

Magnets Working Group Meeting Notes

Magnet Working Group

30 March 2023

Indico Link: <https://indico.cern.ch/event/1240043/>

News

- Kick off meeting for MuC on 28/03/23 -> Please check the slides from the indico link MuCol kick-off: <https://indico.cern.ch/event/1219912/>
- For an upcoming meeting, we could report on the cooling solenoids
- Upcoming annual meeting
- Topics for upcoming meetings
 - Topic: conductors
 - Draft HTS procurement spec (link from 2 meetings ago)
 - Topic: performance limits of collider magnets
 - Topic: radiation protection, discussing what areas are going to be active
 - Topic: moving magnets by roughly 15cm up/down in machine

Annual Meeting Agenda

- Give a presentation in the annual meeting - for the accelerator, collider, cooling etc. what technology options do we have available (mini-report)? And what do we want to do for those options → **Send Luca ideas for preparation.**

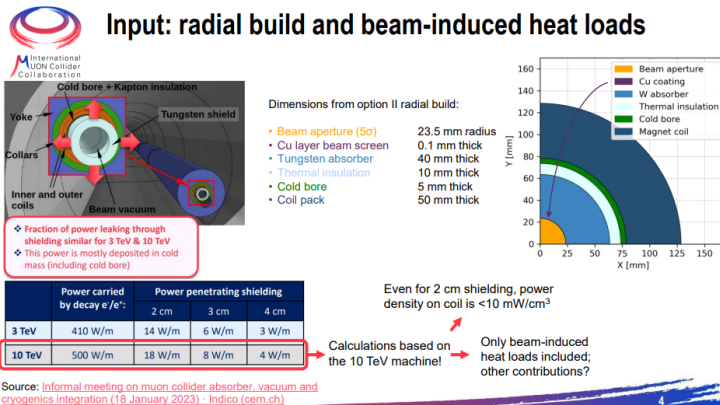
Presentations

- I. Cryogenics options for future accelerators
- II. Solenoids for 6D Cooling

I. Cryogenics options for future accelerators (focused on the collider) – Dr Patricia Tavares Coutinho Borges De Sousa

Some key notes

- a) Radial build for Dipole (and quadrupole) magnets in arc are taking shape
- b) Input radial build diagram (see slide pasted below)
 - a. Absorber can be 2 to 4 cm based on previous meetings



- c) Heat loads (steady-state)
 - a. Heat inleaks: thermal radiations, conduction via supports
 - b. Beam induced: beam decay, image charge, synchrotron radiation, etc.
 - i. Decay (500 W/m)
 - c. Resistive heating (magnet splices, current leads) – yet to be defined!
- d) Final heat load to consider on absorber essentially just from beam decay: 500 W/m
- e) **Heat load estimation – assumptions made:**
 - a. Cold mass temperatures: 2, 4.5, 10, 20 K
 - b. Heat load to cold mass (dependent on absorber thickness and cold mass temperature)
 - i. See slides for detailed specs how each heat load defined in c) is calculated
 - c. Absorber temperature: 80 to 300 K
 - d. Heat load to absorber (independent of absorber geometry): 500 W/m
 - e. External thermal shield around cold mass temperature: 80 K
- f) See slides 8 and 9 (9 includes a heat intercept option) for detailed plots of the heat loads to the cold mass as a function of the varied cold mass temperature and absorber temperature from the various sources. Some key takeaways
 - a. Heat load to coil/cold mass largely independent of coil/cold mass temperature, however, the effort to extract the heat will heavily depend on this temperature!
 - b. Lower absorber temperature is better, reaching down to a minimum of roughly 5 W/m (at absorber temperature 80 K)
 - c. With a heat intercept, the minimum 5 W/m roughly unchanged, but at higher absorber temperatures heat load much less (~half).
- g) How does heat load transfer to operating electric power (assume that 25 MW gets allocated to the collider ring)
 - a. 25 MW for the collider translates to 2.5kW/m -> we aim to stay at or below this!
- h) Increasing the Coil temperature and the absorber temperature helps go toward the target of < 2.5kW/m
- i) Adding a heat intercept between coil and absorber improves things
- j) Fluid Options (**see slides** for advantages/disadvantages for each):
 - a. absorber cooling - for given absorber temps:
 - i. ~300K – single-phase water
 - ii. 250K – two phase CO₂
 - iii. 100K – two phase N₂
 - iv. 80K – two phase N₂
 - b. Cold mass cooling – for given cold mass temps:
 - i. 20K – two phase H₂
 - ii. 10K – supercritical He
 - iii. 4.5-5.5K – supercritical He
 - iv. 2K – He II
- k) Distribution losses – see slides for rough estimation of these losses

