



Materials for magnets & measurements - I

Lecture I, Mon Nov 27

- Introduction and bibliography
- o Magnetic properties of materials: types of magnetic behaviour
- Families and behaviour of magnetic materials

Lecture II, Tue Nov 28

- o Materials for magnets: structural, cryogenics, vacuum
- o Non-magnetic materials, phase transformations and measurements

CAS course on "Normal- and Superconducting Magnets", 19/11 - 02/12/2023, St. Pölten, Austria

Stefano Sgobba



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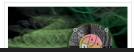
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Introduction and bibliography



Handbook of Magnetism and Advanced Magnetic Materials, 5 Volume Set

We gratefully acknowledge

Cornell University

ar\iv > physics > arXiv:1103.1069

Search...

Physics > Accelerator Physics

[Submitted on 5 Mar 2011]

Ferromagnetism

Physics and measurements of magnetic materials

S. Sgobba (CERN)

Magnetic materials, both hard and soft, are used extensively in several components of particle accelerators. Magnetically soft iron-nickel alloys are used as shields for the vacuum chambers of accelerator injection and extraction septa; Fe-based material is widely employed for cores of accelerator and experiment magnets; soft spinel ferrites are used in collimators to damp trapped modes; innovative materials such as amorphous or nanocrystalline core materials are envisaged in transformers for high-frequency polyphase resonant convertors for application to the International Linear Collider (ILC). In the field of fusion, for induction cores of the linac of heavy-ion inertial fusion energy accelerators, based on induction accelerators requiring some 107 kg of magnetic materials would show the best performance in terms of core losses for magnetization rates as high as 105 T/s to 107 T/s. After a review of the magnetic properties of materials and the different types of magnetic behaviour, this paper deals with metallurgical aspects of magnetism. The influence of the metallurgy and metalworking processes of materials on their microstructure and magnetic properties is studied for different categories of soft magnetic materials relevant for accelerator technology. Their metallurgy is extensively treated. Innovative materials such as iron powder core materials, amorphous and nanocrystalline materials are also studied. A section considers the measurement, both destructive and non-destructive, of magnetic properties. Finally, a section discusses magnetic lag effects.

Comments: 25 pages, presented at the CERN Accelerator School CAS 2009: Specialised Course on Magnets, Bruges, 16-25 June 2009

Subjects: Accelerator Physics (physics.acc-ph); Materials Science (cond-mat.mtrl-sci)

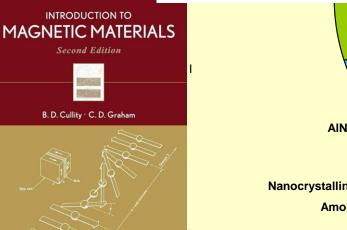
Cite as: arXiv:1103.1069 [physics.acc-ph]

(or arXiv:1103.1069v1 [physics.acc-ph] for this version)

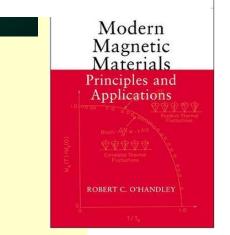
https://doi.org/10.48550/arXiv.1103.1069

Journal reference: CERN-2010-004, pp. 39-63

https://doi.org/10.48550/arXiv.1103.1069



AlNiCo
Nanocrystalline materials
Amorphous materials
Fe-Co alloys



B.D. Cullity, C.D. Graham, Introduction to Magnetic Materials, 2nd ed., Wiley (2009)

11 Augustians and Special-Fulpose Metals, American Society for Metals, Metals Fair, Office 2023-11-2 (1980)



Magnetic properties of materials

1. Some general definitions

2. Types of magnetic behaviour

- a. diamagnetism
- b. paramagnetism
- c. ferromagnetism
- d. antiferromagnetism
- e. [ferrimagnetism]
- f. [spin glasses...]

3. Families and behaviour of magnetic and non-magnetic materials

- a. materials for magnetic applications (with point 2.c)
- b. non-magnetic materials (point 2.b and 2.d)
- 4. Phase transformations and their influence on magnetic behaviour (\rightarrow 28/11)





Magnetic properties of materials

- Focused on temperature range of interest for magnet construction
- Focused on materials of technological interest
- Non-magnetic and structural materials and specific risks covered (examples issued from CERN and ITER applications)
- Applied and technological approach
- SI units used





Magnetic properties of materials, some definitions

- Flux density, magnetic induction B (T)
- Permeability μ (H·m⁻¹)
- Magnetic field strength H (A·m-1)

$$B = \mu \cdot H$$

Magnetization M (A·m⁻¹)

$$B = \mu_0 \cdot (H + M)$$

- Permeability of free space μ₀ (H·m⁻¹)
- Susceptibility K (dimensionless) = M/H



Magnetic properties of materials, some definitions

From above equations

•
$$\mu = \mu_0 \cdot (\mathbf{1} + \mathbf{\kappa})$$

Relative permeability defined as

•
$$\mu_r = \mu / \mu_0 = 1 + \kappa$$

- and frequently encountered in discussions of ferromagnetic materials
- μ , μ_r , κ are properties of materials



Magnetic properties of materials, some definitions

SI units exclusively used

Table 6.1 Units for magnetic properties.

	cgs emu		Conversion Factor,	mks SI	
Property	Symbol	Units	C ^a	Symbol	Units
Flux density, magnetic induction	В	gauss (G)	10 ⁻⁴	В	tesla (T) b
Flux	φ	maxwell (Mx)	10^{-8}	ϕ	weber (Wb)
Magnetic field strength, magnetizing force	Н	oersted (Oe) c	$10^{3}/4\pi$	Н	A·m ^{-1 d}
(Volume) magnetiza-	M	emu·cm ^{-3 e}	103	$M^{\mathfrak{l}}$	A·m ⁻¹
(Volume) magnetiza-	$4\pi M$	gauss (G)	$10^3/4\pi$	M	A·m ⁻¹
(Mass) magnetization	σ, M	emu·g ⁻¹	1	σ, Μ	$A \cdot m^2 \cdot kg^{-1}$
(Volume) susceptibility	χ	dimensionless emu·cm ⁻³ ·Oe ⁻¹ emu·cm ⁻³	4π	к	dimensionless
(Mass) susceptibility	$\chi_{ ho}$	cm ³ ·g ⁻¹ emu·g ⁻¹ ·Oe ⁻¹ emu·g ⁻¹	$4\pi \times 10^{-3}$	$\kappa_{ ho}$	m ³ ·kg ⁻¹
(Molar) susceptibility	Xmol	cm ³ ·mol ⁻¹ emu·g ⁻¹ ·mol ⁻¹ ·Oe ⁻¹ emu·mol ⁻¹	$4\pi \times 10^{-6}$	κ _{mol}	m ³ ·mol ⁻¹
Magnetic moment	m	erg·Oe ⁻¹ , erg·G ⁻¹	10^{-3}	m	$\mathbf{A} \cdot \mathbf{m}^2$, $\mathbf{J} \cdot \mathbf{T}^{-1}$
Permeability	μ	dimensionless	$4\pi\times10^{-7}$	μ	henry·m ⁻¹ (H·m ⁻¹) ^g
Relative permeability		_	1	μ_r	dimensionless

 $^{^{}b}T = Wb \cdot m^{-2} = V \cdot s \cdot m^{-2}$

Dimensionally, 1 Oe = 1 G.

dOften expressed as ampere-turn·m-1.

^{&#}x27;The designation "emu" is not a unit. Sometimes substitution of "erg-Oe-1" or "erg-G-1" will yield correct units. Often called intensity of magnetization, I, or magnetic polarization, J. It is the magnetic moment per unit volume.

 $[^]gH\cdot m^{-1}=Wb\cdot A^{-1}\cdot m^{-1}$.

Magnetic properties of materials, some general definitions

• The basic natural unit for magnetism is the "Bohr magneton"

$$\mu_{\rm B} = {\rm e} \cdot {\rm h} / 4\pi \cdot {\rm m}_{\rm e} = 9.274 \cdot 10^{-24} \, {\rm A} \cdot {\rm m}^2$$

- Three sources of the magnetic force of a free atom (Kittel):
 - a. The spin with which electrons are endowed
 - b. Their orbital angular momentum about the nucleus
 - c. The change in orbital moment induced by an applied magnetic field
 - a and b give paramagnetic contributions to the magnetisation
 - c gives a diamagnetic contribution









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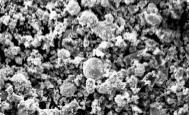




Figure 3

Aimant: prélèvement 1 = poussière prélèvement 2 = particules sur la section de l'aimant

Gant intérieur : prélèvement 3 a l'intérieur du gant

support avec les échantillons

& measur

Magnetic properties of materials

CERN releases analysis of LHC incident

16 OCTOBER, 2008

Geneva, 16 October 2008. Investigations at CERN following a large helium leak into sector 3-4 of the Large Hadron Collider (LHC) tunnel have confirmed that cause of the incident was a faulty electrical connection between two of the accelerator's magnets. This resulted in mechanical damage and release of helium from the magnet cold mass into the tunnel.

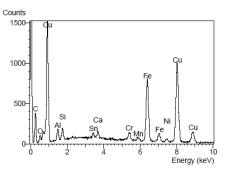
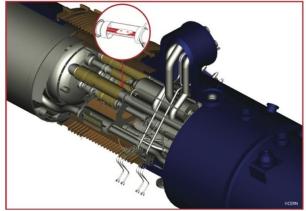


Figure 7: analyse sur particule voir Fig. 5 (flèche rouge): $\mathbf{C} - \mathbf{O} - \mathbf{Al} - \mathbf{Si} - \mathbf{Sn} - \mathbf{Ca} - \mathbf{Cr} - \mathbf{Mn} - \mathbf{Fe} - \mathbf{Ni} - \mathbf{Cu}$



Damage of the LHC magnets in sector 3-4 of the LHC, provoked by the incident which happened on 19 September 2008 (Image: CERN)

]	Elmt	Spec	t. Ele	men	t Atom	ic
		Ty	/pe	%	%	
	Al	lΚ	2	.13	4.61	
	Si	K	1.	89	3.93	
	C	a K	0	.74	1.07	
	C1	· K	2.	.09	2.35	
	\mathbf{M}	n IZ		-00	0.95	
	Fe	K	24	.45	25.58	
7	N	i K	2	.02	2.01	
	Cı	ιK	63	3.47	58.36	
	51	I L	- î		1.13	
	Tota	al	100	.00	100.00	

Magnetic properties of materials

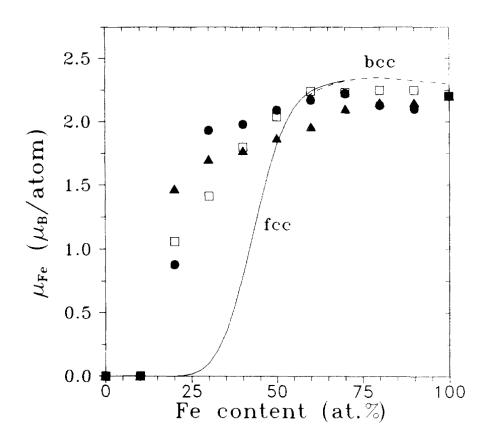


FIG. 5. Magnetic moment per Fe atom (μ_{Fe}) for bcc (dashed lines) and fcc (solid lines) Fe_xCu_{100-x} as a function of Fe content. Symbols denote experimental data (black dots from Ref. 2, triangles from Ref. 4, and squares from Ref. 6).

PHYSICAL REVIEW B

VOLUME 50, NUMBER 2

1 JULY 1994-II

Ferromagnetism in FeCu metastable alloys

P. A. Serena and N. García

Grupo de Física de Sistemas Pequeños, Consejo Superior de Investigaciones Científicas, Universidad Autónoma de Madrid, Cantoblanco, E-28049 Madrid, Spain (Received 7 February 1994)

TABLE I. Magnetization of bcc and fcc Fe_xCu_{100-x} metastables alloys as a function of the Fe content. Nonmagnetic phases are labeled N.M.

