



# Forum on Tracking Detector Mechanics 2023

Low-mass support structures with integrated services for detector systems.

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# Outline

1. Motivation and Introduction
2. Hybrid composite design
3. Simulation results
4. First prototypes
5. Summary, conclusions and future work

Funded by:



# Why is mechanics design important? - Future colliders (FCC-hh like)

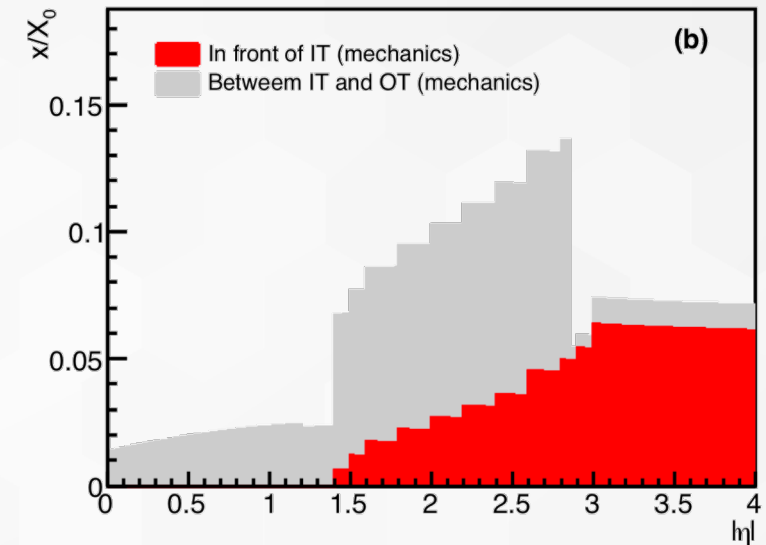
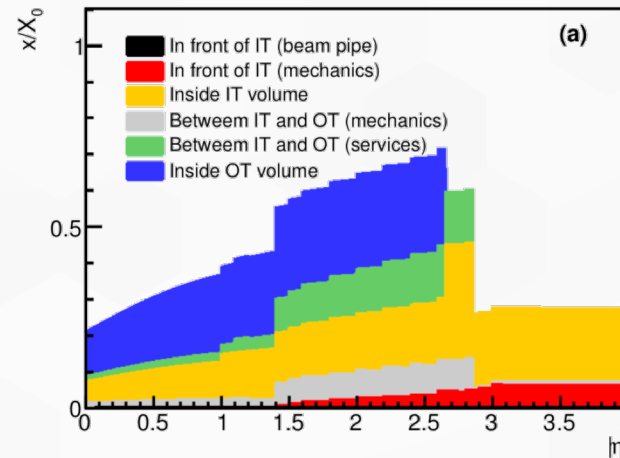
High-luminosity phase of the LHC as example in this talk, but future colliders

- Momenta and angular ranges up by 10x and 2x
- Challenging for forward tracking/detectors
- Pile-up of a thousand results in very harsh conditions

## HL-LHC upgrades as example:

- Support structures need to be optimized, light-weight → minimal mass possible, highly thermally conductive
- CMS HL-LHC upgrades as example

Pixel Layer dose (3.7cm)	HL-LHC $3ab^{-1}$	FCC $3ab^{-1}$	FCC $30ab^{-1}$	FCC (2.5cm) $30ab^{-1}$
$\times 10^{16} n_{eq} cm^{-2}$	1.5	3	30	70
Dose (MGy)	5	10	100	220

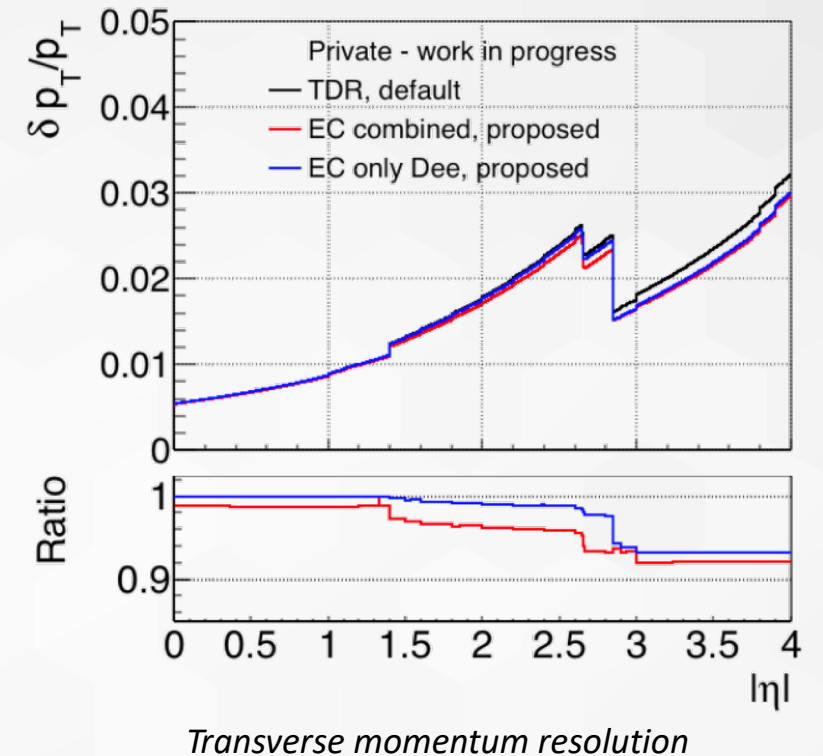
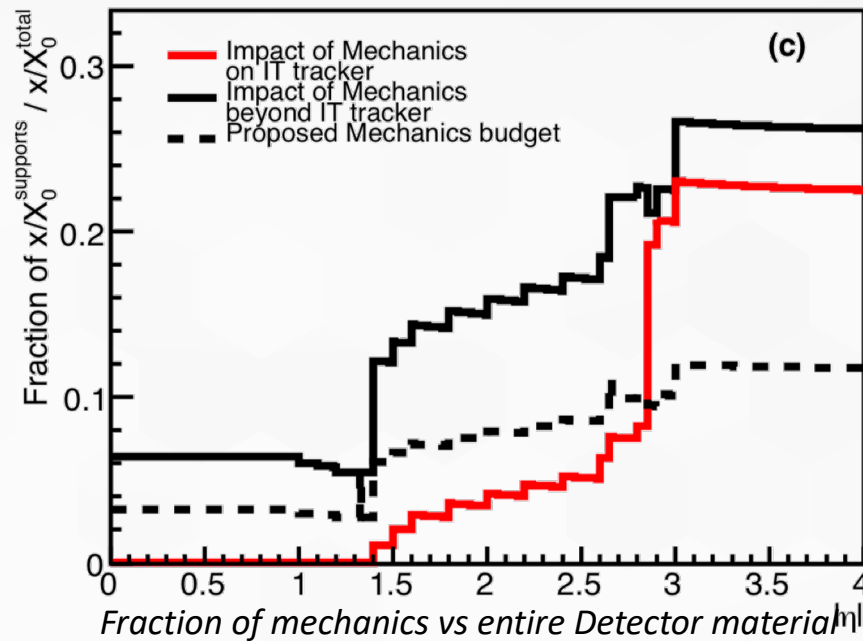


