

Characterization of irradiated silicon structures by microwave absorption techniques

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OUTLINE

- *Motivation of direct control of carrier decays*
- *Measurement regimes: MWA/R - slit antenna, MWR - coaxial cable needle probe*
- *Evaluation of carrier decay parameters*
- *Excess carrier decay temperature variations*
- *Comparison with DLTS data in e-irradiated diodes*
- *Summary*

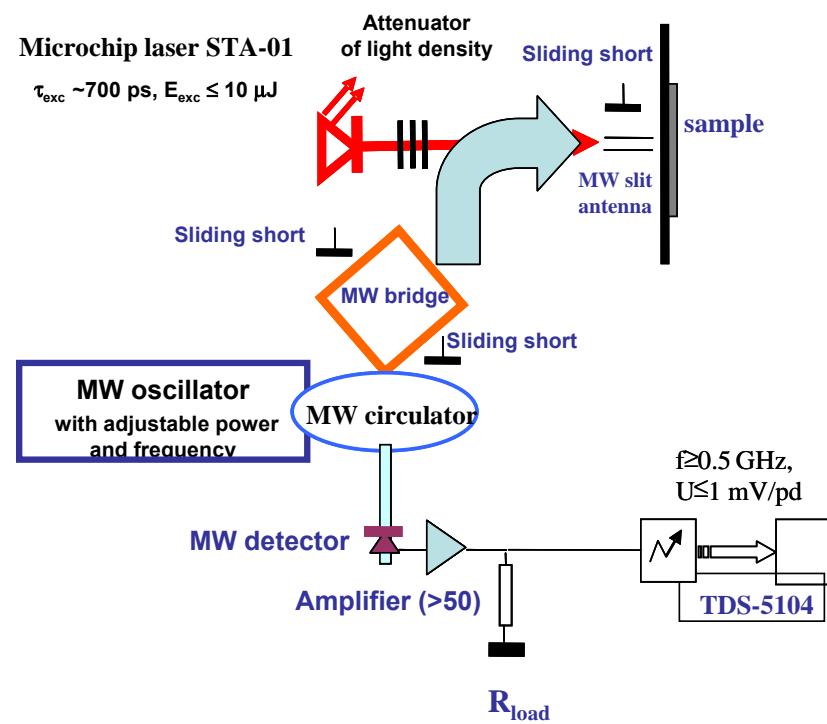
Why lifetime direct control?

- In the irradiated material different types of defects appear: some of them are important in formation of the space charge, while other are prone to transform and “wait” to become active
- Control of the defect types in the sample can be performed by using the direct methods by stimulating defect manifestation, varying measurement regimes and the most important external factors, e.g. λ_{exc} , BI, T, I_{exc} etc.
- The light pulse is a mean to force the defect system to react and the conductivity change can be detected.
- Any change of the system of defects can be revealed: the main difficulty is to interpret the situation, e.g. whether there is transform of traps or a new channel of competition between traps and recombination centers.
- Our activities - to design the instruments for analysis of peculiarities of photoresponse and to suggest the methods of extracting the valuable information from the measurement data.

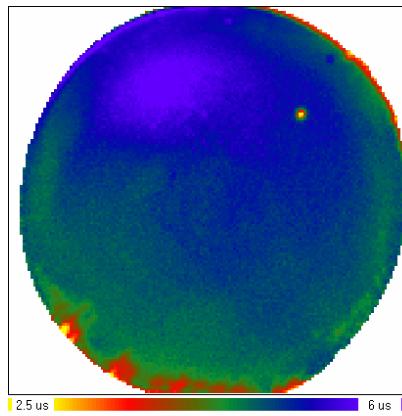
Motivation of non-invasive direct transient techniques

- ☼ PC measurements can be implemented by using contacts (TCT) or by contact-less probe - microwaves.
- ☼ Contacts and polarization of sample under bias involve additional problems. Microwave methods are free of contact problems, thus, enabling one to examine the decay temperature variations in order to extract the activation energy of the recombination and trapping centers, to correlate with parameters estimated by electrical methods as DLTS.
- ☼ The non-invasive contact-less methods can be implemented by using distant measurements, thus, can be applied to control the parameters of detector material just after the irradiation or even during irradiation.

Analyser of the recombination parameters



Round Robin calibration of the MWR instruments by using Ge, Si

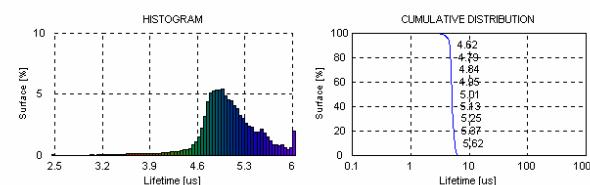


Si Phoenicon (Germany),

Si, Ge Phoenicon-Amecon (IMEC, Belgium),

Si, Ge Semilab WT-85X (Umicore, Belgium)

Si, Ge VUTEG-2 Vilnius

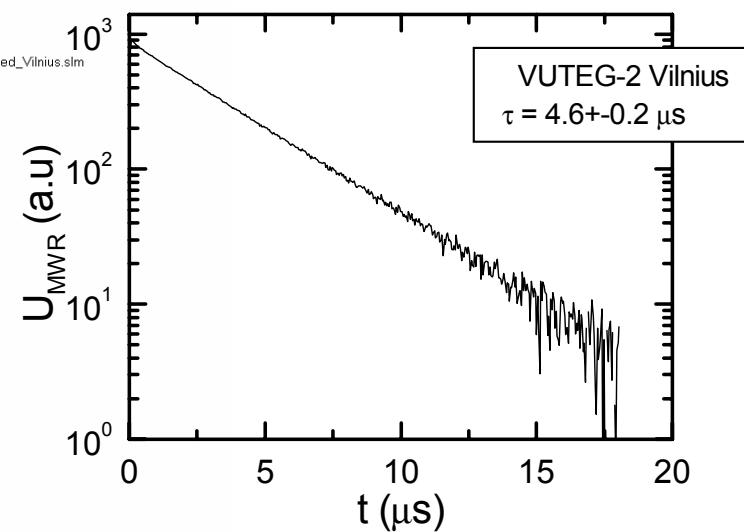


Filename: \WPSERVER301\Users\Manole\110_oxidized_Vilnius.slm
Comment: after oxidation Vilnius 110 Si
Date/Time: 19.07.2005 09:53
Operator: MM
Sample: 110 Vilnius
Raster: 500 um
Size: 3 inch
Scansradius: 38.05 mm, 37.29 mm

■ u-PCD

Lifetime:
Average: 5.053 us
Median: 5.0520 us
Deviation: 8.965 %
Minimum: 1.803 us
Maximum: 6.58 us

Time Range: 0.1 ms
Time Cursor: Auto
Sensitivity: 100 mV
Averaging: 64
MW Freq.: 10.489 GHz
Laser Power: 120 E10
Pulse Width: 200 ns
Bias Lamp Pd20mSun
Laser Wavel. 304 nm
Head Height: 0 mm



Samples and irradiations

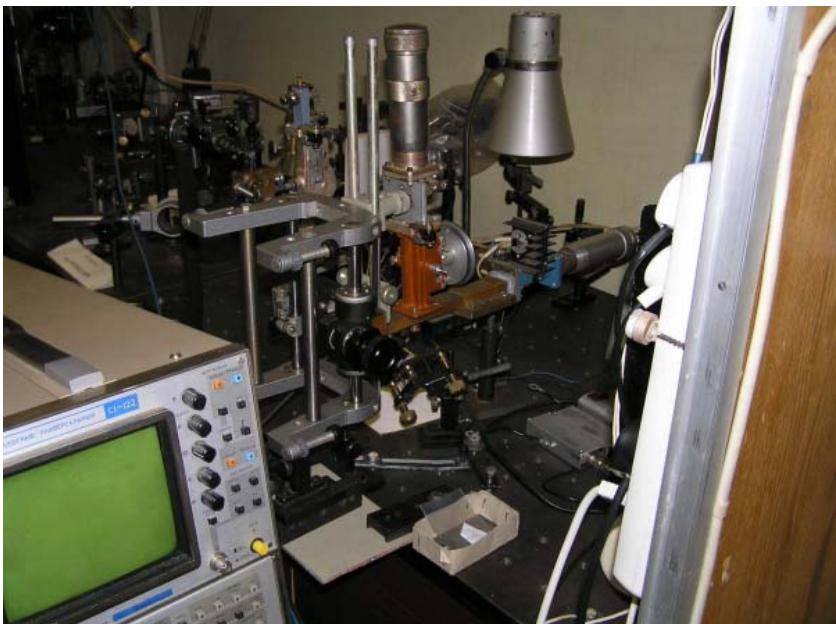
Samples investigated for inter-instrument carrier lifetime calibration:

- I.1. MCZ Si sample $20 \times 5 \times 5$ mm 3 with two surfaces polished. This sample of about 6 kOhm cm resistivity is mounted with load resistor for simultaneous control of contact photoconductivity.
- I.2. Phosphorous doped Cz Si $20 \times 5 \times 5$ mm 3 sample with two surfaces polished.
- I.3. Phosphorous doped Cz Si 5 mm thick half-wafer with polished surfaces.
- I.4. Borum doped Cz Si Cz Si $5 \times 5 \times 5$ mm 3 sample with two surfaces polished.
- I.5. Borum doped Cz Si 5 mm thick half-wafer with polished surfaces.
- I.6. MCZ n-Si wafer piece of $20 \times 20 \times 0.28$ mm 3 dimensions. Surfaces are passivated by thermal oxidation.
- I.7. N-type Ge 352-3 wafer of 500 μm thickness with polished, varnish passivated surfaces.
- I.8. P-type Ge 327-4 wafer of 500 μm thickness with polished, varnish passivated surfaces.

