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Muon Collider Magnet Moving For Neutrino Mitigation

C. Accettura, F. Bertinelli, A. Kolehmainen, T. Rätty

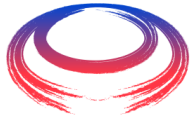
With several inputs of C. Carli, P. Borges de Sousa, L. Bottura, S. Fabbri, K. Skoufaris

IMCC Annual Meeting

21/06/2023, IJCLab (Orsay, France)

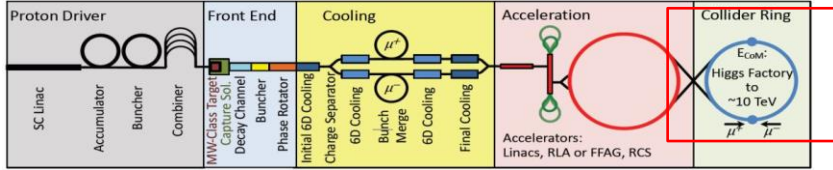
Outline

- Introduction and motivations
- Assumptions
- Magnet alignment and lay-out change jack system – Solution 1
- Combined jack – Solution 2
- Tunnel space
- He supply
- Changing magnet lay-out
- Conclusions

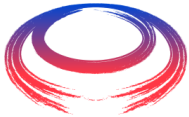


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Collider ring neutrino radiation mitigation

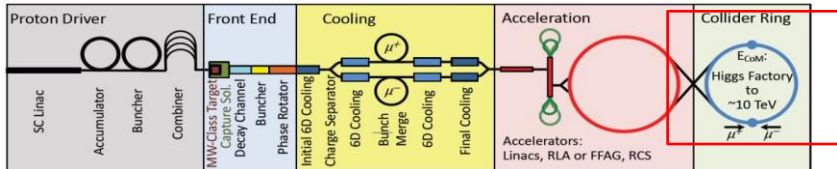


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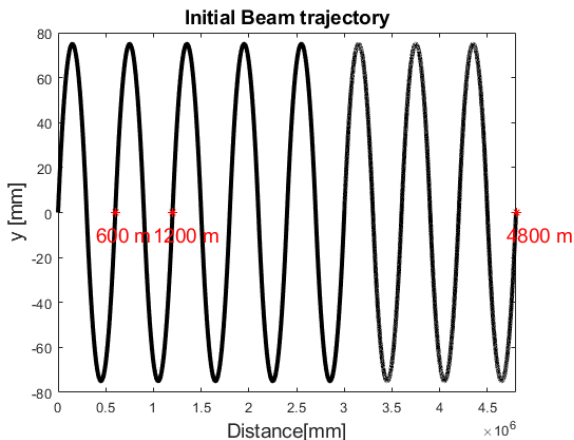


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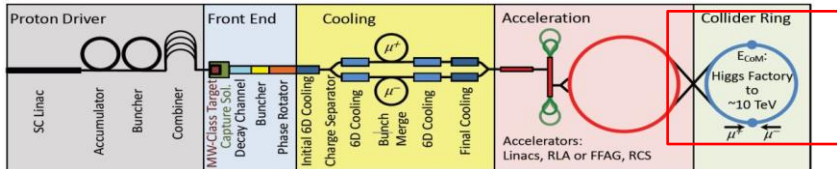
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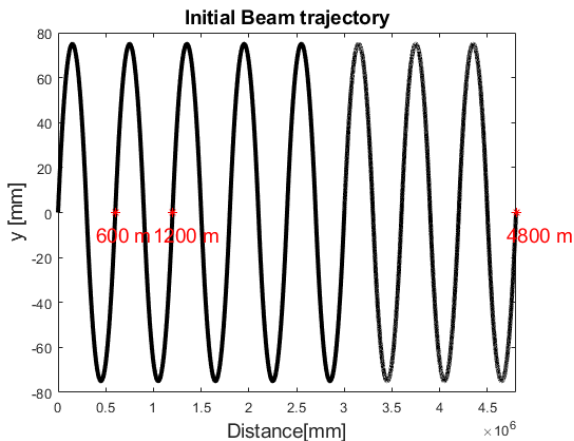
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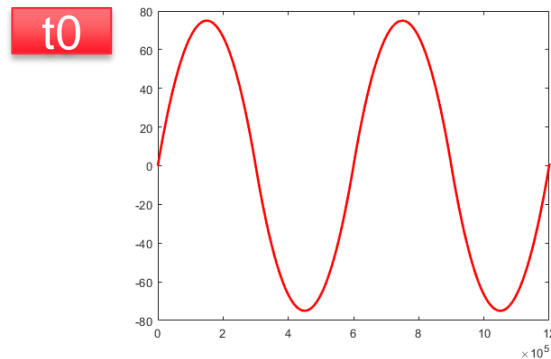
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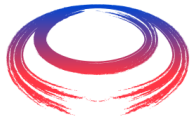


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- Successive beam trajectory obtained by rigid translation of the parabola (10 μrad → 400 steps)

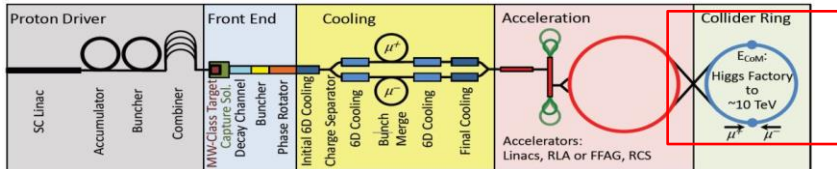
- Period=600m → max. displacement ±150mm





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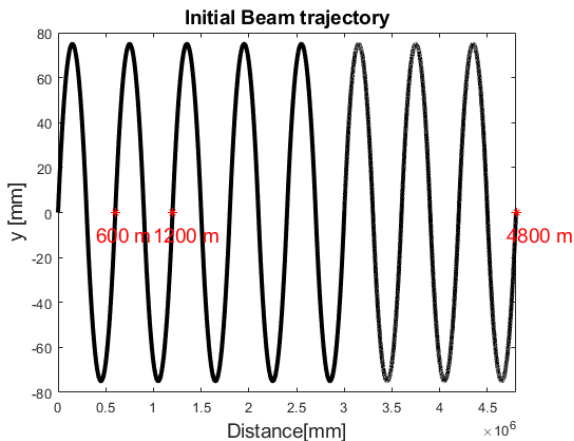
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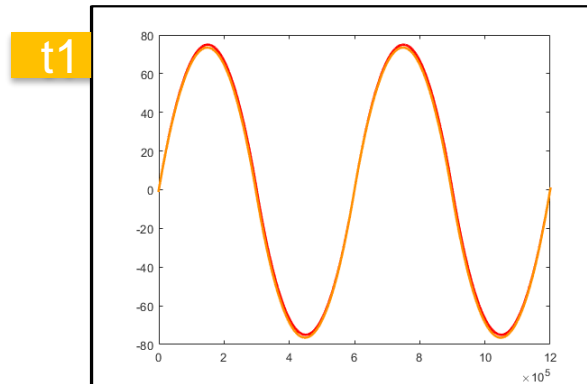
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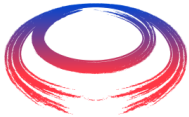


