

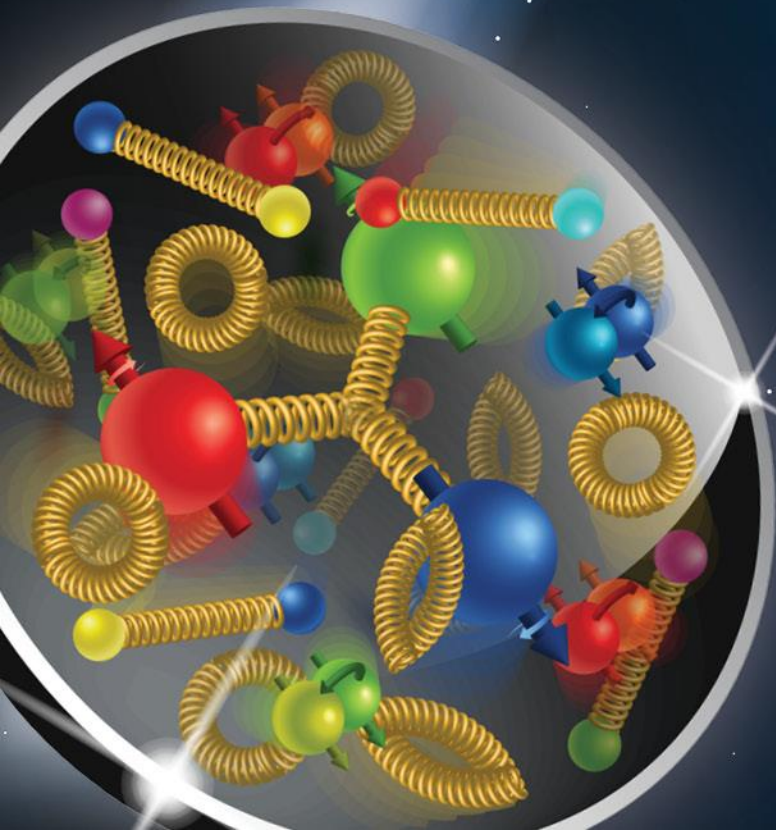
# Electron-Ion Collider User Group Meeting 2023

Valerio Calvelli (CEA Paris-Saclay)  
On Behalf of EIC Detector Magnet team

## Status of MARCO Solenoid

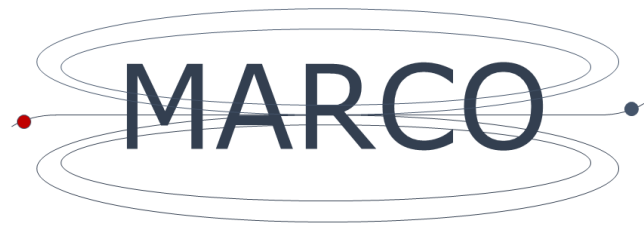
July 27, 2023

Electron-Ion Collider

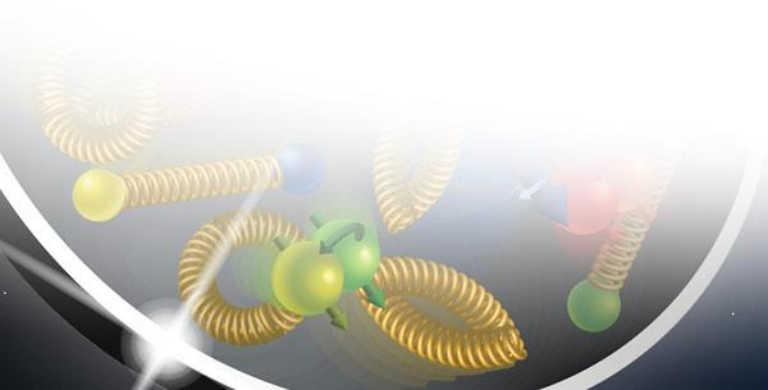


# Outline

- ePIC Detector Solenoid (MARCO) Overview
- MARCO Magnet Specifications
- Status of the Design
- 3D Magnetic Design Results
- Conductor definition
- Mechanical Design
- Cryogenic Design
- Magnet Assembly
- Conclusions



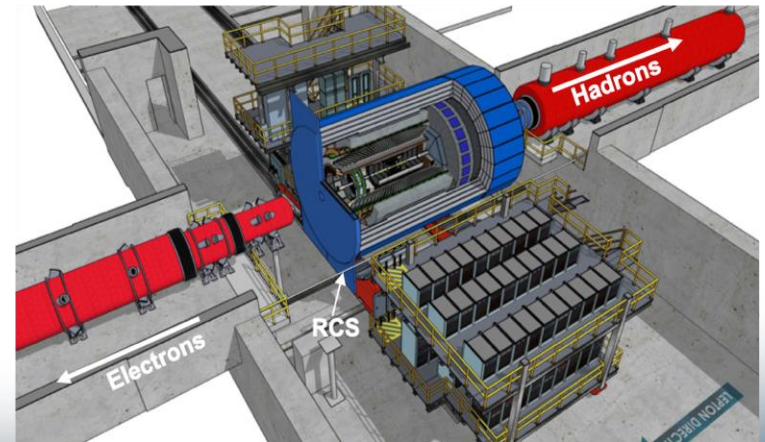
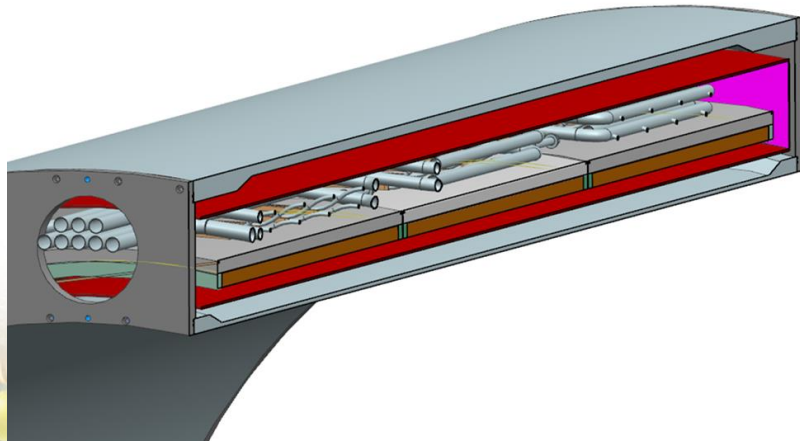
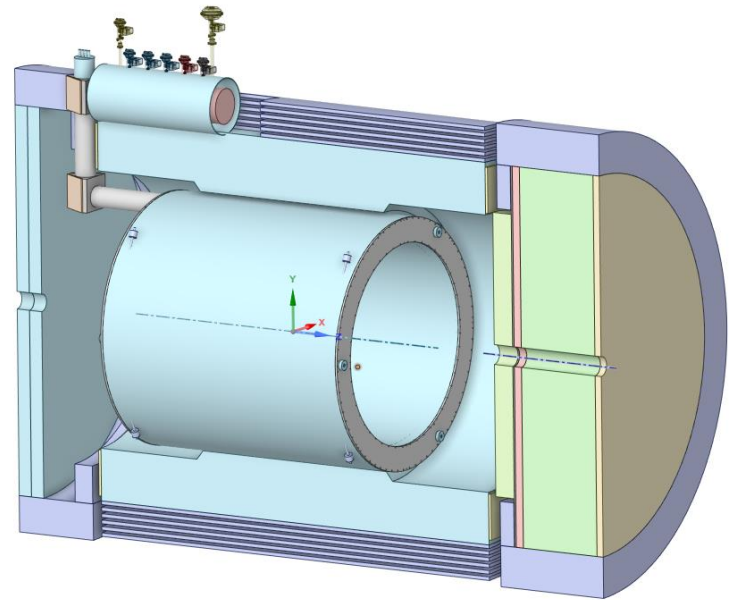
*M*Agnets with *R*enewed *C*Oils



# ePIC Detector Solenoid (MARCO) Overview

## Superconducting Detector Solenoid

- 3.5 m long coil, 2.84 m room temperature bore diameter
- 2 T on-axis field
- Operating Temperature 4.5 K
- Conductor: Copper Cladded, Rutherford Cable made with NbTi superconducting strands