Magnetic moment per Fe atom (μ_B)				
Fe content	at. %	bcc	fcc	
0		N.M.	N.M.	
25		N.M.	N.M.	
50		2.10	2.18	
75		2.32	2.30	
100		2.30	2.42	



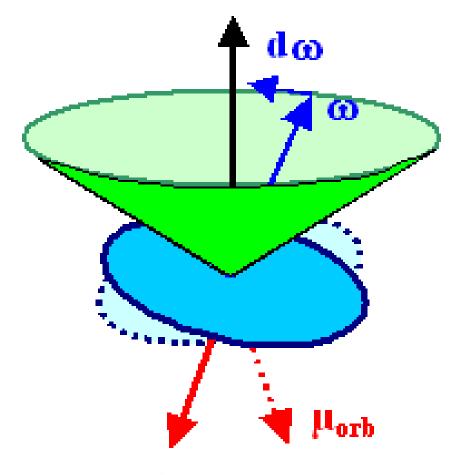


Magnetic properties of materials

Types of magnetic behaviour, diamagnetism

Features:

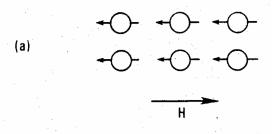
- 1) Materials with a negative magnetic susceptibility are called diamagnetics,
- 2) due to shielding currents giving a moment that opposes the applied field and is proportional to it
- 3) it is constant, negative and small (κ≅10-6)

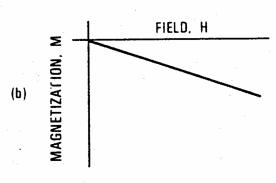


The response of an orbiting electron to a changing magnetic field is a precession of the orbit, i.e. the polar vector describing the orbit now moves in a circle around the magnetic field vector H









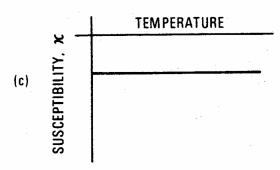
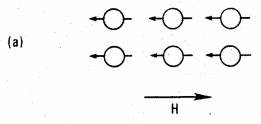
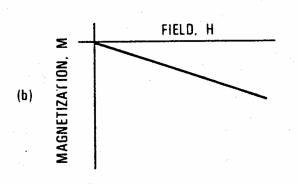


Figure 6.1 (a) Diamagnetic alignment of atomic magnetic moments. (b) Magnetization vs. field for a diamagnet. (c) Susceptibility vs. temperature for a diamagnet.

- The minus sign arises from the fact that the effect of a changing magnetic fields will be opposing the cause in accordance with Lenz's law.
- "Changing" magnetic fields, because there is no way to bring matter into a magnetic field without changing it either be switching it on or by moving the material into the field.
- Induced currents are of the type that persist even when the field is no longer changing
- Occurs in atoms and superconductors (perfect diamagnetism for certain SC, $\kappa = -1$)
- Even in a normal metal there is a diamagnetic contribution from conduction electrons







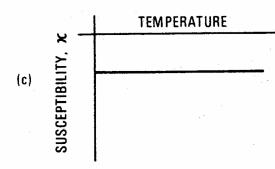


Figure 6.1 (a) Diamagnetic alignment of atomic magnetic moments. (b) Magnetization vs. field for a diamagnet. (c) Susceptibility vs. temperature for a diamagnet.

Copper representative of diamagnetic materials of technical importance

- T-dependent contributions are attributed to Fe impurities
- Most specimens show a significant decrease of their diamagnetism at low T
- Less negative susceptibility in the figure
- Contamination during the wiredrawing process?

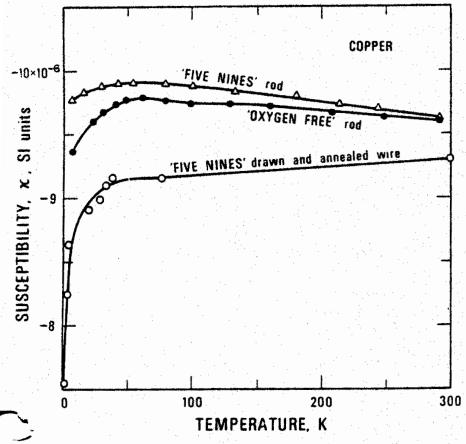


Figure 6.2 Magnetic susceptibility of diamagnetic copper as a function of temperature. △, ● — Hurd (1966); ○ — Bowers (1956).

In most applications diamagnetism not a serious concern

Susceptibility small

Important for some sensitive measurements





United States Pater

Fletcher et al.

[57]

ABS'

The present invention pro separating a gas-liquid min critical cryogenic helium v ducting magnet at low g orbit, permitting conservatended service life of the



gnets M in a experiments encountered magnetic and

f a substance

NASA

National Aeronautics and Space Administration
Goddard Space Flight Center

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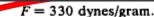




Balloon-borne Experiment with Superconducting Spectrometer

for helium χ_m Γypical values atellite coil M nagnetic body ricinity of the

"An interesting situation has been observed in orbital flights of SC magnets where diamagnetic liquid He is forced away from the high-field regions of the magnet, no doubt much to the consternation of the experimenters" (Fickett and Goldfarb, 1980)

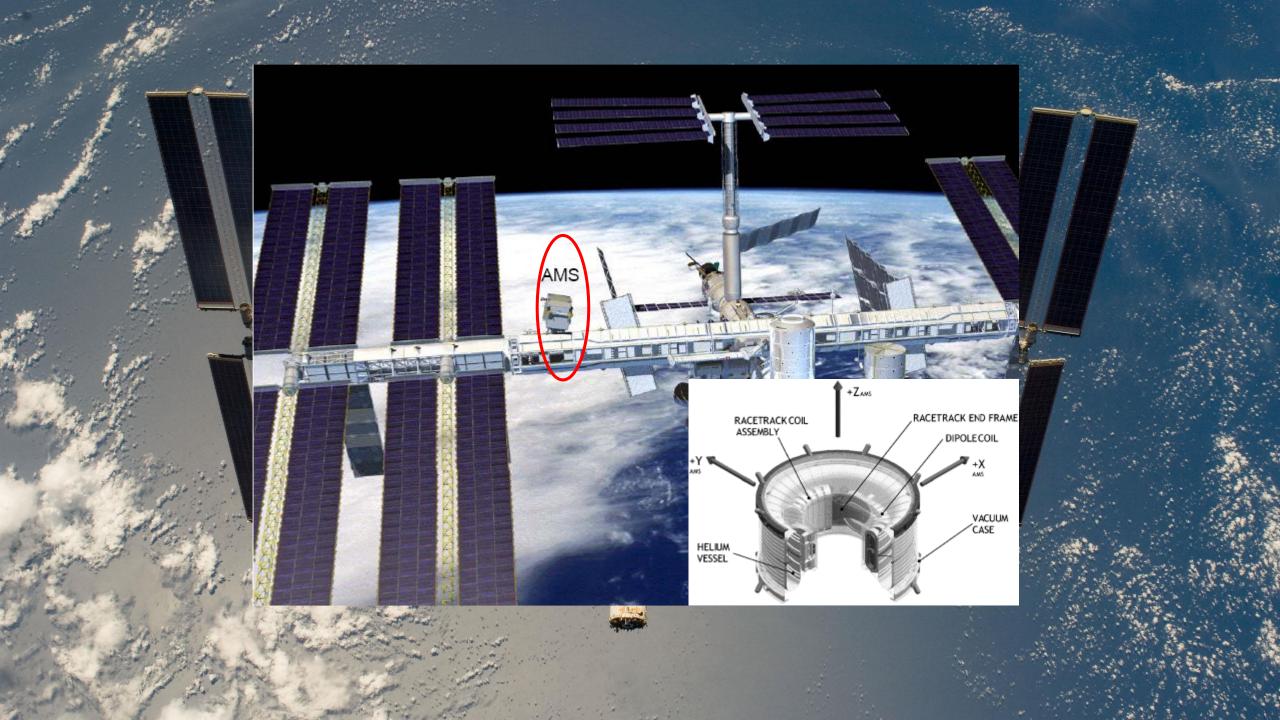


than about 100 cm.

This force corresponds to about one-third the acceleration or gravity at the earth's surface.

In normal laboratory situations a very moderate liquid helium level, for example about 1 centimeter, has sufficient head to maintain contact with the magnet. However, in an orbiting satellite the only forces acting to keep the liquid helium in contact with the coils M are surface tension and accelerations of the spacecraft. For such a coil, surface tension and diamagnetism become comparable for distances from the magnet larger





ALPHA MAGNETIC SPECTROMETER (AMS) EXPERIMENT UTILIZATION PLAN FOR EXPLORATION MAGNET DEVELOPMENT



Revision: Preliminary Draft

March 24, 2005

National Aeronautics and Space Administration

Lyndon B. Johnson Space Center Houston, Texas

The absence of gravity modifies the behavior of the superfluid helium, allowing some of the smaller influences such as diamagnetism and film flow to become significant. The response of the cryogenic system to disturbances and changes may therefore be different in space from those observed on the ground. Measurements in space could therefore yield valuable information on:

- The effect of magnetic field on diamagnetic liquid helium;





Due to unpaired electron spin moments in a material

 Atoms, molecules, lattice defects, possessing an odd number of electrons for which the total spin cannot be zero

Metals



Aligned in the direction of an applied magnetic field

Result in an increased magnetization of the material

Is generally linear with field, gives a positive susceptibility

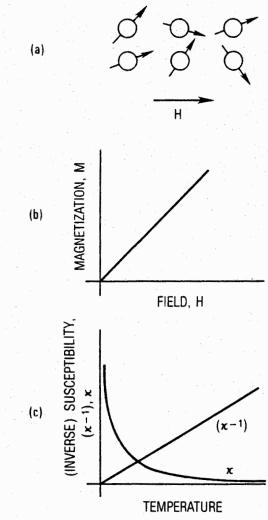


Figure 6.3 (a) Paramagnetic alignment of atomic magnetic moments. (b) Magnetization vs. field for a paramagnet. (c) Susceptibility and reciprocal susceptibility vs. temperature for a paramagnet.



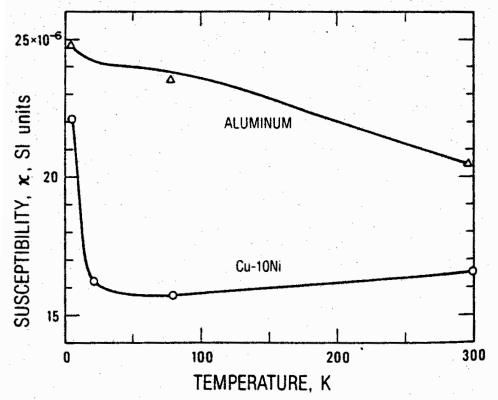


Figure 6.4 Magnetic susceptibility of relatively well-behaved paramagnetic metals. \triangle — Fickett (1976); \bigcirc — Pugh and Ryan (1958). Solid curve for aluminum representing about 30 points from graphical data of Cooper and Miljak (1976).

Different types of temperature dependences:

1) Non-ferromagnetic materials, small κ nearly T-independent, (Pauli paramagnetism due to conduction electrons)

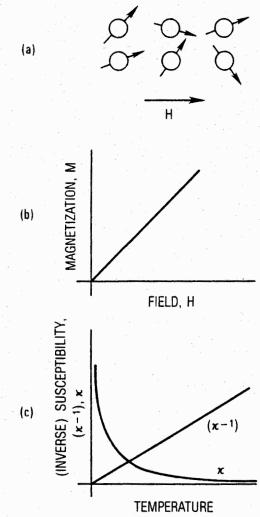
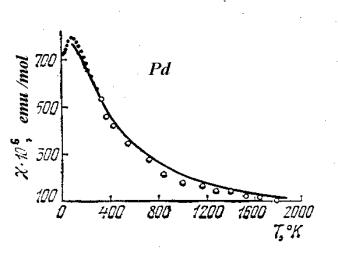
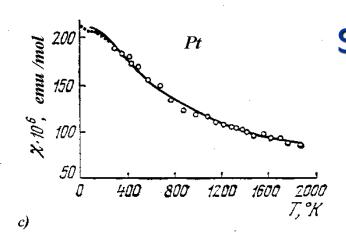


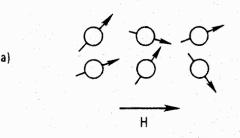
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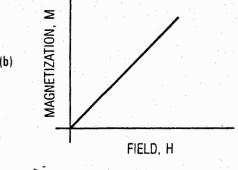
2) Transition metals (unfilled inner shells), quite large κ , increases generally with decreasing T (Pd, Pt, see V.Y. Irkhin and Y.P. Irkhin)





SI reported values
of κ ≅ 7.2·10⁻⁴
at RT and κ ≅
12·10⁻⁴ for Pd
(Nagasawa,
1970)





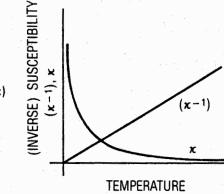
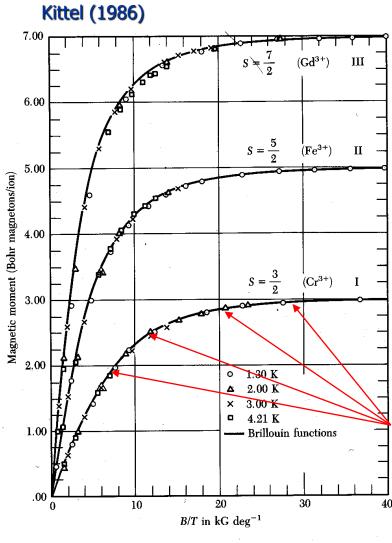


Figure 6.3 (a) Paramagnetic alignment of atomic magnetic moments. (b) Magnetization vs. field for a paramagnet. (c) Susceptibility and reciprocal susceptibility vs. temperature for a paramagnet.