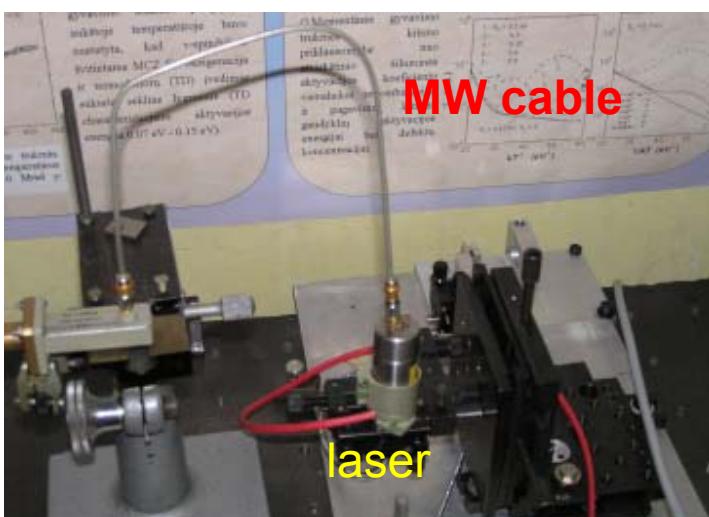
-  high resistivity MCZ and FZ silicon wafers and diode structures
-  irradiated by high energy electrons, γ -rays, and protons

Measurement instruments available at VU: MWA & MWR - slit antenna, MWR - coaxial needle-tip probe, DLS-82

MWA 10 GHZ probe

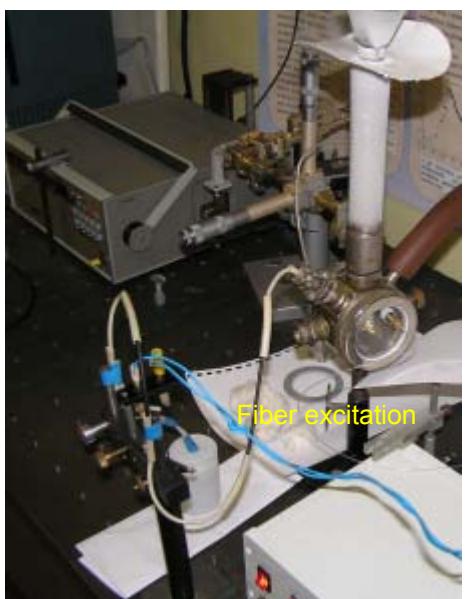
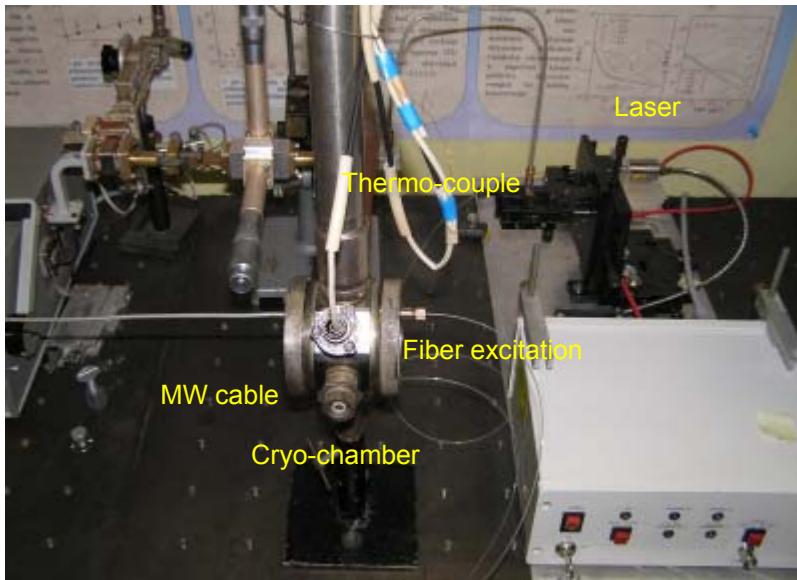


MWR 22 GHZ probe
slit antenna probes

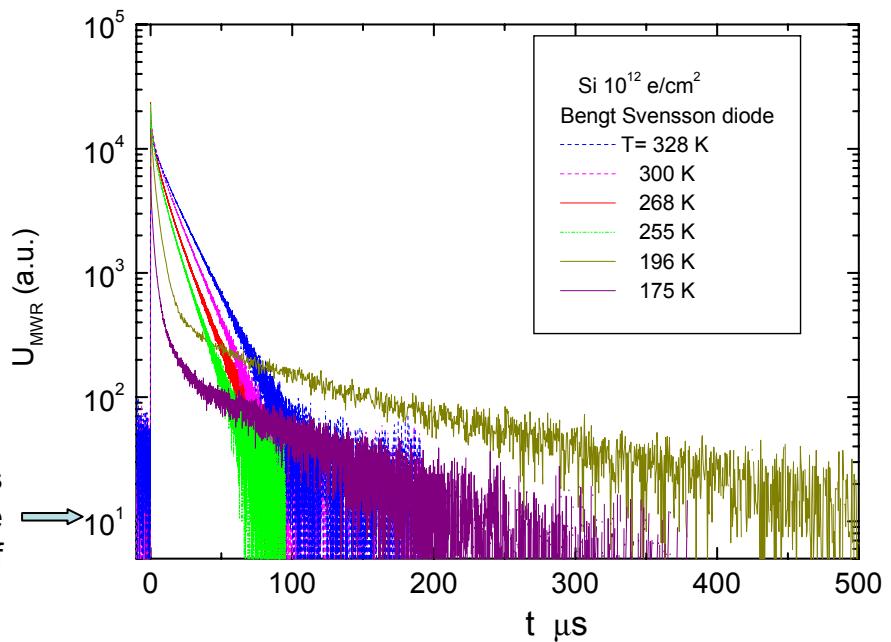


**Microwave coaxial
needle-tip antenna probe**

Cryogenic microwave needle tip -antenna probe integrated with the fiber excitation probe

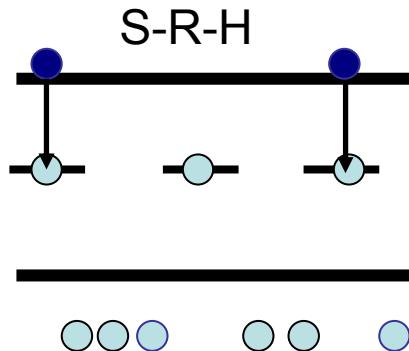


MWR transient variations with temperature in Si diode irradiated with electrons of fluence $3 \times 10^{12} \text{ e/cm}^2$



Dominant single level

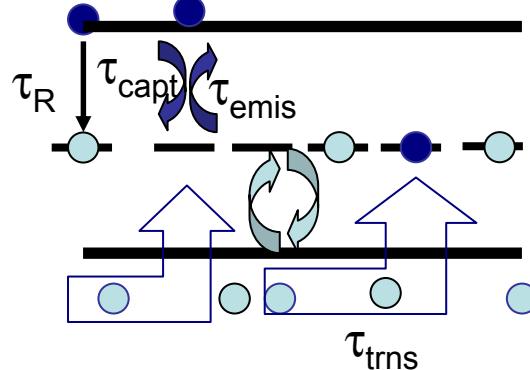
Low defect concentration



Carrier pair decay lifetime

High defect density

Blackmore recombination-trapping



Different e & h decay lifetimes,
while the effective lifetime is the longest of

$$\tau_{\text{capt}}, \tau_{\text{trns}}, \tau_{\text{emis}}$$

$$\tau_{R, \text{S-R-H}} = [\tau_{cp}(n_0 + n_{ex} + N_C e^{-(E_c - E_m)/kT}) + \tau_{cn}(p_0 + n_{ex} + N_V e^{-(E_m - E_v)/kT})] / [n_0 + p_0 + n_{ex}]$$

$$\tau_{g, \text{S-R-H}} = [\tau_{cp} N_C e^{-(E_c - E_m)/kT} + \tau_{cn} N_V e^{-(E_m - E_v)/kT}]$$

$$\tau_{g, \text{S-R-H}} \gg \tau_{R, \text{S-R-H}}$$

$$s_{R, \text{S-R-H}} = s_n s_p [n_{0s} + p_{0s} + n_{exs}] / [s_n (n_{0s} + n_{exs} + N_{it,c} e^{-(E_c - E_{it})/kT}) + s_p (p_0 + n_{ex} + N_{vit} e^{-(E_{it} - E_v)/kT})]$$

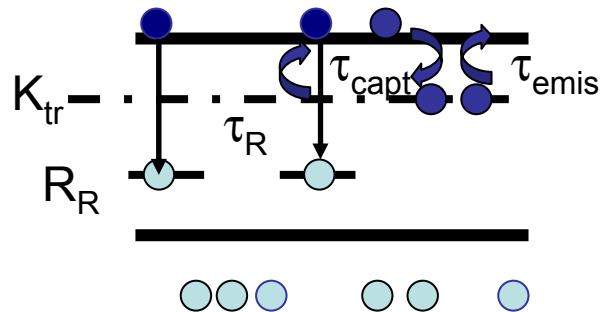
$$s_{g, \text{S-R-H}} = s_n s_p / [s_n N_{it,c} e^{-(E_c - E_{it})/kT} + s_p N_{vit} e^{-(E_{it} - E_v)/kT}]$$

$$s_{g, \text{S-R-H}} \ll s_{R, \text{S-R-H}}$$

$$s_{n,p} = \sigma_{n,p} s v N_{it} = \sigma_{n,p} s v kT D_{it}$$

System of two competing levels

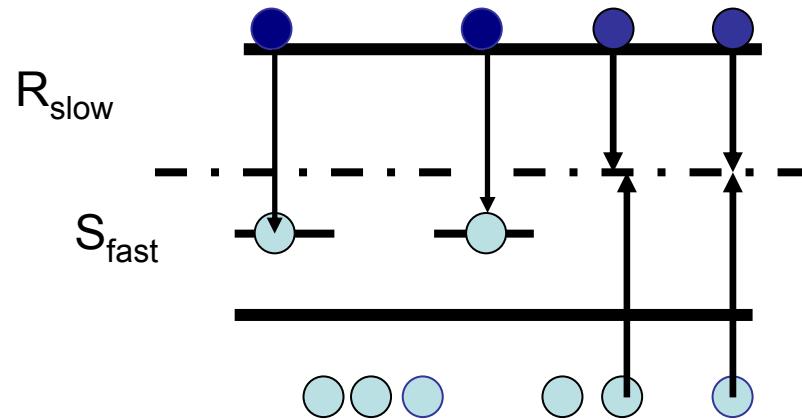
**System of recombination-trapping centers
Ryvkin' model**



Carrier decay instantaneous lifetime

$$\tau_{\text{inst}} = \tau_R K_{\text{tr}} \approx \tau_R (1 + \tau_{\text{gen}} / \tau_{\text{capt}})$$

