

# **LIMITED FREQUENCY BANDWIDTH ON THE INVERSE SCATTERING SERIES AND THE EFFECTS ON SEISMIC PROCESSING GOALS**

by

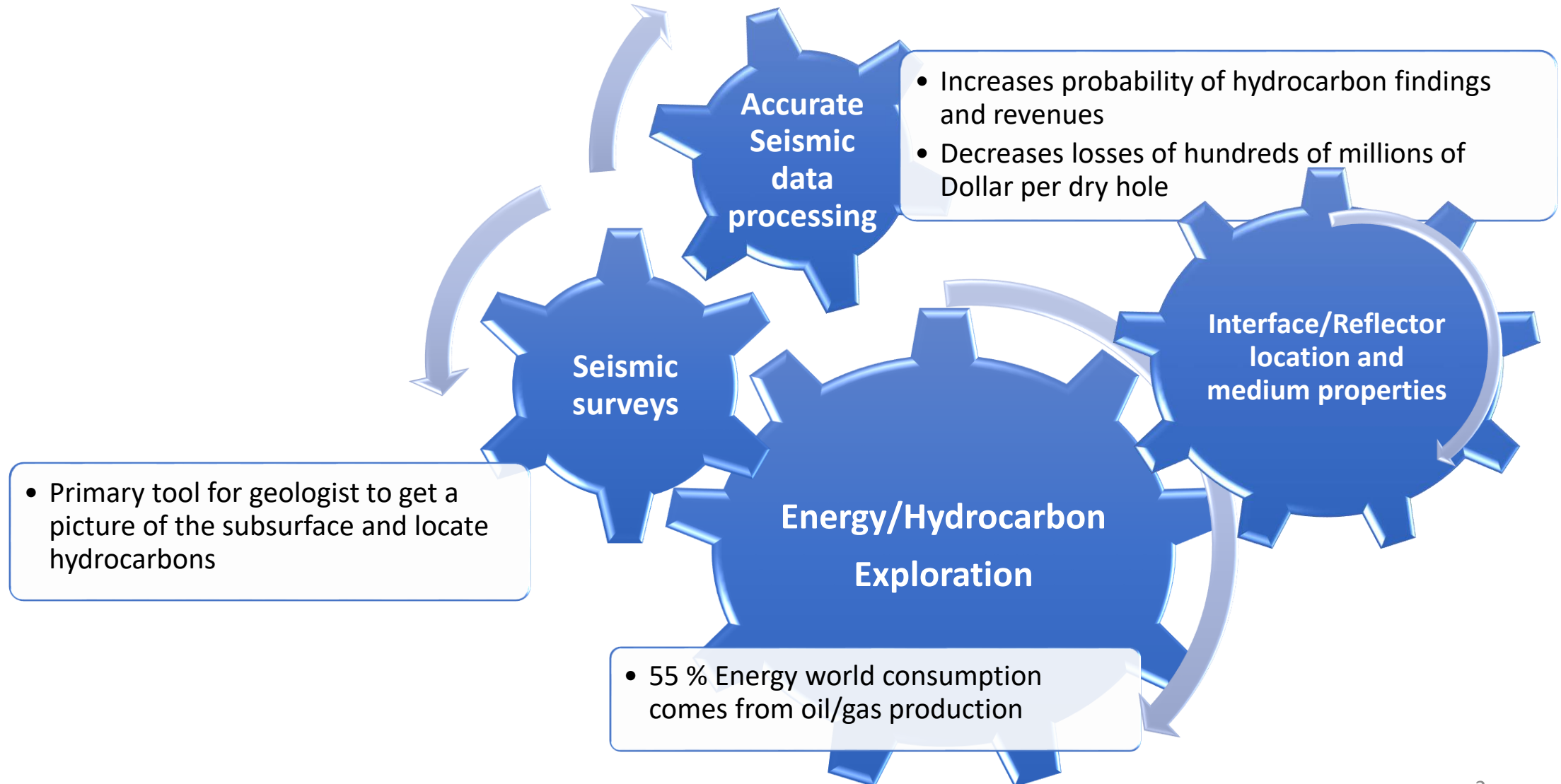
Ms. Ana Gonzalez

Dr. Mark Meier

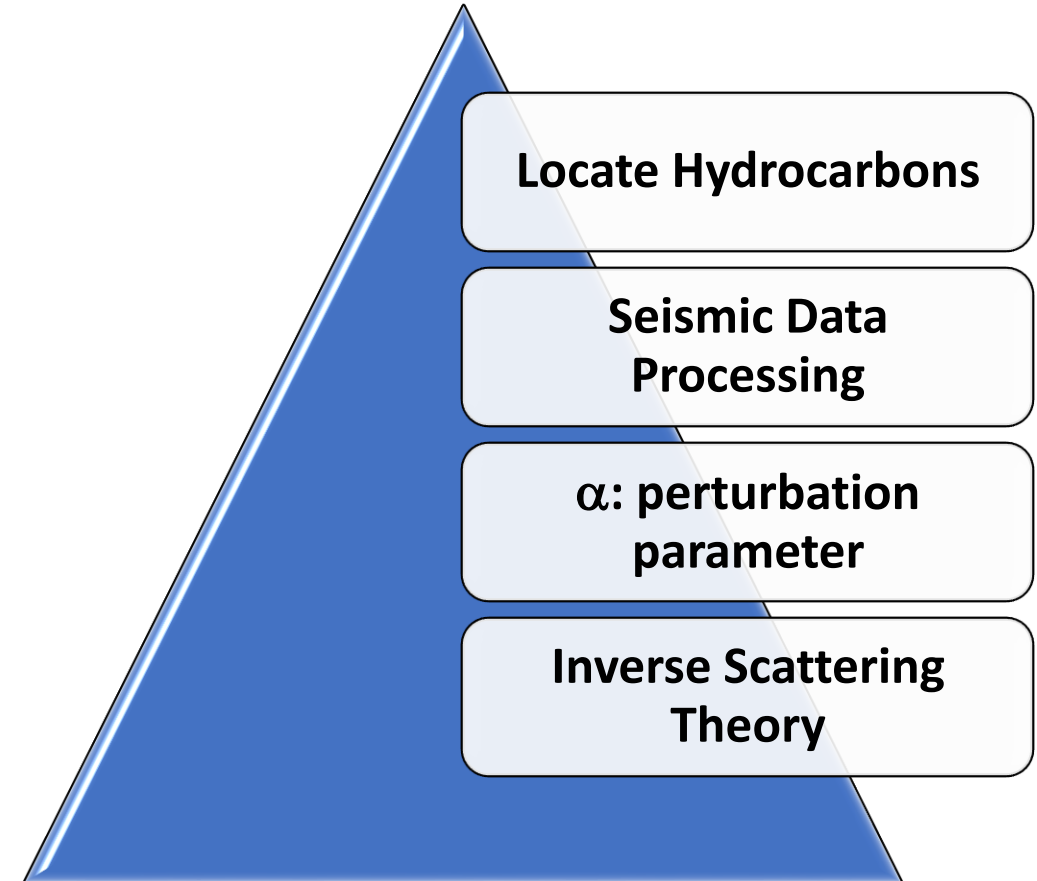
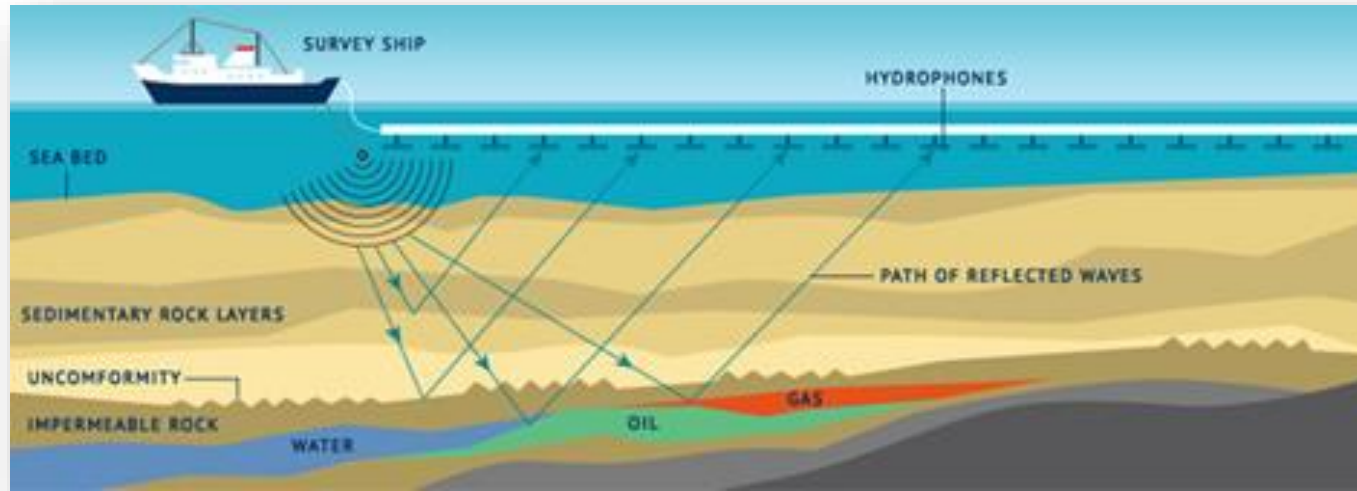
Research day 2023