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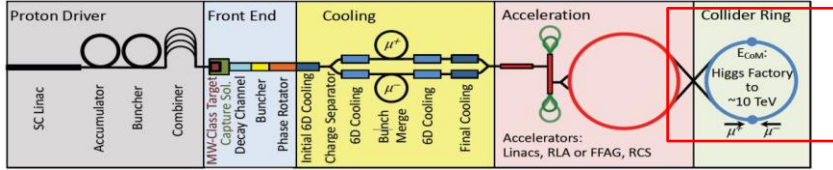
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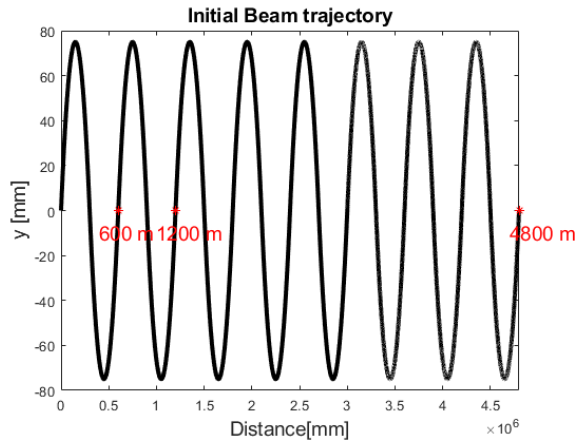
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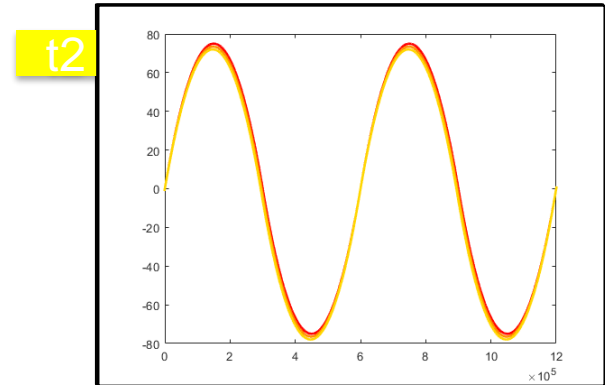
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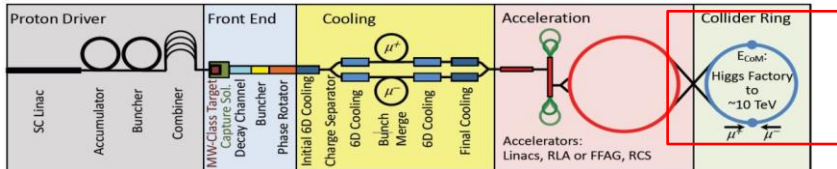
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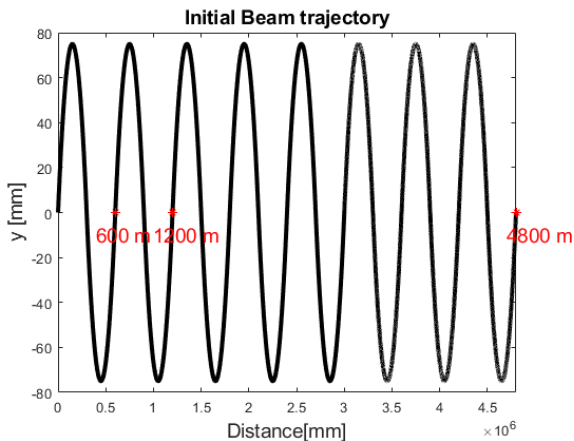


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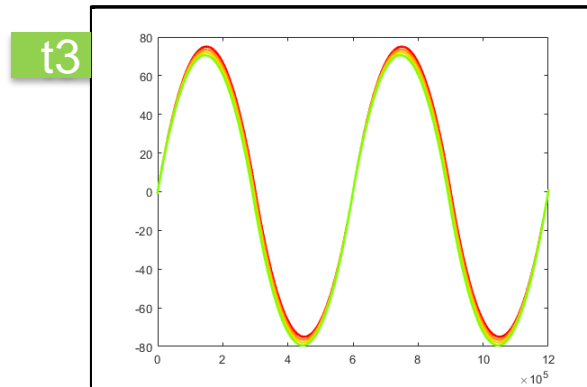
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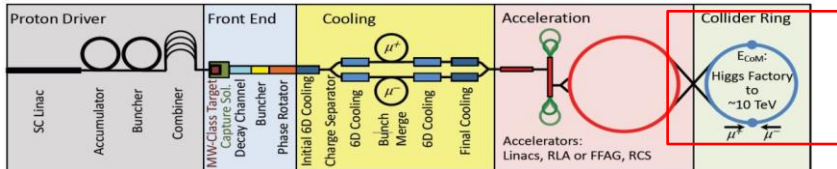
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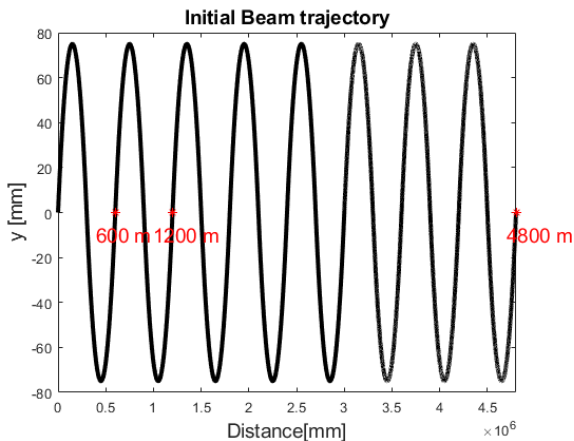
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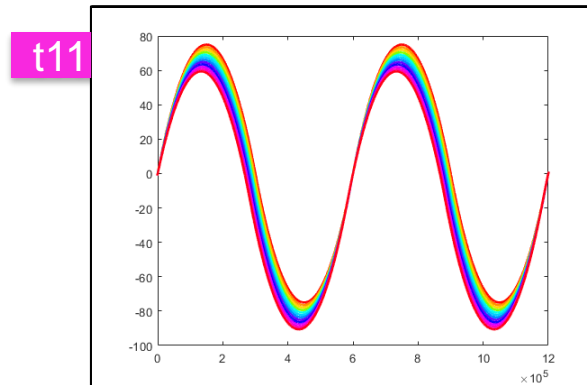
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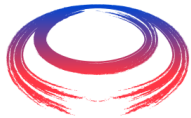


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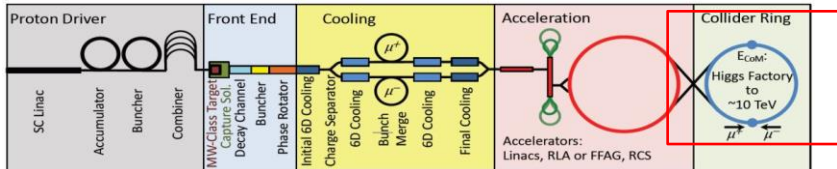
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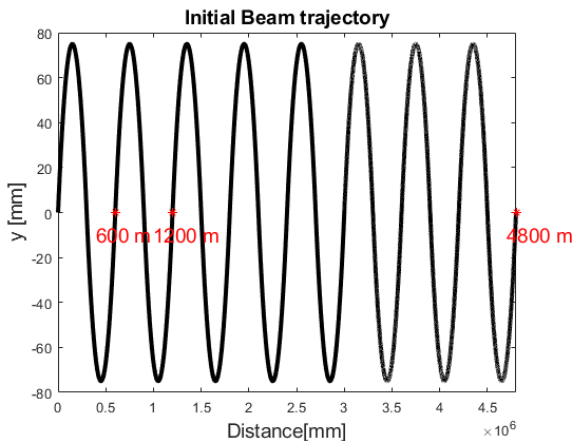
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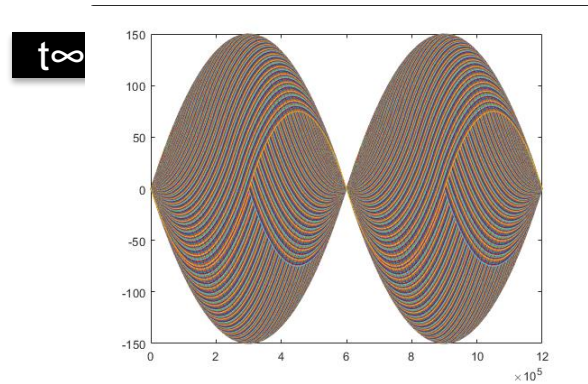
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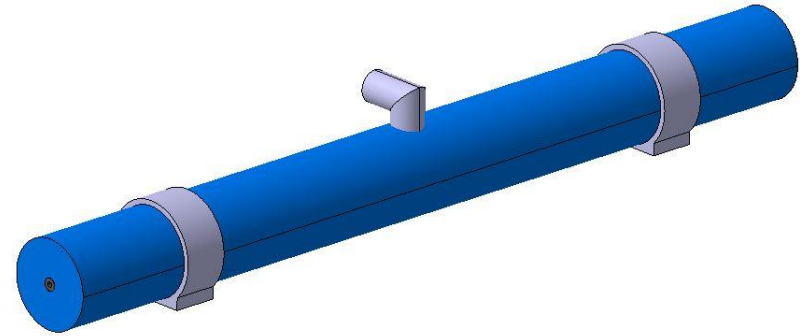


Assumptions

- AIM: understand the *mechanical feasibility* of the moving magnets system.

