



Neutron Sources

Neutron Field Theory, moderation and response function

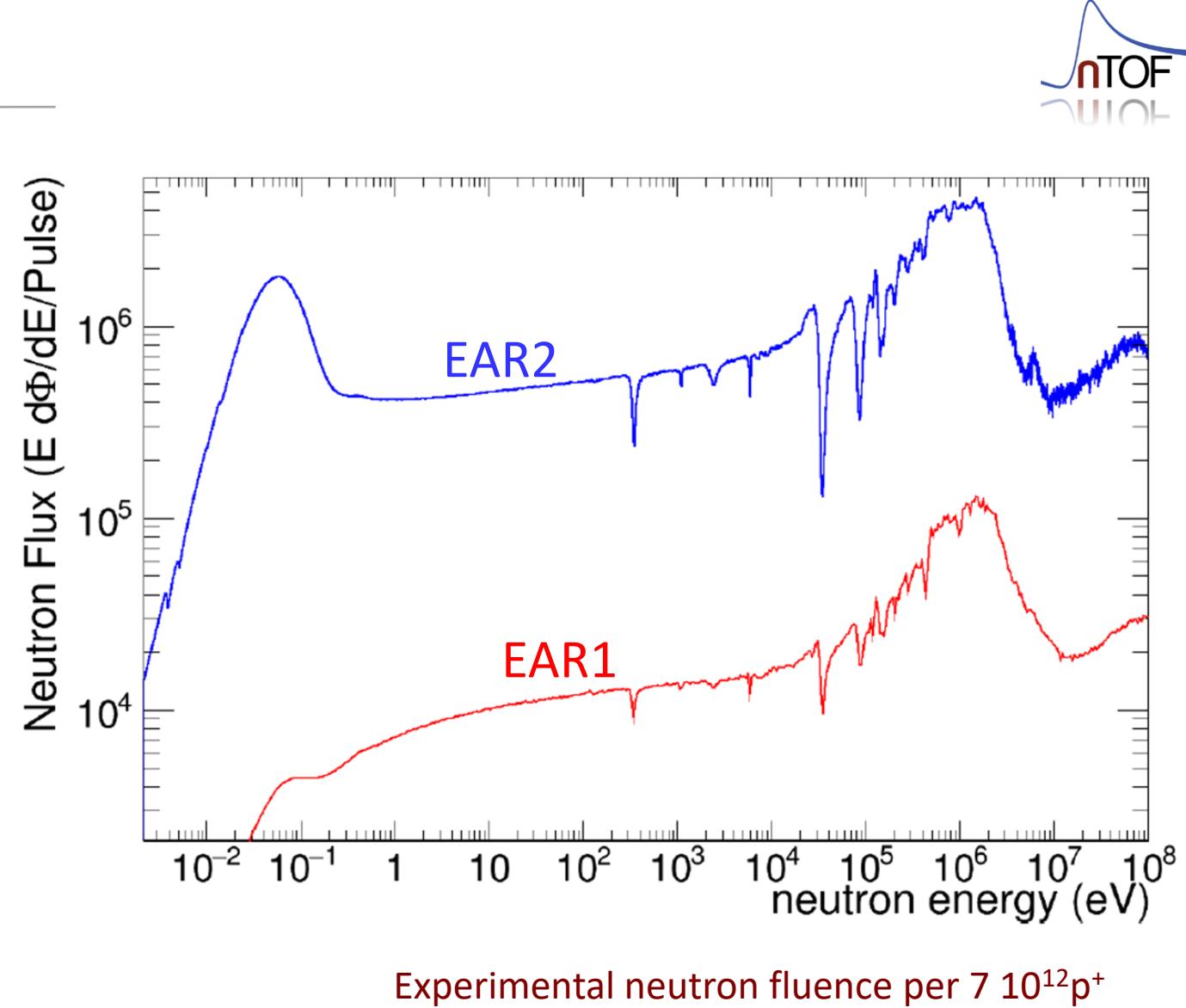
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Outline

- Neutron sources
- Slowing down of neutrons
- Neutron Diffusion
- Flux – Fluence – Current
 - Isolethargic
- Resolution function
 - Energy-Time relation
 - Effective Neutron path
- Spallation target optimization



Neutron Sources

Through Reactions:

With low Binding energy of the last neutron (Neutron Separation Energy)

- light nuclei: typically small apart from α -composed atoms
- intermediate: 7-10 MeV
- heavy: 6-7 MeV

due to Coulomb barrier, light nuclei play the predominate rule
(at low energies)

(α, n)

- Excitation energy ~10 MeV, sometimes exothermic, or endothermic.
→ Continuous energy spectrum
e.g. ${}^9Be + \alpha \rightarrow {}^{12}C + n + 5.704 \text{ MeV}$

(d, n)

- Due to small binding energy of the deuteron (2.2 MeV) and a very highly excited compound nucleus is almost always exothermic
e.g. ${}^7Li + d \rightarrow {}^8Be + n + 15.028 \text{ MeV}$

(p, n)

- typically mono-energetic sources
e.g. ${}^7Li + p \rightarrow {}^7Be + n - 1.646 \text{ MeV}$

(γ, n)

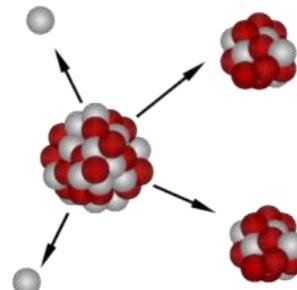
- nearly mono-energetic neutron production
e.g. ${}^9Be + \gamma \rightarrow {}^8Be + n - 1.666 \text{ MeV}$

Nucleus	Binding Energy (MeV)	Nucleus	Binding Energy (MeV)
H^2	2.225	C^{12}	18.720
H^3	6.258	C^{13}	4.937
He^3	7.719	C^{14}	8.176
He^4	20.577	N^{13}	20.326
He^5	-0.956	N^{14}	10.553
Li^6	5.663	N^{15}	10.834
Li^7	7.253	N^{16}	2.500
Li^8	2.033	O^{15}	13.222
Be^8	18.896	O^{16}	15.669
Be^9	1.665	O^{17}	4.142
Be^{10}	6.814	O^{18}	8.047
B^9	18.575	F^{18}	9.141
B^{10}	8.440	F^{19}	10.442
B^{11}	11.456	F^{20}	6.599
C^{11}	13.092		

*Binding energy of the last neutron
in light nuclei*

Neutron Sources

- **Radioactive**
 - (α, n): Ra-⁹Be, Bi-Be, Pu-Be, ...
 - (γ, n): ⁹Be (1.66 MeV), ²H(2.2 MeV) (almost mono-energetic)
- **Fission**
 - On average 2.5 ± 0.1 neutrons
- **Via Bremsstrahlung**
 - Using electron accelerators $E_{e^-} \approx 50-100 \text{ MeV}$
 - Heavy target $\rightarrow \gamma \rightarrow (\gamma, n)$ or photo-fission
- **Spallation**
 - A violent reaction of a high energy particle on a heavy target. Disintegrates the nucleus through intra-nuclear cascade emitting numerous nucleons (protons, neutrons, alpha,...)



Hadron-Nucleus interactions: basics (simplified)

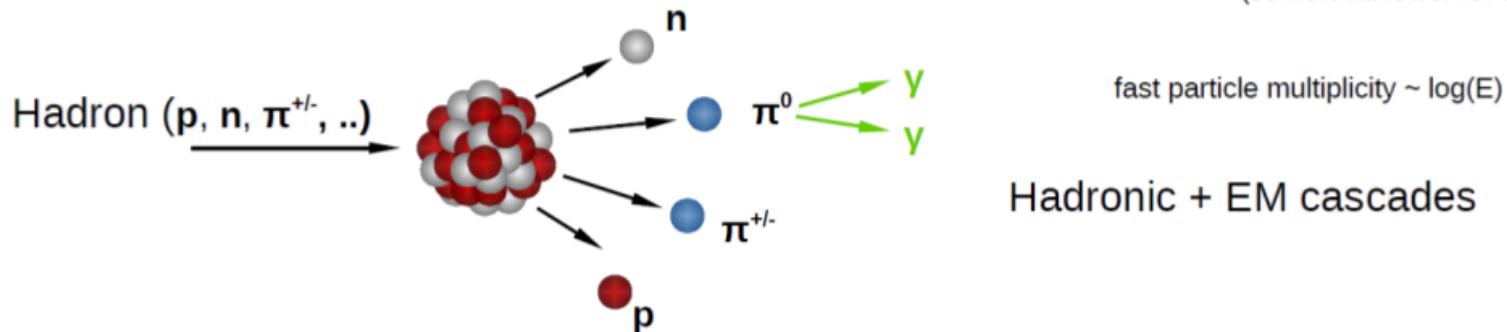
Fast stage (10^{-22} s)

Hadron interacts with nucleons: particle production possible (mainly π)

Intra-nuclear cascade of p, n, π :

- energetic particles can leave nucleus (→ forward directed)
- others can deposit energy in nucleus (→ excited state)

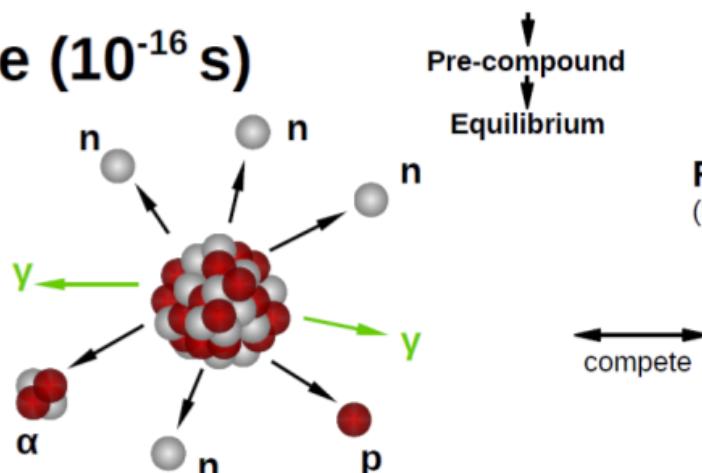
e.g. nucleon-nucleon: π production opens at 290 MeV for a free nucleon (somewhat lower for nucleons in nucleus)



Slow stage (10^{-16} s)

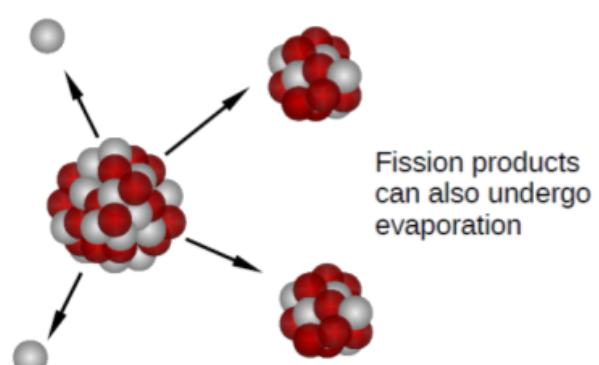
Evaporation (n, light fragments) γ -deexcitation

isotropic emission
few MeV



Fission (heavy elements)

compete

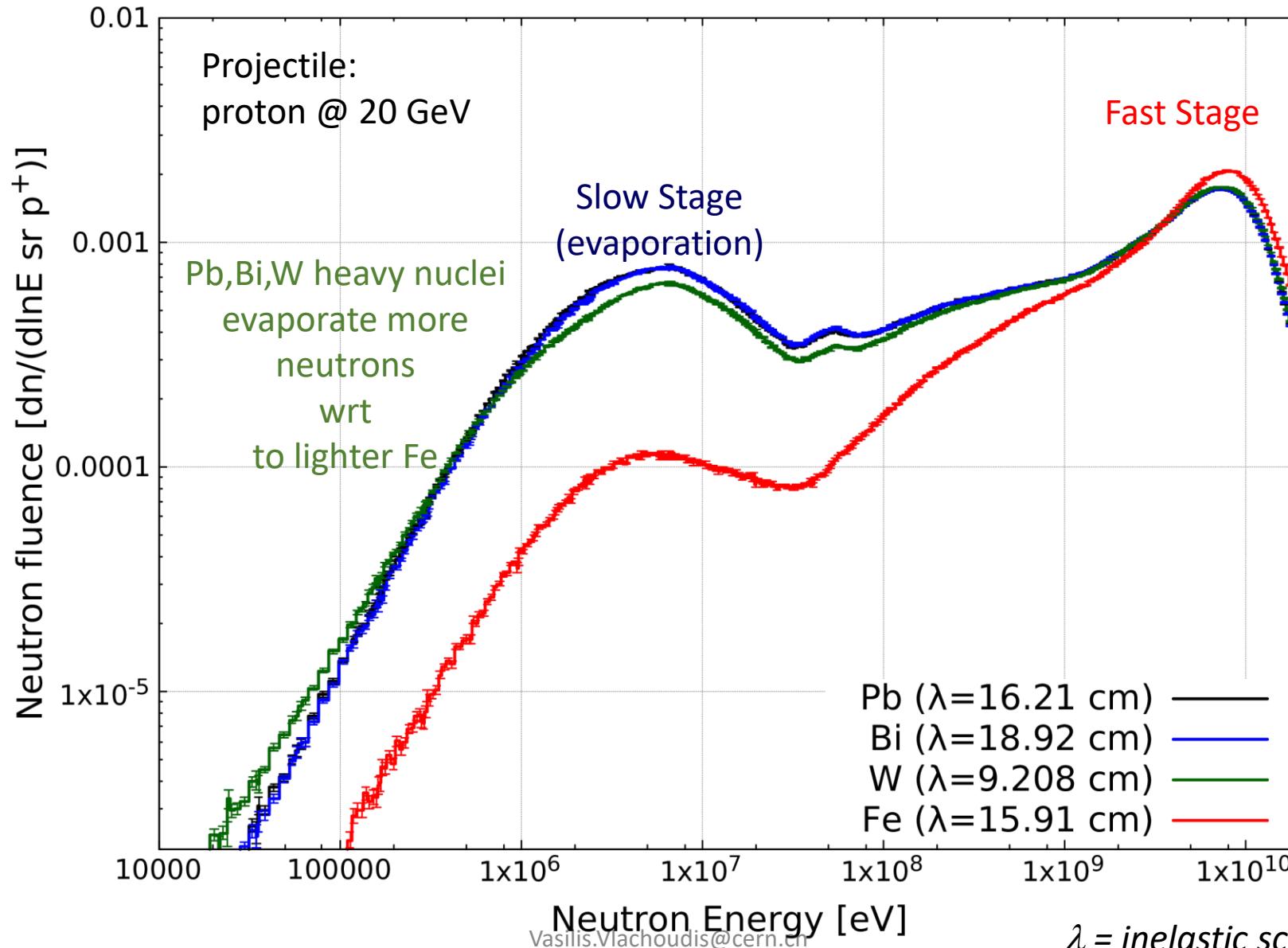


→ residuals can be radioactive

- At GeV energies there is no formation of compound nucleus

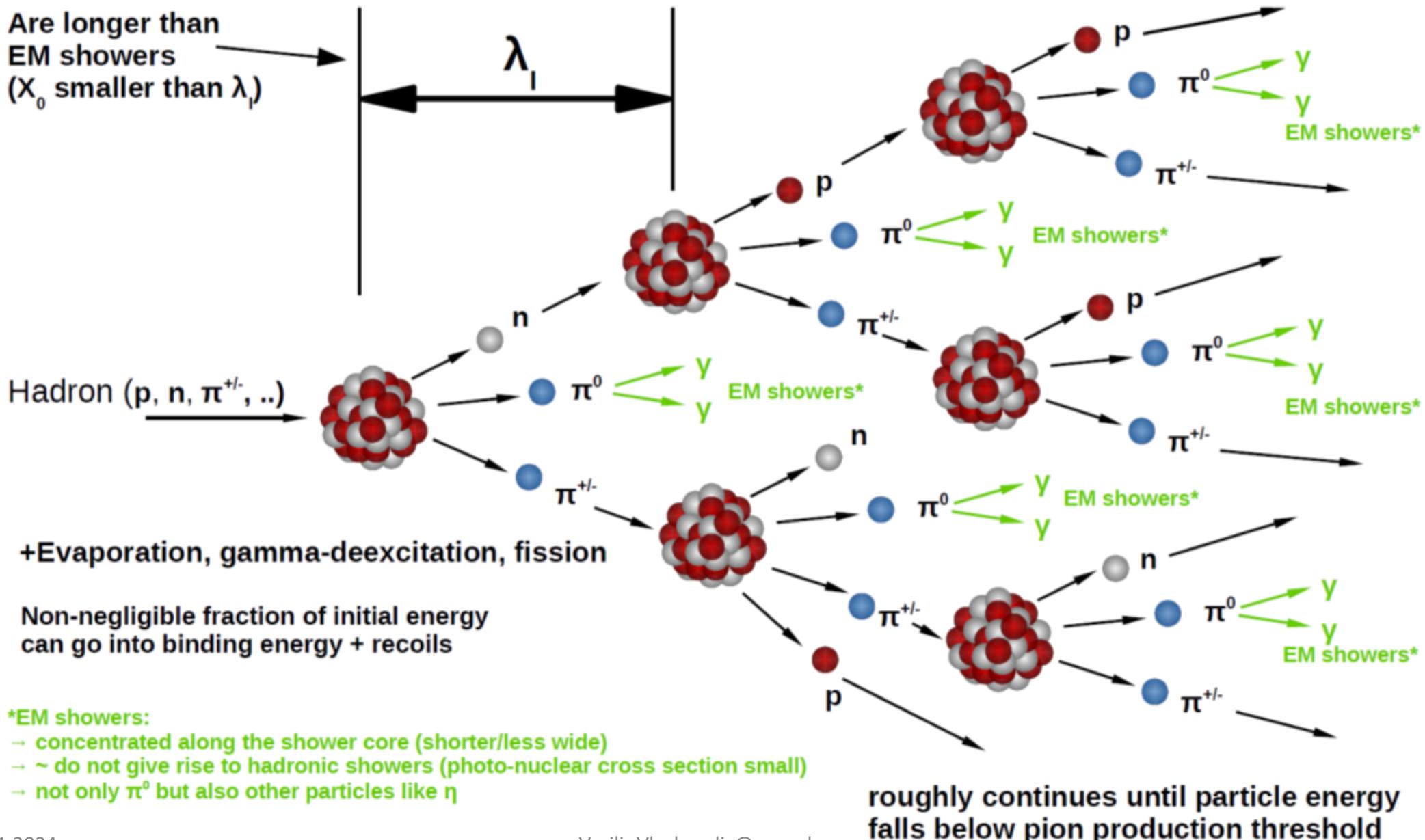
Hadron-Nucleus: Neutron yield

Thin layers: 0.01λ thickness, 2λ radius



Hadronic shower: basics

Are longer than
EM showers
(X_0 smaller than λ_I)