# Material budgets and mechanics

Substantial R&D on all fronts to make a FCC-hh detector a reality

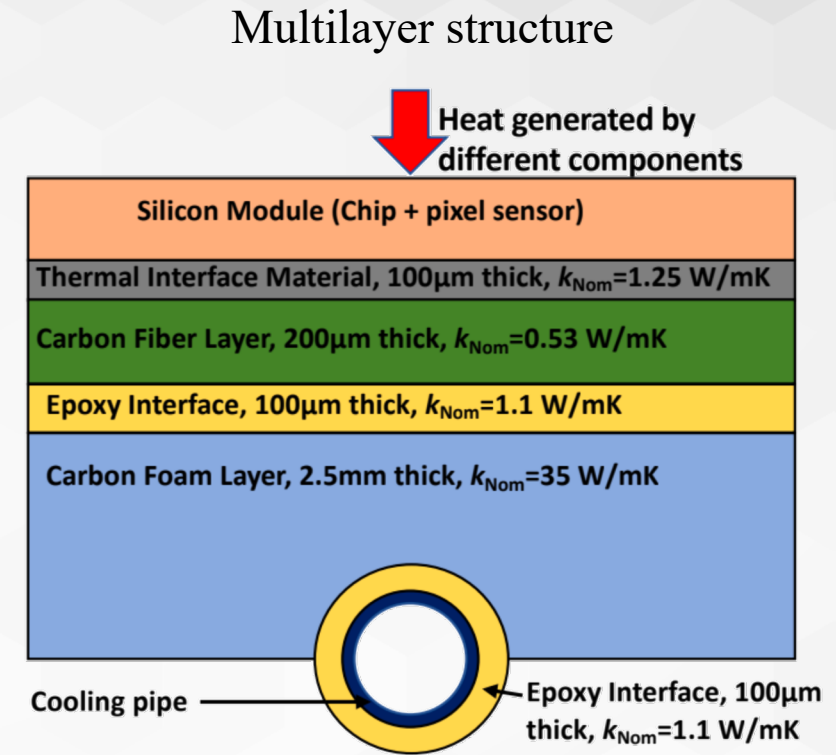
- Support & Cooling constrains Tracker performance, e.g. thermal runaway
- Mechanics is significant fraction of the material budget
- Material testing standardization for irradiation response

- Can improve b-ID efficiencies by 2-3% per b-jet and high b-jet multiplicity ~10-15%
- Significant improvement by novel approach, b-ID relevant for di-Higgs (priority @FCC-hh)



# Current Architecture of Support Systems

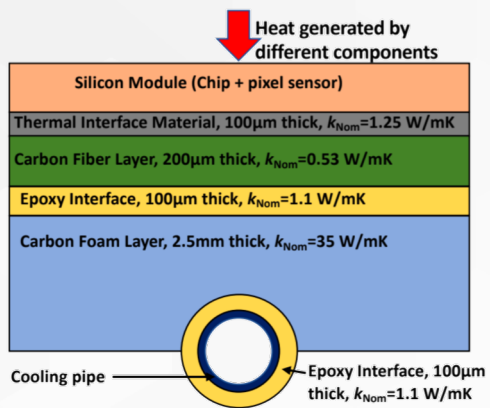
- ◆ State of the Art: Multilayer Structure
  - Integrates layers of different material systems with low thermal conductivity (e.g., epoxy interface)
  - Extensive multi-step fabrication process
  - Involves metallic cooling lines
  - Fabrication process poses additional challenges for non-planar geometries
  - Interfaces between layers involve thermal and thermomechanical considerations



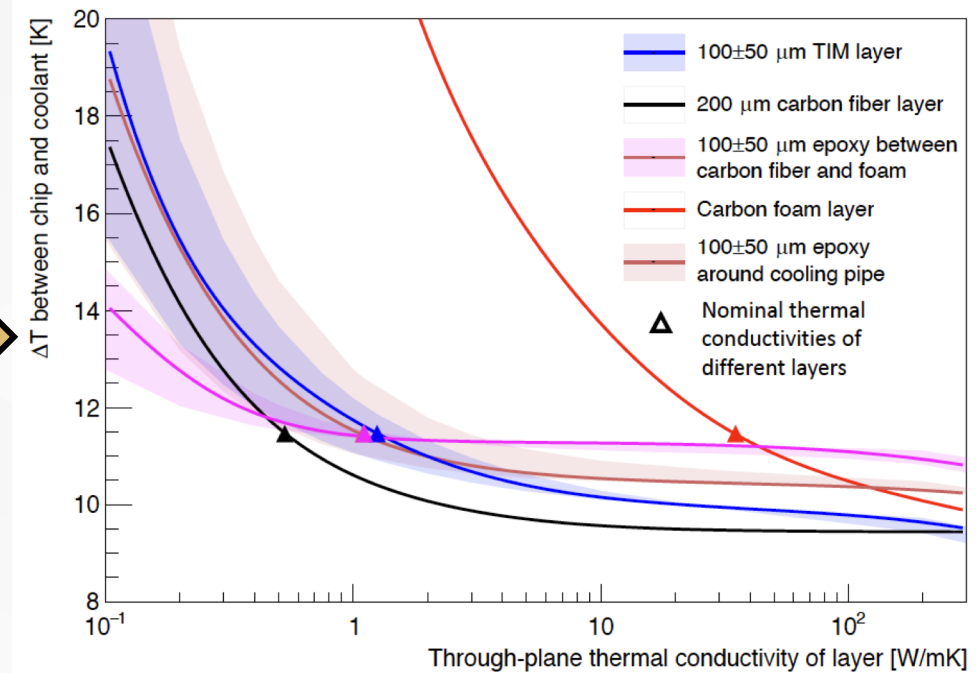
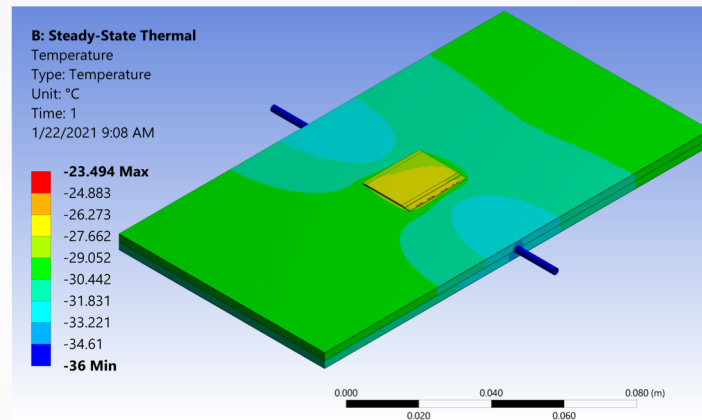
# Thermal Performance of Current Architecture of Support Systems

