

International
UON Collider
Collaboration

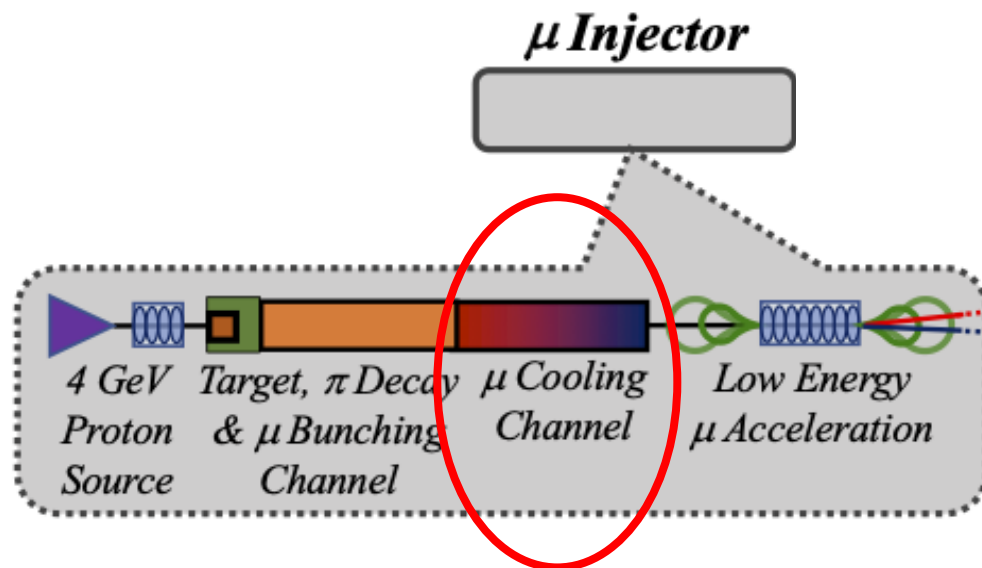


Prospects of Cryo-Cu and HTS high gradient RF cavities

Sergio Calatroni – CERN
With contributions from many Collaborators

Motivation

- Muon cooling system requires RF cavities operating at **high-gradient AND in a strong magnetic field.**



- Normal conducting copper, possibly cryo: [see next talks](#)
- Superconducting: High-Temperature Superconductors (HTS) ?

- HTS cavities in a strong magnetic field
- HTS cavities at high-gradient
- HTS cavities in both strong field and high-gradient
- Future steps

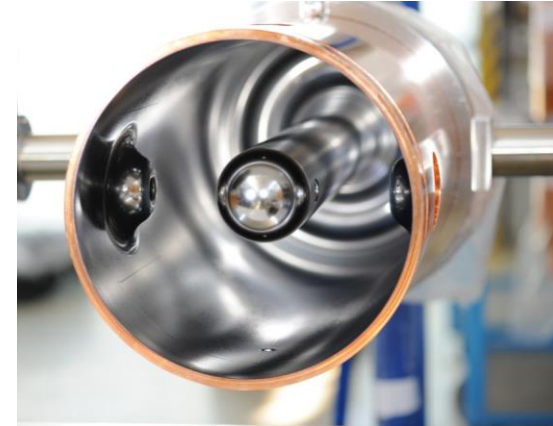
- HTS cavities in a strong magnetic field
- HTS cavities at high-gradient
- HTS cavities in both strong field and high-gradient
- Future steps

Reference case

- Typical SRF accelerator cavities are made of niobium



Strong magnetic shielding needed



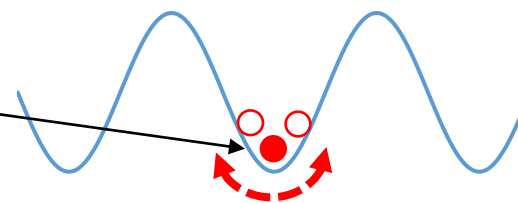
Limited or no magnetic shielding

- Effect of **external magnetic field** on SRF accelerating cavities is mostly due to **flux pinning**, weak pinning in bulk Nb and strong in Nb/Cu
- **Niobium** critical field $H_{c2} < 1$ T, superconductivity is lost at higher fields

Some theory background: fluxon motion in RF

The motion of the **rigid** fluxon lattice behaves as a **harmonic damped oscillator** (neglecting thermal creep)

$$m\ddot{x} + \eta\dot{x} + kx = J_{rf}\phi_0$$



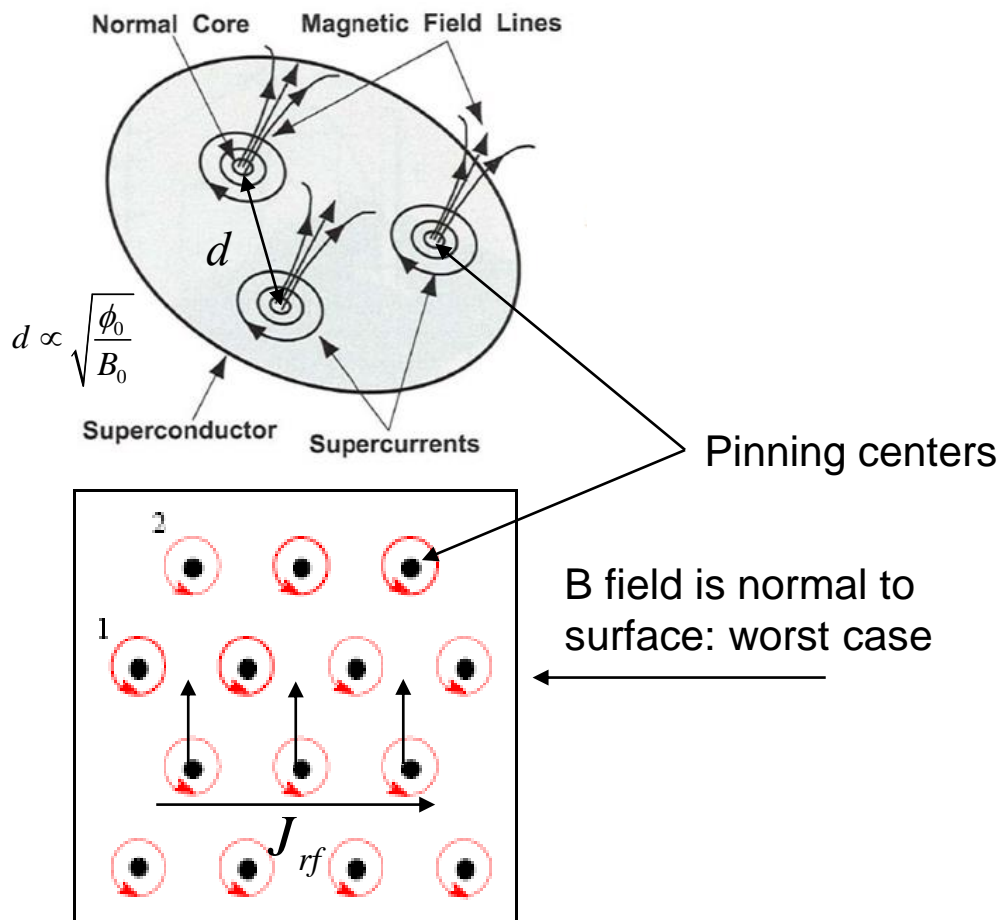
$$\eta = \frac{\phi_0 B_{c2}}{\rho_n} \quad k = \frac{2\pi J_c \phi_0}{d} \quad \omega_o = \frac{k}{\eta}$$

The “**depinning frequency**”

$$f_o(B_o) = \frac{\omega_o(B_o)}{2\pi} = \frac{\rho_n \sqrt{B_o} J_c(B_o)}{\sqrt{\phi_0} B_{c2}}$$

Surface resistance

$$R_f = \frac{\rho_n}{2\lambda} \frac{B_o}{B_{c2}} \frac{f^2}{f_o^2}$$



Gittleman and Rosenblum: Phys Rev. Lett. 16, 734 (1966)
 Calatroni and Vaglio, IEEE Trans. Appl. Supercond. 27 (2017) 3500506
 Coffey, Clem PRL 67, 386 (1991)
 Brandt PRL 67 2219 (1991)
 Silva et al, PRB 78, 094503 (2008)