**System of recombination centers
with different rates Lashkarev' model**

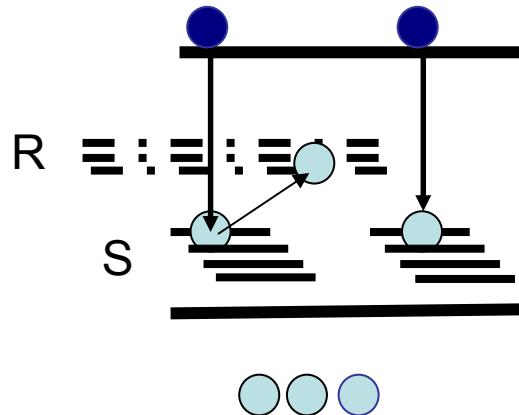


Carrier decay instantaneous lifetime

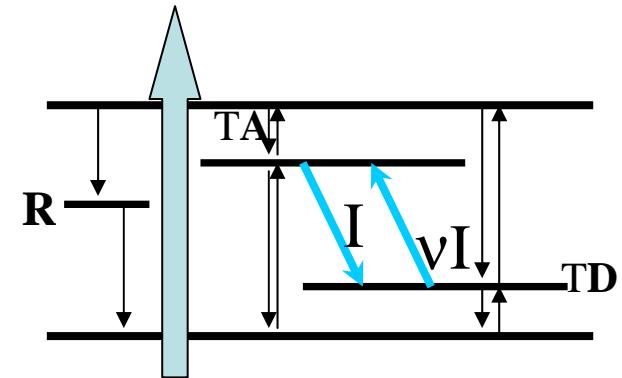
$$\tau_{\text{inst}} = -n / (dn/dt) \approx (A_S e^{-t/\tau_S} + A_R e^{-t/\tau_R}) / (\tau_S^{-1} A_S e^{-t/\tau_S} + \tau_R^{-1} A_R e^{-t/\tau_R})$$

Systems of competing levels

**Systems of recombination centers
Rose' model**



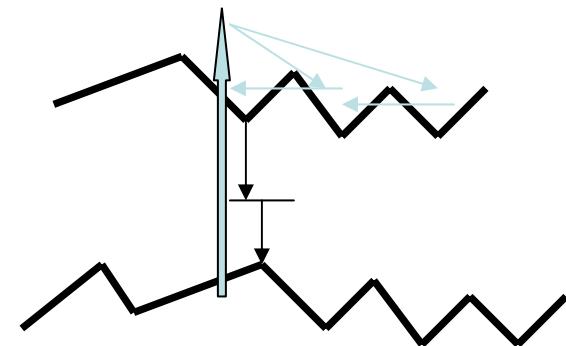
**Systems of recombination centers
W.M.Chen, B.Monemar, E.Janzen, J.L.Lindstrom & Watts' model**



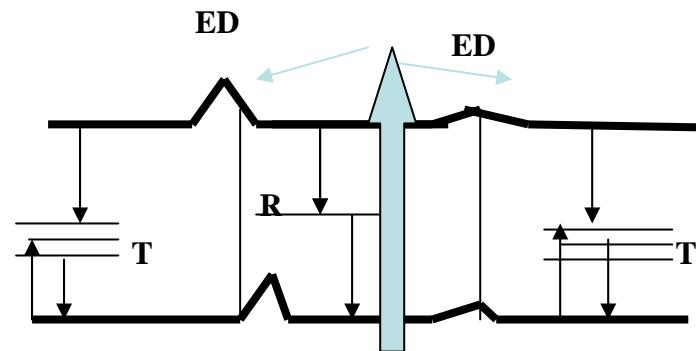
Carrier decay instantaneous lifetime
photoconductivity quenching etc. qualitative analysis

K.Takarabe, P.T.Landsberg, J.K.Liakos. Semic. Sc.Techn.(1997)
W.M.Chen, B.Monemar, E.Janzen, J.L.Lindstrom. Phys.Rev.Lett. (1991)

More complicated recombination-trapping processes

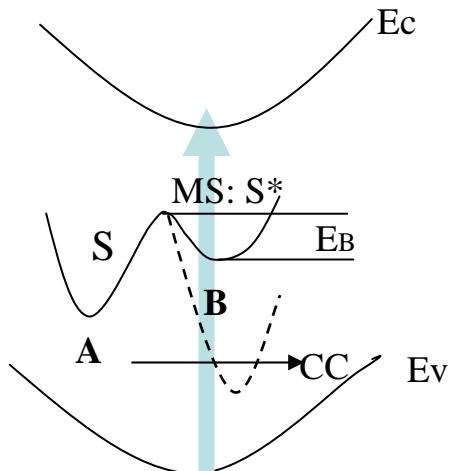


Carrier escape and motion barriers

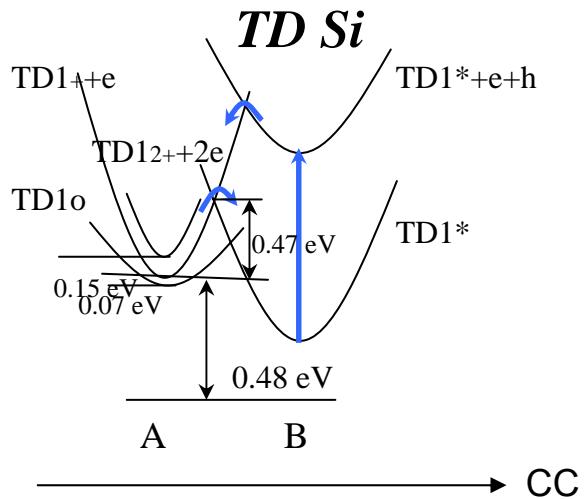


Extended defects: clusters, SiO_x precipitates, disorder etc.

G.Pfister,H.Sher Adv.Phys1978), P.T.Landsberg. Rec. Semic.(1991),
S.Havlin, D.Ben-Avraham. Adv. Phys. (2002)



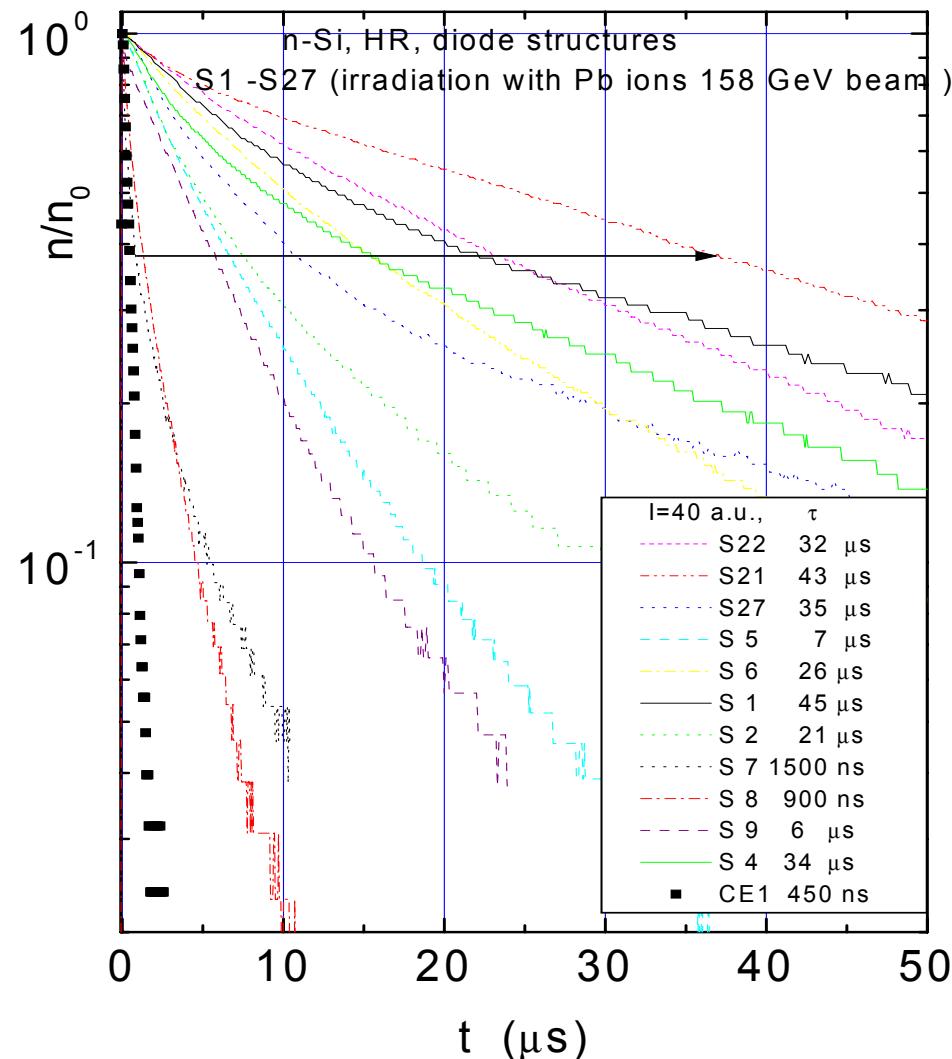
Metastable centres V-O, TD, etc.



G.Watkins SST(1991)
A.Chantre Appl.Ph.A(1989)

Carrier recombination

☀ Recombination in the heavy irradiated material (nearly mono-exponential transients)

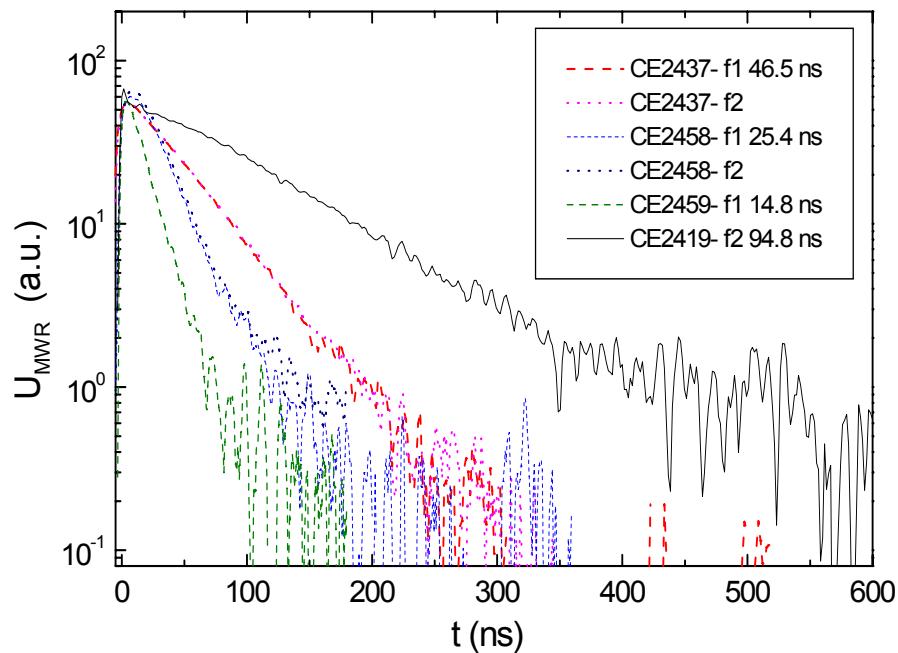


Carrier recombination

Excess carrier decay transients in proton irradiated diodes.

