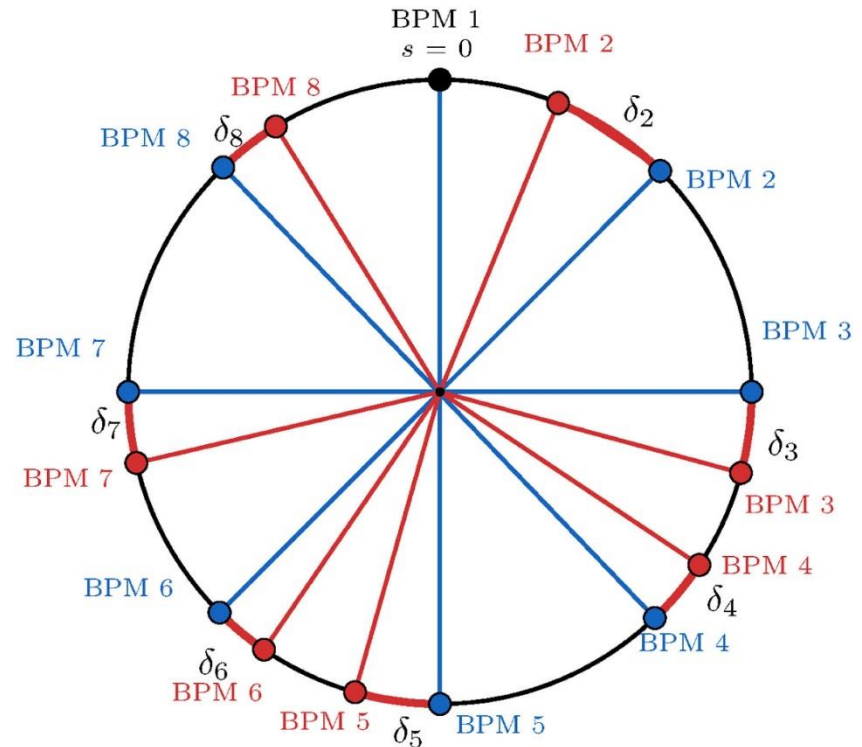


FIG. 1. A hypothetical ring with eight BPMs at longitudinal positions which are marked with red circles. When the mixed BPM method is employed, a sampling error δ_k is introduced, due to the deviation of the BPM positions from hypothetical locations that divide the circumference of the ring in exactly eight equal parts, marked with blue circles. BPM 1 is set as the reference point.

- During the injection process into the CERN PS strong orbit deflectors are activated. In addition to the wanted orbit change this leads also to an unwanted tune change: Needs to be measured
- Single BPM measurements do not have enough time resolution at high frequency resolution

→ use several BPMs
 With remarkable resolution
 for 40 turns

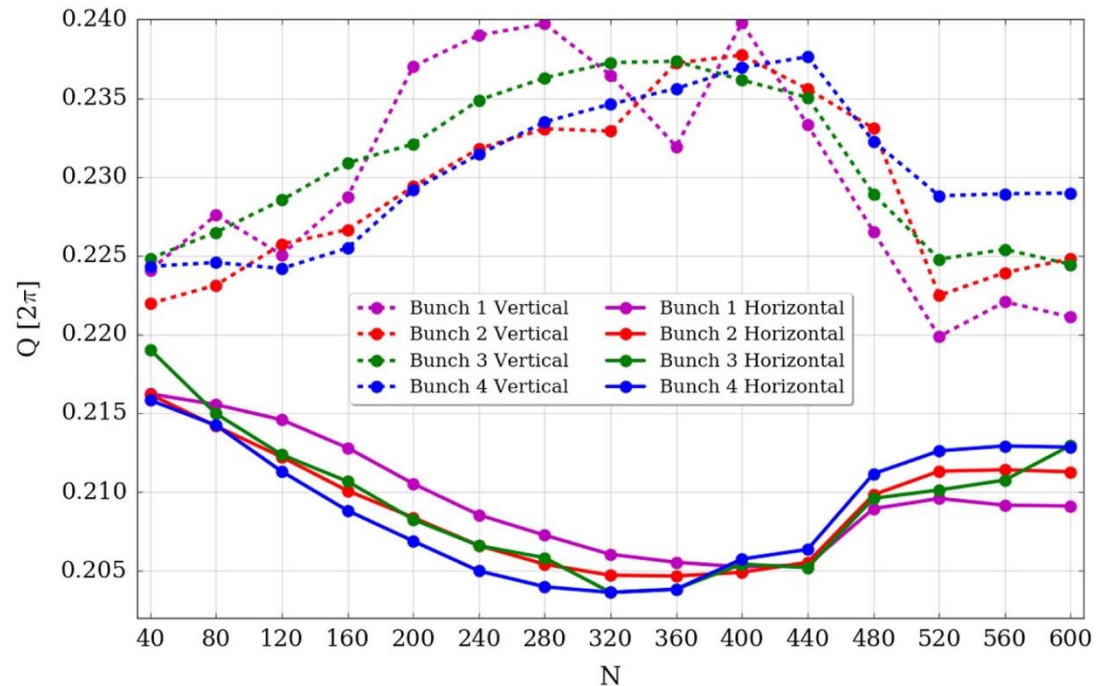
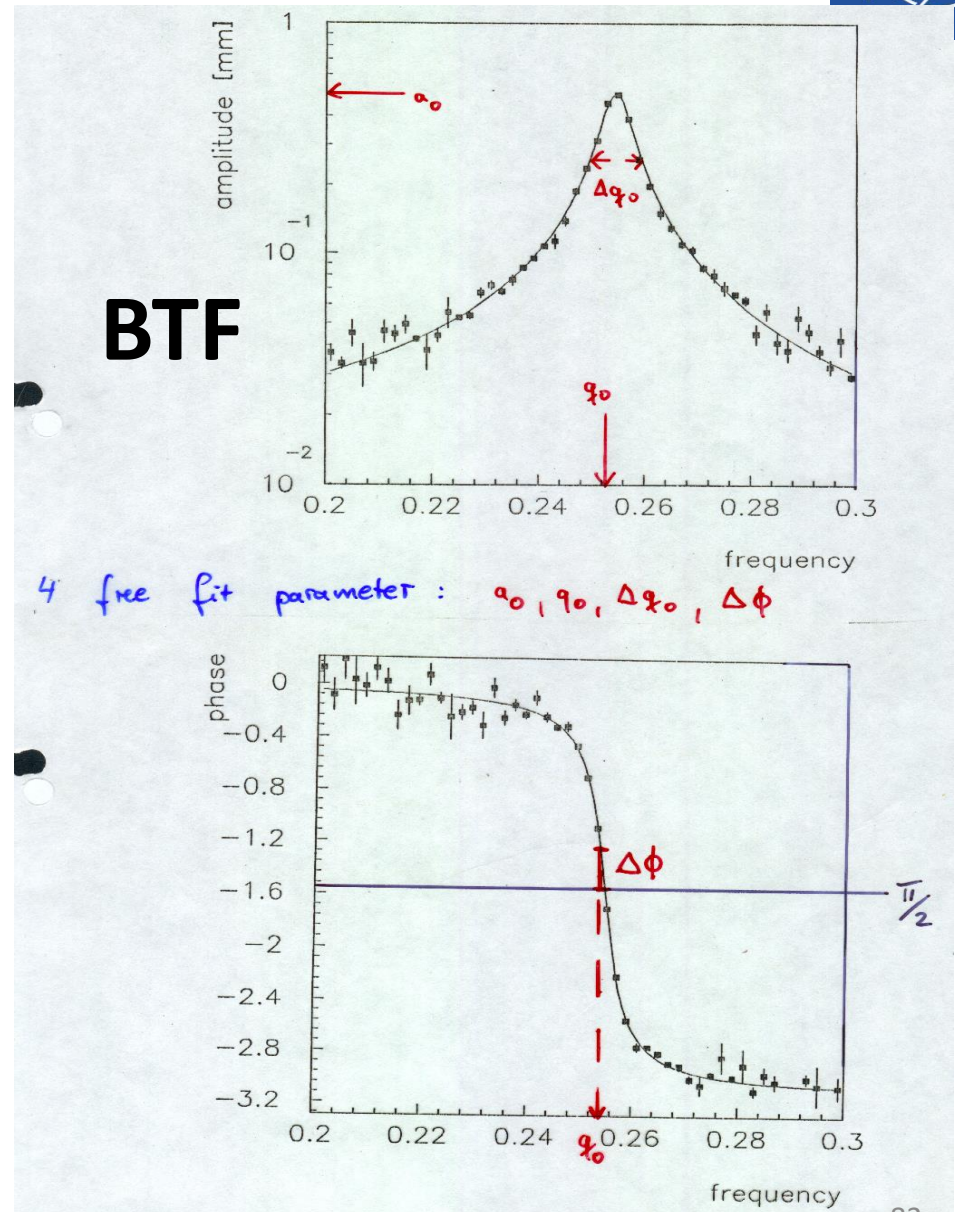