Zoo of superconductors

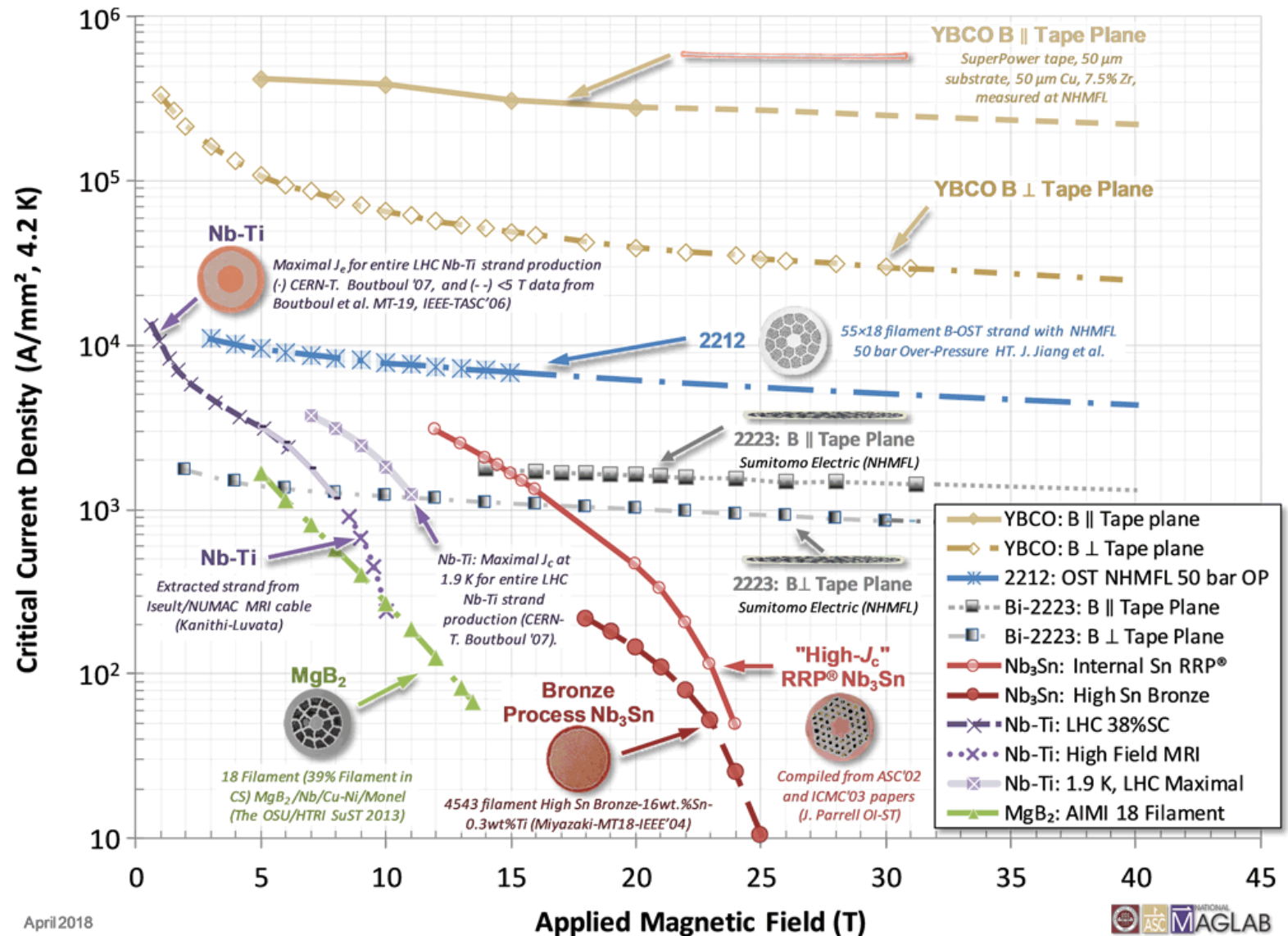
J_c may vary of orders of magnitude.

H_{c2} has much smaller variation.

YBCO most promising candidate

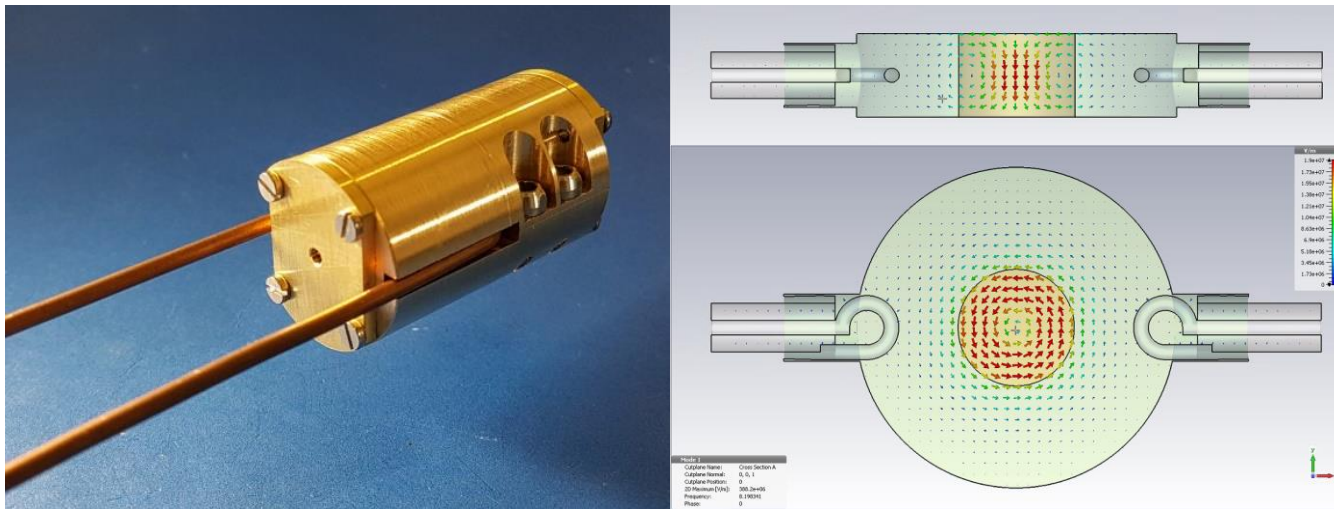
NbTi – NbTiN possible candidates at $B < 10T$

Nb_3Sn for $B < 15 T$



<https://nationalmaglab.org/magnet-development/applied-superconductivity-center/plots>

Validation of RF performance (UPC - ICMAB)



In house developed 8.05 GHz cavity resonator compatible with 25mm bore 9 T magnet at ICMAB

REBCO CCs outperform Cu at 50K and up to 9T
 R_s is microstructure dependent

Puig et al, SuST 32, 094006 (2019)