3) Some metal ions, $\kappa = C/T$, strongly T-dependent, C is a constant determined by the ionic density

At low temperatures and high fields magnetization may approach saturation, thus κ becomes field dependent

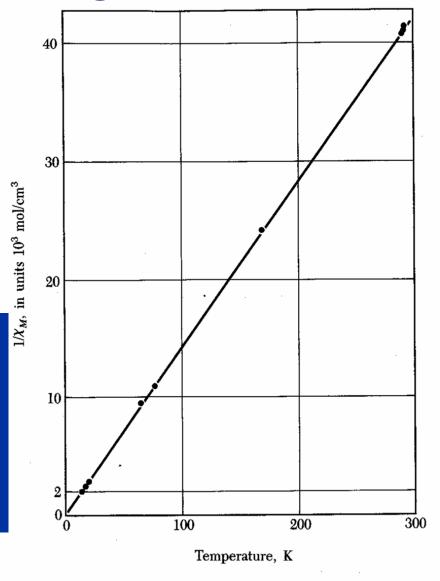


Figure 4 Plot of magnetic moment versus B/T for spherical samples of (I) potassium chromium alum, (II) ferric ammonium alum, and (III) gadolinium sulfate octahydrate. Over 99.5% magnetic saturation is achieved at 1.3 K and about 50,000 gauss. (After W. E. Henry.)

Plot of $1/\chi$ vs T for a gadolinium salt, $Gd(C_2H_5SO_4)_3 \cdot 9H_2O$. The straight line is the (After L. C. Jackson and H. Kamerlingh Onnes.)

- Same « Langevin type » paramagnetism for ferromagnetic and antiferromagnetic materials above a critical temperature
- This temperature is the one above which their spontaneous magnetization breaks down
- This behaviour is expressed by the Curie-Weiss law, κ = C/(T-θ)
 (examples follow)





Magnetic properties of materials,

ferromagnetism

454

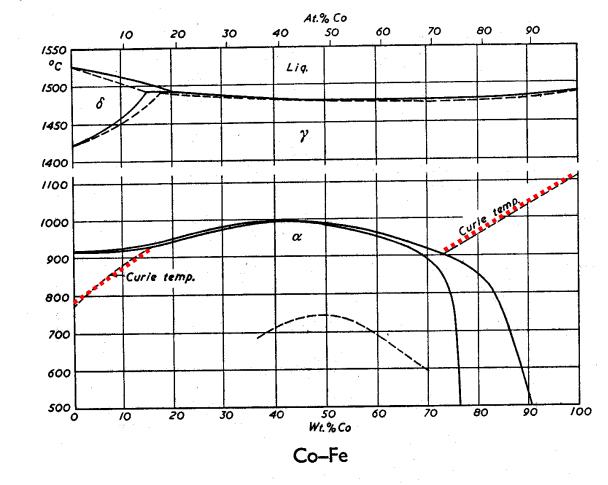
Equilibrium Diagrams

Interaction of atomic spin moments with each other

Occurs in certain instances

To produce:

- Ferromagnetism
- Antiferromagnetism
- Ferrimagnetism



Smithells Metals Ref. Books, 1967



atomic magnetic moments. (b) Magnetization vs. temperature showing saturation magnetization, M_s . (c) Saturation magnetization vs. temperature below the Curie temperature, T_C . (d) Susceptibility and reciprocal susceptibility vs. temperature above the Curie temperature, T_C , showing ferromagnetic (F) and paramagnetic (P) intervals.

Figure 6.5 (a) Perromagnetic alignment of

FIELD, H

TEMPERATURE

TEMPERATURE

MAGNETIZATION, M

SATURATION (GNETIZATION)

(INVERSE) SUSCEPTIBILITY,

(b)

Particular care with Ni-basis superalloys for non-magnetic application at very low T!

Incoloy 800 32.5Ni-21Cr-46Fe

Commercial Names

Trade name. Incoloy 800 UNS number. N08800

Magnetic Properties

Magnetic permeability. Annealed material, 1.0092 at a field strength of 15.9 kA/m

Curie temperature. -115°C (-175°F)

From ASM Handbook



- Large field dependent permeability
- Magnetisation often persists after application and removal of a magnetic field
 - T_C Fe = 1043 K
 - $T_c Ni = 631 K$
 - $T_C Co = 1394 K$
- Ferrous alloys of high interest for magnet applications



Features (Bozorth, 1951)

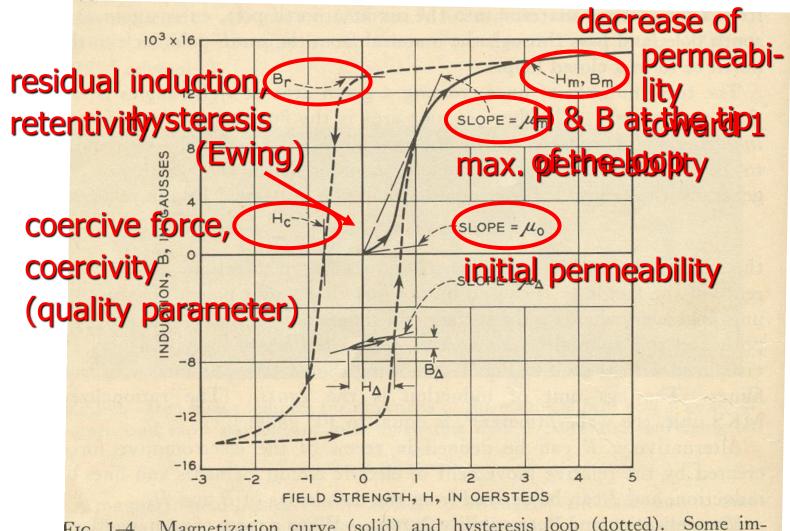
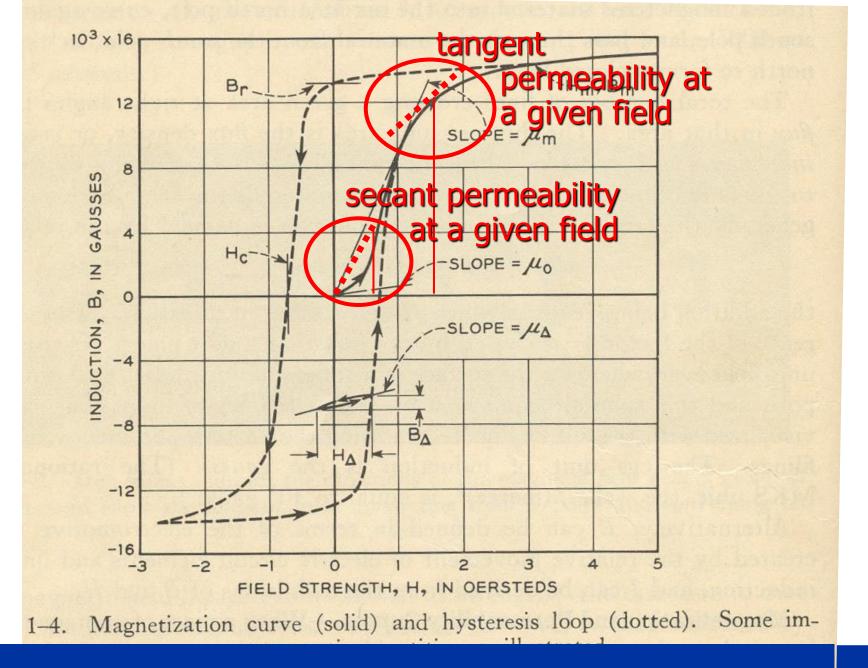


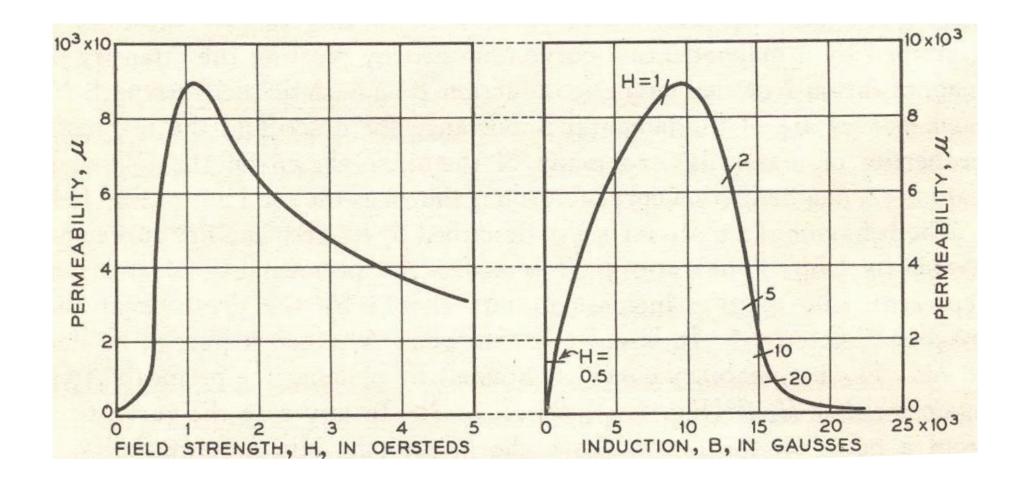
Fig. 1-4. Magnetization curve (solid) and hysteresis loop (dotted). Some important magnetic quantities are illustrated.











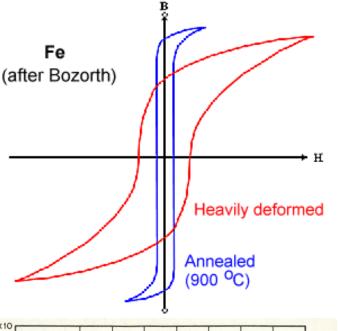




- T_c and saturation magnetization are insensitive to material structure
- All other properties are significantly affected by the physical and metallurgical state of the material: cold working, subsequent annealing...
- Anisotropy effects (texture) can occur (rolled steel)



Magnetic properties of materials, irons and steels



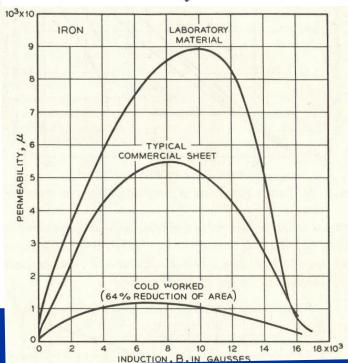
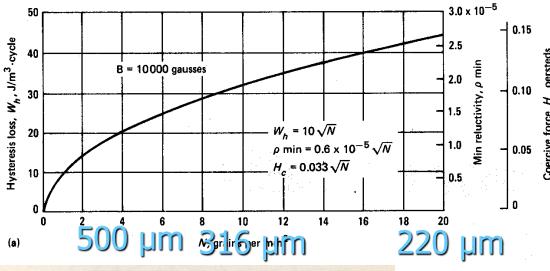


Fig. 2 Effect of grain size on magnetic properties of pure iron and silicon iron



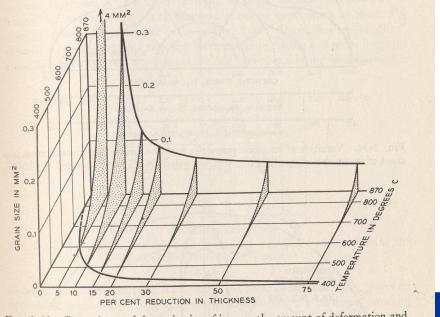


Fig. 2-33. Dependence of the grain size of iron on the amount of deformation and on the temperature of anneal.