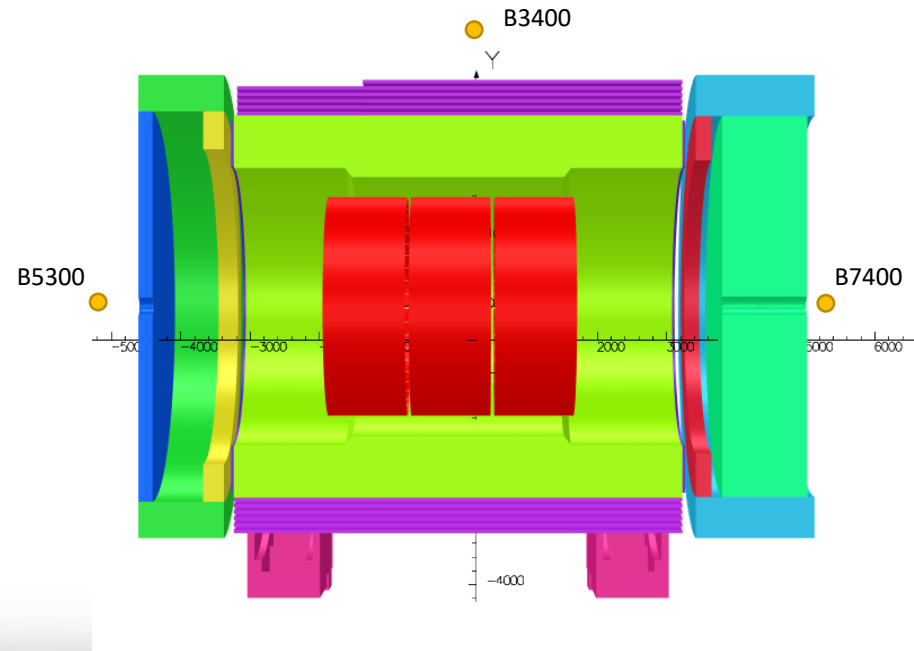


# MARCO Magnet Specifications

Parameter	Value
Coil length	3512 mm
Warm bore diameter	2840 mm
Cryostat length	< 3850 mm
Cryostat outer diameter	< 3540 mm

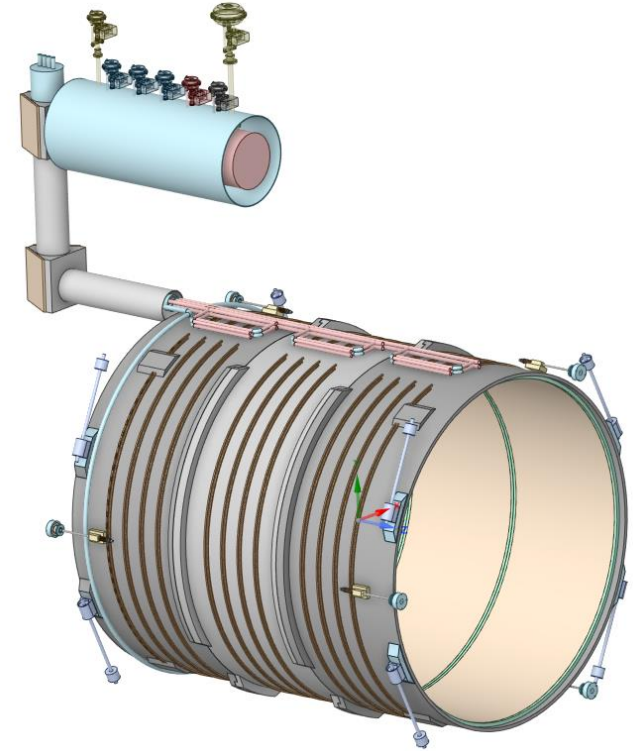
Parameter	Value	Comment
Central Field $B_0$	2.0 T	
Lowest operating field	0.5 T	
Field Uniformity in FFA	12.5 % $\pm 100$ cm around center 80 cm radius	<b>Magnetic Field Properties</b>
Projectivity in RICH Area	< 0.1 (mrad@30GeV/c) < 10 T/A/mm <sup>2</sup> From Z = 180 cm to 280 cm	

Parameter	Value	Comment
B5300 (B @ Z= -5300 mm)	< 10 G	<b>Stray field requirement is based on IR magnet location</b>
B7400 (B @ Z= 7400 mm)	< 10 G	
B3400 (B @ R= 3400 mm)	< 10 G	



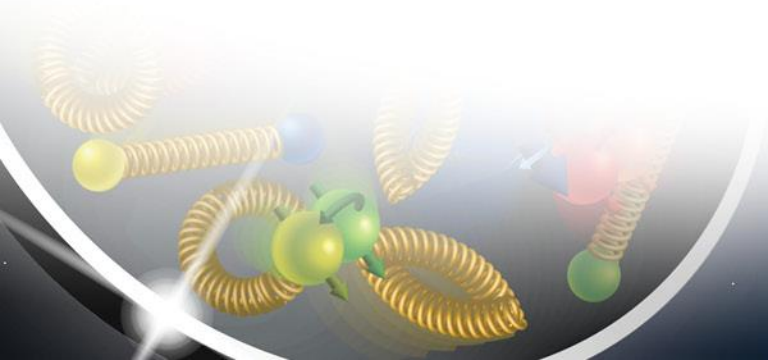
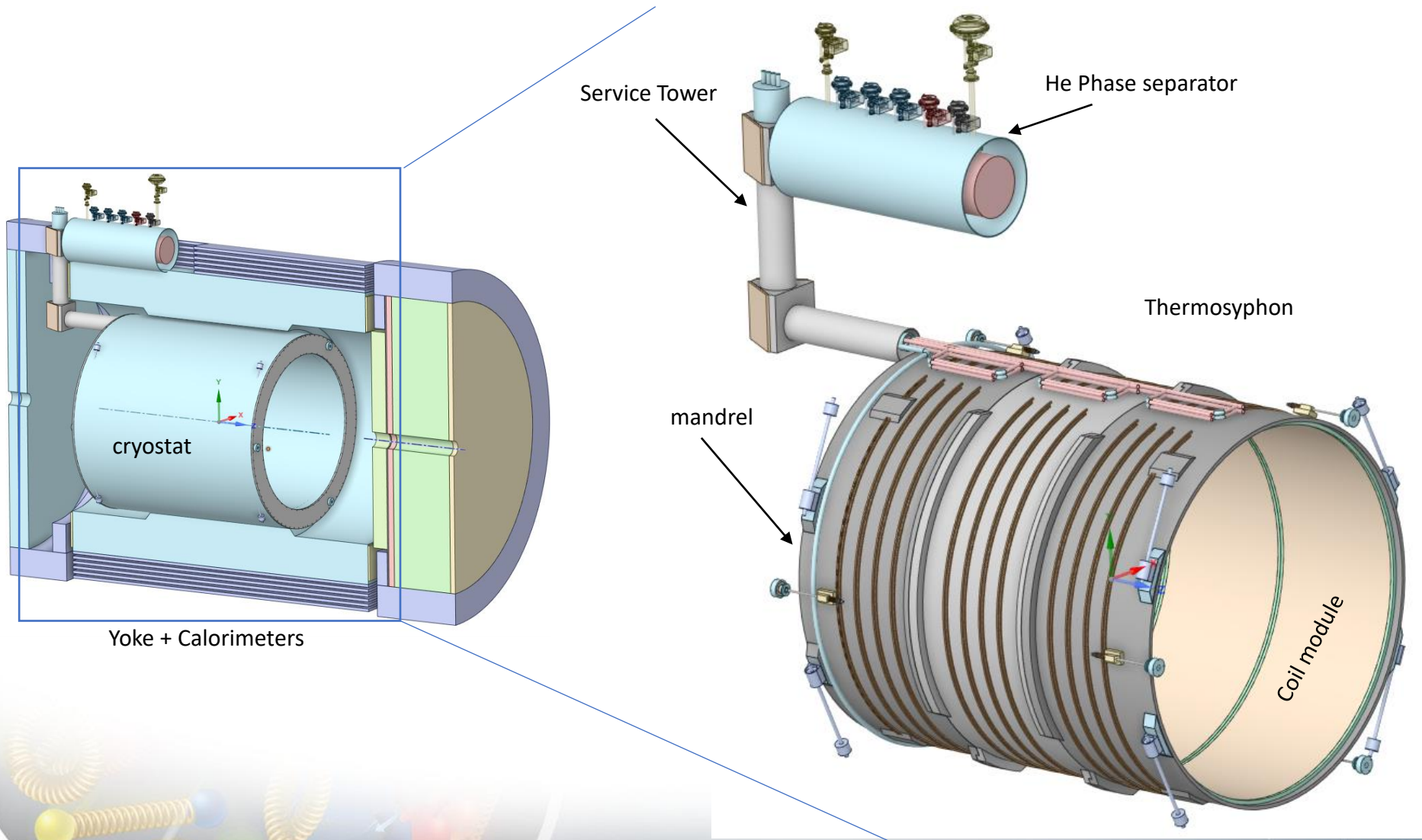
# Status of the Design