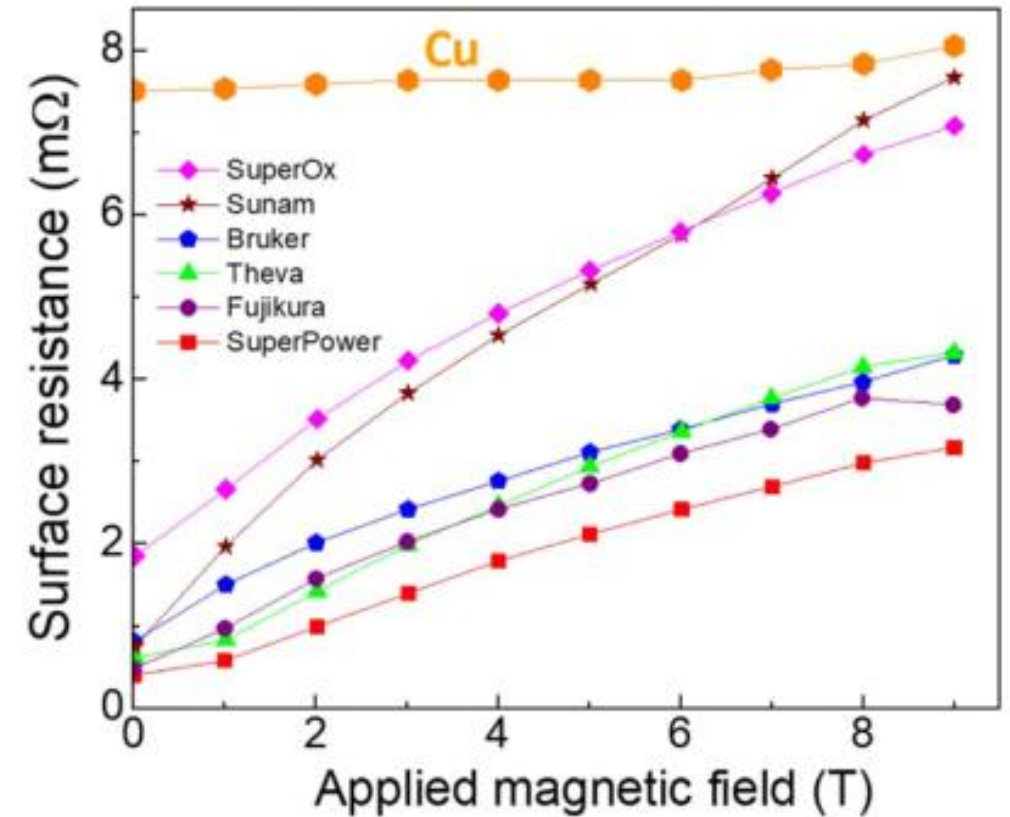
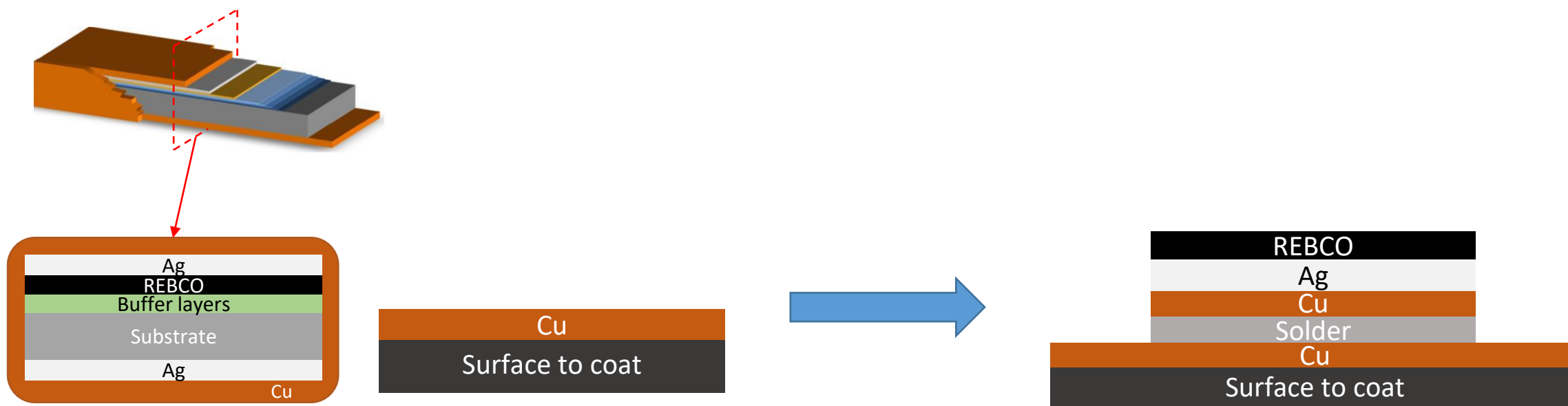


Figure 3. Magnetic field dependence of the surface resistance at 8 GHz and 50 K. Up to 9 T, CCs' R_s outperforms that of copper.

Surface currents equivalent to 0.1 MV/m of a typical accelerating cavity

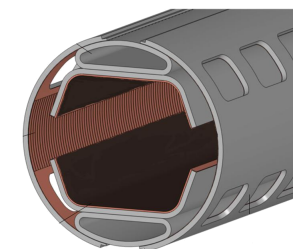
HTS coated conductor soldering and delamination



N. Lamas et al., to be published

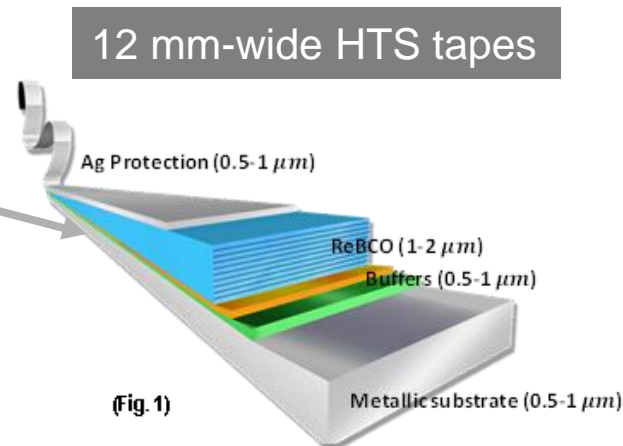
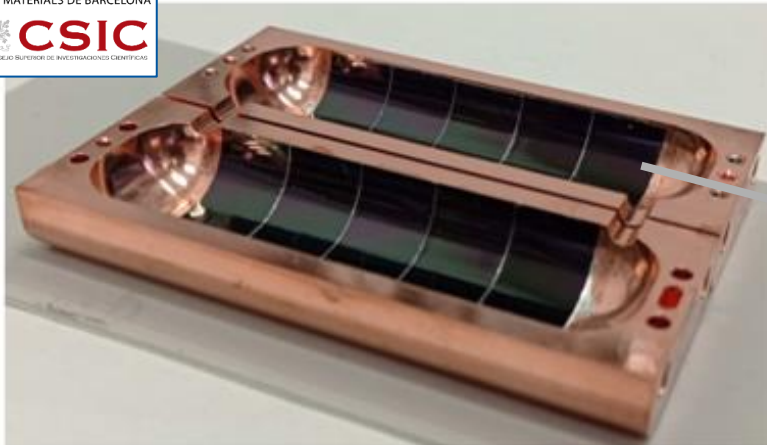


Developed in the context of FCC-hh impedance reduction by coating the beam screen with HTS tapes

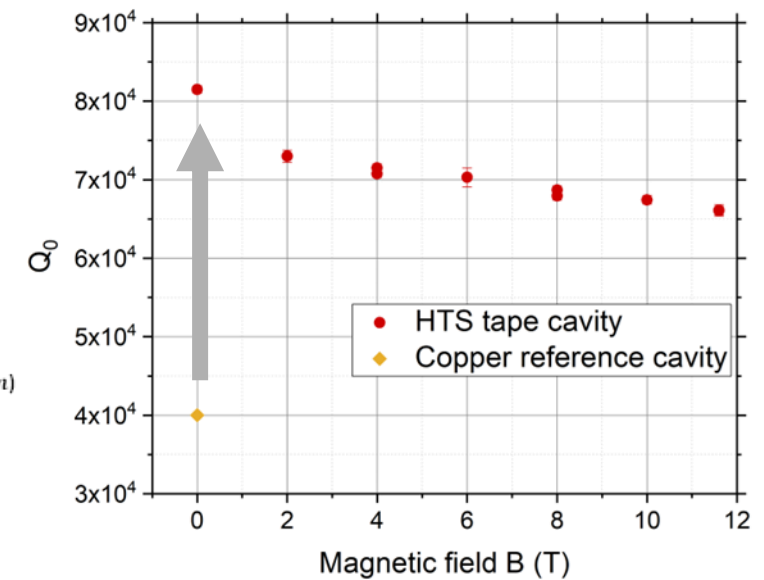


First real cavity, $f \approx 9$ GHz

- We have developed a technology for applying 2D HTS tapes to 3D RF “RADES” cavities demonstrating the potential of HTS for RF applications J. Golm et al., IEEE TAS, Vol. 32, No. 4, (2022) 1500605



