

# Powering Schemes and Optimization

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20.June.23

# Organization of the presentation

- Muon acceleration with RCS: Power and Energy frame
- Power circuit considerations
- Powering Schemes
- The Control problem description
- Technologies
- Working plan
- Conclusions

# Accelerator Power and Energy: a general frame

RCS values from excel sheet

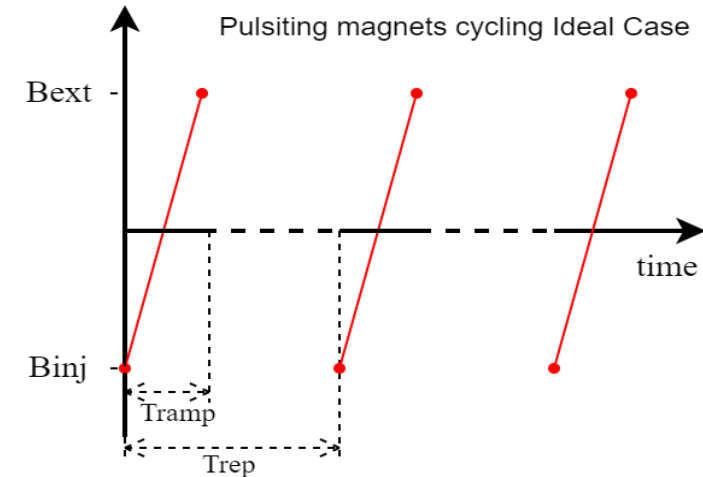
F. Batsch, H. Daimerau.

	RCS1	RCS2	RCS3	RCS4
Inj Energy [GeV]	63	314	750	1500
Acc. length [km]	5.99	5.99	10.7	35.0
Res. mags Lm [km]	3.65	2.54	4.37	20.38
Binj in gap [T]	0.36	-1.8	-1.8	-1.8
Bextr in gap [T]	1.8	1.8	1.8	1.8
B ramp time Tramp [ms]	0.35	1.10	2.37	6.37
Trepetition [ms]	200	200	200	200
Dipoles Gap w [mm]	100	100	100	100
Dipoles Gap h [mm]	30	30	30	30
Dipoles E <sub>gap</sub> @B <sub>ext</sub> [MJ]	14.1	9.8	16.9	78.8
Dipoles E <sub>tot</sub> @B <sub>ext</sub> [MJ]	21.2	14.7	25.3	118.2
Dipoles P <sub>max</sub> [GW]	111	54	43	74

$$E_{\text{gap } B_{\text{max}}} = \frac{B_{\text{max}}^2}{2 \mu_0} \cdot L_{\text{NCmags}} \cdot h_{\text{gap}} \cdot W_{\text{gap}}$$

$$E_{\text{mag}} \approx 1.5 \cdot E_{\text{gap } B_{\text{max}}}$$


$$P(t) = \frac{2 \cdot E_{\text{mag}}}{T_{\text{ramp}}/2}$$



Approximate calculations for the magnetic circuit, show that the total mmf is about **40 ÷ 50 kAturns** with an inductance of about **4.5 ÷ 6.5 uH/m** with a single series conductor.

The correspondent **inductive** voltage for the four RCS would be:

	RCS1	RCS2	RCS3	RCS4
Inductive Voltage of the power supply with a single turn	670 [V/m]	420 [V/m]	200 [V/m]	70 [V/m]
Total magnet voltage	2.4 [MV]	1.07 [MV]	0.9 [MV]	1.5 [MV]

High voltage and power must be divided into several sectors 

# Power Circuit Considerations: sectors in the accelerators

Independent power circuit sectors:

The ground can be placed on each circuit. Lower voltage to ground  
Much easier operation of power converters

**What accuracy is required intra-sector?**

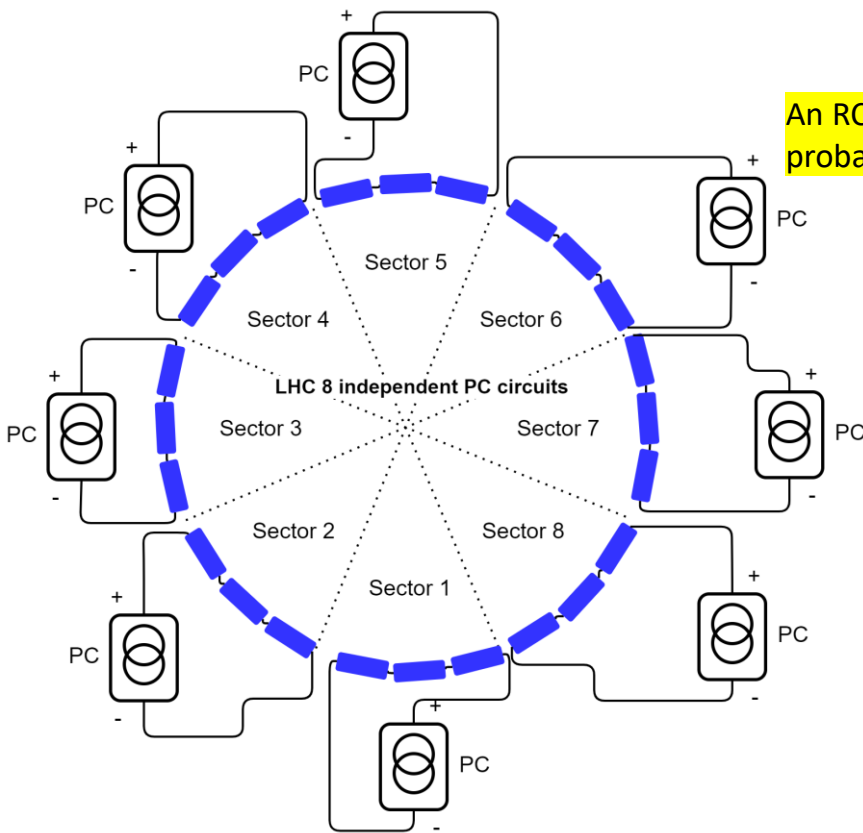
Pulse to pulse reproducibility stem from the intra-sector accuracy

Quasi-Series connection of all power circuit sectors:

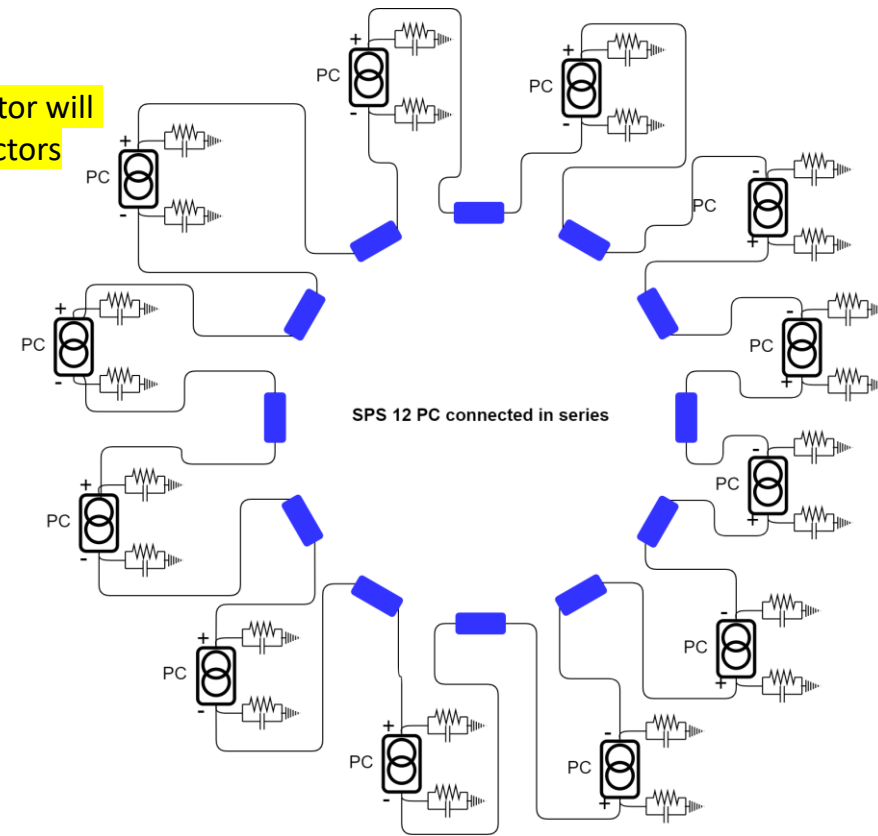
Current is the same in all circuits.

Complicated tuning of ground RCs particularly with high  $dV/dt$ .

Pulse to pulse reproducibility still to be specified



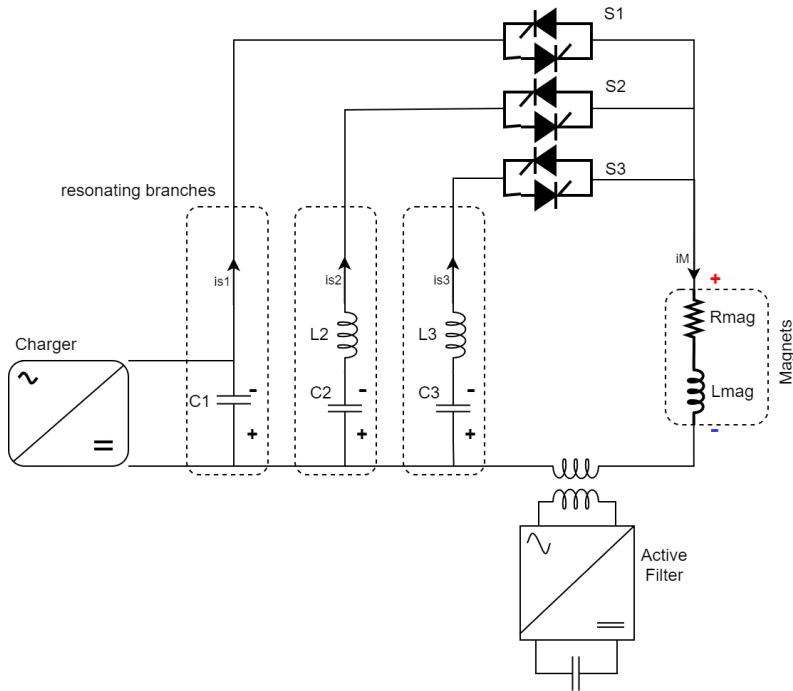
**An RCS for the muon accelerator will probably need around 200 sectors**



# Powering Schemes

Two macro concepts identified. **Both based on resonance**. Several possible realization circuits.

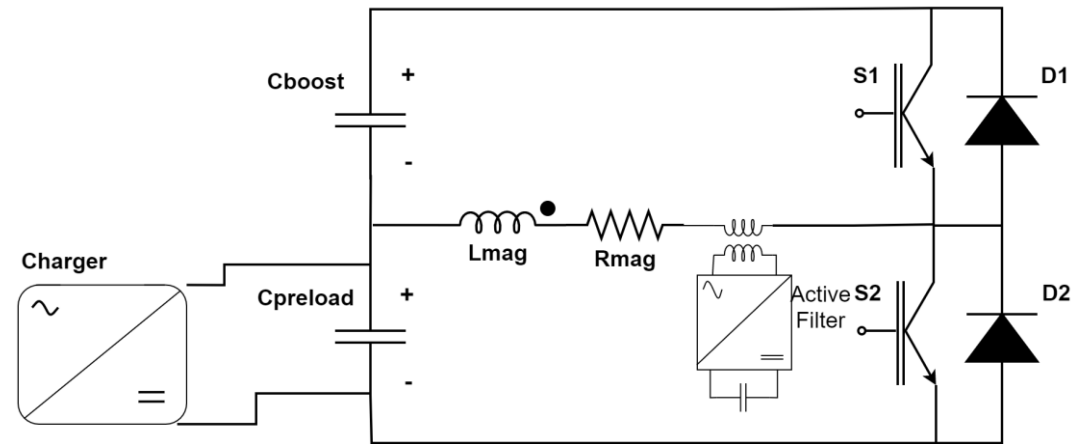
Concept 1: full wave resonance



2-3 Harmonics add to shape the current / magnetic field in the magnets.