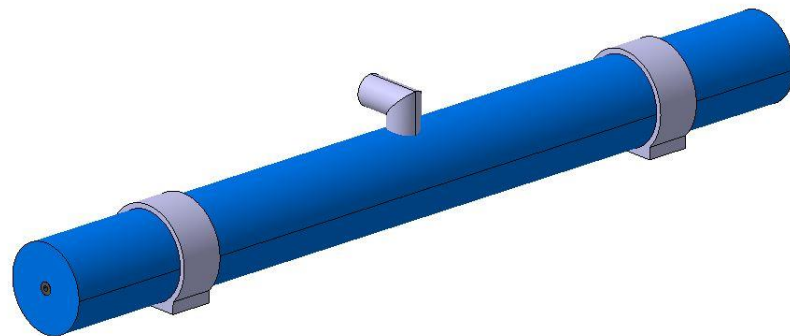
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- **DIPOLE MAGNET MODEL**
 - Inspired by LHC magnets
 - $L = 10\text{ m}$, $D = 1\text{ m}$
 - Mass: 24.5 T approximately (based on LHC D2 magnet and W-shield model)
 - Length of interconnection = 500 - 800 mm (coldmass – coldmass)
 - Cold bore $\varnothing 50\text{ mm}$
 - Three jack supporting
 - Radiation similar to LHC – See talk of Claudia Ahdida for details!



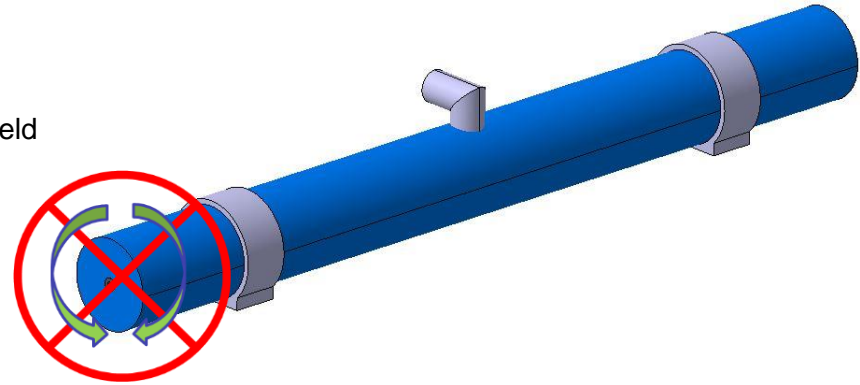
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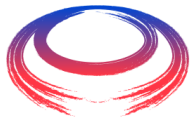
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 - On dipole only from gravity (LHC tunnel angle of 1.4%) and alignment jack tilt



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- **LATERAL FORCES:**
 - On dipole only from gravity (LHC tunnel angle of 1.4%) and alignment jack tilt
- **MOTORIZED MAGNET MOVEMENT:**
 - Only vertical movements have been studied
 - Horizontal field (for vertical kick) not given by magnet tilting (i.e. Correctors are needed)





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Overview of proposed solutions



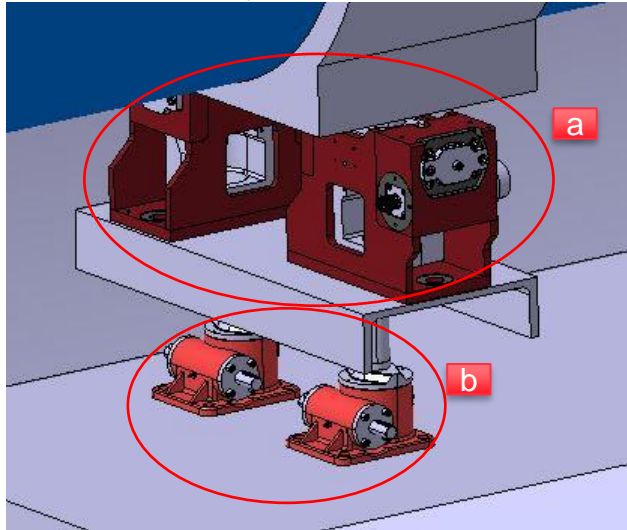
▪ Solution 1: TWO JACKING SYSTEMS

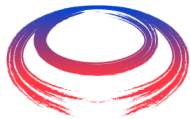
a. ALIGNMENT JACKS

- Magnet alignment
- HL-LHC Jack

b. MOTORIZED JACKS

- Only vertical movement
- Commercial jack





Overview of proposed solutions



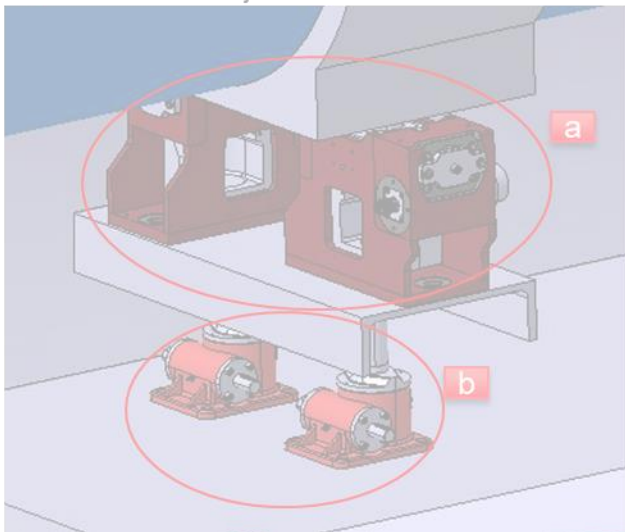
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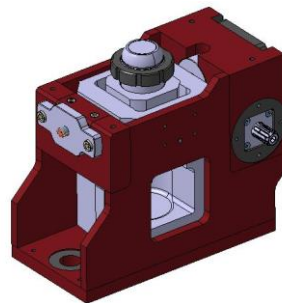


▪ Solution 2: COMBINED JACK

- Combine the functions of the two jacks – alignment and lay-out change
- Muon Collider specification requires a new design – concept work initiated with a jack supplier

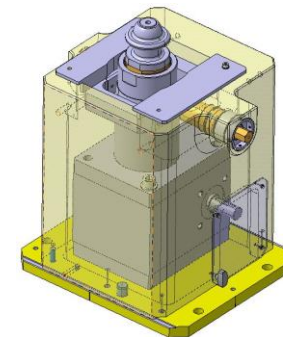
HL-LHC JACK

- Max load 17 T
- Vertical stroke ± 20 mm

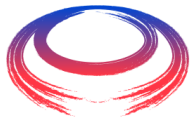


L4 JACK – inspired by LHC jack

- Max load 5 T
- Vertical stroke ± 15 mm
- Commercial wormgear jack

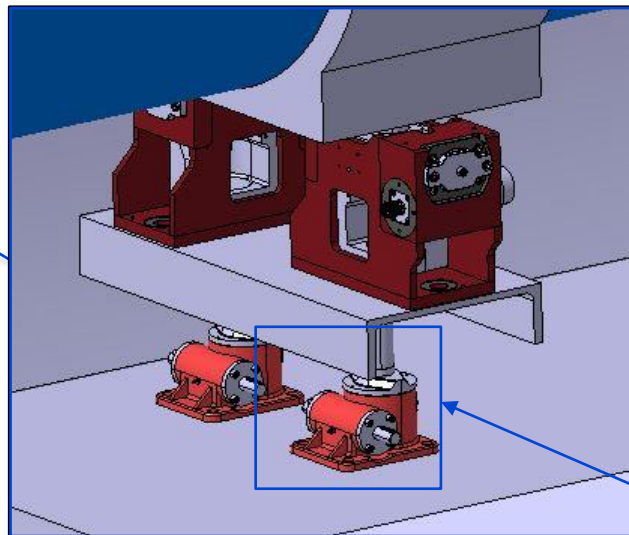
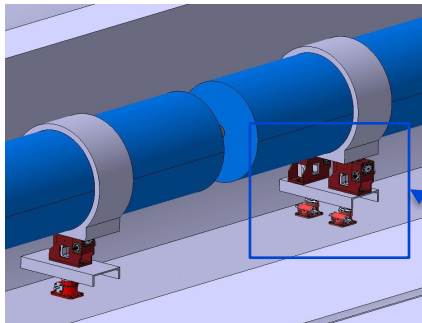


Both require three jacks together to create an isostatic support system!