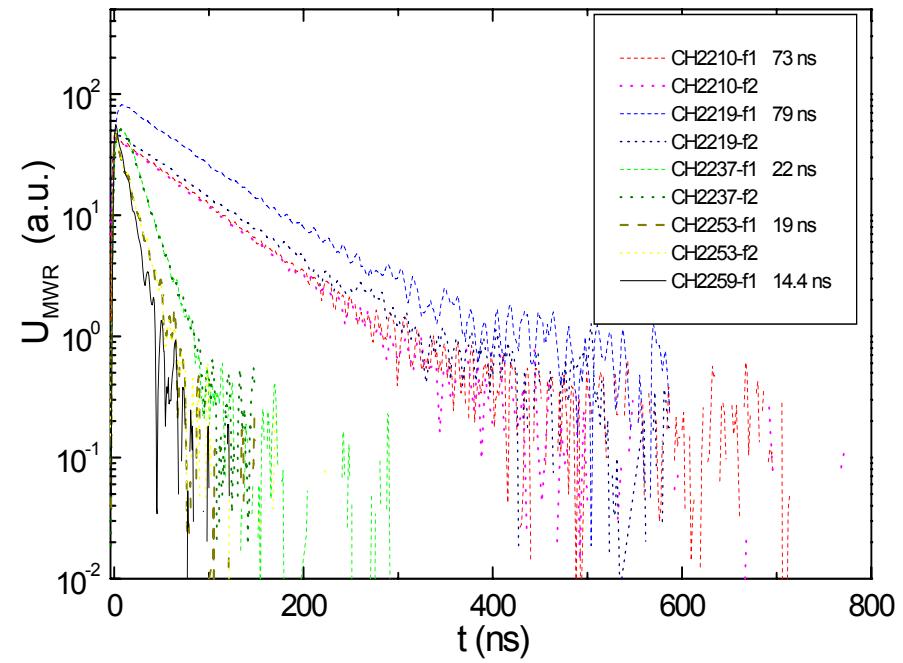
Material: Wacker FZ Si, <100>, $6\text{k}\Omega\text{ cm}$

CIS CE O-diff no

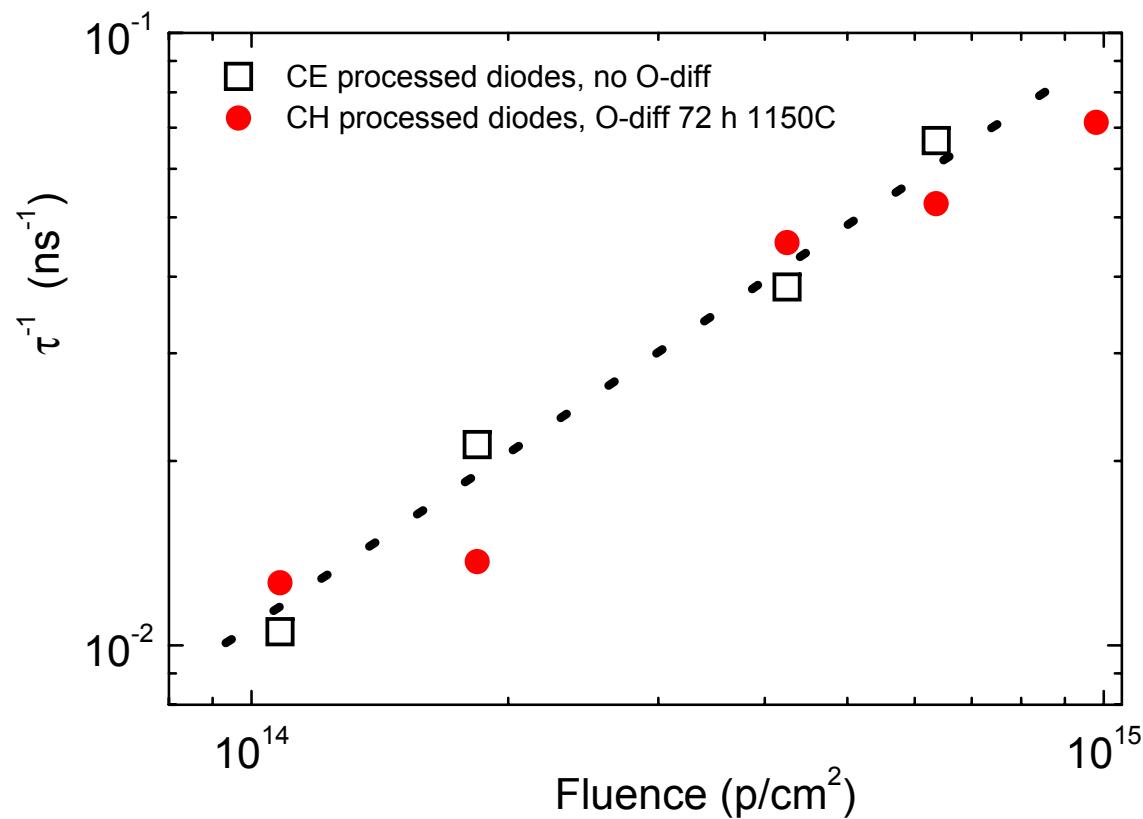


Diodes processed:

CIS CH O-diff 75hN2 1150C



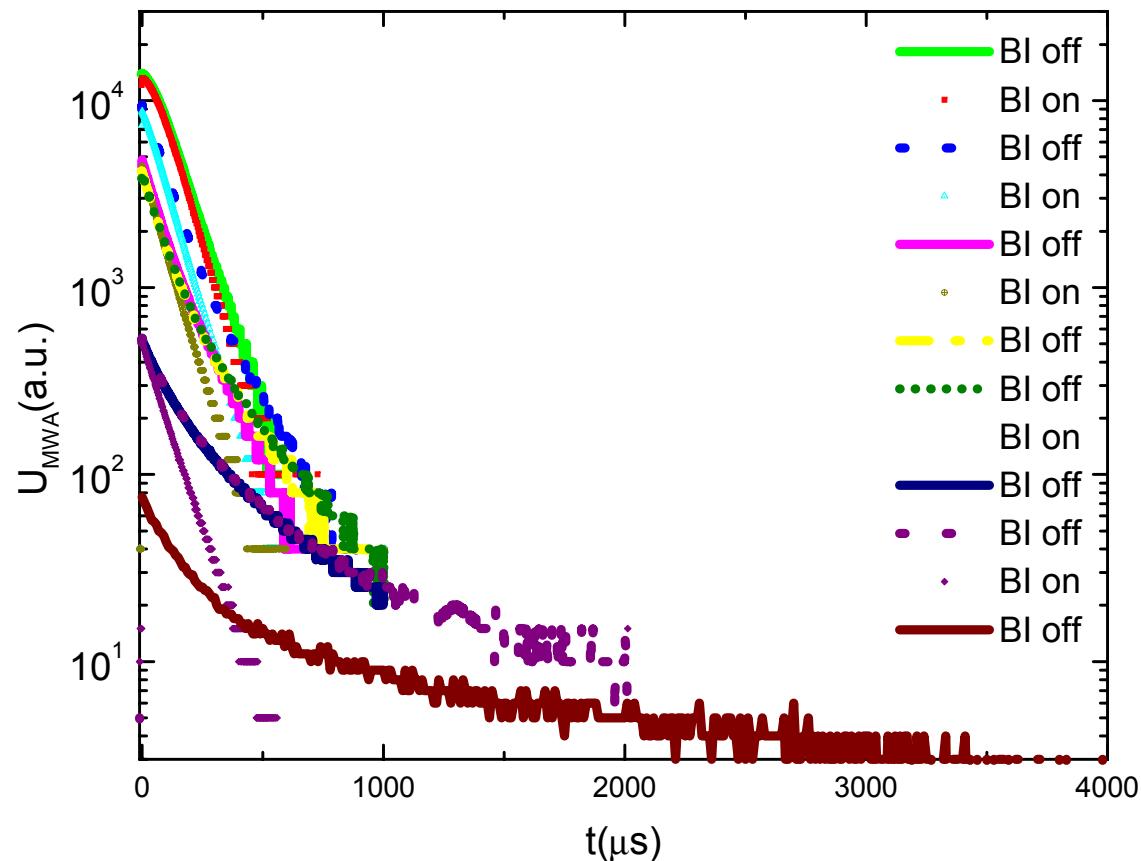
Carrier recombination



Decay lifetime dependence on irradiation fluence

Carrier recombination and trapping

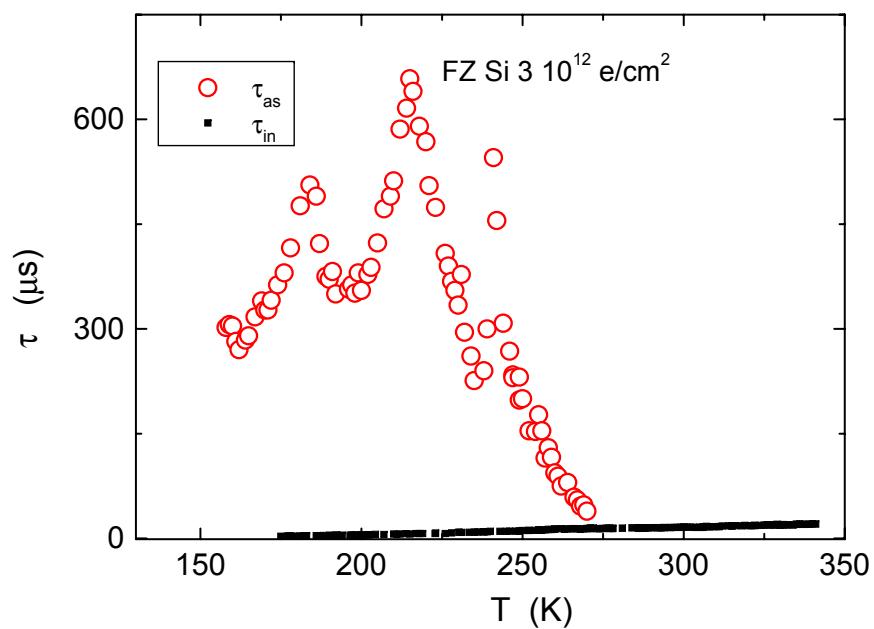
⌚ Recombination (fast) and trapping (slow) constituents within transients of microwave absorption by free carriers (MWA) have been distinguished by combining analyses of the excess carrier decays dependent on the excitation intensity and bias illumination (BI).



