

Optics Tuning Challenges at SuperKEKB

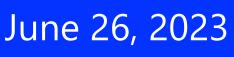
Thanks to H. Sugimoto, A. Morita, H. Koiso, D. Zhou, K. Ohmi, K. Oide, P. Raimondi, M. Biagini, C. Milardi, A. Bogomyagkov, J. Keintzel, R. Tomas, and all members of SuperKEKB International Task Force



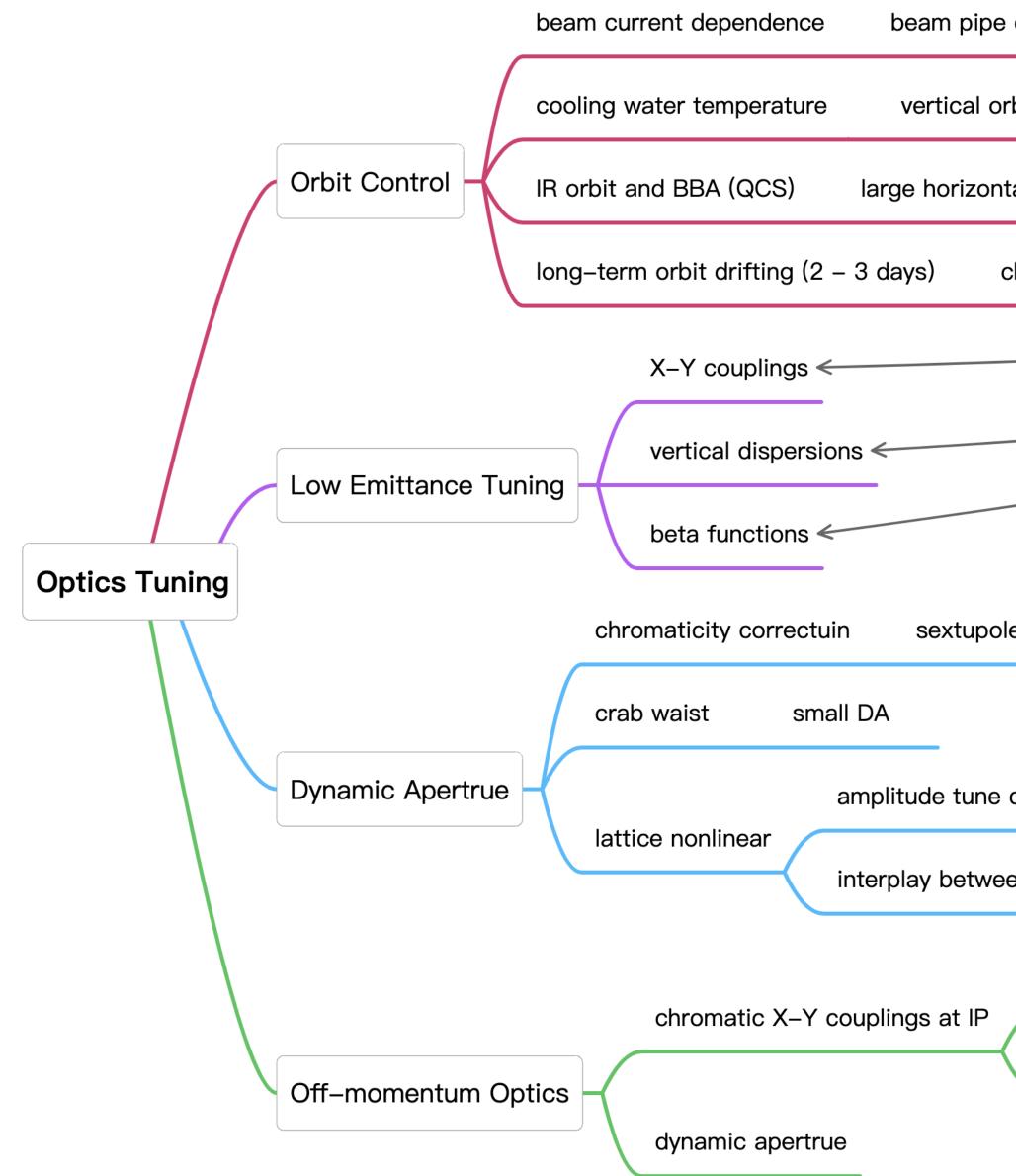
The invitation link of ITF is as follows: https://skb-itf-chat.kek.jp/signup_user_complete/?id=dwcachrpgpgbfnggdcrcbda68h&md=link&sbr=fa

Y. Ohnishi / KEK

Please join !





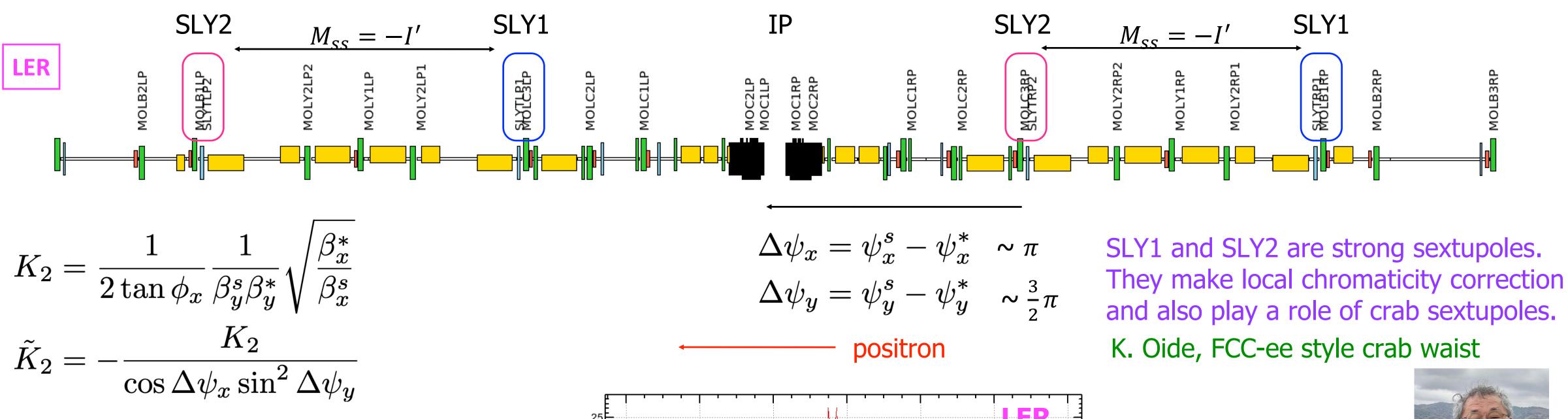


Challenge of Optics Tuning at SuperKEKB

e deformation due to intense SR	BPM pushes a sextupole (horizontal)	large beta-beat
orbit fluctuation (7 min)		
ntal and/or vertical angle at IP		
change of BPM gain ? poor rep	ouroducibility	
ole optimization		
dependence		
en beam-beam and lattice nonlinea	r	
luminosity performance		
dynamic apertrue		



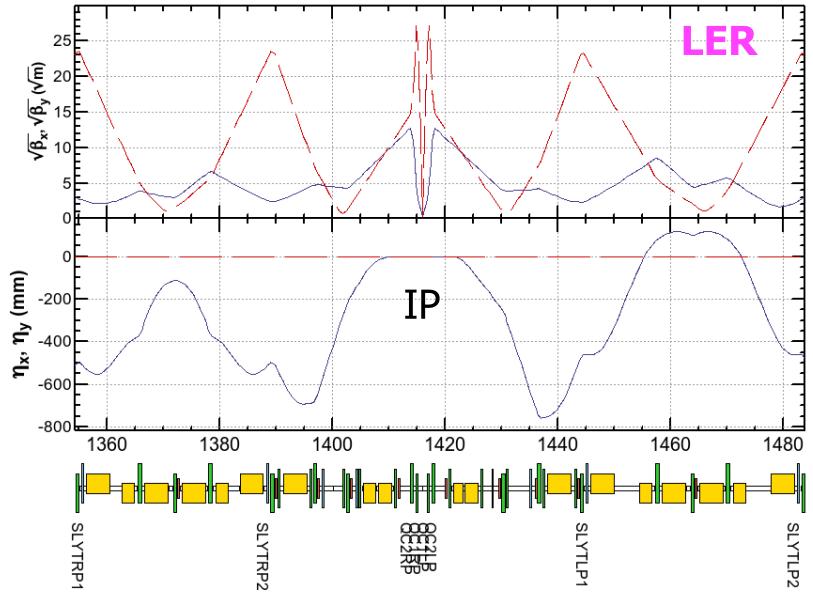




$$\Delta \psi_x = \psi_x^s - \psi_x^* \quad \sim \pi$$
$$\Delta \psi_y = \psi_y^s - \psi_y^* \quad \sim \frac{3}{2}\pi$$

 c_r is crab-waist ratio and K₂^{SLY} is the original setting (CW 0%);

$$\begin{split} K_2^{SLY1} &= -c_r \frac{\tilde{K}_2}{2} + K_2^{SYL} \\ K_2^{SLY2} &= c_r \frac{\tilde{K}_2}{2} + K_2^{SYL} \end{split}$$



The difference of K2 between SLY1 and SLY2 makes crab waist effect. The crab waist ratio, c_r is defined by the difference between them.

$$\Delta \psi_x = \psi_x^s - \psi_x^* \sim \pi$$
$$\Delta \psi_y = \psi_y^s - \psi_y^* \sim \frac{3}{2}\pi$$