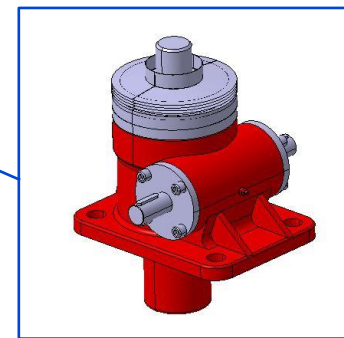
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Two jacking systems – solution 1



COMMERCIAL JACK

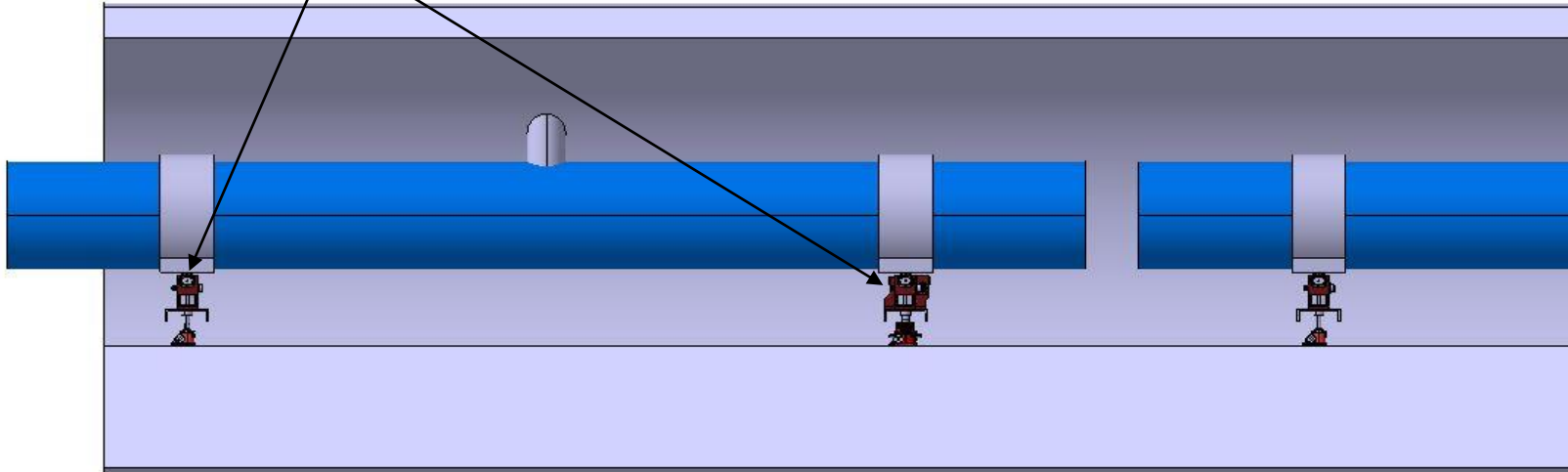
- Precision: ± 0.5 mm
- Mechanically driven
- Self-locking mechanism



Challenges: Alignment and lay-out change

ALIGNMENT JACKS

- Magnet alignment



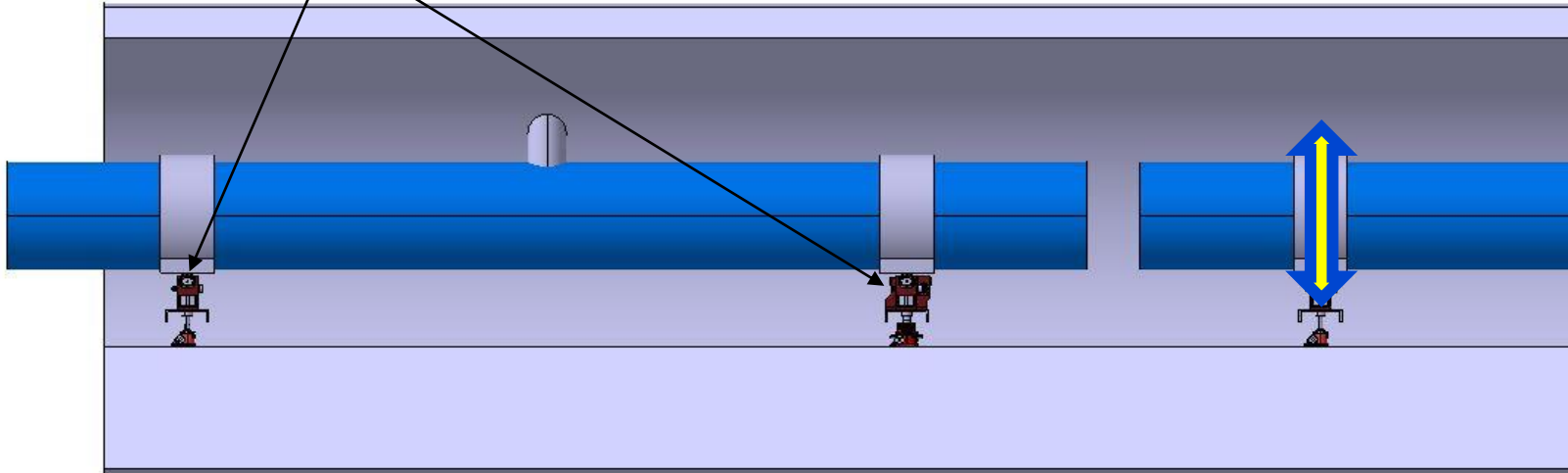
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ALIGNMENT JACKS

- Magnet alignment

MOTORIZED JACKS

- Vertical movement ± 50 mm



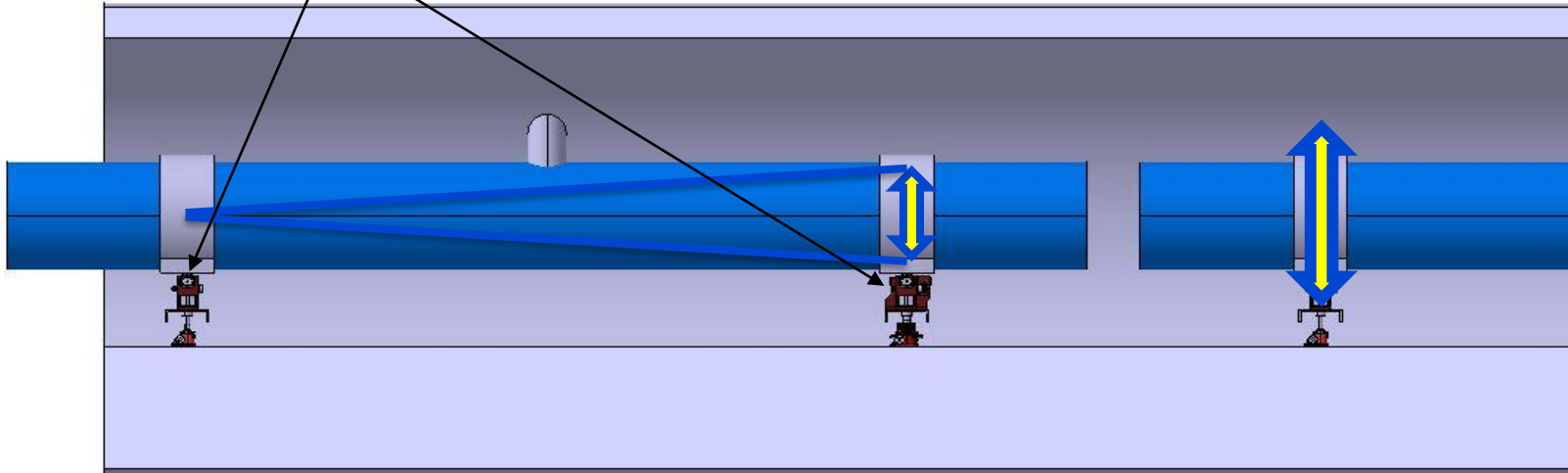
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ALIGNMENT JACKS

- Magnet alignment

MOTORIZED JACKS

- Vertical movement ± 50 mm
- Magnet tilt
- Parasitic movements in the alignment jack ($< 3\mu\text{m}$)



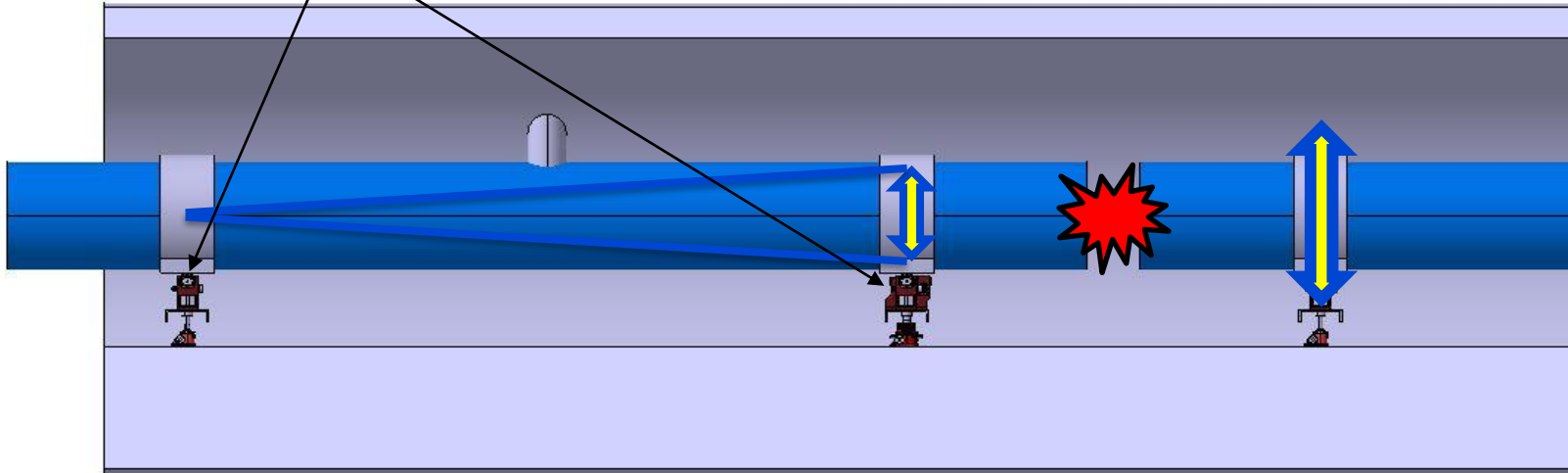
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ALIGNMENT JACKS