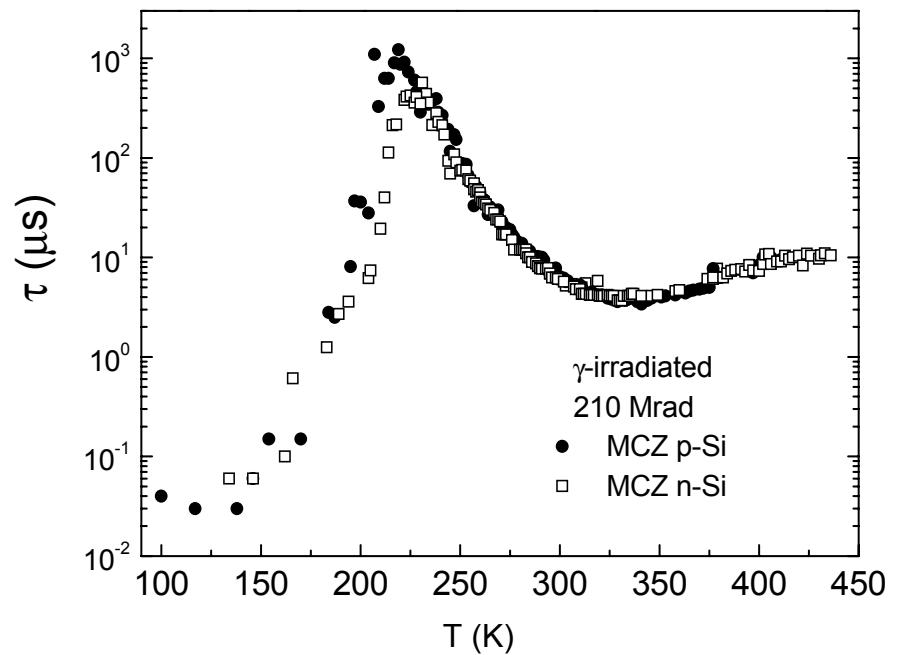
Variation of MWA decays with excitation intensity (proportional to the initial amplitude) with and without additional cw illumination

Excess carrier decay temperature variations

MWR coaxial needle-tip probe
e-irradiated FZ Si

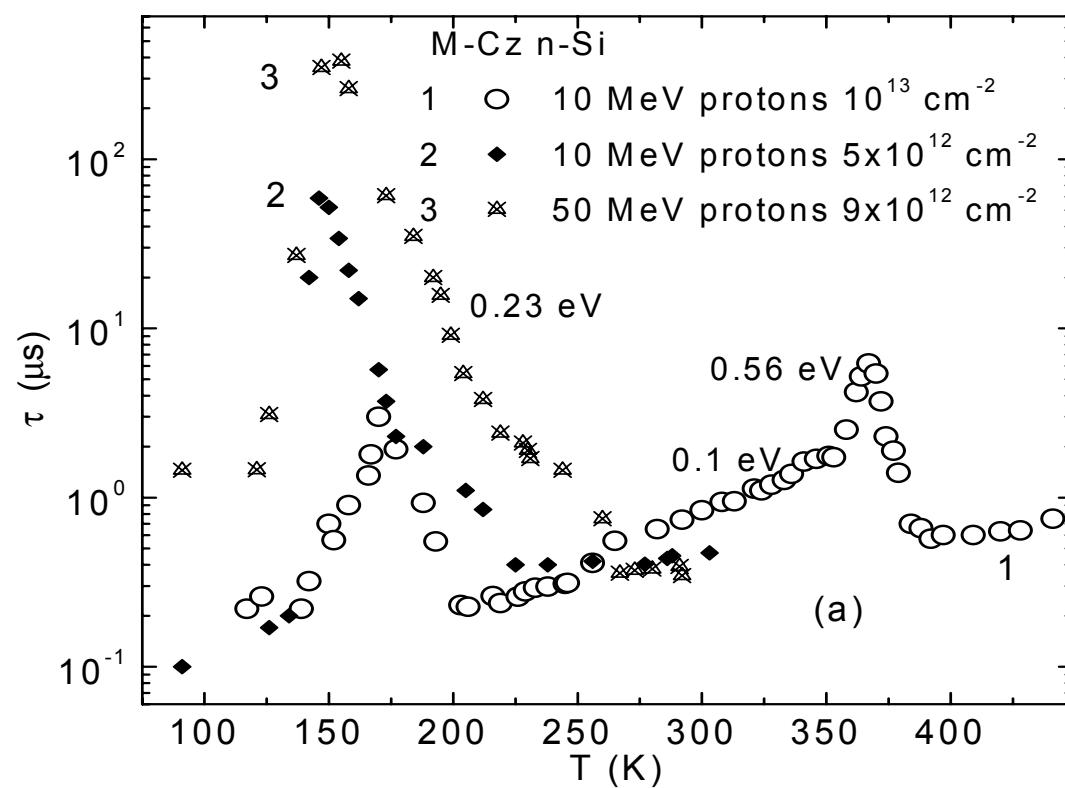


MWA slit antenna
 γ -irradiated MCZ Si

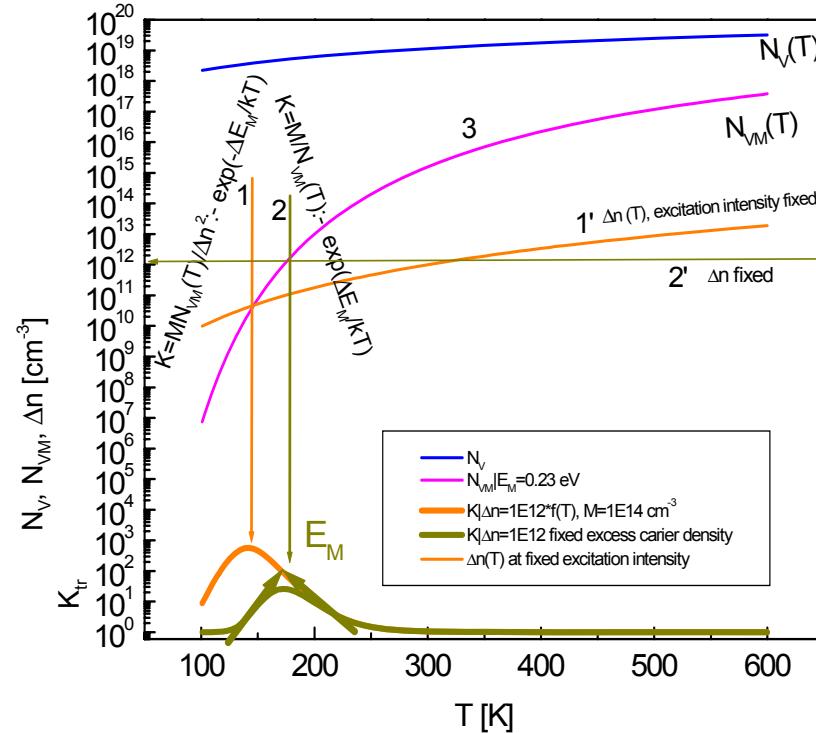
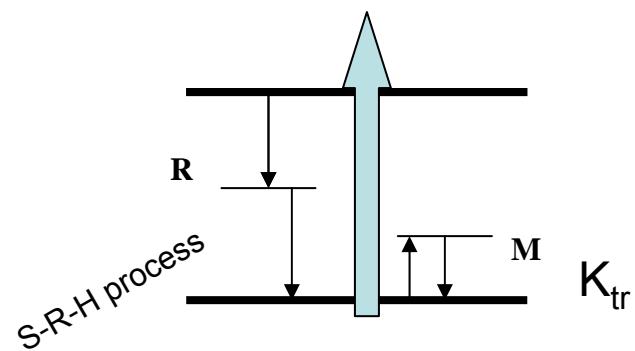


Excess carrier decay temperature variations

MWR proton-irradiated FZ Si



Qualitative simulation of the temperature dependent lifetime variations

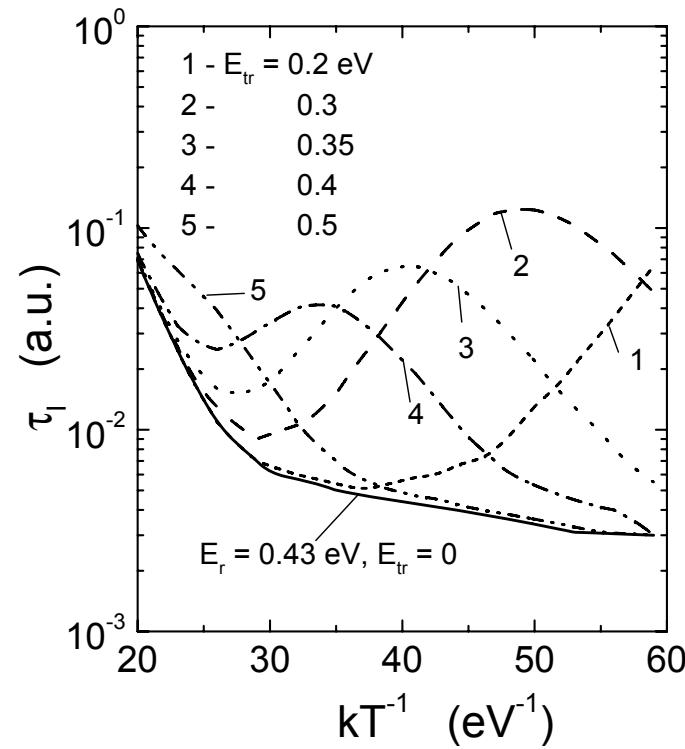


Variation of trapping coefficient K_{tr} with temperature, and formation of lifetime extrema at either fixed excess carrier density or for invariable excitation intensity

$$\tau_{inst} = \tau_R K_{tr} (1),$$

$$K_{tr} = [1 + M N_{VM}/(N_{VM} + \Delta n)^2] (2)$$

$$N_{VM} = N_V \exp(-\Delta E_M/kT)$$



Variation of instantaneous lifetime with trap level position vs. inverse thermal activation factor at simultaneous recombination and trapping