MAGNETIC Design	COMPLETED
CONDUCTOR Design	COMPLETED
MECHANICAL Design	FINALIZING
CRYOGENICS Design	FINALIZING
DEFAULT SCENARIO	FINALIZING
DRAWINGS	FINALIZING

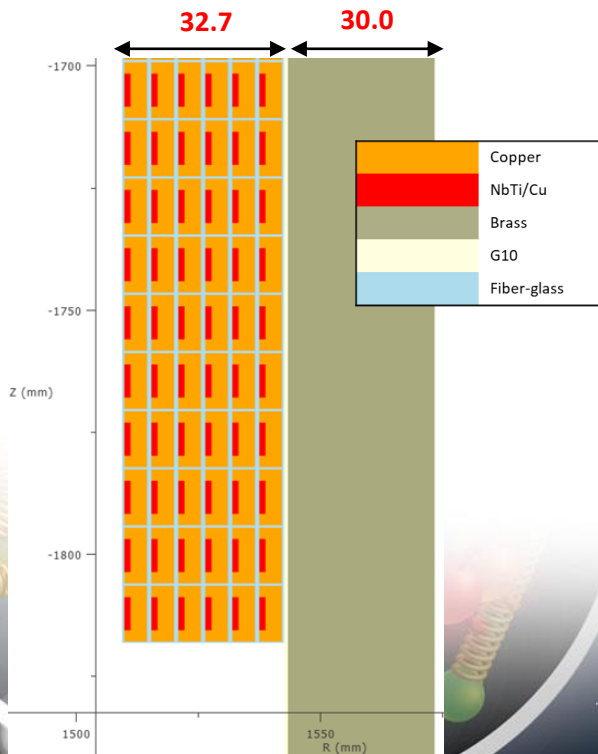
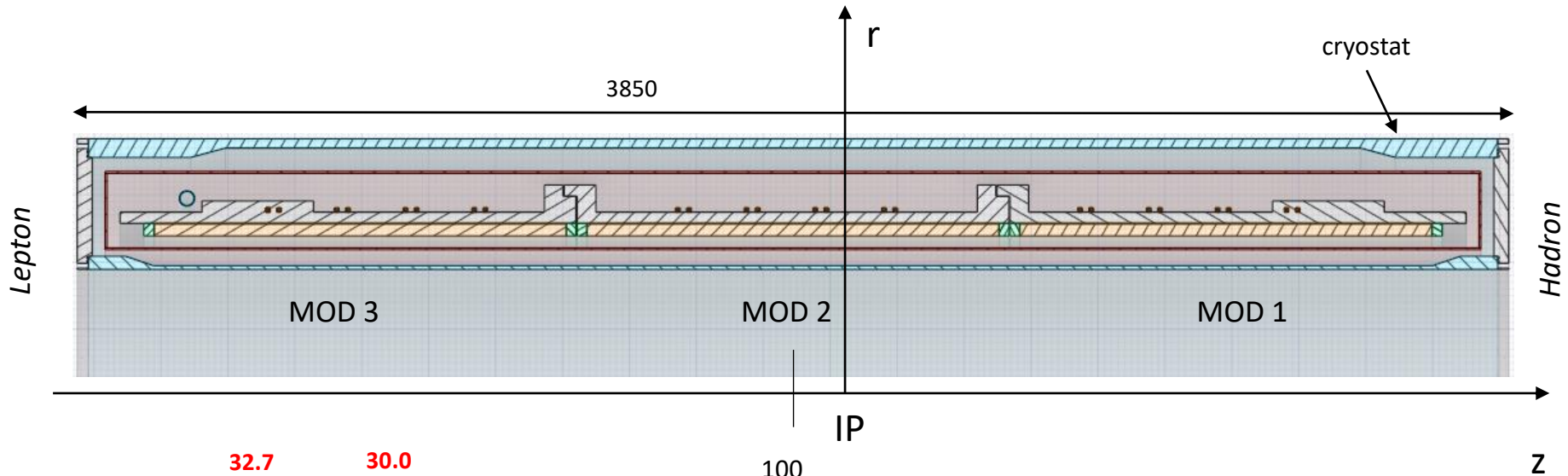


**We are on schedule for the DOE Review in Nov. 2023**

# Status of the Design



# Magnet Design – Cold Mass



- 3 modules
- 6 layers
- 1668 turn

**Cold mass average thickness = 63.7 mm**

# Interaction Length Limits

## TRANSPARENCY

*for the transverse momentum*

Mean range

$$\Delta x = \int 1/S(E)dE$$

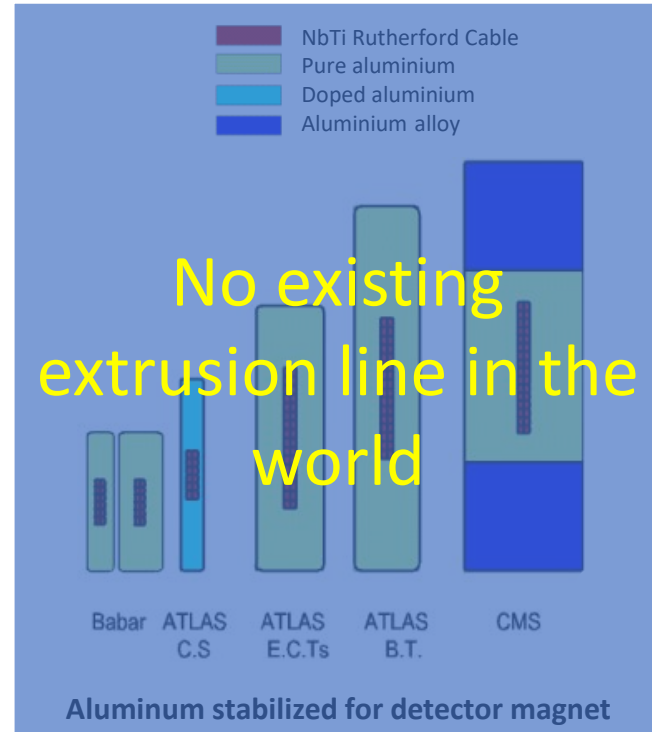
$S(E) = dE/dx \propto \rho Z/A$  (Bethe equation)

Stabilizer material for conductor

Copper  $\rho \frac{Z}{A} = 4124 \frac{kg}{m^3}$

Aluminium  $\rho \frac{Z}{A} = 1350 \frac{kg}{m^3}$

3x less stopping power with the same coils dimensions and NbTi fraction in the cable if Aluminum is used



Conclusions from Workshop on Superconducting Detector Magnets @ CERN, 12/14 Sept 2022

**We will not be able to use Aluminum stabilized conductors for long long time**

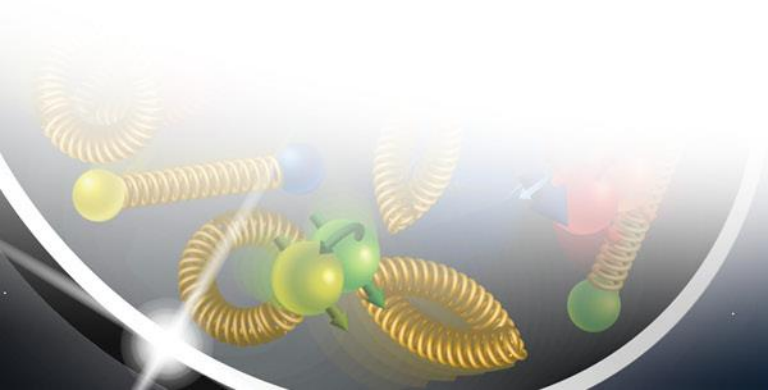


# Interaction Length Limits

Material	Thickness/Nuclear interaction length			
	BaBAR 1.4 T	ATHENA SOCRATE	Marco 1.5 T (4 layers)	Marco 2T (6 layers)
Al	0.382	0.650	0.113	0.113
Cu	0.011	0.170	0.114	0.166
SS/Brass	0.000	0.417	0.136	0.181
NbTi	0.007	0.020	0.003	0.008
G10			0.009	0.028
<b>Total</b>	<b>0.400</b>	<b>1.258</b>	<b>0.372</b>	<b>0.468</b>