Hadronic Showers: numbers



Average π^0 fraction:

$$\frac{\pi^0}{all} \approx 0.10 \log(E)$$

For $E=20\text{ GeV}$
0.3

Average ratio electromagnetic and hadronic particles:

$$\frac{e}{h} \approx 1.1 - 1.35$$

Shower maximum:

$$d_{\max} \approx [0.6 \log(E) - 0.2]\lambda$$

1.6 λ

Shower depth for 95% longitudinal containment:

$$d_{95\%} \approx d_{\max} + 4E^{0.15}\lambda$$

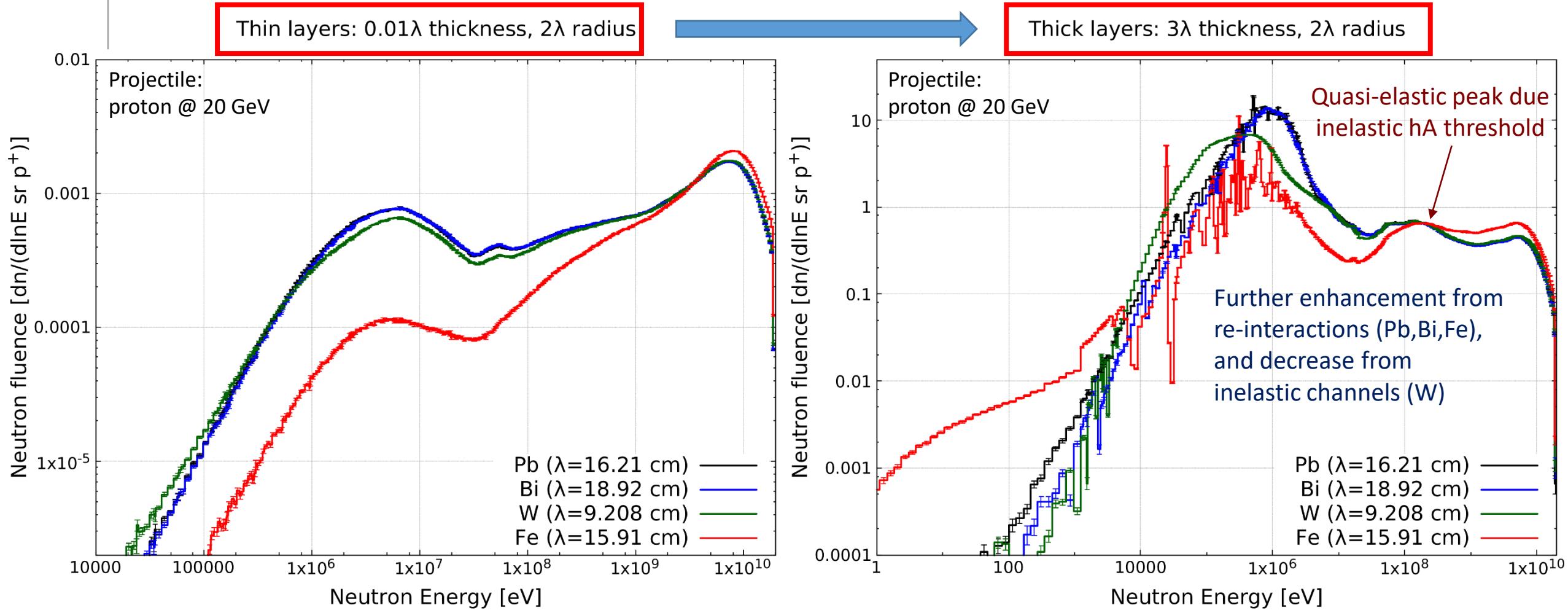
7.9 λ

Shower radius for 95% radial containment:

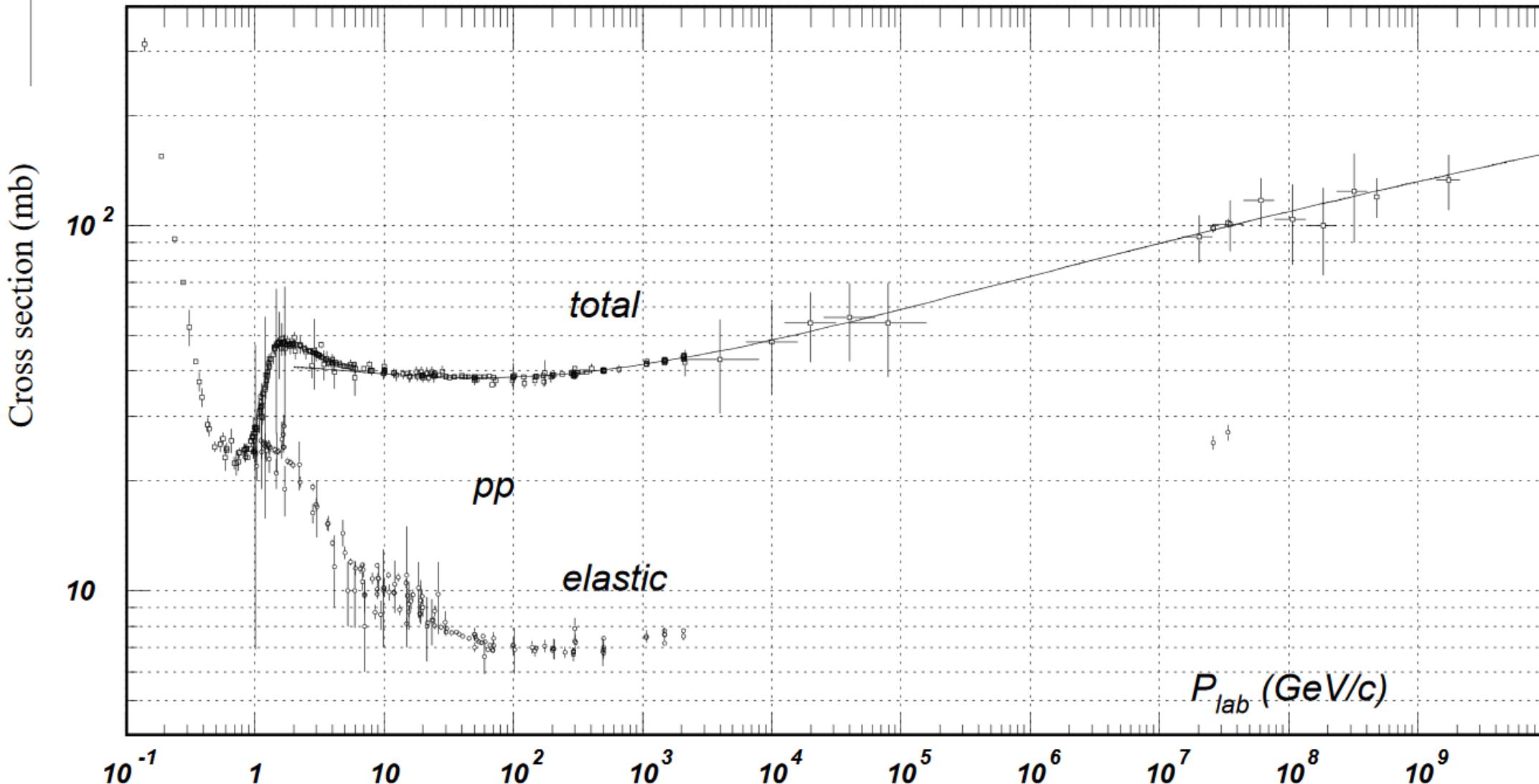
$$R_{95\%} \approx \lambda$$

with: E in GeV

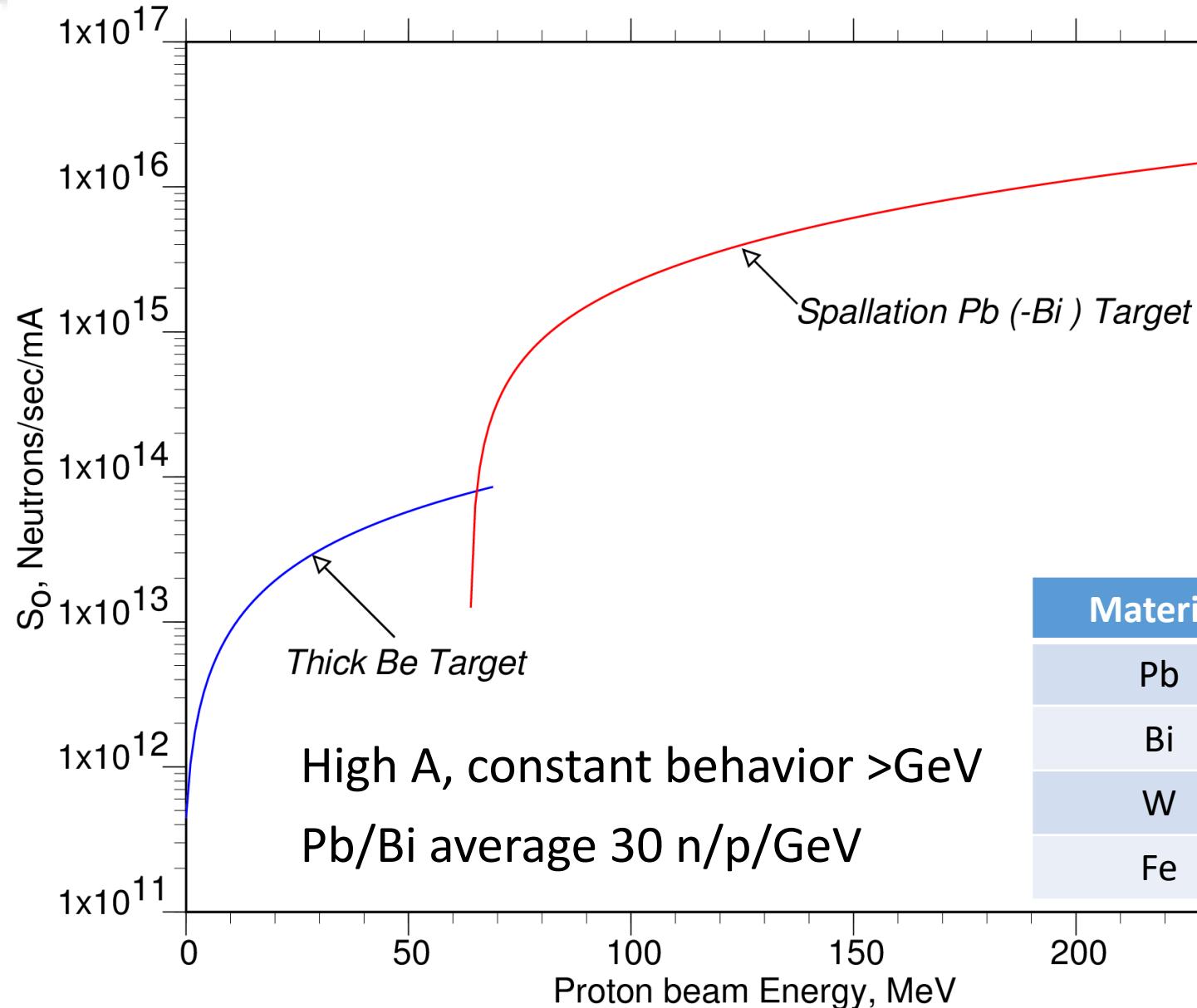
Hadronic shower: Neutron yield



Hadron-hadron collision



Neutron production on thick targets



- Why spallation Sources:
- Spallation x10 more neutrons per heat than fission
 - Efficient spallation sources requires proton $E > \sim 100 \text{ MeV}$
 - Pulsed sources allows time-of flight

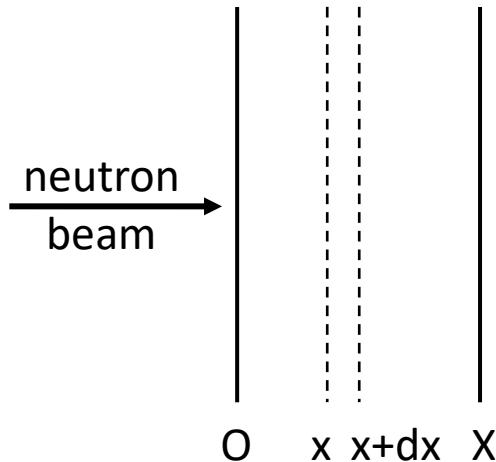
Material	$1\% \times \lambda$	$3 \times \lambda$	Infinite
Pb	1.6	19	29
Bi	1.6	19	28
W	1.4	17	18
Fe	0.35	6	10

Neutron yield /proton/GeV/(1-e^{-x/λ})

Figure 8

Interaction with matter

- Neutron beam traversing a thickness of dx suffers a small diminution of dI (from dI to $I-dI$) in intensity

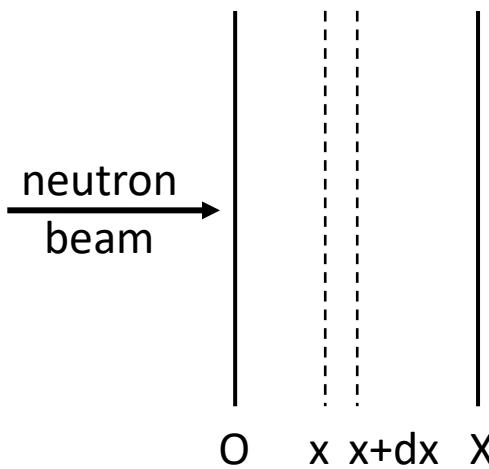


$$-\frac{dI}{I} = \frac{\sigma N S dx}{S}$$

where:

S = surface [cm^2],
 $N = N_A \rho / A$ = atom density [cm^{-3}],
 σ = effective target area [$barn=10^{-24} cm^2$]
 σ_t = total cross section [$barn$]
 $\sigma_t = \sigma_\gamma + \sigma_f + \sigma_s + \dots$

Interaction with matter



- Integrating gives:
- Probability of loss:
- Average penetration:

$$I = I_o e^{-\sigma N X}$$

$$1 - \frac{I}{I_o} = 1 - e^{-\sigma_t N x}$$

$$\begin{aligned}\bar{x} &= \int_0^{\infty} x e^{-\sigma_t N_o x} \sigma_t N dx \\ &= \frac{1}{\sigma_t N} = \frac{1}{\Sigma_t} = \lambda\end{aligned}$$

λ = known as *mean free path* [cm]

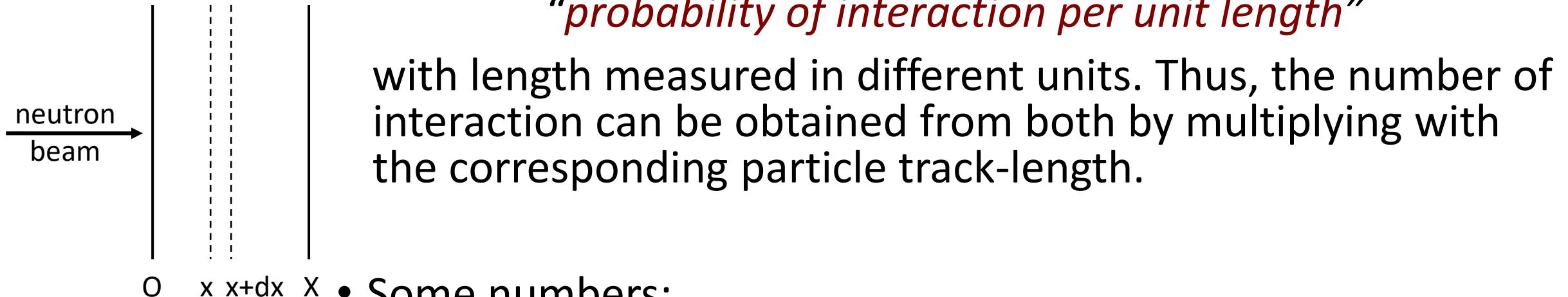
$\Sigma_t = \sigma_t N$ = *macroscopic cross-section* [cm⁻¹]

- σ, λ, Σ : are a function of particle type, material, and energy

Interaction with matter

- Both microscopic and macroscopic cross section are shown to have a similar physical meaning of:

“probability of interaction per unit length”



with length measured in different units. Thus, the number of interaction can be obtained from both by multiplying with the corresponding particle track-length.

- Some numbers:

C:	$\sigma_s(1\text{keV}) = 4.7 \text{ b}$	$\lambda_s = 2.1 \text{ cm}$
Al:	$\sigma_s(1\text{keV}) = 1.42 \text{ b}$	$\lambda_s = 11.7 \text{ cm}$
Pb:	$\sigma_s(1\text{keV}) = 10.7 \text{ b}$	$\lambda_s = 2.8 \text{ cm}$
H ₂ O:	$\sigma_{sH}(1\text{keV}) = 20.3 \text{ b},$ $\sigma_{sO}(1\text{keV}) = 3.85 \text{ b},$	$\lambda_s = 0.67 \text{ cm}$

- The number of interactions (*reaction rate*) [$\text{cm}^{-2} \text{s}^{-1}$] with a sample in a beam:

$$\frac{n(\mathbf{r}) dx \sigma N}{dt} = n(\mathbf{r}) \frac{dx}{dt} \Sigma = n(\mathbf{r}) v \Sigma = \frac{n(\mathbf{r}) v}{\lambda}$$

where: $n(\mathbf{r})$ = neutron density [cm^{-3}], having velocity v [cm/s]

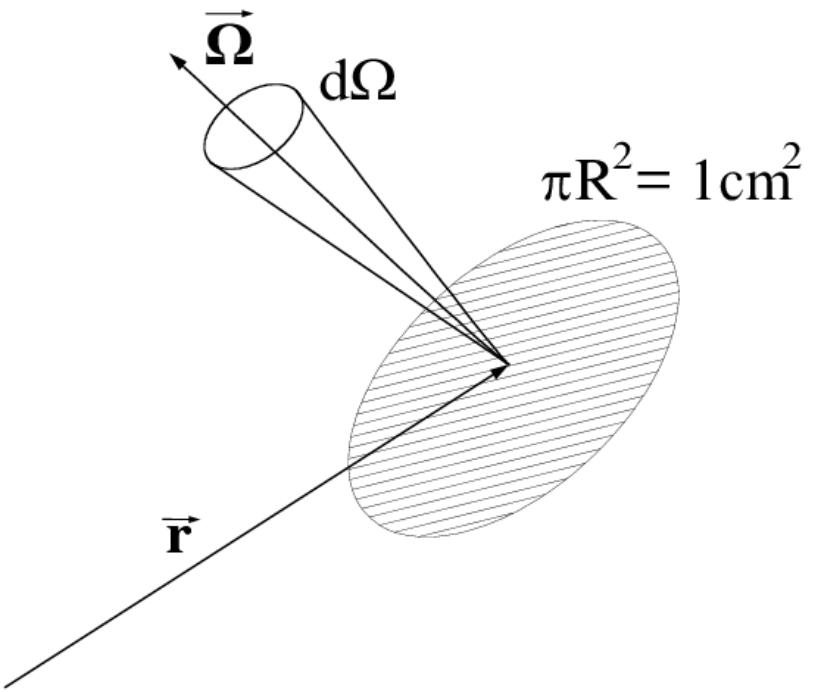
- The quantity $\Phi(E, \mathbf{r}, \Omega, t) = n(\mathbf{r}, \Omega)v$ is known as *differential neutron flux*
- Integrating over all solid angles

$$\Phi(E, \mathbf{r}, t) = \int_{4\pi} \Phi(E, \mathbf{r}, \Omega, t) d\Omega = n(E, \mathbf{r}, t)v$$

- we get the *fluence rate* or *flux density*

Flux / Fluence

- has dimensions:
 $[cm^{-3} \text{ cm s}^{-1}] = [cm^{-2} \text{ s}^{-1}]$.
- The time integral of the flux density $\Phi(E, r)$ is the **fluence** $[cm^{-2}]$
- Fluence is measured in *particles per cm²* but in reality it describes the **density of particle tracks** $[cm/cm^3]!$
- The number of reactions inside a volume V is given by the formula:
 (where the product $\sum \Phi V$ is integrated over energy or velocity)



Fluence is equivalent to the particles crossing a surface of 1 cm^2 always perpendicular to the particle direction. Or a sphere with cross section of 1 cm^2

Properties: Isotropic vs Uniform?

Current vs Fluence

Surface crossing

- Imagine a surface having an infinitesimal thickness dt . A particle incident with an angle θ with respect to the normal of the surface S will travel a segment $dt/\cos\theta$.
- Therefore, we can calculate an average surface fluence by adding $dt/\cos\theta$ for each particle crossing the surface, and dividing by the volume $S dt$:

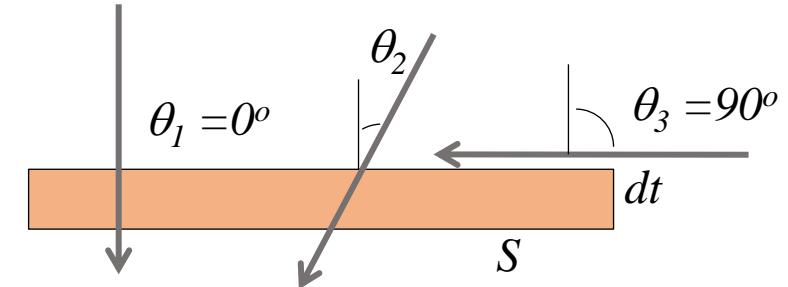
$$\Phi = \lim_{dt \rightarrow 0} \frac{\sum_i \frac{dt}{\cos \theta_i}}{S dt}$$

- While the **current** J counts the number of particles crossing the surface divided by the surface:

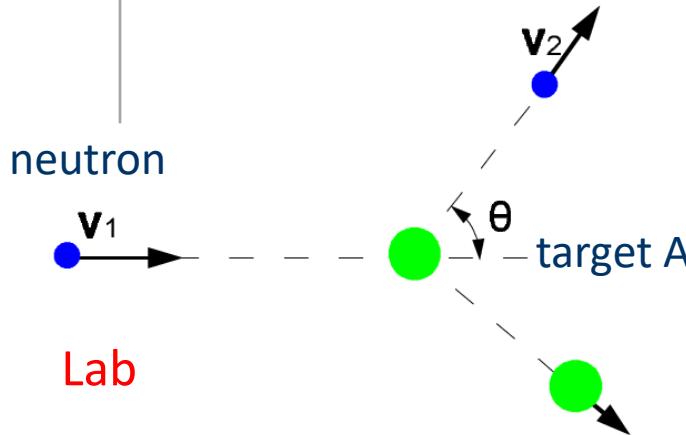
$$J = dN/dS$$

The **fluence** is independent from the orientation of **surface S** ,
 while the **current** is NOT!