FIG. 20. Instantaneous betatron tune measurements with the mixed BPM method, during the injection process at the PS. The estimation of the horizontal tunes is shown in thick lines and of the vertical tunes in dashed lines. The analysis is performed for four bunches (bunch 1 in magenta, bunch 2 in red, bunch 3 in green, and bunch 4 in blue) by using a sliding window of 40 turns.

1. So far all methods use exclusively the amplitude information (BTW: in the case of self excited oscillations this is the only way!)
2. But if you drive a betatron oscillation of the beam through an external force, one can use the phase between the exciter and the beam response as observable



Principle of PLL tune measurements

Recall: $\sin a \sin b = 1/2 (\cos(a - b) - \cos(a + b))$

Due to $\cos(\varphi) = 0$ at resonance this system “looks” to the 90 deg. point of the BTF

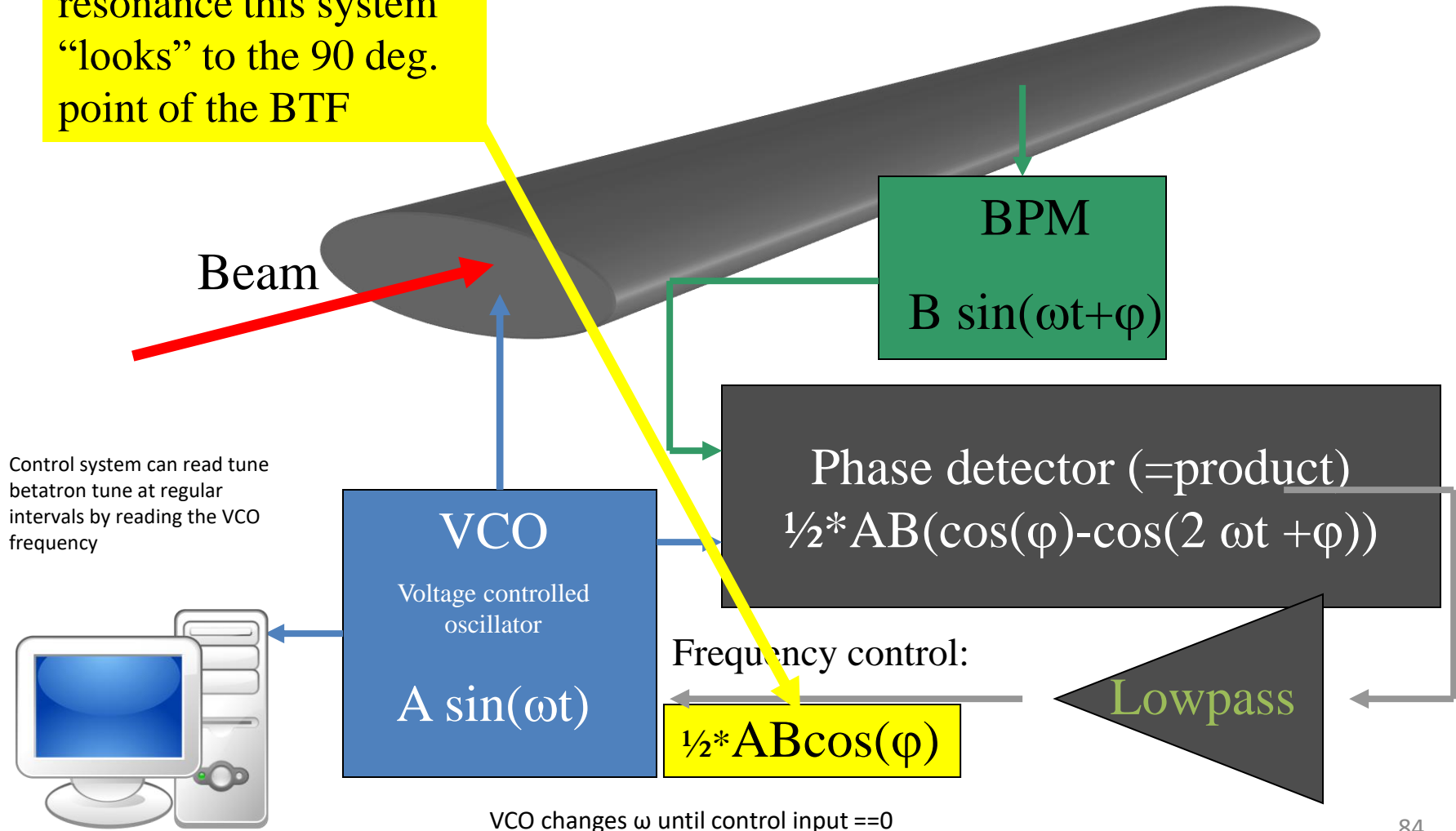
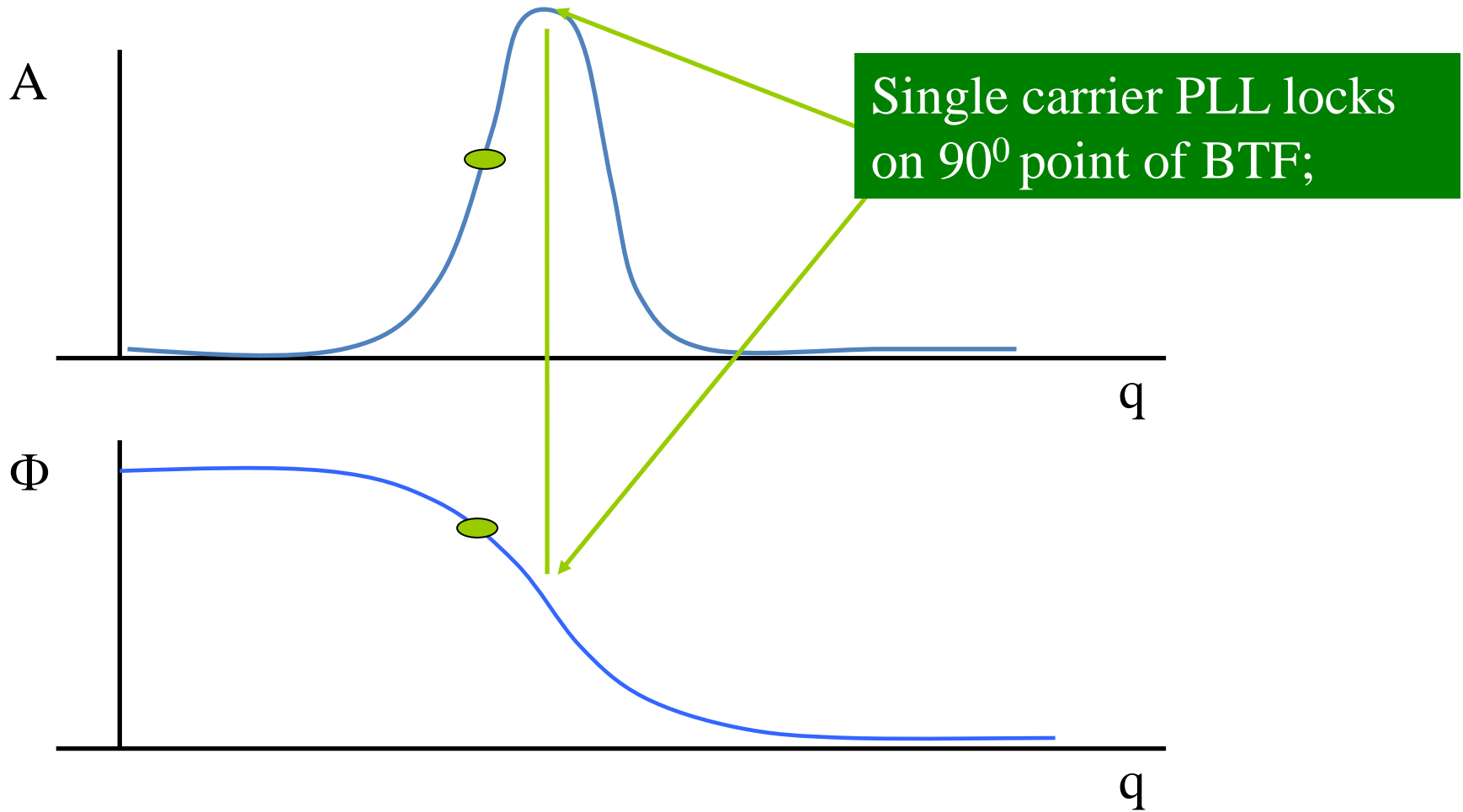
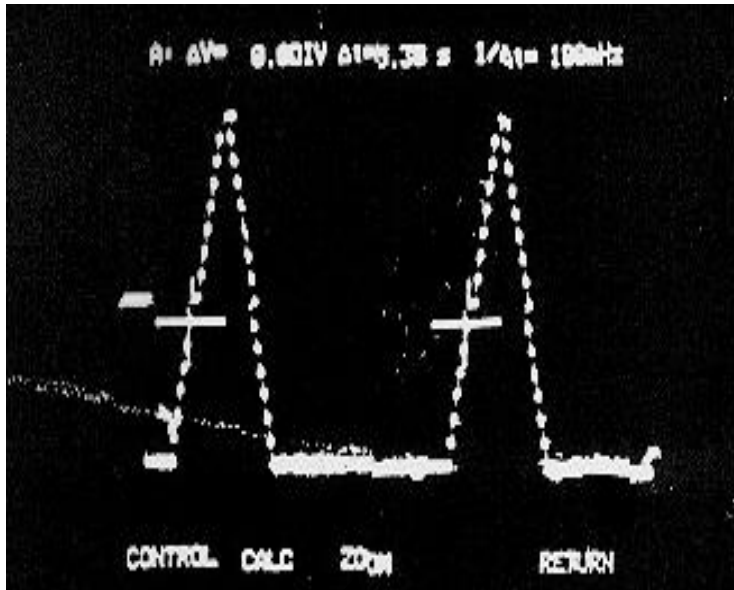
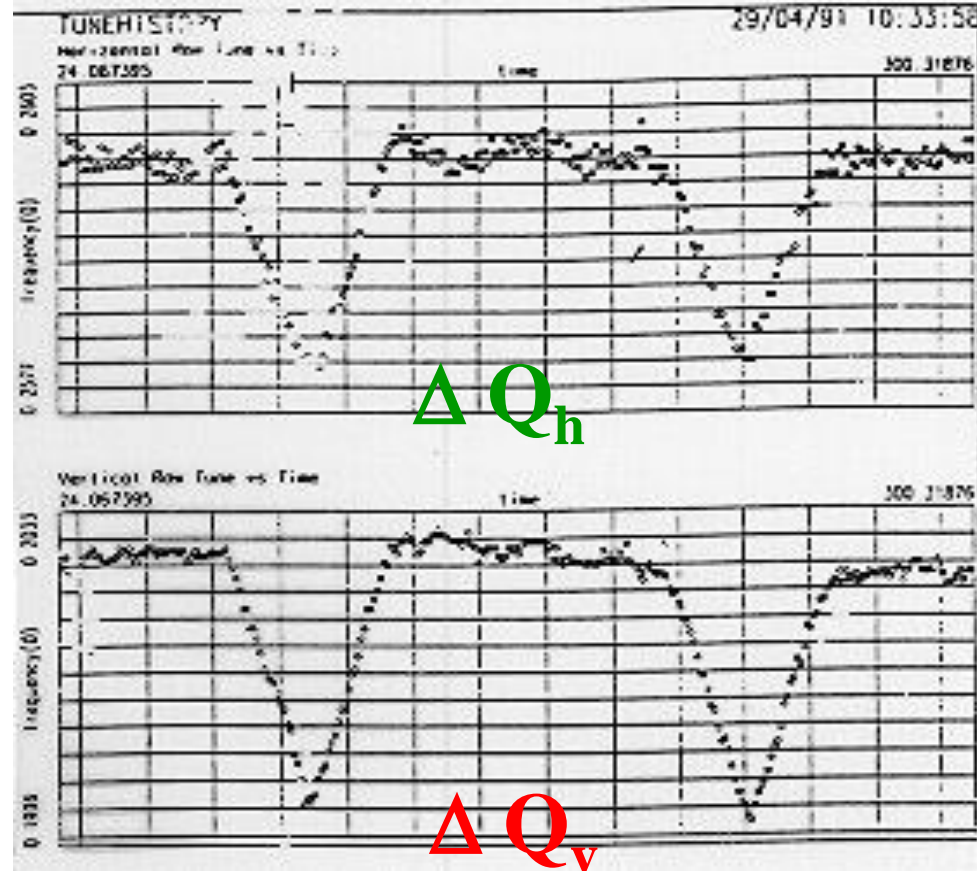