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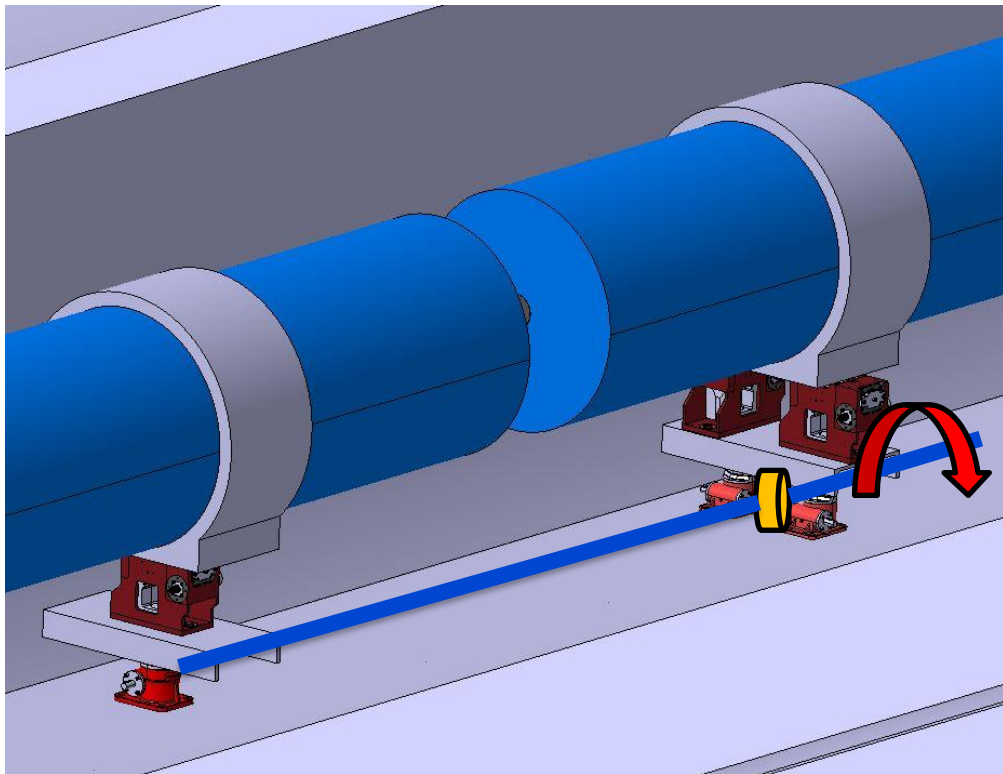
MOTORIZED JACKS

- Vertical movement ± 50 mm
- Magnet tilt
- Parasitic movements in the alignment jack ($< 3\mu\text{m}$)



Maximum stroke in opposite direction over the interconnection will destroy the bellows!
SAFE OPERATION SHALL NOT RELY ON THE CONTROL SYSTEM!

Two jacking systems – solution 1a



- **PARALLEL OPERATION OF JACKS ACROSS THE INTERCONNECTION**
 - Connect jacks mechanically
 - 4-way gearbox
 - Shafts
 - Single motor on the gearbox
 - IN STUDY – redundant system with two motors, requires two gearboxes
- **BELLOWS OFFSET BLOCKED**
- **ANGLE BETWEEN MAGNETS ALLOWED**

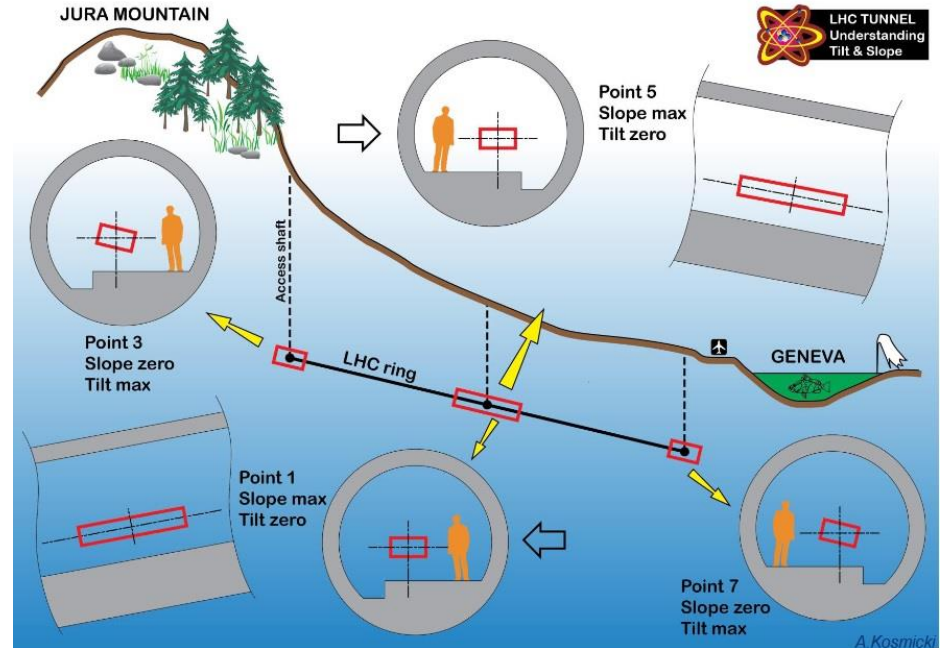


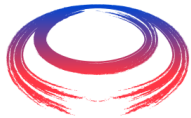
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Supporting of motorized jacks



- **BENDING MOMENT ON THE MOTORIZED JACK**
 - From magnet tilt or roll due to the tunnel

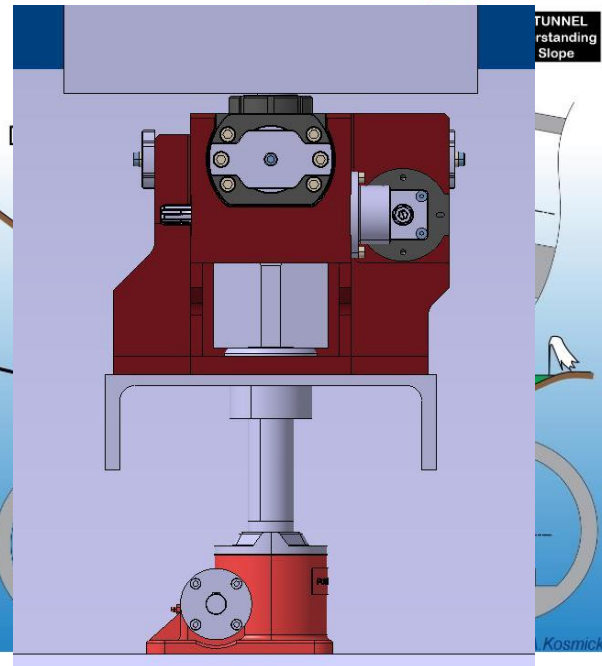
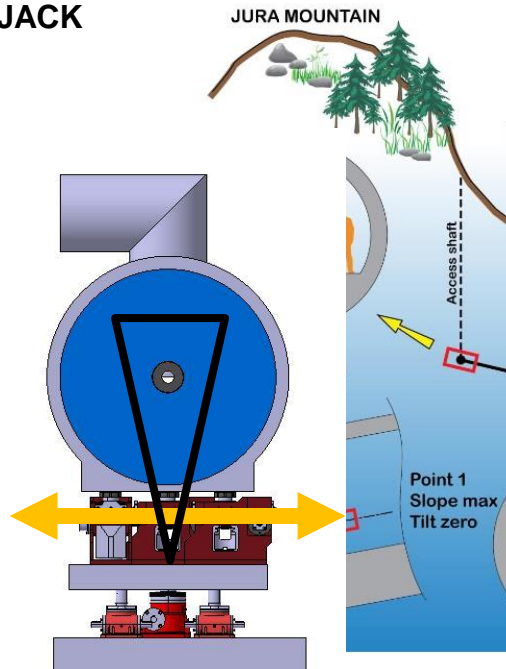
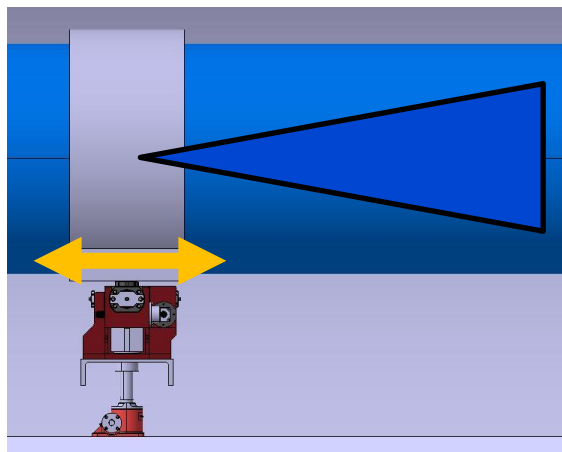