Magnetic properties of materials, irons and steels

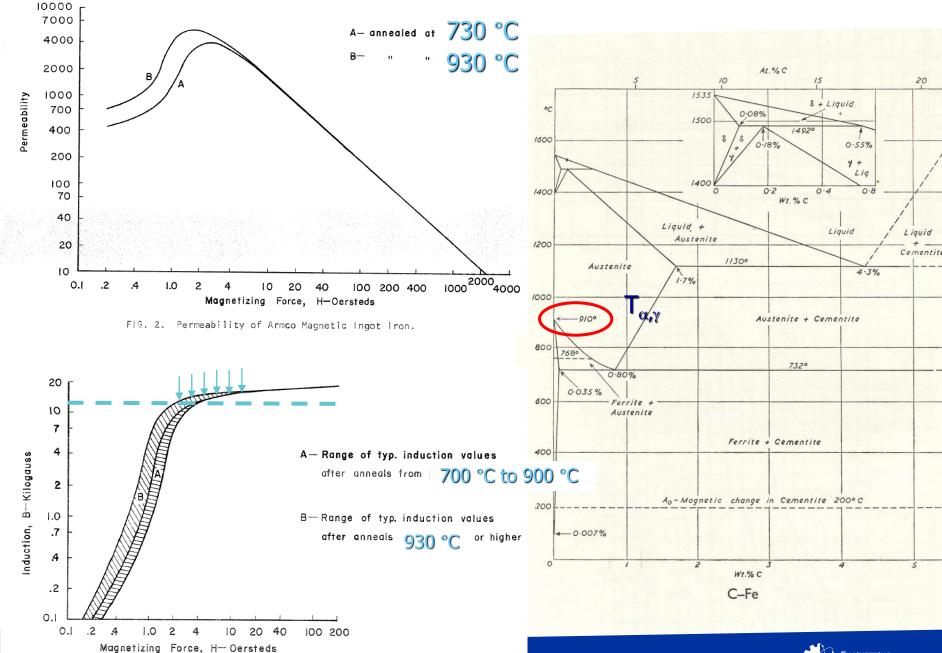


FIG. 3. Typical medium and low induction values for annealed Armco Magnetic Ingot Iron.

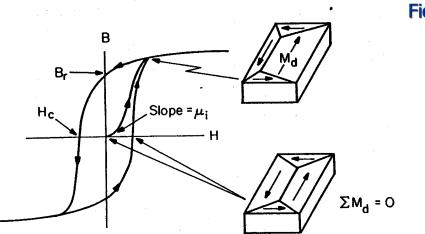


Soft ferromagnets

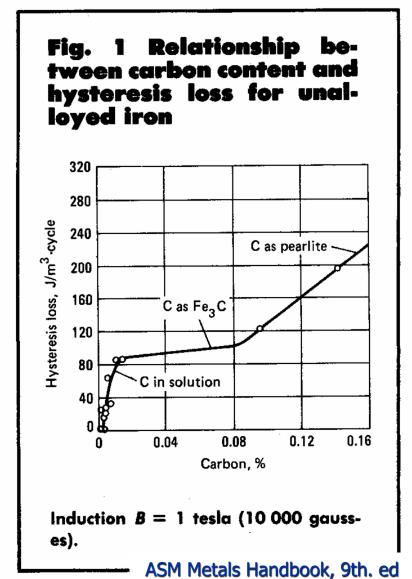
- Easily magnetised and demagnetised (transformer cores, ferrite cores, shielding of magnetic fields)
- Usually metals
- Narrow hysteresis loops (low values of H_c)
- High permeabilities
- Low eddy-current loss from electric currents induced by flux changes
- High magnetic saturation inductions



- C, S, N, O are deleterious to fm properties
- They distort the lattice and even in small amounts (ppm) may greatly interfere with easy movements of magnetic domains
- C in excess of 30 ppm in pure Fe cause excess solute to precipitate in GB



Fiorillo, 2007



Comparison of the Thermal Conductivity, Electrical Resistivity, and Seebeck Coefficient of a High-Purity Iron and an Armco Iron to 1000°C*

W. FULKERSON, J. P. MOORE, AND D. L. McELROY

Metals and Ceramics Division, Oak Ridge National Laboratory, Oak Ridge, Tennessee

(Received 6 December 1965)

Iron referred to as "high purity" when total concentration of impurities (mainly C, N, O, P, S, Si and Al) does not exceed a few hundred ppm

Otherwise Low Carbon Steel or Non-alloyed Steel

Very pure Fe \Rightarrow high electrical conductivity \Rightarrow unsuitable for AC applications

Table I. Chemical analysis of high-purity iron, ORNL Armco iron, and BMI Armco iron.

	Concentration (at.%) $\times 10^3$		
		ORNL	BMI
	High-purity	Armco	Armco
Element	iron	iron	iron
Al Ca	0.21-2.1 0.14-1.4	<105	< 0.4
Cr		< 54	< 0.9
Ču	0.09-0.9	90	0.09 - 0.9
Mn		51	1-10
Mo		< 29	<6
Ni	0.95-9.5	95	1-10
Si	2.0 - 20	<40	0.2 - 2
Ti		<12	<1.1
V C P S		<22	<1.1
С	14	61	75
P	2.0	11	16
	5.2	40	51
${ m H}_2$	< 5.6	< 5.6	95
O_2	8.8	304	210
N_2	2.0	20	328
Totals:			
Minimum including oxygen	40.99	672	777
Minimum without oxygen	32.19	368	567
Maximum including oxygen	71.50	940	807
Maximum without oxygen	62.7	636	597



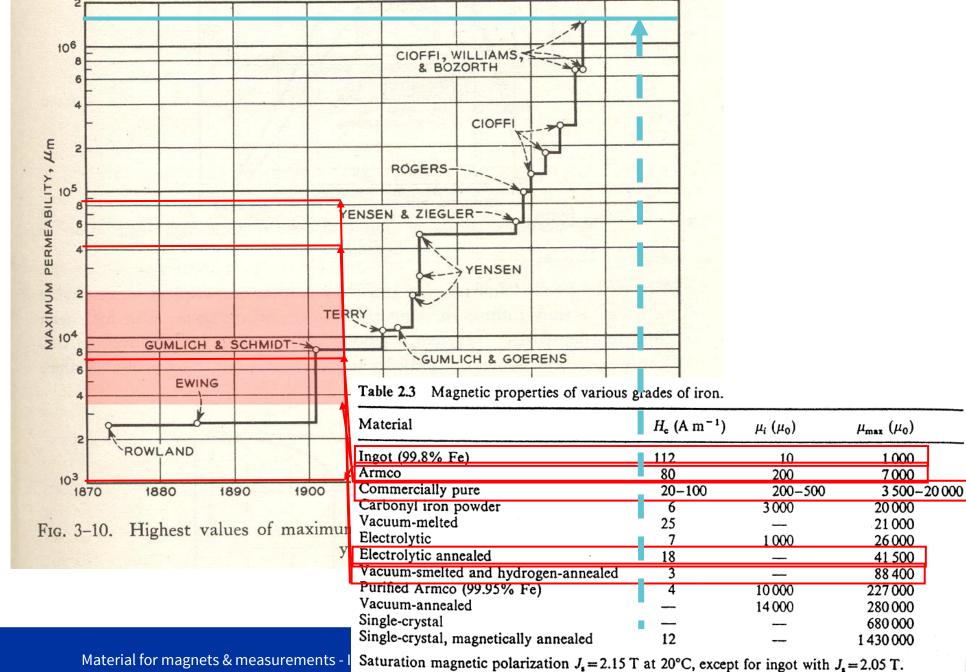
^a Al, Ca, Cr, Cu, Mn, Mo, Ni, Si, Ti, V analyzed by emission spectroscopy (semiquantitative); C, P, S, H₂, O₂, N₂ analyzed by quantitative analysis.

High-purity iron Armco iron Temperature ORNLb ORNL° NPL^d NRC^e ORNL^f USS# (°C) -2691.02(5.0)h 0.96(6.8)h $0.40(6.1)^{h}$ 1.47(11) 5.95(11) -195.71.74(14)1.01(17) 6 19(9) 5.31(10) -79 1 9.64 10.0 10.4 9.04 8.63 9.97 0 50 12.7212.3012.5 11.37 11.7215.45 15.6 15.6 100 15.81 14.70 14.46 150 19.21 18.85 19.1 17.86 18.06 23.00 22.65 23.1 23.0 21.84 21.60 200 26.95 27.1 250 27.29 26.10 25.85 32.1 30.55 300 32.05 31.71 30.72 350 37.15 36.81 36.5 35.90 35.55 42.51 42.0 43.1 41.51 41.13 400 42.84 49.04 450 500 55.63 62.88 550 600 70.66 78.95 650 88.02 700 98.64 750 800 107.61 850 111,74 900 114.69 115.19 910 920 114,96 116.15 950 1000 117.95 11.0 $\rho_{300}/\rho_{4.2}$ a In each column, the first entry b Armco iron specimen machine Armco iron specimen machine annealed state of the iron. d Values were calculated from da Values were calculated from da ORNL high-purity iron specin Values calculated from data re communication with Dr. Arajs. h Numbers in parentheses after <-- 0.01 IN.→ ←-0.01 IN.->

Table IV. Smoothed values of the resistivity $(\mu\Omega \cdot cm)$ of Armco irons and high-purity irons as reported by several sources.



Fig. 1. Microstructure of (a) ORNL Armco iron, (b) ORNL high-purity iron, and (c) BMI Armco iron. (×200). The ORNL Armco iron and BMI Armco iron specimens were etched with a solution of 2% nitric acid in ethyl alcohol. The high-purity iron was first electrolytically polished and then etched with a solution consisting of 3.2% picric acid and 0.4% nitric acid in ethyl alcohol.





Low C steels

TABLE 2.2 Typical impurities and their concentrations (wt ppm) in several grades of iron and in low-carbon steel

Iron type	C .	N	0	Mn	P	S	Si	Cu	Ni
ARMCO	150	20	150	280	50	250	30	150	
Electrolytic	40	100	100	15	20	30	30	40	10
H ₂ treated	30	10	30	280	40	<30	•		
Zone refined	7	< 10	2	0.5	< 0.1	0.2		1.5	0.50
Low-carbon steel	50-1000	30-200	20-100	5×10^3	200-1000	50300	10 ³ -10 ⁴	100	

F. Fiorillo, Measurement and Characterization of Magnetic Materials, Elsevier-Academic Press, Amsterdam (2004)

Low-Carbon Steels

For many applications that require less than superior magnetic properties, low-carbon steels (type 1010, for example) are used. Frequently, higher-thannormal phosphorus and manganese contents are used to increase electrical resistivity. Such steels are not purchased to magnetic specifications.