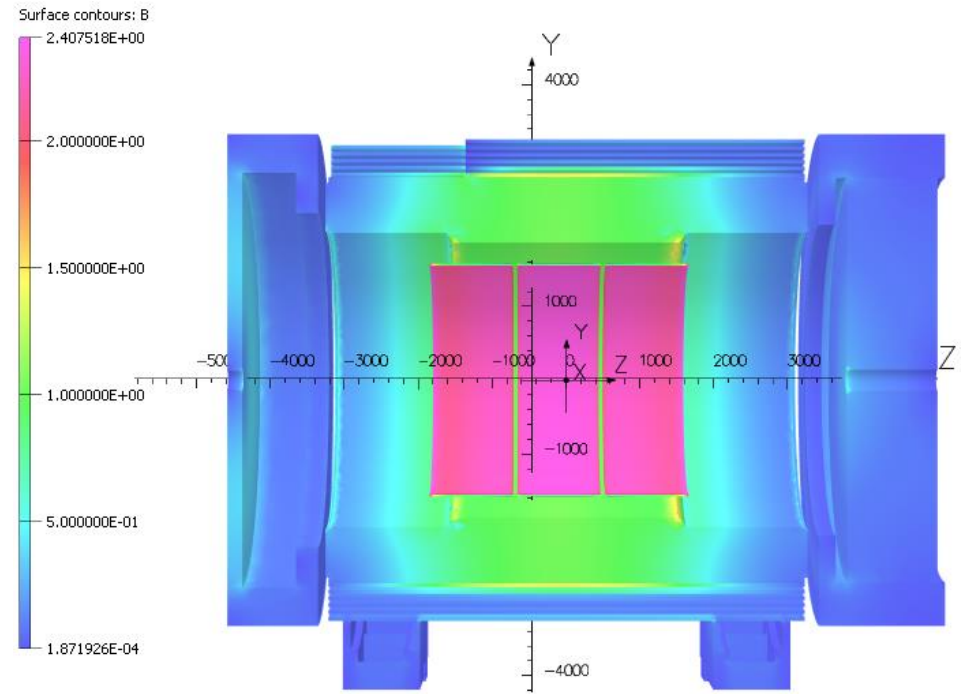
*By R. Rajput-Ghoshal*

**We can have a magnet working at 2T with essentially the same transparency as BaBAR**



# Magnetic Design Results

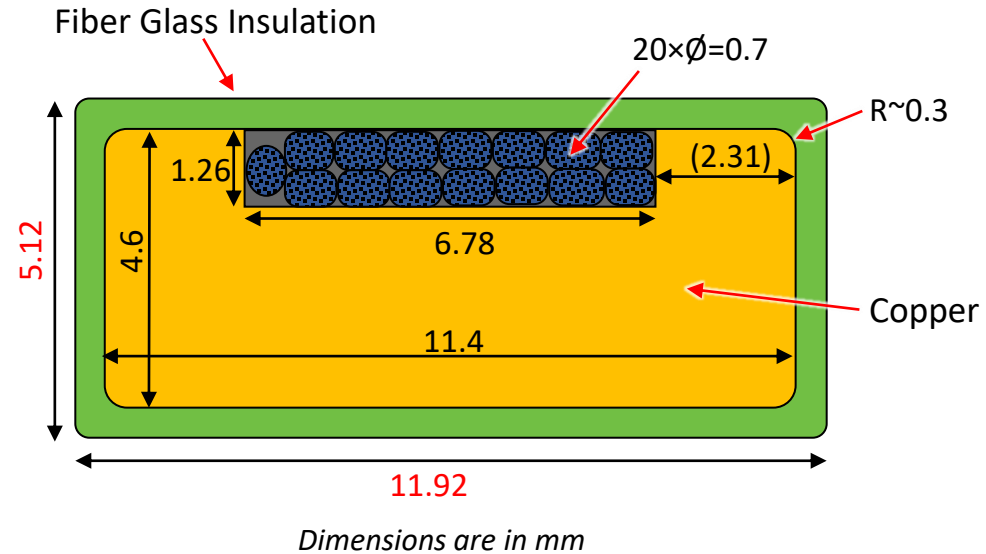
Parameter	V7.6.2.2.10 3D	Units
<b>Current</b>	<b>3924</b>	<b>A</b>
# turns	1668	
<b>B<sub>0</sub></b>	<b>2.000</b>	<b>T</b>
<b>Homogeneity</b>	<b>12.7</b>	<b>%</b>
<b>Projectivity</b>	<b>3.28</b>	<b>Tmm<sup>2</sup>/A</b>
Bpeak (MOD 3)	2.671	T
<b>Energy</b>	<b>45.010</b>	<b>MJ</b>
Inductance	5.846	H
Fz MOD 1	11.88	MN
Fz MOD 2	57.5	kN
Fz MOD 3	-11.97	MN
<b>Fz tot</b>	<b>-32.4</b>	<b>kN</b>
<b>Fr Tot</b>	<b>112</b>	<b>N</b>
<b>B5300</b>	<b>15.3</b>	<b>G</b>
<b>B7200</b>	<b>10.9</b>	<b>G</b>
B3400	2.4	G



Fringe field will be compensated with local shielding around the focusing magnet

# Conductor Design

	Parameters	Values	Units
Strand	Strand diameter	0.7	mm
	Cu/NbTi	1.3	
	Ic @ 2.6T & 4.7K	> 680	A
	Filament diameter	< 30	μm
	RRR Cu	> 80	
Cable	NbTi strands	20	
	Transposition pitch	50	mm
Channel	RRR Cu	> 100	
	Copper section (Final)	43.7	mm <sup>2</sup>
Conductor	Nominal current	3924	A
	RRR conductor	> 100	
	Temp. margin @ 2.6T & 4.7K	2.5	K
	Hot spot Temperature	71.4	K
	$\sigma_{0.2\%}$ @ 293K	> 165	MPa
	Unit length	1.05	km
	Total length	18.9	km

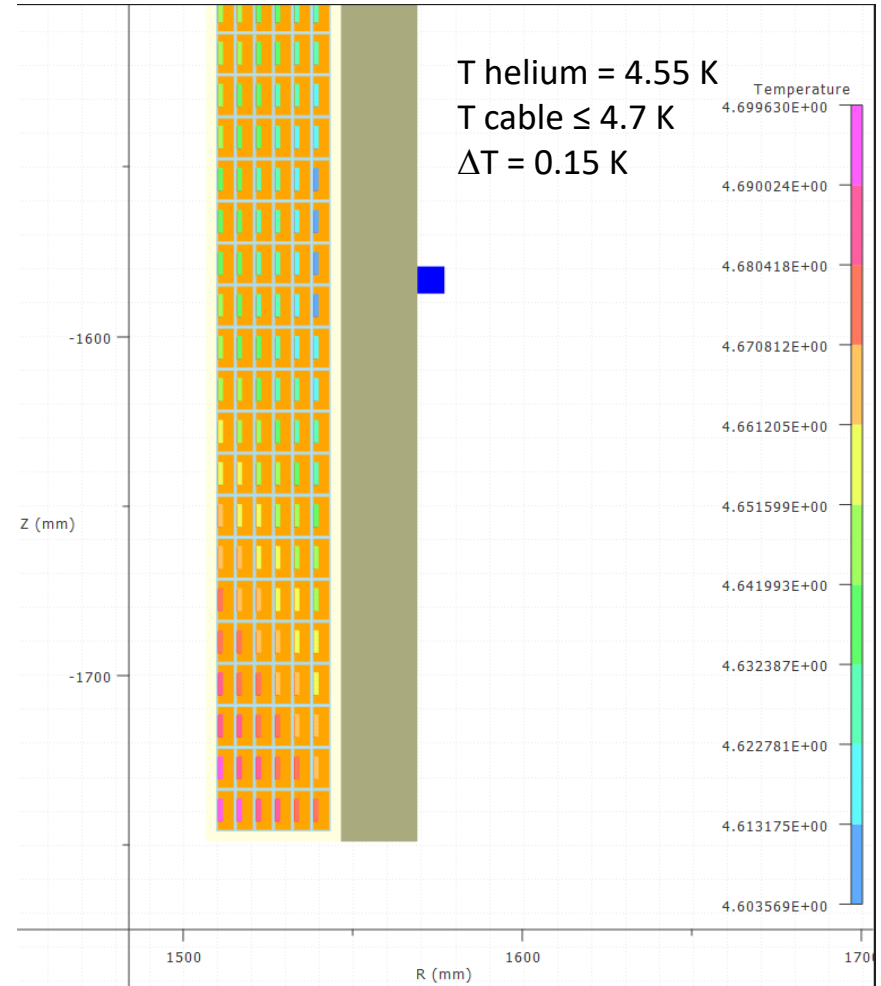
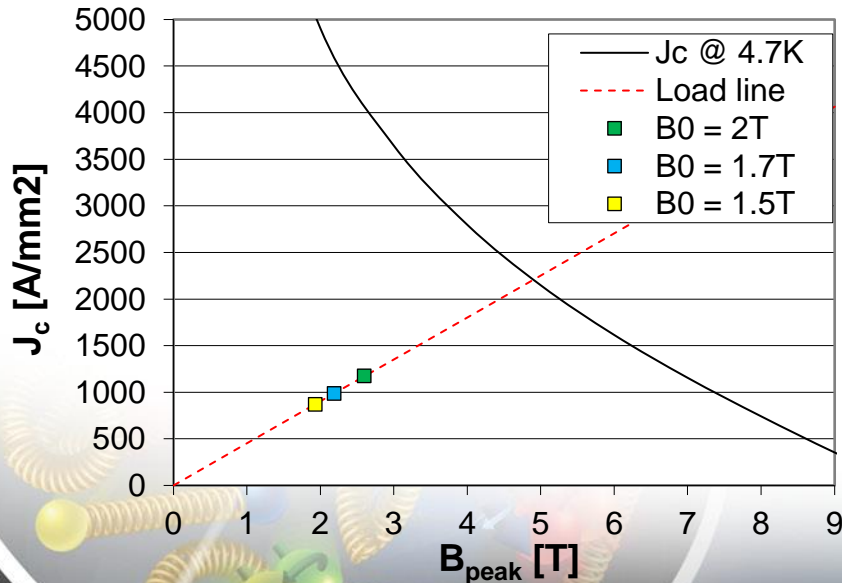