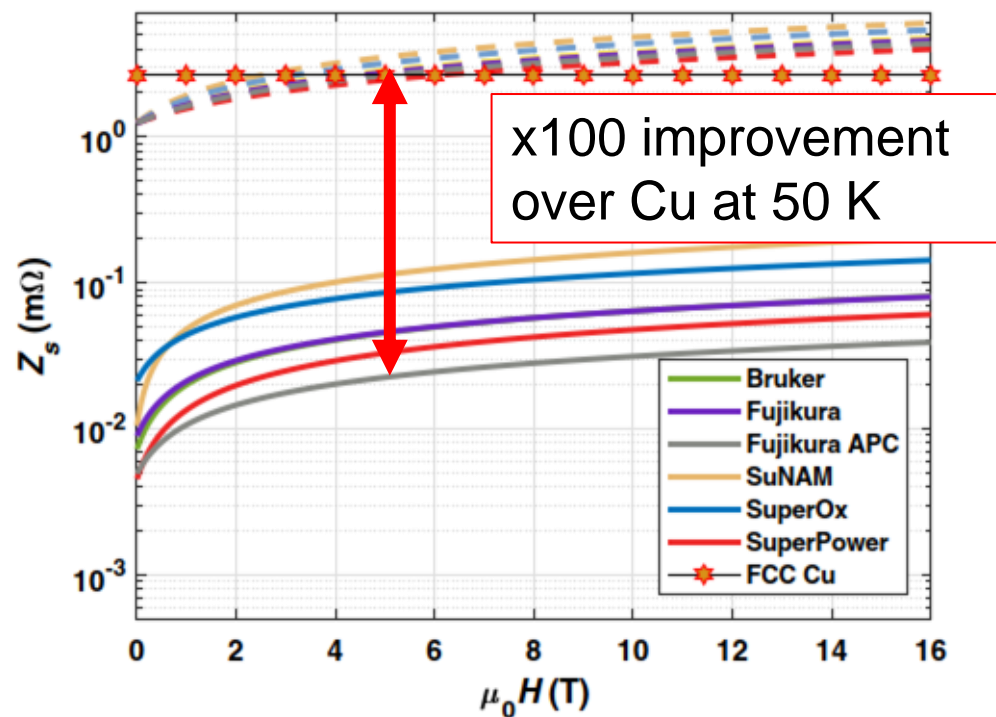
2x improvement of RF quality factor compared to copper
(newer prototype 5x improvement)



RADES cavity for axion searches

Scaling to lower frequency

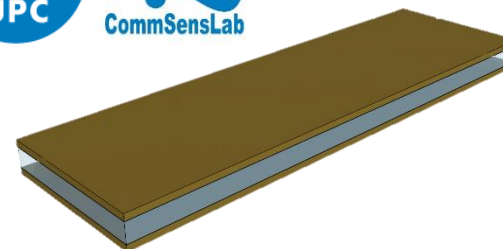
REBCO **scaled** to 1 GHz at 50 K



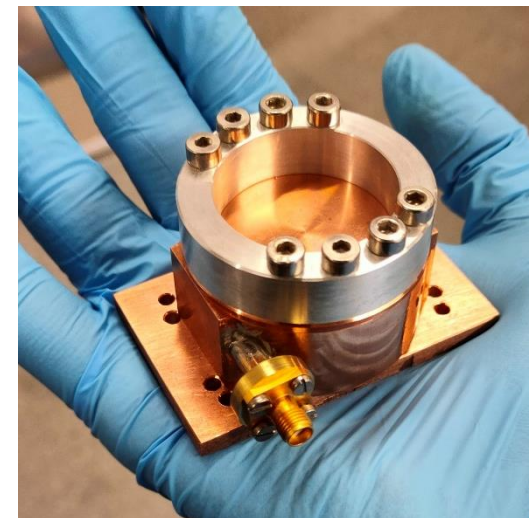
Romanov et al, SciRep 10:12325 (2020)

For HTS R_s scales as f^2
For Cu R_s scales as $f^{1/2}$

A **parallel-plate resonator** is being commissioned to test samples at ~ 1 GHz



38x12 mm samples
50 mm bore
16 T
 $X_s(T)$ at all frequencies



Will demonstrate **real experimental frequency scaling** on samples

- HTS cavities in a strong magnetic field
- **HTS cavities at high-gradient**
- HTS cavities in both strong field and high-gradient
- Future steps

Potential motivation: linear colliders

- Linear collider studies fall essentially in two categories



Superconducting niobium, CW



Normal conducting copper, pulsed

- Linear collider studies result in **roughly similar power consumption** for equivalent machines (ie ILC vs CLIC)
- We want to see if **HTS in pulsed RF mode** allows an optimal gain compared to both Nb and Cu

Cryo-cooled copper -> HTS ?

- The C³ study aims at cryogenically cooled copper, to attain a larger gradient and save cost in the RF power stations
- A further advantage could come from combining the advantage of higher gradients at lower temperatures, with the higher Q factor of HTS coatings -> **energy efficiency**

TABLE I. Summary of the accelerating parameters of the distributed-coupling accelerating structure at 300 and 77 K. The peak fields are calculated for an average accelerating gradient of 100 MV/m.

Parameter	300 K	77 K
Frequency (GHz)	11.402	11.438
Q_0	10000	22500
Q_{ext}	10000	10000
Shunt impedance (M Ω /m)	155	349
Peak surface E (MV/m)	250	250
Peak surface H (MA/m)	0.575	0.575
Steady state rf power (MW)	17	9
Iris diameter (mm)	2.6	2.6
Length (cm)	26	26

Cryoplant efficiency (Carnot + engineering)

SRF temperature	Ratio W_{300K}/W_{cryo}
77 K	13
50 K	20
4.2 K	230
1.9 K	920

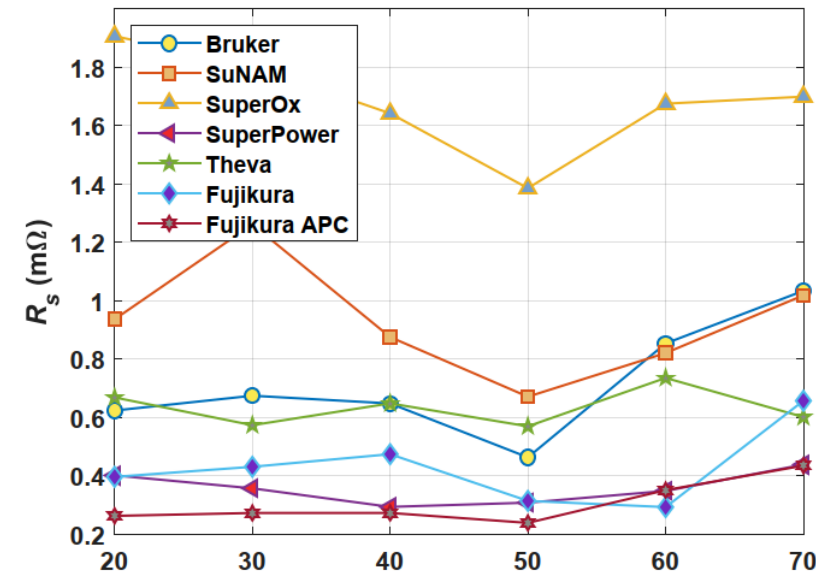
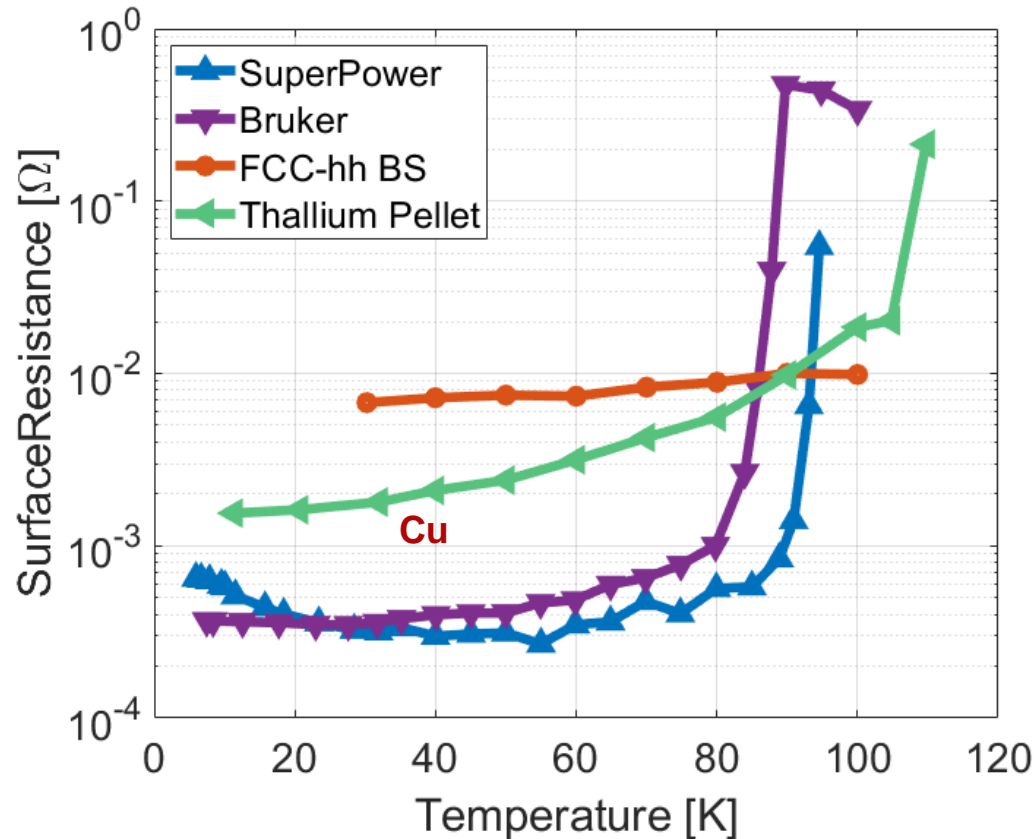
Thanks to T. Koettig, CERN