Department of Physics

# Background



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$$\alpha(\vec{r}) = \alpha_1(\vec{r}) + \alpha_2(\vec{r}) + \alpha_3(\vec{r}) + \dots$$

# **Statement of the problem**

## **Objective**

**Determine the effects of limited frequency bandwidth in the inverse scattering series and examine the impact of improved bandwidth in achieving seismic processing goals.**

# Inverse Scattering Series

$$\begin{aligned}
 (\psi_s)_{ms} &= (G_o^+ V_1 P_o)_{ms} \\
 (G_o^+ V_2 P_o)_{ms} &= -(G_o^+ V_1 G_o^+ V_1 P_o)_{ms} \\
 (G_o^+ V_3 P_o)_{ms} &= -(G_o^+ V_1 G_o^+ V_2 P_o)_{ms} - (G_o^+ V_2 G_o^+ V_1 P_o)_{ms} \\
 &\vdots
 \end{aligned}$$

**\* Assumption:** Homogeneous, acoustic medium (no absorption or dispersion) with constant density, varying velocity.

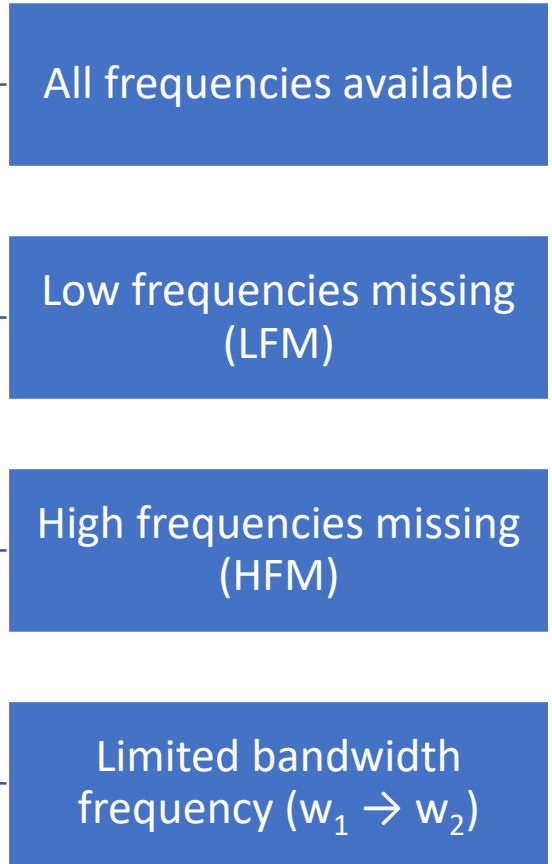
Analytical method /numerical evaluation (Python)

**\* One interface**

**\* Assuming plane waves propagating in one-dimension, normal incidence**

**\* Reference medium with defined velocity  $C_o$ .**

$\alpha_1$   
 $\alpha_2$



$$V_1(\vec{r}) = k^2 \alpha_1(\vec{r})$$

$$V_2(\vec{r}) = k^2 \alpha_2(\vec{r})$$

$$V_3(\vec{r}) = k^2 \alpha_3(\vec{r})$$

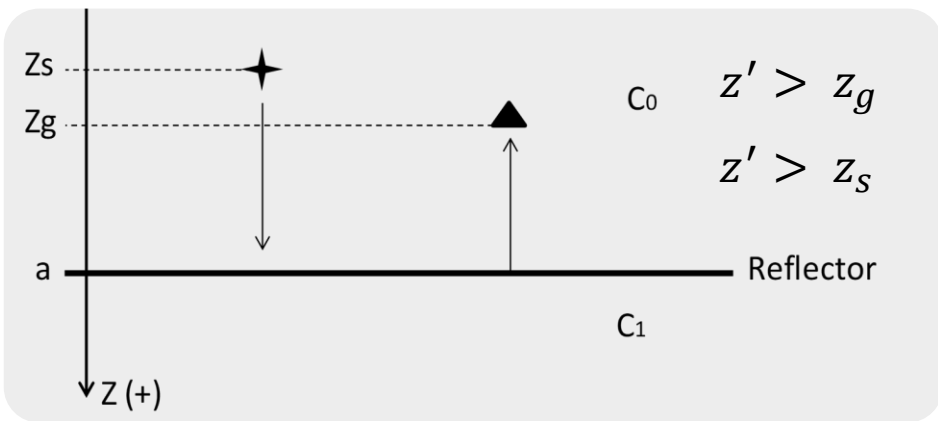


$$\alpha(\vec{r}) = \alpha_1(\vec{r}) + \alpha_2(\vec{r}) + \alpha_3(\vec{r}) + \dots$$

**Error analysis**

Weglein et al, 1981.  
Weglein et al, 2003.

# Determining $\alpha_1$ analytically for an active source with all frequencies available



According to inverse scattering series the recorded data for the linear inverse problem at  $Z = Zg$  is:

$$\text{DATA} = \int_{-\infty}^{\infty} G_0^+(z', z_g, w) V_1(z', w) P_0(z', z_s, w) dz'$$

Weglein et al, 1981.  
Weglein et al, 2003.