Q: In an isotropic field can be easily seen that on a flat surface $J = \Phi/2$



Slowing down of neutrons*



The Center of Mass System CMS is moving with

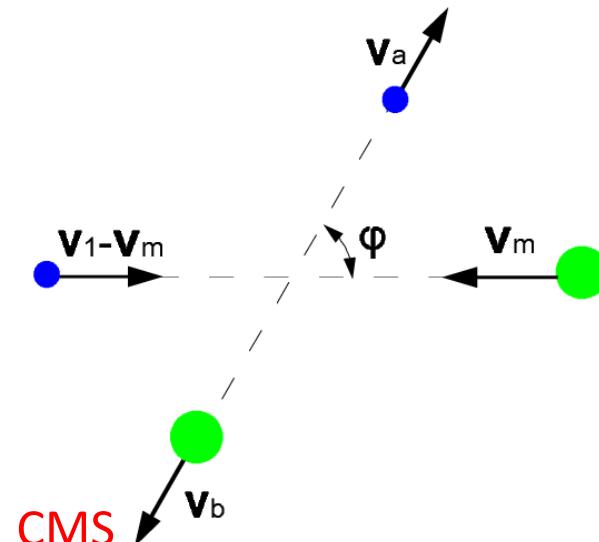
$$v_m = \frac{v_1}{A + 1}$$

From conservation energy & momentum we have

$$|v_a| = |v_I - v_m| \quad \text{and} \quad |v_m| = |v_b|$$

Transforming back to the lab

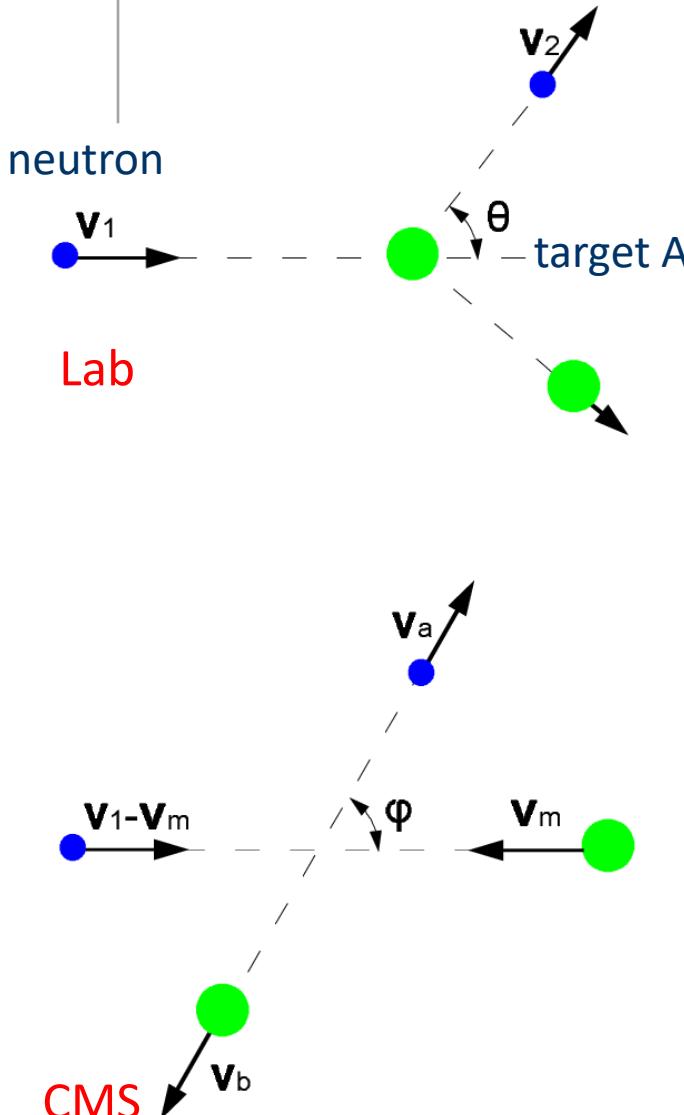
$$\frac{E_2}{E_1} = \frac{v_2^2}{v_1^2} = \frac{A^2 + 2A\cos\phi + 1}{(A + 1)^2}$$



* Assumptions:

- i) Non-relativistic kinematics
- ii) neutron in epithermal region
- iii) target nucleus at stand-still

Slowing down of neutrons



For low energies <MeV angle ϕ in C.M. is isotropic
 → flat distribution in $\cos\phi$
 → anisotropic in the θ LAB

$$b = \overline{\cos\theta} = \frac{2}{3A}$$

The scattering probability to have a final energy in the interval $(E, E+dE)$ is

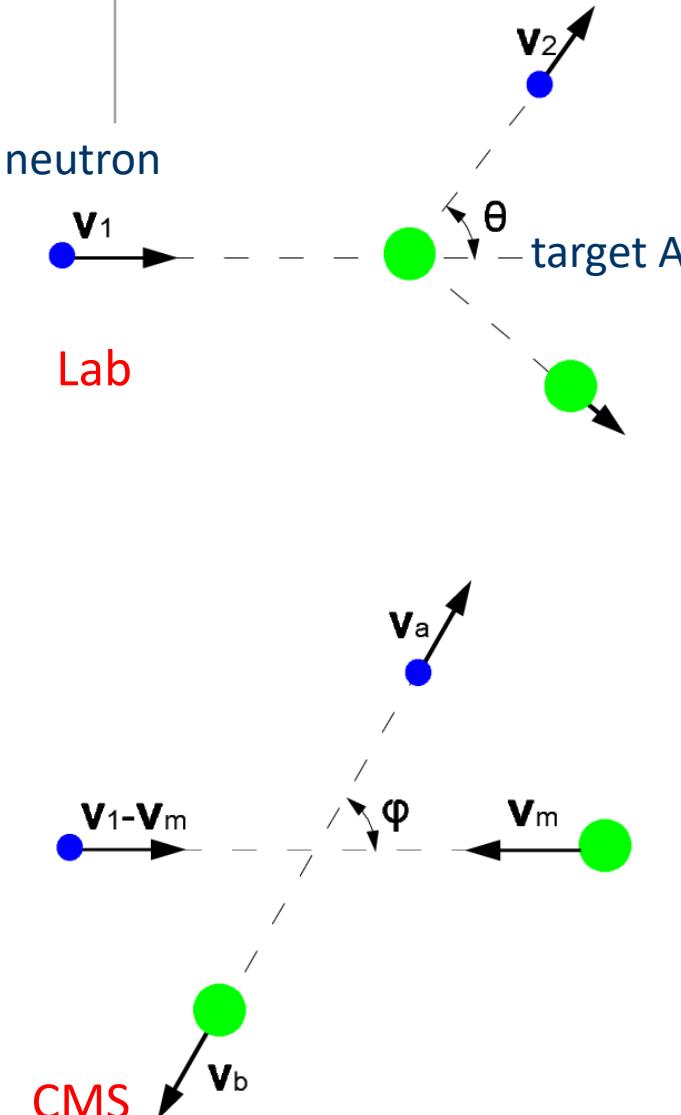
$$F(E)dE = \frac{2\pi \sin\phi d\phi}{4\pi} = -\frac{d(\cos\phi)}{2}$$

Integrating the $F(E)dE$ we get that

$$\frac{\overline{\Delta E}}{E} = \frac{1-a}{2}$$

$$\text{with } a = \left(\frac{A-1}{A+1}\right)^2$$

Slowing down of neutrons



The quantity $\ln(E_1/E_2)_{avg}$ is called *lethargy* and represents the *average logarithmic energy loss per collision*:

$$\xi = \overline{\ln \frac{E_1}{E_2}} = 1 + \frac{a}{1+a} \ln a$$

Taylor approximation gives us (for $A>1$):

$$\xi \approx \frac{2}{A+2/3}$$

- For $A \geq 10$ is a good approximation.
- For $A=2$ the error of the approximation is 3%

For mixtures:

$$\bar{\xi} = \frac{\sum_i N_i \sigma_s^i \xi_i}{\sum_i N_i \sigma_s^i}$$

Slowing down of neutrons

- lethargy can be used to estimate the number of collisions to moderate from the initial energy E_i to E_f

$$n\xi = \ln \frac{E_i}{E_f}$$

- Giving a neutron fluence

$$\Phi(E) = \frac{C}{\bar{\xi} \Sigma_s E}$$

Slowing down power: $\bar{\xi} \Sigma_s$ → Moderation ratio: $\xi \Sigma_s / \Sigma_a$

- larger ξ → faster slow down; larger Σ_s → more often collisions

	H	D	He	Li	Be	C	O	Pb	U
A	1	2	4	7	8	12	16	207	238
a	0	0.111	0.360	0.562	0.640	0.716	0.778	0.981	0.983
ξ	1.0	0.725	0.425	0.268	0.209	0.158	0.120	0.00963	0.00838
n	18	25	43	67	86	114	150	1888	2172

Slow down parameters from 2MeV → 0.025 eV (thermal)

Thermal Neutrons

The velocities of thermal motion of the material nuclei are distributed with a Maxwellian distribution

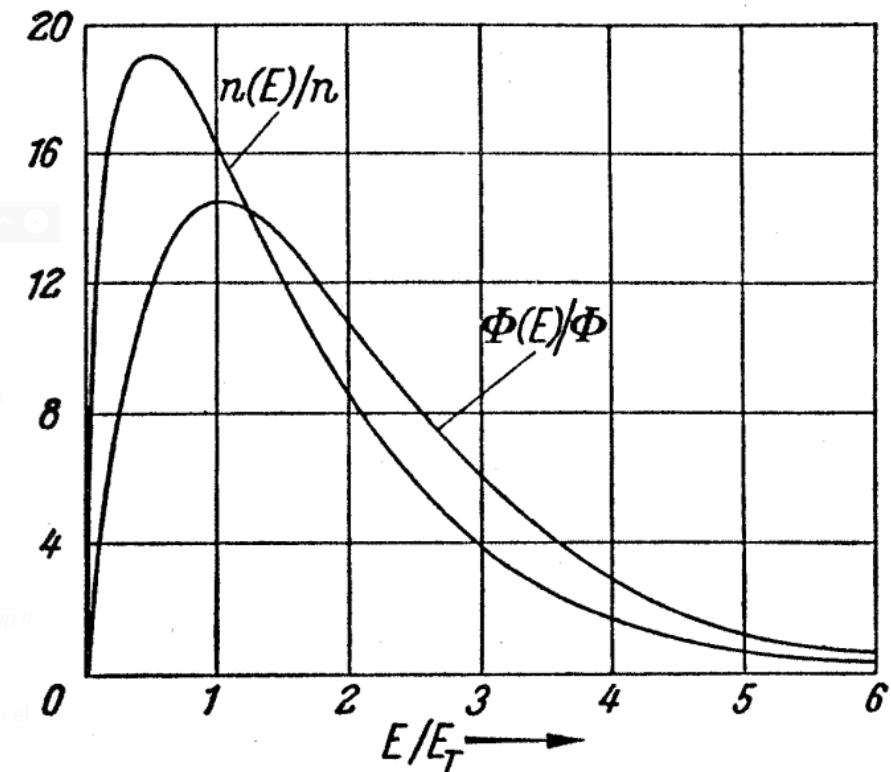
$$n(E)dE = \frac{2\pi n}{(\pi kT)^{3/2}} e^{-E/kT} \sqrt{E} dE$$

where $n(E)dE$ is the number of neutrons per cm^3 with energies $[E, E+dE]$, n is the total density

The average energy is $\bar{E} = \frac{3}{2} kT$

The most probable energy is $E_T = kT$

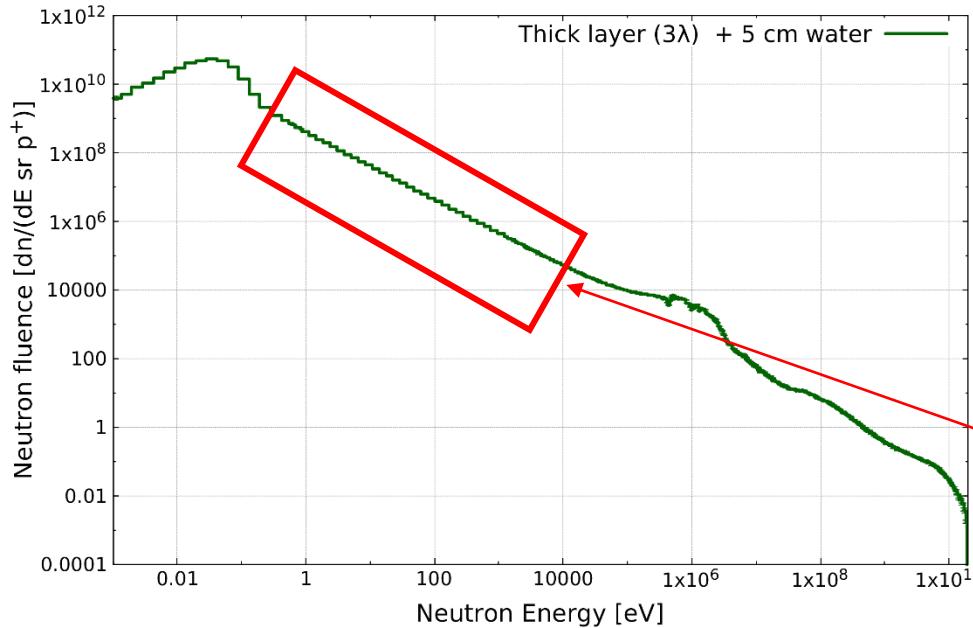
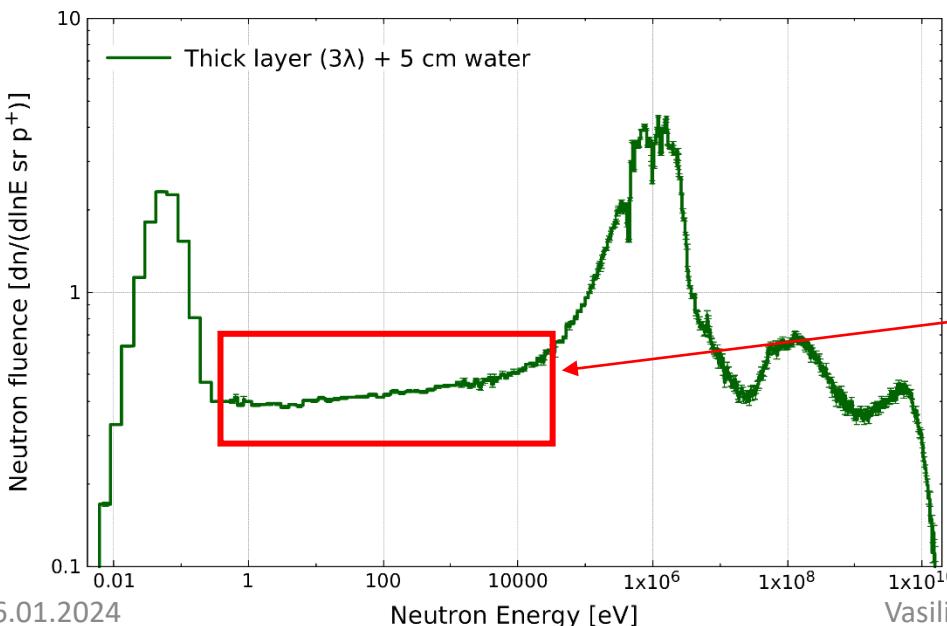
At $T=20^\circ C=293K$, $kT = 0.0253eV$,
 $v=2200m/s$



Neutron flux is given

$$\frac{\Phi(E)dE}{\Phi} = e^{-E/E_T} \frac{E}{E_T} \frac{dE}{E_T}$$

Flux/Fluence – Isolethargic

 dn/dE  $dn/d\ln E$ 

- Textbook representation of fluence as $\Phi(E) = dn/dE$ is spanning over several orders of magnitude
→ hides a lot of information

- For energies above thermal the flux is almost: $\Phi(E) \approx \frac{C}{\xi \Sigma_s E}$

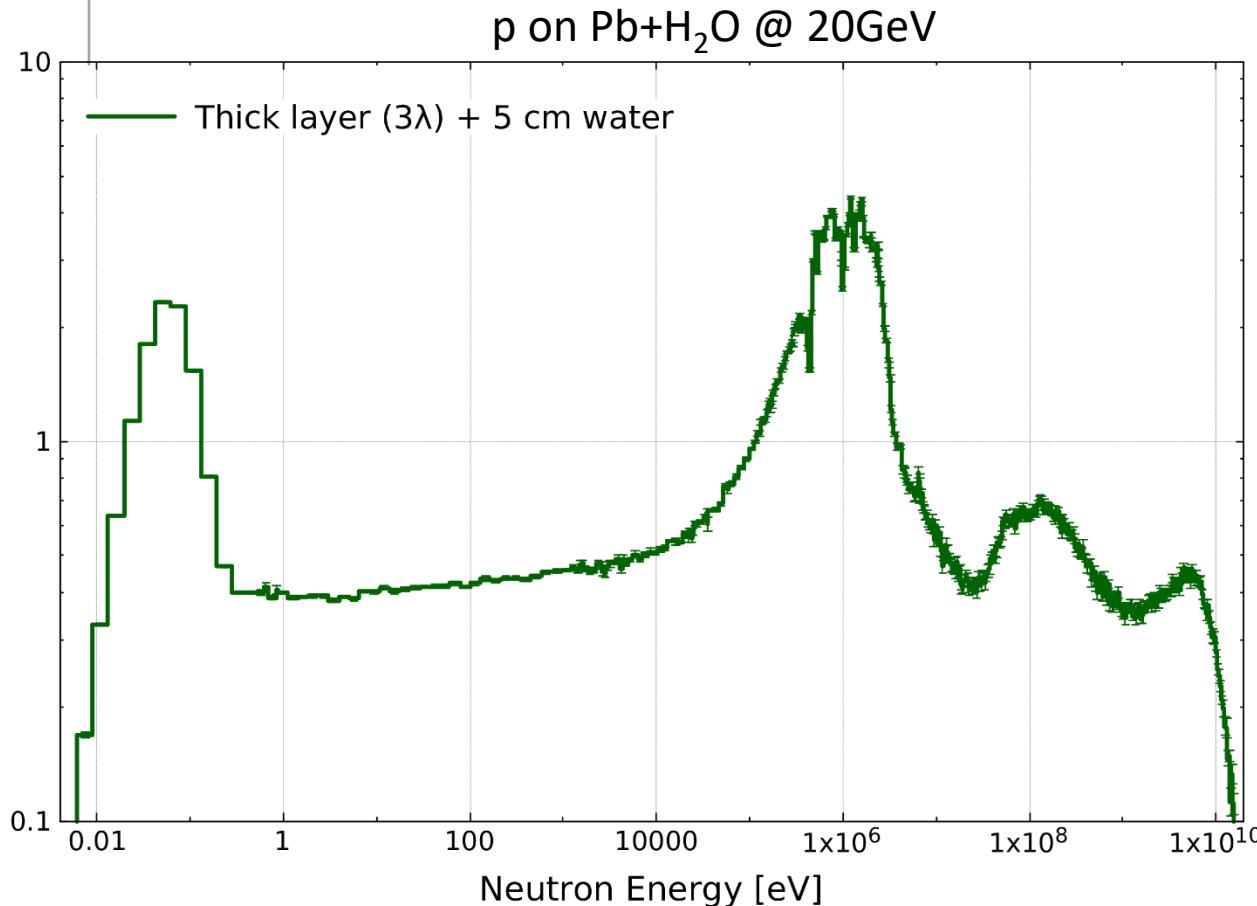
which can be converted to

$$E \Phi(E) = E \frac{dn}{dE} \approx C / \xi \Sigma_s$$

$$\Leftrightarrow \frac{dn}{d\ln E} \approx C / \xi \Sigma_s = \text{const}$$

- Resulting to a histogram “flat” in log space in the epithermal region

Isolethargic or Lethargy Plot



Advantages:

- Structures are more visible
- The Y scale is independent on the X unit since $d\ln E = dE/E = \text{unit less}$
- When X in log, the areas represent the integral of neutrons

How to read:

- It gives the amount of neutrons at energy E for an energy interval $\Delta E = E$

Converting histogram to Isolethargic

Logarithmic Histogram (base-10):

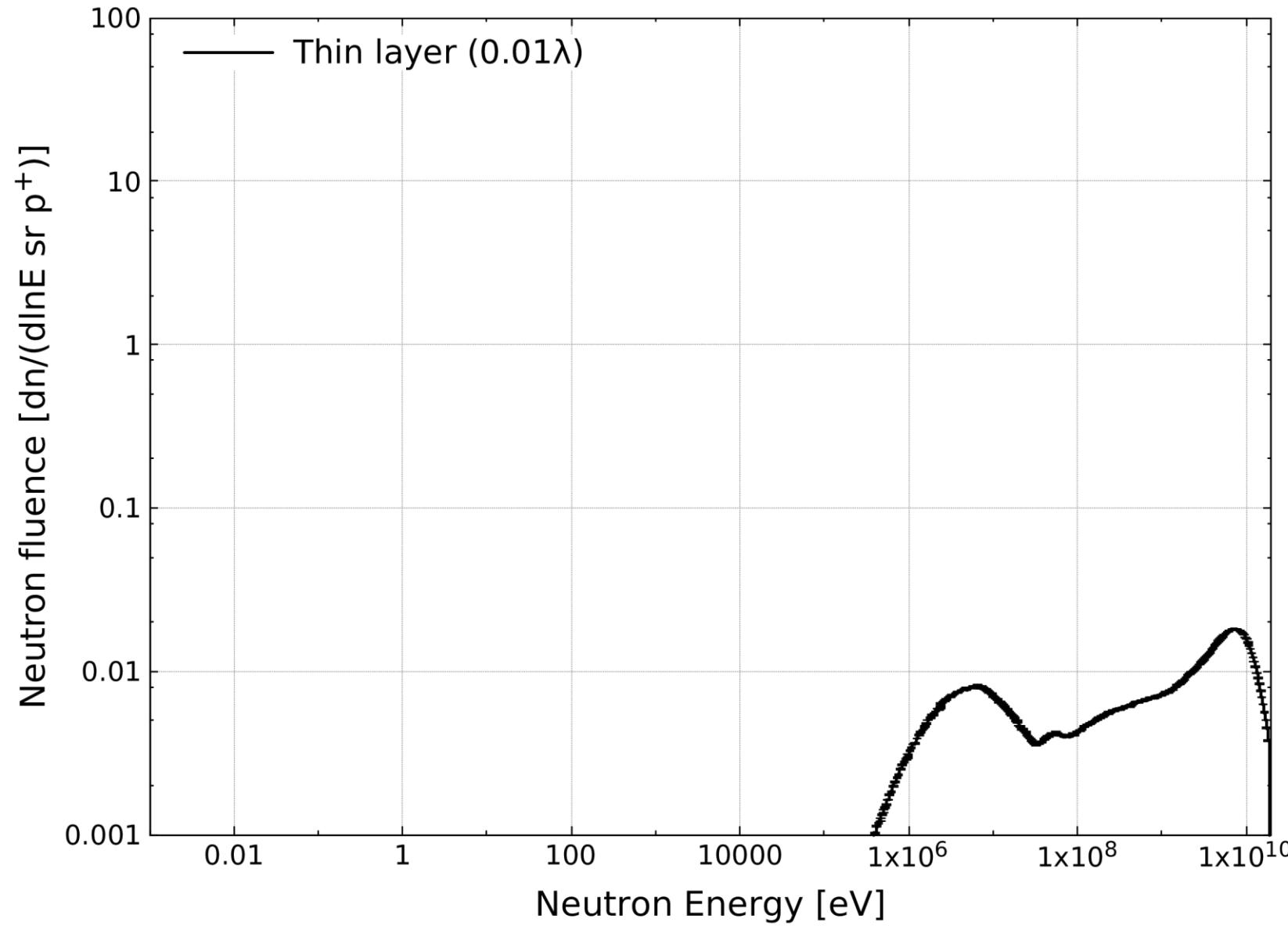
- Defined as: $X_{min} = \log_{10}(E_{min})$, $X_{max} = \log_{10}(E_{max})$, N_{bins}
- Log step: $s = (X_{max} - X_{min})/N_{bins}$
- Lower Energy of each bin: $E_i = 10^{X_{min} + i \cdot s}$
- Width of each bin: $\Delta E_i = 10^{X_{min} + (i+1) \cdot s} - 10^{X_{min} + i \cdot s}$
- Geometric Mean of the each bin: $\bar{E}_i = \sqrt{E_i \cdot E_{i+1}} = 10^{X_{min} + (i + \frac{1}{2}) \cdot s}$
- To convert to isolethargic can be done by multiplying with:

$$f = \frac{\bar{E}}{\Delta E} = \frac{10^{X_{min} + (i + \frac{1}{2}) \cdot s}}{10^{X_{min} + (i+1) \cdot s} - 10^{X_{min} + i \cdot s}} = \frac{\sqrt{10^s}}{10^s - 1}$$

Q: difference of geometric mean vs mean for 20 bins per decay?

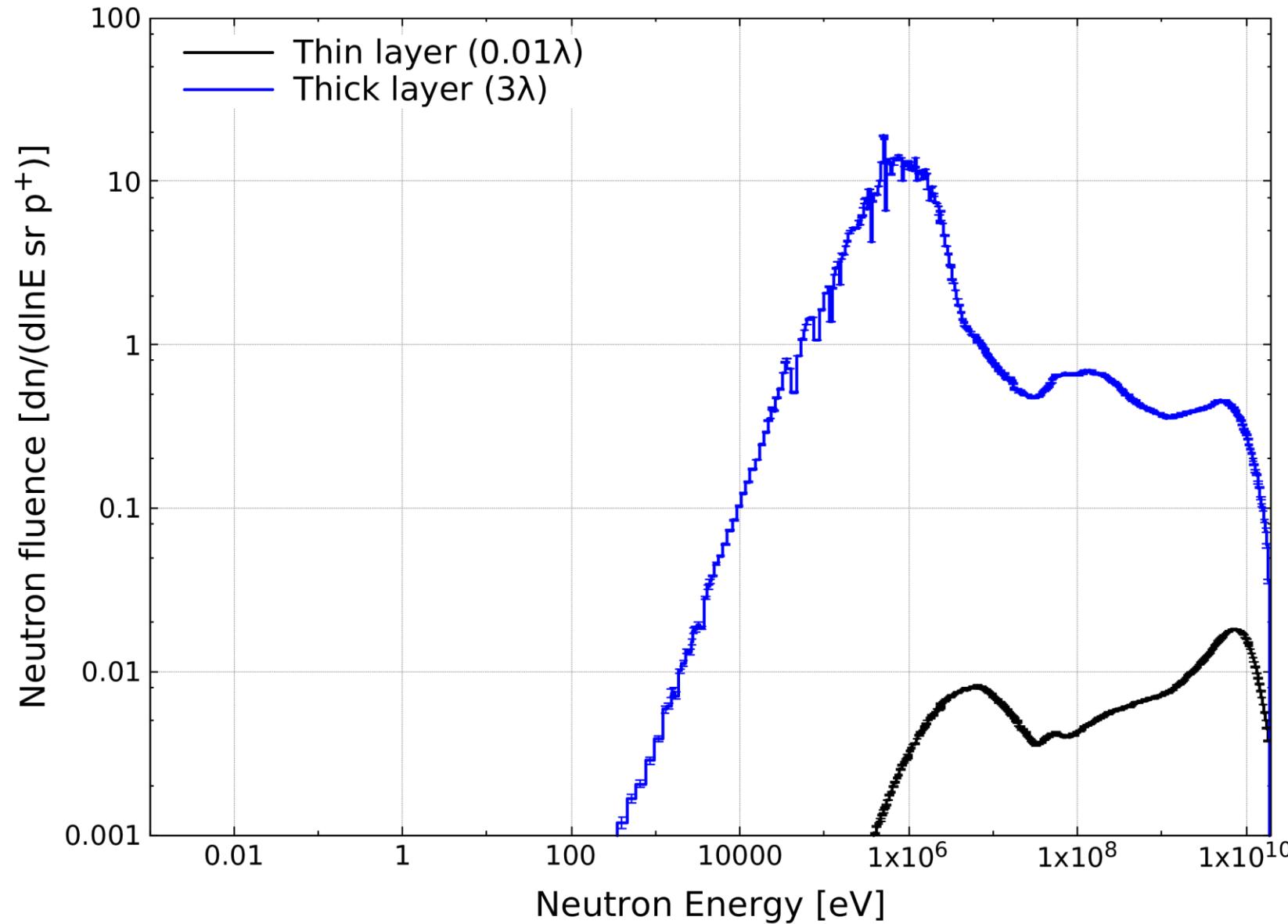
Neutron Yield

Pb ($\lambda=16.21$ cm)



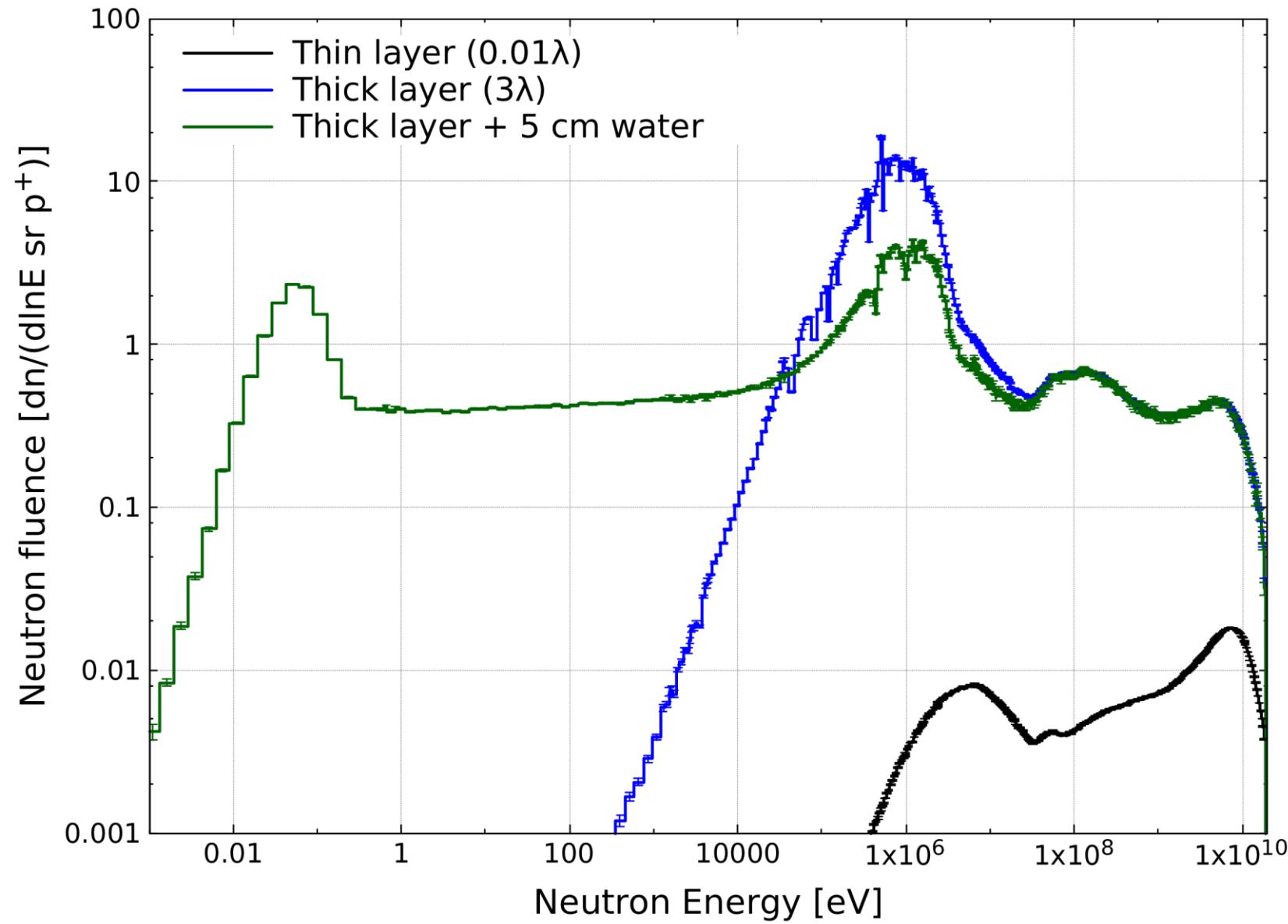
Neutron Yield

Pb ($\lambda=16.21$ cm)



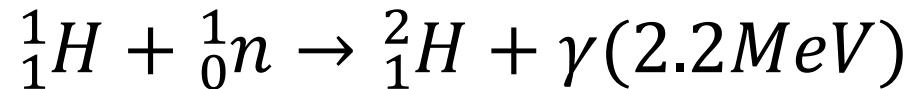
Neutron Yield

Pb ($\lambda=16.21$ cm)

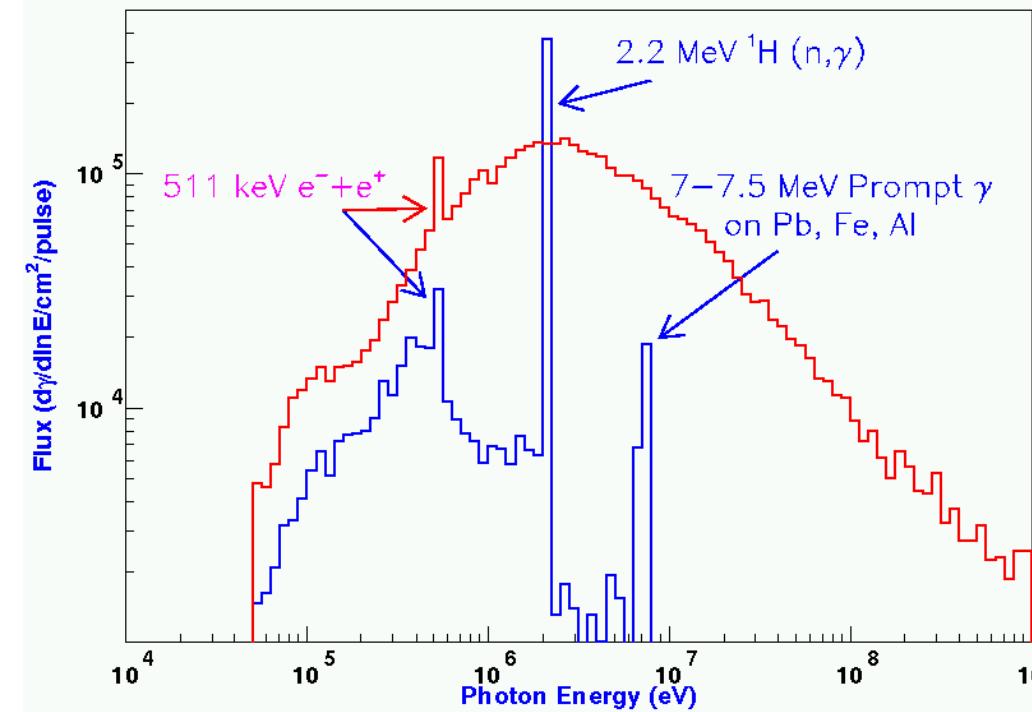
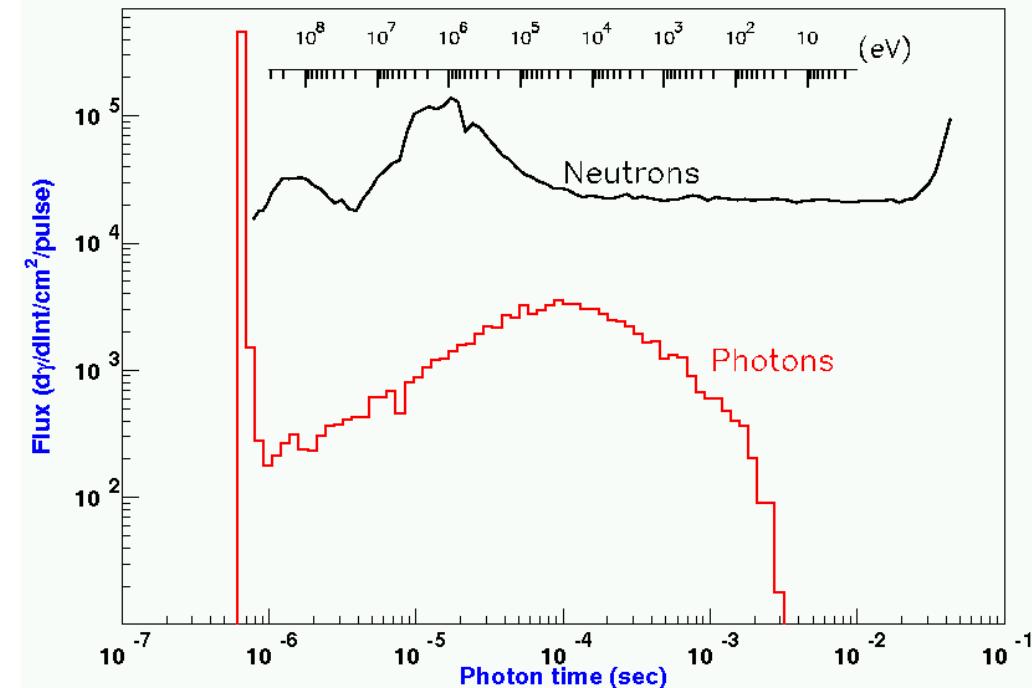


In beam Gamma background

In beam gamma background mostly comes from thermal neutrons radiative capture on 1H