E. Nanni et al., PRAB 24, 093201 (2021)

A factor x10 improvement in Q factor compared to copper could pave the way for significant energy savings

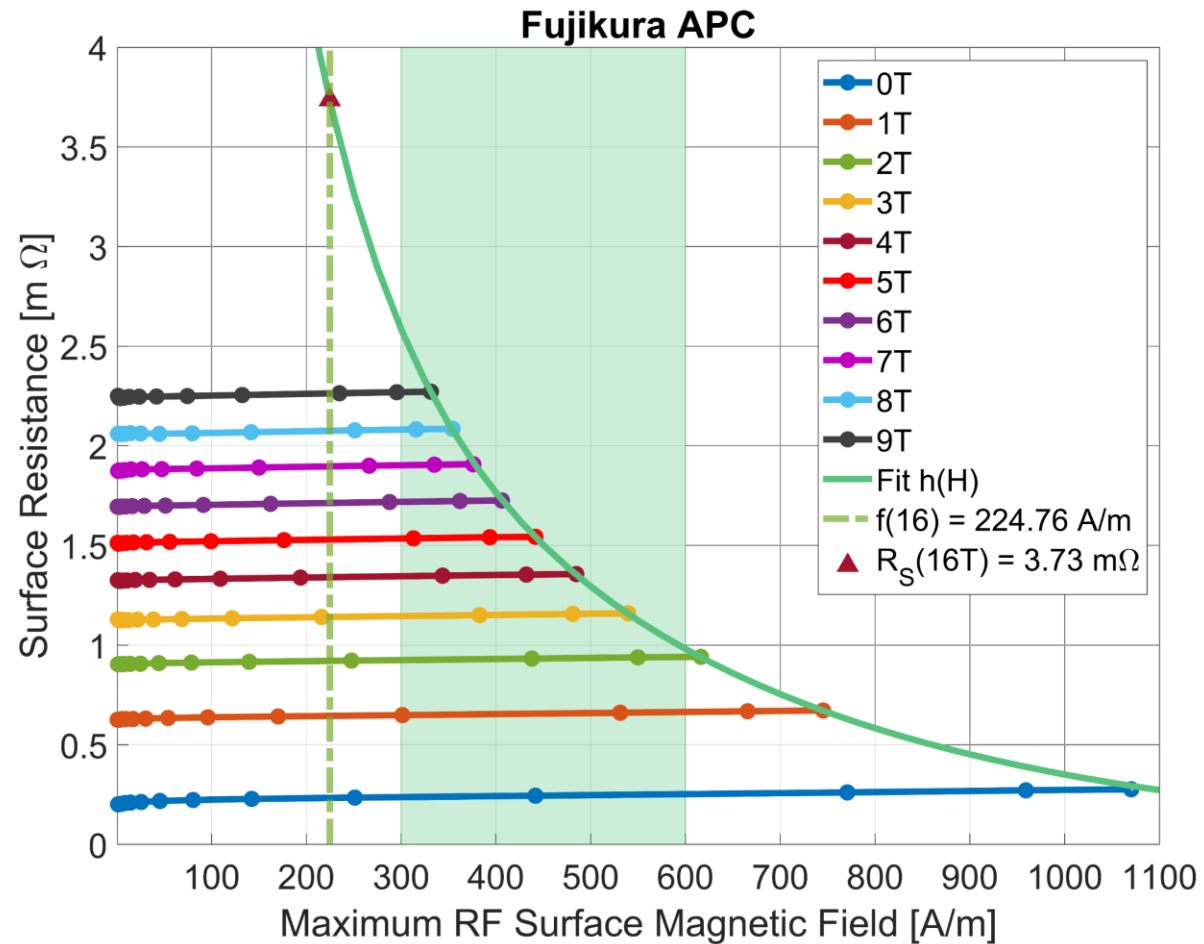
Low-power measurements

- A potential **improvement at least x10** compared to copper ($R_s=8\text{m}\Omega$) has been **measured on samples of tapes** (8 GHz) at low RF power



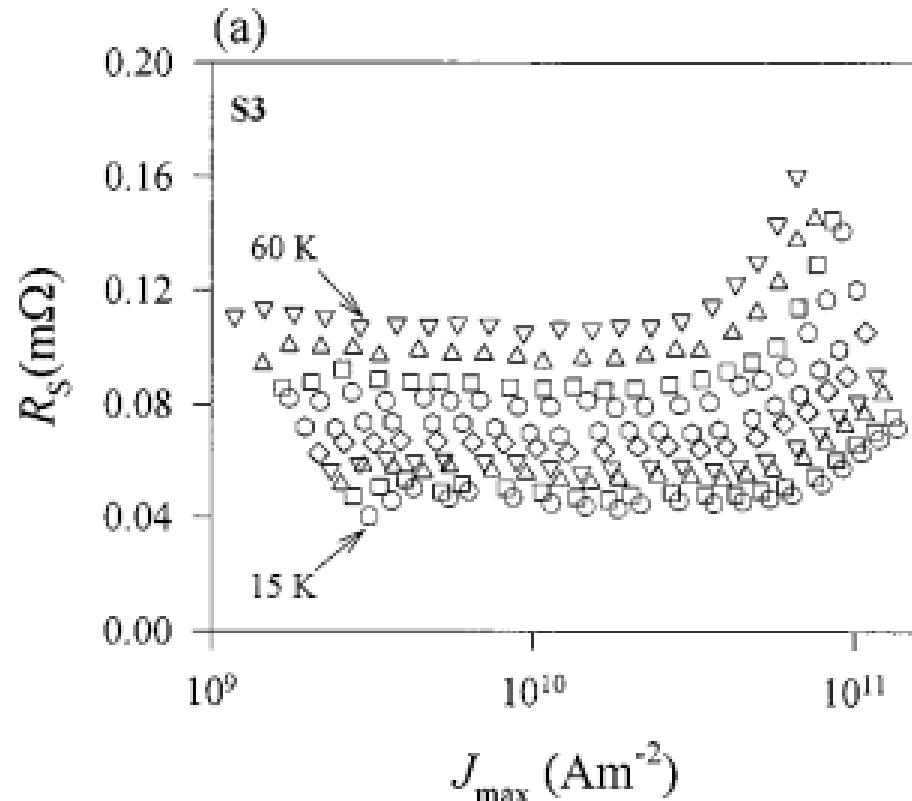
(adapted from Romanov et al, [Sci. Rep. \(2020\) 10:12325](#))

HTS tape at 8 GHz (dielectric resonator)



Patrick Krkotic, PhD dissertation, UPC Barcelona 2022

- There are very few measurements on HTS at high RF currents (mostly microstrip resonators). But physics is proven.