Comparison with DLTS data in e-irradiated diodes

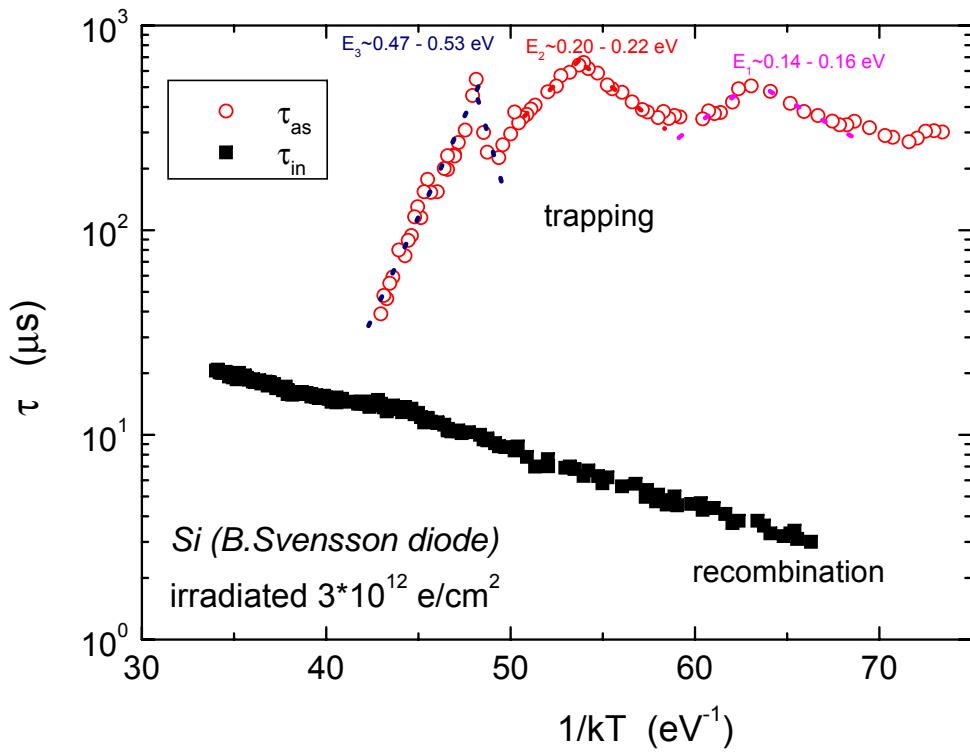


Fig. 1. Level activation energy determined by τ (T) characteristics in Si diode irradiated with electrons of fluence of $3 \times 10^{12} \text{ e/cm}^2$ by employing MWR

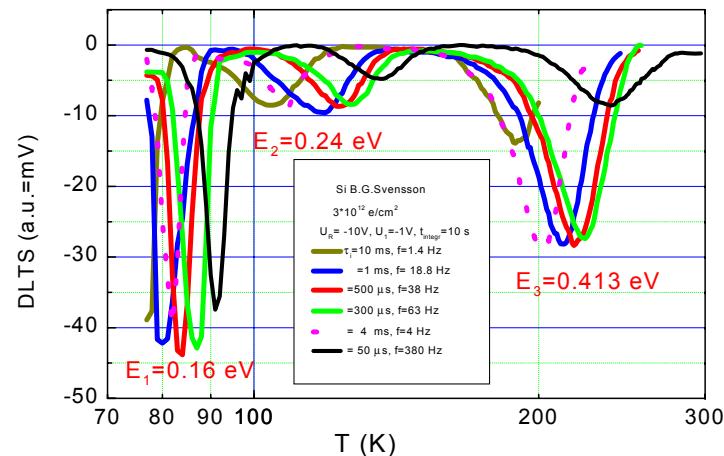
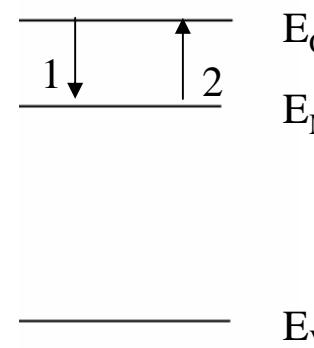
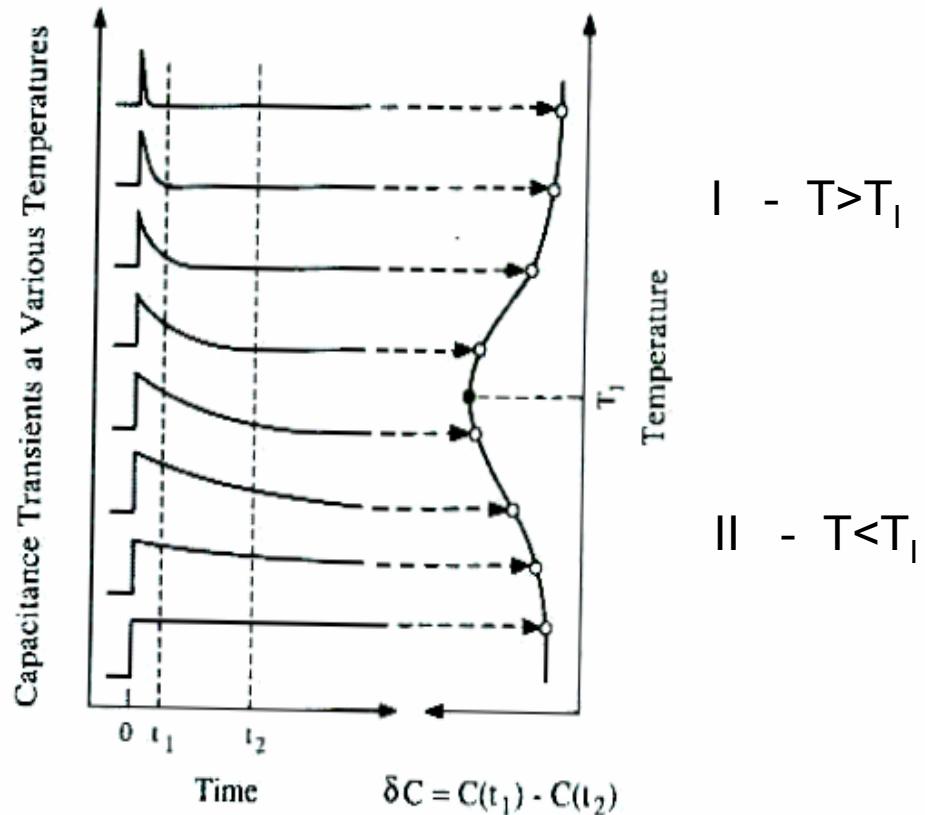


Fig. 2. Capacitance DLTS spectra measured in Si diode irradiated with electrons of fluence of $3 \times 10^{12} \text{ e/cm}^2$ by employing the temperature scan regime for different lock-in frequencies.