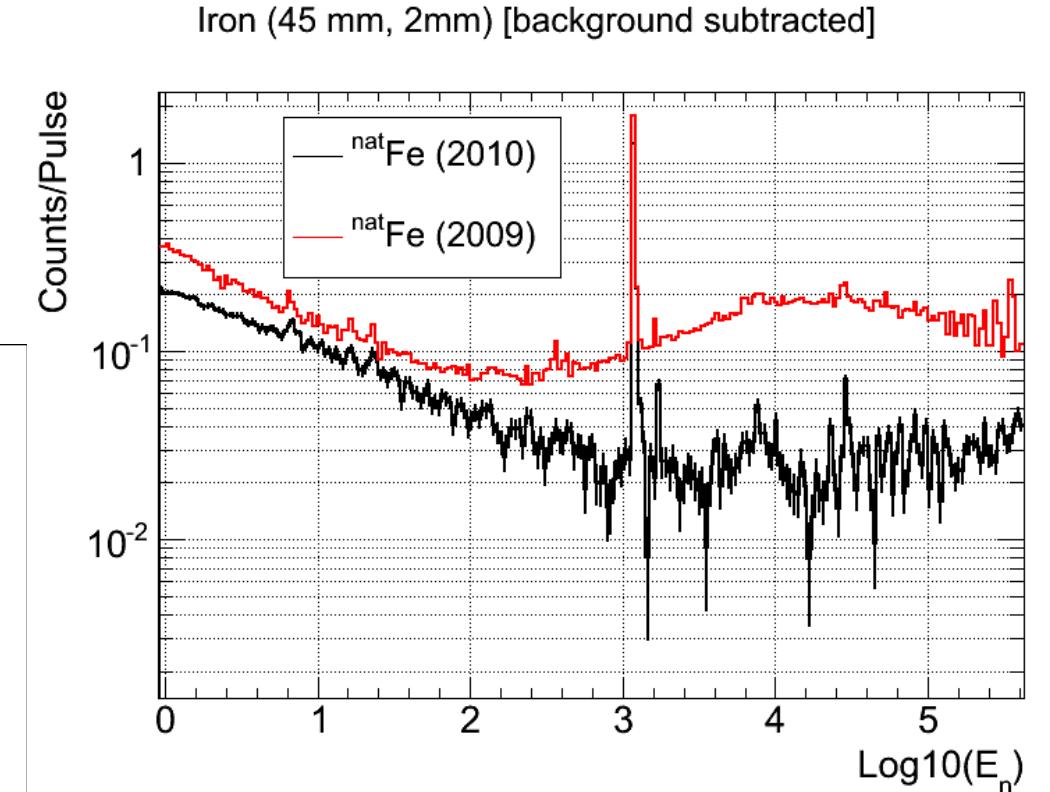
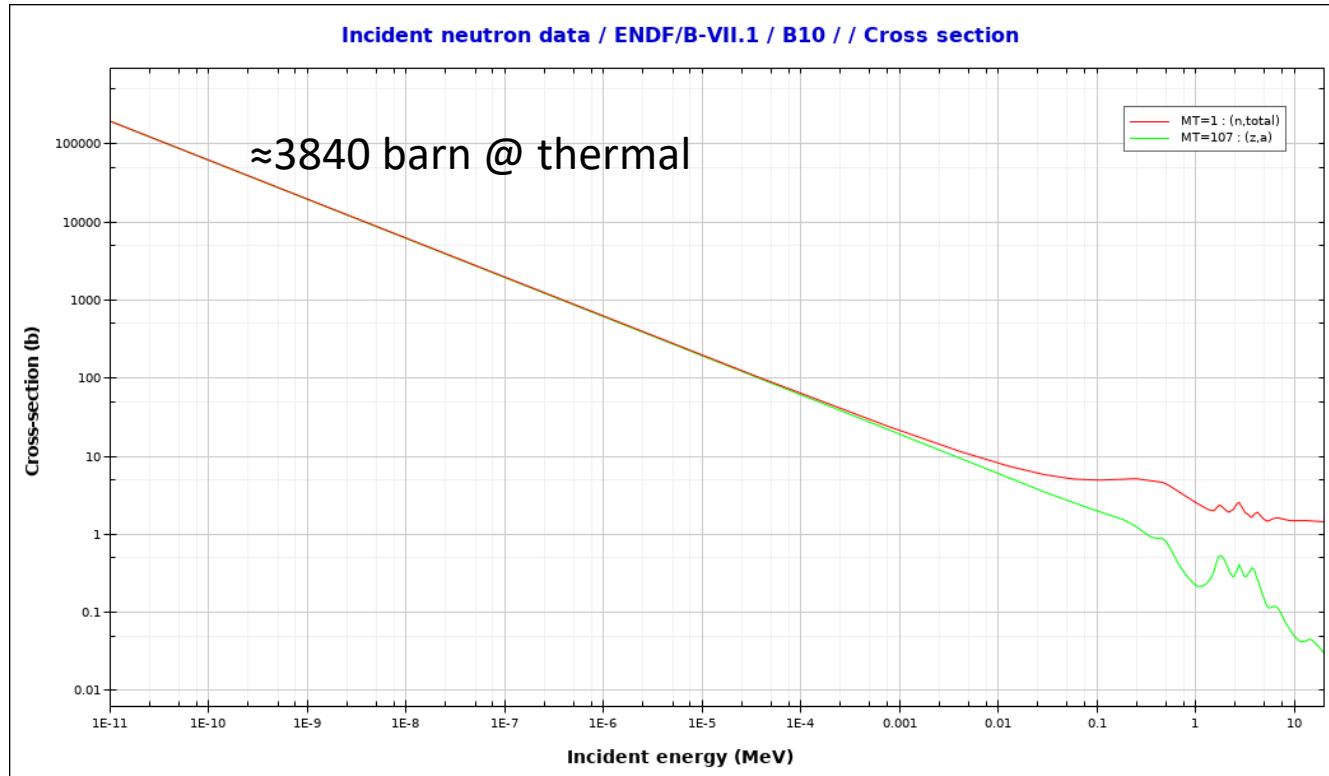
at n_TOF they arrive to the experimental area EAR1 @185m distance, at times in the range of $\mu s...ms$, together with the keV...100keV neutrons



Borated Water effect

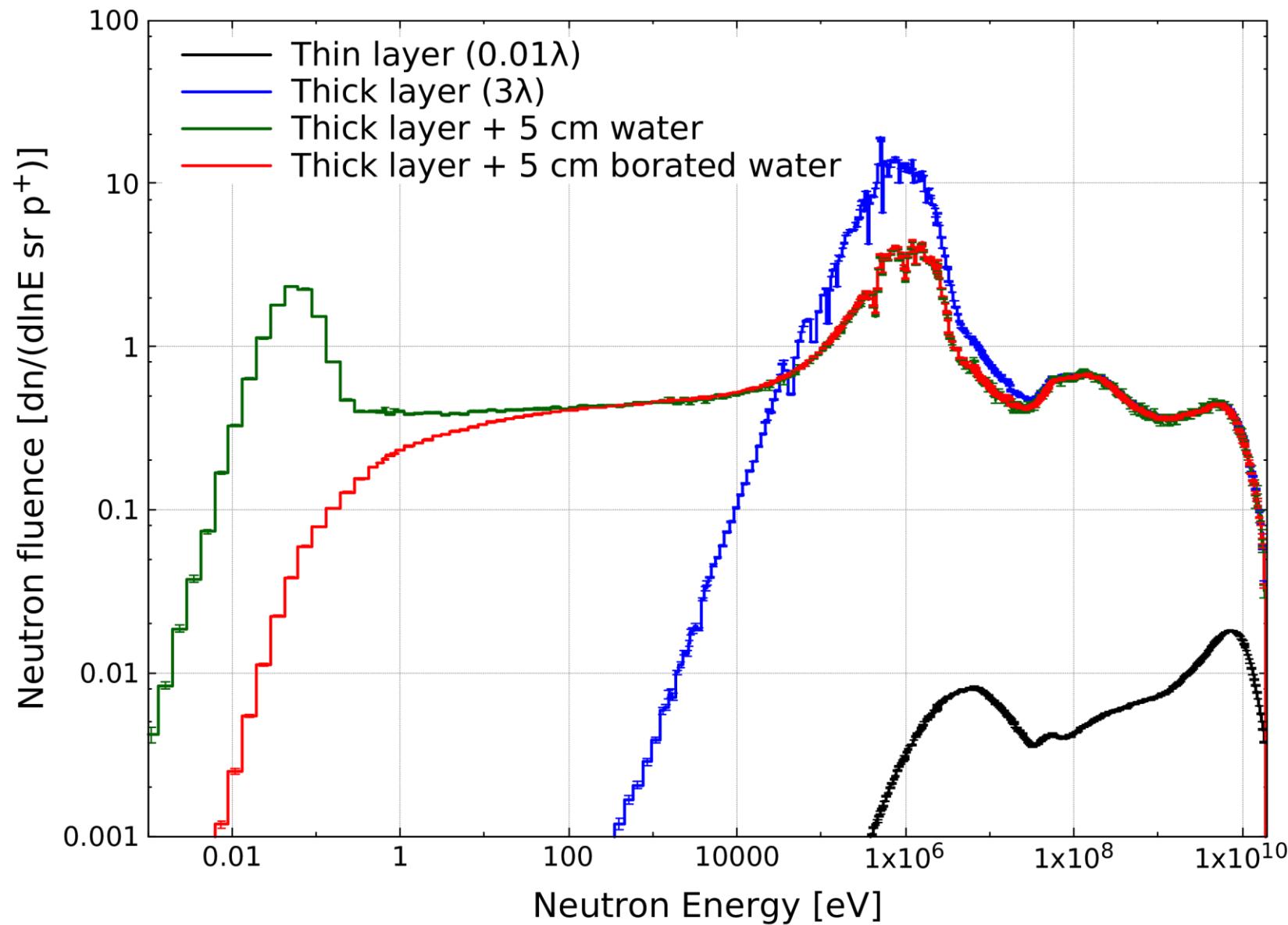
One option to suppress this background, was the addition of Boric Acid in the moderator circuit.

Boric acid: Saturated at 1.28 % enriched with 95% ^{10}B



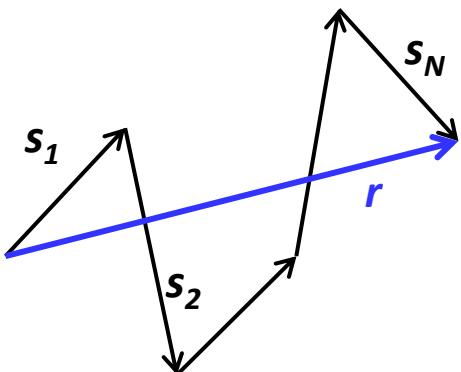
The 2.2 MeV γ is replaced by a 484 keV (94%) from the $^{10}\text{B}(n,\alpha)$ 6% gives 2.79 MeV

Neutron Yield

Pb ($\lambda=16.21$ cm)

Total vector of travel during moderation

$$\mathbf{r} = \sum_{i=1}^N \mathbf{s}_i$$



Thus

$$\mathbf{r} \cdot \mathbf{r} = \mathbf{r}^2 = \sum_{i=1}^N \sum_{j=1}^N \mathbf{s}_i \cdot \mathbf{s}_j = \sum_{i=1}^N \mathbf{s}_i^2 + \sum_{i \neq j}^N \mathbf{s}_i \cdot \mathbf{s}_j$$

If we make the bold assumption we are isotropic in LAB (normally for low energies it is isotropic in CMS not in LAB) \rightarrow the second term will average to zero

$$\overline{\mathbf{r}^2} \cong N \overline{\mathbf{s}^2}$$

Neutron diffusion

Combining the probability of a neutron traversing a distance s without making interaction and then making a collision in ds we have

$$e^{-\frac{s}{\lambda_s}} \frac{ds}{\lambda_s}$$

Assuming that $\Sigma_s \gg \Sigma_a$

$$\overline{s^2} = \int_0^\infty s^2 e^{-\frac{s}{\lambda_s}} \frac{ds}{\lambda_s} = 2\lambda_s^2$$

For n steps

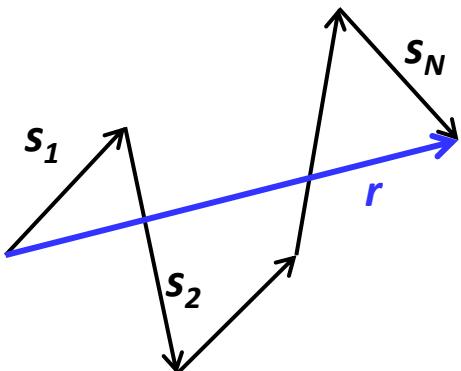
$$\overline{r^2} = 2n\lambda_s^2$$

Including the mean cosine per scattering

$$\overline{r^2} = \frac{2n\lambda_s^2}{1 - \overline{\cos\theta}}$$

Finally with the lethargy

$$|r| = \sqrt{\frac{2 \ln \frac{E_i}{E_f}}{\xi(1 - \overline{\cos\theta})} \lambda_s}$$

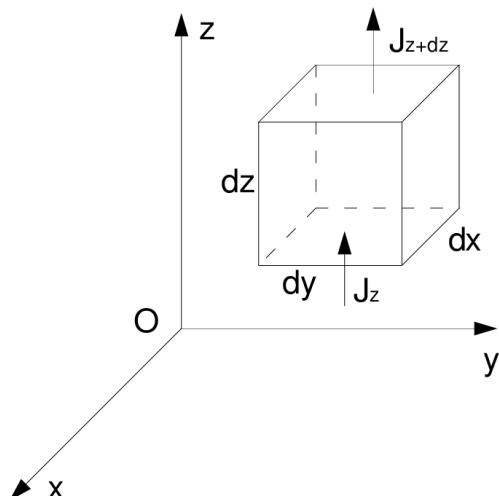


Neutron diffusion

Outflow in z direction in a small volume $dV=dx dy dz$

$$(J_{z+dz} - J_z) dx dy = -D \left[\left(\frac{\partial \Phi}{\partial z} \right)_{z+dz} - \left(\frac{\partial \Phi}{\partial z} \right)_z \right] dx dy$$

$$= -D \frac{\partial^2 \Phi}{\partial z^2} dx dy dz$$



where $D = \lambda_s / 3(1 - \overline{\cos \theta})$ diffusion length coefficient

Combining it in 3D it gives $D \nabla^2 \Phi(\mathbf{r})$

The balance of neutrons per unit volume

→ diffusion equation

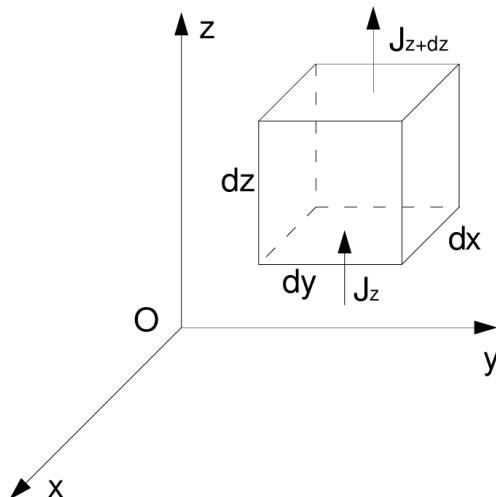
$$\frac{\partial \Phi(\mathbf{r})}{\partial t} = S(\mathbf{r}) + D \nabla^2 \Phi(\mathbf{r}) - \Sigma_a \Phi(\mathbf{r})$$

production	outflow	absorption
rate	rate	rate

Neutron diffusion

For a point like source in the center (Ficks'law)

$$\frac{S(\mathbf{r})}{D} + \nabla^2 \Phi(\mathbf{r}) - \frac{\Sigma_a}{D} \Phi(\mathbf{r}) = 0$$



where $L = \sqrt{D/\Sigma_a} \approx \sqrt{\frac{\lambda_a \lambda_s}{3}}$ = **Diffusion length [cm]**

→ specifies the average distance between the place where a neutron is born and the place where it is absorbed.

Notes:

- A neutron reflector should be of the order of a diffusion length
- Infinite medium should be at least one diffusion length

Some numbers:

Carbon: $L \approx 48 \text{ cm}$

Lead: $L \approx \text{order of } 150 \text{ cm}$

Neutron diffusion

- For an infinite medium the solution (Green's function)

$$\Phi(r) \approx S_o \frac{e^{-r/L}}{4\pi Dr}$$

where

S_o =neutron source rate [n/s]

L= diffusion length [cm]

D = diffusion length coefficient

- Flux Enhancement with the use of a moderator:

For a region close to the source $r/L \ll 1$

$$\Phi(r) \approx S_o / 4\pi Dr$$

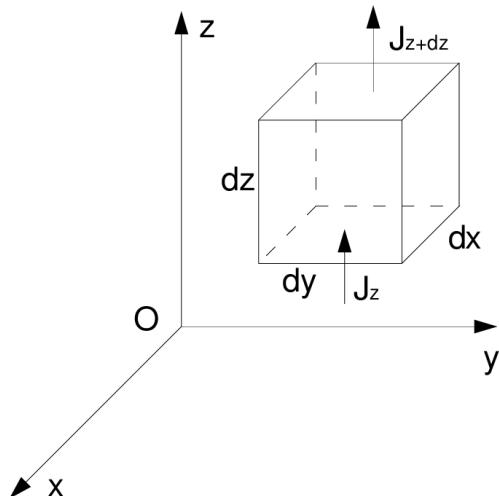
Considerably higher with respect to absence of moderator

$$\Phi_o(r) \approx S_o / 4\pi r^2$$

$$\text{Enhancement } f = \frac{\Phi(r)}{\Phi_o(r)} = r/D$$

Carbon: @30cm, $f=30/(2.1/3) = 42.8$

Lead: @30cm, $f=30/(2.8/3) = 32.1$



Energy Time relation

The average increase in lethargy per unit of time during moderation is
 $u=n\xi$

$$\frac{du}{dt} = \xi \Sigma_s \frac{dx}{dt} = \xi \Sigma_s v$$

From the lethargy $u = n\xi = \ln\left(\frac{E_i}{E_f}\right)$ we have $v_f = v_i e^{-\frac{u}{2}}$

Therefore:

$$\frac{dv}{dt} = -\frac{\xi \Sigma_s}{2} v^2$$

Integrating:

$$t = \frac{2}{\xi \Sigma_s} \int_{v_i}^{v_f} \frac{dv}{v} = \frac{2}{\xi \Sigma_s} \left(\frac{1}{v_f} - \frac{1}{v_i} \right)$$

Converting to energy: $E = \frac{2m_n}{(\xi \Sigma_s t)^2} v(t)$

Energy-Time relation

for A=1

$$\overline{E(t)} = \frac{3m_n}{(\Sigma_s t)^2} = \frac{1.8 eV \mu s^2}{t^2}$$

for A>>1

$$\overline{E(t)} = \frac{m_n}{2} \frac{A(A+2)}{(\Sigma_s t)^2} \approx \frac{A^2}{(\Sigma_s t)^2} 0.522 \text{ eV} \mu \text{s}^2 \text{cm}^{-2}$$

more accurately*

$$\overline{E(t)} = \frac{K}{(t+t_o)^2}$$

where $K = \frac{m_n \lambda_s^2 (1-a)^2}{2a^2}$ and $t_o = (1-a) \frac{\lambda_s}{a} \sqrt{\frac{m_n}{2E_0}}$

* R.E.Slovacek et al, Nucl. Sci. and Eng. 62:445-462, 1977

Energy-Time relation

Moderation:

$$\overline{E(t)} = \frac{K}{(t + t_o)^2}$$

Flight:

$$E = \frac{m_n L^2}{2 t^2}$$

Relativistically:

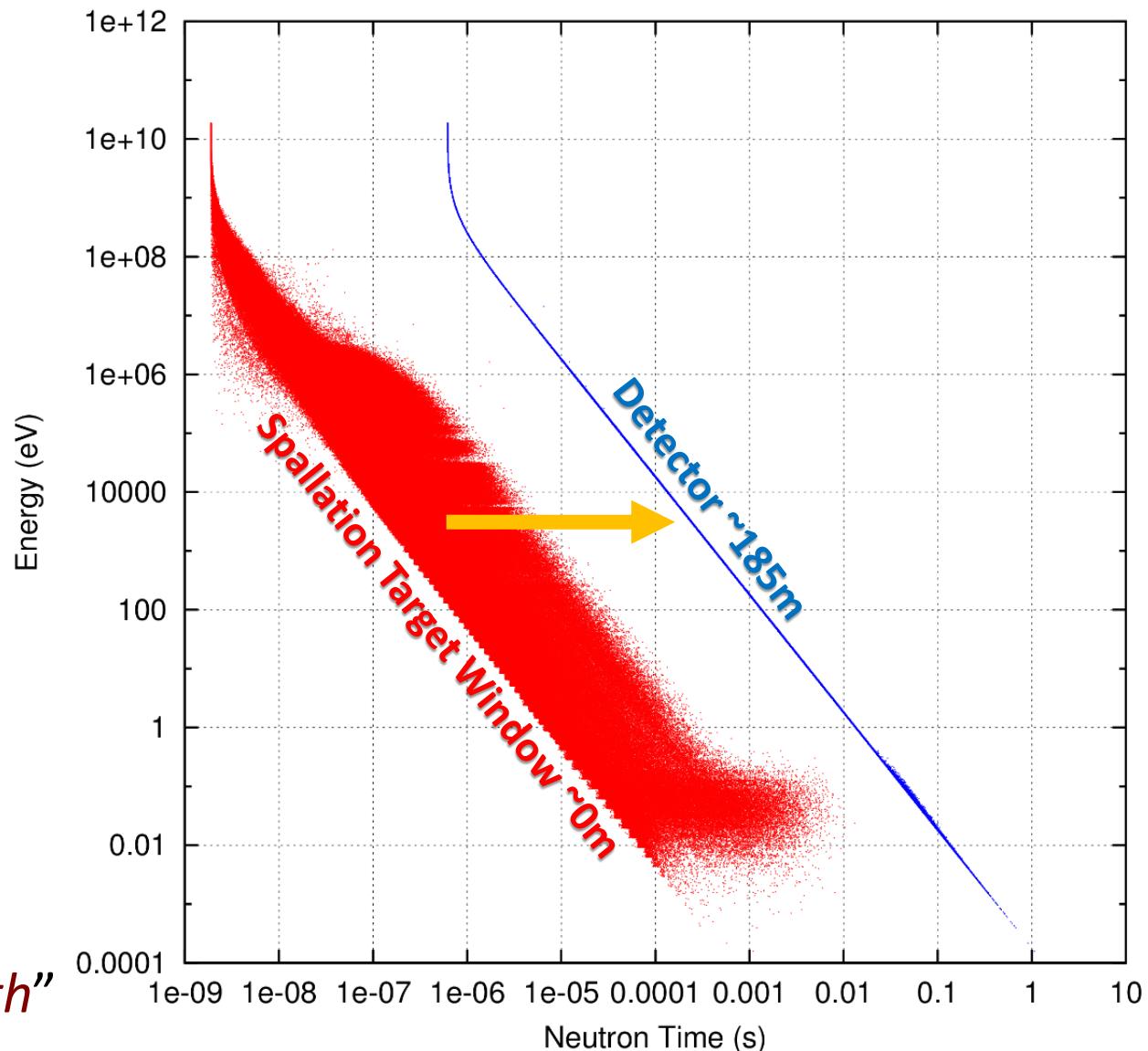
$$\gamma = 1 / \sqrt{1 - \left(\frac{L}{t c}\right)^2}$$