ASM Metals Handbook Ninth Edition, Vol. 3



Table 11 Direct-current magnetic properties of relay steels and alloys after annealing

Metal	Magnetizing force, H _{max} from B = 10 000	H _c , coercive force(a), oersteds	B_r , kilogausses from B = 10 000	Perme Initial	eability, µ Maximum	Flux density at max per- meability, kilogausses	Saturation induction, kilogausses	Resis- tivity, μΩ·cm
Low-carbon i	ron and steel	Marie Land						
Low-carbon iron	. 2.0 to 5.8	0.80 to 1.70	7.0 to 8.5	200(b) 500 to 1000(c)	2 200 to 5 500	6.4 to 7.5	21.5	10
1010 steel	. 3.0	1.00 to 2.00	8.4	200(b)	. 3- 800 %	7.5	21.0	12

U.S	S.A.						U.S.A	14					U.S.A.
Baustähle			issofose	18	Aciers	de con	structi	on	Structu	ral and	al and constructional steels		
NE O		Norm	Unified Numbering	Analyse		92\	dadA A	Analys	se	× -		Composition	WNr. No.
No.	sM Mil	ndard	System	С	Si	Mn	Par	Sale	Cr	Мо	Ni	Sonstige Autres – Otl	
	SAE	AISI	UNS	%	%	%	≤ %	≤ %	%	%	%	%	- Type
3330	1005	1005	I.à.c. et usin	é à froid, fil	, tubes								geage, barres
3	1005 1006	1000		rolled and		nished bars	s, wire ro	ds, seam	less tul	oplicable on bing	ly for sen	<u>iifinished pr</u> od	AUBUDS "'DEE
4		1006	G10050 G10060	t rolled and ≤ 0,06 ≤ 0,08	cold fi a; b a; b	nished bars ≤ 0,35 0,25–0,40	0,030	ds. seam 0,050	less tut	oplicable on bing 	ly <u>fo</u> r <u>se</u> n _	<u>nifinished pr</u> od _ _	1.0314
_	1008		G10050	≤ 0,06	a; b	n <u>is</u> hed bars ≤ 0,35	s, wire ro	ds, seam	less tub	oplicabl <u>e on</u> bing - -	ly <u>fo</u> r <u>se</u> n - -	nifinished prod - - -	AUBUDS "'DEE
5		1006	G10050 G10060	≤ 0,06 ≤ 0,08	a; b a; b	nished bars ≤ 0,35 0,25–0,40	0,030 0,030 0,030	0,050 0,050 0,050	less tub	oblicable on bing _ _ _ _	ly <u>fo</u> r <u>se</u> n - - -	28,0-81,0 28,0-87, <u>0</u> 28,0-08, <u>0</u> 28,0-08,0	1.0314 1.0313
5 7	1008	1006 1008	G10050 G10060 G10080	≤ 0,06 ≤ 0,08 ≤ 0,10	a; b a; b a; b	nished bars ≤ 0,35 0,25-0,40 0,30-0,50	0,030 0,030 0,030 0,030	0,050 0,050 0,050 0,050	less tub	oblicable on bing	ly for sen	28.0-80 <u>-</u> 28.0-80 <u>-</u> 28.0-80 <u>-</u> 28.0-80 <u>-</u> 1.112	1.0314 1.0313 1.0204/1.0330/1.0318/ 1.0211/1.0212







CLIC Main Beam Quadrupole (V4, T.Zickler)

Aperture radius: 5.00 mm

Integrated gradient: 70 (170, 270, 370) Tm/m

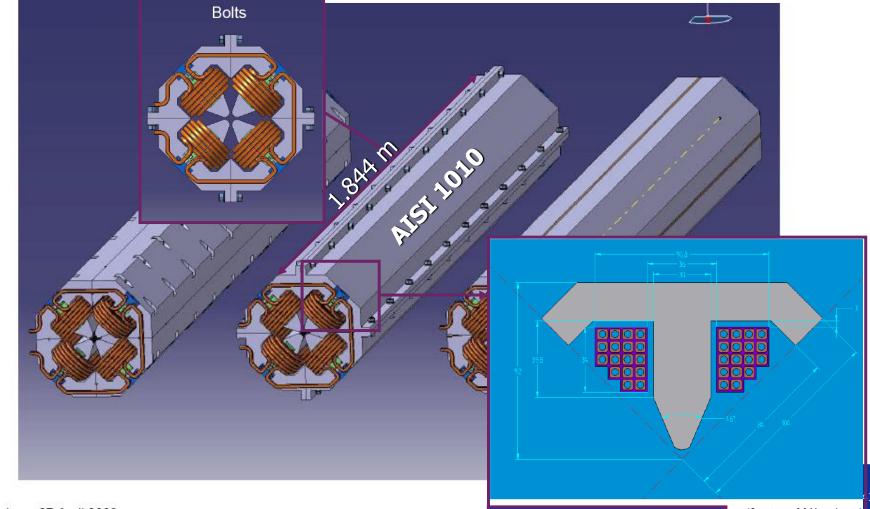
Nominal gradient: 200.1 T/m

Iron length: 344 (1844) mm

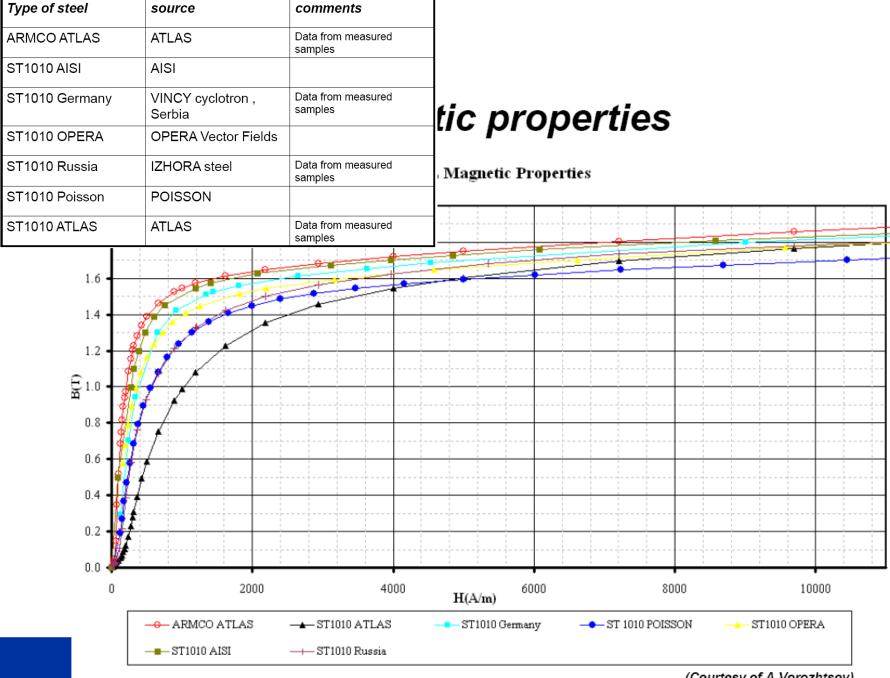
Magnetic length: 349 (1849) mm

Total length: 414.7 (1914.7) mm Magnet width: 192 mm Magnet height: 192 mm

Magnet weight: 109.3 (393.3) kg









Magnetic ageing

Group Code.: EDMS No.:

SL-MS 115684

SL Division Project

$\Delta P(t_{\rm g}) / P(0)$ 10⁵ 10⁴ 10⁶ 10⁷ 10⁸ **FIGURE 2.5** Relative increase of power losses ($f = 50 \,\mathrm{Hz}$, $J_p = 1.5 \,\mathrm{T}$) in a lov carbon steel lamination (Si = 0.3 wt%) after aging at 150 °C up to 600 days [2.17 Different curves refer to different C concentrations, ranging between 156 an 21 ppm.

156 ppm

57 ppm

45 ppm

Technical Specification of the Low Carbon Steel for the

Fiorillo, 2004

0.6

0.5

0.4

0.3

Low-carbon steel

T=150°C

3.1.1.3 Ageing

The steel supply shall be entirely stable with respect to time in both coercivity and permeability. Since the operating temperature of the magnet cores is expected to vary in the range 27 °C - 45 °C, the stability of the magnetic properties refers to many years of operation in this temperature range. The ageing properties of the steel sheets will be evaluated by re-measuring the coercivity after 100 hours of accelerated ageing at 150 °C on samples taken throughout the whole production. The coercivity values of the aged samples shall not exceed those measured before the treatment by more than 10%. The accelerated ageing and the subsequent measurements are to be carried out by the steel producer at least twice for every melt.

MBG and QTG Magnets of the CNGS Project



... by final purification under pure hydrogen:

Fe + C +
$$2H_2$$
 = Fe + CH_4
Oxygen, Sulfur, Nitrogen \Rightarrow H_2O , H_2S , NH_3

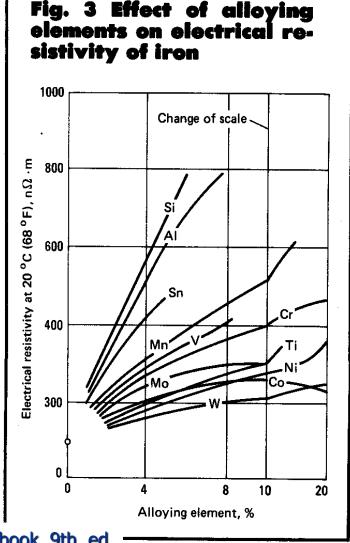
TABLE 5

Maximum permeability of Armco iron with different degrees of purification, effected by heat treatment in pure hydrogen at 1475°C for the times indicated (P. P. Cioffi). Analyses from R. F. Mehl (private communication).

Time of Treatment	4	Composition (%)							
(hours)	μ_m	С	S	0	N	Mn	P		
0	7 000	0.012	0.018	0.030	0.0018	0.030	0.004		
1	16 000	.005	.010	.003	.0004				
3	30 000	.005	.006	.003	.0003				
7	70 000	.003		.003	.0001				
18	227 000	.005	< .003	.003	.0001	.028	.004		
Precision of analysis:		.001	.002	.002	.0001				



- Pure Fe very soft but requires special handling
- Used extensively in dc applications
- Low electrical resistivity makes unsuitable for ac circuits
 - ⇒ FeSi alloys
- Grain growth can be promoted
- Saturation induction reduced by all alloying elements except Co



ASM Metals Handbook, 9th. ed



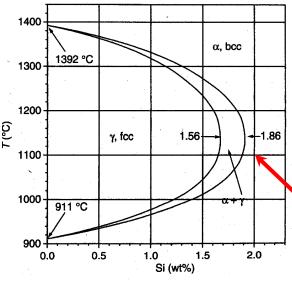
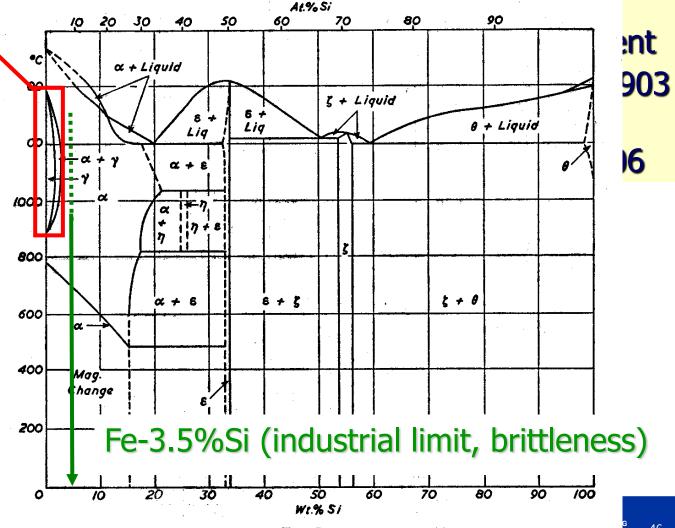


FIGURE 2.7 Fe-Si phase diagram: the γ loop.

Fe-Si alloys accidentally discovered by Hadfield (1882), 1.5 % Si

Magnetic properties reported in 1900



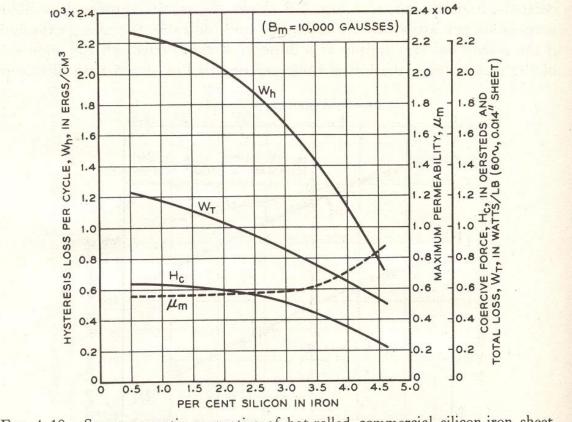


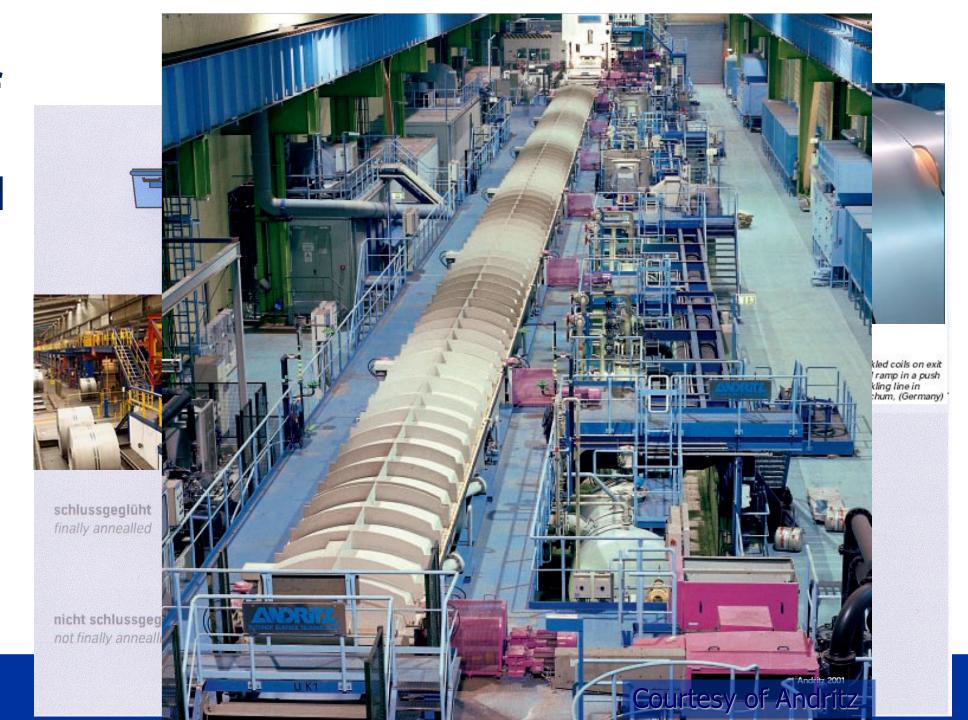
Fig. 4-10. Some magnetic properties of hot-rolled commercial silicon-iron sheet. Some of the change with composition is due to the higher annealing temperature of the material having higher silicon contents.