- Multi-resonance evolves until current is zero again
- Limited flexibility to change working conditions
- Simpler power electronics

Concept 2: commutated resonance



The discharge evolves in two phases:

- Magnets are preloaded to the injection Bfield, and quickly switched onto field rapid step up.
- Increased flexibility to change working conditions
- Power electronics more complicated

# Powering scheme: magnet model for calculations

Worst case model: Highest stored energy and highest losses

Model from early work in JAI “A Design for a 3 TeV Rapid Cycling Synchrotron for Muon Acceleration in the SPS Tunnel”

[https://cds.cern.ch/record/2723310/files/JAI%20Muon\\_RCS.pdf](https://cds.cern.ch/record/2723310/files/JAI%20Muon_RCS.pdf)

Inspired to MAP Hourglass design: “Pulsed Synchrotrons for very rapid acceleration”

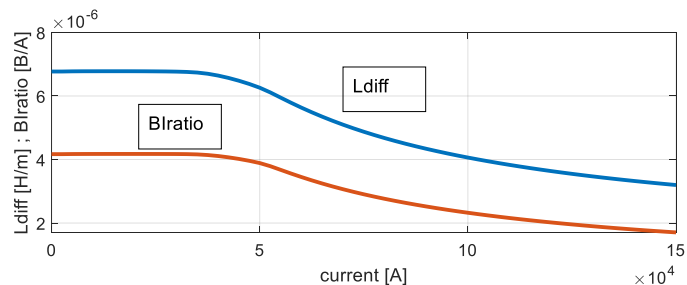
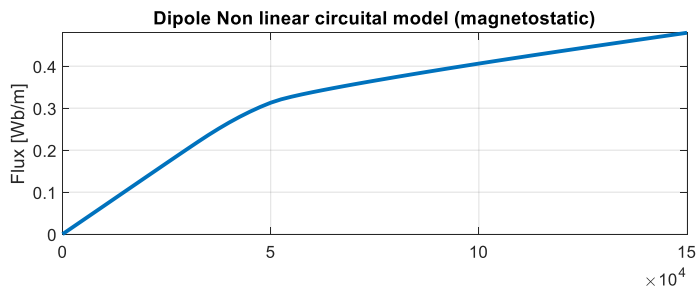
<https://doi.org/10.1063/1.4965683>

Losses values taken by the work from UNIBO “Resistive Magnet Design Studies”

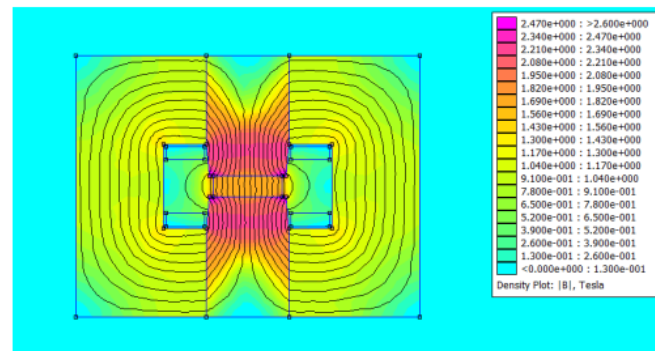
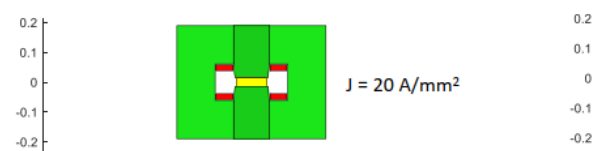
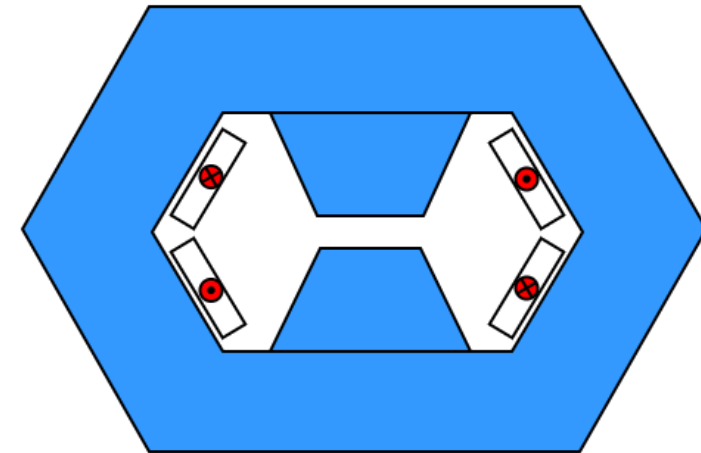
$L_{mag}$  (differential-unsaturated) = 6.6uH/m

$R_{mag}$  = 0.2mOhm/m

mmF (@1.8T) = 46 kA

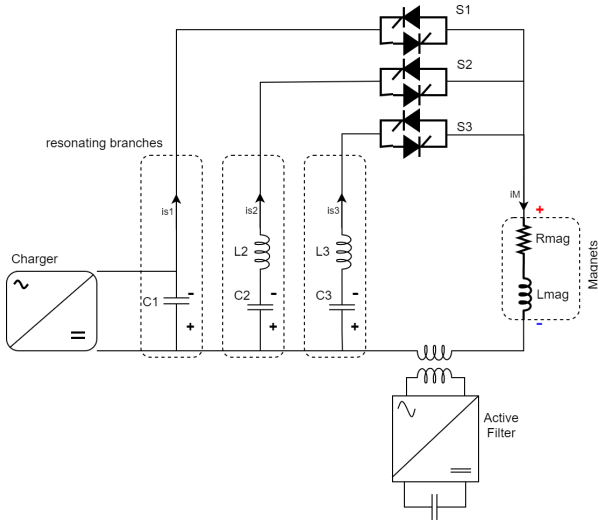


Hourglass frame magnet



# Powering Schemes: Full wave resonance analysis

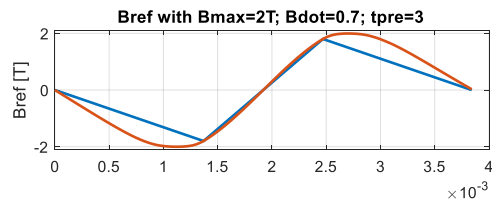
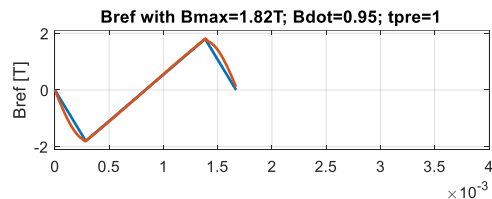
Full wave resonance: comparison of two extreme situations



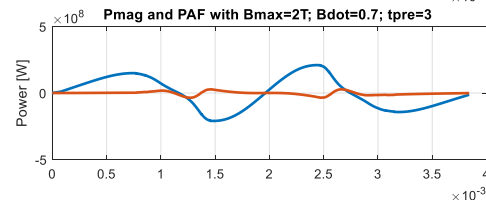
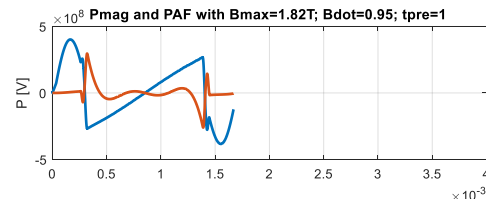
Linear (almost) Bref