*Order of conductor samples put in place based on these specifications*

- **First samples in October 2023**
- **Contacting labs to test them**

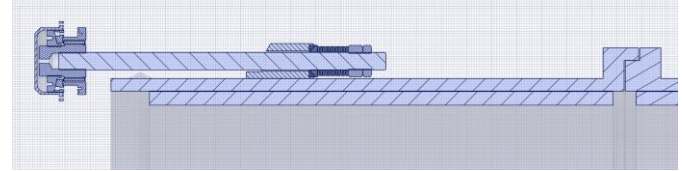
# Conductor Margins

$B_0$	1.5 T	1.7 T	2.0 T	Units
Current	2900	3296	3924	A
$B_{peak}$	1.925	2.187	2.602	T
<b>Temp. margin</b>	<b>3.1</b>	<b>2.9</b>	<b>2.5</b>	<b>K</b>
<b>Enthalpy margin</b>			<b>7.4</b>	<b>kJ/m<sup>3</sup></b>
Load line margin	60.6	55.3	46.8	%
$I / I_c(T_m, B_{peak})$	17.3	21.3	28.8	%



**CMS works at 1.8K of margin**

# Mechanical Design

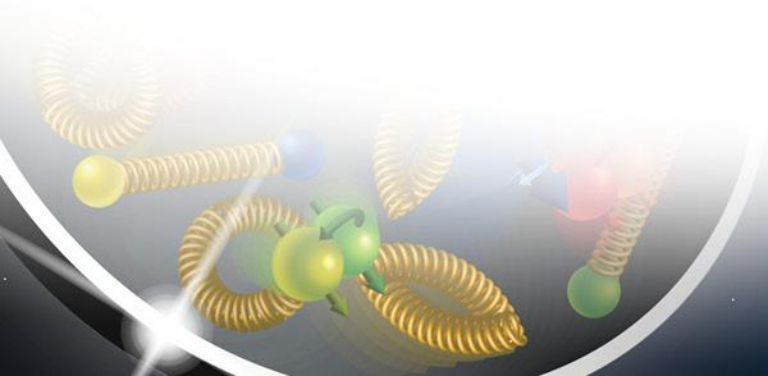
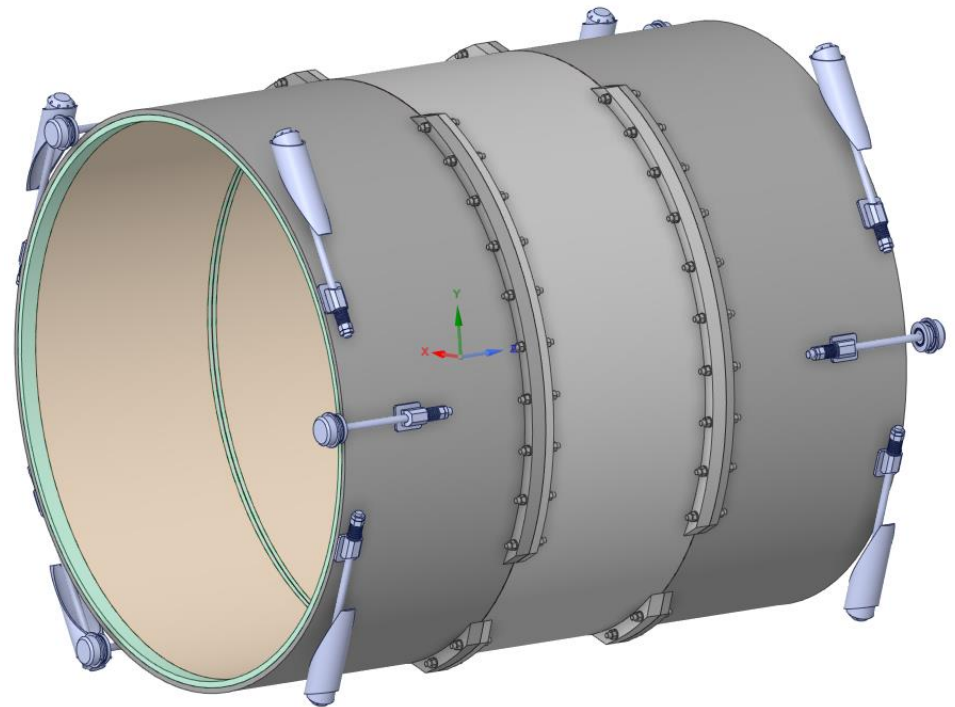