## Contribution of Each Layer to Thermal Response

### Multilayer Structure



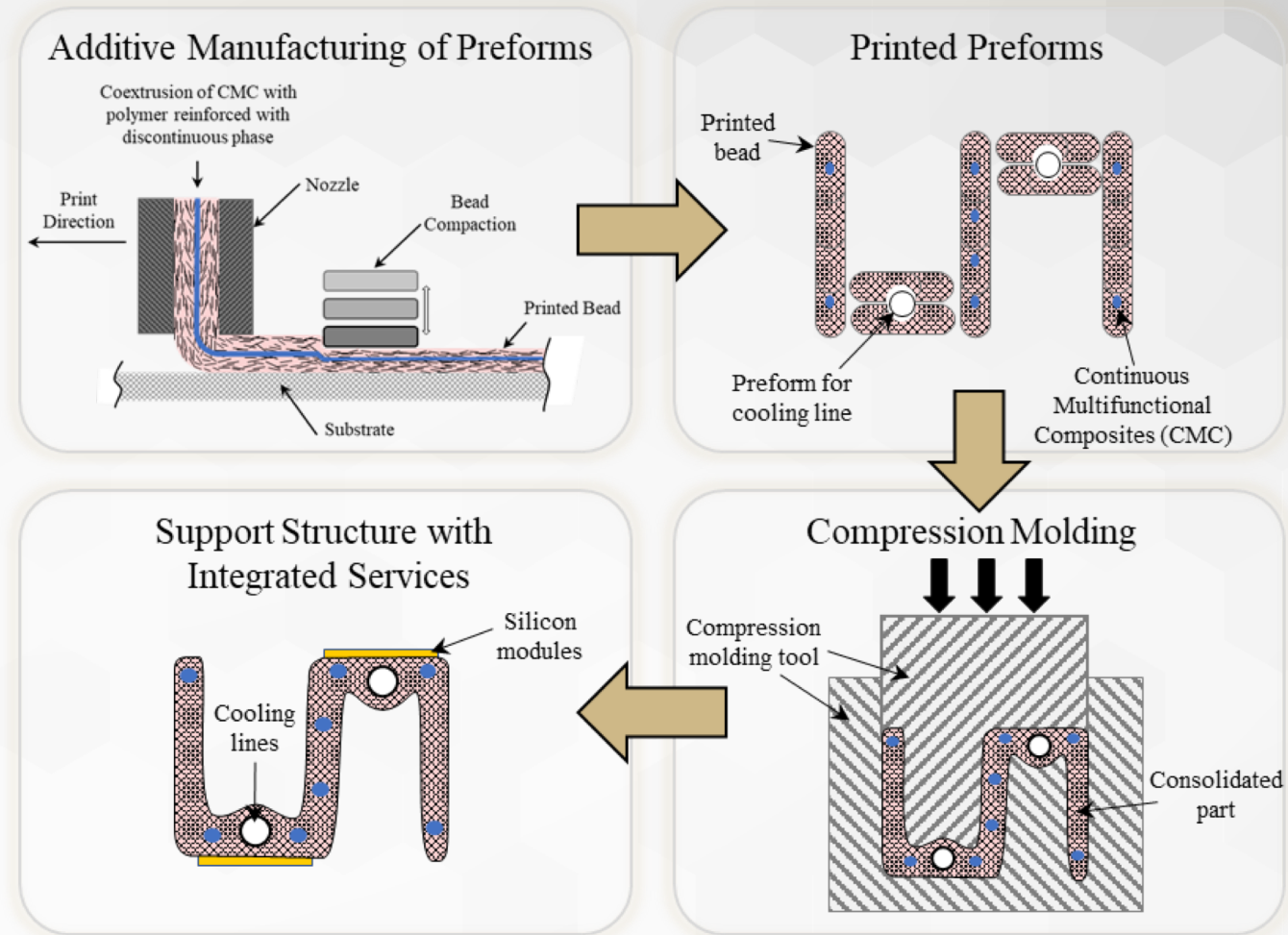
### Thermal FEA



# Hybrid Composites for Support Structures with Integrated Services

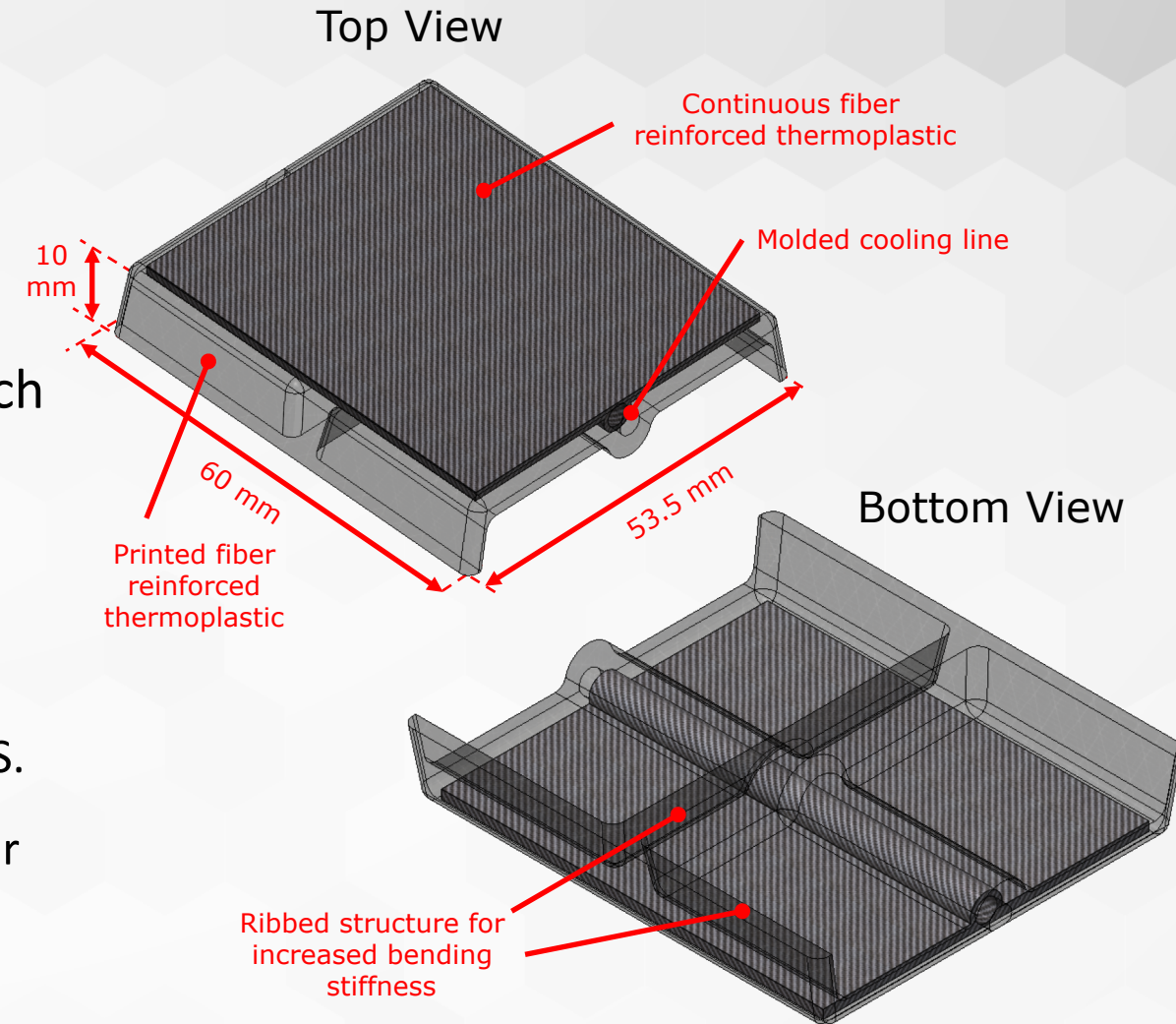
Two-step manufacturing process to produce monolithic hybrid structures with integrated services

- Additive manufacturing of preforms to provide control of continuous fiber orientation
  - Fiber orientation is driven by thermal and thermomechanical performance requirements
- Compression molding to consolidate printed preforms and to integrate cooling lines
  - Remove voids and reduce effect of interfaces between dissimilar layered materials



## Prototype Support Structure with Integrated Services

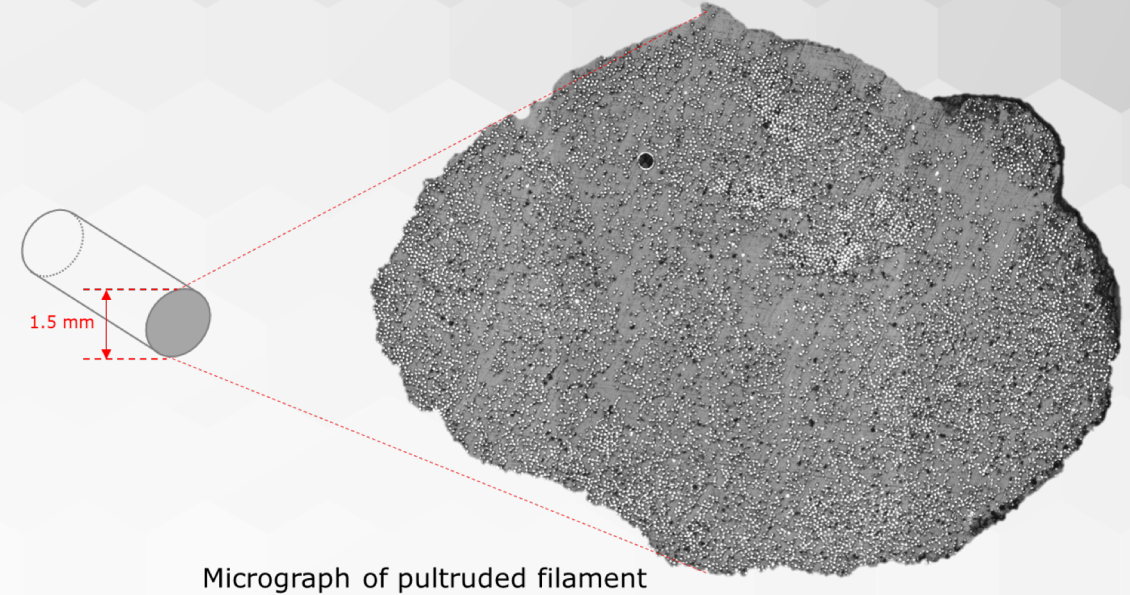
- Cooling lines molded in.
- Thermal pathways provided by continuous carbon fibers.
- Stiffness provided by ribbed structure and continuous carbon fiber (Weight 60% < sandwich structure).
- Strength provided by continuous carbon fiber
- Compression molding process included:
  - Preform of continuous fiber impregnated with PPS.
  - Printed continuous and discontinuous carbon fiber reinforced PPS.