“cheaper” Bref

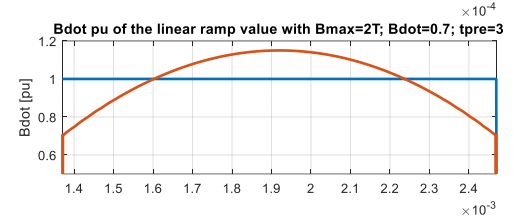
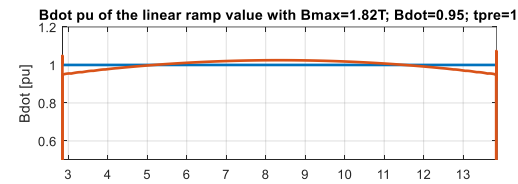
FreeOscillOptim	Global				Global			
Bmax	1.82 k				2 k			2
Bdotkappa	0.95 m				0.7 m			2
tprepostkappa	0.00015745 f				0.00207691 f			13.1912009
	RCS1	RCS2	RCS3	RCS4	RCS1	RCS2	RCS3	RCS4
<b>Nsect</b>	200	200	200	200	200	200	200	200
<b>Mag curr[kA]</b>	44	45	45	45	55	55	56	56
<b>Mag Power [MW]</b>	954	419	338	623	441	195	156	283
<b>Mag energy@extraction [kJ]</b>	114	79	137	640	114	79	136	636
<b>Mag energy@Bmax [kJ]</b>	115	80	137	640	142	99	168	776
<b>Caps NRG [kJ]</b>	308	213	366	1741	276	194	339	1723
<b>Caps volt [kV]</b>	81	36	28	48	32	15	12	25
<b>L2 NRG [kJ]</b>	97	67	115	524	55	39	76	517
<b>L2 curr [kA]</b>	29	29	29	28	22	22	23	25
<b>AF power [MW]</b>	839	358	290	680	86	38	35	87



AF helps following the “cheaper” Bref



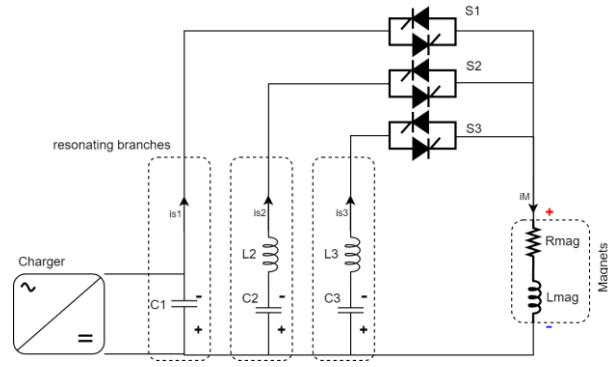
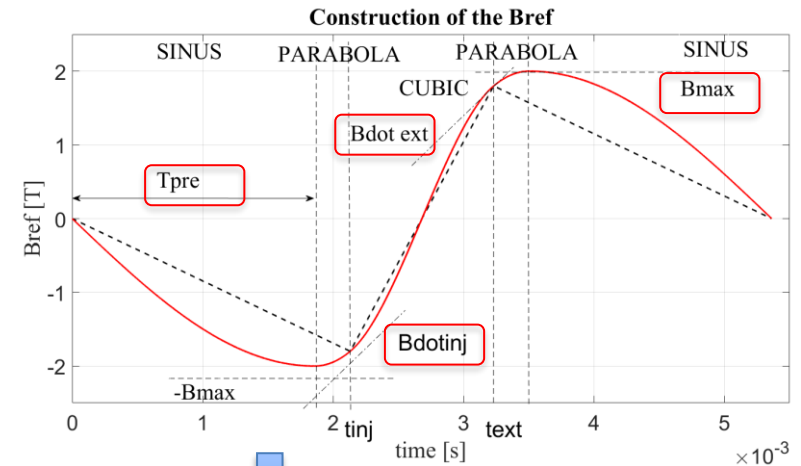
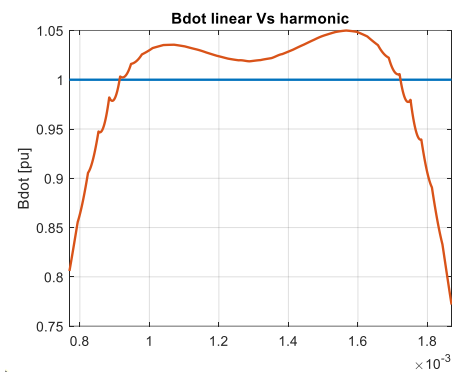
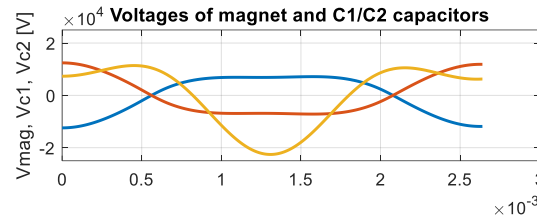
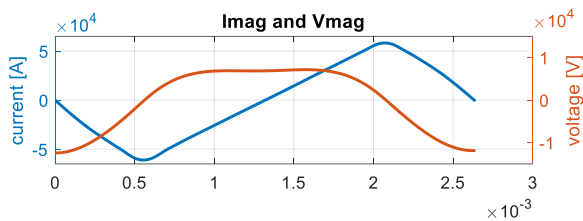
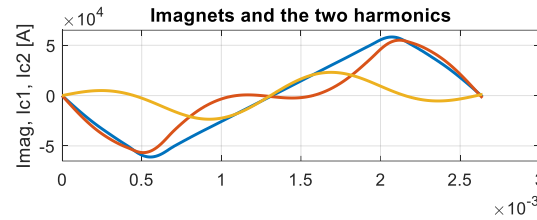
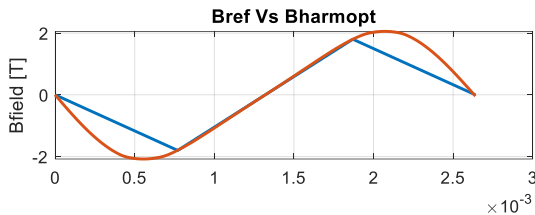
The cheaper solution comes at the cost of increased Bdot