$G_0^+(z', z_g, w)$  is the causal Green's Function  $\frac{e^{i\frac{w}{c_0}|z'-z_g|}}{2ik}$

$$V_1(z', w) = k^2 \alpha_1(z')$$

Considering  $Z > Zs$ , the wave field traveling away from the source to the reflector is given:

$$P_0(z, w) = e^{i w \frac{(z-z_s)}{c_0}}$$

The reflected wave field at  $Z = Zg$  is:

$$P_R(z_s, z_g, w) = \text{Re} \frac{i w}{c_0} (2a - z_s - z_g) = \text{DATA}$$

Fourier transforming from  $Z$  to  $Kz$

$$\widetilde{\alpha}_1(k_z) = -\frac{4i}{k_z} \text{Re}^{-ik_z a}$$

Inverse Fourier transforming from  $Kz$  to  $Z$

$$\alpha_1(z) = 4R H(z - a)$$

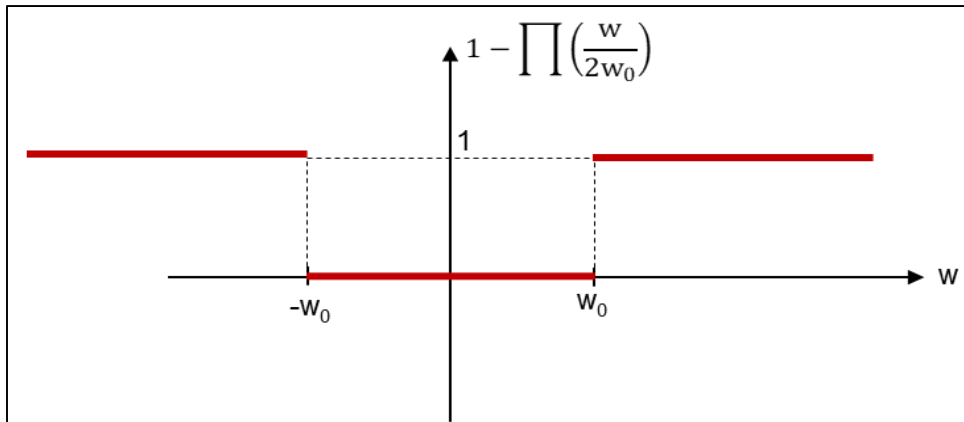
# Determining $\alpha_1$ analytically for an active source with Low frequencies Missing (LFM)

$$\text{DATA} = \int_{-\infty}^{\infty} G_0^+(z', z_g, w) V_1(z', w) P_0(z', z_s, w) dz'$$

The wave field coming from the source at  $z = z_s$  is given

by:

$$P_0(z = z_s, w) = 1 - \Pi\left(\frac{w}{2w_0}\right)$$



$$P_R(z_s, z_g, w) = \text{Re} \left[ e^{i\frac{w}{c_0}(2a - z_s - z_g)} \left[ 1 - \Pi\left(\frac{w}{2w_0}\right) \right] \right] = \text{DATA}$$

Fourier transforming from  $Z$  to  $K_z$

$$\tilde{\alpha}_1(k_z) \left[ 1 - \Pi\left(\frac{w}{2w_0}\right) \right] = -\frac{4i}{k_z} \text{Re}^{-ik_z a} \left[ 1 - \Pi\left(\frac{w}{2w_0}\right) \right]$$

$$\tilde{\alpha}_1(k_z) \left[ 1 - \Pi\left(\frac{w}{2w_0}\right) \right] = \tilde{\alpha}_1(k_z)_{\text{estimated}} = \tilde{\alpha}_1(k_z)_{\text{est}}$$

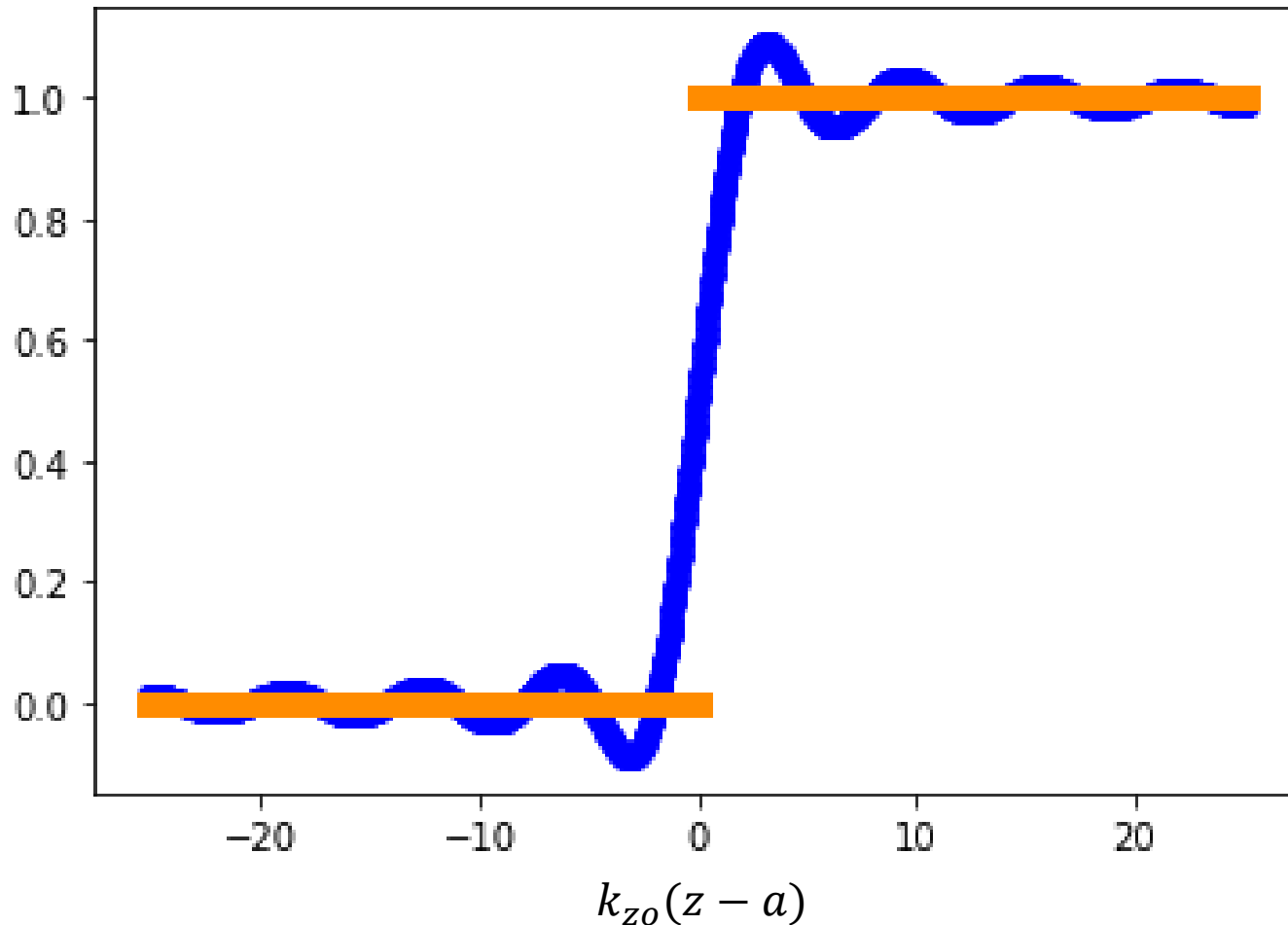
Inverse Fourier transforming from  $K_z$  to  $Z$

$$\frac{\alpha_1(k_{z_0} z)_{\text{est}}}{4R} = H(z) - \frac{1}{2} - \frac{1}{\pi} \int_0^z \frac{\sin k_{z_0} z'}{z'} dz'$$

$$\frac{\alpha_1(z)_{\text{est}}}{4R} = H(z - a) - \frac{1}{2} - \frac{1}{\pi} \int_0^{k_{z_0}(z-a)} \frac{\sin z'}{z'} dz'$$

# Analysis for $\alpha_1$ with an active source with HFM

For High Frequencies Missing (HFM)