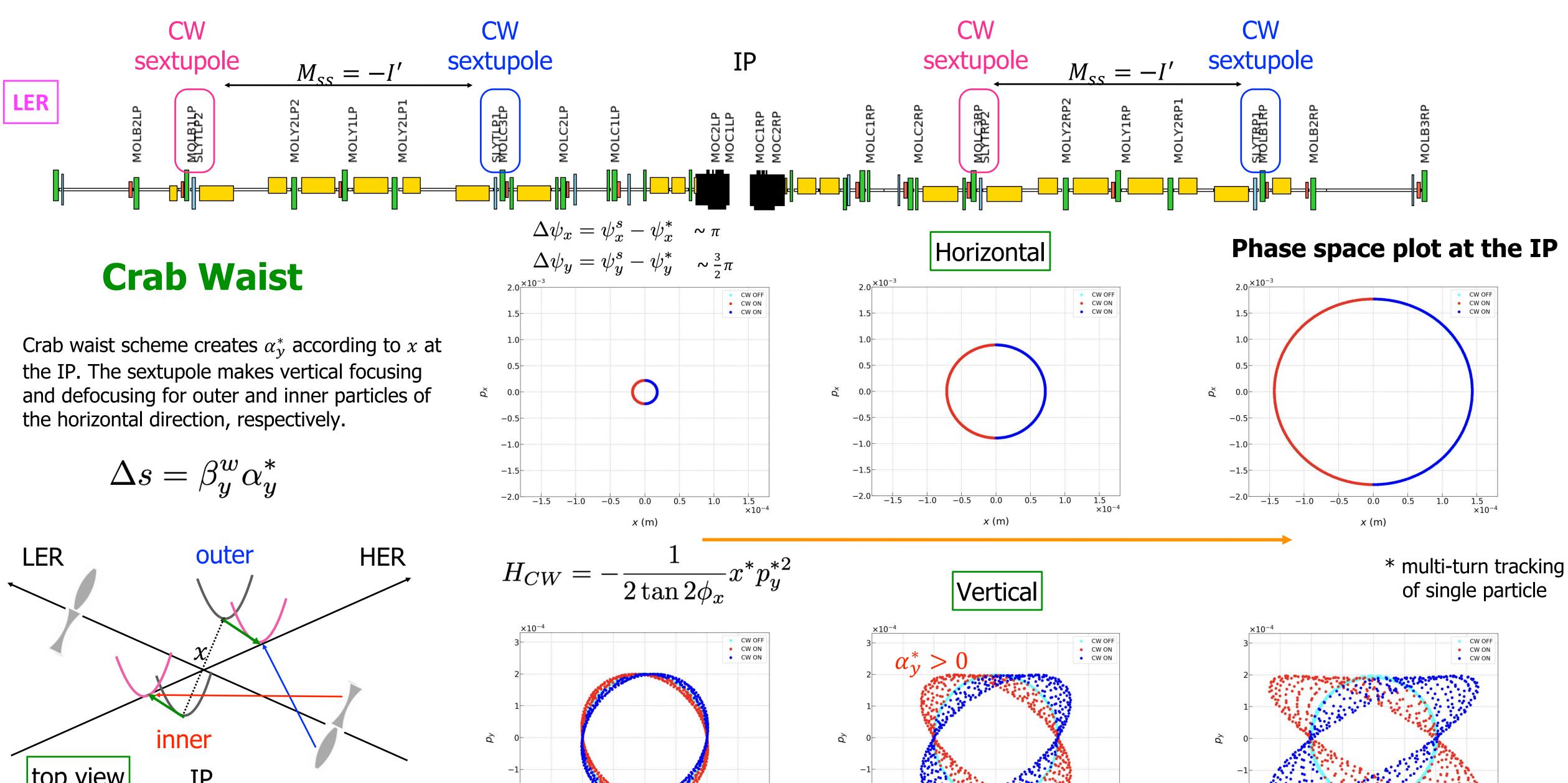


P. Raimondi, The first crab sextupole in the world (DAFNE).

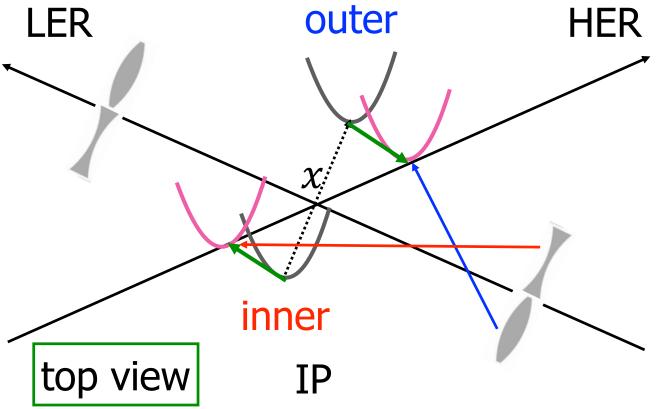




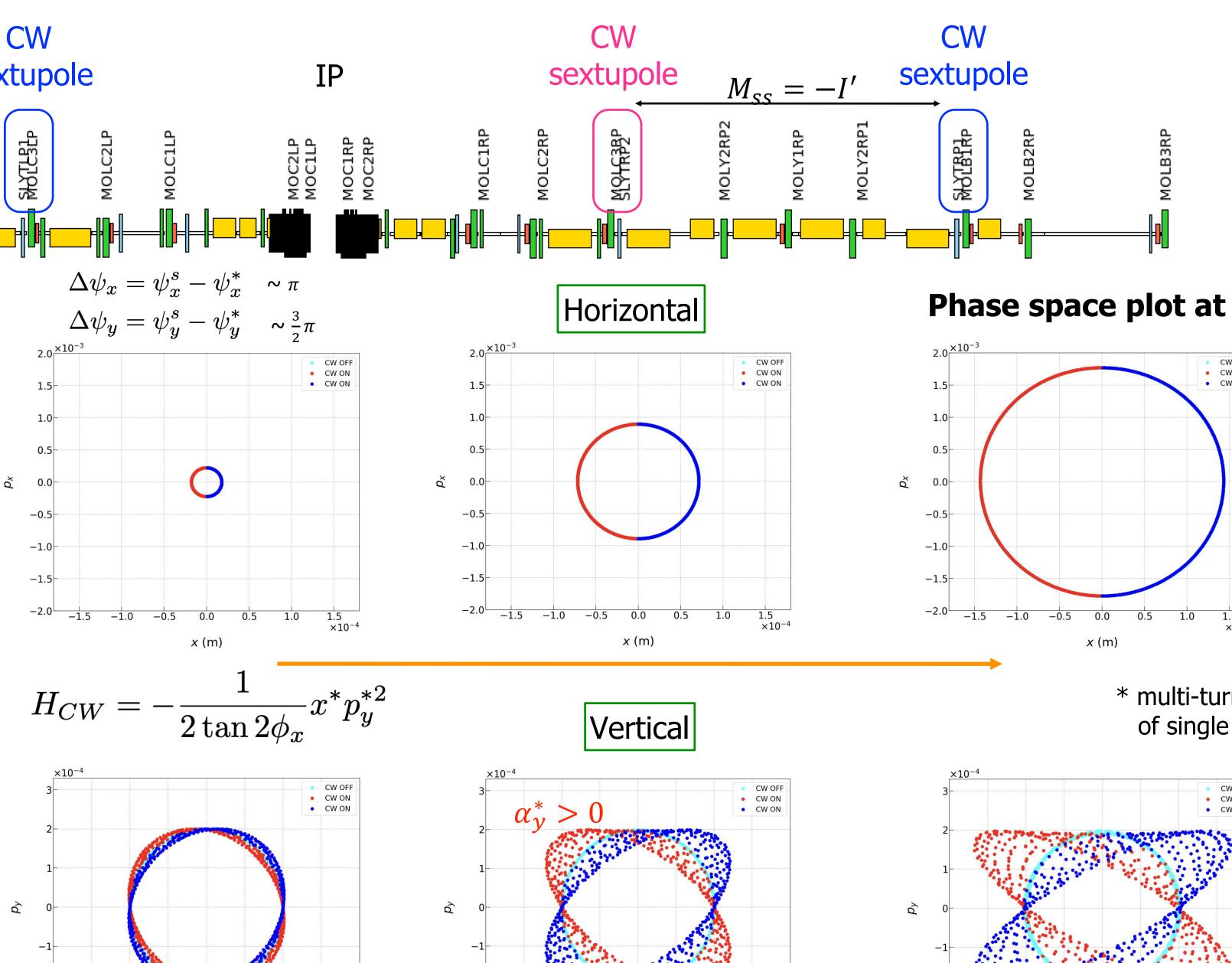


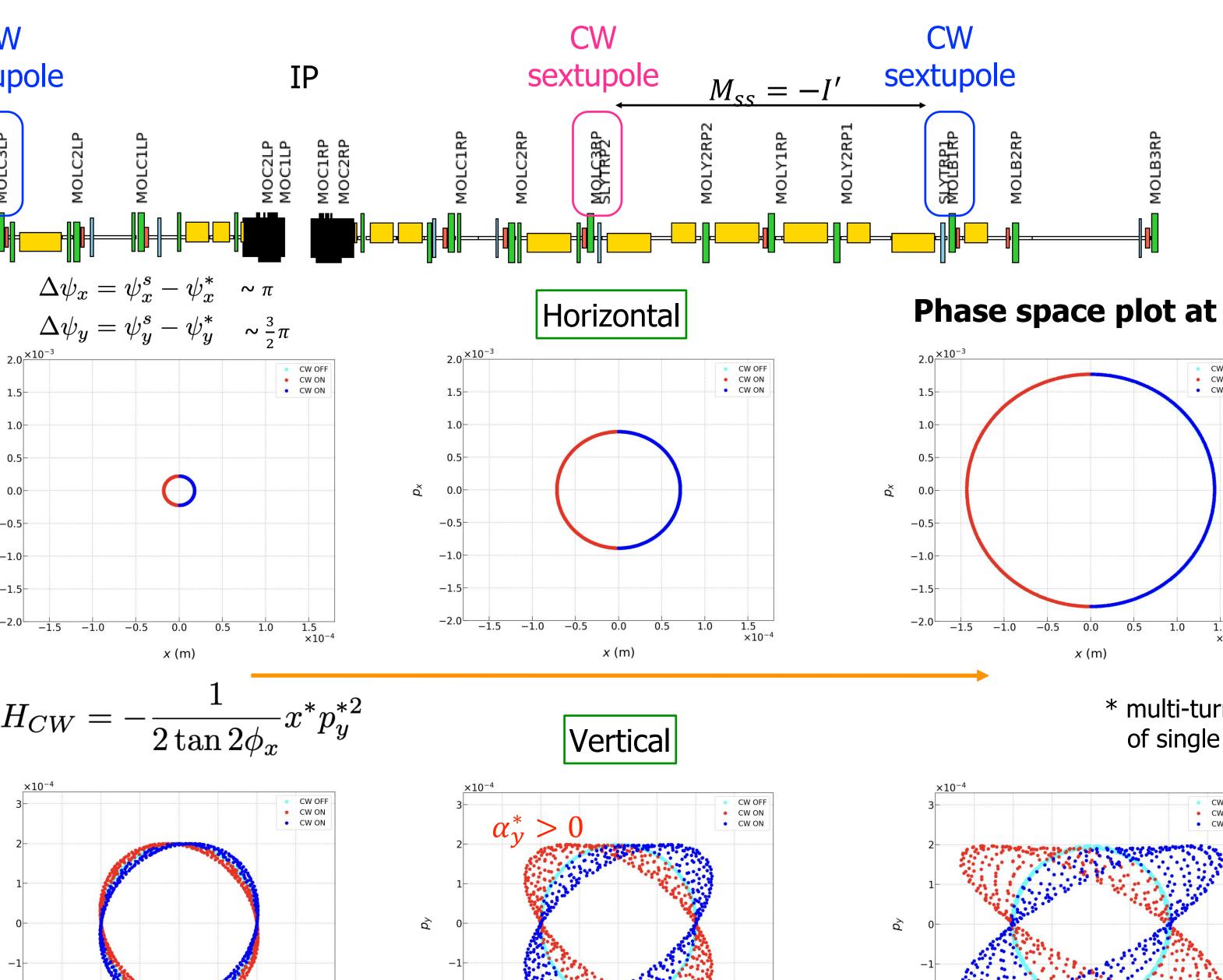


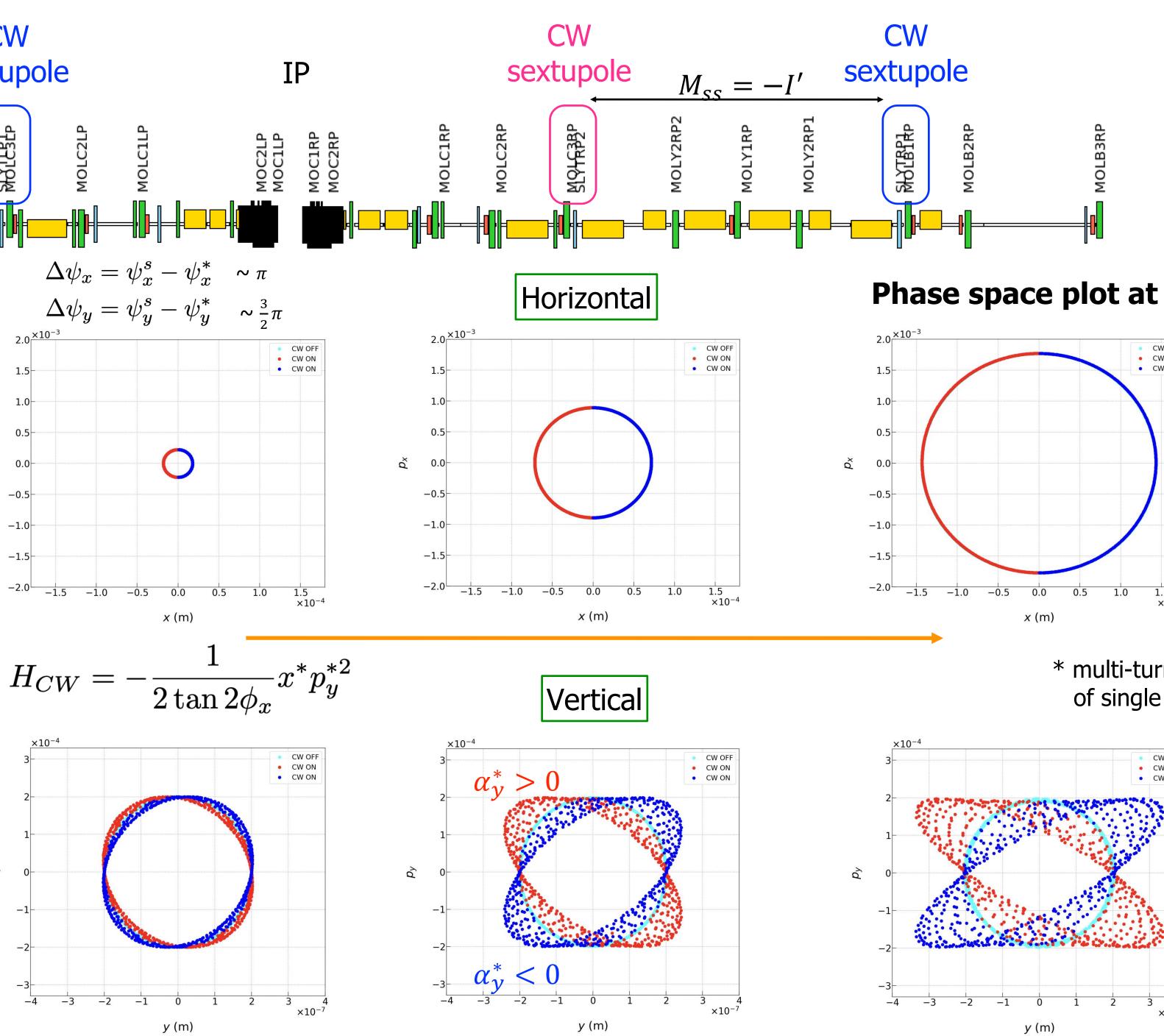
$$\Delta s = \beta_y^w \alpha_y^*$$

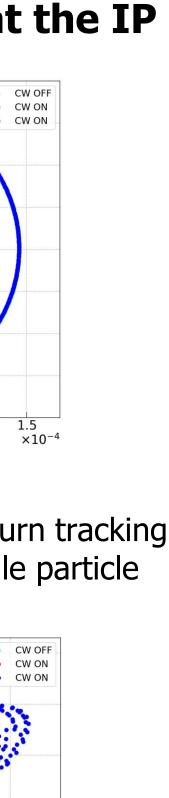


It is expected to reduce resonance lines and bean-tail due to beam-beam.