Illustration of PLL tune tracking



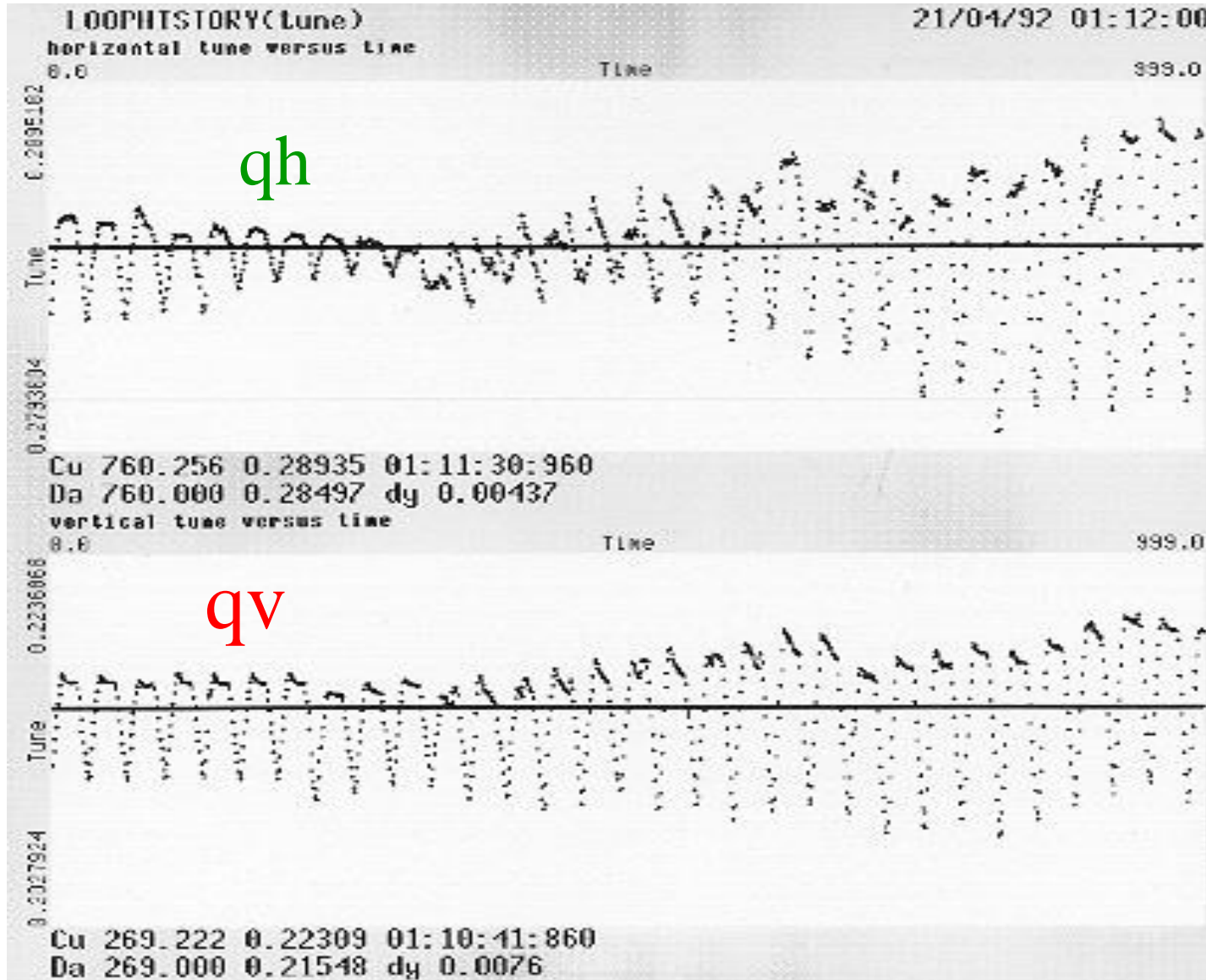


Applied Frequency Shift
 ΔF (RF)



Amplitude & sign of chromaticity
calculated from continuous tune plot

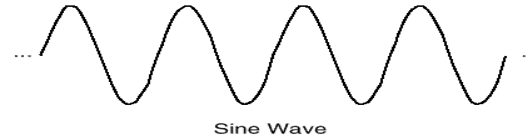
Measurement example during changes on very strong quadrupoles in the insertion: LEP β -squeeze



What is Wavelet Analysis ?



- And...what is a wavelet...?