$$E_{kin} = (\gamma - 1) m_n$$

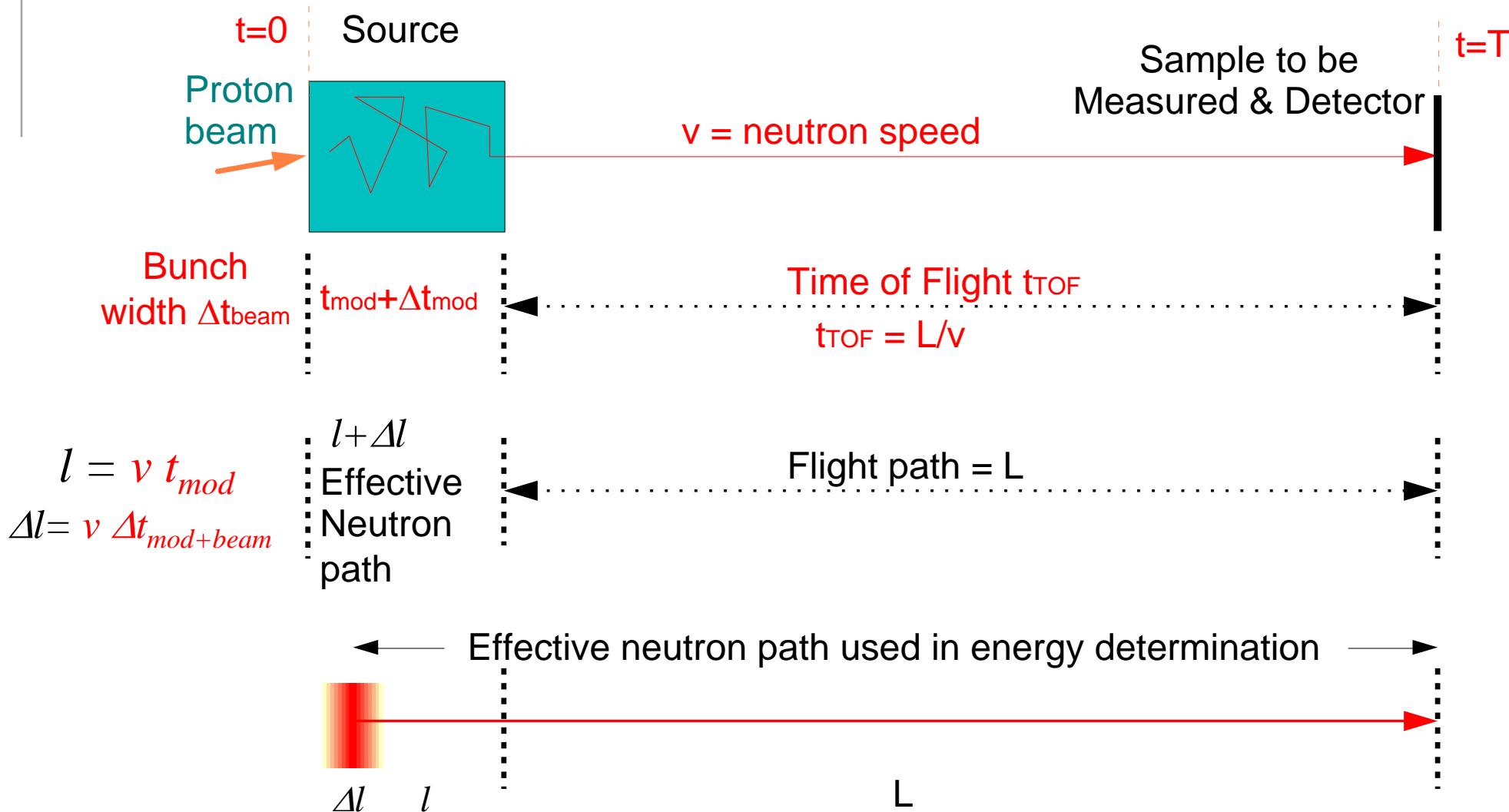
Differentiating we get the uncertainty:

$$\frac{\Delta E}{E} = -2 \frac{\Delta t}{t} = 2 \frac{\Delta l}{L + l}$$

l = virtual quantity “*effective neutron path*”



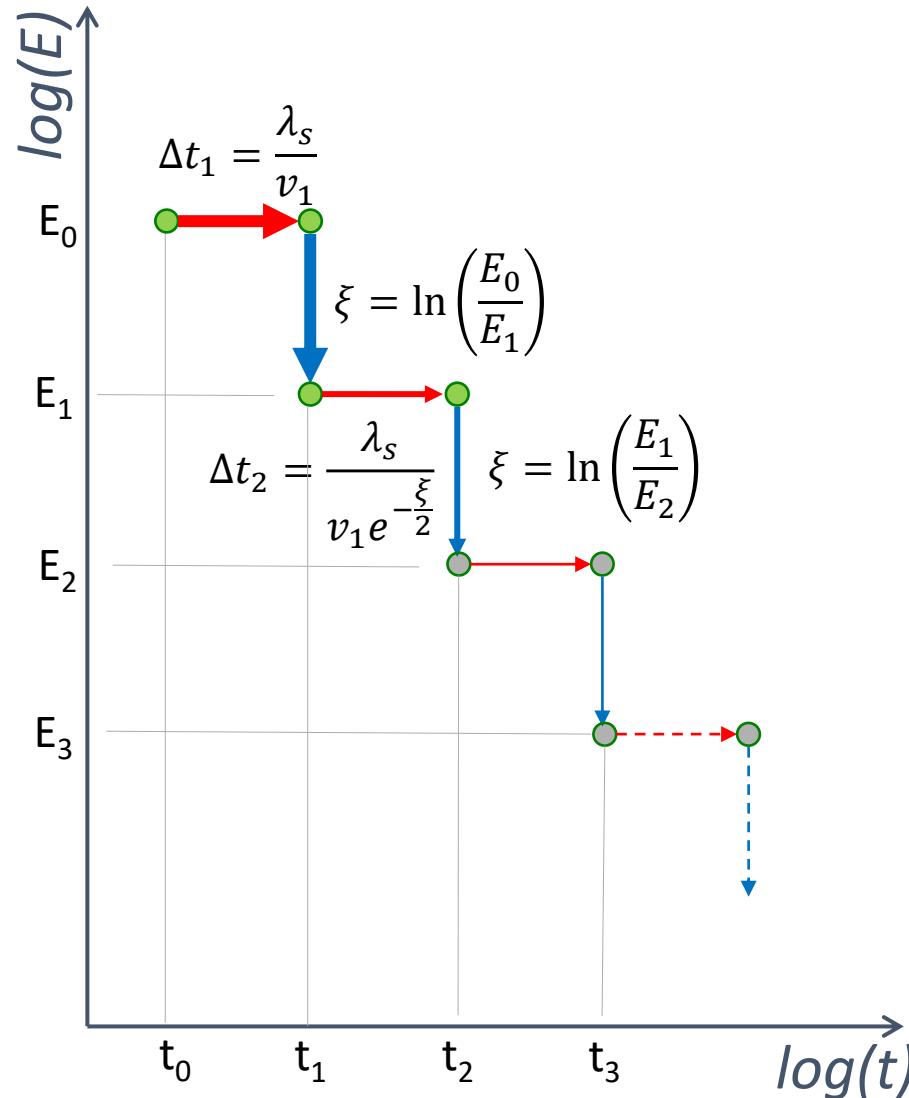
Effective Neutron Path l



The neutron velocity v is derived from the “effective neutron path”
 $v=(L+l)/t$ with an uncertainty $\Delta v = \Delta l/t$

WARNING:
Moderation path ≠ effective neutron path

Neutron Moderation



Mean free path

$$\lambda_s = \frac{1}{\Sigma_s} = \frac{1}{\sigma_s \frac{N_A}{4} \rho} \approx \text{const}$$

Average energy loss in collision

$$\xi = \ln\left(\frac{E_1}{E_2}\right) \approx \frac{2}{A + 2/3}$$

Velocity after n collisions

$$v_n = v_1 \cdot e^{-\frac{n-1}{2}\xi}$$

Time after n collisions

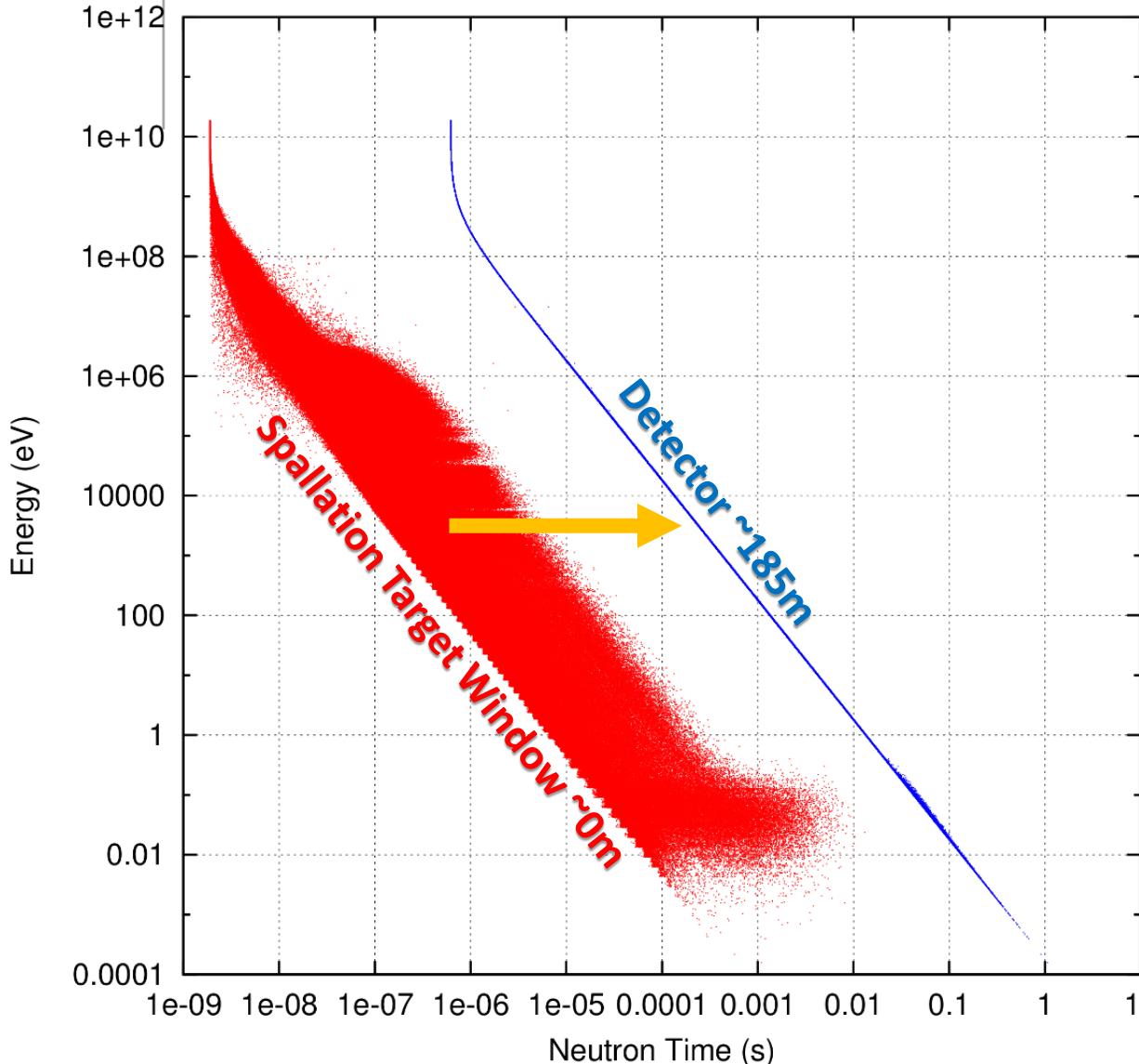
$$t_n = \frac{\lambda_s}{v_1} \sum_{i=1}^n e^{\frac{i-1}{2}\xi}$$

Effective length l_n after n collisions

$$l_n = v_n \cdot t_n = v_1 \cdot e^{-\frac{n-1}{2}\xi} \cdot \frac{\lambda_s}{v_1} \sum_{i=1}^n e^{\frac{i-1}{2}\xi}$$

$$l_\infty \approx 2 \frac{\lambda_s}{\xi}$$

Neutron Moderation



Mean free path

$$\lambda_s = \frac{1}{\Sigma_s} = \frac{1}{\sigma_s \frac{N_A}{4} \rho} \approx \text{const}$$

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$$l_\infty \approx 2 \frac{\lambda_s}{\xi}$$