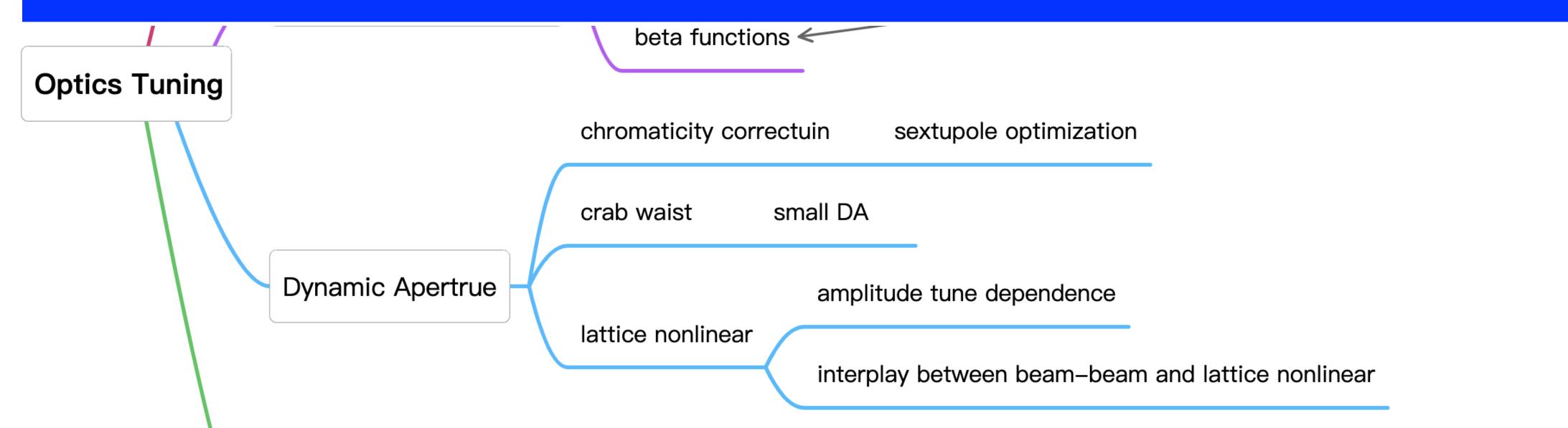




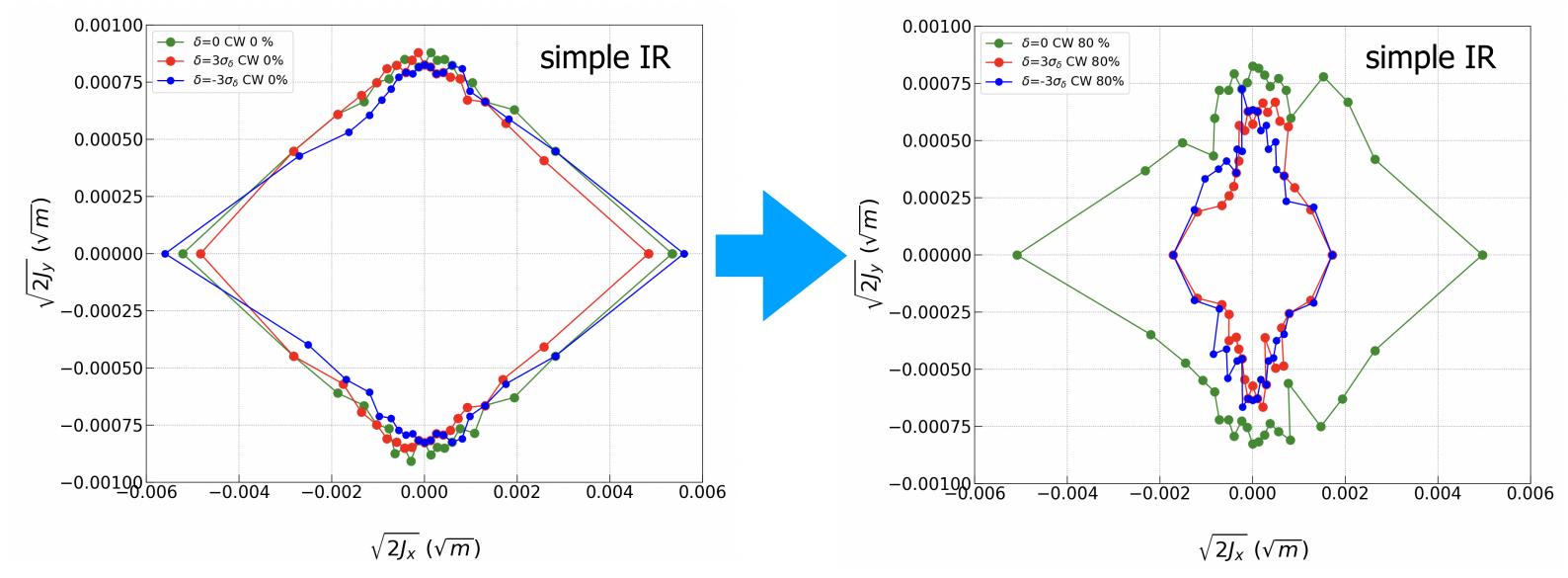








CW : 0 %



Dynamic Aperture and Crab Waist

CW : 80 %

Crab waist reduces dynamic aperture significantly. (off-momentum)

How does it work?

PA (collimator) is slightly smaller than DA in the normal operation, so far. ... to suppress beam backgrounds.

Does PA increase in conjunction with DA?









Tune expanded around the beam center:

$$\nu_{x,y}(J_x,J_y) = \nu_{x0,y0} + \left(\frac{\partial\nu_{x,y}}{\partial J_x}J_x + \frac{\partial\nu_{x,y}}{\partial J_y}J_y\right) + \cdots$$

Hamiltonian equation:

$$\left(\begin{array}{c}\frac{\partial\psi_{x,y}}{\partial s}\\\frac{\partial J_{x,y}}{\partial s}\end{array}\right) = \left(\begin{array}{cc}0&1\\-1&0\end{array}\right) \left(\begin{array}{c}\frac{\partial H}{\partial\psi_{x,y}}\\\frac{\partial H}{\partial J_{x,y}}\end{array}\right)$$

Definition of the tune:

$$\nu_x = \frac{1}{2\pi} \oint \frac{\partial \psi_x}{\partial s} ds \qquad \nu_y = \frac{1}{2\pi} \oint \frac{\partial \psi_y}{\partial s} ds$$

Change of the tune within one magnet of the length L:

$$\Delta \nu_{x,y} = \frac{1}{2\pi} \int_L \frac{\partial \langle H \rangle}{\partial J_{x,y}} ds \quad \text{ for over many turns}$$

Amplitude Detuning

E.H. Maclean, T. Pugnat, B. Dalena, A. Franchi, R. Tomas, et al.

Normal octupoles:

$$H_3(x,y) = \frac{1}{4!} k_3 (x^4 - 6x^2y^2 + y^4)$$
$$x, y = \sqrt{2J_{x,y}\beta_{x,y}} \cos \psi$$

$$< H_3 > = \frac{k_3}{16} (J_x^2 \beta_x^2 - 4J_x J_y \beta_x \beta_y + J_y^2 \beta_y^2)$$

$$\frac{1}{2\pi} \int \frac{\partial \langle H_3 \rangle}{\partial J_x} ds = \sum_i \frac{k_3 L_o}{16\pi} \beta_x^2 J_x - \sum_i \frac{k_3 L_o}{8\pi} \beta_x \beta_y J_y$$
$$= a_{xx} J_x + a_{xy} J_y$$

$$\frac{1}{2\pi} \int \frac{\partial \langle H_3 \rangle}{\partial J_y} ds = -\sum_i \frac{k_3 L_o}{8\pi} \beta_x \beta_y J_x + \sum_i \frac{k_3 L_o}{16\pi} \beta_y^2 J_y$$
$$= a_{yx} J_x + a_{yy} J_y$$









E. Forest et al., Nucl. Inst. Meth. in Physics Research, A269 (1988) K. Oide and H. Koiso, Phys. Rev. E, 47, 3 (1993) Quadrupole nonlinear fringe (Normal)

$$H_{f\pm} = \pm \frac{k_1}{12} (x^3 p_x - 3x^2 y p_y + 3y^2 x p_x - y^3 p_y)$$

(+: entrance, -: exit)

Average of H_f

$$< H_{f+} > = -\frac{k_1}{8}\beta_x \alpha_x J_x^2 + \frac{k_1}{4}(\beta_x \alpha_y - \beta_y \alpha_x)J_x J_y + \frac{k_1}{8}$$

Amplitude detuning:

$$\frac{1}{2\pi} \int \frac{\partial \langle H_{f+} \rangle}{\partial J_x} ds = -\sum_i \frac{k_1}{8\pi} \beta_x \alpha_x J_x + \sum_i \frac{k_1}{8\pi} (\beta_x \alpha_y - \beta_y \alpha_x) J_y$$
$$= a_{xx} J_x + a_{xy} J_y$$

$$\frac{1}{2\pi} \int \frac{\partial \langle H_{f+} \rangle}{\partial J_y} ds = \sum_i \frac{k_1}{8\pi} (\beta_x \alpha_y - \beta_y \alpha_x) J_x + \sum_i \frac{k_1}{8\pi} \alpha_y \beta_y J_y$$
$$= a_{yx} J_x + a_{yy} J_y$$
$$\alpha_y = -\frac{L^*}{\beta_y^*} \quad k_1 L_Q = -\frac{2}{L^* + L_Q/2}$$

Nonlinear Fringe Field of Quadrupole, Kinematic Term

A. Bogomyagkov et al., PR-AB, 19, 121005 (2016)

Kinematic term

Average of H_k

$$H_k = \frac{(p_x^2 + p_y^2)^2}{8}$$

 $\frac{1}{2}\beta_{y}\alpha_{y}J_{y}^{2} \qquad < H_{k} > = \frac{1}{16}(3\gamma_{x}^{3}J_{x}^{2} + 2\gamma_{x}\gamma_{y}J_{x}J_{y} + 3\gamma_{y}^{2}J_{y}^{2})$ approximation: $\gamma_{x,y}^2 = \frac{(1 + \alpha_{x,y}^2)^2}{\beta_{x,y}^2} \simeq \frac{1}{\beta_{x,y}^2}$ $\frac{1}{2\pi} \int \frac{\partial \langle H_k \rangle}{\partial J_x} ds = \frac{1}{16\pi\beta_x^*} \left(L^* + \frac{L_Q}{2} \right) \left(\frac{3}{\beta_x^*} J_x + \frac{1}{\beta_y^*} J_y \right)$ $=a_{xx}J_x+a_{xy}J_y$

$$\frac{1}{2\pi} \int \frac{\partial \langle H_k \rangle}{\partial J_y} ds = \frac{1}{16\pi\beta_y^*} \left(L^* + \frac{L_Q}{2} \right) \left(\frac{1}{\beta_x^*} J_x + \frac{3}{\beta_y^*} J_y \right) ds$$
$$= a_{xx} J_x + a_{xy} J_y$$

from IP to the 1st quadrupole magnet

(IP side)











K. Oide and H. Koiso, Phys. Rev. E, 47, 3 (1993) A. Bogomyagkov et al., PR-AB, 19, 121005 (2016) Sextupole: thick lens

$$H_s = -\frac{(k_2 L_S)^2 L_S}{48} (x^2 + y^2)^2$$

Average of H_f

$$< H_s > = -\frac{(k_2 L_S)^2 L_S}{16} \left(\frac{\beta_x^2}{2} J_x^2 + \frac{2}{3} \beta_x \beta_y J_x J_y + \frac{\beta_y^2}{2} J_y^2\right)$$

Amplitude detuning:

$$\frac{1}{2\pi} \int \frac{\partial \langle H_s \rangle}{\partial J_x} ds = -\sum_i \frac{(k_2 L_S)^2 L_S}{32\pi} \beta_x J_x - \sum_i \frac{(k_2 L_S)^2 L_S}{48\pi} \beta_x \beta_y J_y$$
$$= a_{xx} J_x + a_{xy} J_y$$

$$\begin{aligned} \frac{1}{2\pi} \int \frac{\partial \langle H_s \rangle}{\partial J_y} ds &= -\sum_i \frac{(k_2 L_S)^2 L_S}{48\pi} \beta_x \beta_y J_x - \sum_i \frac{(k_2 L_S)^2 L_S}{32\pi} \beta_y J_y \\ &= a_{yx} J_x + a_{yy} J_y \end{aligned}$$

We can turned OFF and ON for each items in the tracking simulations.

case	1	2	3	4	5
Kinematic term	X	Ο	X	X	X
QC1 fringe	X	X	Ο	X	X
QC2 fringe	X	X	X	Ο	X
Sextupole thick lens	X	X	X	X	Ο