Optimizations are possible, however in preliminary evaluations, the Active filter showed to be a very expensive element. It seems very difficult to reduce its power to an acceptable level, there it will not be considered in the following of this presentation

# Powering Schemes: full wave resonance

Each harmonics allows better approximation to the linear Bref profile. Case RCS2



$$C_1 = \frac{1}{L_{mag}\omega_f^2(1+n^2) - L_{mag}\omega_p^2}$$

$$C_2 = \frac{n^2\omega_f^4 - n^2\omega_f^2\omega_p^2 - 2\omega_p^2 + \omega_p^4}{n^2\omega_f^4 L_{mag}(n^2\omega_f^2 + \omega_f^2 - \omega_p^2)}$$

$$L_2 = \frac{2L_{mag}(n^2\omega_f^2 + \omega_f^2 - \omega_p^2)}{(\omega_f^2 - \omega_p^2)(n^2\omega_f^2 - \omega_p^2)}$$

$L_{mag}$  Magnets inductance  
 $\omega_f$  main resonating frequency  
 $\omega_p$  Pole frequency: additional dof  
 $n$  Order of the additional harmonic. Assumed  $n=2$   
 $I_{k1}$  Required current first harmonic value  
 $I_{kn}$  Required current nth harmonic value

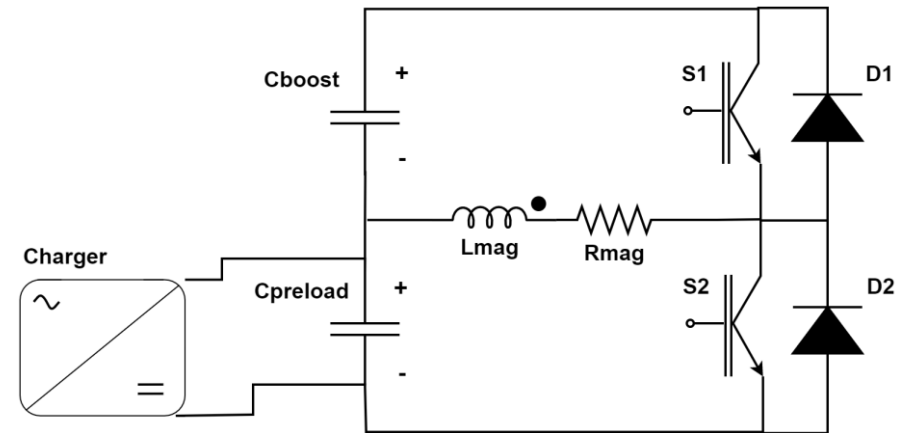
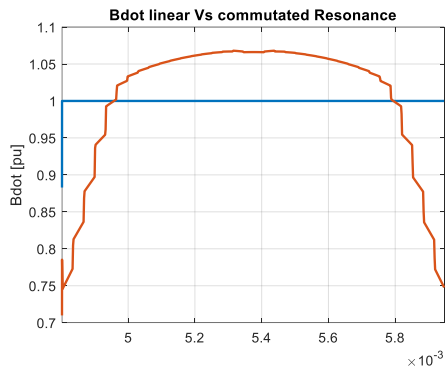
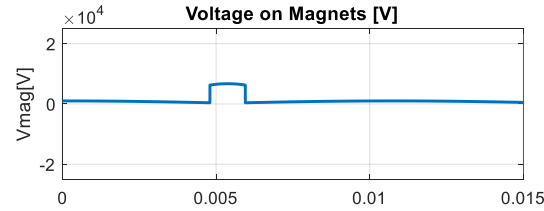
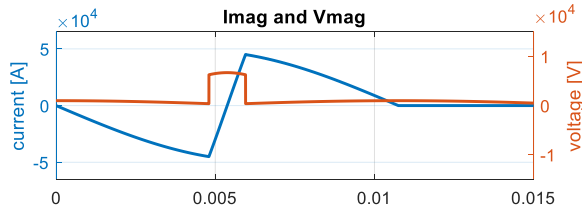
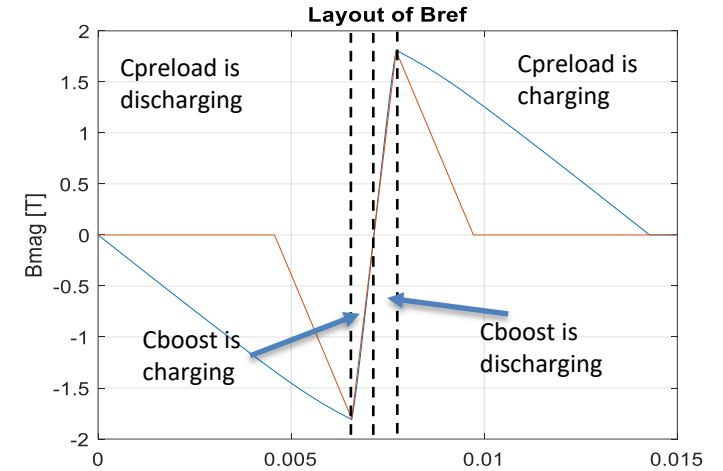
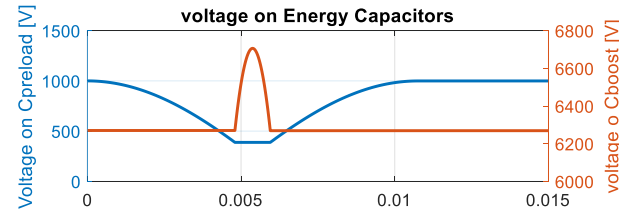
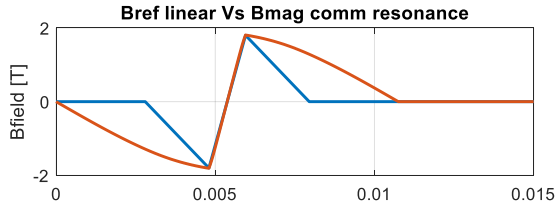
$$V_{C1}(0) = L_{mag}\omega_f(I_{k1} + I_{kn}n);$$

$$V_{C2}(0) = \frac{L_{mag}n\omega_f^3(I_{k1}(n^3\omega_f^2 - n\omega_p^2) + I_{kn}(n^2\omega_f^2 - n\omega_f^2 + \omega_f^2 - \omega_p^2))}{(\omega_f^2 - \omega_p^2)(n^2\omega_f^2 - \omega_p^2)}$$

Resonating parameters are very interlinked. Uncertainties in the circuit parameters cannot be corrected. Additional bulky hardware is required.