## Finalizing the detailed design

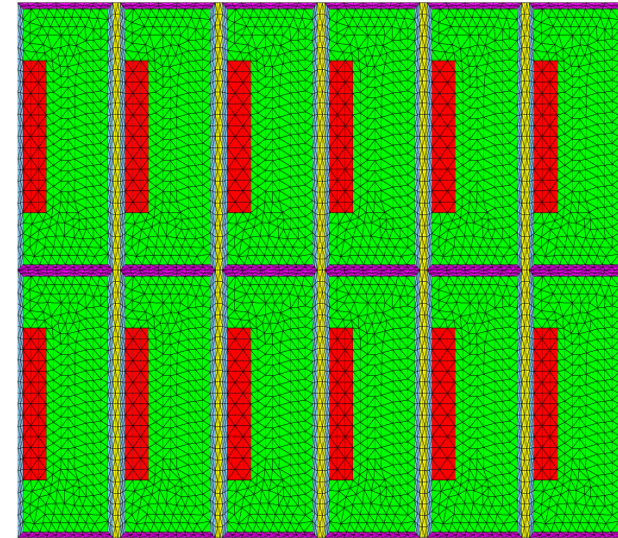
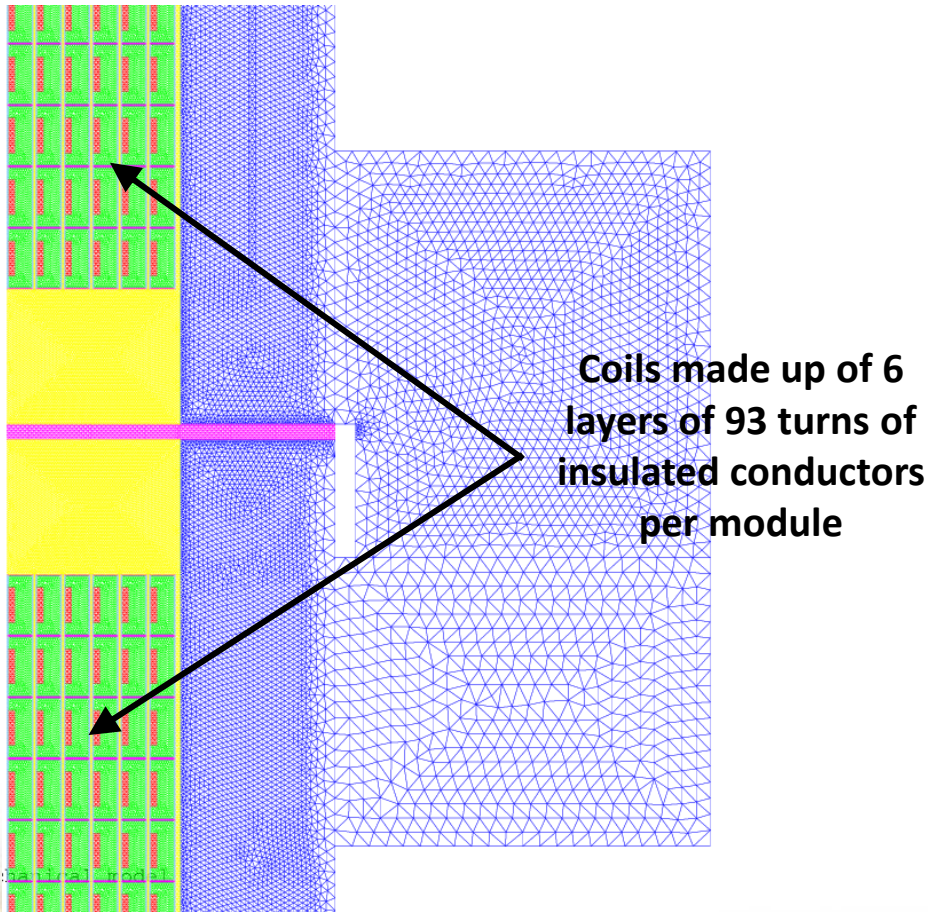
- Mandrel design completed
- Tie-rods finalizing
- 2D Model ready
- 3D Model finalizing

## MECH Design includes

- Nominal CASE
- How to transport the magnet
- Tolerances



# Magnetic Design 2D Results

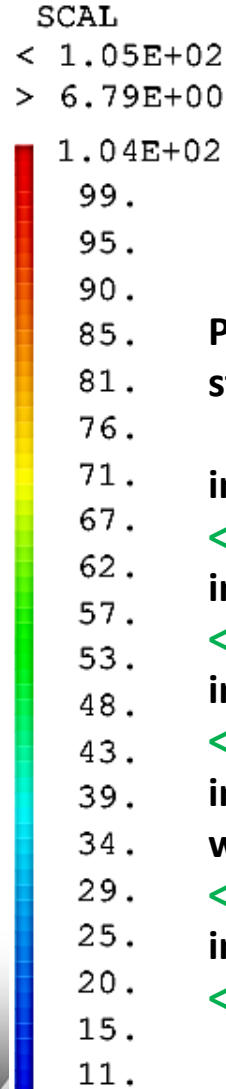
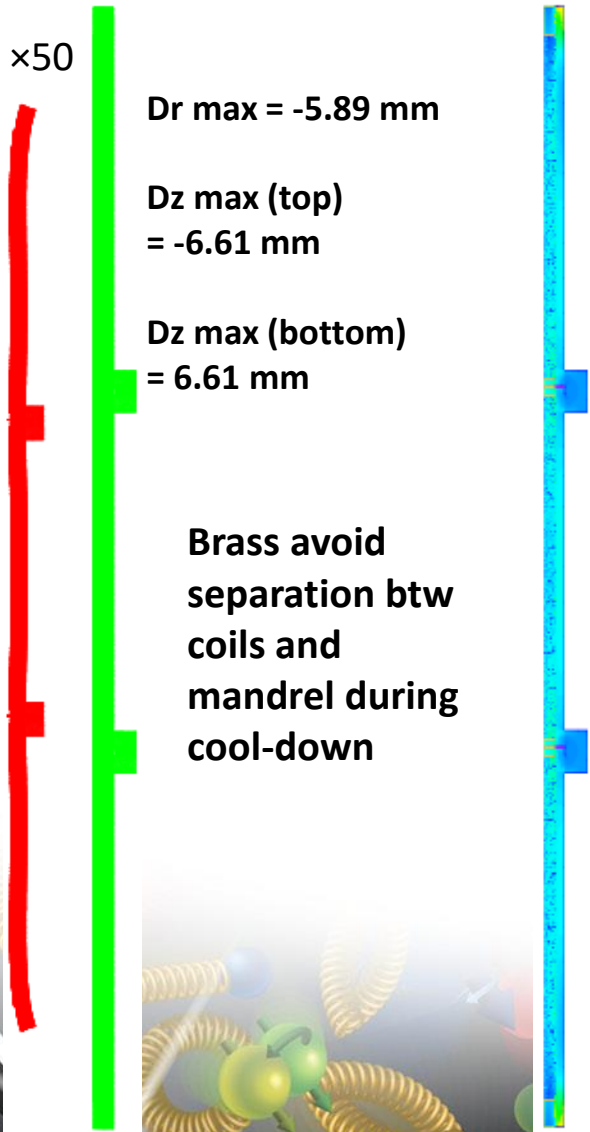


Each insulated conductor is composed of:

- Superconducting cable (in red) where magnetic forces are calculated for energization simulation
- Cu stabilizer (in green)
- Horizontal (in pink) and vertical (in blue) conductor insulation made of glass fiber

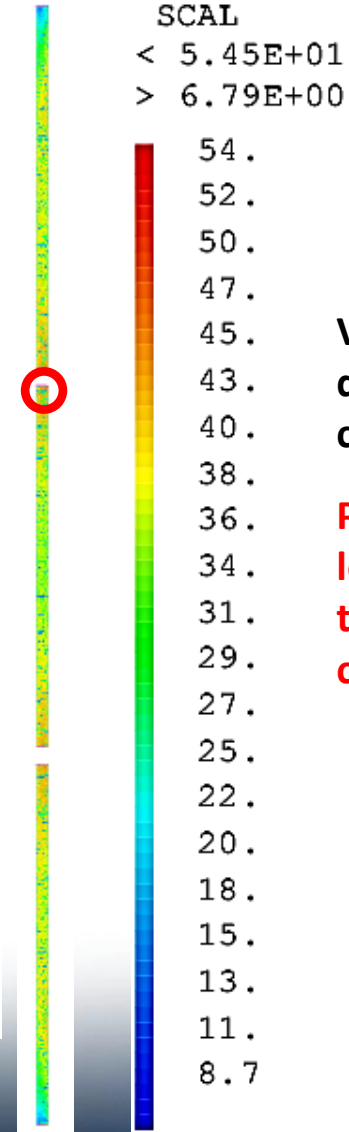
# Magnetic Design 2D Results

## Deflection



Peak Von Mises stress (MPa):

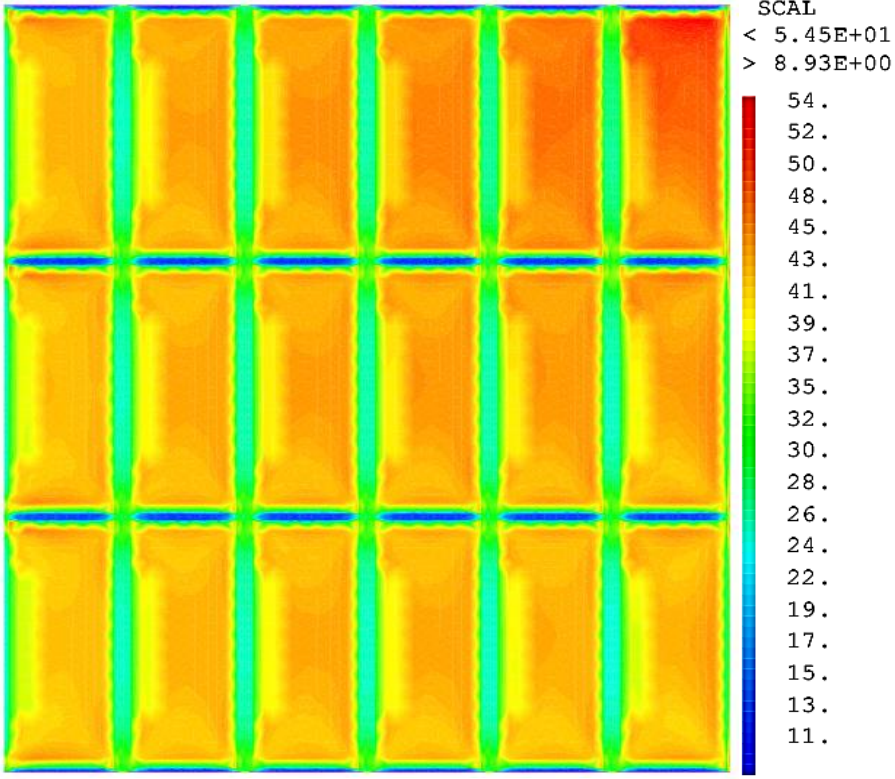
- in coils = 55 < 133
- in ground ins. = 53 < 198
- in coil wedges = 84 < 198
- in inter-module wedges = 54 < 198
- in structure = 105 < 345