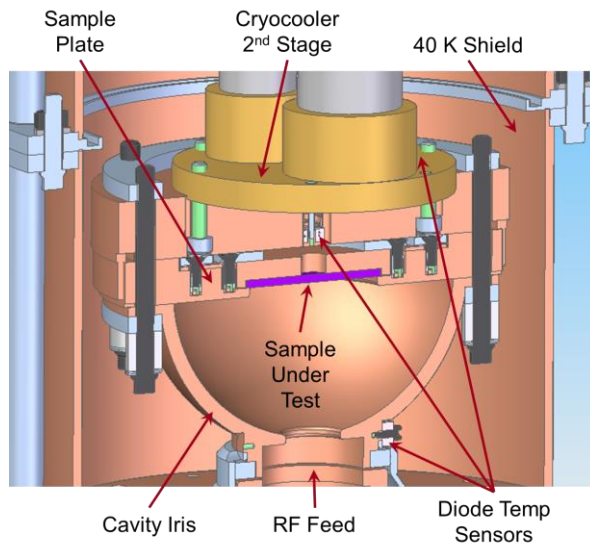
$\sim 10^{11}$ A/m^2 RF current (microstrip resonator, 200 μm , 350 nm thick, 8 GHz)

Powell et al. Journal of Applied Physics 86, 2137 (1999)

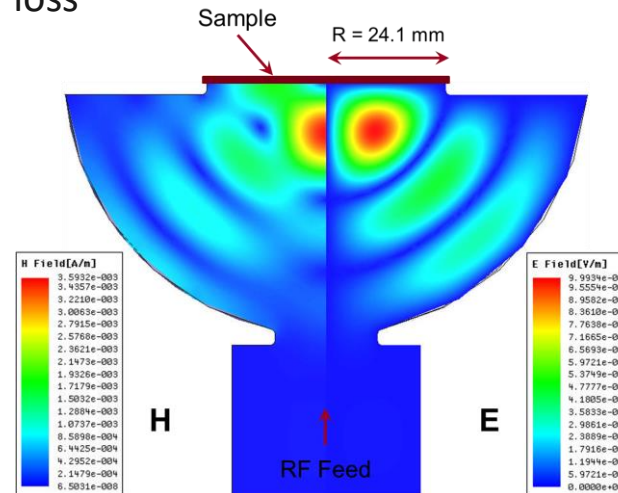
For 1 μm thickness this is equivalent to 10^5 A/m ($\cong 0.1$ T $\cong 25$ MV/m)
in the “high-gradient” range

High-gradient testing at SLAC – supported by I.FAST IIF

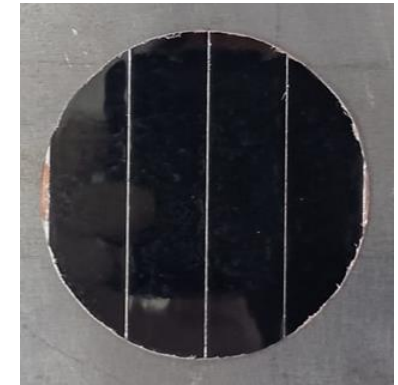
- Demountable high-power RF cavity
- Can achieve H_{peak} of about 360 mT using 50 MW XL-4 Klystron.



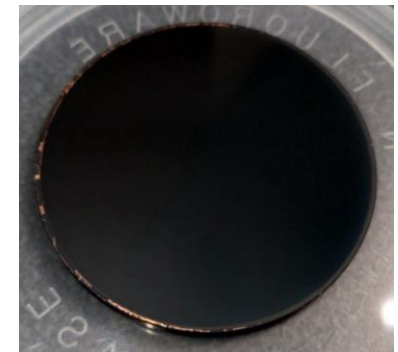
- High-Q X-band hemispheric cavity with a TE_{032} -like mode at 11.4 GHz.
- Zero E-field on the sample
- Maximum H-field on the sample
- Sample accounts for $\frac{1}{3}$ of total cavity loss



HTS-coated with tapes
By CSIC-ICMAB



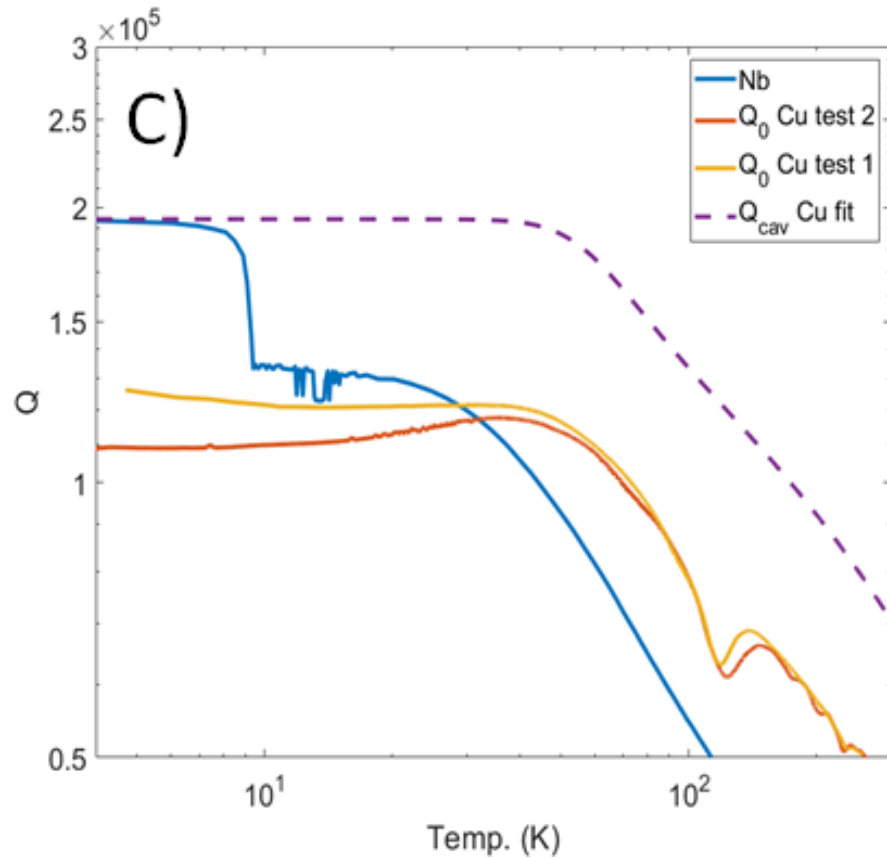
HTS-coated sample
By CERACO



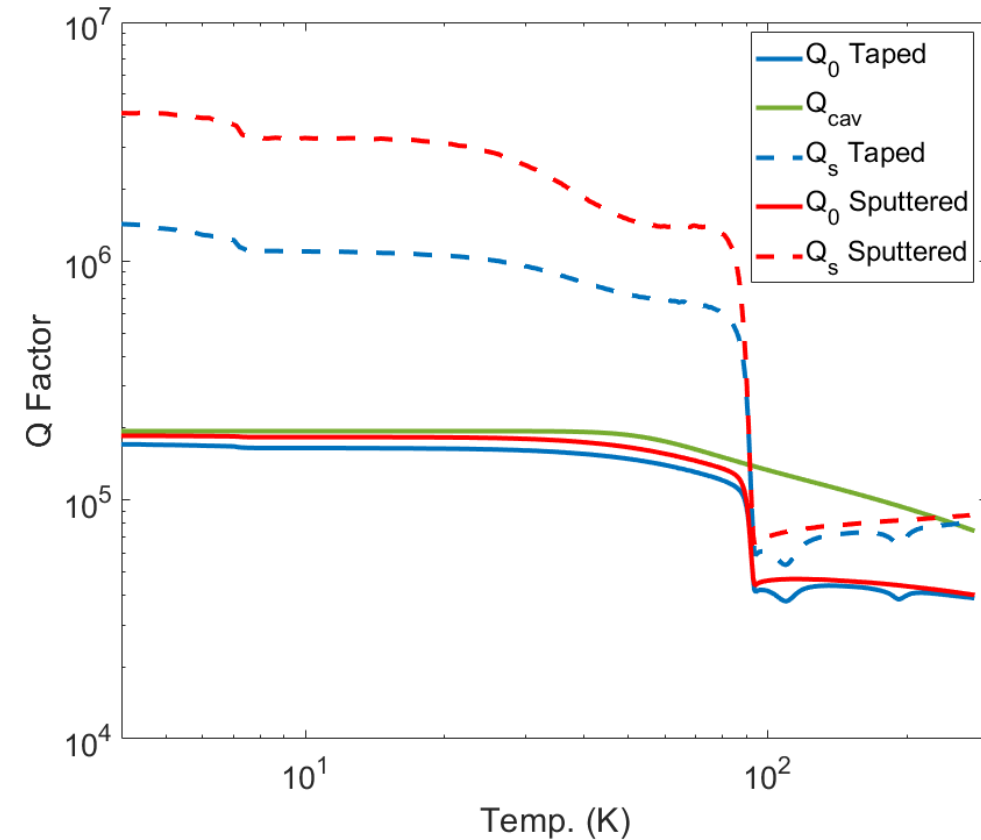
Goal: demonstrate high-gradient pulsed operation of HTS, at cryo-temperatures, and develop large size coatings (50 mm wide tapes)