Supporting of motorized jacks



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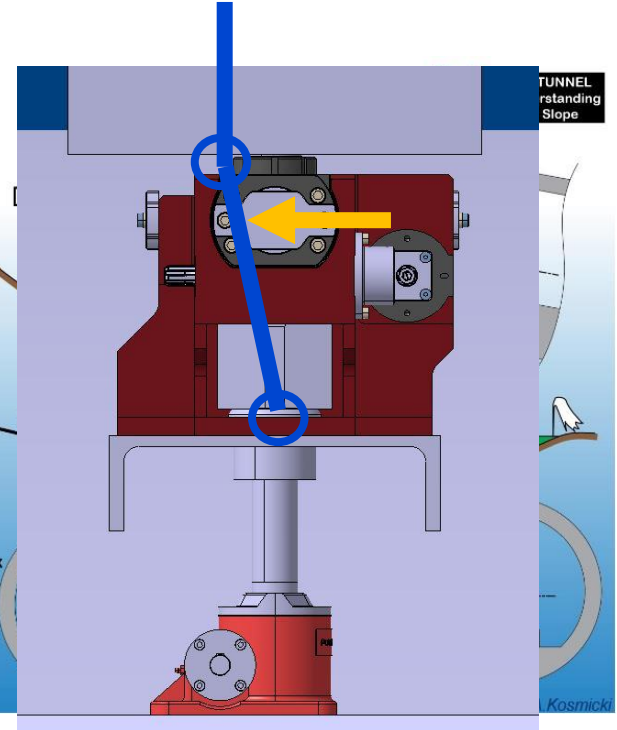
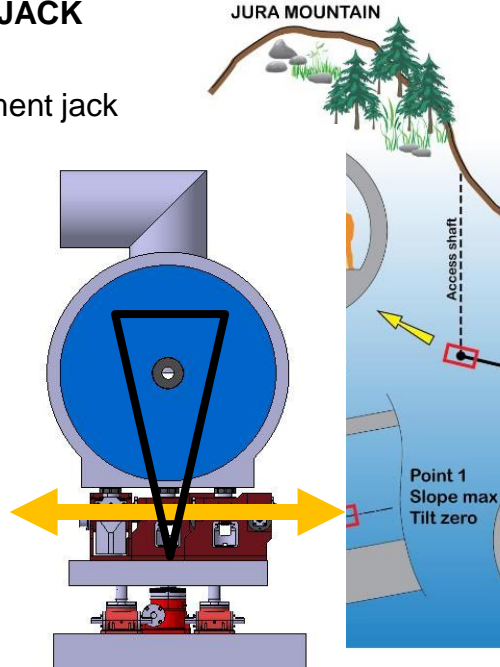
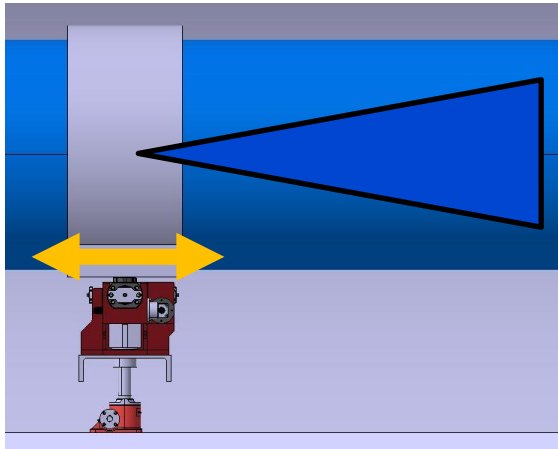




Supporting of motorized jacks



- **BENDING MOMENT ON THE MOTORIZED JACK**
 - From magnet tilt or roll due to the tunnel
 - From maximum lateral stroke of the alignment jack



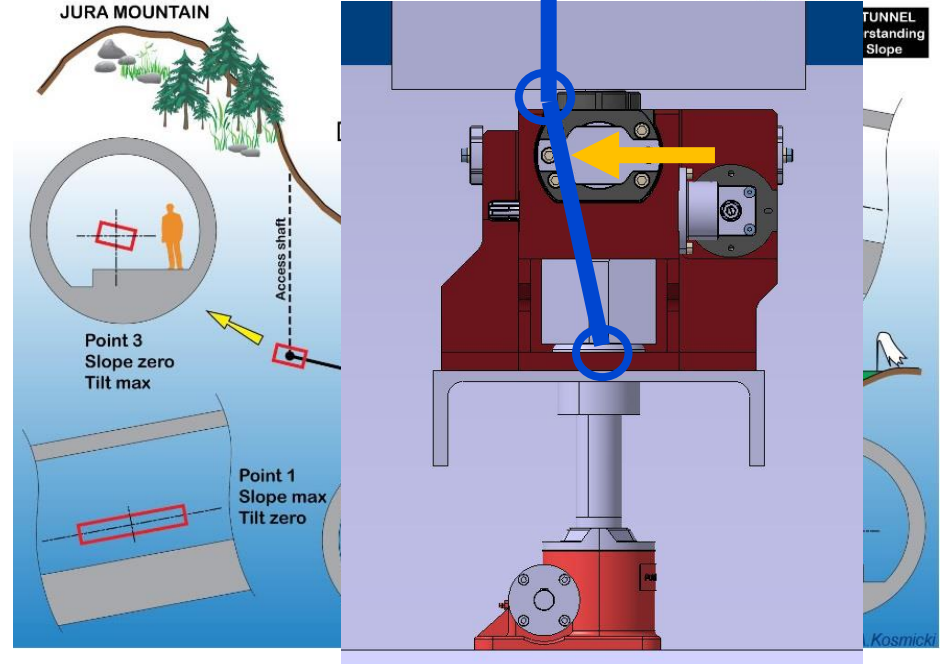


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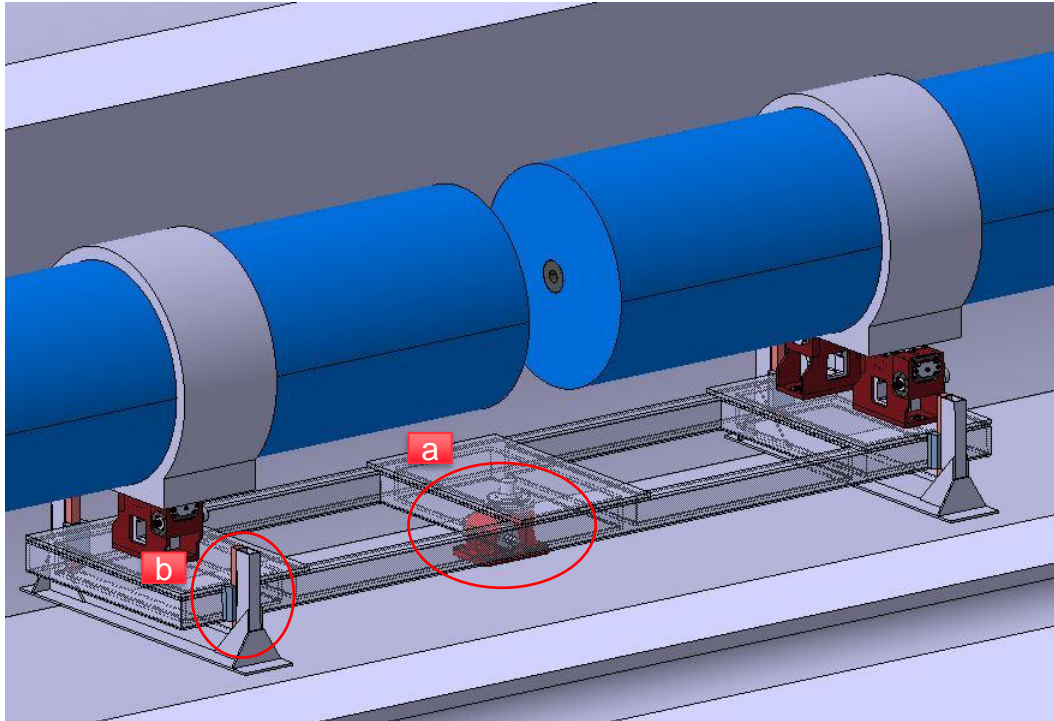
Supporting of motorized jacks