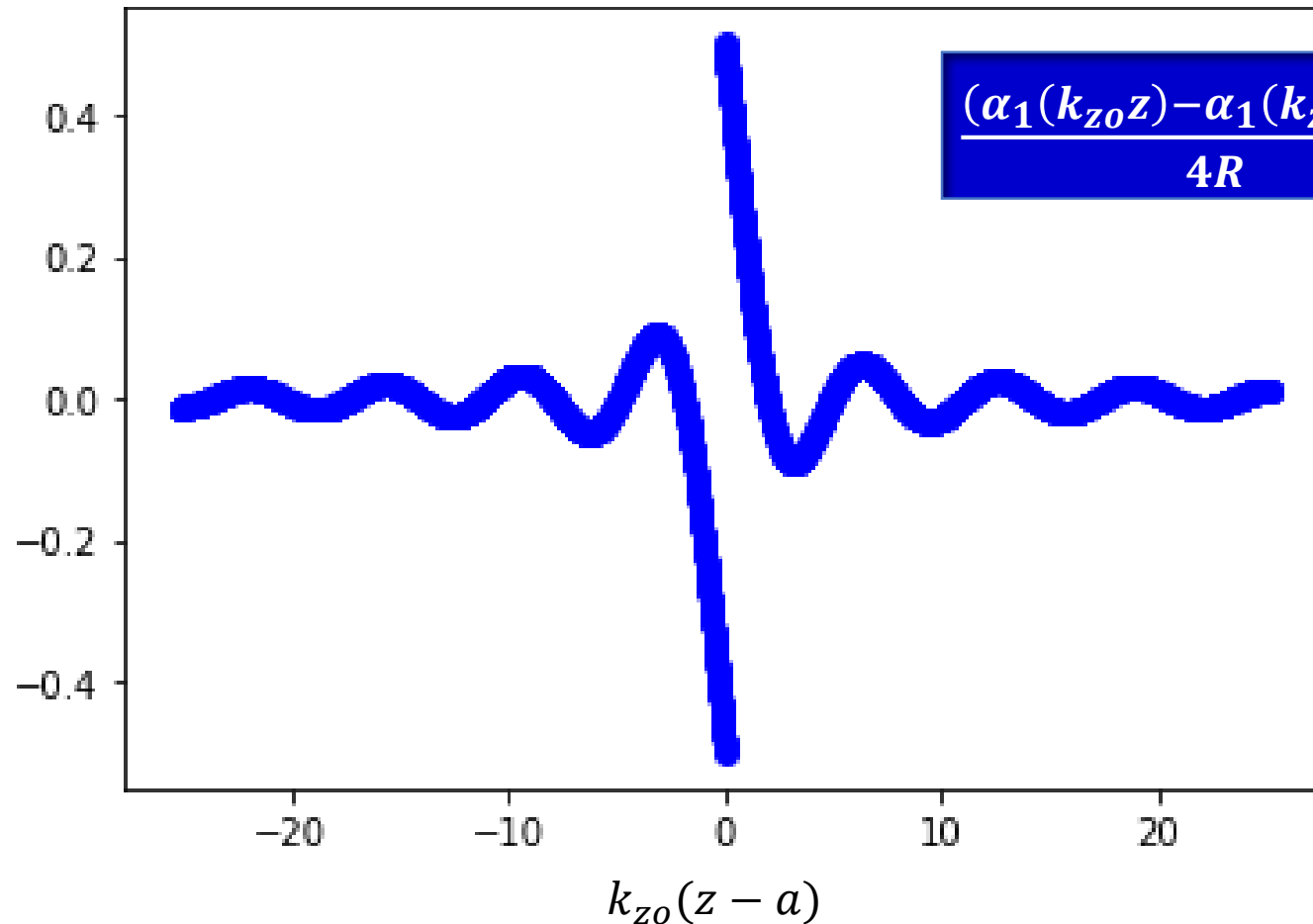
$$\frac{\alpha_1(z)}{4R} = H(z-a)$$

$$\frac{\alpha_1(z)_{est}}{4R} = \frac{1}{2} + \frac{1}{\pi} \int_0^{k_{zo}(z-a)} \frac{\sin z'}{z'} dz'$$



# Analysis for $\alpha_1$ with an active source with HFM

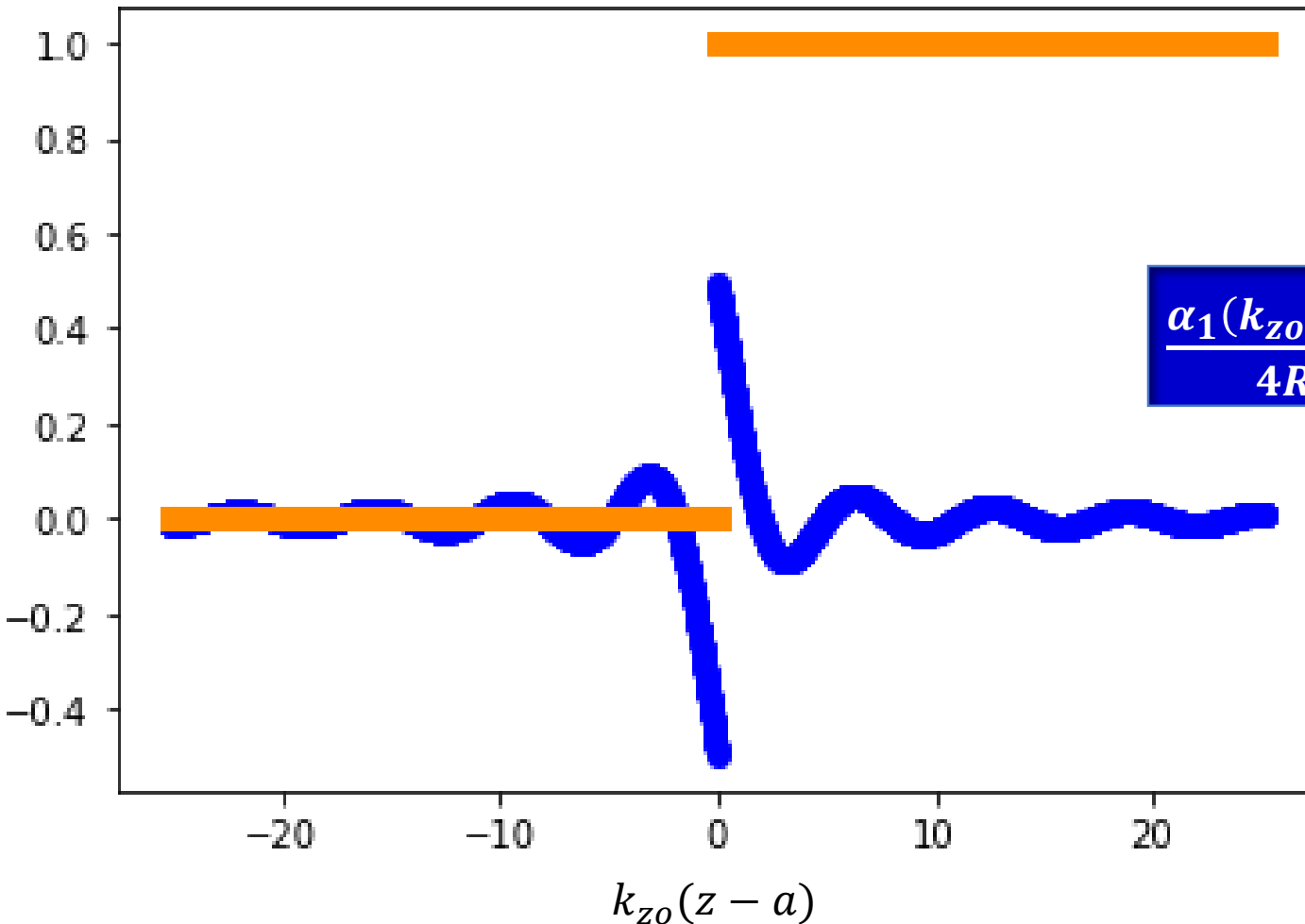
Error For High Frequencies Missing (HFM)



$$\frac{(\alpha_1(k_{zo}z) - \alpha_1(k_{zo}z)_{est})}{4R} = H(z - a) - \frac{1}{2} - \frac{1}{\pi} \int_0^{k_{zo}(z-a)} \frac{\sin z'}{z'} dz'$$

# Analysis for $\alpha_1$ with an active source with LFM

For Low Frequencies Missing (LFM)