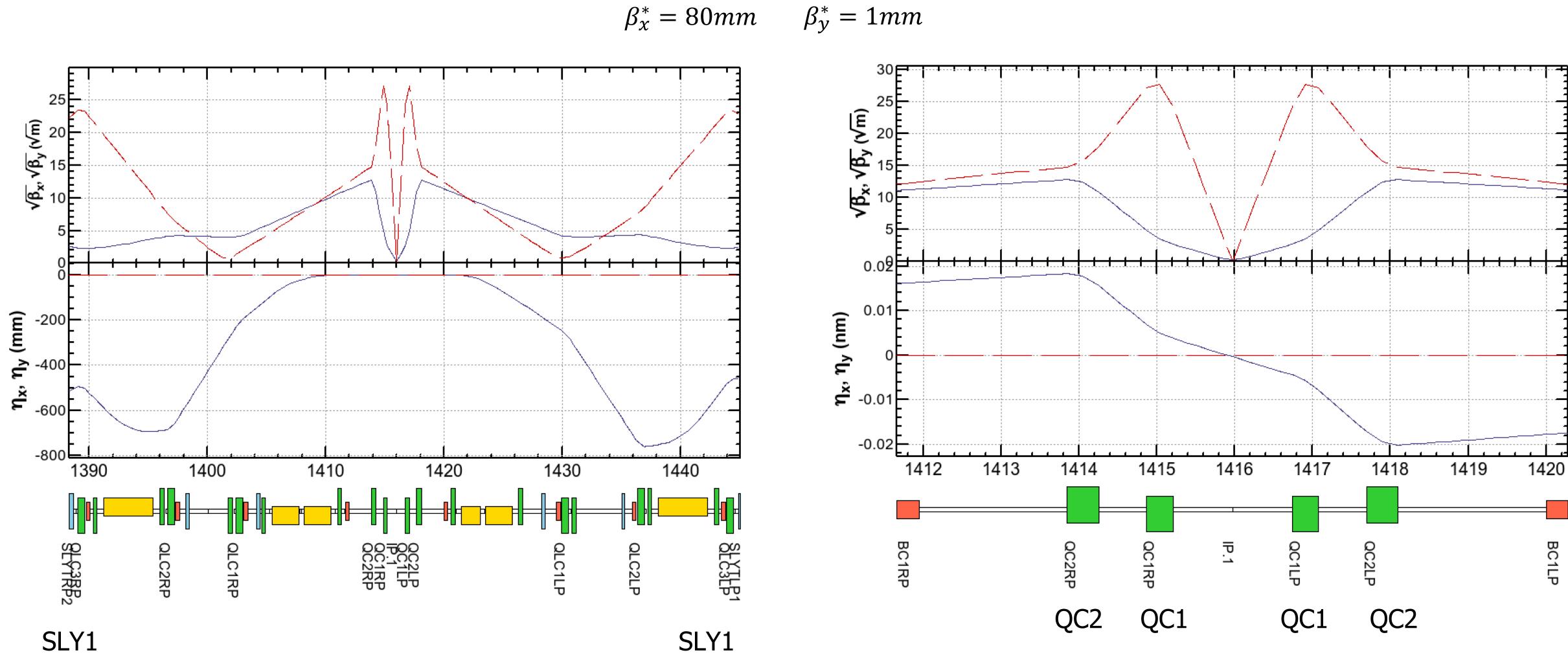








No solenoid, no higher order multipole fields, no X-Y couplings, no offset of magnets





(crab sextupole)

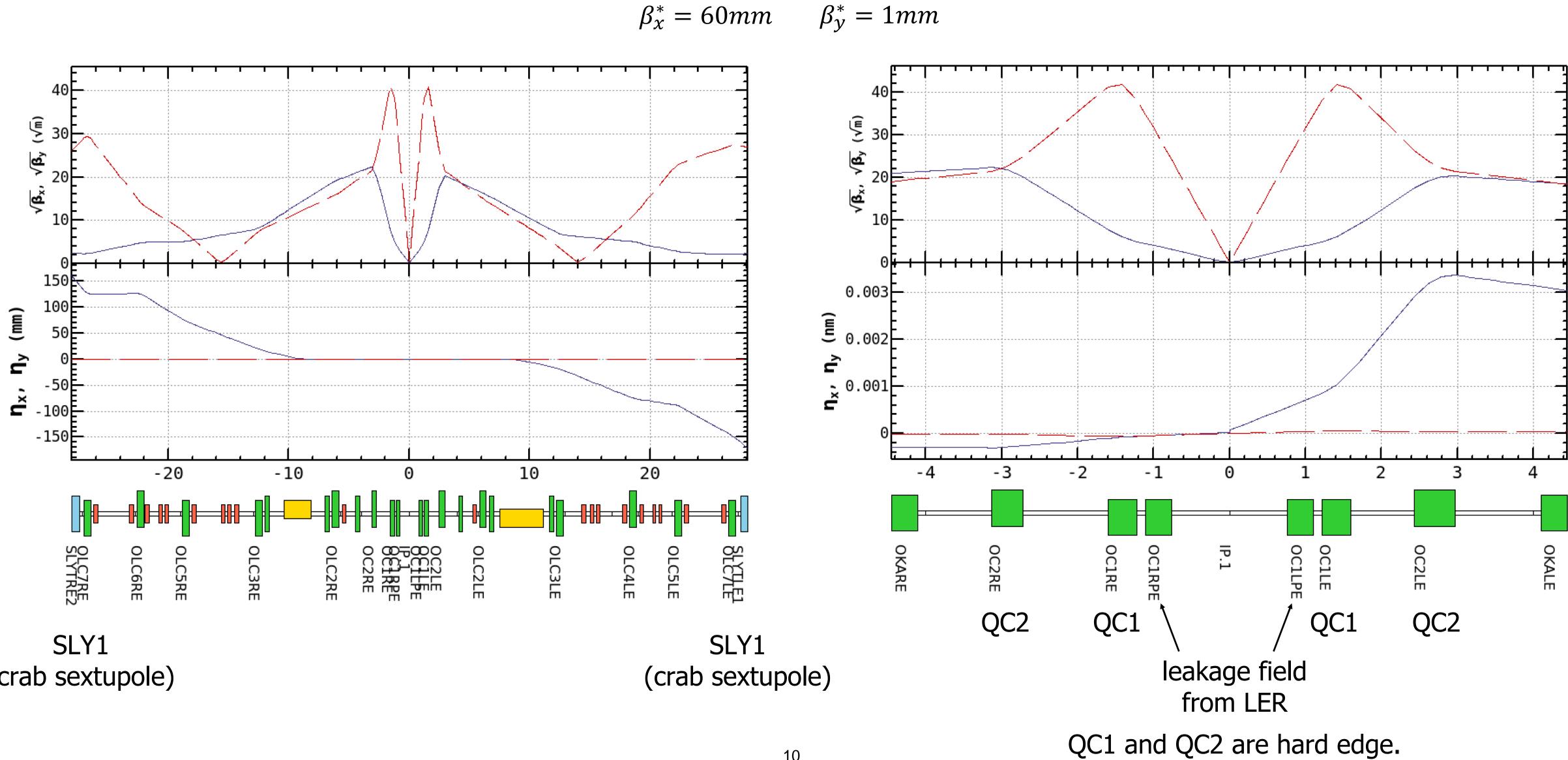
Simple IR Model in LER

QC1 and QC2 are hard edge.





No solenoid, no higher order multipole fields, no X-Y couplings, no offset of magnets

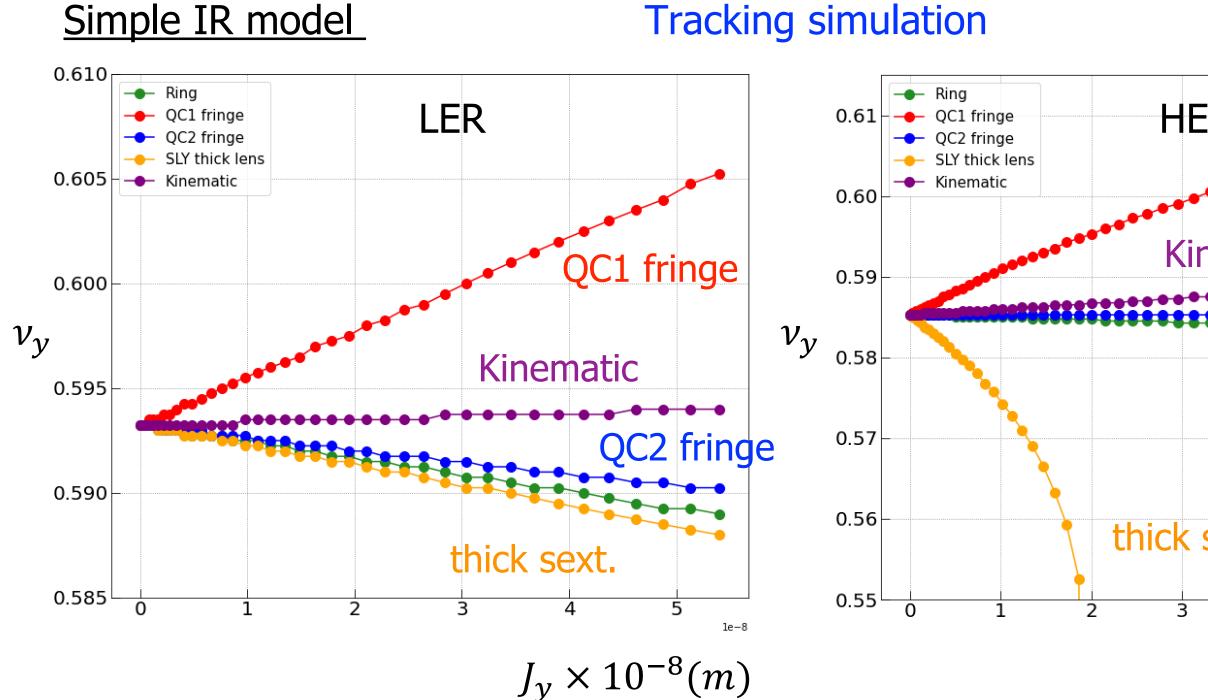


(crab sextupole)

Simple IR Model in HER







The largest detuning of a_{yy} is QC1 fringe in the LER. The thick sextupoles compensate the detuning of QC1 fringe and in the HER.

Estimation of Amplitude Detuning

upper: tracking / lower: analytic

ER	a_{yy}	LER	HER
QC1 fringe	Beta at IP	80 mm / 1 mm	60 mm / 1
inematic	crab waist	80%	40%
reference (case 1)	Kinematic trem	0.91 x 10 ⁵	1.05 x 1
sext. $J_y \times 10^{-8} (m)$		1.12 x 10 ⁵	1.68 x 1
	QC1 fringe	3.01 x 10 ⁵	5.80 x 1
		3.01 x 10 ⁵	6.47 x 1
	QC2	0.12 x 10 ⁵	0.30 x 1
	fringe	0.14 x 10 ⁵	0.25 x 1
	SLY	-0.17 x 10 ⁵	-7.24 x 1
	thick lens (crab waist)	-0.24 x 10 ⁵	-9.44 x 1

The tracking simulation is consistent with analytic calculation.