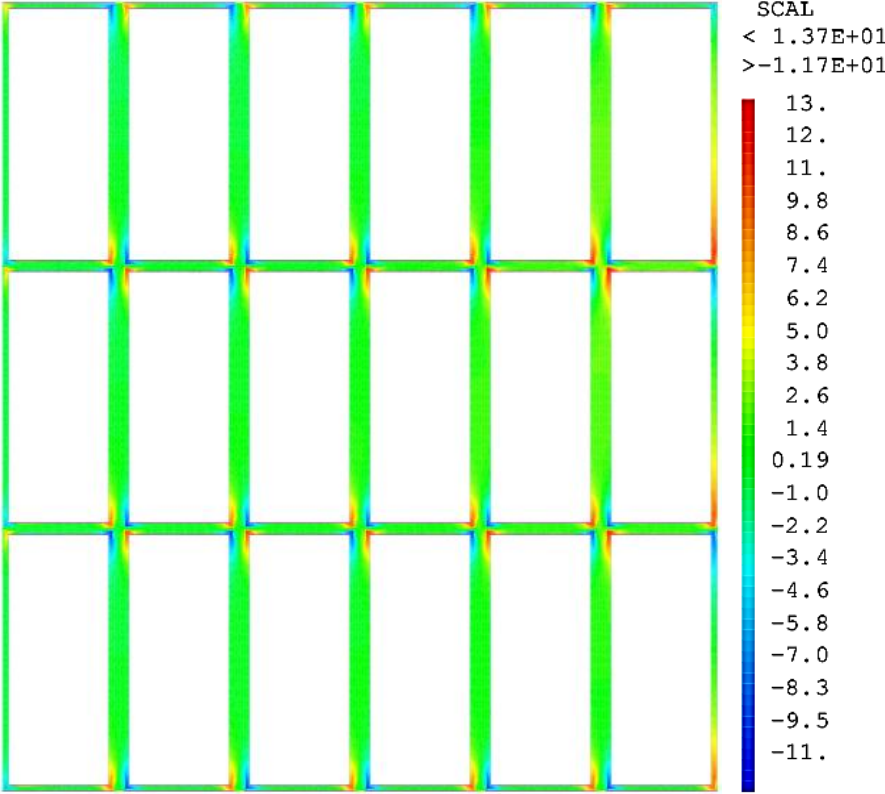
Von Mises stress distribution in coils (MPa)

Peak stress localized at the top side of the central coil

# Magnetic Design 2D Results



**Peak Von Mises stress (MPa):**  
in supercond. cable = 50 < 150  
in Cu stabilizer = 55 < 133  
in glass fiber ins. = 49 < 198

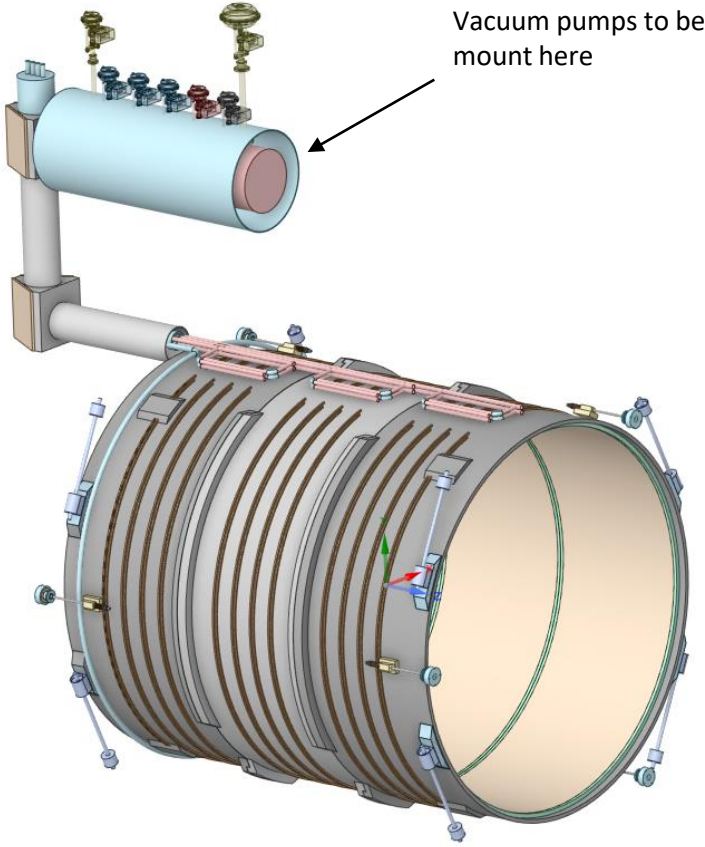


**Peak Sigma RZ stress (MPa) in  
conductor insulation:**  
14 = 14



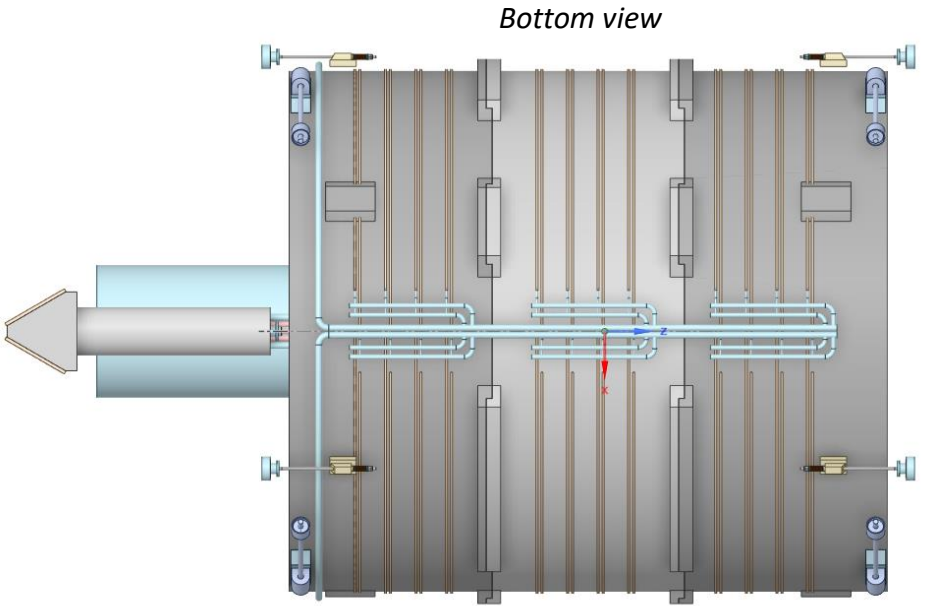


# Cryogenics Design

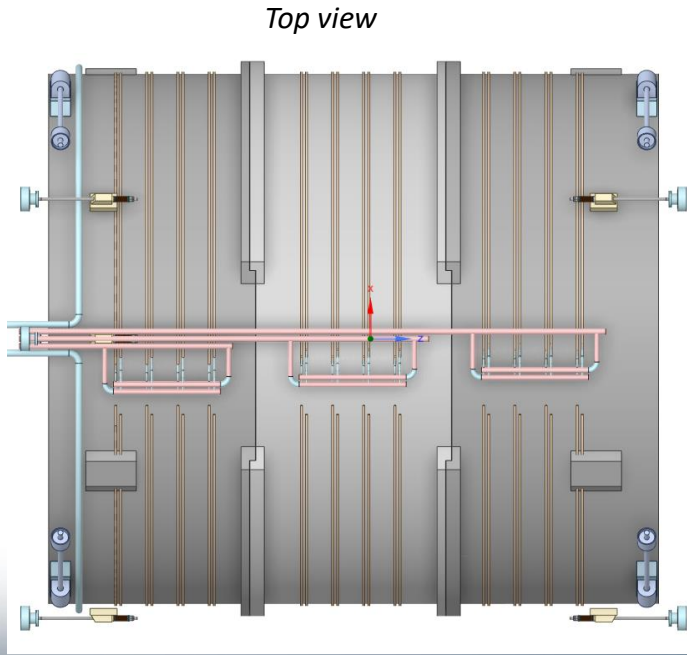


Vacuum pumps to be mount here

- 2 thermosiphons (main + spare)
- Phase separator design finalizing
- Thermal screen design finalizing