- **BENDING MOMENT ON THE MOTORIZED JACK**
 - From magnet tilt or roll due to the tunnel
 - From maximum lateral stroke of the alignment jack
 - To be calculated for different motorized jack options
 - Compare with allowed moments for the motorized jacks
 - Higher the stroke – higher the moment
 - **Motorized jacks may need supporting guides to protect them from bending moments!**



Two jacking systems – solution 1b

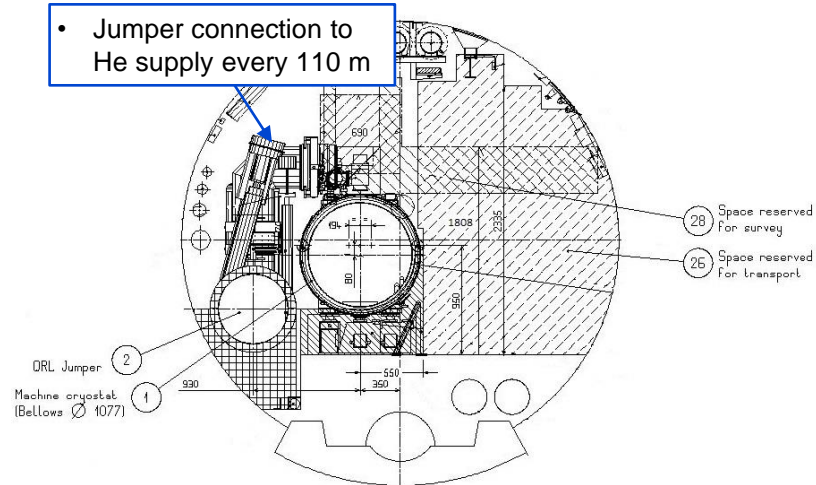


- **ALIGNMENT JACKS ACROSS THE INTERCONNECTION ON COMMON PLATFORM**
 - a. One central jack for the height change
 - b. Platform must have linear guides to avoid bending moment on the jack
 - One motor per interconnection = magnet
 - Motor for redundancy required?
- **Bellows offset blocked**
- **Angle between magnets allowed**

He supply

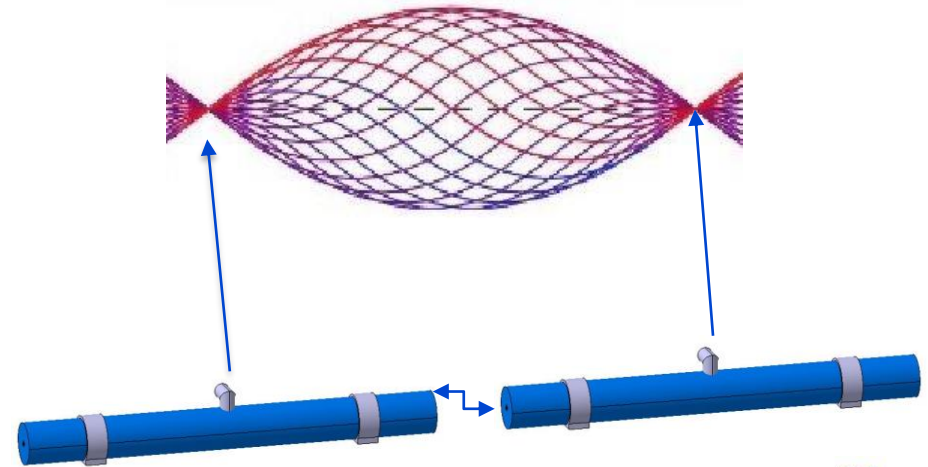
▪ LHC TUNNEL

- Jumper connection to He supply every 110 m



▪ MUON COLLIDER TUNNEL

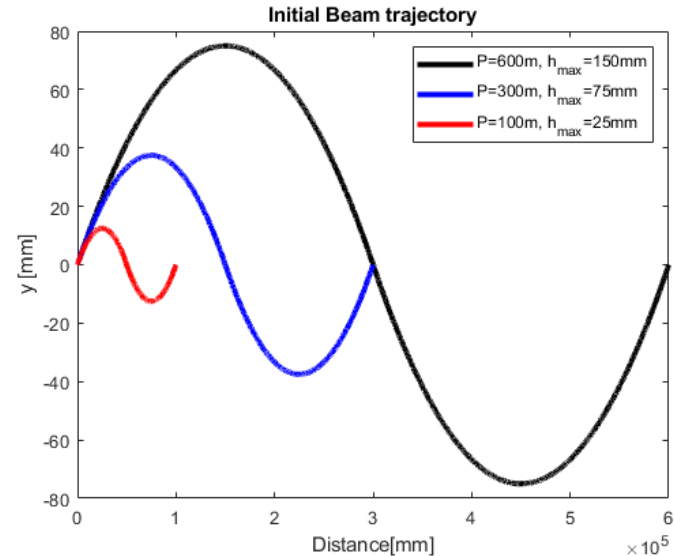
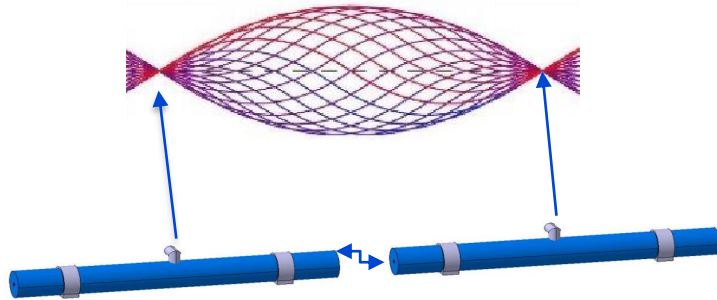
- Must be placed around the period node points – current jumper designs do not allow the vertical movement of the collider dipoles w.r.t rigid cryogenic supply installation



He supply

■ MUON COLLIDER TUNNEL

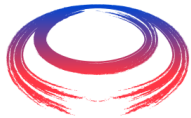
- First estimation: He supply at the ~LHC distance \rightarrow ~100m
- Reduction of period
- Reduction of maximum vertical displacement \rightarrow ± 25 mm
- Stronger vertical kick (horizontal field)



- **200 days of physics annually leads to 400 trajectory changes → 20 years 8000 changes**
- **Power_{total} = N_{magnets} X N_{jacks} X Power_{motor} ,if 10 m dipoles and 0.8 m interconnection > 800 magnets**

- **With 1 kW motor around 1 MW for parallel operation of jacks**
- Control system for movement and monitoring
- Reliable push-button lay-out change!
- Do we need to confirm measurements with external system?