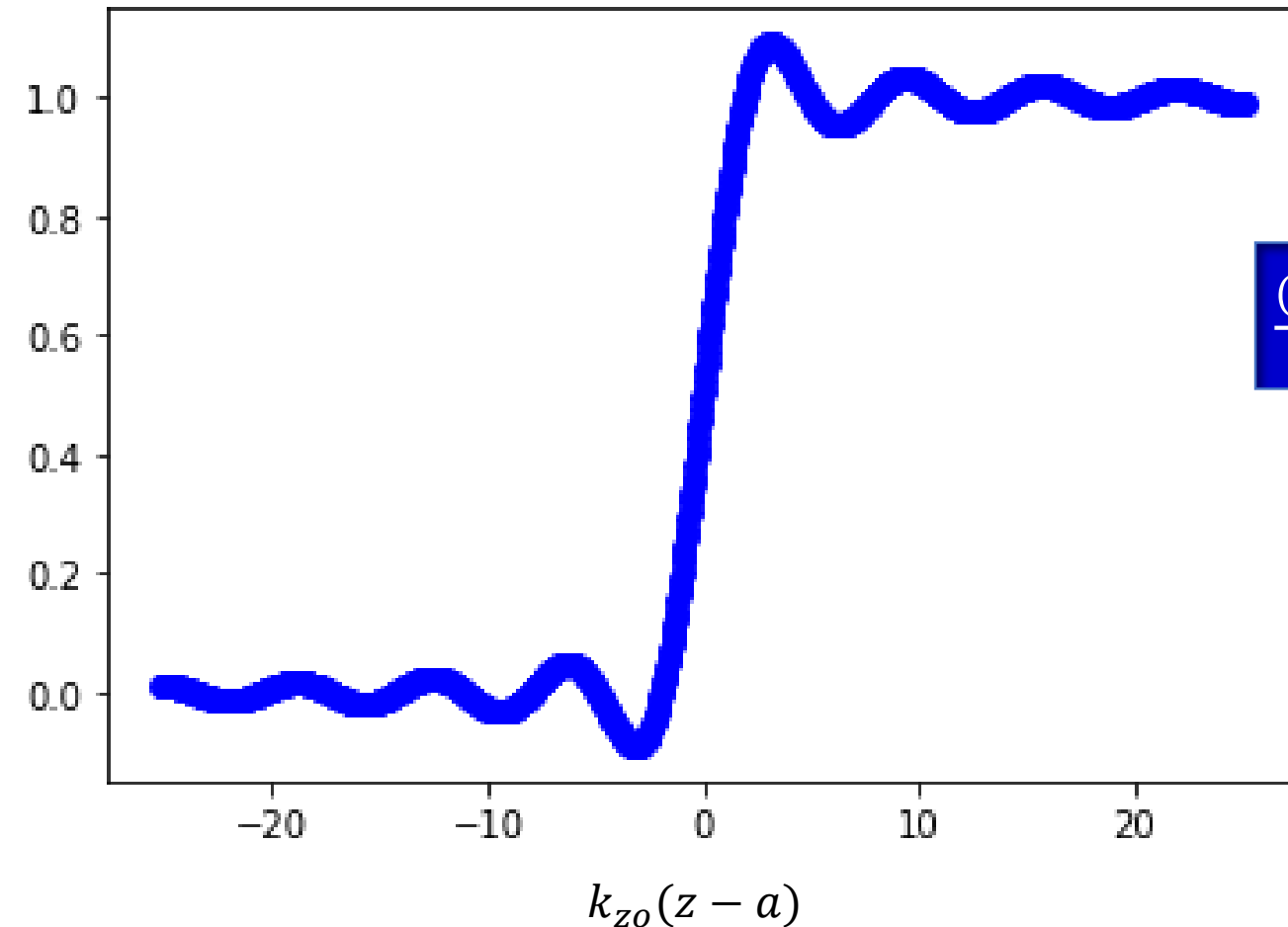


$$\frac{\alpha_1(z)}{4R} = H(z - a)$$

$$\frac{\alpha_1(k_{zo}z)_{est}}{4R} = H(z - a) - \frac{1}{2} - \frac{1}{\pi} \int_0^{k_{zo}(z-a)} \frac{\sin z'}{z'} dz'$$

# Analysis for $\alpha_1$ with an active source with LFM

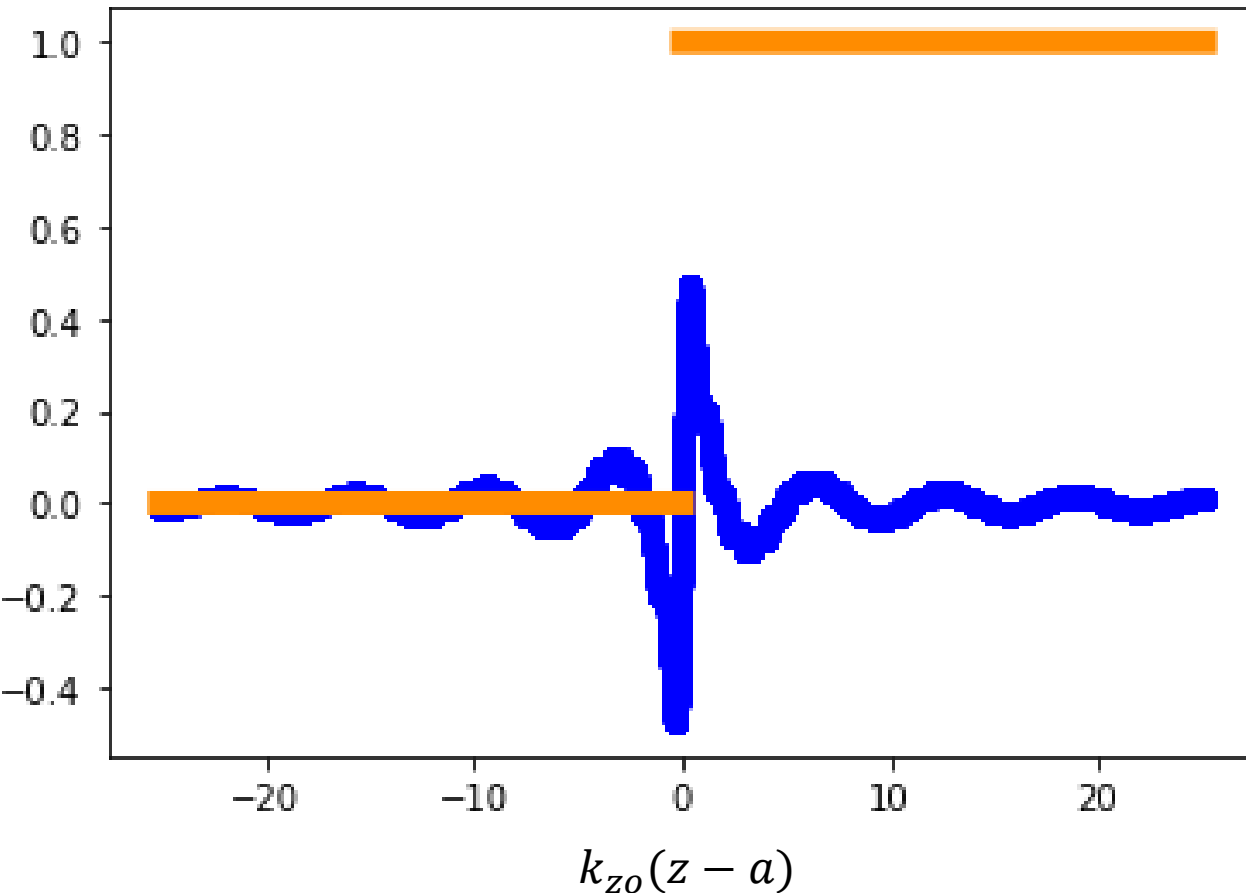
Error For Low Frequencies Missing (LFM)



$$\frac{(\alpha_1(k_{zo}z) - \alpha_1(k_{zo}z)_{est})}{4R} = \frac{1}{2} + \frac{1}{\pi} \int_0^{k_{zo}(z-a)} \frac{\sin z'}{z'} dz'$$