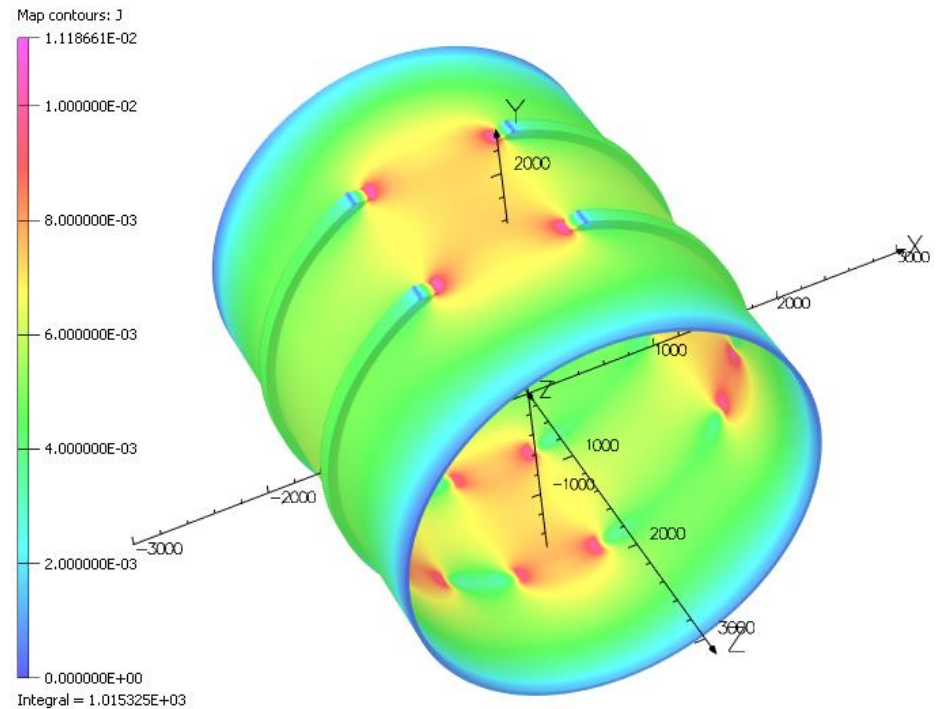
Bottom view



Top view

# Ramp-up / Ramp-down

Parameter	V7.6.2.2.10	Units
Current	3924	A
Inductance	5.846	H
<b>Ramp</b>	<b>1</b>	<b>A/s</b>
Power	3.642	W
Eddy current	-1015.32	A
R mandrel ( $P/I^2$ )	3.516	$\mu\Omega$
M mandrel	3.570	mH
L mandrel*	2.346	$\mu\text{H}$
k	0.964	



**Magnet can be ramped-up/down to full field at 1 A/s → 1h15 min**

**Full 3D Thermal Analysis ongoing to know how long it takes to cool it down  
(estimated 8 days from room temperature)**

# Other On-going Activities

## Tolerances

→ Monte Carlo simulation to study the effect of tolerances and the robustness of the design

## Protection

→ Finalizing the QUENCH simulations  
→ Finalizing the protection circuits  
→ Expected hot-spot temperature < 100 K

## Sensors

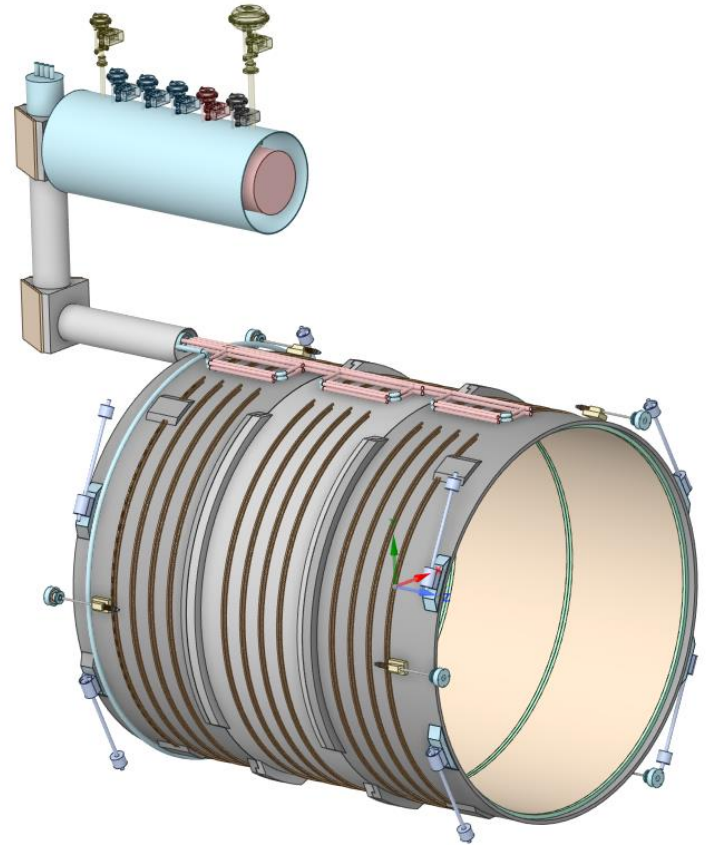
→ List completed  
→ Finalizing the positions

## FMEA Analysis

→ Ongoing for all components

## Drawings

→ Updated daily



# Conclusions

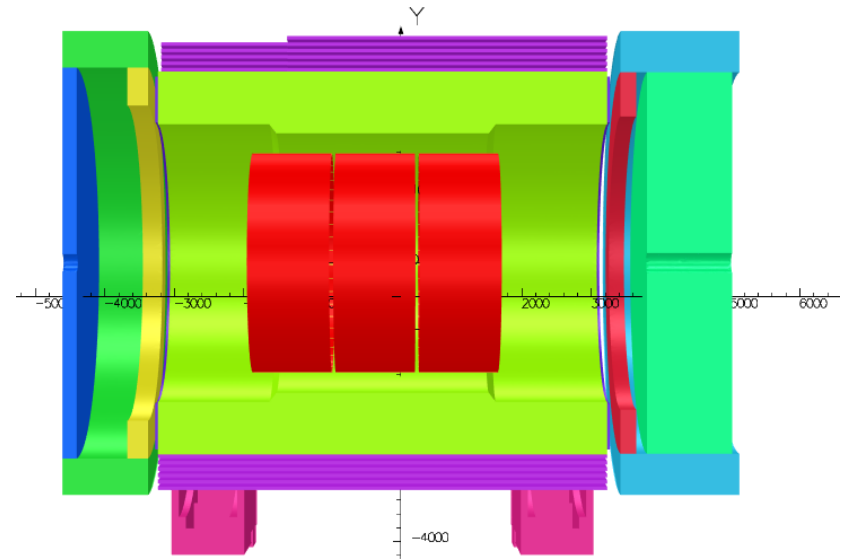
## Superconducting Detector Solenoid

3.5 m long coil, 2.84 m room temperature  
bore diameter  
2 T on-axis field

Conductor sample in production

Robust mechanical design

Magnet design is full of redundancies to  
make it work for more than 30 years



Working hard to deliver the design for the Final Review in Oct 5/6!



# How we work

- Collaboration of Jefferson Lab, CEA Saclay and Brookhaven National Lab
- 30% Design done as in-kind contribution by CEA Saclay in collaboration with Jefferson Lab Magnet Group
- BNL provides subject matter expert information on infrastructure and integration
- 60% design done as contract with CEA Saclay augmented with Jefferson Lab work and further in-kind contributions of CEA Saclay
- 90% design work is in progress in collaboration with CEA Saclay
- Expectation is that vendor contract may follow similar pattern for vendor oversight.
- Further discussions ongoing on international engagement on magnet construction phase.
- **October 5/6 Final Review**