Advantages:

- Increase in permeability
- Decrease in hysteresis loss
- Eddy current loss decrease due to higher resistivity (Al and Mn added as well)
- No ageing (due to AI \Rightarrow AIN)





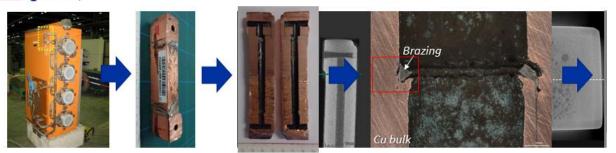




Magnetic properties of materia steels

Analysed samples & method

All the conducts under study correspond to Cu based sections mostly brazed with Sil-Fos (**self**-with Ag and P)



Analysed samples

No-leaking samples extracted from different PSB locations

Quadrupoles/ Dipoles/ Bending Magnets

After different service time

From 2 weeks to 50 years

Common cooling circuit of demineralized water

Equivalent for all accelerators circuits

Samples examina

Type of

Non-destructive test by comp Selection of the cutting planes Dry cutting to access the inr Inspection and chemical an Metallurgical preparation (poli Examination of the brazec

Common effort from TE-MSC, HSE-RP, EN-CV, EN-MME and TE-VSC to ensure the appropriate proc



2023-06-14

Subtask-2: Analysis and understanding of the failure modes - A.T. Perez, S. Sgobba - EN-MME-MM

PS Booster magnets Task Force day, 14/06/2023



A. Bartkowska & S. Sgobba



21.08.2023

Technical Sheet EDMS N°: 2930603

Technical sheet for the supply of cold rolled non-oriented fully processed electrical steel sheets or strip for the PSB quadrupole magnets

REQUIREMENTS							
Normative references	EN 10106, EN 10251, IEC 60404-2, EN 10342, EN 10204						
Steel grade and dimensions	M700-100A (1.0894) accordingly to EN 10106 • 1±0.02 mm × 1670 mm × 600 mm (final exact dimensions will be reconfirmed by the blanking company) • Minimum stacking factor (0.98) and other geometric and technological properties, tolerances and inspection procedures as per EN 10106						
Manufacturing process	Cold rolled and delivered in sheets (strip may be an option). The steel shall be delivered fully processed. Material shall be supplied with trimmed edges.						
Structure and composition	Non-oriented. Indicative composition 2.3 % Si, 0.2% Mn, specification on magnetic properties prevails on composition.						
Magnetic properties	Coercive force: target value $H_c = 35 \pm 3.5$ A/m, for cycles up to 1.5 T. Relative permeability μ_r :						
	are allowed. The properties specified by EN 10100 should also be respected.						

magnet	Composition	Total sales
Hard	Ferrite 56%, Sm-Co 10%, Nd-Fe-B 26%, Alnico, etc. 8%	\$5 billion
Semihard	Particulate media 65%, thin films 35%	\$15 billion
Soft	Electrical steels 86%, ferrites 12%, amorphous 2%	\$8 billion

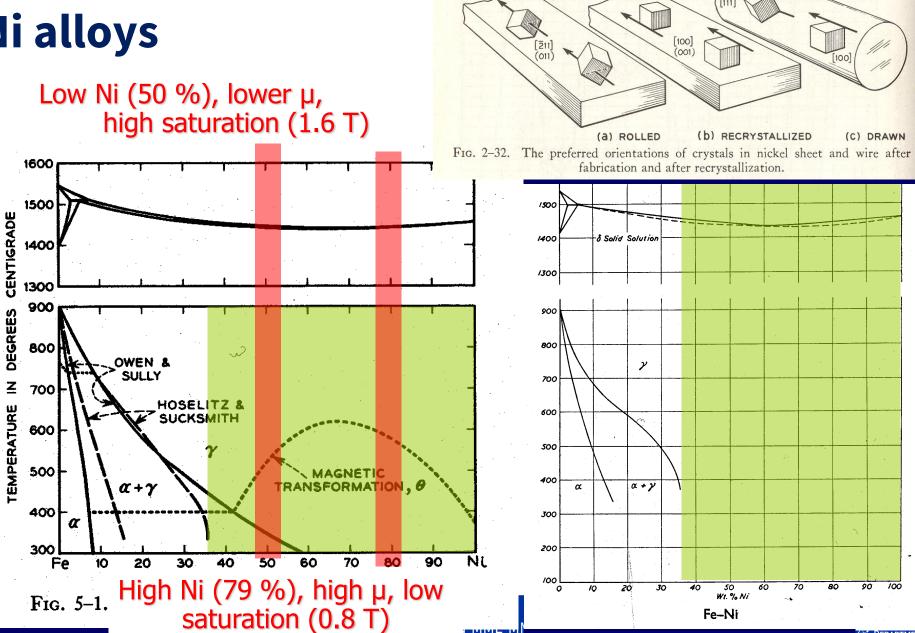
Table 1. Estimate of the world market for magnetic materials in 1997.

256 t of electrical steel

roviding surface insulation resistance,

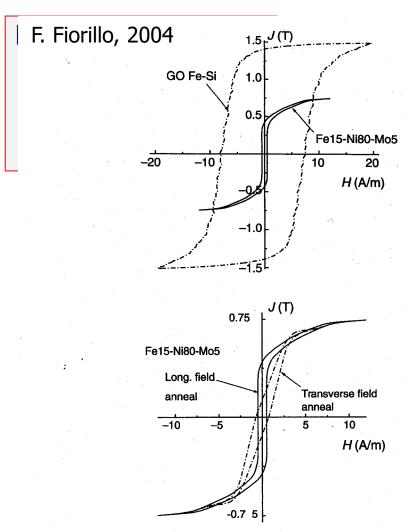
y. Coating should be according to the

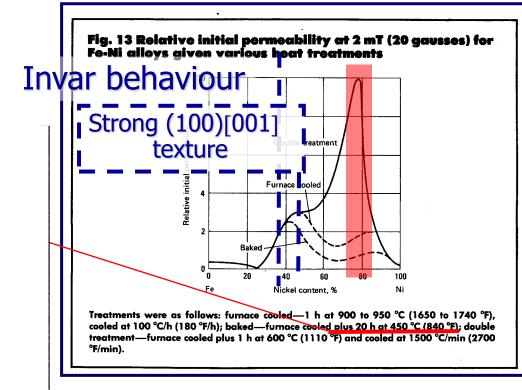






From Bozorth, Ferromagnetism, 1951









CERN

CH-1211 Geneva 23 Switzerland



LHC Project Document No.

LHC-VCRS-ES-0001 rev 1.0

CERN Div./Group or Supplier/Contractor Document No.

AT/VAC

EDMS Document No.

405734

Date: 2004-05-12

Functional specification

VACUUM CHAMBERS FOR THE CIRCULATING BEAMS IN THE LHC INJECTION AND EXTRACTION SEPTA





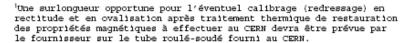


Groupe Logistique
Section Standardisation

A.J. Mager, Magnetic Shields, IEEE Trans. on Magnetics, 6 (1970) 67

N° de codification CERN	SCEM: 39.74.60.059.9
Désignation	TUBE EN MUMETAL® 77 Ni-5Cu-4Mo-Fe POUI CHAMBRES SPECIALES LSS

(CARACTERISTIQUES
Matière	Mumetal® 77Ni-5Cu-4Mo-Fe
Dimensions et tolérances	Diamètre ext. = 59.80 mm ± 0.15 mm, diamètre in
Dimensions et tolerances	58 mm, épaisseur = 0.90 mm ± 0.09 mm, ovalisati
	0.4 mm, tolérance sur diamètre moyen = ± 0.2 mn
	tolérance sur rectitude ≤ 1 mm sur 2.5 m.
	Longueur 5100 mm -0/+10 mm¹.
Quantités	La quantité minimale à produire est de 69 longs de 5100 mm avec une tolérance -0+10%.
Documents applicables	Soudure : EN 288-3, EN 1435, ISO 5817 Niveau B
Documents applicables	(qualité à garantir en qualification et fabrication).
	Matière de base : IEC 404.4, EN 10204.
Etat de livraison	Les tubes seront livrés à l'état roulé-soudé ce
	nécessitera un traitement thermique de restaur ${f F}$
	des propriétés magnétiques à effectuer au Cl
	Dans le cas de perte des tolérances dimensions
	due au traitement thermique, notamment
	ovalisation et flèche, un calibrage (redressage)
	effectué par le fournisseur. Absence d'oxydation sur le cordon fondu.
Caractéristiques indicatives de la	Etat de la matière de base : adouci.
matière de base à l'état roulé-	Perméabilité initiale ≡ 1000, maximale ≡ 10000, champ
soudé, avant traitement thermique	à saturation ≤ 0.77 T.
final	a saturation ≘ 0.77 1.
Contrôles	100 % visuel, dimensionnel et RX (ce dernier sur
	soudure). Acceptation : dimensionnel selon cette fiche
	technique, RX et visuel selon EN 288-3 (ainsi
	qu'EN 1435 pour RX) et ISO 5817 Niveau B.
	Une coupe macro-micro d'échantillon suiveur par
	jour de production sera effectuée (acceptation selon EN 288-3 et ISO 5817 Niveau B).
Caractéristiques garanties après	Perméabilité initiale ≥ 60000, maximale ≥ 120000,
traitement thermique de	champ à saturation ≥ 0.77 T.
a and a second decade	I



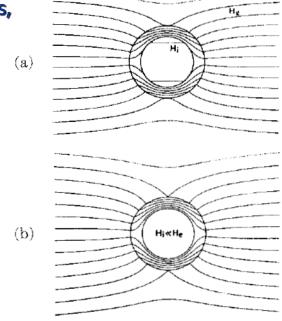


Fig. 1. Calculated field distribution for cylinders with ratio of inner to outer diameter of $D_i/D_o = 0.7$ in field transverse to axis; H_e , external field, H_i , field in the interior of the shield. (a) For a permeability of $\mu = 20$. (b) For a very high permeability.

$$S_T = \frac{1}{4}\mu(1 - D_i^2/D_o^2) + 1 = (\mu d/D_o)(D_m/D_o) + 1,$$

cylindrical shell (transverse field).

⇒Inforce field lines of an external perturbing field H_{ext} through the magnetic material

⇒Weakens the H_{int} field



Report n. 98/10/06

Att. 4, page 1 of 1

Testing of magnetic properties and relative results

Graph, Table: , Summary of the evolution of the measured magnetic properties on the

Mumetal rings.

Material: Mumetal

Samples ID: ring 1, ring 2

Density: 8.6

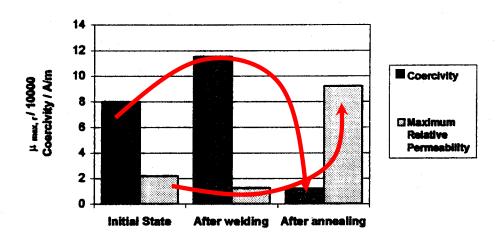
Weight before welding: ring (1&2) - 28.98 g

Weight after welding: ring 1 - 14.47 g

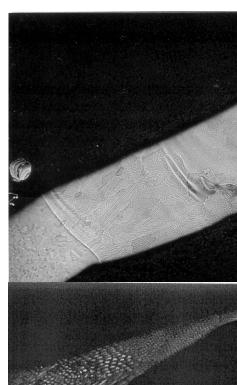
ring 2 - 14.42 g

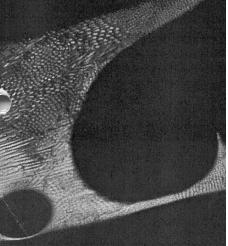
90 turns used for excitation Permeameter:

180 turns used for detection



Note: The properties of the initial state were measured on the two rings coupled. After the TIG welding, they were measured on both rings together and on each one separately. Since the measured values of the magnetic properties were reproducible between ring 1 and ring 2, further operations and measurements were performed only on one ring (ring 1).