Effective Neutron Path

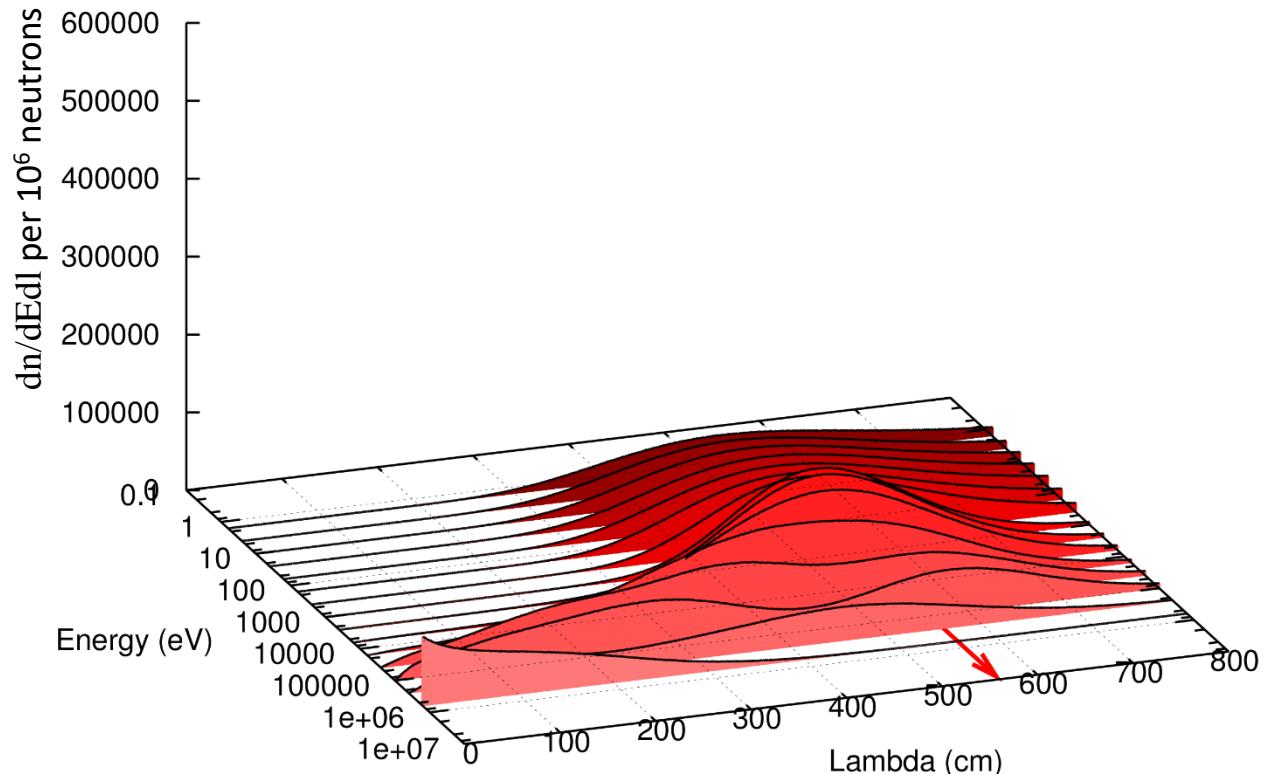
- **Lead:**

$$\sigma_s(1\text{keV}) = 11.35 \text{ b}$$

$$\lambda_s = 2.7 \text{ cm}$$

$$\xi = 9.6 \times 10^{-3}$$

$$l \approx 560 \text{ cm}$$



Effective Neutron path in infinite block with $E_0=1\text{MeV}$

Effective Neutron Path

- **Lead:**

$$\sigma_s(1\text{keV}) = 11.35 \text{ b}$$

$$\lambda_s = 2.7 \text{ cm}$$

$$\xi = 9.6 \times 10^{-3}$$

$$l \approx 560 \text{ cm}$$

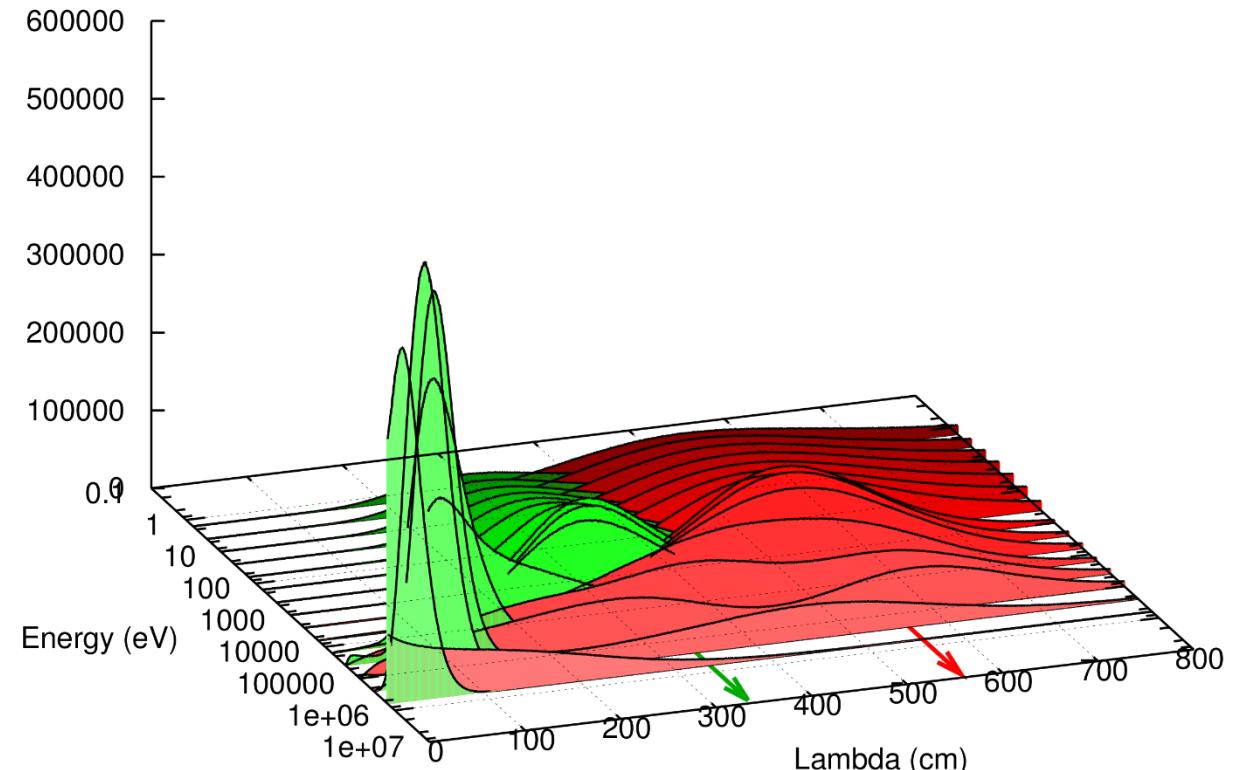
- **Aluminum:**

$$\sigma_s(1\text{keV}) = 1.42 \text{ b}$$

$$\lambda_s = 11.7 \text{ cm}$$

$$\xi = 7.2 \times 10^{-2}$$

$$l \approx 320 \text{ cm}$$



Effective Neutron Path

- **Lead:**

$$\sigma_s(1\text{keV}) = 11.35 \text{ b}$$

$$\lambda_s = 2.7 \text{ cm}$$

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- **Aluminum:**

$$\sigma_s(1\text{keV}) = 1.42 \text{ b}$$

$$\lambda_s = 11.7 \text{ cm}$$

$$\xi = 7.2 \times 10^{-2}$$

$$l \approx 320 \text{ cm}$$

- **Water:**

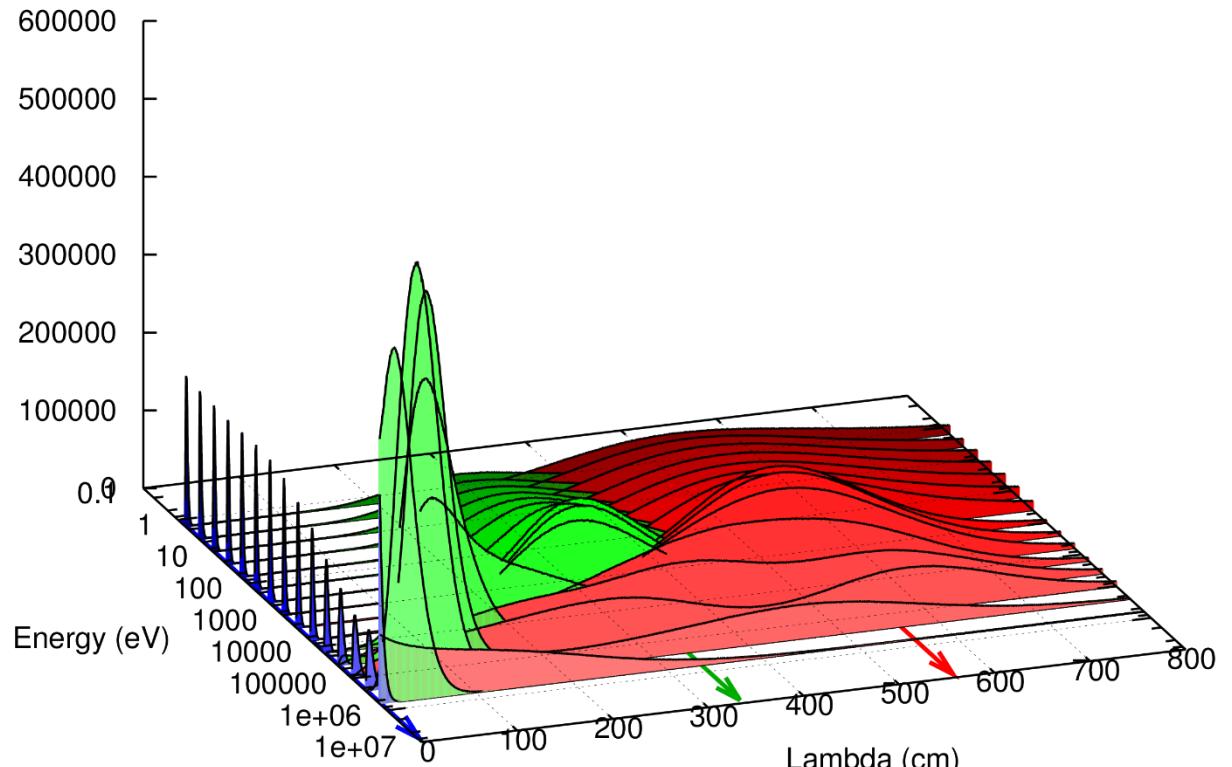
$$\sigma_{H_s}(1\text{keV}) = 20.3 \text{ b}$$

$$\sigma_{O_s}(1\text{keV}) = 3.85 \text{ b}$$

$$\lambda_s = 0.67 \text{ cm}$$

$$\xi_H = 1, \xi_O = 0.12$$

$$l_H \approx 1.5 \text{ cm}$$



Effective Neutron Path Spread

The lambda spread is determined by the spread of energy loss after collision

Maximum ($\theta=0^\circ$)

$$E_{2max} = E_1$$

Minimum ($\theta=180^\circ$)

$$E_{2min} = \left[\frac{A - 1}{A + 1} \right]^2 E_1$$

and a mean scattering angle

$$b = \overline{\cos\theta} = \frac{2}{3A}$$

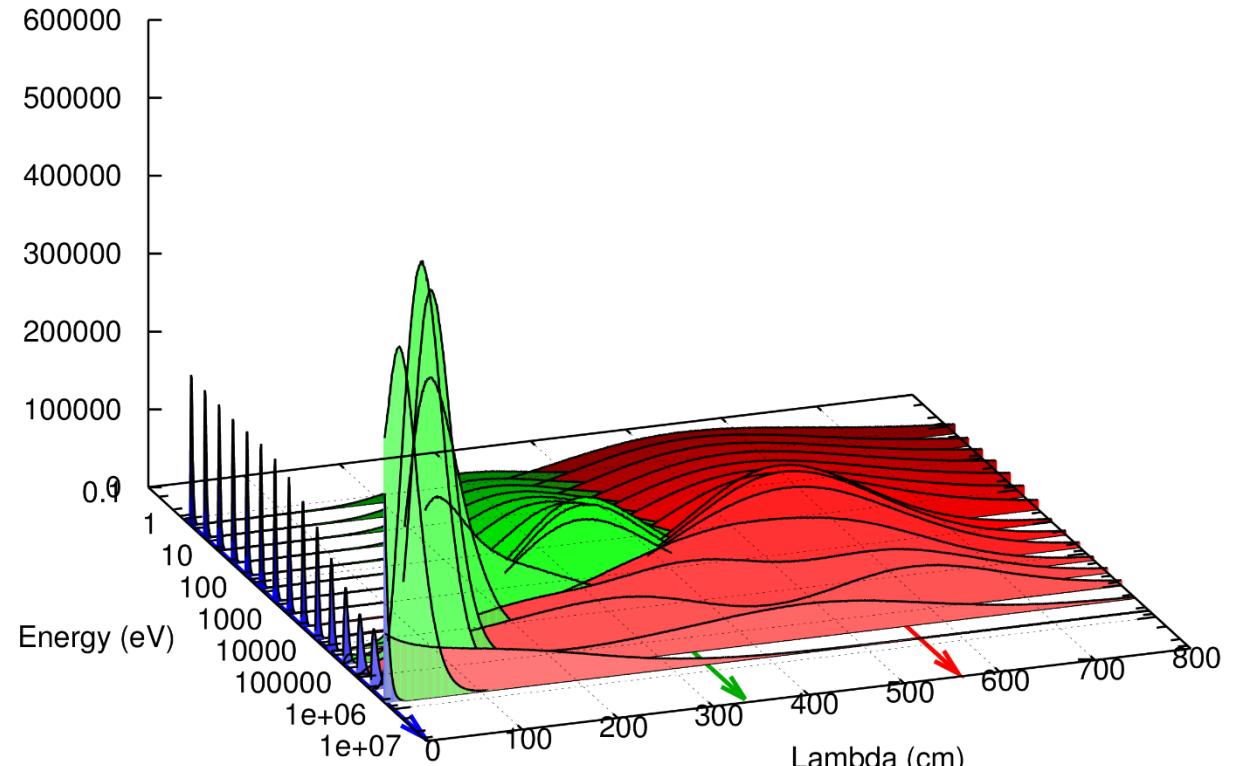
using the central limiting theorem to sum up all contributions:

For ($A \gg 1$)

$$\overline{\left(\frac{\Delta E}{E} \right)^2} \approx \frac{8}{3A}$$

For H ($A=1$)

$$\overline{\left(\frac{\Delta E}{E} \right)^2} = \frac{7}{3}$$



Effective Neutron Path Spread

- **Lead:**

$$\sqrt{(\Delta E/E)^2} = 11.4\%$$

$$\Delta l \approx 32\text{cm}$$

- **Aluminum:**

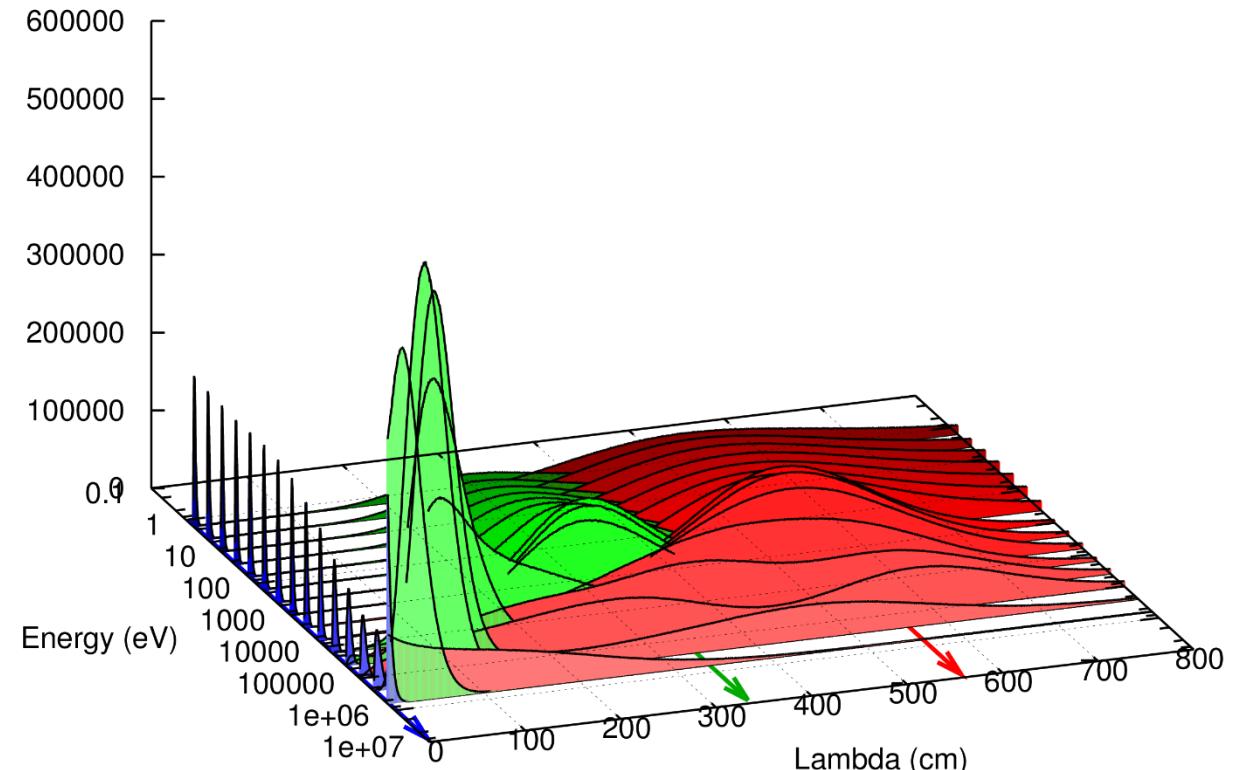
$$\sqrt{(\Delta E/E)^2} = 31.4\%$$

$$\Delta l \approx 53\text{cm}$$

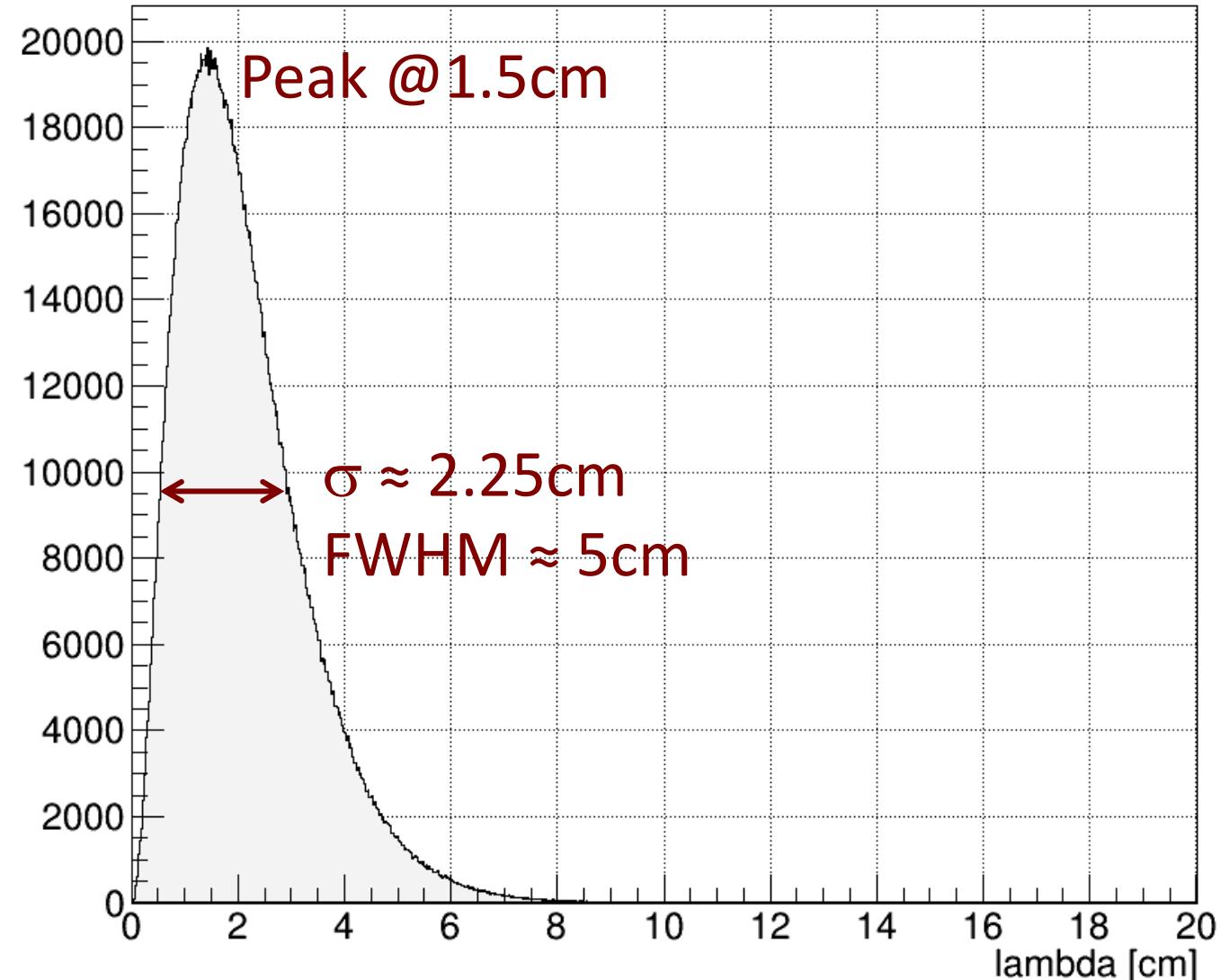
- **Water:**

$$\sqrt{(\Delta E/E)^2} = 150\%$$

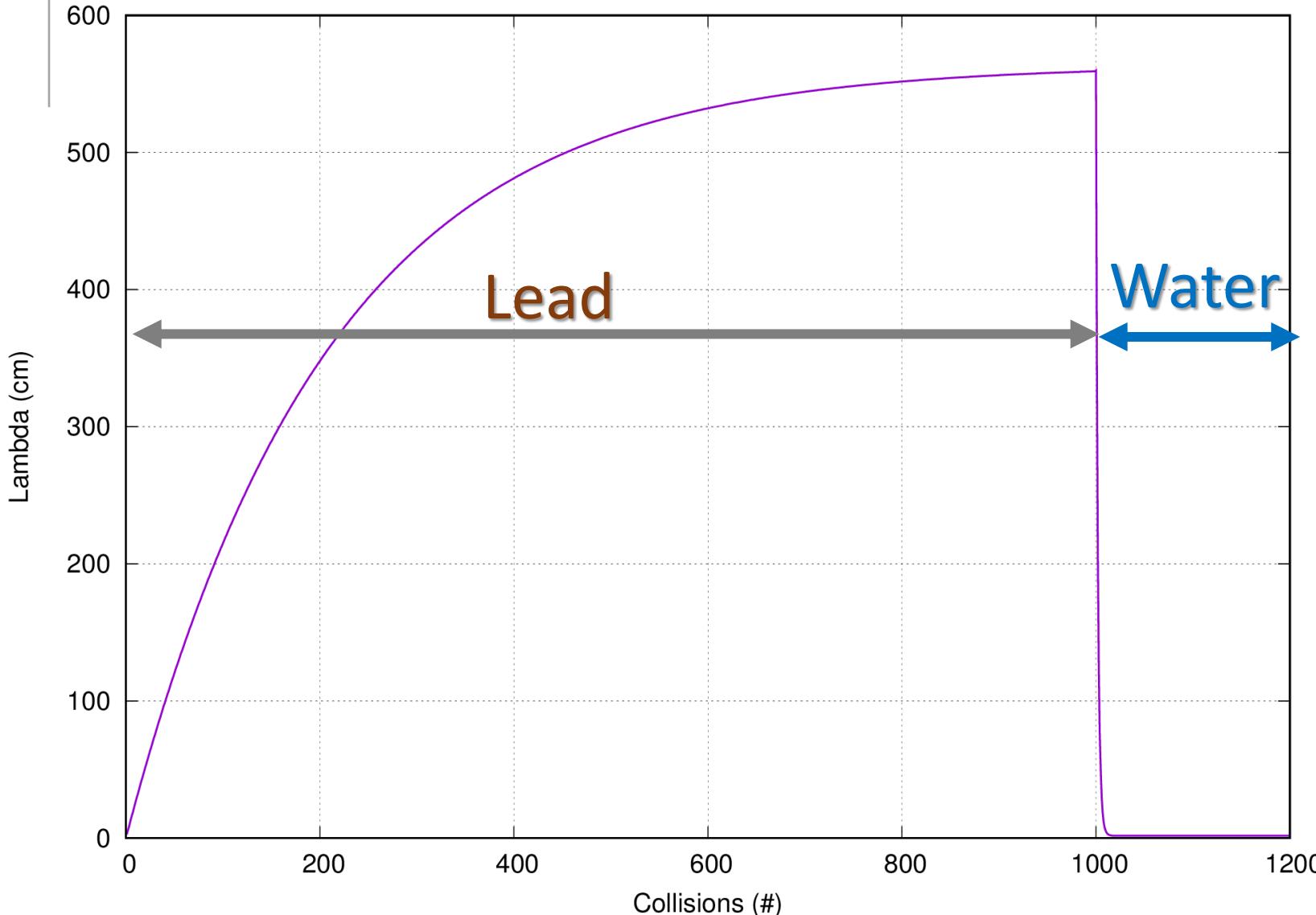
$$\Delta l \approx 2.25\text{cm}$$



Water Energy resolution @1eV



Lambda vs # neutron collisions

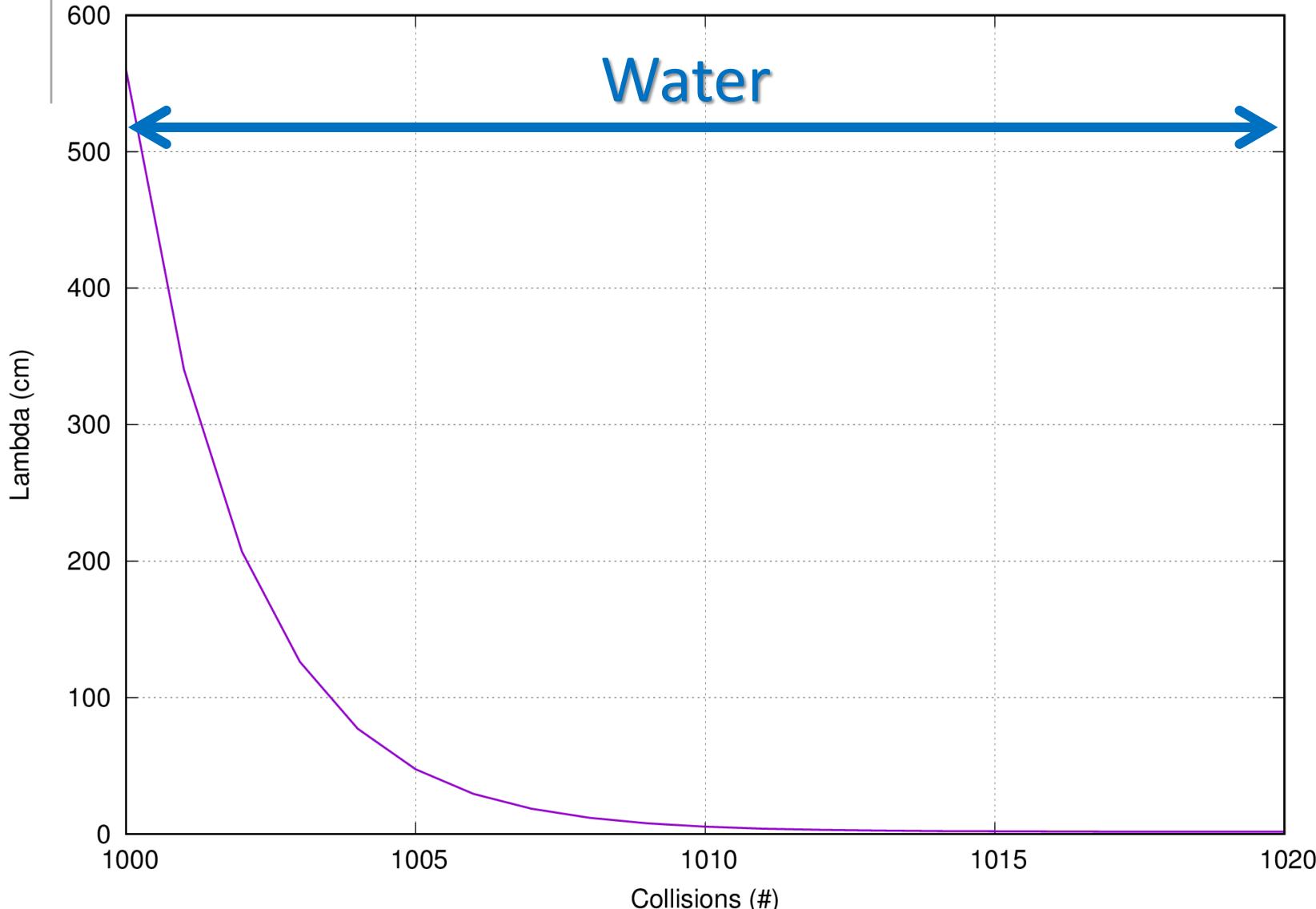


Note:

- to thermalize 2MeV in Pb we need ~ 1900 collisions
- $n=1000 \text{ col} \approx \text{keV}$ energies
- Average distance traveled (moderation path)

$$\begin{aligned} r &= \sqrt{2n\lambda_s^2} \\ &\approx \sqrt{2 \cdot 1000 \cdot 2.5^2} \\ &= 111 \text{ cm} \end{aligned}$$

Lambda vs # collisions

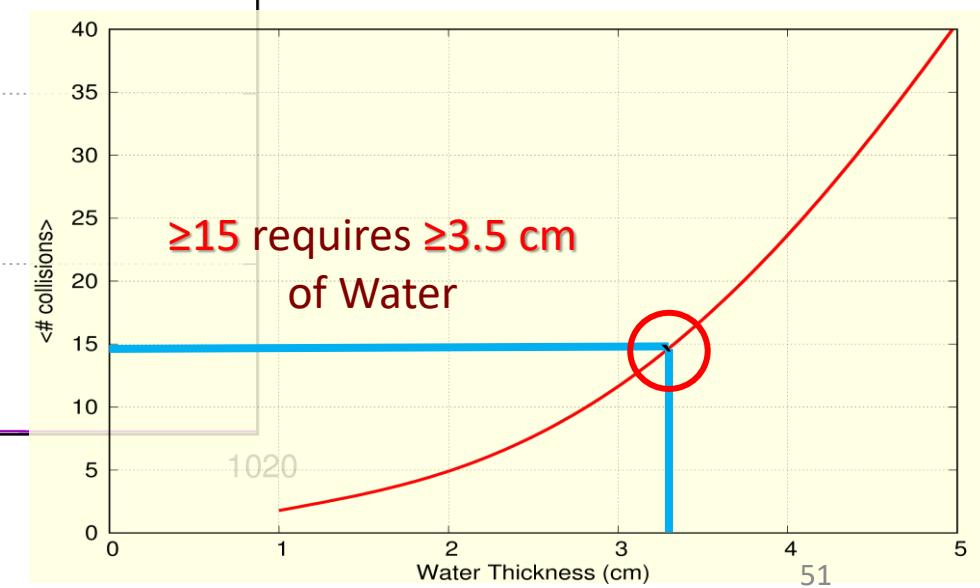
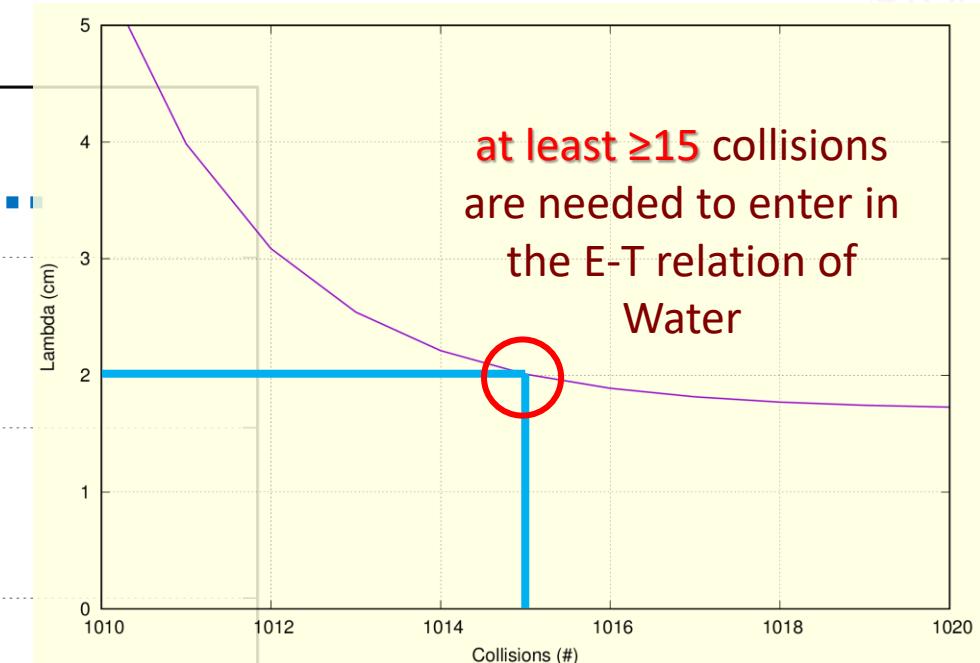
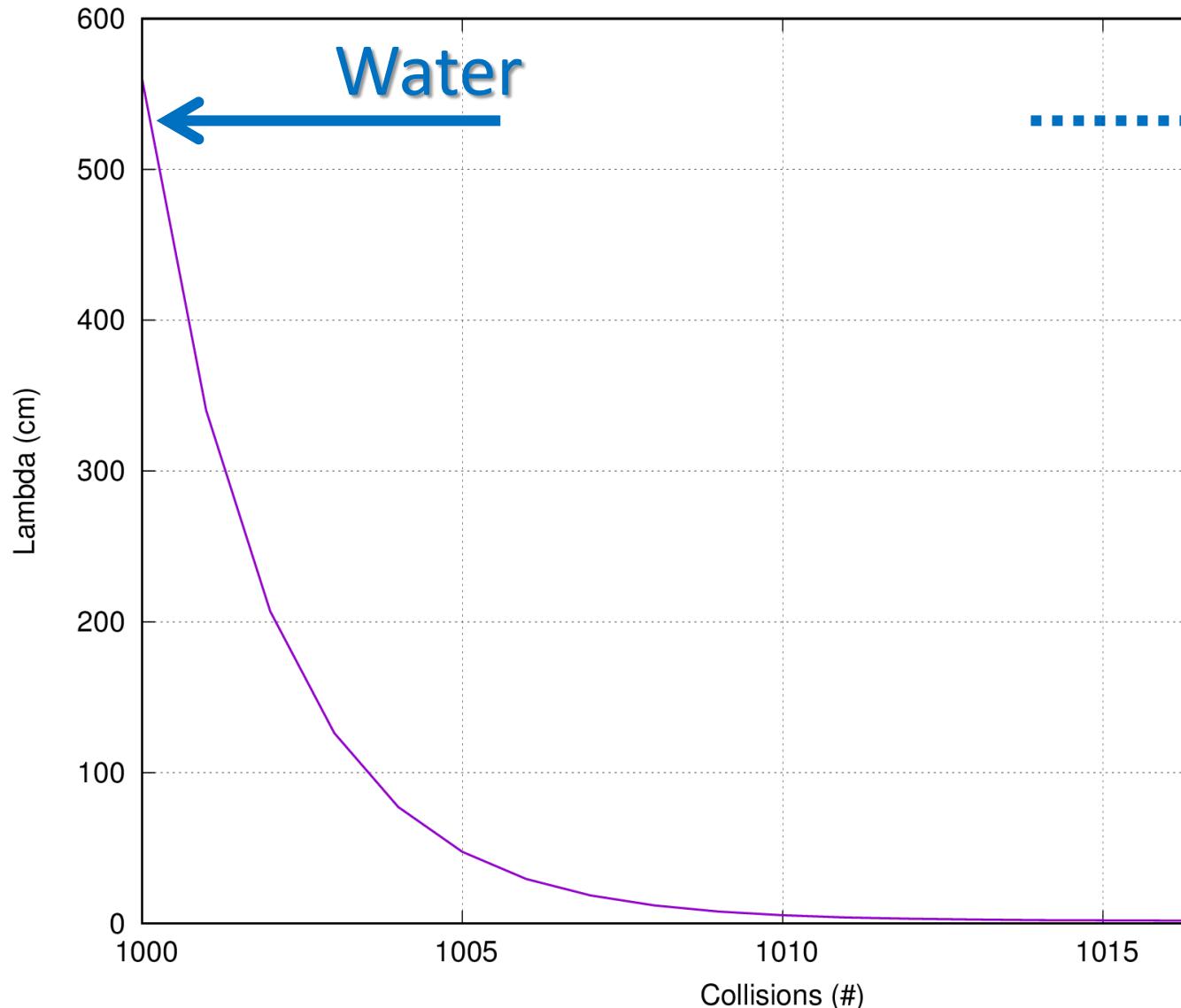


Note:

- to thermalize 2MeV in Water (due to H) we need ~ 18 collisions
- $n=10$ col \approx keV energies
- Average distance traveled (moderation path)

$$\begin{aligned} r &= \sqrt{2N\lambda_s^2} \\ &\approx \sqrt{2 \cdot 10 \cdot 0.67^2} \\ &= 3.0 \text{ cm} \end{aligned}$$

Lambda vs # collisions



Optimization: Figure of Merit

Distance dependence

- Neutron Fluence:

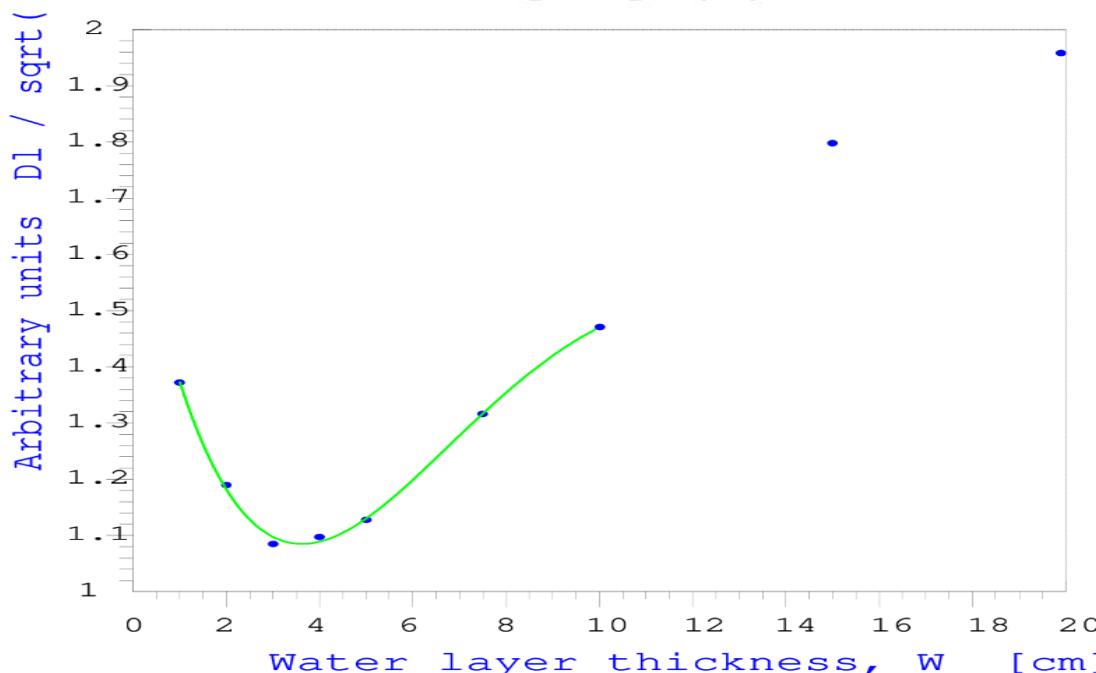
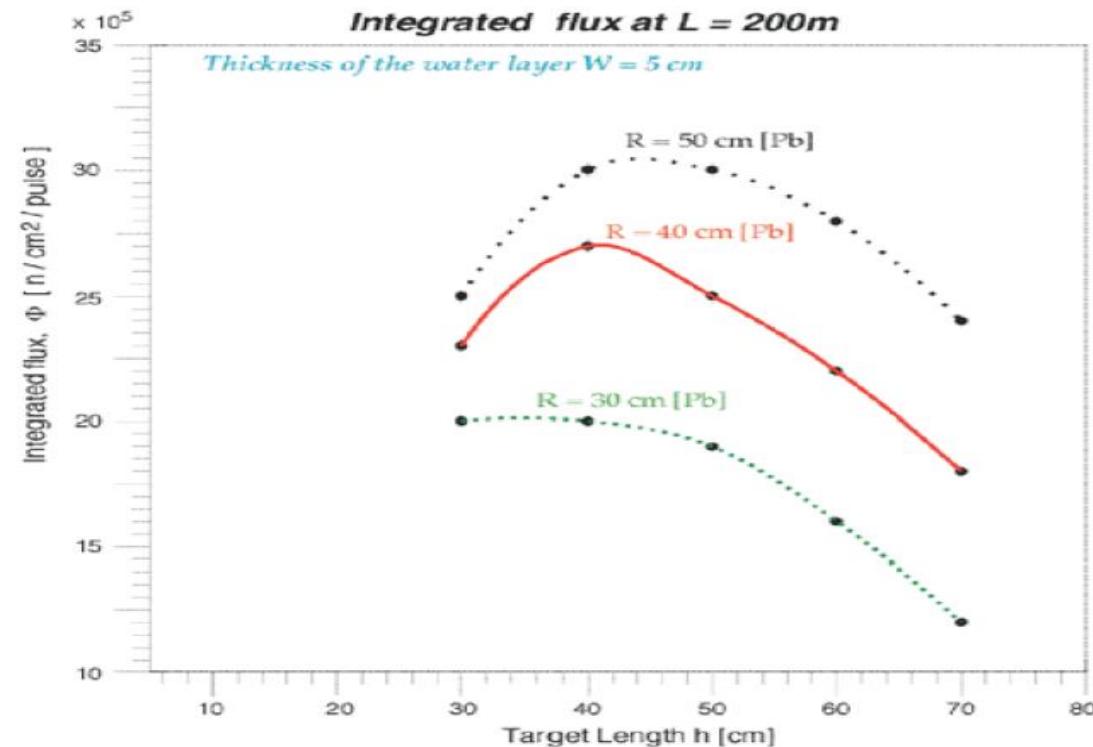
$$\Phi = \frac{\Phi_0}{L^2}$$

- Resolution:

$$\frac{\Delta E}{E} = 2 \frac{\Delta l}{L + l} \approx 2 \frac{\Delta l}{L}$$

- Figure of Merit

$$\frac{\Delta E/E}{\sqrt{\Phi}} \approx \frac{2\Delta l}{\sqrt{\Phi_0}}$$



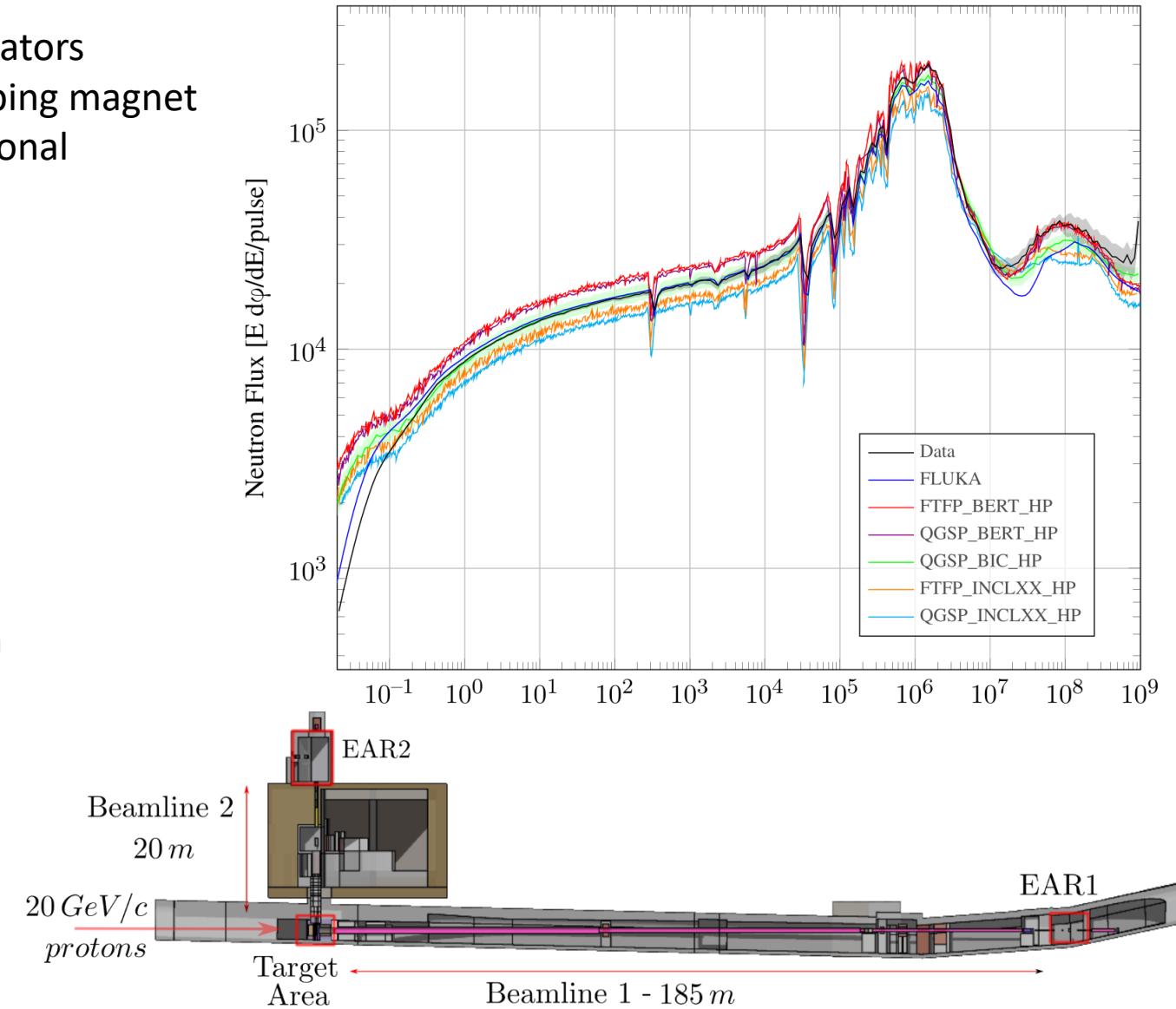
Neutron source optimization recipe

Ingredients:

- A fast accelerator
- 2 collimators
- Freshly heavy A target (with low XS)
- 1 sweeping magnet
- Room temperature water
- ^{10}B optional

Instructions:

1. If you have a fast accelerator lying around, Spallation is your best friend.
2. Cut the heavy A target to dimensions (to contain 95% of the shower):
 - Length $3\text{-}4 \lambda_{\text{inel}}$
 - Radius $>1 \lambda_{\text{inel}}$
3. Shoot fast protons on it
4. Soak the produced spallation neutrons in room temperature water, $\sim 4\text{cm}$ in length
 - Optional: to spice it up add a jest of ^{10}B
5. let them fly in vacuum
6. collimate
7. use a sweeping magnet to remove charged particles
8. collimate again
9. enjoy your neutron spectrum



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