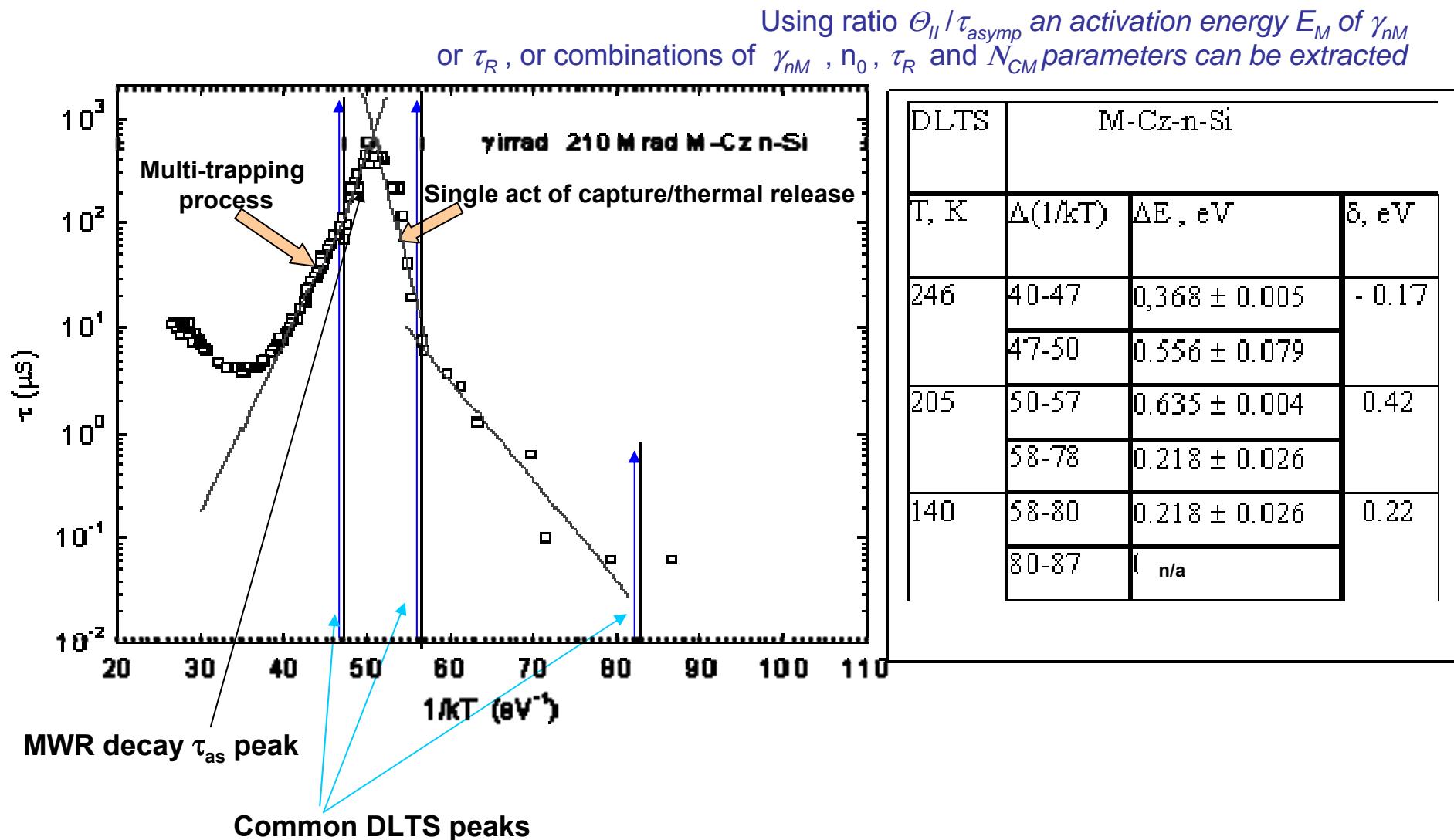
DLTS



$$\begin{aligned}
 1 \quad \tau_M &= 1/\gamma_{nM}(M-m) \\
 2 \quad \tau_N &= 1/\gamma_{nM}N_{CM} \\
 \Theta_I &= 1/[\gamma_{nM}N_{CM} + \gamma_{nM}(M-m)] \\
 \Theta_{II} &= 1/[\gamma_{nM}N_{CM}]
 \end{aligned}$$

Fig. 7.11 Implementation of a rate window by a double boxcar integrator. The output is the average difference of the capacitance amplitudes at the sampling times t_1 and t_2 . Reprinted with permission after Miller et al.^[55]

Precise simulation of the temperature dependent lifetime variations correlating with DLTS peaks – J.Vaitkus' method



Summary

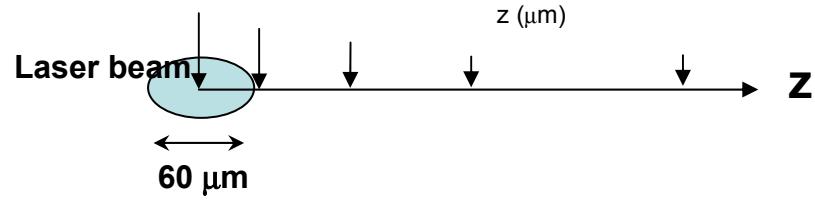
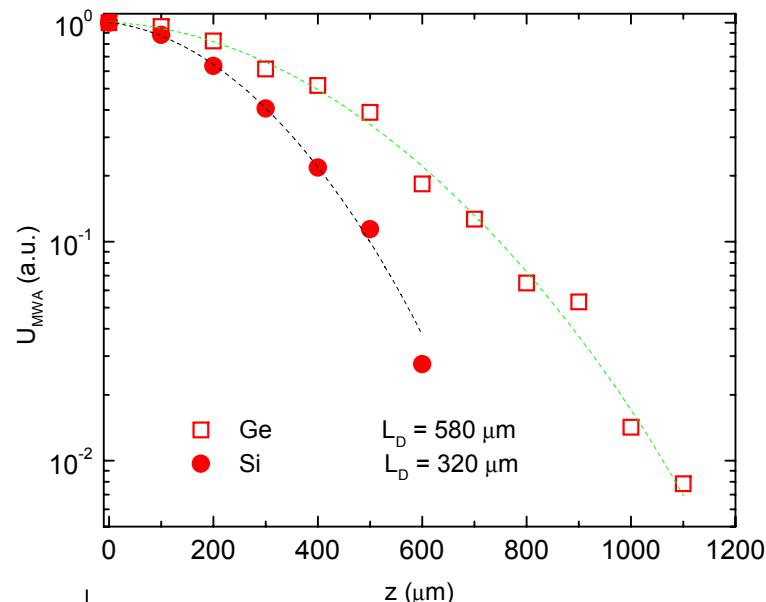
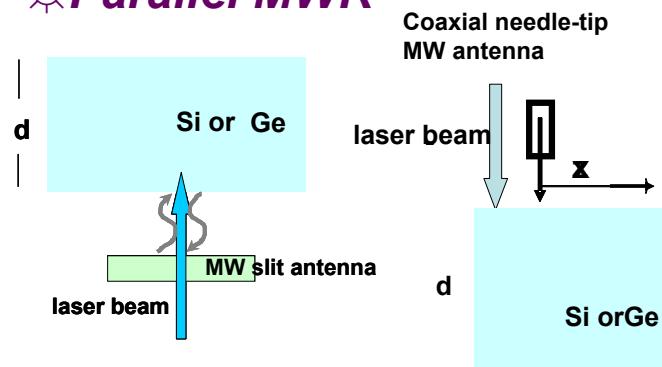
- ☼ MWR instrumentation and regimes are tested, models adjusted, software for analysis made up.
- ☼ tentative examination of recombination characteristics dependent on fluence and particle species, by MWR using $\tau(T)$, I_{exc} , λ_{exc} , BI are carried out; $\tau_{as}(T)$ variations are correlated with those determined by DLTS technique.
- ☼ activation factors of trapping (release) centers $E_1 = 0.14 - 0.16$ eV, $E_2 = 0.23$ eV and $E_3 = 0.48$ eV, have been evaluated in e-irradiated FZ Si diode from carrier lifetime variations with temperature in the range of $140 \rightarrow 350$ K. These trap activation energy values, measured by MWR using $\tau(T)$, are in agreement with those determined by DLTS technique.
- ☼ in γ -rays irradiated MCZ Si, the activation energy values of trapping and recombination (E_M and E_R) centers were obtained as follows: $E_1 = 0.14$ eV, $E_2 = 0.28 - 0.30$ eV, $E_3 = 0.38$ eV, and $E_4 = 0.48 - 0.56$ eV, by MWA using $\tau(T)$.
- ☼ Correlating DLTS and MWR transients, additional information about the centre can be extracted concerning the type of the center, capture barrier etc

Thank You for attention!

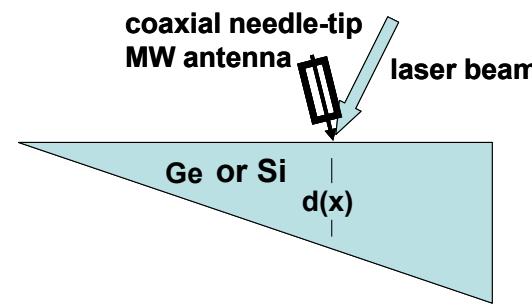
Perspective development of the MW techniques for:

- estimation of carrier transport parameters

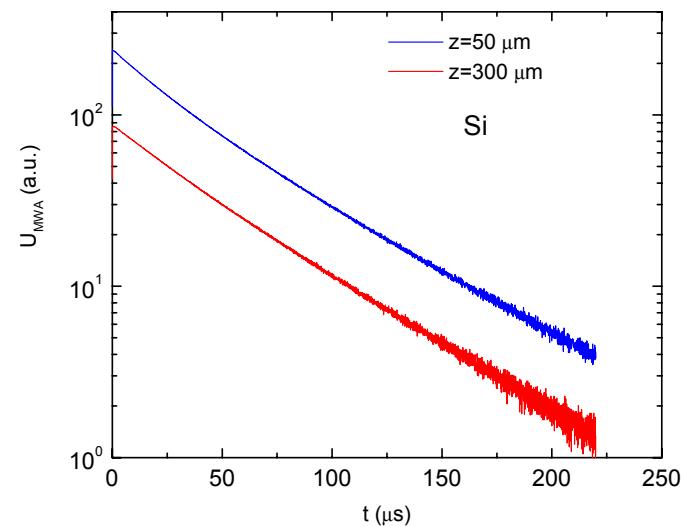
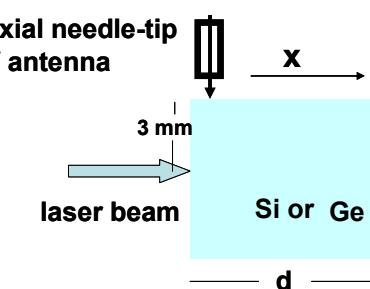
Parallel MWR