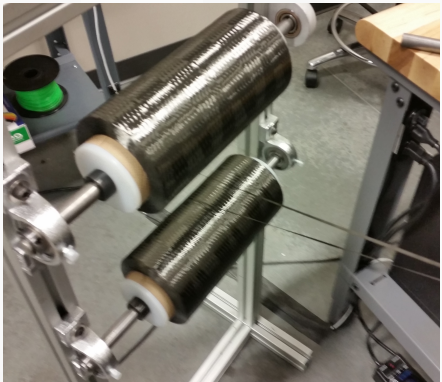


# Continuous Carbon Fiber Inclusion in 3D printed preforms

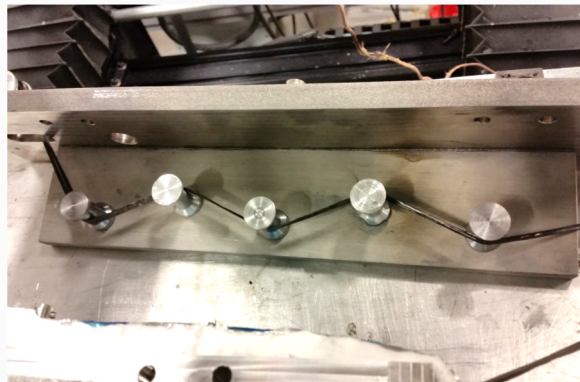
- Continuous carbon fiber filament produced by pultrusion process.
- 40% by volume of carbon fiber
- Average impregnated filament diameter of 1.5 mm
- Achieved high level of impregnation (>95%)
- Commercial grade of carbon fiber compounded with PPS was used for printing (50% wt. CF-PPS).



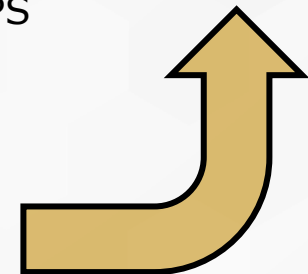
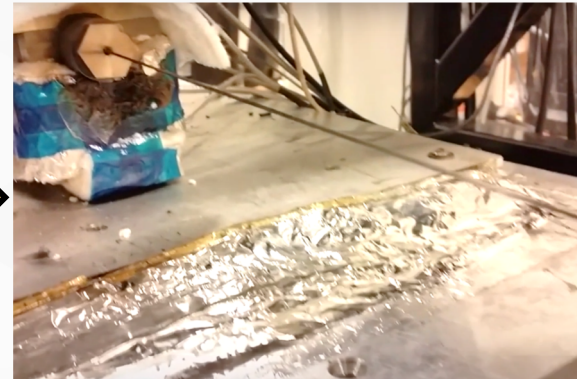
Spools of Carbon Fiber



Interior of Impregnation Chamber

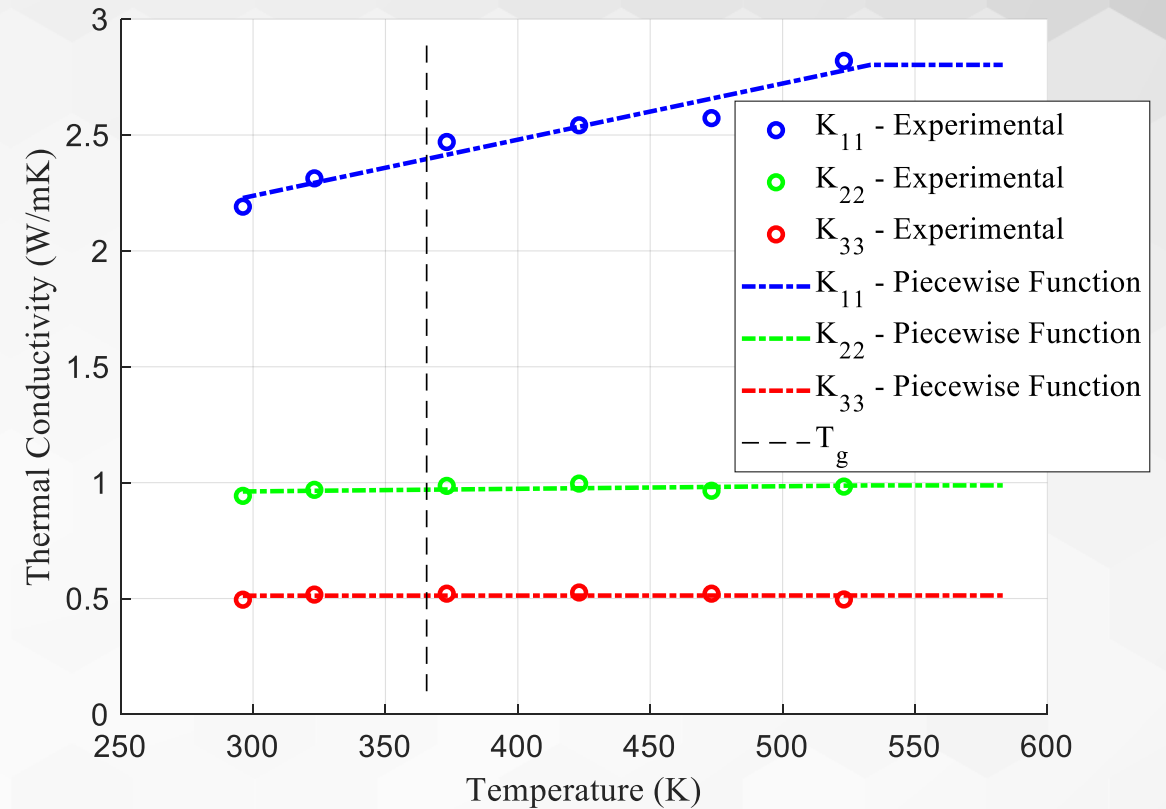
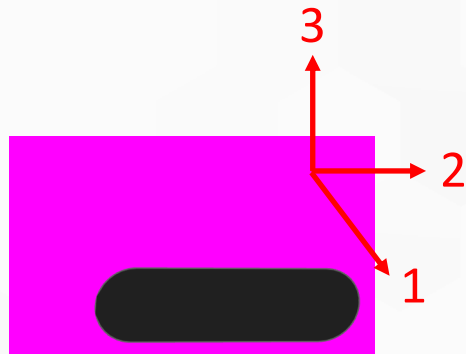


Carbon Fiber Impregnated with PPS



# Characterization of Thermal Conductivity

- Laser flash technique (ASTM E1461) used for characterizing thermal conductivity of printed material (50% by wt. of carbon fiber reinforced PPS)
- Micromechanics models to predict thermal conductivity of filament with continuous carbon fiber.



Thermal conductivity in the three principal directions of printed short carbon fiber reinforced PPS.