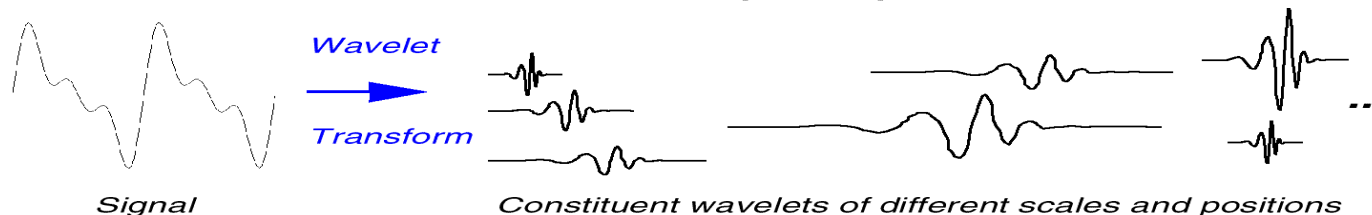
A wavelet is a waveform of effectively limited duration that has an average value of zero.

In a Fourier transform (FT) we represent the data by the **weighted sum of infinite sine waves** with different frequencies.

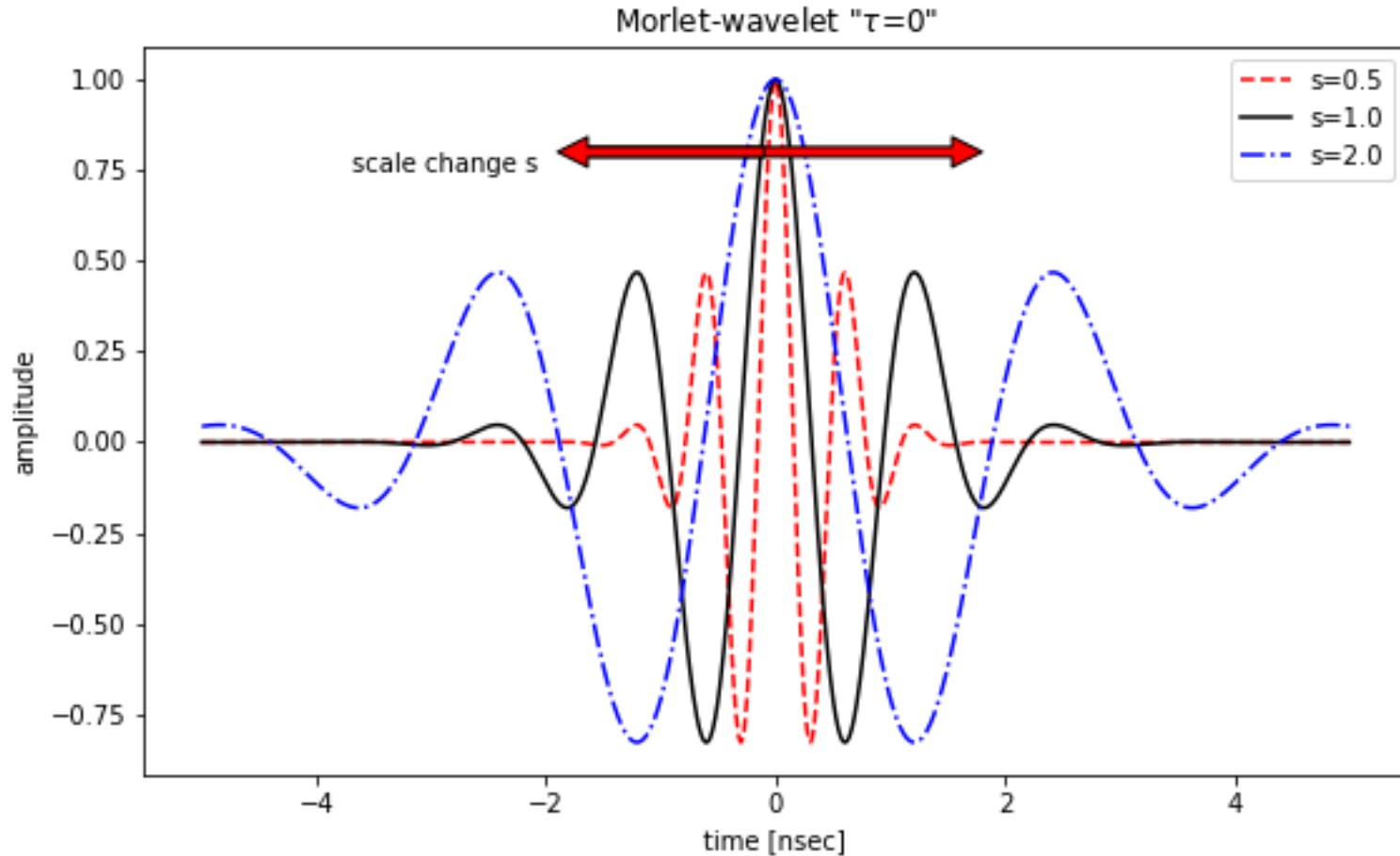
So the “signal analyzing” functions are infinite sine waves.

In the continuous wavelet transform (CWT) we represent the data by the weighted sum of **appropriately scaled and shifted wavelets**.