Oblique MWR



Perpendicular MWR



$$L_{\min} = \sqrt{D_{\min} \tau_R}$$

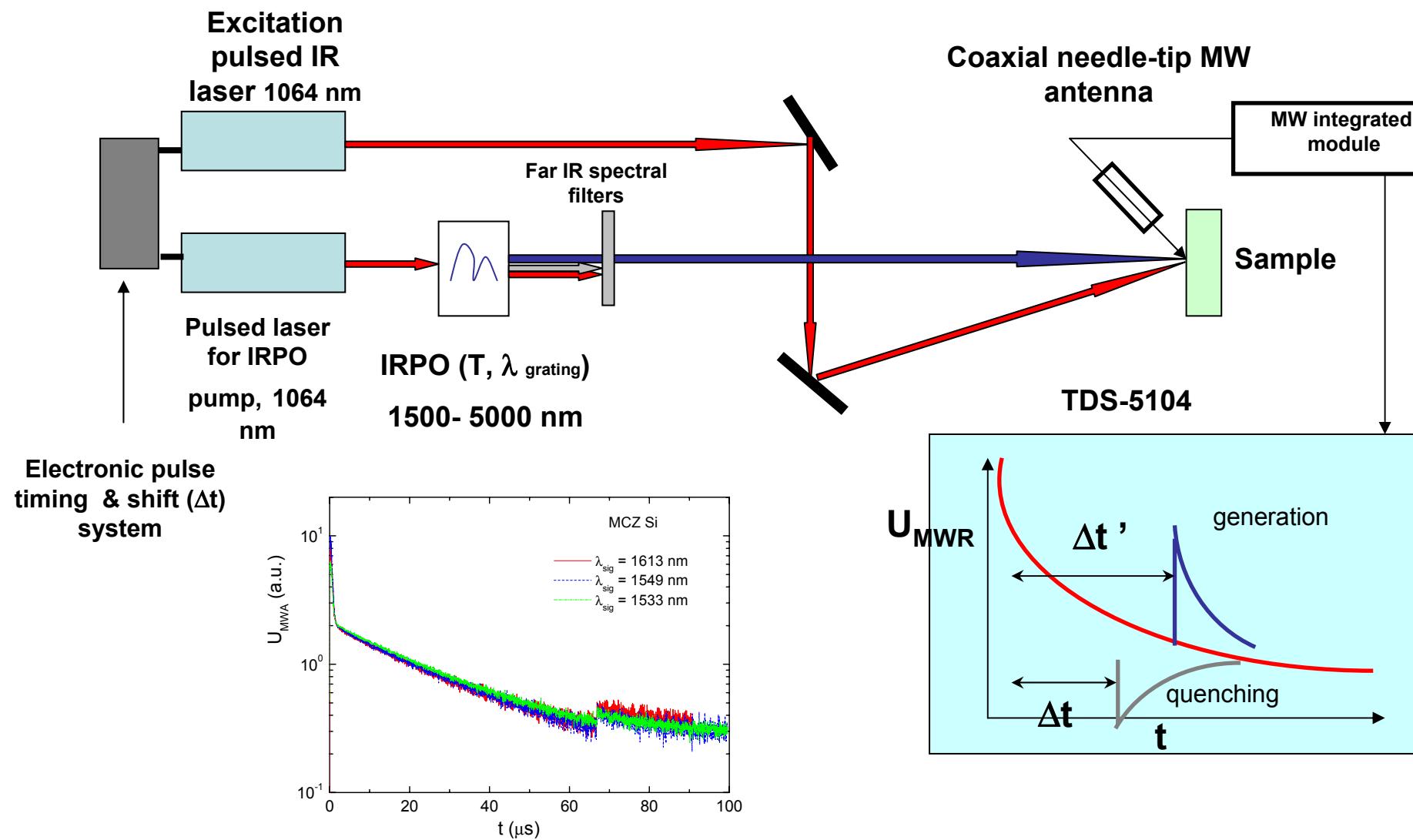
$D \approx 67 \text{ cm}^2/\text{s}$ p-Ge

$D \approx 21 \text{ cm}^2/\text{s}$ p-Si

Perspective development of the MW techniques

for:

- estimation of trap spectral parameters



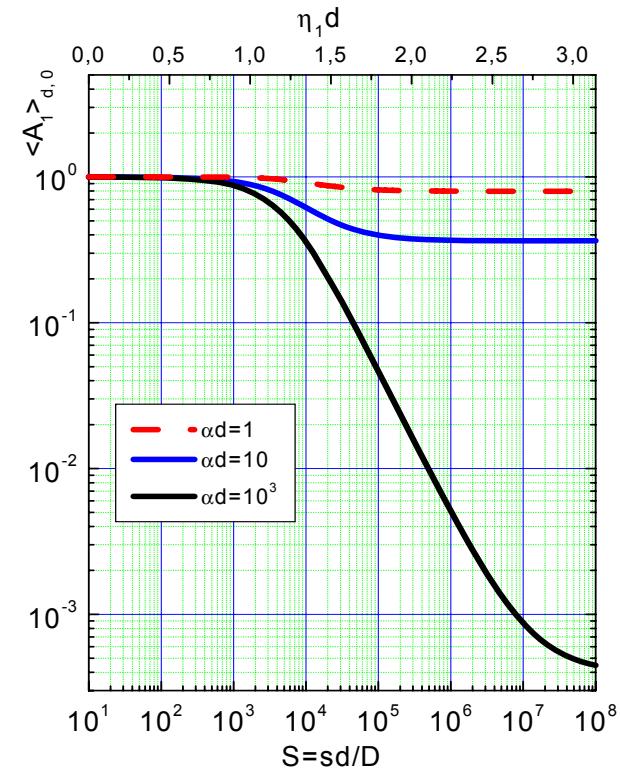
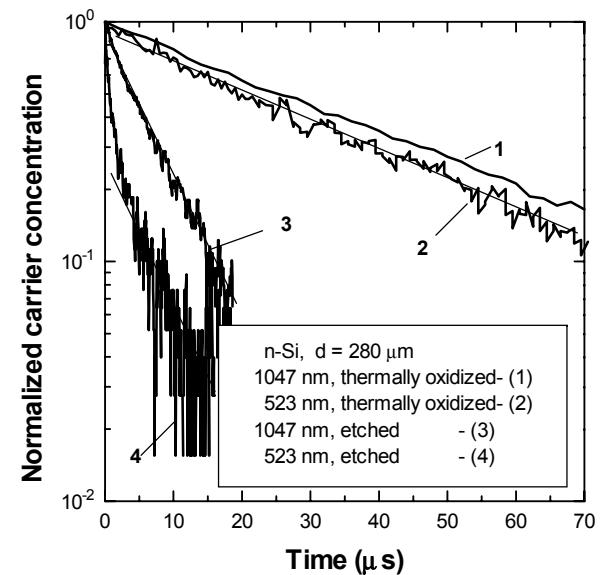
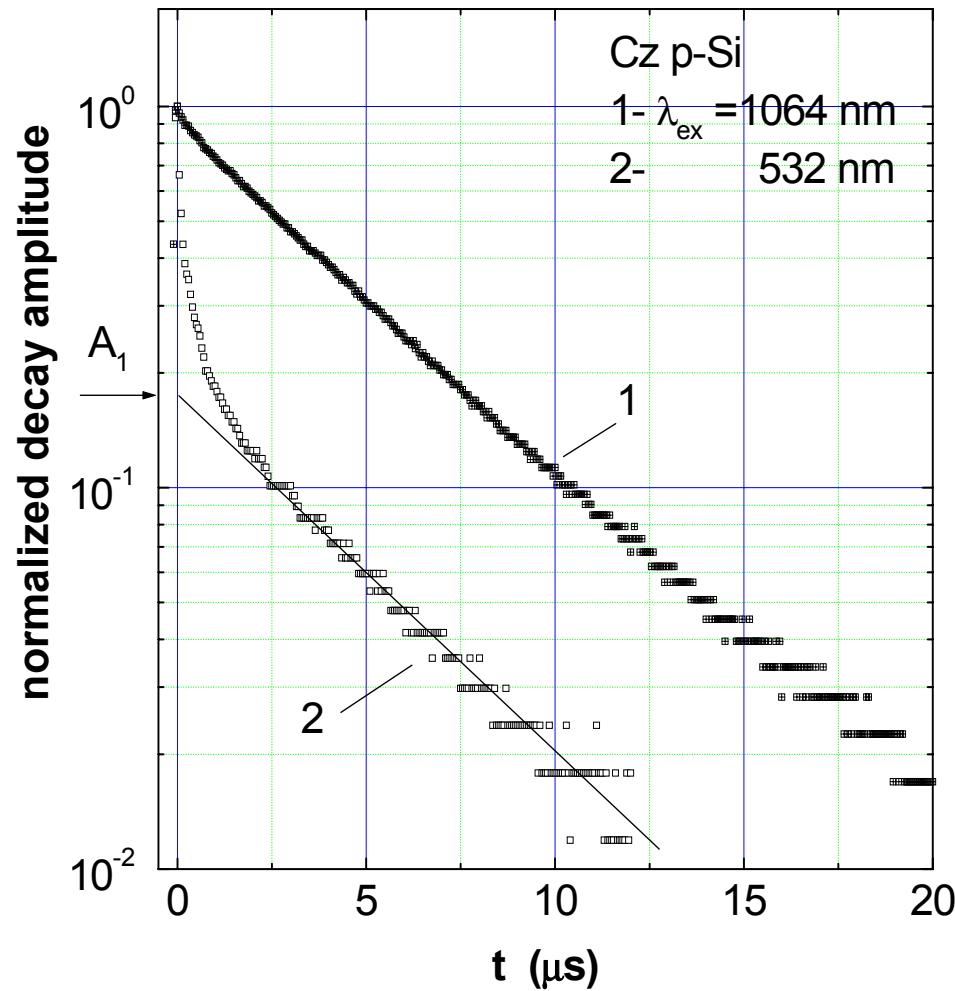
Carrier recombination in the bulk and at surface

☀ Transitional and main decay mode constituents within transients.

Surface and bulk recombination parameters can be separated

by varying excitation domain.

$$\frac{\langle n(t) \rangle_d}{\langle n(0) \rangle_d} = \sum_{m=1}^{\infty} A_m(\eta_m d, \alpha d) e^{-\frac{t}{\tau_m}} e^{-\frac{t}{\tau_b}}$$



Carrier decay/trapping parameters

DLTS

$$e \sim 1/\tau_e = \sigma v N_{C,Vm} = e^{|\Delta E_c, V - \Delta E_m|/kT} / \sigma v N_{C,V}$$

MWR

$$\tau_{as} \sim \tau_e = 1/\sigma v N_{C,Vm} = e^{|\Delta E_c, V - \Delta E_m|/kT} / \sigma v N_{C,V}$$

I-V n+p junction - according to D.Schroder Sol.St.Phen. v.6&7 (1989) 383

$$I_F \approx I_{diff} = I_{sat} (e^{qV/kT} - 1) = q A N_c N_v e^{-Eg/kT} [D_p e^{\Delta Eg/kT} / N_D L_{peff} + D_n / N_A L_{neff}] (e^{qV/kT} - 1)$$

$$L_{n,p\ eff} = L_{n,p} [1 + (s_r L_{n,p} / D_{n,p}) \tanh(d/L_{n,p})] / [(s_r L_{n,p} / D_{n,p}) + \tanh(d/L_{n,p})] \Big|_{d < L_n} \approx d [(s_r + D_n/d) / (s_r + d/\tau_R)];$$

$$L_{n,p} = (D_{n,p} \tau_R)^{1/2}$$

MWR $\tau \sim \tau_R$ - monoexp; $s_r \leftarrow A_1, \tau_{Reff}$, 2-compon.

$$I_{Rev} \rightarrow I_{rev}(scr) + I_{rev}(qnr) = q n_i W A / \tau_{geff} + q A N_c N_v e^{-Eg/kT} [D_p e^{\Delta Eg/kT} / N_D L_{peff} + D_n / N_A L_{neff}]$$

$$\tau_{geff} = \tau_g / (1 + 2 s_g \tau_g / r)$$

$$I_{Rev} |_{FD} \approx q n_i W A / \tau_{geff}$$

MWR $\tau_{as} \sim \tau_e + \tau_{tr}$