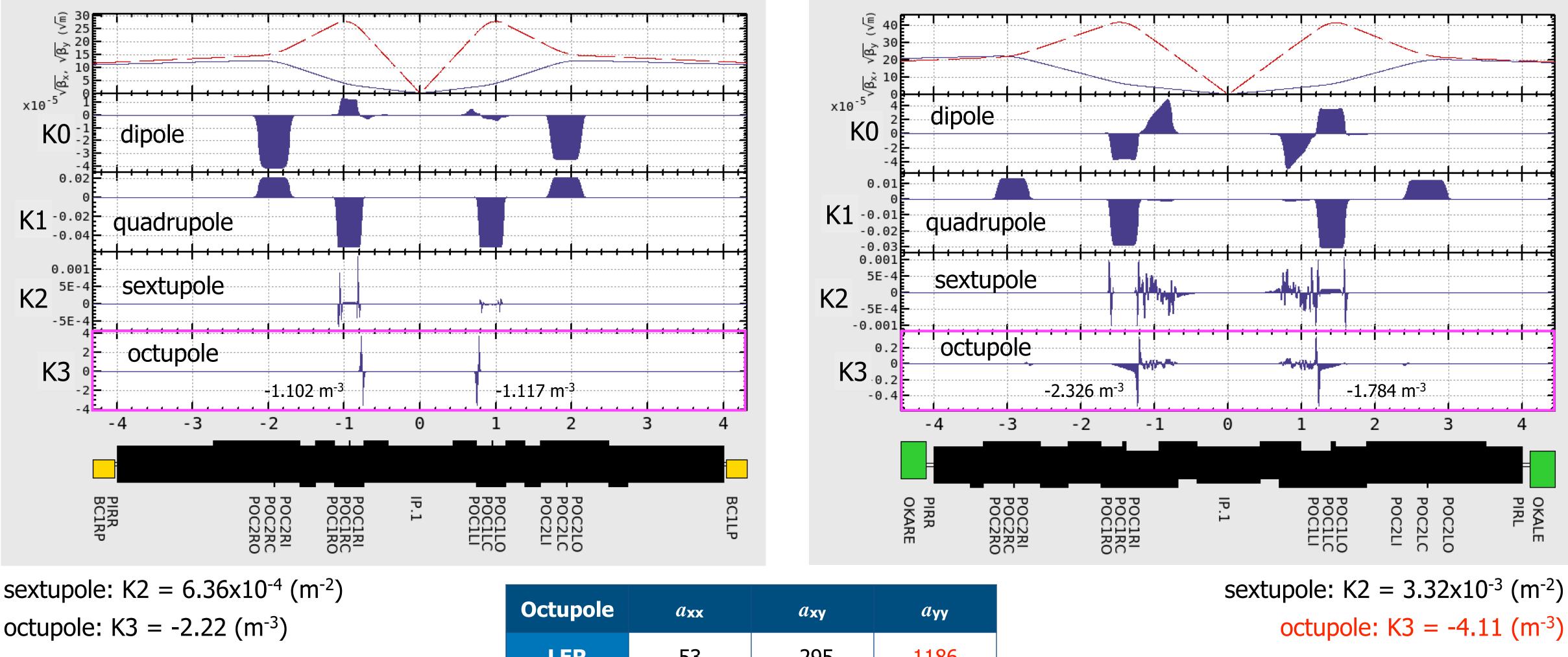








SuperKEKB: $\beta_v^* = 1mm$ Realistic model calculation in the IR LER



octupole: $K3 = -2.22 (m^{-3})$

Octupole	axx	а _{ху}	a _{yy}
LER	53	-295	1186
HER	-128	10315	-256676

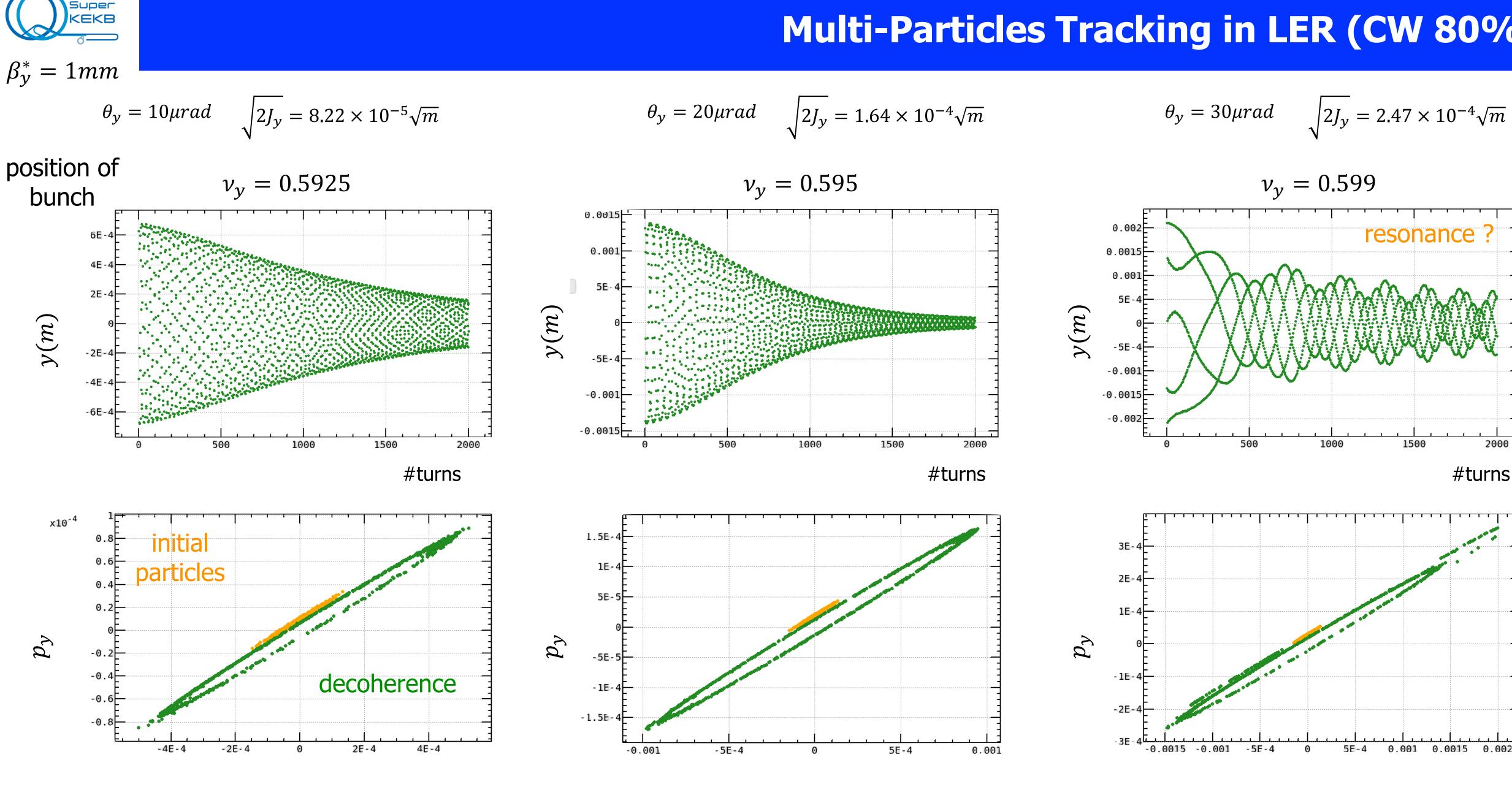
Higher-Order Multipole Magnetic Field

The slice of 1 cm for \pm 4m region from IP HER

Different sign between IR in LER and HER



12



y(m)

Multi-Particles Tracking in LER (CW 80%)

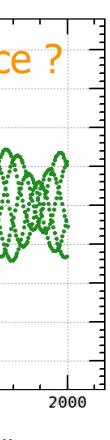
$$urad \quad \sqrt{2J_y} = 1.64 \times 10^{-4} \sqrt{2}$$

y(m)

y(m)



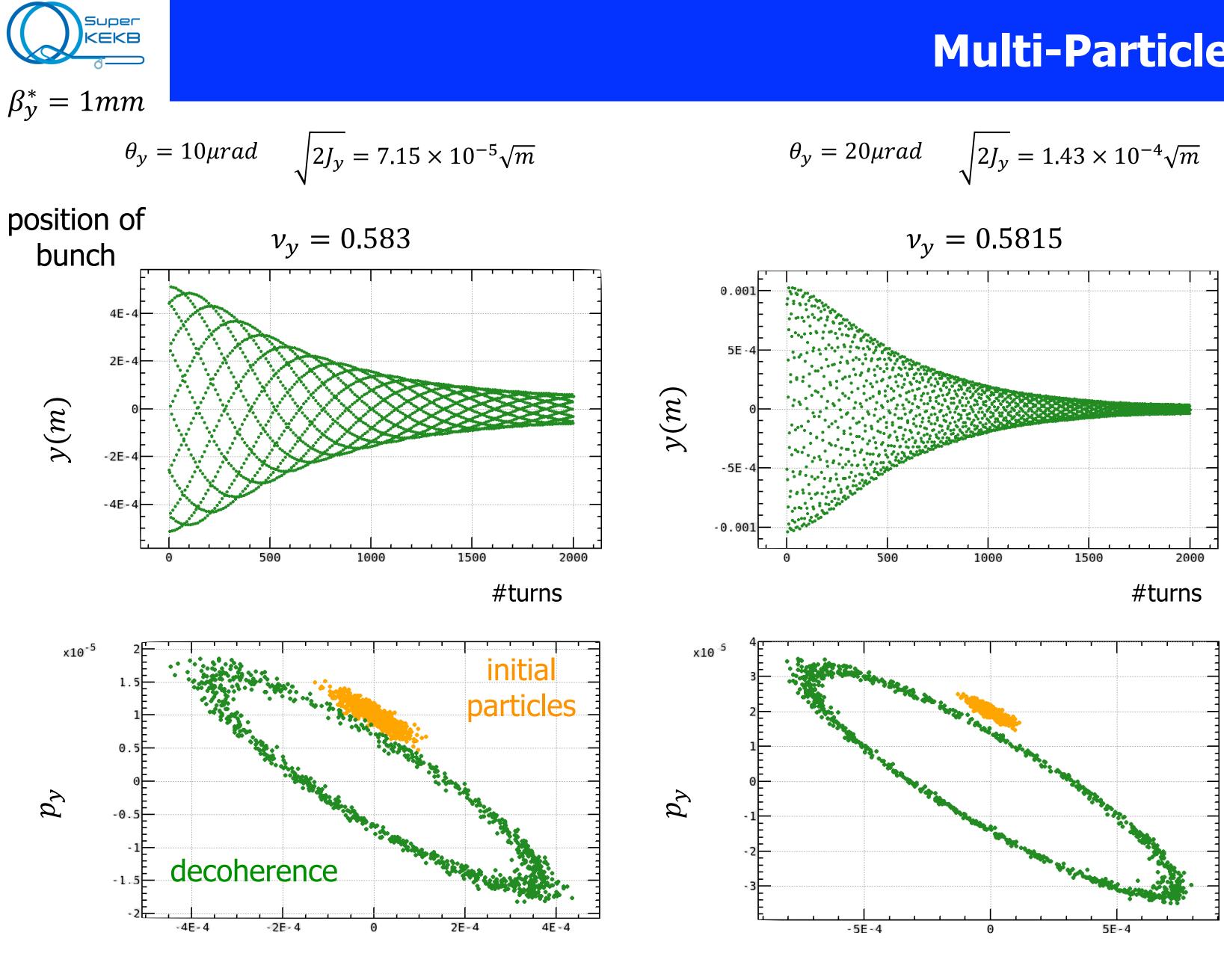






1500



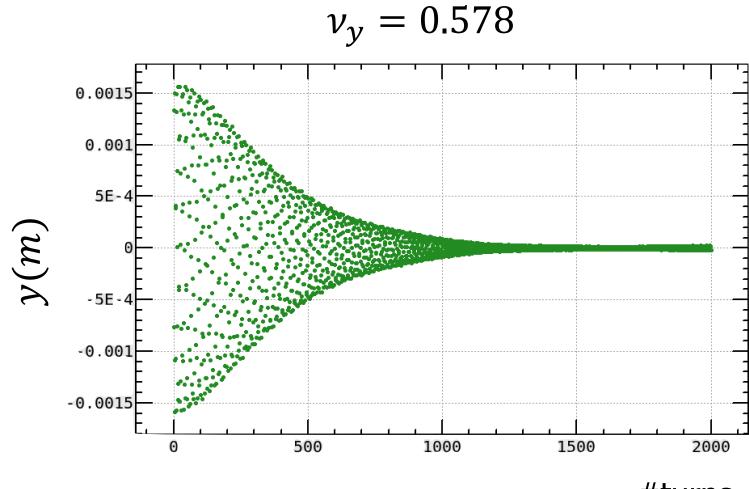


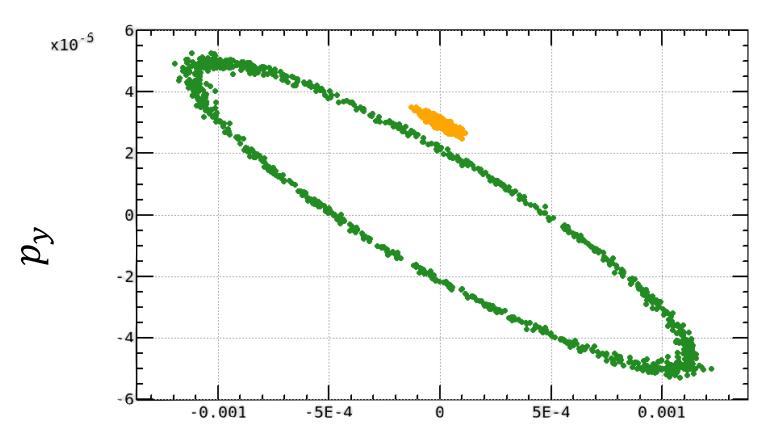
y(m)

Multi-Particles Tracking in HER (CW 40 %)

arad
$$\sqrt{2J_y} = 1.43 \times 10^{-4} \sqrt{m}$$

 $\theta_y = 30 \mu rad$ $\sqrt{2J_y} = 2.14 \times 10^{-4} \sqrt{m}$





y(m)

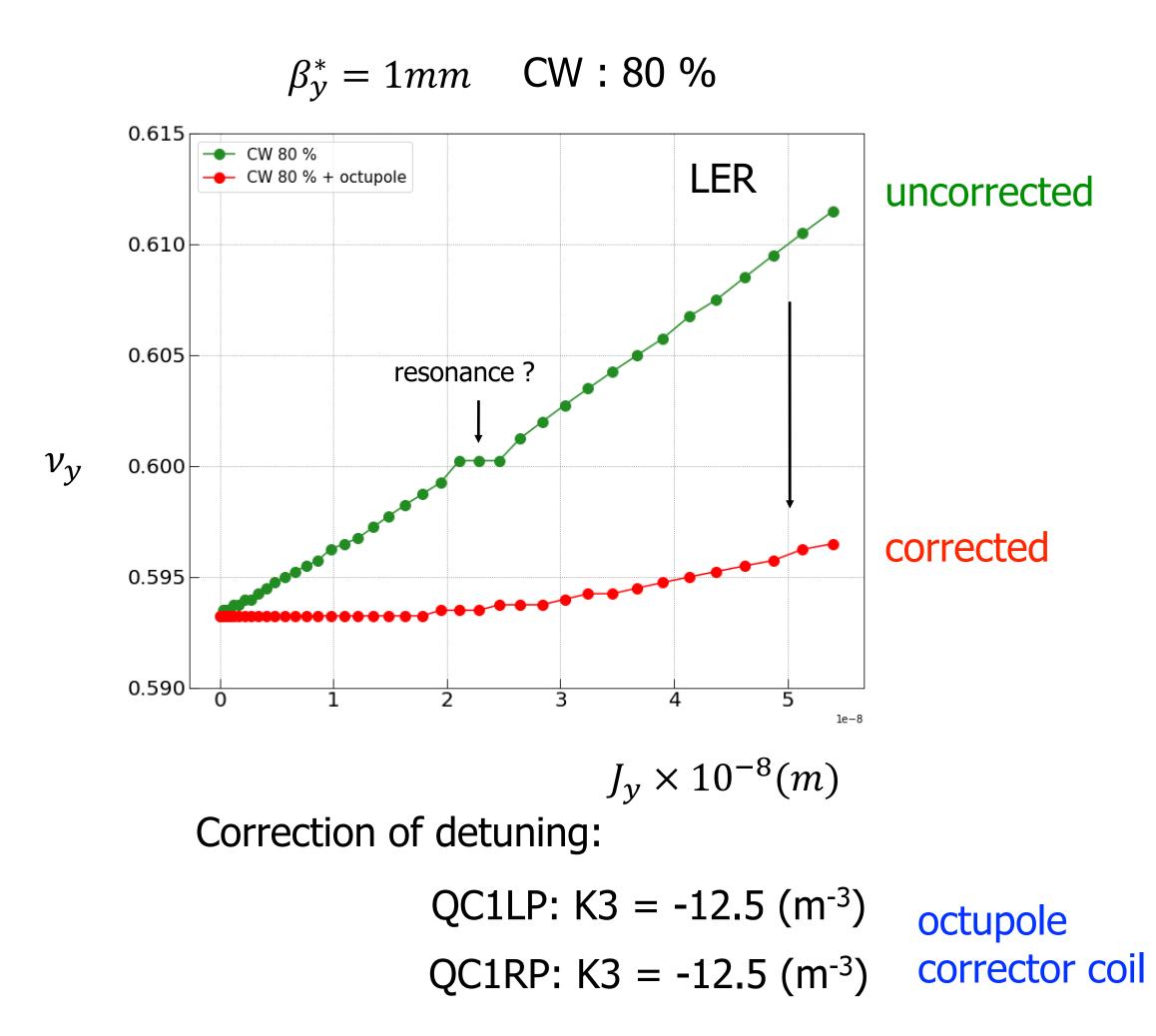
y(m)