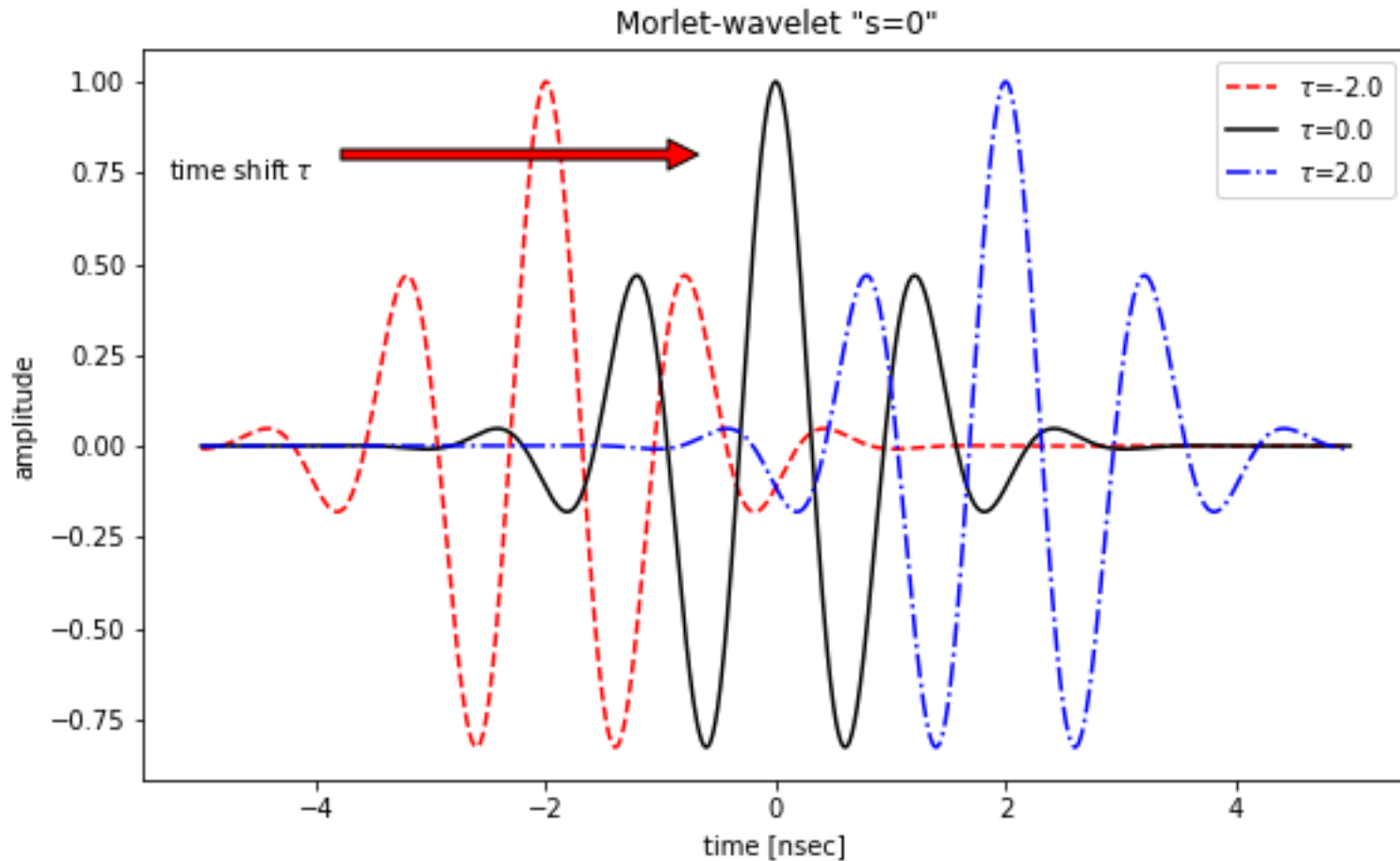
So instead of only infinite sine waves we take frequency dependent wavelets (by scaling) and time dependent wavelets (by shifting) as “two dimensional set of analyzing functions”



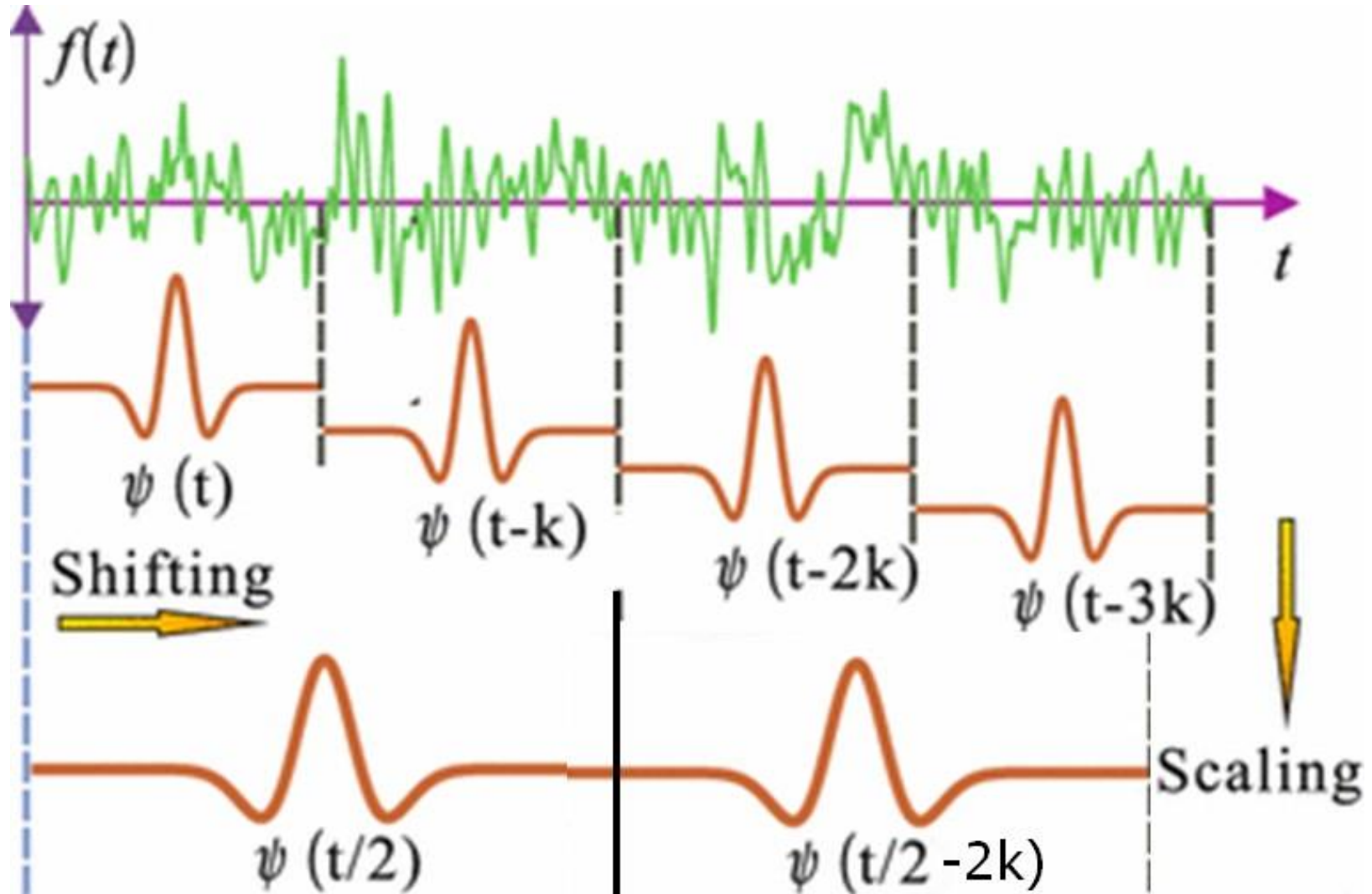
- Time stretching or frequency scaling:



■ Time shifting:



Wavelet Analysis by Shifting and Scaling



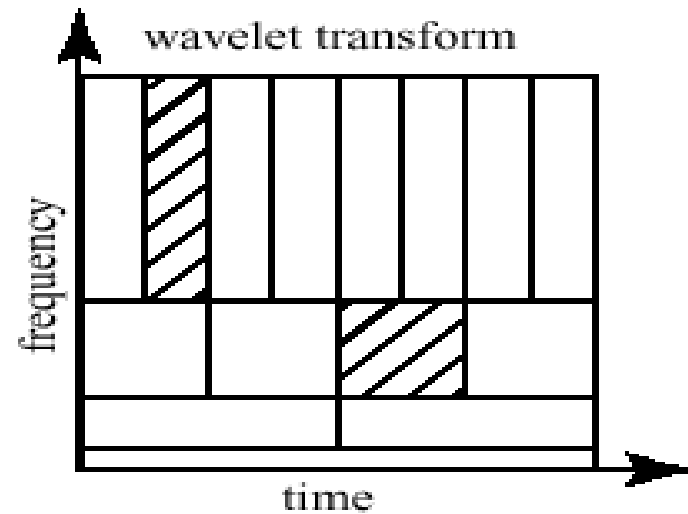
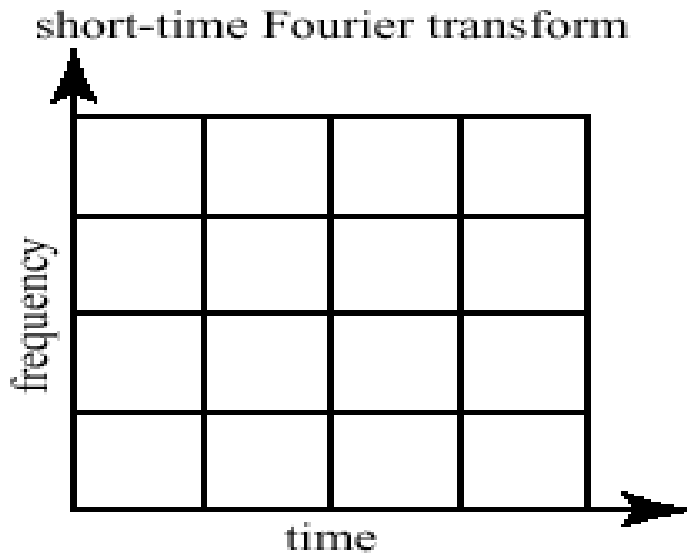
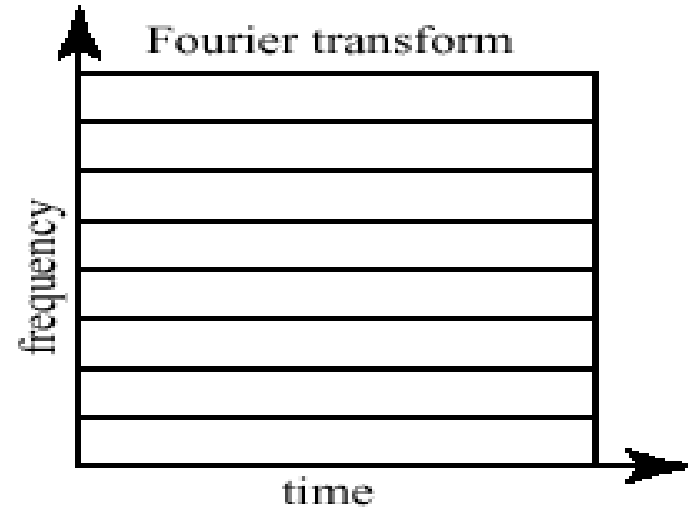
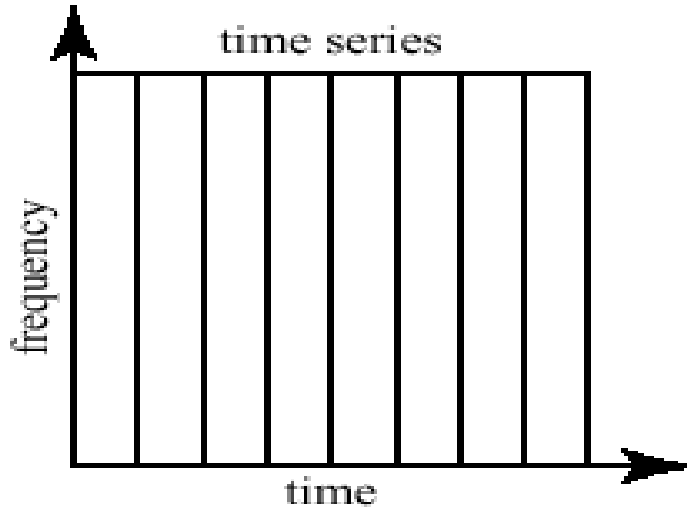
Historical Development of wavelet transforms (main contributors)

- Pre-1930
 - Joseph Fourier (1807) with his theories of frequency analysis
- The 1930^s
 - Using scale-varying basis functions; computing the energy of a function
- 1960-1980
 - Guido Weiss and Ronald R. Coifman; Grossman and Morlet
- Post-1980
 - Stephane Mallat; Y. Meyer; Ingrid Daubechies; wavelet applications today