# Powering Schemes: commutated resonance



Simpler resonance principle. Voltages of Cboost and Cpreload can be used for regulation (pulse to pulse).

# Powering Schemes: comparison

Full wave resonance	RCS2
C1 capacitor bank (per sector)	130 [kJ]
C1 peak positive and negative voltage	+12.5 -7.2 [kV]
C2 capacitor bank (per sector)	90 [kJ]
C2 peak positive and negative voltage	+11.4 -22.6 [kV]
L2 inductor bank (per sector)	45 [kJ]
<b>Total installed energy (RCS2)</b>	<b>53 [MJ]</b>
Total magnet energy @ extraction (RCS2)	17 [MJ]
Total magnet energy @ peak (RCS2)	22 [MJ]
RMS current in the magnet (RCS2)	4.2 [kA]
Magnet losses x m	3.6 [kW/m]
PK current in the magnet (RCS2)	58 [kA]
Field derivative [pu]	1.06

Commutated resonance	RCS2
Cpreload capacitor bank (per sector)	100 [kJ]
Cpreload peak positive and negative voltage	+1 +0.4 [kV]
Cboost capacitor bank (per sector)	670 [kJ]
Cboost peak positive and negative voltage	+6.9 +6.0 [kV]
L2 inductor bank (per sector)	0 [kJ]
<b>Total installed energy (RCS2)</b>	<b>150 [MJ]</b>
Total magnet energy @ extraction (RCS2)	17 [MJ]
Total magnet energy @ peak (RCS2)	17 [MJ]
RMS current in the magnet (RCS2)	6.6 [kA] (*)
Magnet losses x m	8.7 [kW/m] (*)
PK current in the magnet (RCS2)	45 [kA]
Field derivative [pu]	1.06

- The capacitors have double polarity excitation and are very high voltage. Much less energy density.
- Inductors for second harmonic are bulky and costly elements.
- The peak current can be high in order to be more linear. High saturation.
- The rms current in the magnet is close to the minimum possible.
- The power electronics is the simplest possible (thyristors)

- The installed capacitor energy is ~ 4 times that of the full wave resonance, but there is no voltage polarity reversal, therefore the quantity of material will probably be the same or lower and so the cost.
- No additional inductors are required.
- Peak current is smaller. No or limited saturation
- The rms current is considerably higher than the full wave resonance. (\*)
- The power electronics is more complex.

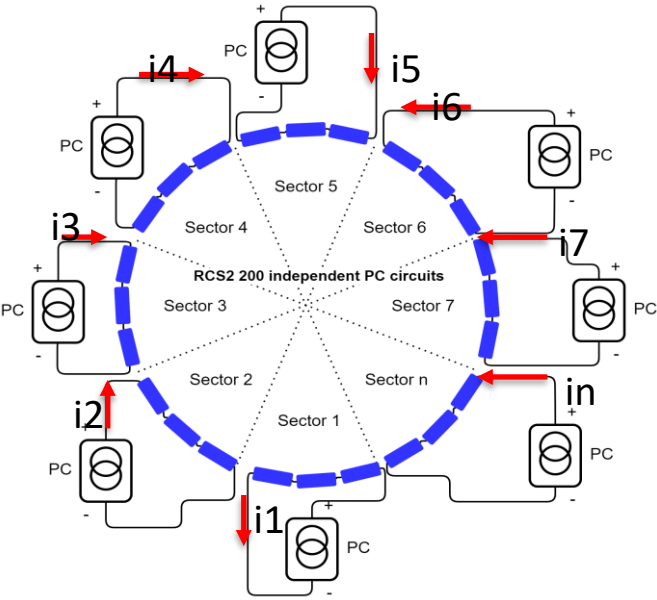
(\*) Can be decreased if Higher preload voltage is considered.

As a reference, the PS accelerator (@CERN) has about 4.8kW/m of losses

# The control problem description

## Independent sectors:

How small must the **tracking error** among sectors be?



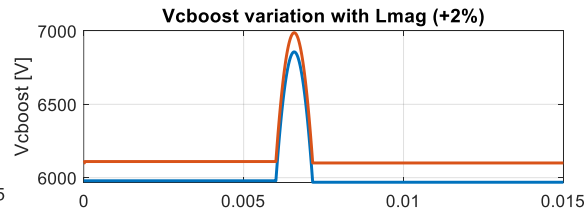
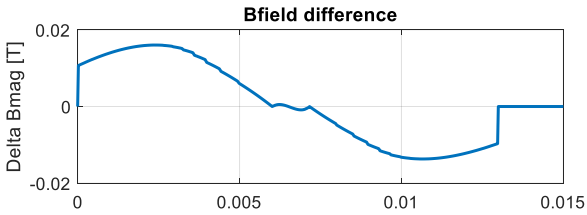
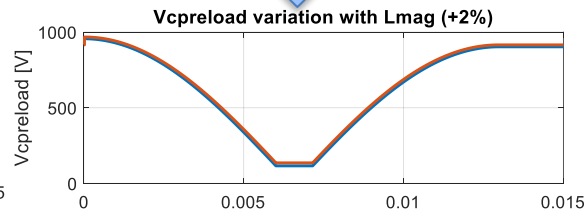
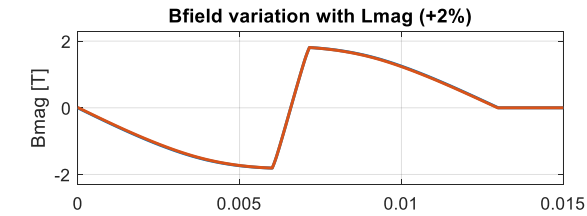
## Control performance requirements

During acceleration  
 😞 Very hard as acceleration is quick

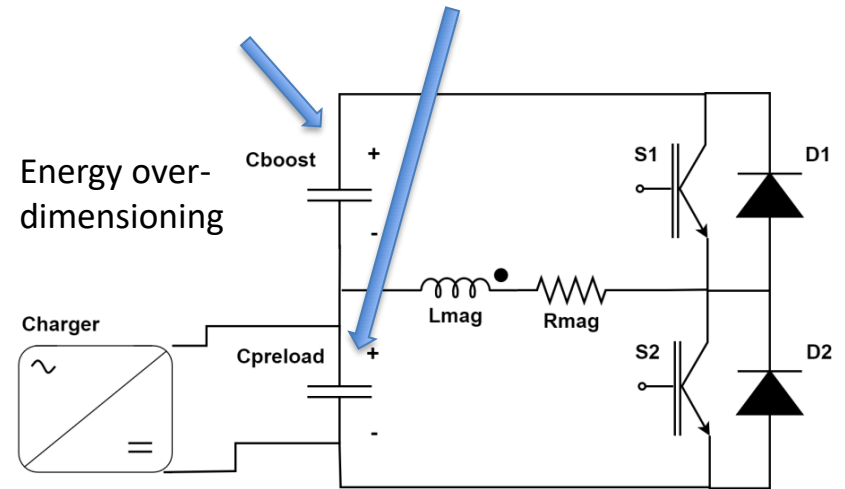
From pulse to pulse  
 🤔 With a good model of the system we can recover the error in each sector

It means there can be pulses where the tracking error among sectors is out of the limits but then a sort of "Iterative Learning Control" recovers the error.