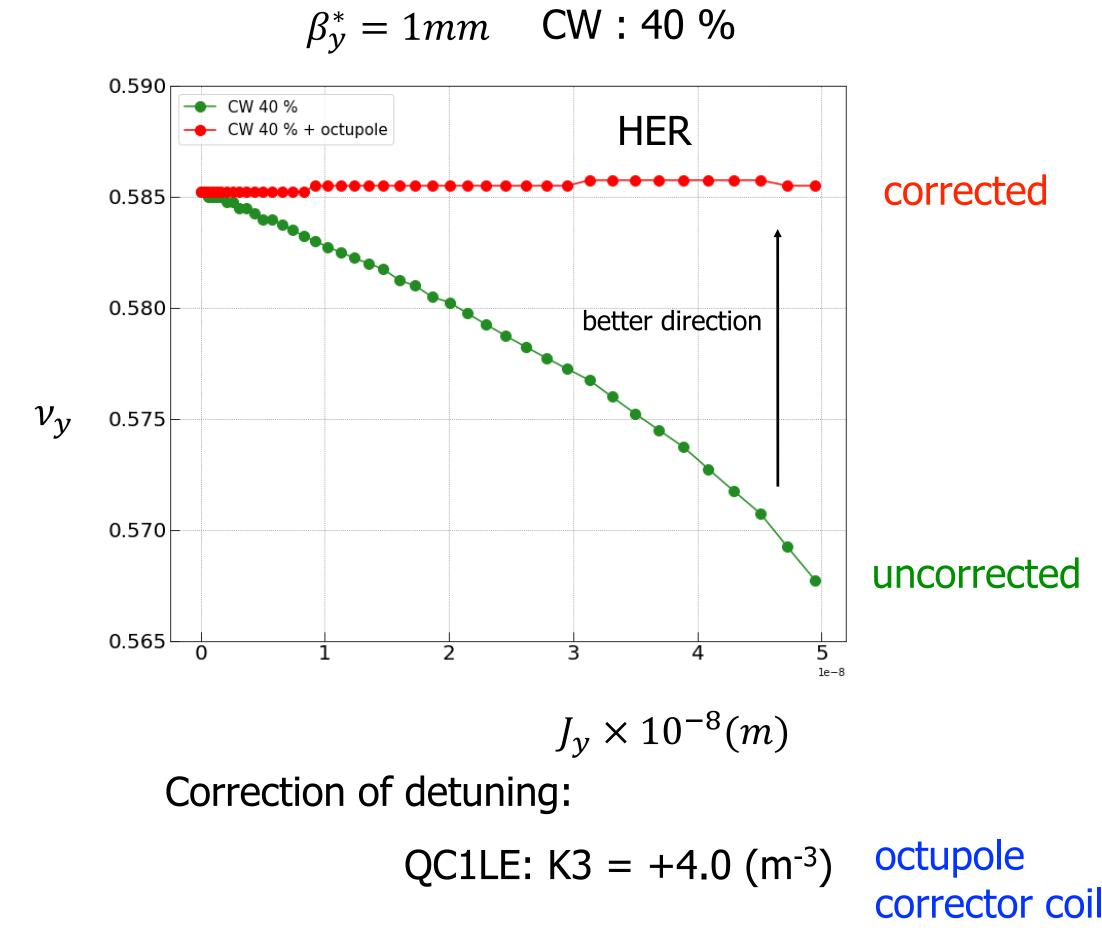




The detuning of LER comes from QC1 fringe.

Max. field of octupole corrector is 15 $(1/m^3)$ for each QC1 and QC2.

Realistic IR Model



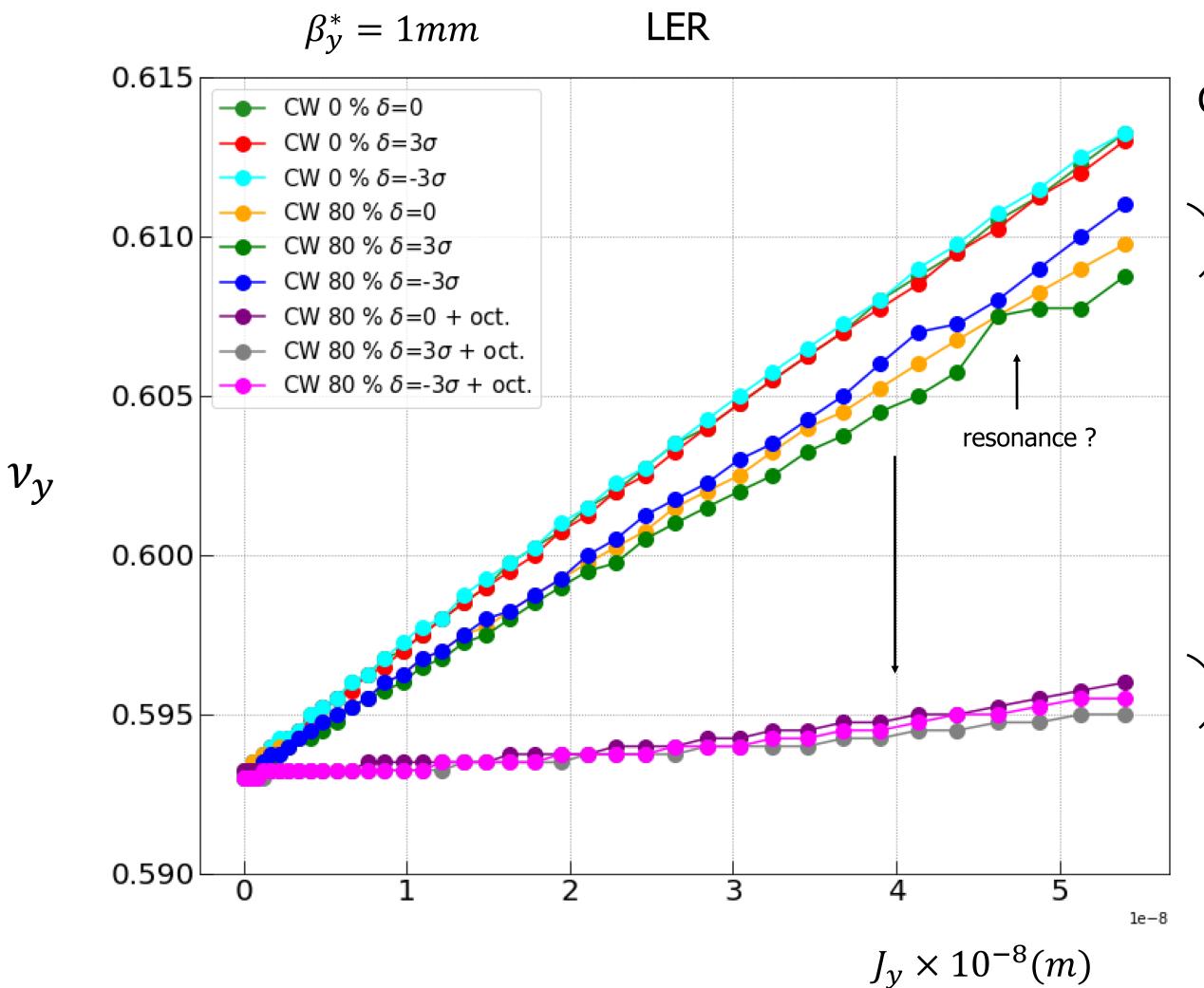
The detuning of HER comes from residual octupole field, QC1 fringe and SLY thickness are almost cancelled each other.



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Correction of Amplitude Detuning (Simple IR Model)

CW 0 % The momentum dependence is small.

CW 80 %

The momentum dependence is larger than CW 0 %.

Off-momentum amplitude matching is necessary?

CW 80 % + correction of detuning with octupoles

nonlinear vs nonlinear



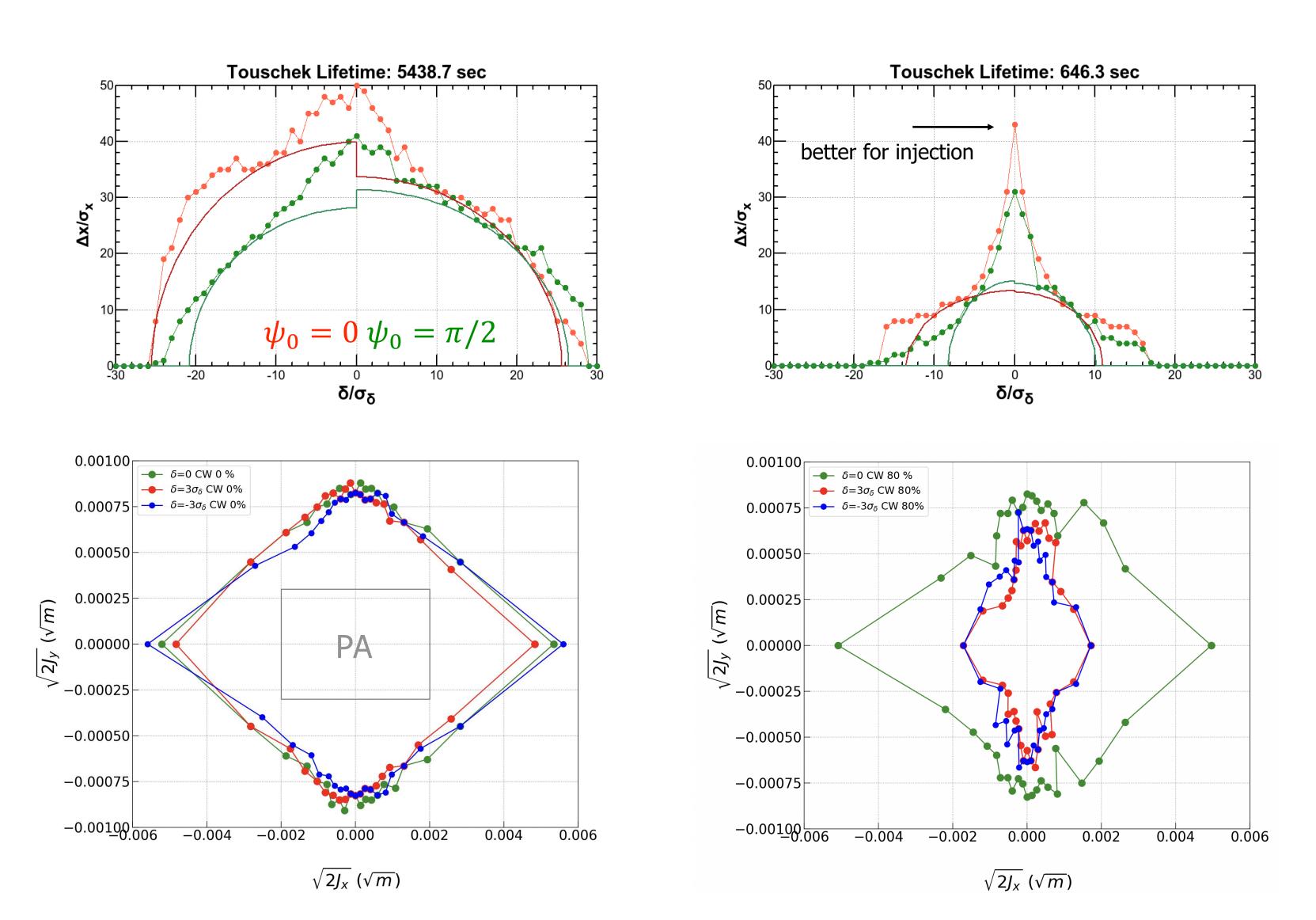






LER $\beta_{\gamma}^* = 1mm$

CW 0 %



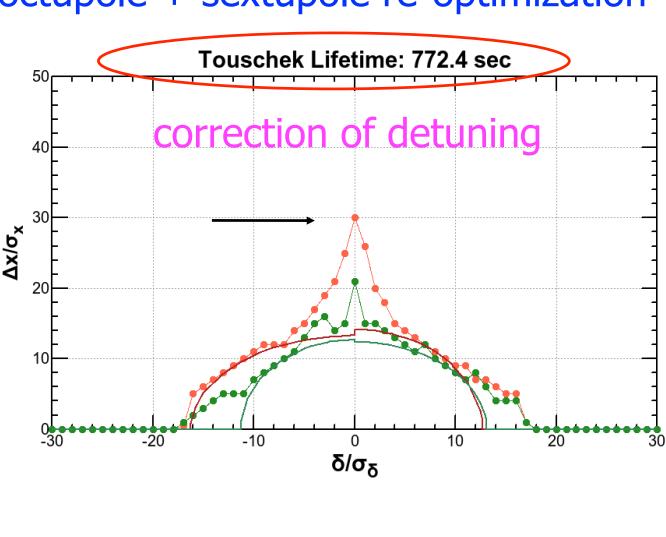
Comparison of Dynamic Aperture (Simple IR Model)