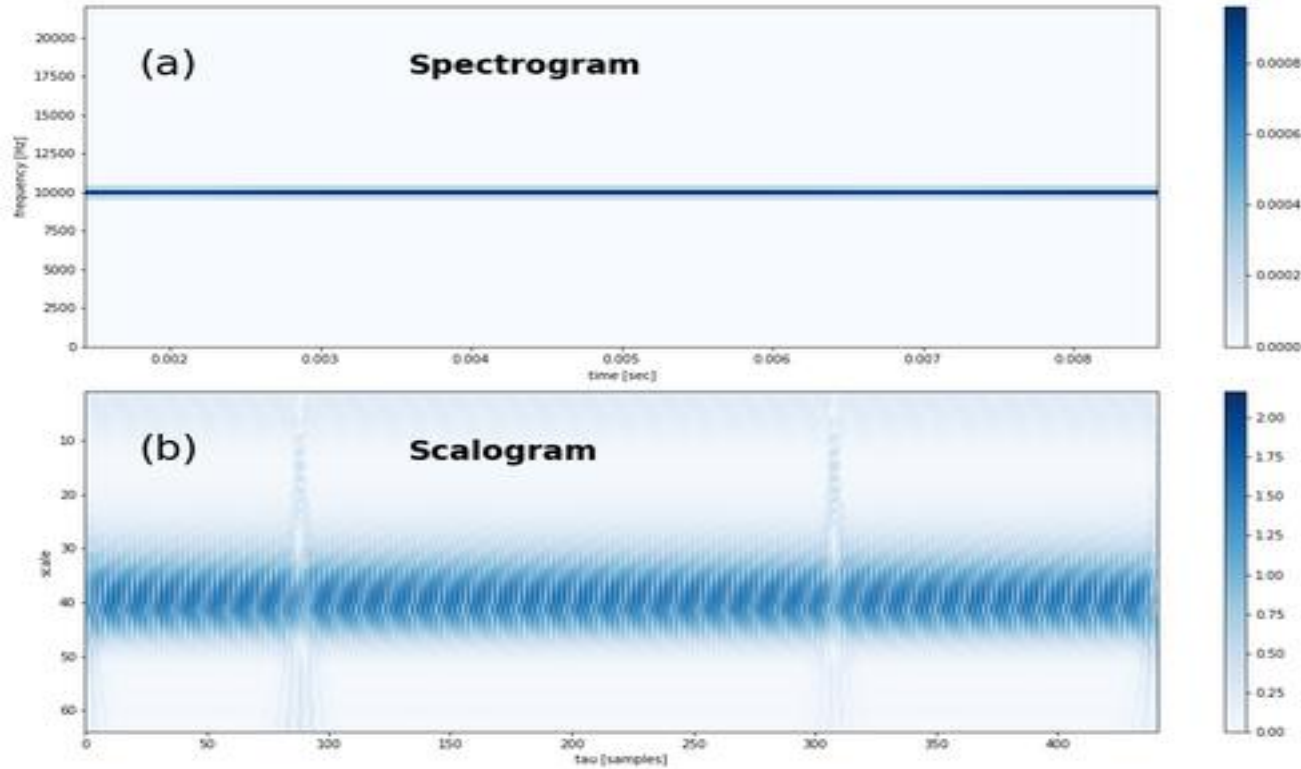
Transform	Mathematical Expression
Fourier Transform (FT)	$\mathcal{F}_x(\omega) = \int_{-\infty}^{+\infty} x(t) \cdot e^{-j\omega t} dt$
Gabor Transform (STFT)	$G(\tau, \omega) = \int_{-\infty}^{\infty} x(t) \cdot e^{\alpha\pi(t-\tau)^2} \cdot e^{-j\omega t} dt$
Wavelet Transform (WT)	$\Psi_x^\psi(\tau, s) = \frac{1}{\sqrt{s}} \int_{-\infty}^{+\infty} x(t) \cdot \psi\left(\frac{t-\tau}{s}\right) dt$

The variables in red are linked to frequency resolution, the variables in blue to time resolution.

COMPARISON in terms of time and frequency resolution



Example (STFT vs WT)



In a continuously sampled sine wave two artefacts (value set to 0) are introduced at two different times.

In the result of the STFT (top trace: Spectrogram) there is no effect visible,

In the result of the WT (bottom trace: Scalogram) the location of the irregularities can be spotted.

- Stationary Signals:
windowed FFT with interpolation/fitting.
!!! Depending on the S/N the gain from very sophisticated methods needs to be evaluated!!!
- Time varying Signals:
 - Good S/N + lots of data: STFT (spectrograms)
i.e. most of the accelerator applications
 - Small S/N + few data: wavelets
possible case: instabilities at threshold
- Alternatively (if not complete spectral information is required): PLL tune tracking

- Single beam passage in a detector produces a signal with a continuous frequency spectrum. The shorter the bunch, the higher the frequency content.
- Repetitive bunch passages produce a line spectrum. The individual spectral lines are called revolution harmonics. Details of the bunch pattern, differences in bunch intensities etc. determine the final spectral distribution.
- Transverse or longitudinal oscillations of the bunch around the equilibrium produce sidebands around all revolution harmonics.
- These sidebands are used for the measurement of the betatron tunes and/or the synchrotron tune.
- The standard tool for obtaining spectral information is a Fourier transform (FFT) of time sampled signals.
- Windowing and interpolation allow measurements with higher frequency resolution.
- Spectrograms or STFTs are consecutive FFTs of larger datasets, which allow to follow time varying spectra. A compromise has to be found between time resolution and frequency resolution.
- Phase locked loops can be used for continuous tune tracking, hence one obtains the time evolution of the main beam resonance (tune). No other spectral information!
- Wavelet analysis instead of Spectrograms are an alternative analysis tool. This is really useful in the case of few time samples.

Appendix I: Python Code for bunch pattern display

Appendix Ia: Python code for bunch pattern simulation 1st part

- `import numpy as np`
- `from numpy import fft`
- `import matplotlib.pyplot as plt`

- `N=16384`

- `NBUNCH=100`
- `sigmax = 0.5`

- `deltax=10`

- `T=1/N`

- `NLEFT=-50`
- `NRIGHT=50`

- `x1= np.linspace(NLEFT,N-NLEFT,N)`
- `xtime=np.linspace(NLEFT,NBUNCH*deltax + NRIGHT,N)`
- `IB=0`
- `y=NBUNCH*np.exp(-(x1*x1)/(2*sigmax*sigmax))`
- `ytime=NBUNCH*np.exp(-(xtime*xtime)/(2*sigmax*sigmax))`
- `y1=0`
- `y2=0`
- `y3=0`
- `ytime=0`

- `while True:`
-
- `y1=y1+np.exp(-(x1-IB*deltax)*(x1-IB*deltax)/(2*sigmax*sigmax))`
- `ytime=ytime+np.exp(-(xtime-IB*deltax)*(xtime-IB*deltax)/(2*sigmax*sigmax))`
- `IB=IB+1`
- `if IB==NBUNCH:`
- `break`

Appendix Ib: Python code for bunch pattern simulation 2nd part



- `ffty=(fft.fft(y))`
- `ffty1=(fft.fft(y1))`
- `x2=np.linspace(0.0,500,N/2)`
- `y2=2.0*np.abs(ffty1[:N//2])/float(N)`
- `y3=2.0*np.abs(ffty[:N//2])/float(N)`

- `plt.rcParams["figure.figsize"] = [15,4]`
- `plt.subplot(1,2,1)`

- `plt.plot(xtime,ytime,'b-')`

- `plt.ylabel('amplitude')`
- `plt.xlabel('time [nsec]')`

- `plt.subplot(1,2,2)`

- `plt.plot(x2,y3,'r-')`
- `plt.plot(x2,y2,'b-')`
- `plt.ylabel('amplitude')`
- `plt.xlabel('frequency [MHz]')`

- `plt.tight_layout()`
- `plt.savefig('whatever.png')`

- `plt.show()`