Magnetic properties of materials, Fe-Ni vs. Fe-Co

Table 7 Typical magnetic properties for various Fe-Ni and Fe-Co alloys

	Material	Nominal composition(a)	Typical anneal(b)	Perme At B=20	ability Max	Saturation induction, gausses	Coercivity, H_c , oersteds	Retentivity, B_r , gausses
	45 Permalloy	. 45Ni	1920 °F	2 500	30 000	16 000	0.20	8000
			(H ₂ ,)2150 °F	4 000	50 000	16 000	0.06	8000
	4750 alloy		H ₂ , 2050 °F	4 000	50 000	16 000	0.07	8000
	Carpenter 49 alloy	. 47-50Ni	H ₂ , 2050 °F	4 000	50 000	16 000	0.07	8000
	Conpernik	. 50Ni	• • •	1 500	2 000	16 000		
	Orthonol		H ₂ , 1825 °F	•	60 000	15 600	0.20	14500
L	78 Permalloy		1920 °F	8 000	100 000	10 700	0.05	6000
	4-79 Moly Permalloy		2000 °F, Q	20 000	100 000	8 700	0.03	5000
	Hymu 80	79Ni, 4Mo	2000 °F, Q	20 000	10000	700	0.05	5000
	Supermalloy	79Ni, 5Mo	(H ₂ ,)2375 °F, Q	Up to	1300	200	- 0.00c	E000
Г	Mumetal	77Ni, 5Cu,	2050 °F	20,000	100 000	500	Tc = 98	30°C
		2.75Cr						
Г	Permendur	50Co	1470 °F	800	5 000	24 500	2.00	14000
_	ATT TO							- 1000

1470 °F 8 000 800 24 000 Hiperco 2.7..... 37Co, 0.6Cr 650 10 000 24 200 60 000 24 000 2-81 Moly Permalloy powder 81Ni, 2Mo 1200 °F 125 130 Carbonyl iron powder 60 150

(a) Remainder iron plus deoxidizer. (b) H2, annealed in hydrogen; Q, quenched or controlled cooled. (c) Grain oriented.



14000

On-board high speed

aircraftes

generators for

spacecrafts and

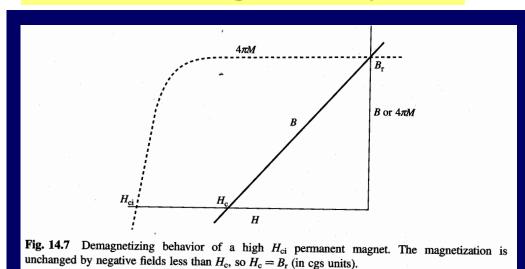
Volume reduction

Magnetic properties of materials, pern

Rare earths (hard magnetic)

Permanent magnet materials:

→ Materials of high coercivity



"Ideal" return curve of a permanent magnet (Cullity and Graham, ibid)

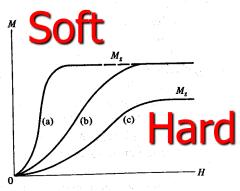


Fig. 1.14 Magnetization curves of different materials.

B.D. Cullity, C.D. Graham, Introduction to Magnetic Materials, 2nd ed., Wiley (2009)

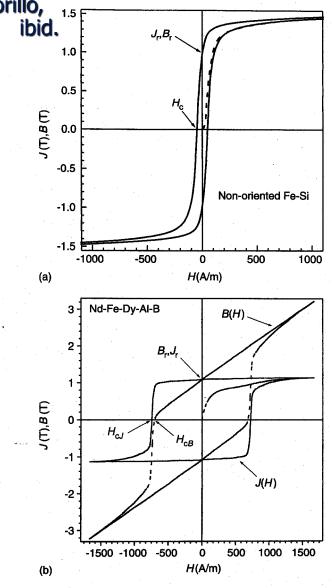


FIGURE 1.7 Examples of hysteresis loops in soft and hard magnets. In the soft Fe–Si laminations, there is no detectable difference between the B(H) and J(H) curves for magnetizations and fields of technical interest. The difference is instead apparent in permanent magnets. It leads to two different definitions of coercive field: H_{cB} is the field required to bring the induction to zero value starting from the saturated state and H_{cJ} is required to reduce to zero the polarization J (i.e. magnetization M). It is always $H_{cJ} > H_{cB}$ (courtesy of E. Patroi).



Magnetic properties of materials, permanent magnets

F. Fiorillo, Characterization and Measurement of Magnetic Materials, Elsevier, 2004

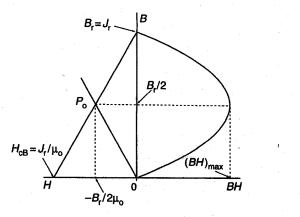


FIGURE 3.3 Return curve and energy product in an ideal permanent magnet. If the material is brought to the saturated state $(J_r = J_s)$, the maximum theoretical energy product $(BH)_{\rm max} = J_s^2/4\mu_0$ is attained at the working point P_0 .

(BH)max parameter of merit

→ attained at Br/2





Magnetic properties of materials, permanent magnets

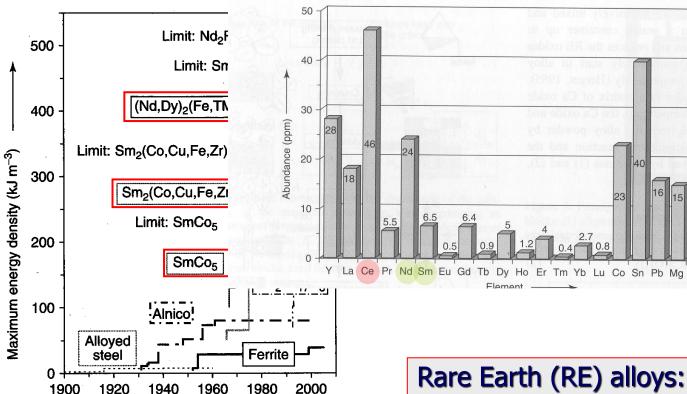


Figure 1. Progress in the maximum energy density of permanent magnets. For RE-TM magnet materials, the theoretical limits are indicated.

Time (years)

W. Rodewald, Rare-earth Transition-metal Magnets, in: Handbook of Magnetism and Advanced Magnetic Materials, vol. 4, Wiley (2007)

Rare Earth (RE) alloys: Ce the most abundant, but limited use

Technological families:

- > SmCo₅
- > "Sm₂Co₁₇"
- "NdFeB"



Magnetic properties of materials, permanent magnets

High Energy Quad Design

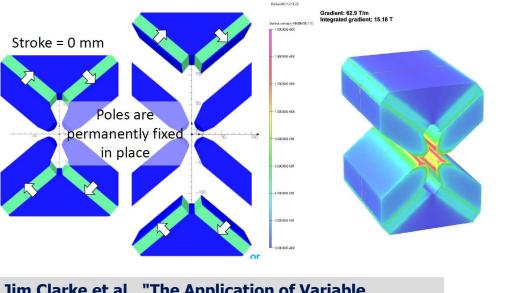
- NdFeB magnets with $B_r = 1.37 T$ (VACODYM 764 TP)
- 4 permanent magnet blocks each 18 x 100 x 230 mm

Max gradient = 60.4 T/m (stroke = 0 mm)

Min gradient = 15.0 T/m (stroke = 64 mm)

opera

- Pole gap = 27.2 mm
- Field quality = $\pm 0.1\%$ over 23 mm



Jim Clarke et al., "The Application of Variable **Strength Permanent Magnet Dipoles and** Quadrupoles", CLIC Workshop 2016, CERN

Stroke = 64 mm

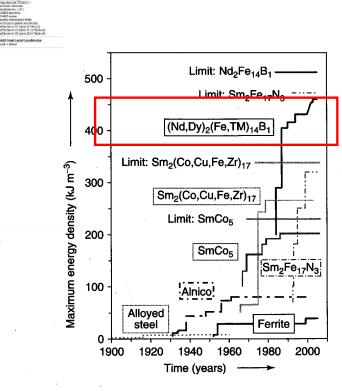


Figure 1. Progress in the maximum energy density of permanent magnets. For RE-TM magnet materials, the theoretical limits are indicated.





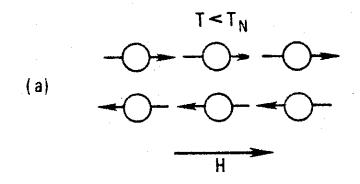
Magnetic properties of materials, antiferromagnetism

Antiparallel arrangement of magnetic moments

Zero net magnetic moment for the material

Cr, Mn and "non magnetic" steels are antiferromagnetic

Exists below a critical temperature (Néel or antiferromagnetic transition temperature T_{af})



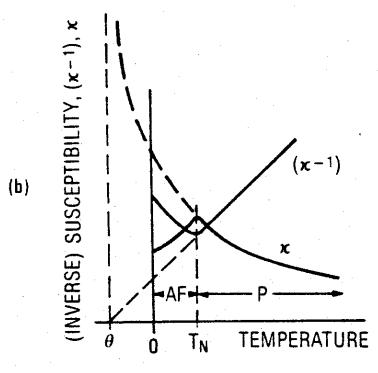
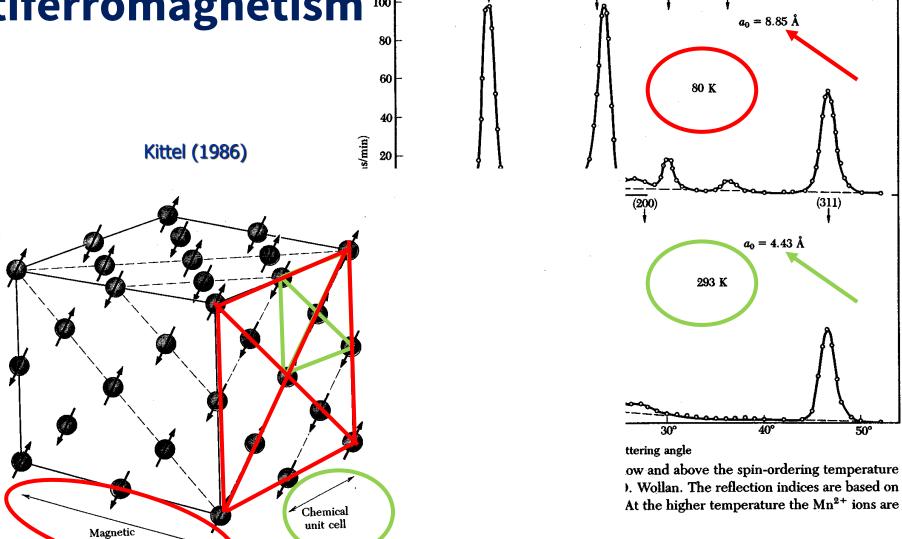


Figure 6.8 (a) Antiferromagnetic alignment of atomic magnetic moments. (b) Susceptibility and reciprocal susceptibility vs. temperature showing antiferromagnetic (AF) and paramagnetic (P) intervals.



Magnetic properties of materials, antiferromagnetism •

unit cell







(311)

(511)

Magnetic properties of materials, antiferromagnetism

- Neutrons are sensitive to the magnetic moment of electrons (interaction of their magnetic moments)
- X-rays are not
- Several other physical properties have discontinuities at T_{af}

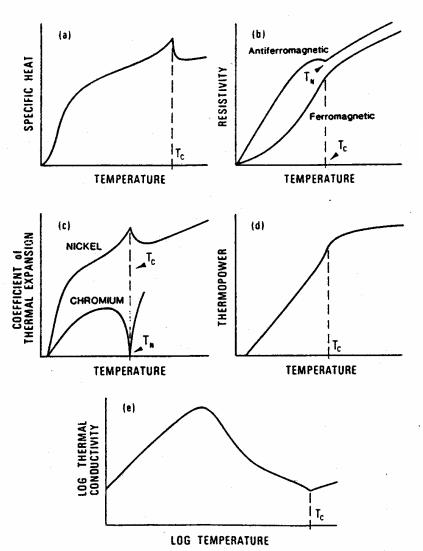


Figure 6.16 The effect of ferro- and antiferromagnetic transitions on a number of material properties.