Cu and Nb reference measurements



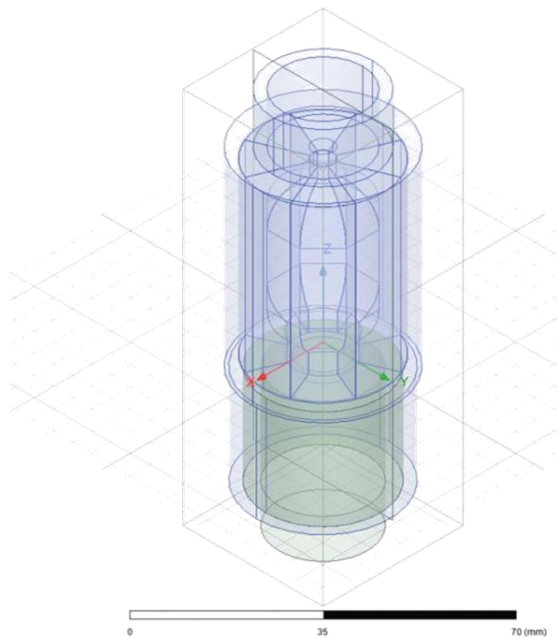
HTS measurements



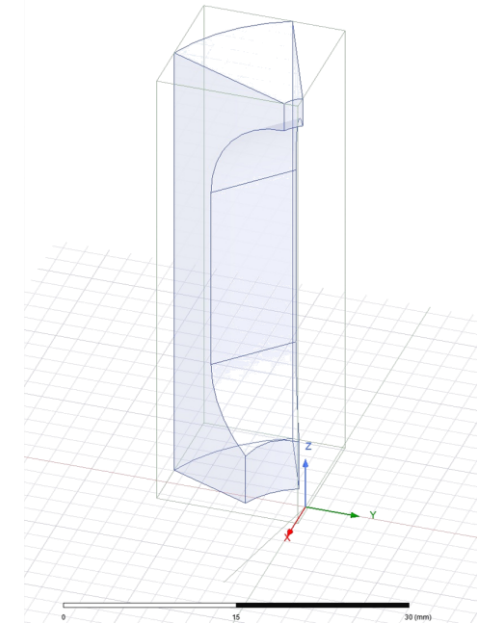
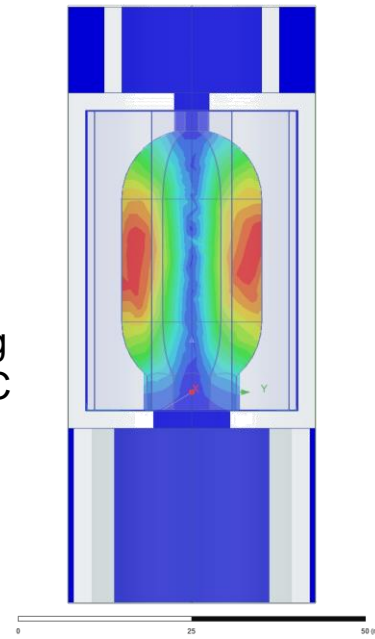
High-gradient tests foreseen shortly

First device validation – supported by I.FAST Innovation Fund

- Device approach: X-band pulse compressor (SLAC) as first “real” device
- Coated with small tapes by CSIC-ICMAB for device validation
- Future goal: full device with large-size tapes (or directly coated on copper, ideally)



Courtesy Greg LeSage, SLAC



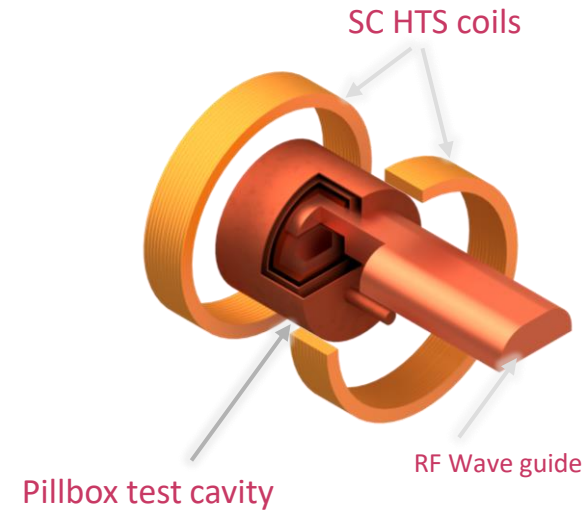
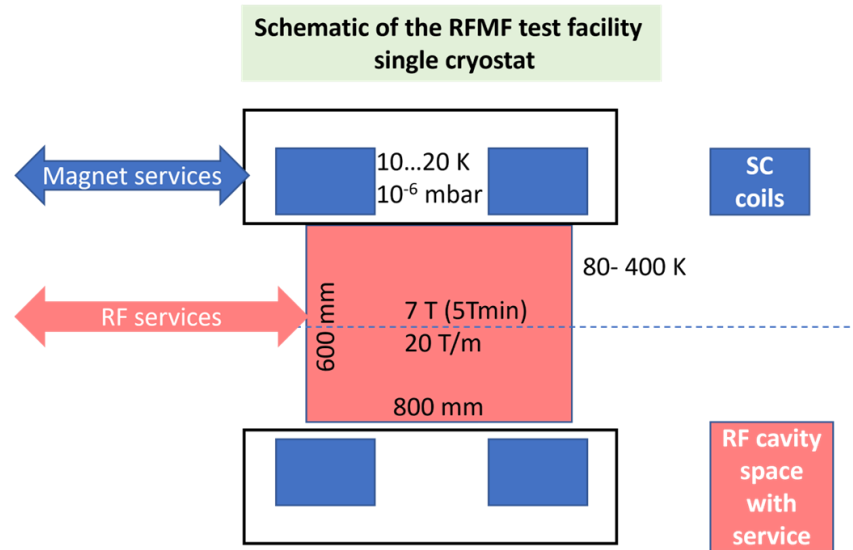
Max surface field 3.126 MA/m

- HTS cavities in a strong magnetic field
- HTS cavities at high-gradient
- **HTS cavities in both strong field and high-gradient**
- Future steps

- HTS cavities in a strong magnetic field
- HTS cavities at high-gradient
- HTS cavities in both strong field and high-gradient
- **Future steps**

Possible test in a dedicated RF stand

- See talk of Dario Giove later today



Sc magnet/cryostat sketch by M. Castoldi & Stefano Sorti, UMIL & INFN-LASA
(RF drawing by Guillaume Ferrand -CEA)



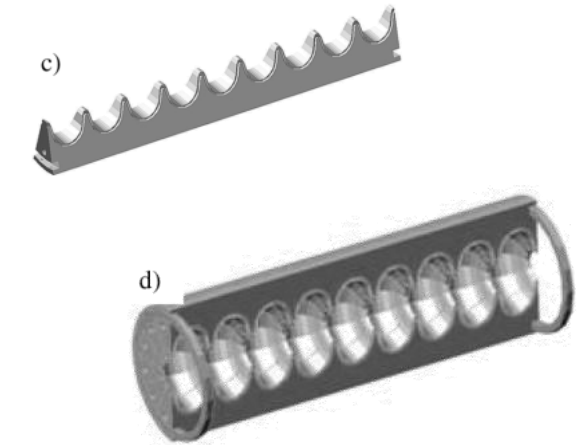
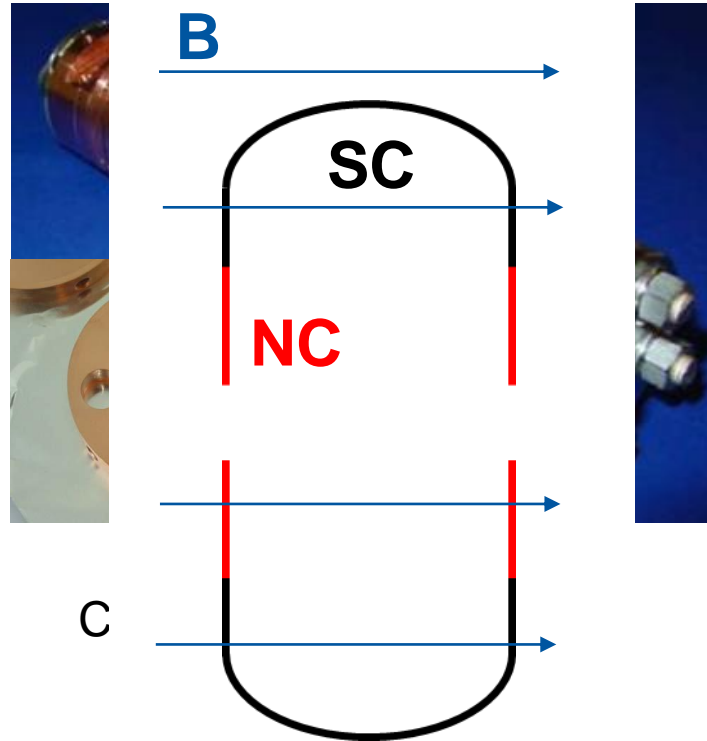
- Availability of a high-field / high-gradient test stand foreseen within the MuCol study could be beneficial for the entire HTS-HFF community