## Characterization of Thermal Conductivity

- Micromechanics predictions of thermal conductivity for 40% by volume of continuous carbon fiber reinforced PPS.
  - Two-step homogenization using Mori-Tanaka method.
  - Types of fiber considered: Hexcel AS4<sup>1</sup> and Nippon CN-90
  - Polymer considered: Celanese Celstran 0203P6 PPS<sup>2</sup>

Hexcel AS4

Direction	Thermal Conductivity (W/mK)
$K_{11}$	2.918
$K_{22}$	0.5
$K_{33}$	0.5

Nippon CN-90

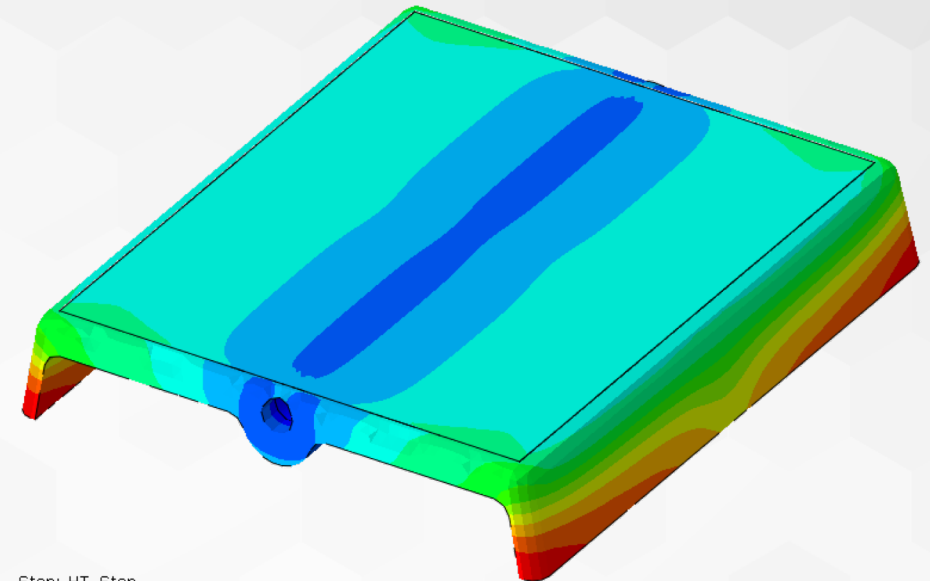
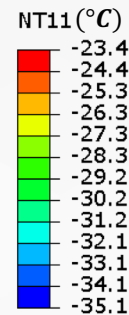
Direction	Thermal Conductivity (W/mK)
$K_{11}$	200.2
$K_{22}$	0.72
$K_{33}$	0.72

<sup>1</sup> Hexcel Corporation. HexTow® AS4 Carbon Fiber Product Data Sheet. 2020.

<sup>2</sup> Celanese. FORTRON® PPS POLYPHENYLENE SULFIDE (PPS). Short-Term Properties Guide. 2016.

## Steady State FE Heat Transfer Analysis

- Heat transfer analysis used to drive design of continuous fiber and to investigate effects of fiber thermal conductivity
- Surface heat flux ( $0.1 - 1 \text{ W/cm}^2$ ) applied over detector's surface (heat flow of  $2.5 - 25.85 \text{ W}$ )
- Cooling line set to  $-35 \text{ }^\circ\text{C}$
- Convection ( $h = 7.5 \frac{\text{W}}{\text{m}^2\text{ }^\circ\text{C}}$ ) and radiation ( $\epsilon = 0.92$ ) from exposed surfaces to ambient temperature of  $-20 \text{ }^\circ\text{C}$
- Assumed ideal bonding between material systems (no thermal resistance)



Step: HT\_Step  
Increment 2: Step Time = 2.000  
Primary Var: NT11

# Finite Element Mesh

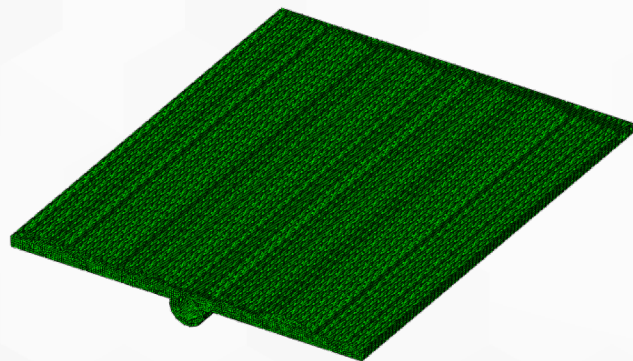
## Continuous Fibers Reinforcements:

- Hexahedron element mesh (DC3D8)
- Thermophysical properties of continuous carbon fiber reinforced PPS (investigated Hexcel AS41 and Nippon CN-90)
- Considered orthotropic elastic properties and thermal conductivity based on material orientation (Fibers oriented across cooling line)

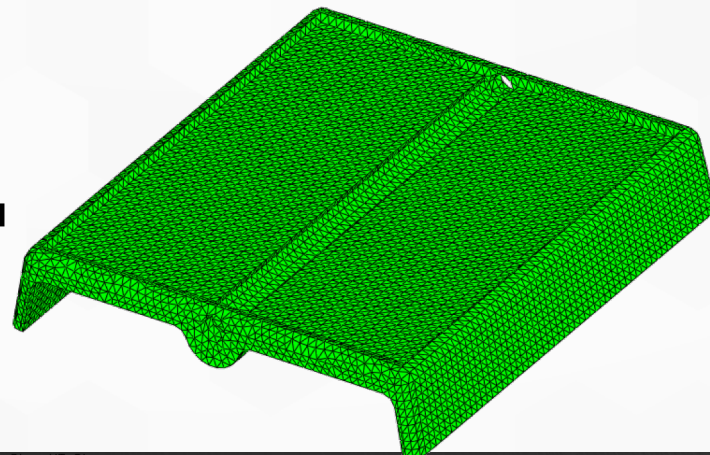
## Discontinuous Fibers Structure:

- Tetrahedral element mesh (DC3D4)
- Considered properties of short-carbon fiber reinforced PPS (measured experimentally)
- Neglects anisotropic thermal conductivity

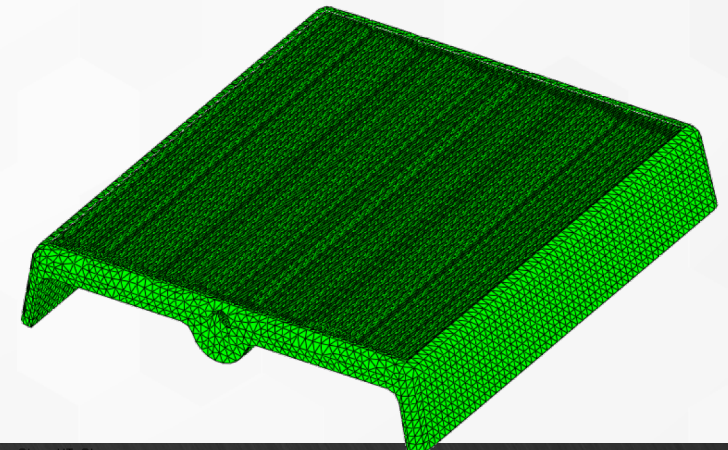
Continuous Fiber System



Discontinuous Fiber System



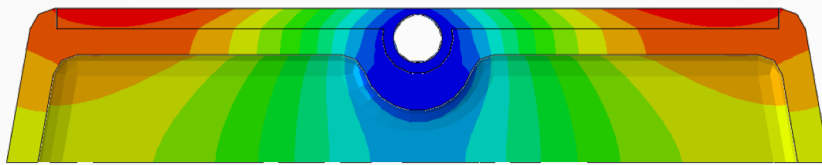
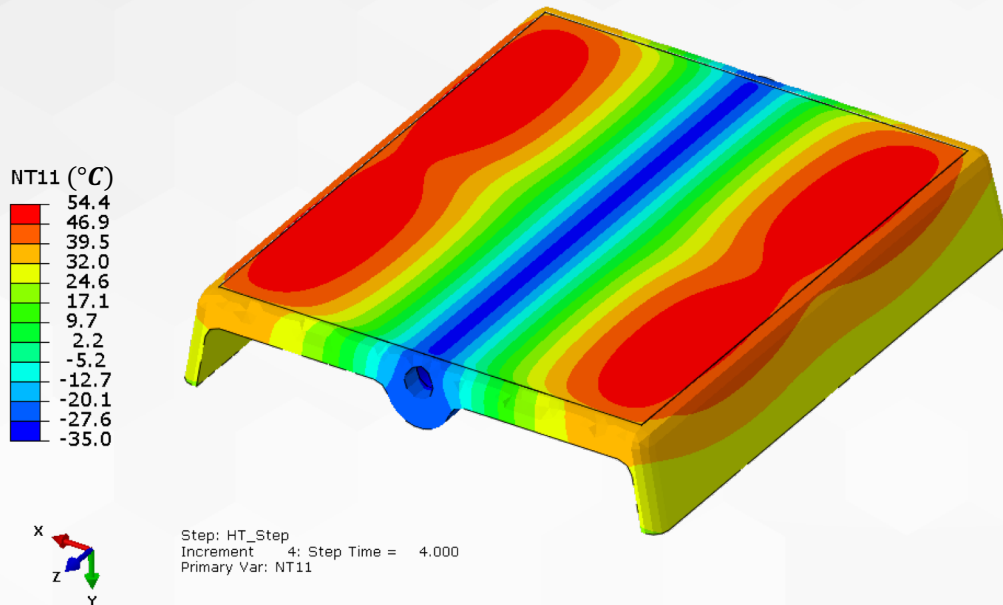
Hybrid Compression Molded Structure