Cpreload and Cboost voltage adjusted



Energy over-dimensioning



# Technologies: Capacitors

## Ageing Factors: self healing

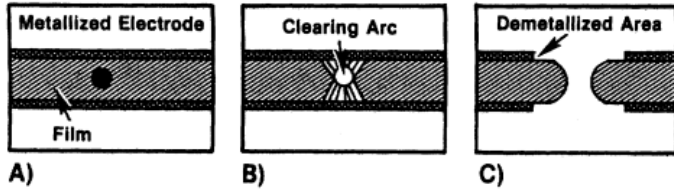
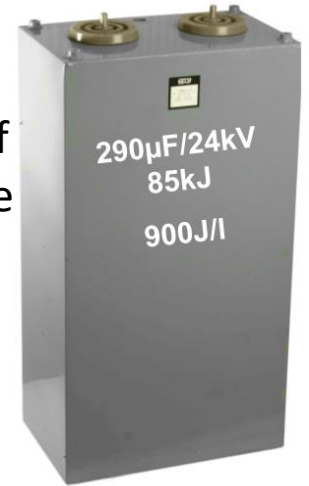


Fig. 2: Schematic diagram of the clearing sequence.  
 A) Metallized film with a defect. B) Voltage applied between electrodes causes breakdown at the defect site and high fault current flows and C) heat from fault current vaporizes electrode and isolates the defect site.

Polypropylene metallized film capacitors are capable to **self heal**. Self heal comes with a loss of capacitance and it is therefore an ageing factor. The lower the Electric field, the lower the self-healing loss of C.

It is accepted to have short circuits in the design. Ex LMJ capacitors experience a large number of self healings but it's OK because they only have to make 25'000 pulses in their lifetime.



First discussions with supplier:

Comparing the application to POPS (CERN Main Power Converter for PS)

Full wave resonance  $NRG_{DensityMUco} = NRG_{DensityMUco} \cdot \left[ \frac{E_{fullWave}}{E_{POPS}} \right]^2 = 274 J/l \cdot \left[ \frac{65 V/\mu m}{250 V/\mu m} \right]^2 = 274 J/l \cdot \frac{1}{15}$

Commutated resonance  $NRG_{DensityMUco} = NRG_{DensityMUco} \cdot \left[ \frac{E_{comm}}{E_{POPS}} \right]^2 = 274 J/l \cdot \left[ \frac{250 V/\mu m}{250 V/\mu m} \right]^2 = 274 J/l$



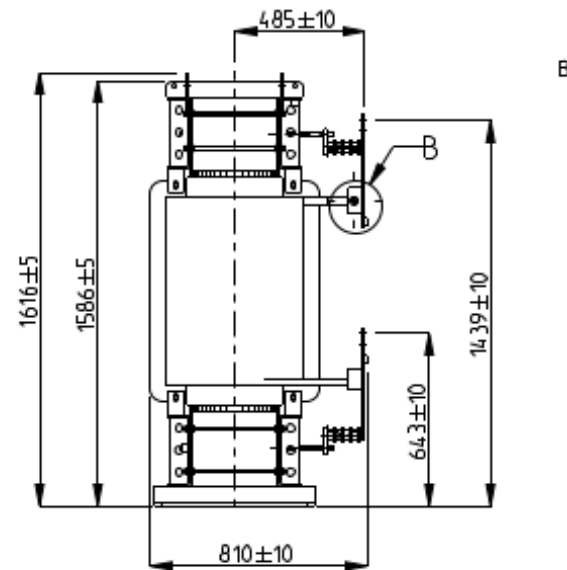
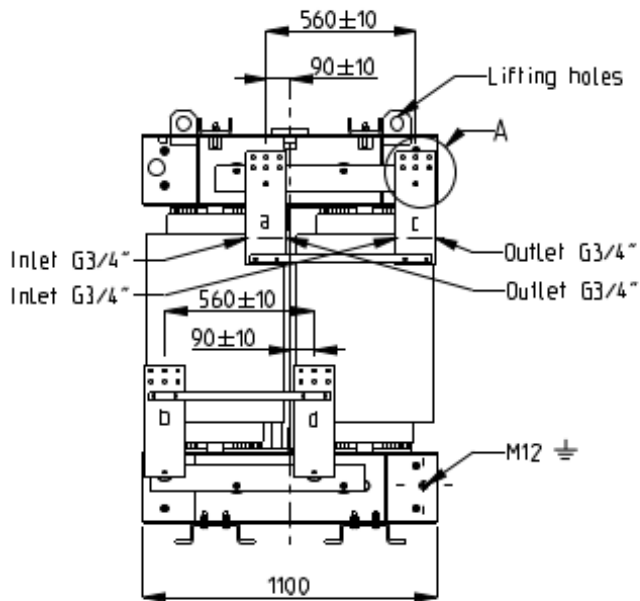
POPS container 12mx2.5mx2.5m; 26tons; 0.5MCHF;  
 Full wave resonance → 0.22MJ  
 Commutated resonance → 3.3MJ

# Technologies: Inductors

Still to be analysed but for the order of magnitude:

POPS AC inductor:

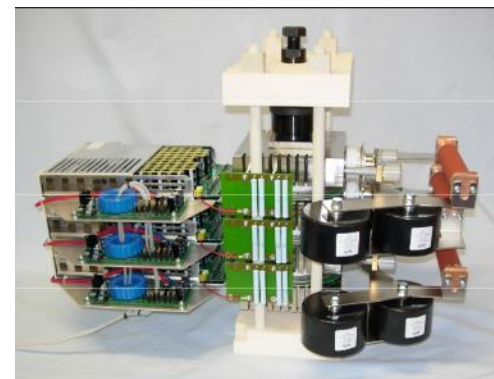
- Energy 18 kJ
- Current 6kA
- Weight 3 tonnes
- Cost 40 kEur