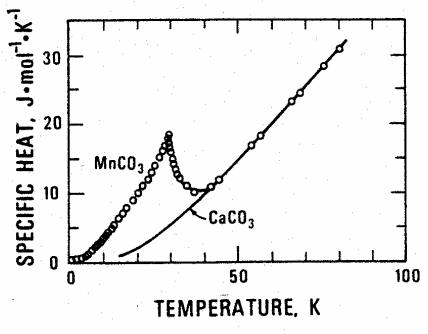
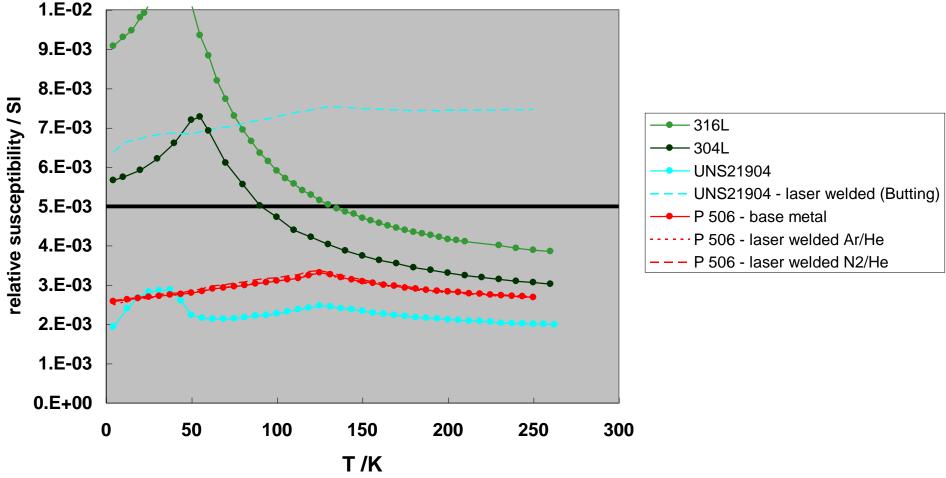


Figure 2.9 Specific heats of MnCO₃ and CaCO₃ (Kalinkina, 1963) illustrate the general effect of a magnetic transition. The Néel temperature for MnCO₃ is 29.4 K.



Magnetic properties of materials, antiferromagnetism



S. Sgobba, G. Hochörtler, A New Non-Magnetic Stainless Steel for Very Low Temperature Applications, Proceedings of the International Congress Stainless Steel 1999: Science and Market, Chia Laguna (I), 6-9 June 1999, Vol. 2, p. 391-401



Magnetic properties of materials, summary

Туре	Dependence of Dep M on H	pendence of κ or μ on T	Magnitude of κ	Magnetic Remanence	Example of Material
Diamagnetism	Linear Independ	lent ^a	Small (<0)	None	Cu, organic
Туре	Material	At <i>T</i> ≅ 295 K ^a	References	and Comments	erconductors low critical
Type	Material	At <i>T</i> ≅ 295 K ^a	$Af T = 4.2 \text{ K}^2$	Referenc	es and Comments
Diamagnetic	Cu Nb	$\kappa = -9.3 \times 10^{-6}$ Paramagnetic	$\kappa = -9.4 \times 10^{-6}$ $\kappa = -1$	Fickett (1976); ve Superconductor	
Paramagnetic Al Ce Potassium- chrome-alum ^b		$\kappa = 2.0 \times 10^{-5}$ $\kappa = 1.6 \times 10^{-3}$ $\kappa = 1.6 \times 10^{-3}$	$\kappa = 2.5 \times 10^{-5}$ $\kappa = 23 \times 10^{-3}$ $\kappa = 32 \times 10^{-4}$ c	Fickett (1976) Edelstein (1968) DeHaas and Gor	ter (1930)
	Fe-22Cr-13Ni-5Mn stainless steel	$\kappa = 2.1 \times 10^{-3}$	Antiferromagnetic	Ledbetter and Co	ollings (1979)
Ferromagnetic	Low-carbon steel	$\mu_r = 5250$ (max.)	$\mu_r = 4900 \text{ (max.)}$	McInturff and C	laus (1970a)
	Si steel (1.8% Si)	$\mu_r = 6250$ (max.)	$\mu_r = 9700 \text{ (max.)}$	McInturff and C	laus (1970a)
Ferrimagnetic	Fe ₃ O ₄	$\mu_r \ge 5.3$	$\mu_r \geq 5.5$		K; Nagata (1961) – RT ation at 0.11 MA·m ⁻¹
Antiferromagnetic	c Fe-22Cr-13Ni-5Mn stainless steel	Paramagnetic	$\kappa = 6.0 \times 10^{-3}$	Ledbetter and Co	ollings (1979)
^a Si units ^b Cr ₂ (SO ₄) ₃ ·K ₂ SO ₄ ·2 ^c T = 14 K	4H ₂ O				
	4H ₂ O				

R.P. Reed, A.F. Clark (1983)





Spare slides

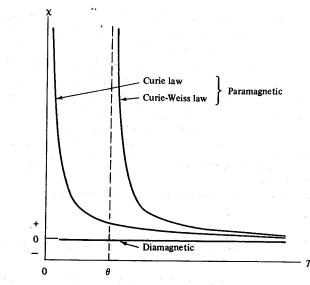




Magnetic properties of materials, ferromagnetism

- Systematic measurements reported by P. Curie in 1895
- Susceptibility for paramagnets \Rightarrow $\kappa_p = C/T$ (Curie law)
- Weiss (J. Phys. 6 (1907) 66) postulated interaction of elementary moments (⇒ molecular field)
- Fictitious internal field postulated
- $H_e = \lambda M (\lambda, molecular field constant)$
- Total magn. $M = \kappa_p(H_a + H_e) = C/T (H_a + \lambda M)$

$$\kappa = M/H_a = C/(T-C\lambda), T_c = C\lambda$$



Variation of mass susceptibility with absolute temperature for para- and diamagnetics.

B.D. Cullity, C.D. Graham, Introduction to Magnetic 2nd ed., Wiley (2009)

- ⇒ 1) T_c connected to the "mean" or "molecular field constant"
- ⇒ 2) Theory is consistent with existence of spontaneous magnetisation at T_c and below



Magnetic properties of materials, ferromagnetism

As a rule of thumb:

In general b.c.c. ferrous phases are ferromagnetic, f.c.c. are not

Phases, not alloys (see austenitic stainless steels)!



Properties affected by the T and t of annealing, and by cooling rate

Latter especially critical in the 900 °C to 800 °C range due to $\gamma \Rightarrow \alpha$ transformation

If $T_{\alpha,\gamma}$ is exceeded, cooling rate slow, approx. 5 °C/min

Higher max. μ is obtained by exceeding $T_{\alpha,\gamma}$ than by not allowing the material to transform to γ at all

Hence, for high μ_{max} an anneal at 925-1000 °C with cooling < 5 °C/min recommended

For high permeability at B≥1.2 T, advisable to anneal at max 800 °C and to cool slowly (Armco steel Co., 1943)

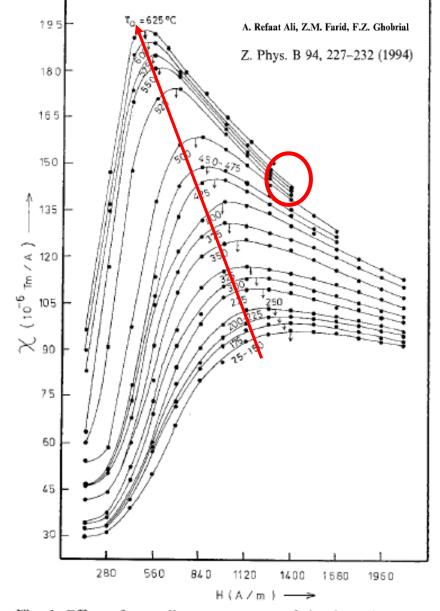
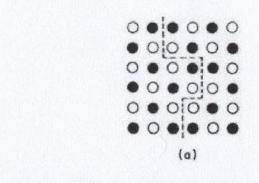


Fig. 1. Effect of annealing temperature of the dependence of the magnetic susceptibility (χ) on the magnetic field (H) of heavily cold-worked Fe-0.006 wt.% C, t_a = 15 min





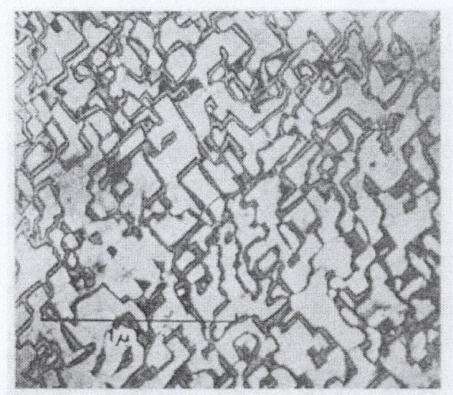


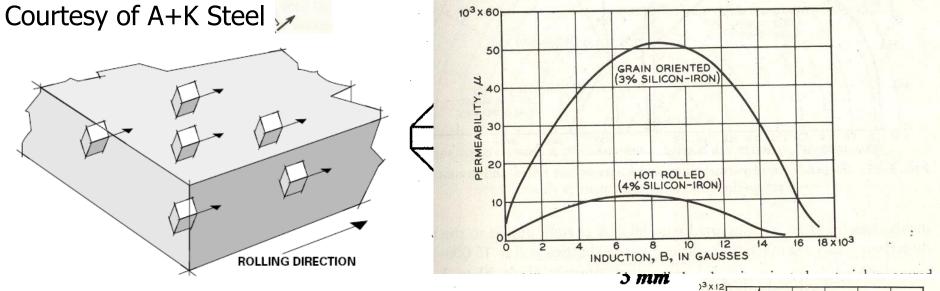
Fig. 5.54. Antiphase domain boundaries characterizing short-range order. (a) A two-dimensional diagram showing the like-atom pairs across the boundary and (b) electron microscopy evidence ((b) Fisher and Marcinkowski [1960]).

- "Directional-order" theory (Néel, Taniguchi and Yamamoto, Chikazumi and Oomura)
- Any solid solution which is not completely ordered contains some pairs of nearest neighbor like atoms
- At T≤ Tc, but high enough for diffusion to occur, like-atom pairs tend to be aligned in the direction of the local magnetization.
- When the temperature drops so low that diffusion can no longer occur at an appreciable rate, the like-atom pairs are frozen in place, and produce a uniaxial anisotropy in the material.

[Gordon and Sery, IEEE Trans. Nuclear Science, vol. NS-I 1, pp. 105-110 (1964)]



"Goss" (1934-37) texture (110)[001]



Fe single crystals exhibit

- minimum coercivity
- maximum permeability

when magnetized along one of the <001> axes

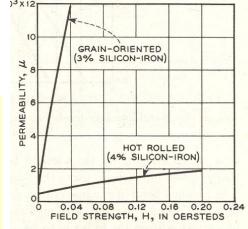


Fig. 4–13. Permeability in low fields, showing non-linear relation.



RD_m10 mm



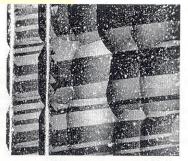


FIGURE 2.11 Domains in HGO Fe–Si laminations. They are oriented along the [001] axis and tend to multiply upon scribing the sheet surface.

F. Fiorillo, Characterization and Measurement of Magnetic Materials, Elsevier, 2004

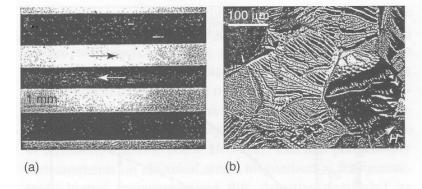


Figure 1. Typical static domain images in (a) grain-oriented and (b) nonoriented electrical steel. (Reproduced from Hubert *et al.*, 1998.) With permission from Springer-Verlag GmbH. © 1998.)

A.J. Moses, in: Handbook of Magn. and Adv. Magn. Mat., Wiley, 2007

Texture + large grain size + low impurity content

- coercive fields as low as 4-10 A/m
- 2. maximum permeability around 5 x 10⁴

in GO alloys (10 x NGO)

- 1. Conventional GO (7° dispersion) 80 % of the market 1 M ton/y, 1500 M EUR/y
- 2. High permeability GO (3° dispersion)

of the [001] axes around RD