# Temperature Field with Different Fiber Systems

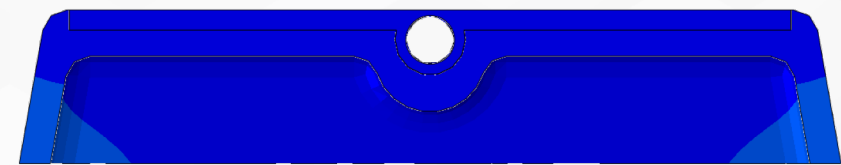
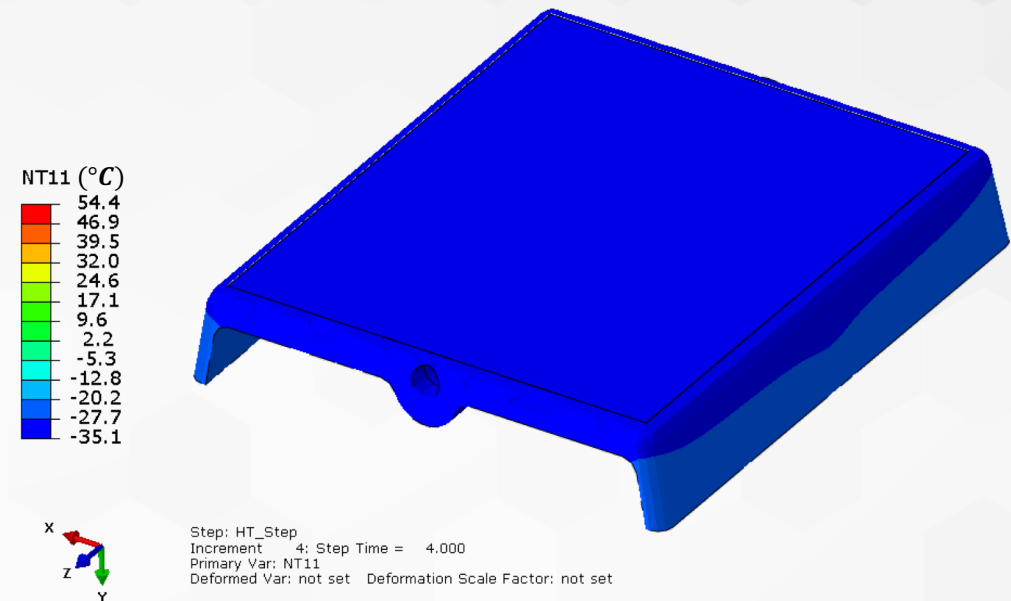
Steady state temperature field at heat flow of 10.34 W

Hexcel AS4



Cross section

Nippon CN-90

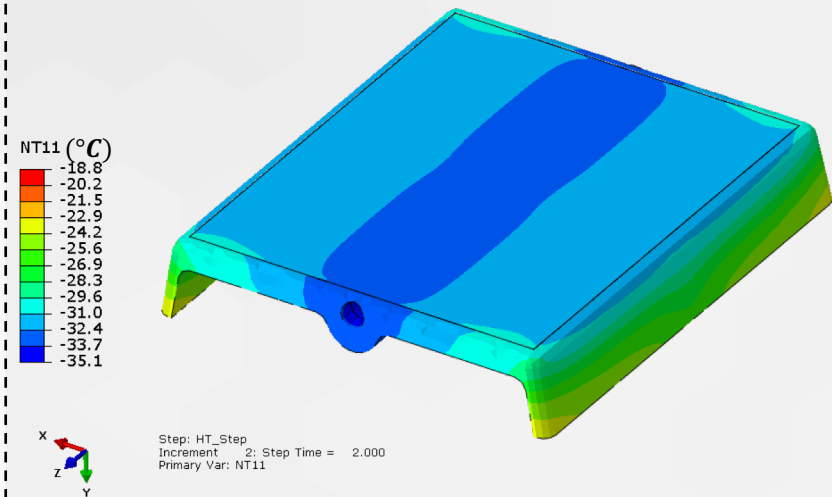


Cross section

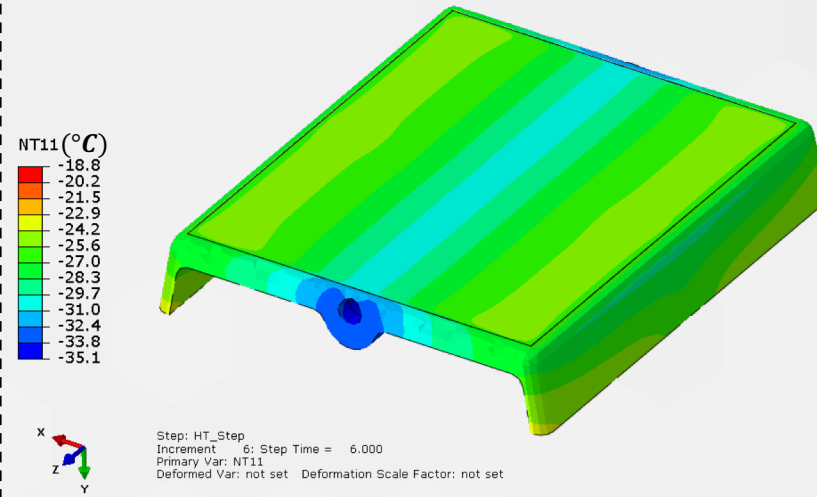
# Temperature Fields at Different Heat Flows

- Fiber system considered: 40% vol. Nippon CN-90 reinforced PPS

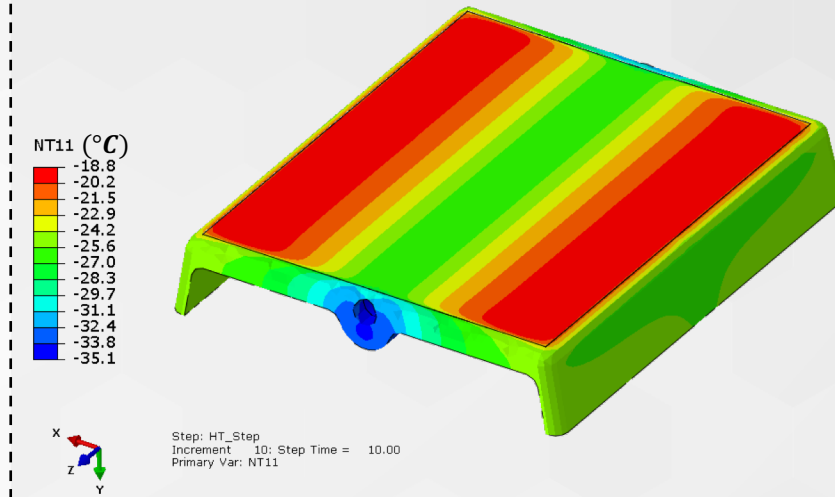
Heat flow = 5.17 W  
(0.2 W/cm<sup>2</sup>)



Heat flow = 15.51 W  
(0.6 W/cm<sup>2</sup>)