# Analysis for $\alpha_1$ with an active source with limited bandwidth frequencies ( $w_1 - w_2$ ), 3 octaves

For LBF  $w_1$  to  $w_2$  (3 octaves)

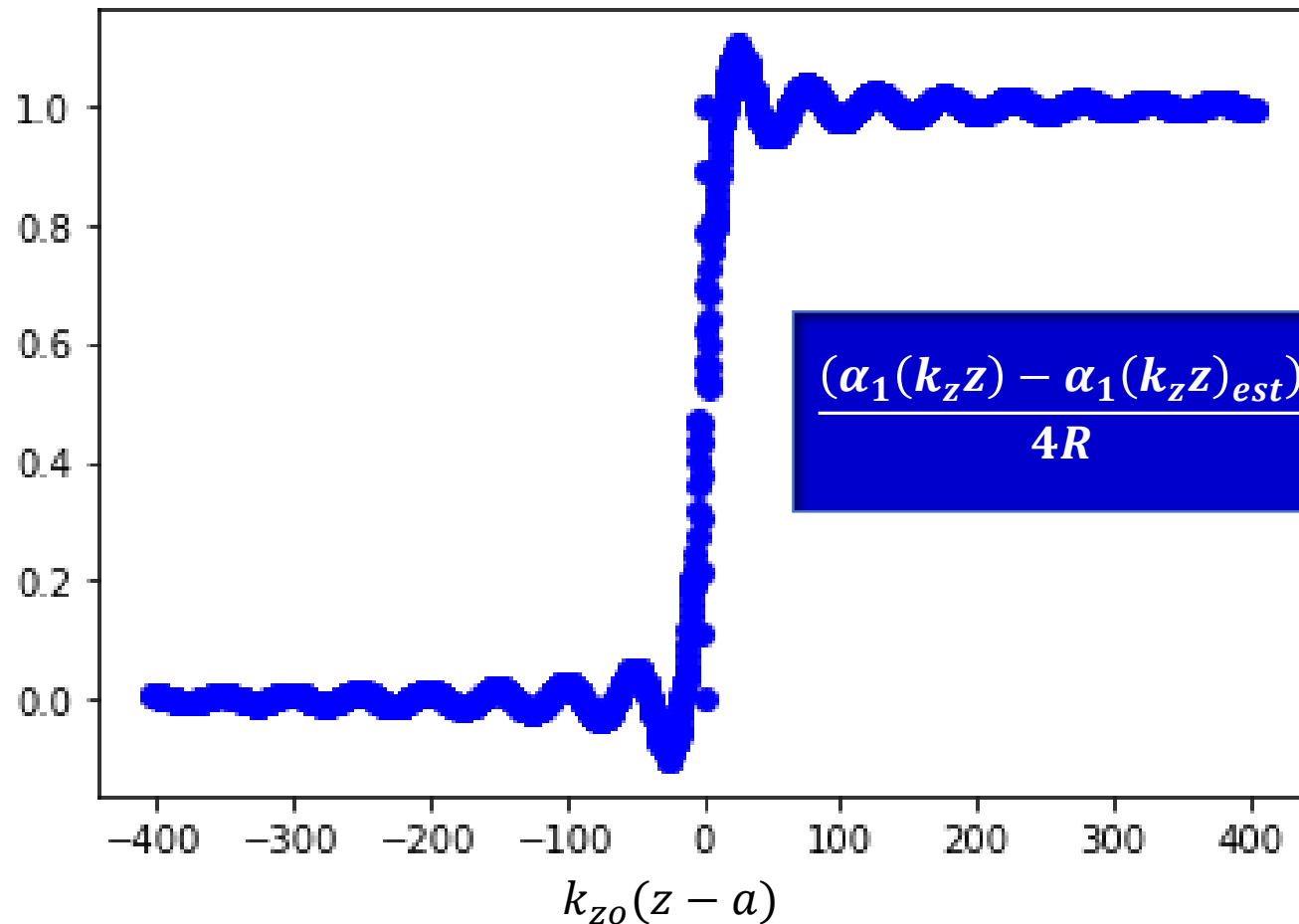


$$\frac{\alpha_1(z)}{4R} = H(z - a)$$

$$\frac{\alpha_1(k_z z)_{est}}{4R} = \frac{1}{\pi} \left[ \int_0^{k_{z2}(z-a)} \frac{\sin z'}{z'} dz' - \int_0^{k_{z1}(z-a)} \frac{\sin z'}{z'} dz' \right]$$

# Analysis for $\alpha_1$ with an active source with limited bandwidth frequencies ( $w_1 - w_2$ )

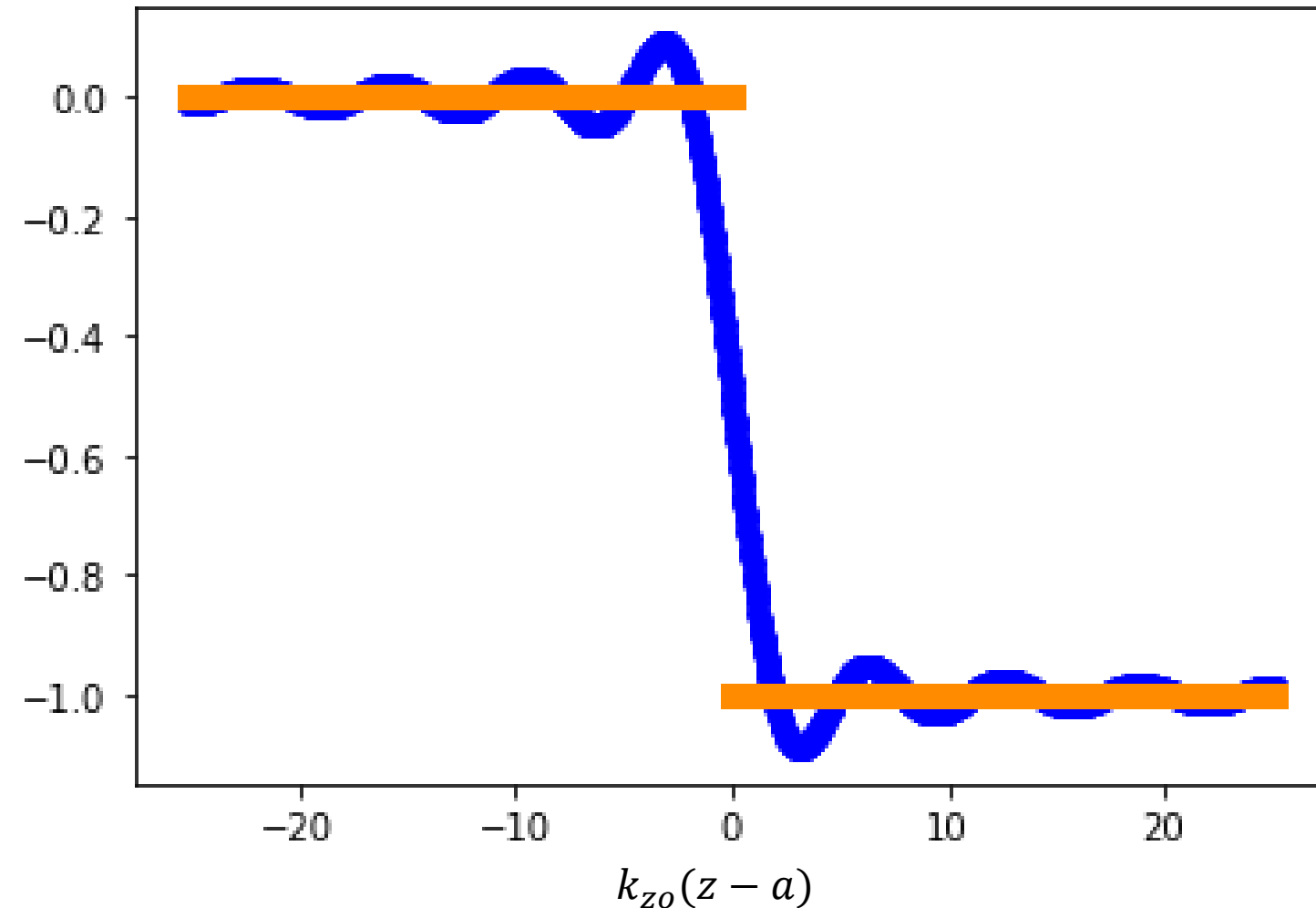
Error LBF  $w_1$  to  $w_2$  (3 octaves)