- **Assume change propagated in smaller groups**
- Max number of motors to be defined
- Assume: group of 50 motors -> around 20 groups to move
- 3 minutes per group leads to one hour

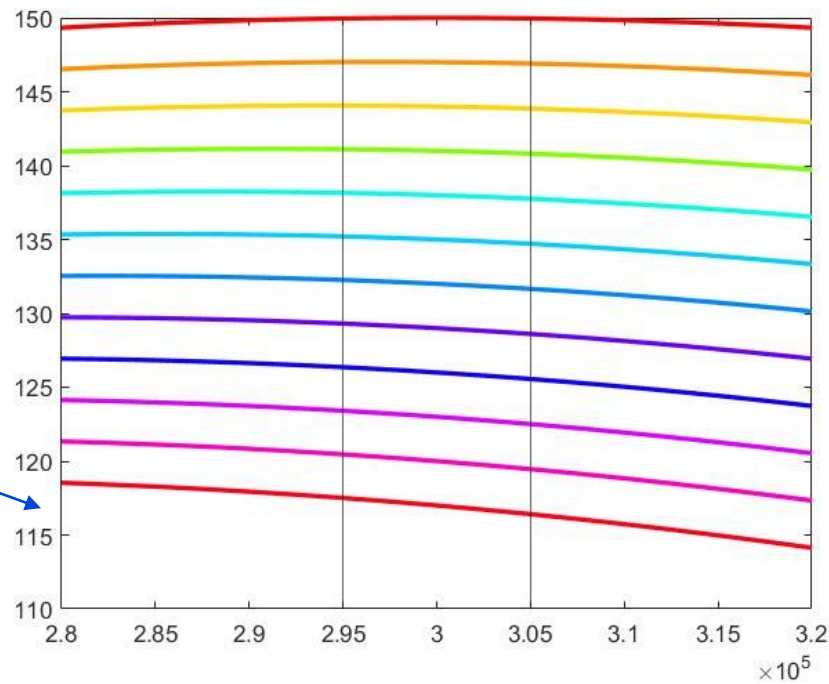
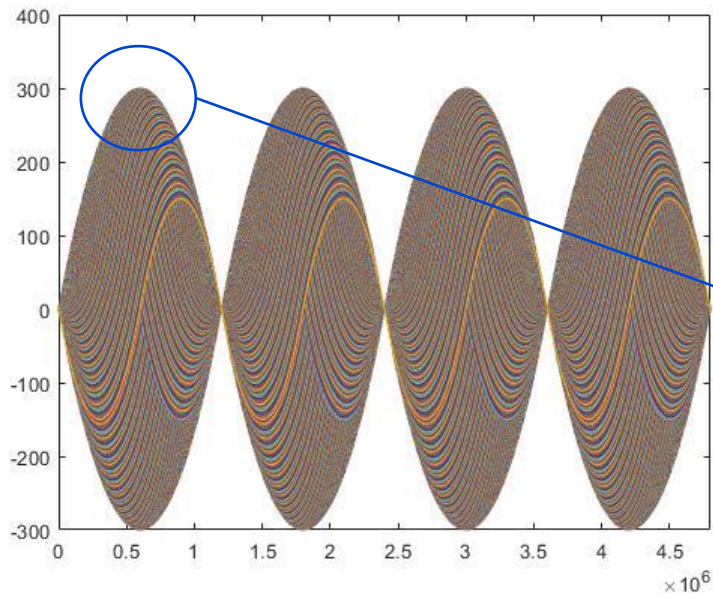


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Beam trajectories vs. Magnet movements



- **MAGNET APERTURE:**
- Can we accommodate several trajectories into one magnet?

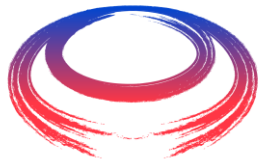


Conclusions

- **In order to mitigate the neutrino radiation, the possibility of having moving magnet around the collider ring has been studied**
- **So far, no showstopper have been individuated, however open points to be clarified**
- ± 25 mm seems ok for cryogenic and for jack mechanics \rightarrow is it acceptable? Increase of factor 6 in the horizontal magnetic field (~ 0.67 T)
- Two solutions to move the magnets presented \rightarrow is the precision enough (~ 0.1 mm)?
- Can we extend this approach to all the muon collider arc magnets?

Next step

- **Concept selection and design engineering**
- **Two-magnets mock up-What do we need?**
 - 6 LHC jacks
 - 2 dipoles (2 LEP dipole magnets + additional weight? LHC dipoles? Resistive magnets?)

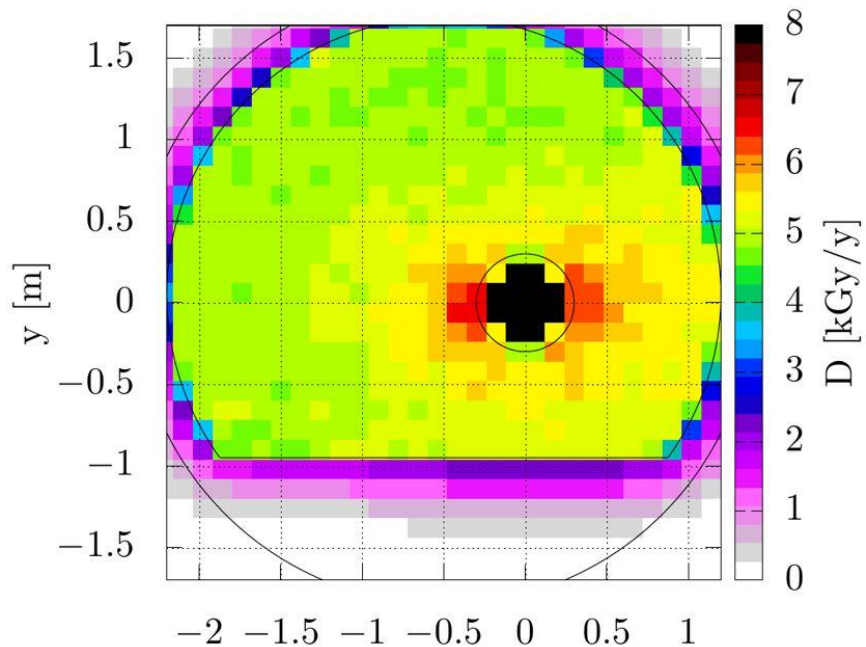


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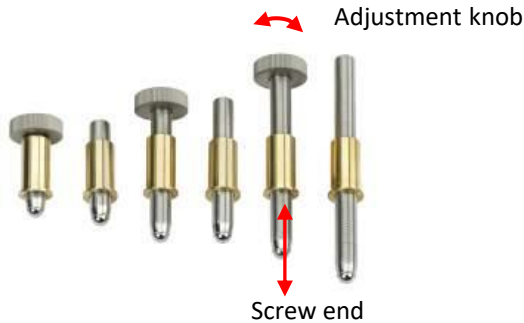
***Thank you
for your attention!
Your questions please?***

Yearly dose projection, 200 days of operation



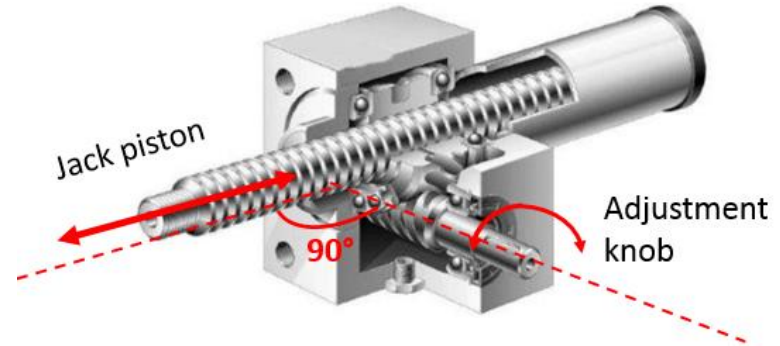
Courtesy of Daniele Calzolari

Real impact of play in adjustment jigs (screw mechanisms, jacks) on adjustment performance



• Simple screw adjustment

- Play (seen on *screw end*) depends on quality of the thread machining
 - For typical machined threads (M x, Tr x, etc ...) – play at *screw end* can vary from tenths um-s to even mm for bigger screws
 - For ball screws play depends on fitting quality – it is much lower than for ‘standard’ threads (typically 0 .. 20 um)
- Angular backlash ‘seen’ on adjustment knob is proportional to screw pitch



• More complex mechanisms (e.g. power jack)

Play (seen on *jack piston end*) depends on quality of the *Jack piston* thread machining, and is relevant as in simple screw mechanisms. Backlash seen on *Adjustment knob* is much bigger and depends on *Jack piston* thread play and worm mechanism play.

Real impact of play in adjustment jigs (screw mechanisms, jacks) on adjustment performance

- For mechanisms using adjustment screws, the preloading of screws/thread pair plays big role to get best adjustment performance
 - For pre-loaded 'classical' screws, the resolution (minimum motion) and precision (repeatability of position) of adjustment is typically in range of $\sim 5..50\mu\text{m}$ (this is e.g. classical configuration for vertical screws, supporting the load of adjusted components; for radial adjustment pre-loading springs are useful, to suppress screw play)
 - Pre loading of 'classical' screws can give resolution/precision parameters which are satisfactory and even comparable with ball screws in some cases
 - For non-pre-loaded screws, the adjustment resolution can be still $\sim 5..50\mu\text{m}$ (in single motion direction), but precision of adjustment will be defined by play on screw/thread

Use of closed-feedback-loop position control

Adding of position sensor, motorization and closed control loop to adjustment mechanisms allows to minimize the play effects in mechanisms – the controller follows the position measured by sensor
The control system components and mechanics shall be designed/chosen in a way to fulfil also the other system requirements (stiffness, 3D play in supporting system, safety, etc..)