- l) Summary and combination of all requirements
 - a. To stay below 2.5 kW/m, absorber temperature must be above 230 K
- m) **Combining requirements** from both energy consumption and what is feasible at absorber and coil levels:
 - a. Absorber temperature ≥ 250 K
 - b. Coil temperature ≥ 4.5 K
 - c. Power consumption ≤ 2.5 kW/m

Some questions and comments

- Reducing absorber thickness from 4 cm to 3 cm, heat load doubles, but heat conduction from support reduced only by 30 %
- [LB] – power allotted for collider ring (25 MW) needs to be re-looked at (based on an initial power estimation for MuC of 300 MW). [DS] – “in the initial estimations, got 35 MW for the cooling of the collider ring”
 - ‘You have to compute in the power calculation, must include distribution loss multiplied by copper temperature’ – LB ...*
- Coil and cold mass distinction – assumed these temperatures are temperature levels in the cooling pipe... but if cooling tube is far away in yoke maybe need to consider coil temp could be a bit higher.
- Absorber material is Tungsten. consider other materials with better heat conduction ex. with water.

II. Initial Evaluations of the Cooling Solenoids for the Rectilinear 6D Cooling Channel –

Jonathan Pavan, Dr Siara Fabbri

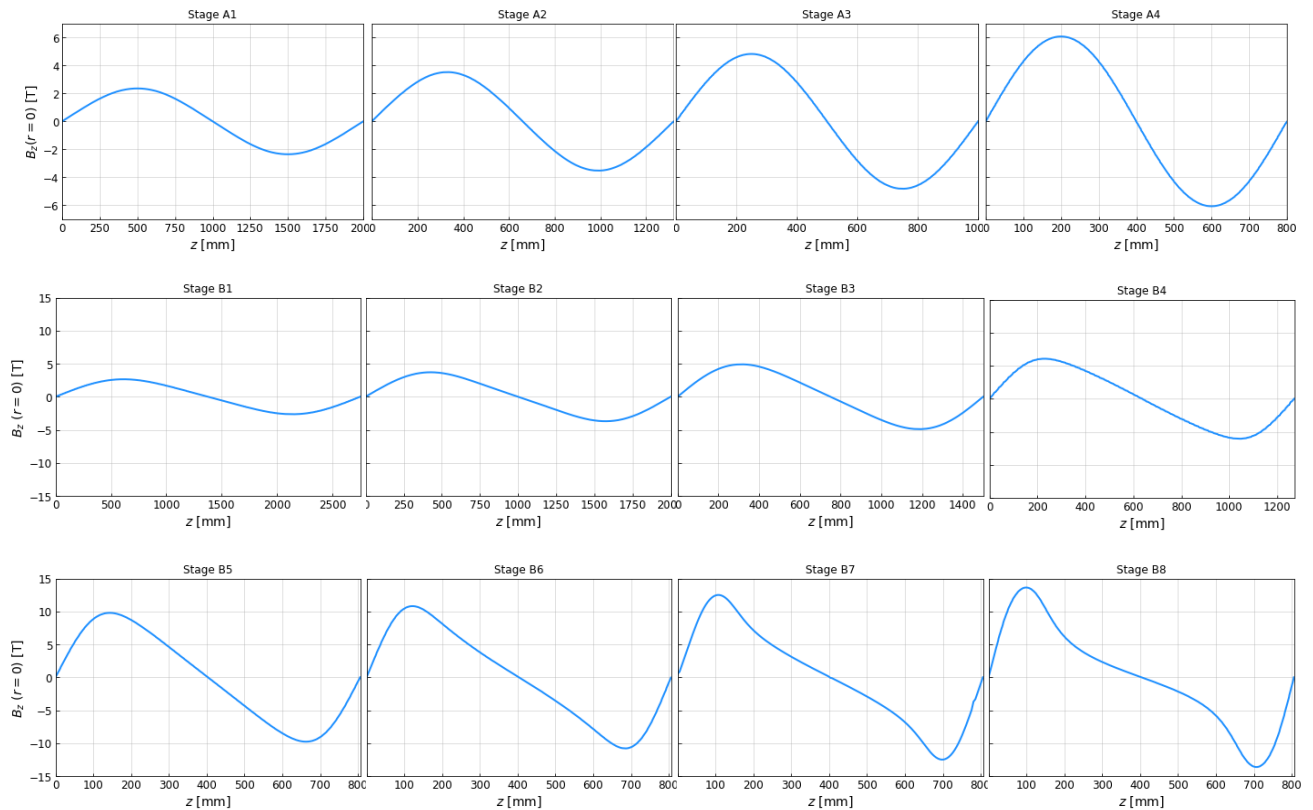
Some key notes

- a) Goal of study presented: Simulate and characterize the cooling solenoid magnets based on geometries and parameters from US MAP study
- b) Simulation Study:
 - Methods: COMSOL, validated against analytic equations and supplied G4beamline fieldmaps
 - Parameters computed: magnetic fields, stray fields, inductance and stored energy, stresses, forces, mechanical props (mass of coils)
 - Computation types: single coil types, single cells, cell in a lattice
 - See slides for more details on mesh and computation...
- c) Overview of cooling stages as provided by US MAP study:
 - 12 unique stages: 4 before bunch recombination (A1 to A4), 8 after bunch recombination (B1 to B8)
 - Each stage has a unique number of a repeating cell type
 - Each cell type consists of at least 2 to 6 solenoids, symmetric with opposite polarity.
 - **Fields on axis: 2 to 14 T**
 - Cell Lengths: 0.8 to 2.7 m
 - Total length of all Stages: ~ 1 km

- 18 unique coil types
 - 2 to 6 coils per cell
 - Inner bore diameter from 90 mm to 1540 mm
 - Lengths from 80 mm to 210 mm
 - Current densities from 63 to 220 A/mm²

- Total number of solenoids: 2432

d) On axis fields:



e) Key takeaway points:

- Very high possible self inductance in large coils such as those in B1 (Ex. w/ REBCO 12x0.11mm tape, self inductance in single coil around 6000 H)
- Largest single coil mass: B1 coil – 3567 kg.
- Very high total magnetic energy in some coils (B1 single coil – 27 MJ). For reference, LHC dipoles store 7 MJ.
- Very high peak fields at the conductor (above 17 T, max 18.9T in single cell B6) -> gets difficult for Nb3Sn.
- Large stray fields.
- Hoop stresses up to 336 MPa (above 150 MPa requires reinforcement), radial stresses which are in tension (this is a problem), large longitudinal forces (peak 36.8 MN...).

f) What this study didn't include:

- A more complicated mechanical structure
- Matching sections b/w stages
- Iron, realistic space requirements, ...
- Dipole magnets.

Some key questions and comments (from later discussions with Chris Rogers)

- If iterating the magnet design, just need to match on axis field profile (and analyze the harmonics)
- The demonstrator will likely be B2 or B3 (B7 maybe too complicated)
- Next steps – iterate the design process around a radial build (RF design Alexej.grudiev@cern.ch, shielding, insulation) and the magnet parameters -> explore the limits of overlap between optimal/desirable magnet parameters and the desired on axis field profile.