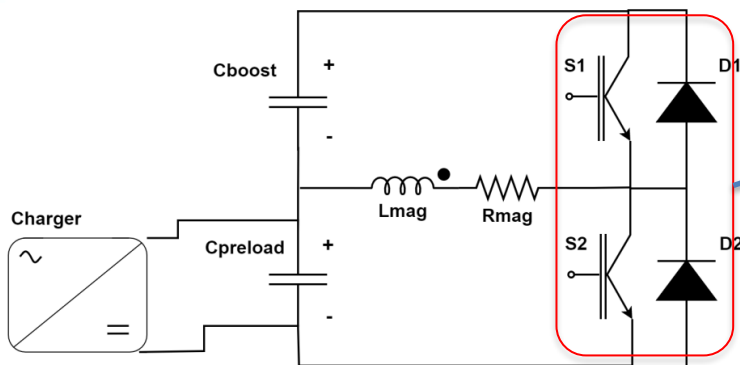
# Technologies: Thyristors and IGBTs/IGCTs

IGCT

Voltage: up to 6kV  
 Turn-on/off current: up to 6kA  
 Several series/parallel required

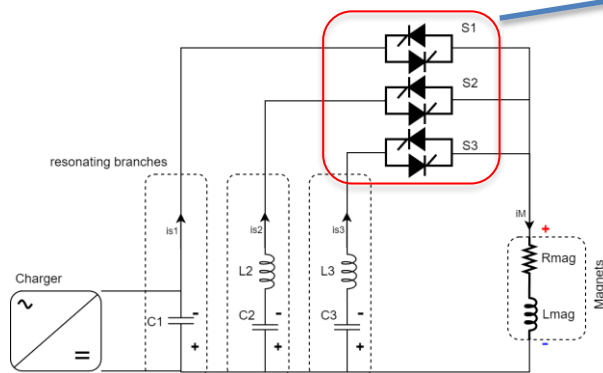


IGBT

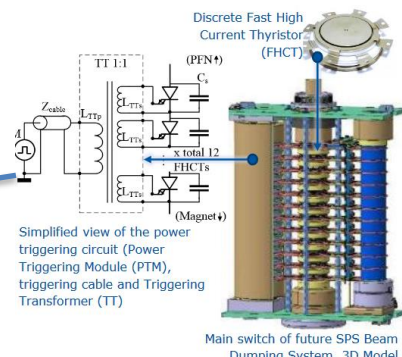


50 kA turn off current;  
 10 kV blocking voltage;  
 6 kA rms current;  
 100A/us di/dt;

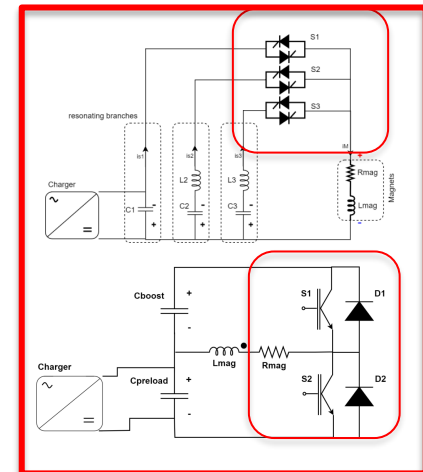
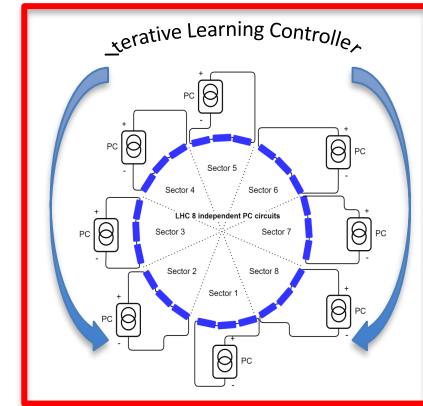
Pulsed power thyristors  
 To be completed



50 kA peak current;  
 20 kV blocking voltage;  
 100A/us di/dt  
 Several series/parallel required



# Working plan

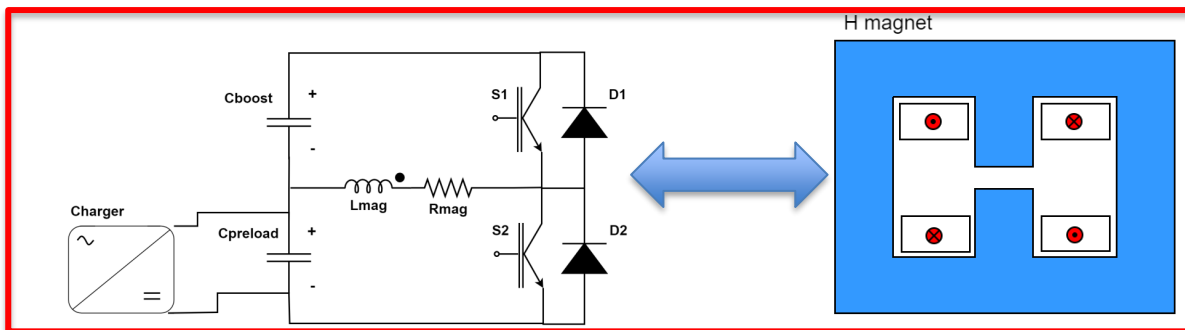


- 1) Circuitual studies of a reduced scale model to prove the possibility of controlling the field in pulse-to-pulse mode
- 2) Identification of circuitual parameters variation: Magnet, Capacitors, IGBT jitter etc...

3) Design rules of the power electronics elements

4) Design rules of the capacitors and inductors

5) Coupled Power converter – magnet optimization with cost estimation



# Conclusions

- The extremely high peak power requires division into several sector. These can be connected either in series or be independent;
- Two resonance mode powering schemes have been presented. The commutated resonance is potentially more flexible but requires a more complicated power electronics development. R&D will be required for it;
- The different resonating scheme have an impact on the design of the energy storage elements;
- Tracking control accuracy very difficult to achieve → pulse to pulse control → **Input required: control accuracy;**
- Design rules for the main components of the powering system needs to be checked with suppliers;
- Eventually an optimization of the powering scheme Vs the magnet design must be performed to find lowest cost solution.