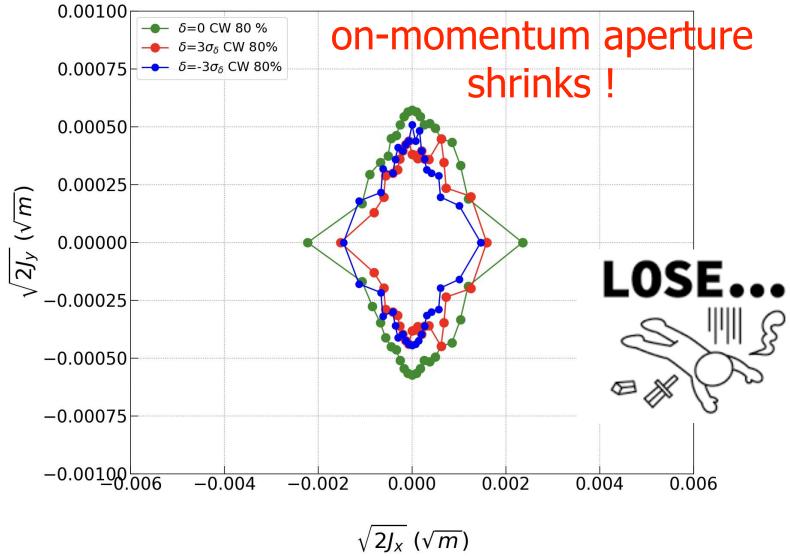
1% coupling, 0.62 mA/bunch for lifetime estimation

CW 80 %

CW 80 %

octupole + sextupole re-optimization





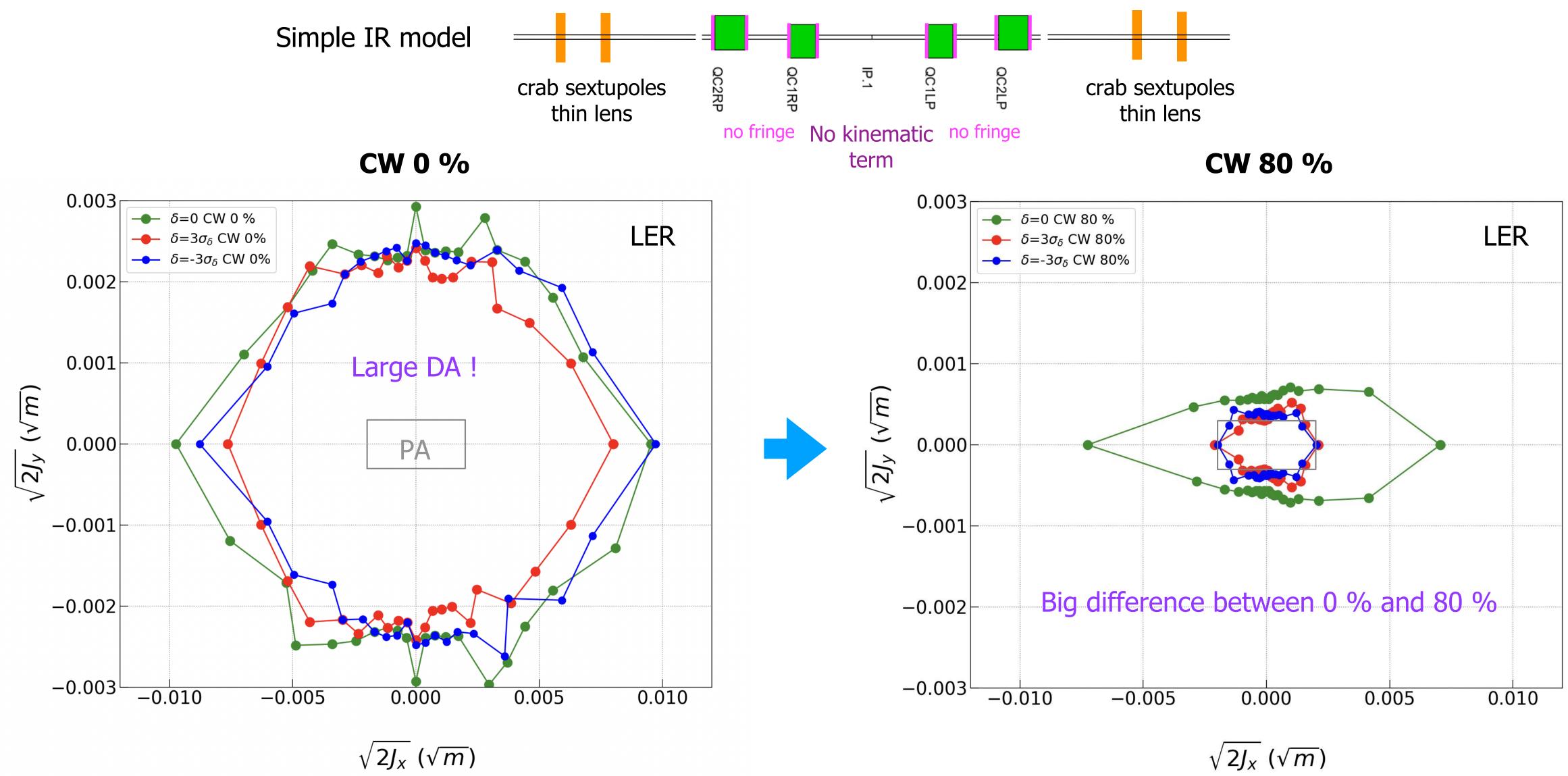






Comparison of Dynamic Aperture (Simple+Linearized IR Model)

Case 1: Kinematic term, QC1 nonlinear fringe, QC2 nonlinear fringe, Crab sextupole thickness are turned OFF in the LER.







Motivation:

Dynamic and physical aperture is one of the most important issue. Evaluation of both horizontal and vertical aperture is necessary to optimize sextupole magnets. Collimator aperture can be calibrated.

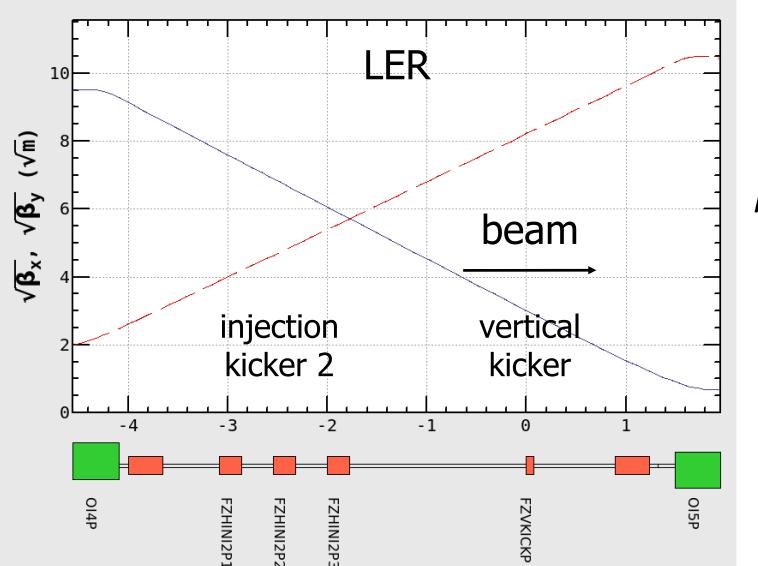
Nonlinear effects should be also evaluated.

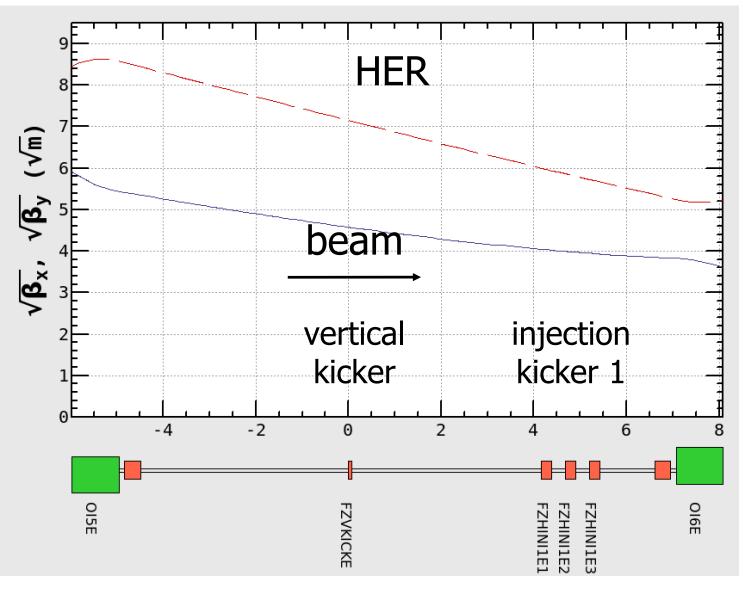
Method:

Injection and vertical kickers with TBT BPMs, DCCT (to measure beam loss)

No vertical kicker so far, this is just a plan. But the ceramic chamber exists.

We also have to prepare power supplies.



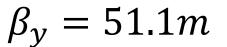


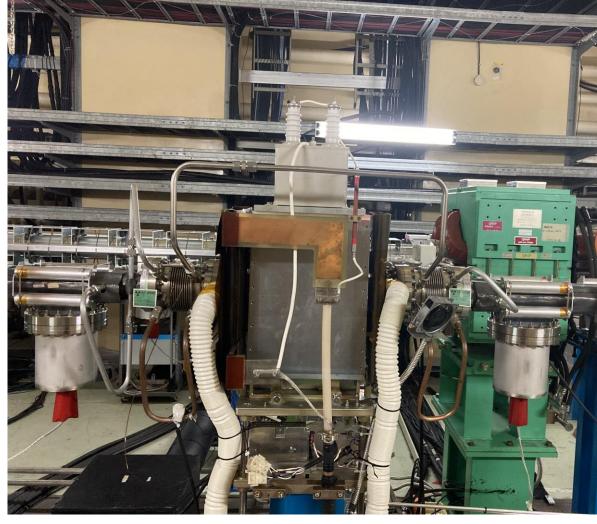
Possible Location of Vertical Kicker

$$\beta_y = 67.5m$$



LER













- Lattice nonlinearity is strong for both rings. 0
 - Amplitude detuning (vertical) is positive in LER, negative in HER. (Realistic IR Model) 0
 - QC1 nonlinear fringe is dominant in the LER. 0
 - Thickness of crab sextupole compensates with QC1 fringe in the HER. Residual octupole field makes negative detuning. 0
 - TBT BPM data with a vertical and/or horizontal kicker is useful to evaluate nonlinear effects and amplitude detuning. 0
 - J. Keintzel, the presentation with injection kickers is found in https://kds.kek.jp/event/45852/. 0
- Amplitude detuning (vertical) can be corrected by octuple correctors in the QC1 and QC2. 0
 - Dynamic aperture is not improved in the LER even though the vertical detuning is corrected, so far. 0
- Vertical kicker can be used to survey vertical aperture of the ring. (Dynamic and Physical Aperture) 0
 - In the horizontal direction, injection kickers (making unbalance of 2 kickers) can be used to measure DA precisely. 0
 - If both horizontal and vertical kickers can be used simultaneously, DA in the x-y plane can be surveyed. 0
 - This system is necessary for sextupole optimization to make Touschek lifetime longer. (select better sextupole setting)
 - Off-momentum aperture can be also evaluated with RF frequency shift.





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Appendix







Comparison

Parameter	Closed Orbit Distortion	Turn-by-Turn		_	
Tarafficter	Closed Orbit Distortion	Injection Kicker	Phase Lock Loop		
BPMs in HER	466	68	68 Mo	– ore TbT BPMs	It depends on b
BPMs in LER	444	70	70 pos	ssible?	The electric circ
Hor. optics measurement	yes	yes	yes		so can we get F
Ver. optics measurement	yes	no	yes		
RDTs measurement	no	some	yes		
Calibration independent	no	yes	yes		
Status for measurements	stable	stable	being explored		
Trigger to record data	yes	yes	no		
Time for measurement	$\approx 20 \mathrm{mins}$	$\approx 2 \text{ mins}$	$\approx 2 \text{mins}$	TbT typically faster	
	<u>↑</u>				

The optics correction uses COD based measurements.