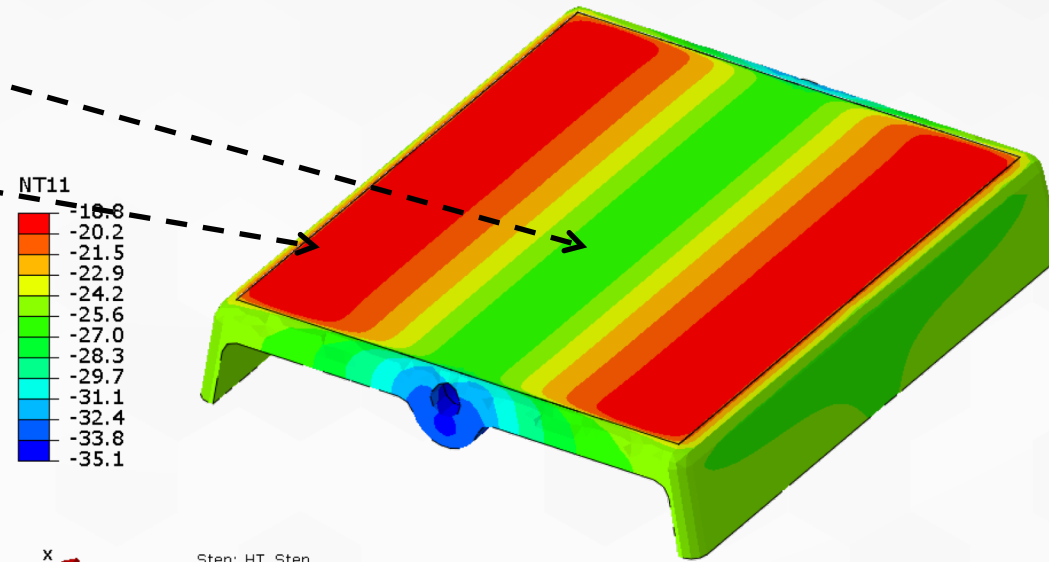
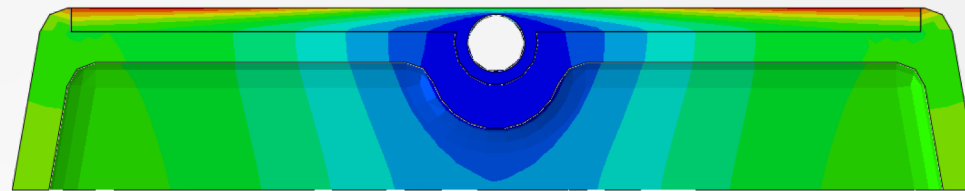


Heat flow = 25.85 W  
(1.0 W/cm<sup>2</sup>)



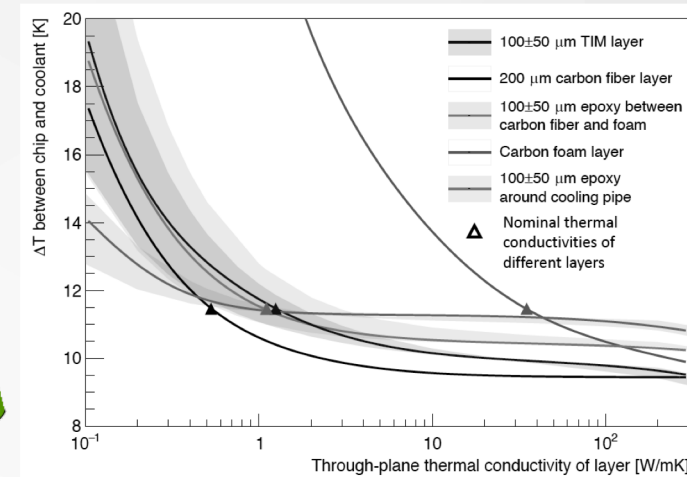
# Temperature Difference Between Detector and Coolant

- Temperature difference between detector and coolant varies between  $4.2\text{ }^{\circ}\text{C}$  and  $15\text{ }^{\circ}\text{C}$  across the detector



Step: HT\_Step  
Increment 10: Step Time = 10.00  
Primary Var: NT11

Heat flow =  $25.85\text{ W}$  ( $1.0\text{ W/cm}^2$ )

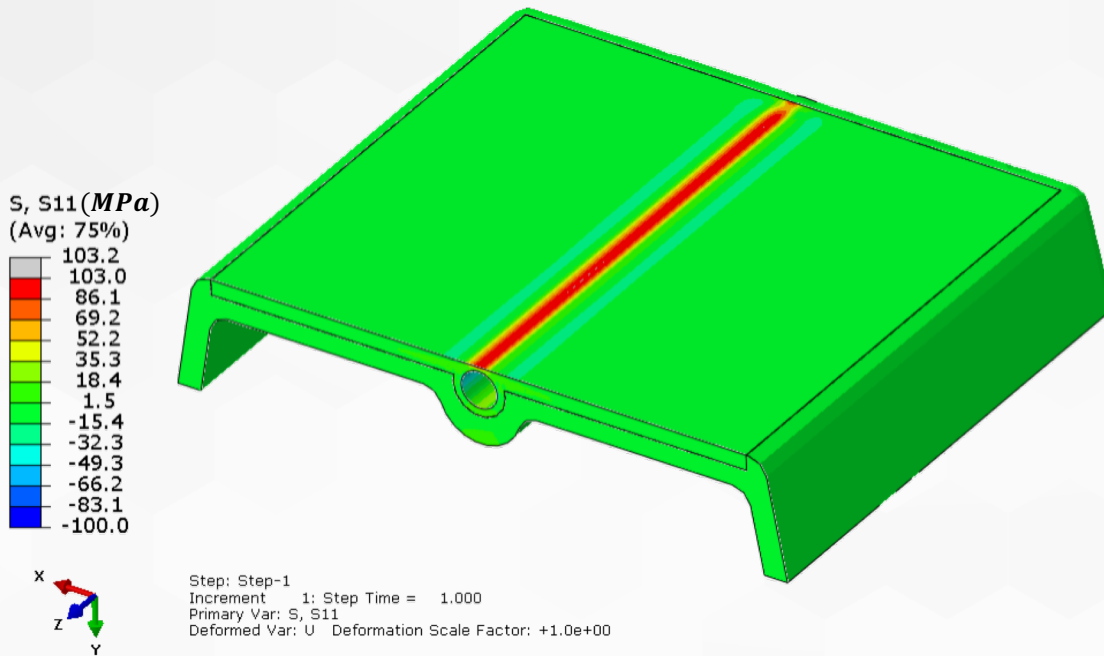




# Stress Analysis of Hybrid Structure Under Pressure

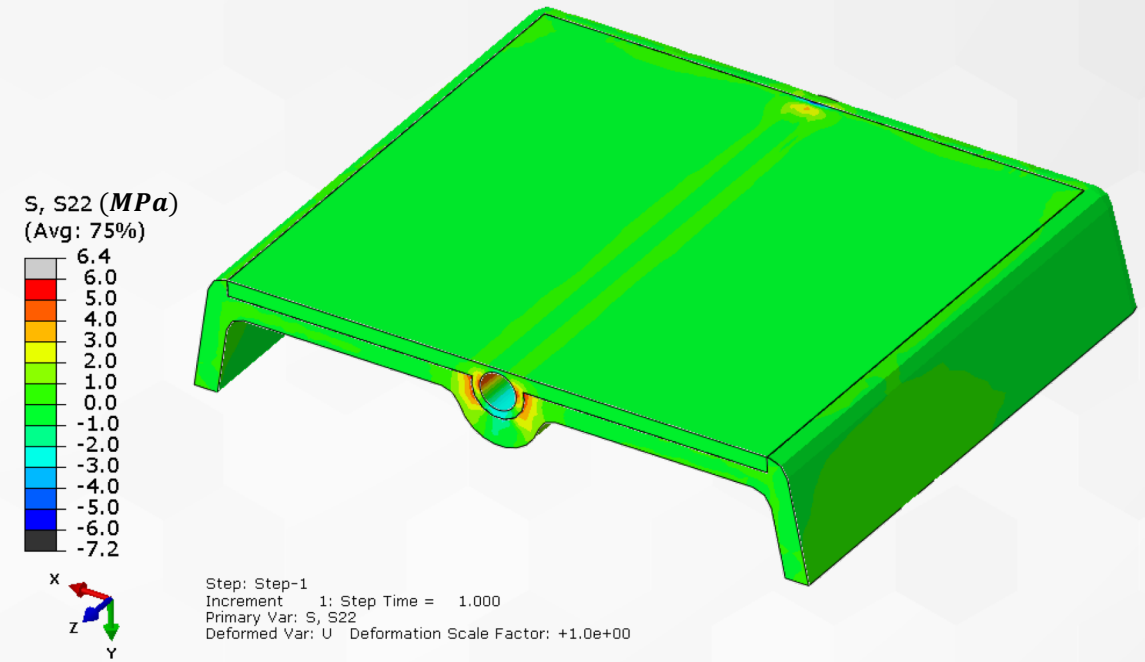
- ◆ Cooling line pressurized at 68.9 Bar