$$\frac{(\alpha_1(k_z z) - \alpha_1(k_z z)_{est})}{4R} = H(z-a) - \frac{1}{\pi} \left[ \int_0^{k_{z2}(z-a)} \frac{\sin z'}{z'} dz' - \int_0^{k_{z1}(z-a)} \frac{\sin z'}{z'} dz' \right]$$

# Analysis for $\alpha_2$ with an active source with HFM

For High Frequencies Missing (HFM)

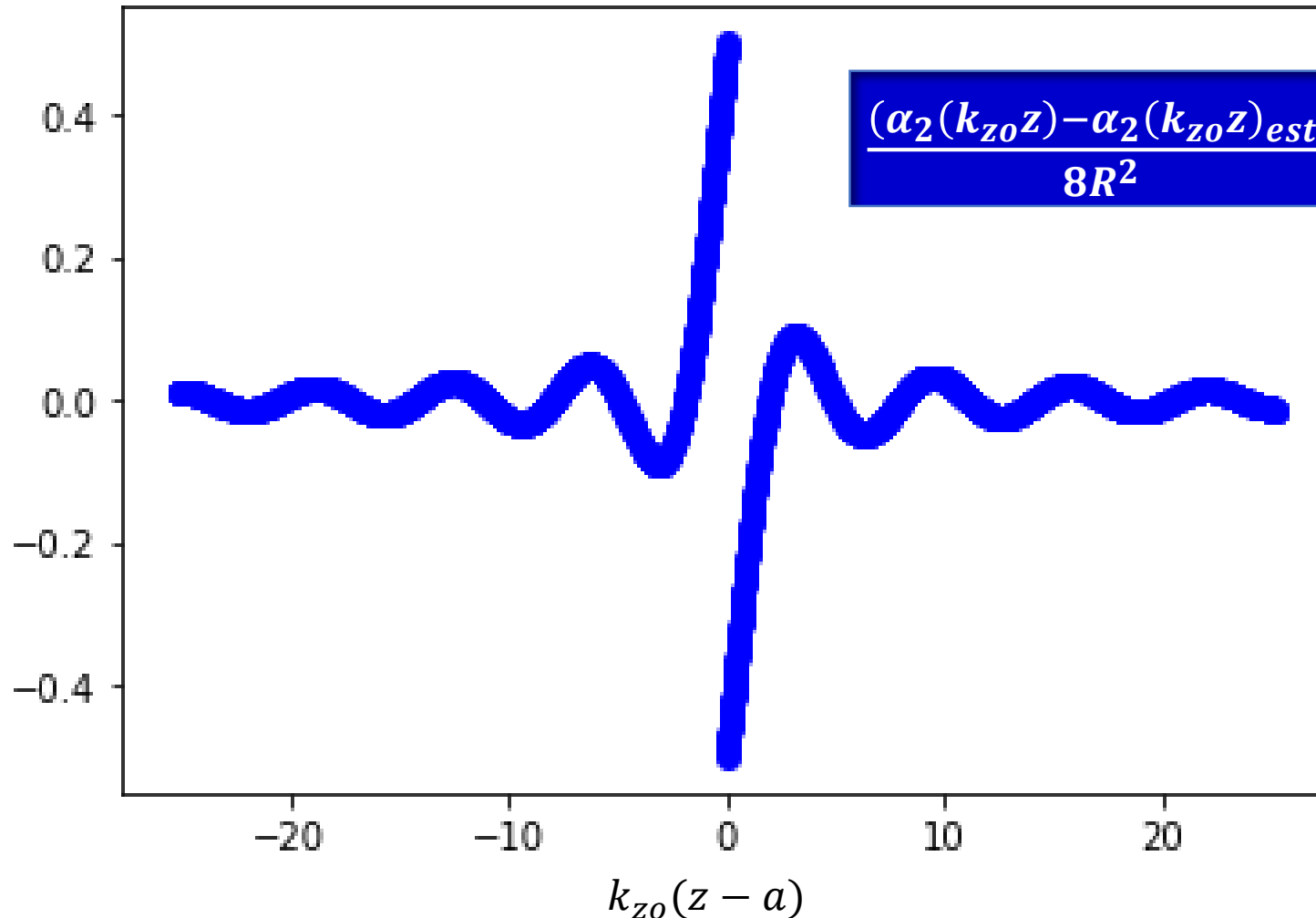


$$\frac{\alpha_2(z)}{8R^2} = H(z-a)$$

$$\frac{\alpha_2(k_{z0}z)_{est}}{8R^2} = -\frac{1}{2} - \frac{1}{\pi} \int_0^{k_{z0}(z-a)} \frac{\sin z'}{z'} dz'$$

# Analysis for $\alpha_2$ with an active source with HFM

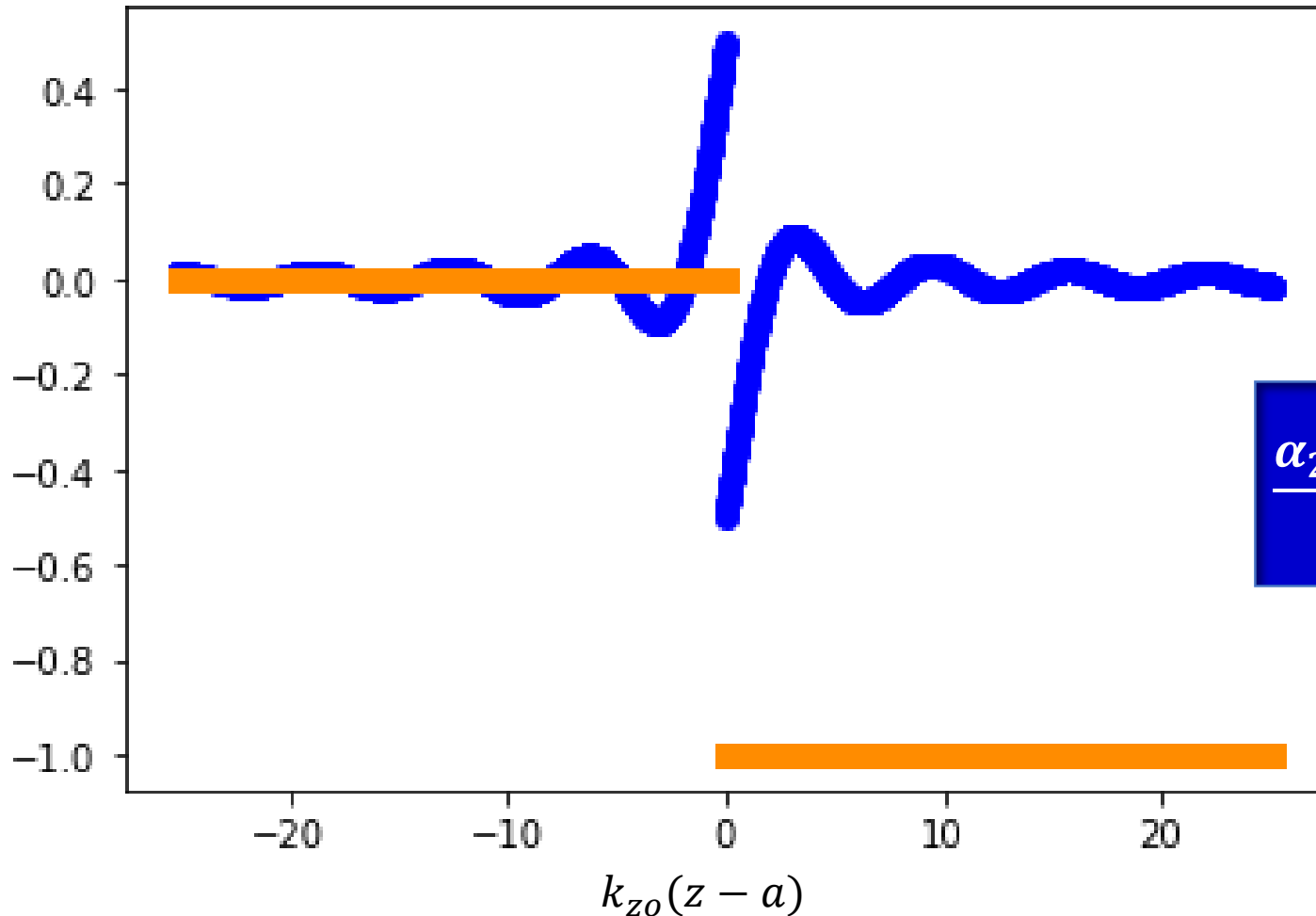
Error For High Frequencies Missing (HFM)