COD-BPM Measurement and TBT-BPM Measurement

J. Keintzel, "Turn-by-Turn Optics Measurements in SuperKEKB" SuperKEKB ITF Optics Tuning Meeting, March 14, 2022

JACQUELINE KEINTZEL TBT OPTICS MEASUREMENTS



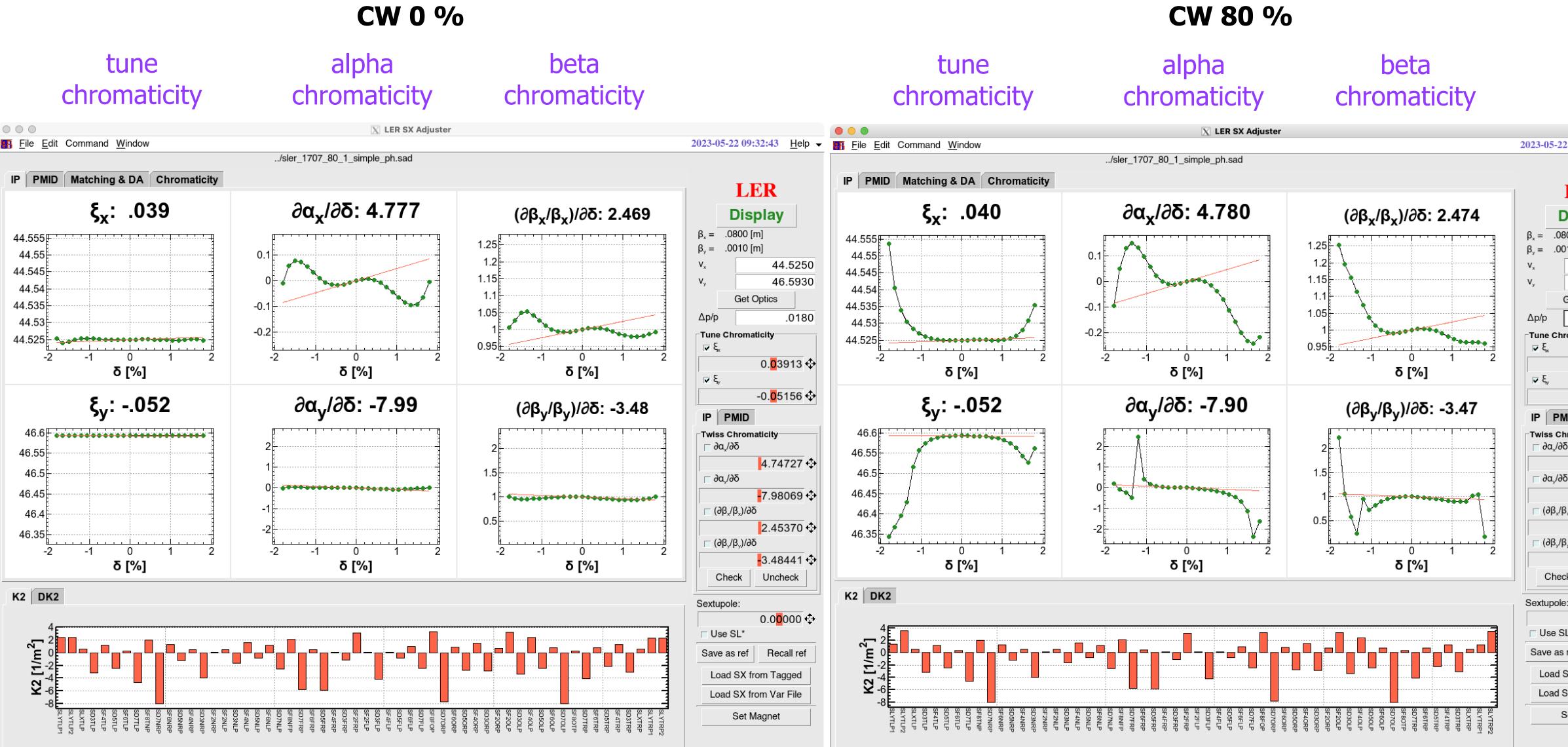
budget. cuit is old, FPGA ?.



tune

alpha

beta



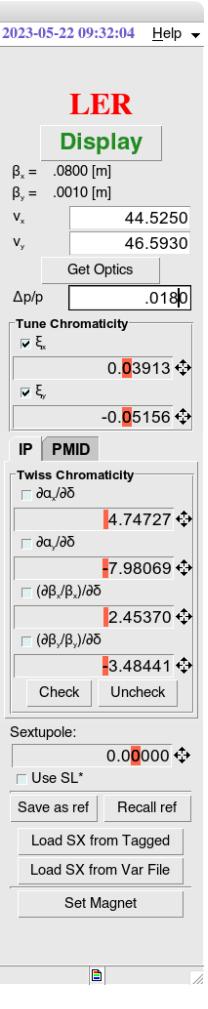
Main Application Area

Chromaticity in LER (Simple IR Model)

Menu Bar

The momentum deviation larger than 1 % is different from CW 0 %.

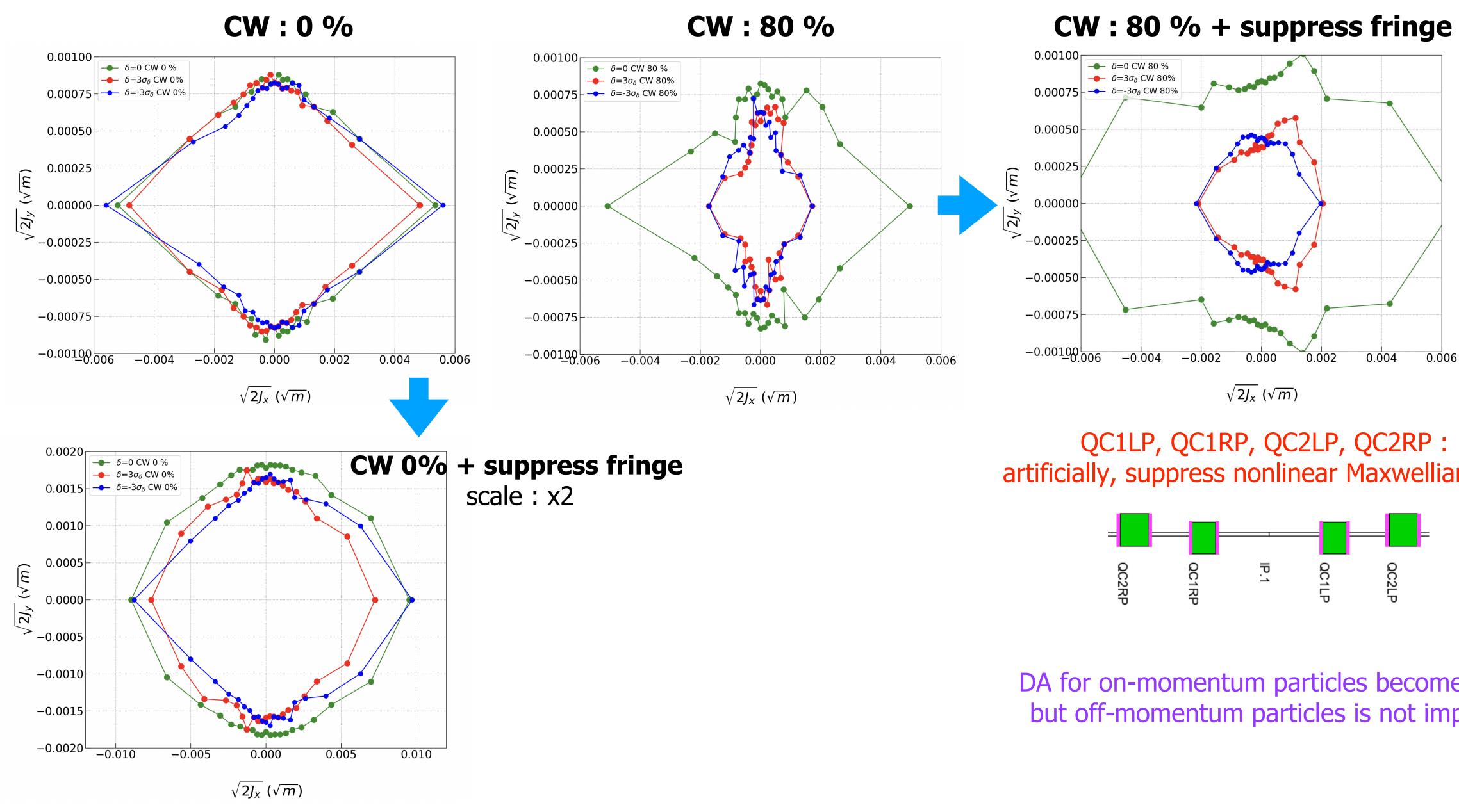












Dynamic Aperture in LER (Simple IR Model)

artificially, suppress nonlinear Maxwellian fringe

DA for on-momentum particles becomes large, but off-momentum particles is not improved.







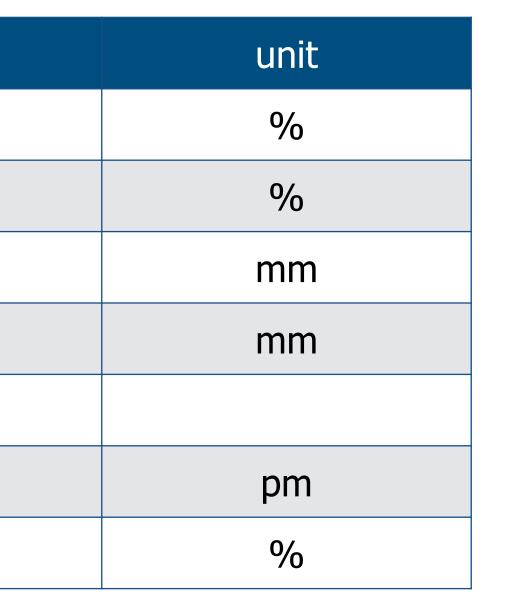


- The optics correction is performed at a low beam current. Typically, about 50 mA.
- Performance of optics corrections (beta, dispersions, X-Y couplings) for $\beta_v^* = 1mm$:

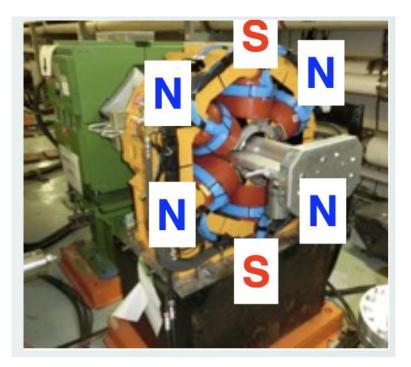
LER	HER
5	5
5	5
10	30
5	5
0.016	0.012
25	40
0.63	0.87
	5 5 10 5 0.016 25

- These results are obtained at low beam currents. The operation beam current is larger than 1 A.
- Beam pipe is deformed due to intense SR heating. BPM with beam pile is connected with a neighbor quadrupole magnet tightly. BPM can push the quadrupole magnet horizontally, horizontal kick is induced.
- Horizontal orbit at the strong sextupole creates large beta-beat.

Optics Corrections

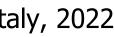


Vertical dispersions and X-Y couplings are corrected by using skew quad-like correctors.







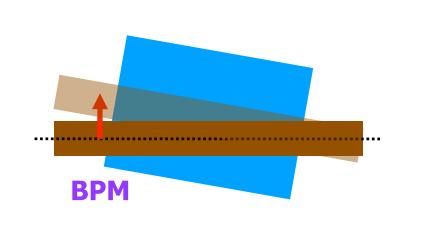




BPM is fixed at quadrupole magnet and displacement monitor measures relative deviation (horizontal and vertical) between the BPM and the sextupole magnet.

BPM and Quadrupole Magnet



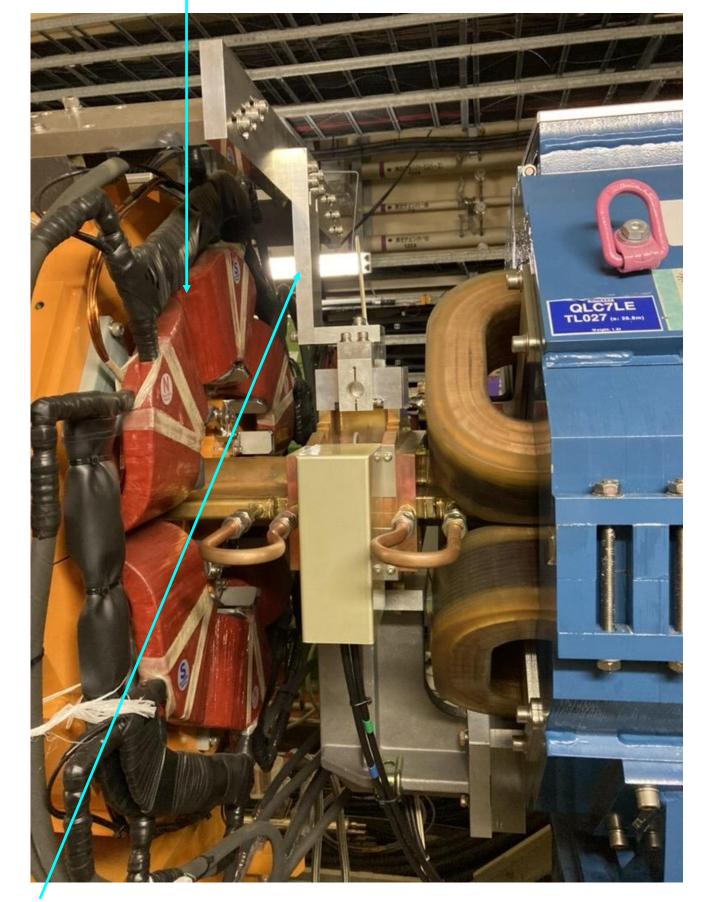


The beam pipe (BPM) is fixed to the quadrupole magnet.

BPMs, Quadrupoles, and Sextupoles

Crab Sextupole in the HER

Quad. moves like yaw and horizontal shift if BPM pushes quad.



Gap sensor measures ($\Delta x, \Delta y$) between BPM and sextupole. Relation between BPM and quad. does not change. (see left fig.)