Stress in Fiber Direction



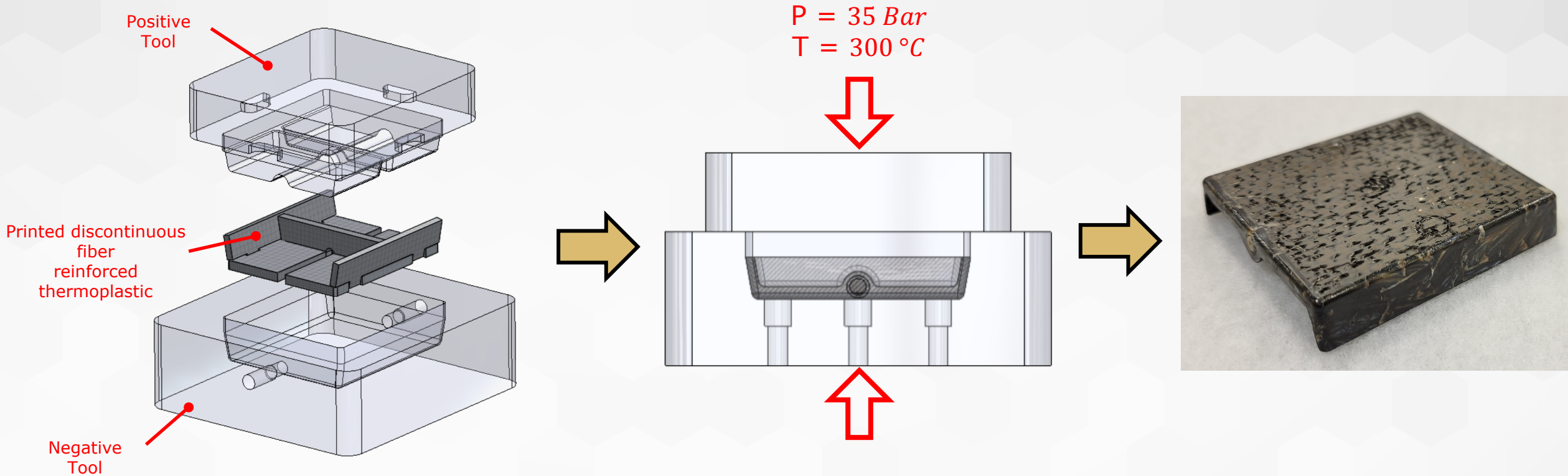
$$\sigma_{11} \ll X_1^T \sim 300 - 500 \text{ MPa}$$

Stress Transverse to Fiber Direction



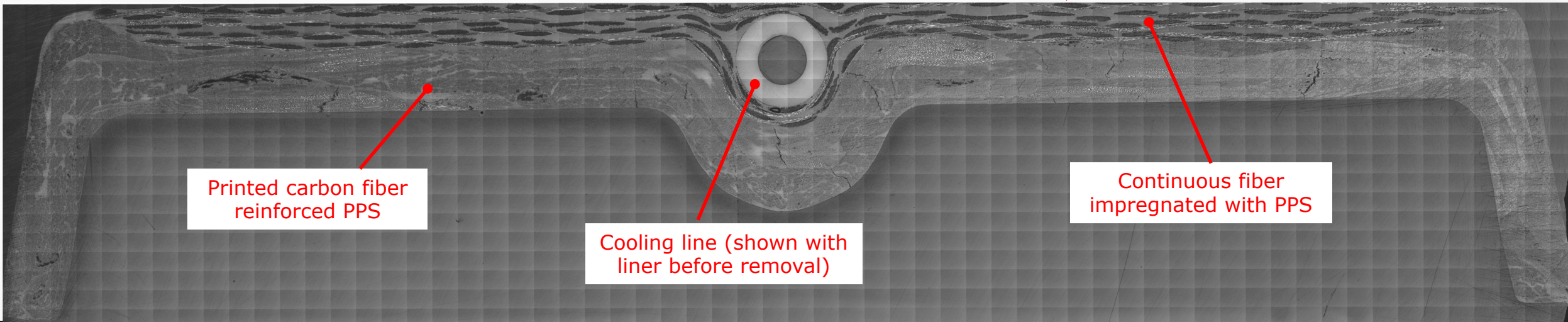
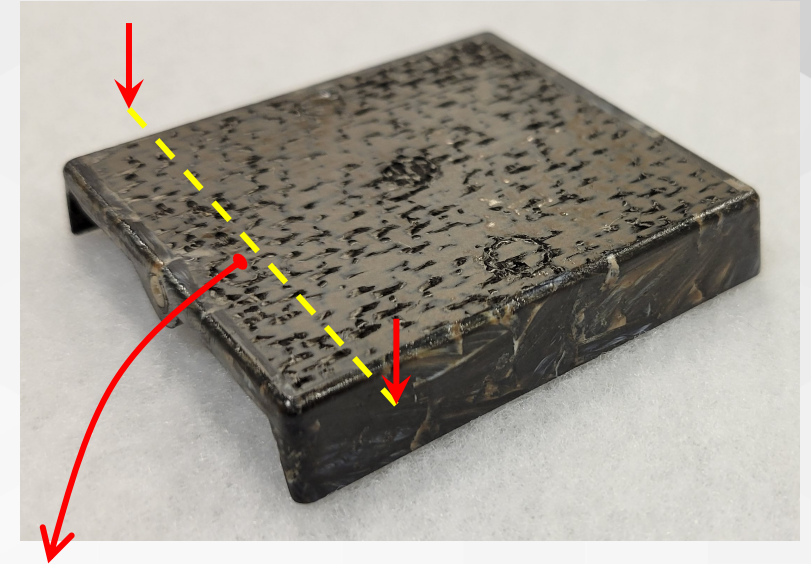
$$\sigma_{22} \ll X_2^T \sim 30 - 50 \text{ MPa}$$

# Compression Molding Process



# Prototype Support Structures with Integrated Services

- Cross section of molded prototype demonstrates:
  - Feasibility of integrating cooling line with non-metallic liners
  - Hybrid continuous and discontinuous fiber architecture
  - Consolidation of multiple material systems through compression molding



Printed carbon fiber reinforced PPS

Cooling line (shown with liner before removal)

Continuous fiber impregnated with PPS

## Summary and Conclusions

- ◆ The hybrid structures with integrated services offer the potential to reduce manufacturing time, cost, and to improve thermal performance.
  - ◆ Reduces the number of thermal interfaces
  - ◆ Provides engineered thermal paths through microstructures printed with highly thermally conductive fibers
  - ◆ Offers the potential to remove metallic liners used in traditional designs
  - ◆ Allows for complex non-planar designs
- ◆ The heat transfer and structural analyses showed the potential to meet the thermal and structural requirements of support structures
- ◆ The prototype demonstrated the feasibility of manufacturing support structures with integrated cooling

## Future Work

- ◆ Conduct experimental validation on prototype
  - ◆ Structural integrity of structure under cooling's line pressure
  - ◆ Integrity of custom developed non-metallic cooling line connections
  - ◆ Thermal performance at different power levels
  - ◆ Verify simulation predictions for temperature fields in representative conditions
- ◆ Apply technology to full size support structure
  - ◆ Potential for modular designs

# Acknowledgments



# Thank You!