$$\frac{(\alpha_2(k_{z0}z) - \alpha_2(k_{z0}z)_{est})}{8R^2} = -H(z - a) + \frac{1}{2} + \frac{1}{\pi} \int_0^{k_{z0}(z-a)} \frac{\sin z'}{z'} dz'$$

# Analysis for $\alpha_2$ with an active source with LFM

For Low Frequencies Missing (LFM)



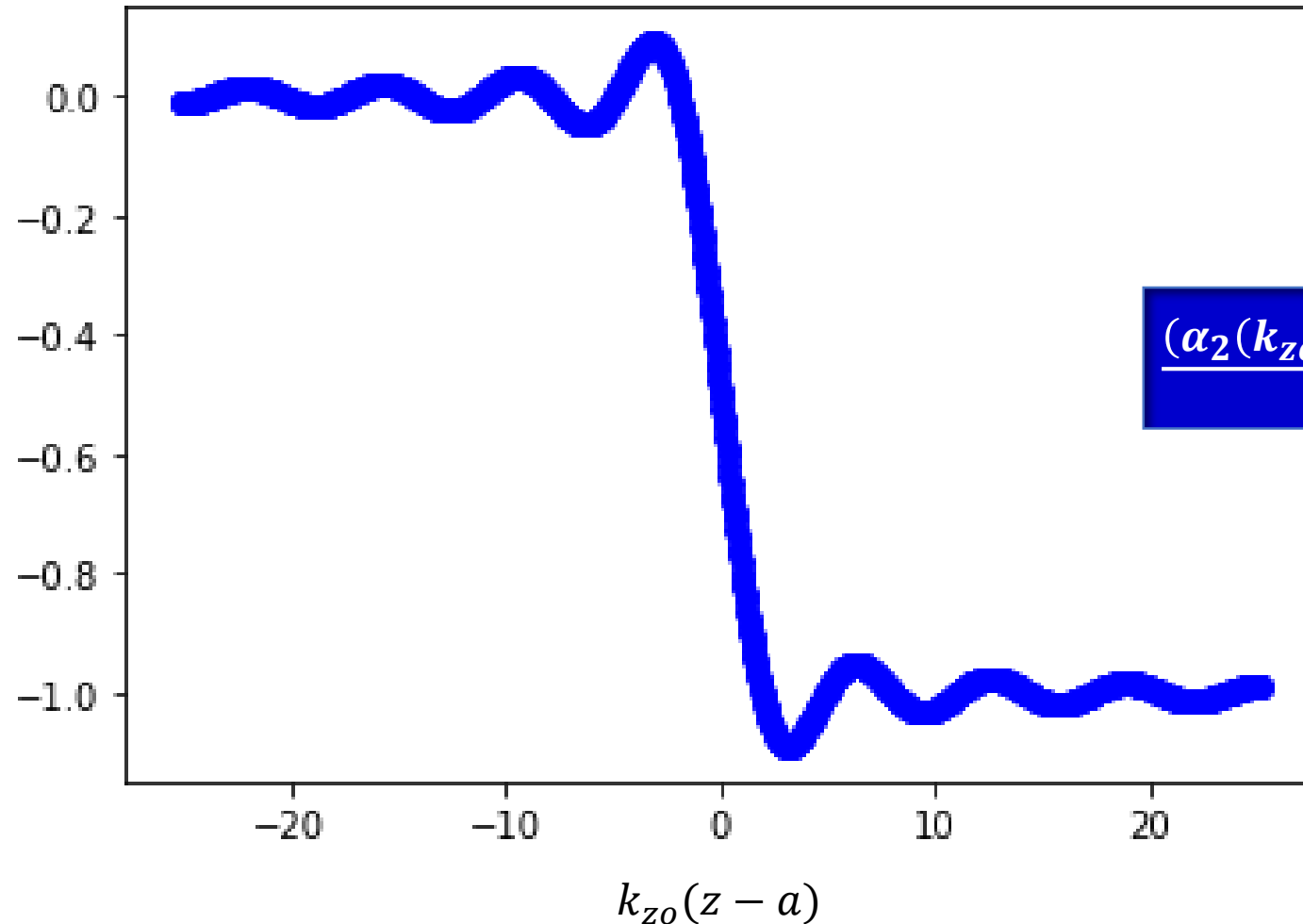
$$\frac{\alpha_2(z)}{8R^2} = -H(z-a)$$

$$\frac{\alpha_2(k_{zo}z)_{est}}{8R^2} = -H(z-a) + \frac{1}{2} + \frac{1}{\pi} \int_0^{k_{zo}(z-a)} \frac{\sin z'}{z'} dz'$$



# Analysis for $\alpha_2$ with an active source with LFM

Error For Low Frequencies Missing (LFM)



$$\frac{(\alpha_2(k_{zo}z) - \alpha_2(k_{zo}z)_{est})}{8R^2} = -\frac{1}{2} - \frac{1}{\pi} \int_0^{k_{zo}(z-a)} \frac{\sin z'}{z'} dz'$$

# Summary

For an acoustic model medium with constant density and varying velocity, 1-D normal incidence plane wave, and one interface:

- ❖  $\alpha_1$  and  $\alpha_2$  cannot be fully determined when frequencies are missing, but portions of  $\alpha_1$  and  $\alpha_2$  can be determined which are defined as  $\alpha_{1\text{est}}$  and  $\alpha_{2\text{est}}$ .
- ❖ The error is defined as the difference between  $\alpha_1$  and  $\alpha_{1\text{est}}$ , and as the difference between  $\alpha_2$  and  $\alpha_{2\text{est}}$ , respectively; and for both:
  - if only high frequencies are missing, the error is largest near the interface and decreases going away from the interface,
  - if low frequencies are missing, the error is increasing approaching the interface and remains large going deeper from the interface,
  - the same behavior is observed for three octave bandwidth.
- ❖ A band limited source restricts solutions to  $\alpha_{1\text{est}}$  and  $\alpha_{2\text{est}}$  affecting the accuracy of seismic inversion. Improving low frequency bandwidth has the greatest benefit. Though still under study, it appears band limit effects for seismic imaging and internal multiple removal are considerably less and are absent for surface multiple removal.

# References

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