Possible practical implementation of HTS tape-coated cavities

- How could a future cavity look like? **Bimetallic cavities**



J. Haimson, WEPMS085, PAC07 (s.steel inserts)



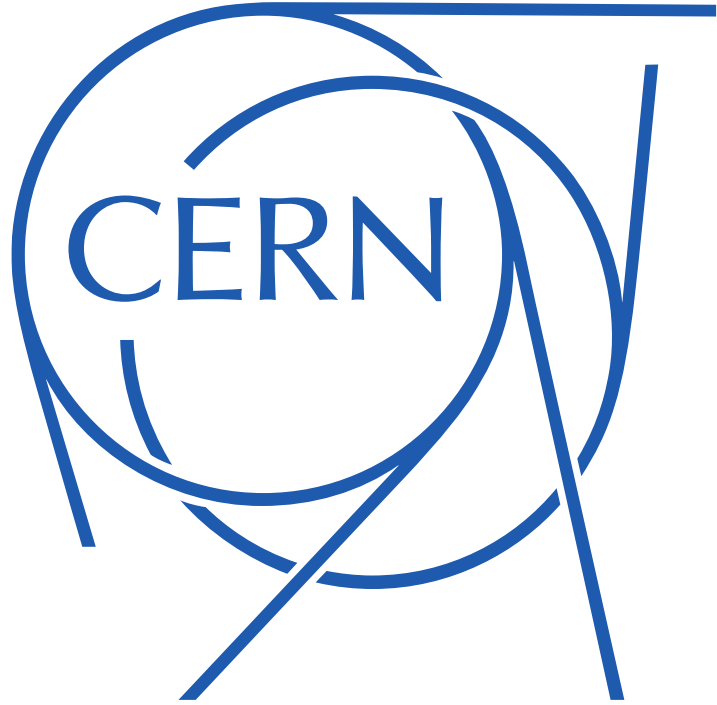
P. McIntyre et al., IEEE TAS 19 (2009) 1380

Composite cavities exist and have ∂d .

Joints at low-current regions are standard practice even in SRF cavities (ie QWRs)

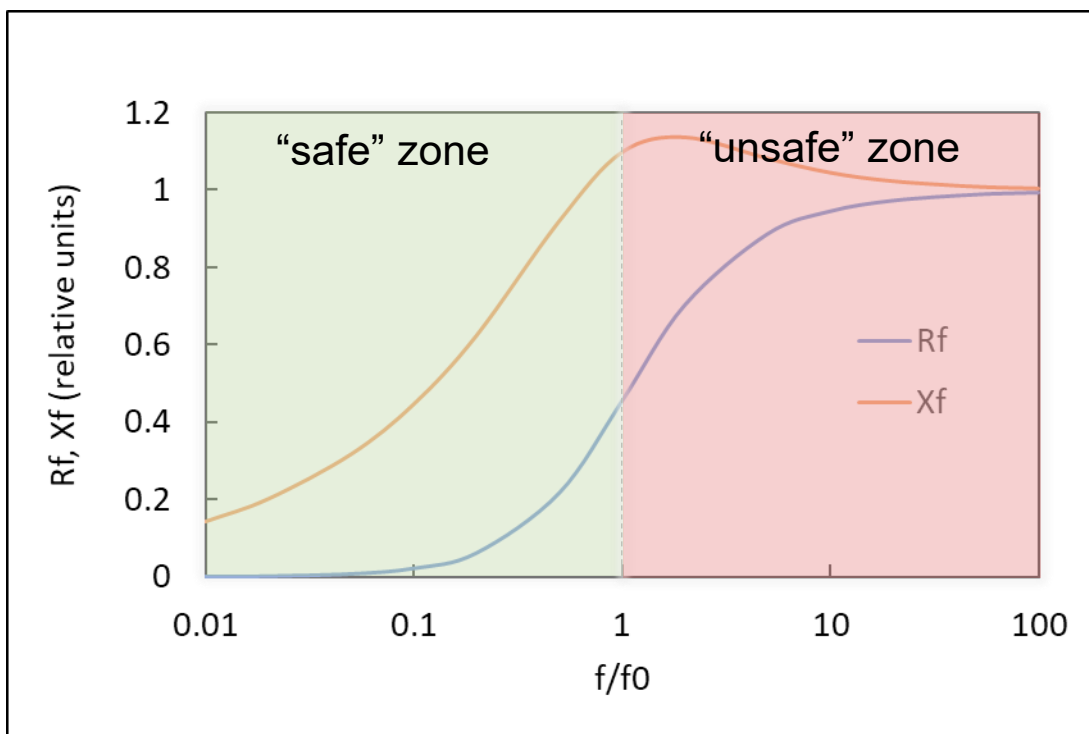
Segmentation at zero-current region is possible, see device being designed at SLAC

- **No data for HTS at high-gradient and in strong magnetic field exist (either samples or cavities): experiments needed**
- Overall energy efficiency would have to be studied, taking into account: **operating temperature, cryo-efficiency, possible Q-factor, pulsed operation**
- Fabrication technologies for real cavities have to be assessed: **wider soldered tapes**, or develop a **direct HTS coating** technique?



Effect of magnetic field: fluxon losses in RF

Surface **resistance**, **reactance** due to vortex motion



Case $f < f_0$

$$R_f = \frac{\rho_n}{2\lambda} \frac{B_o}{B_{c2}} \frac{f^2}{f_0^2} \quad B_0 \ll B_{c2}$$

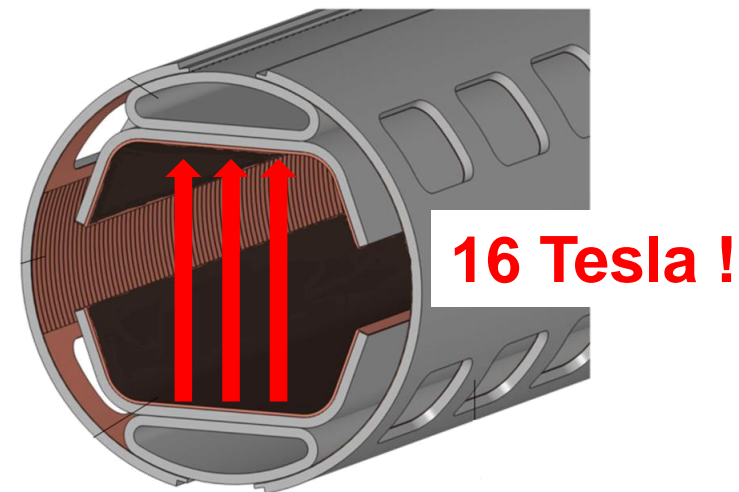
$$R_f = \frac{R_n}{\sqrt{2}} \sqrt{\frac{B_o}{B_{c2}}} \left(\frac{f}{f_0} \right)^{3/2} \quad B_0 \ll B_{c2}$$

$$f_0(B_o) = \frac{\omega_o(B_o)}{2\pi} = \frac{\rho_n \sqrt{B_o} J_c(B_o)}{\sqrt{\phi_o} B_{c2}}$$

To maximize f_0 and minimize fluxon losses we need **high J_c materials**

HTS for the FCC-hh beam screen

- Recent work motivated by the need of **HTS materials** for replacing copper in the **FCC-hh beam screen**, to reduce **beam coupling impedance**.
- Beam produces **RF fields**
- Extremely challenging requirements:
 - **HTS must operate at 50 K and 16 T**
 - **Critical fields H_{c2} , $H_{irr} \gg 16T$**
 - **$J_c > 25 \text{ kA/cm}^2$ ($2.5 \times 10^8 \text{ A/m}^2$)**
 - **Surface resistance R_s better than for copper**
- **Compatible with accelerator environment**
 - **Minimize dipole field distortion** due to persistent currents (Note 1)
 - **UHV compatible, low SEY, lifecycle assessment, etc..**

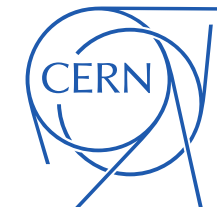


Calatroni, IEEE TAS 26, 3500204 (2016)
Calatroni et al, SuST 30, 075002 (2017)

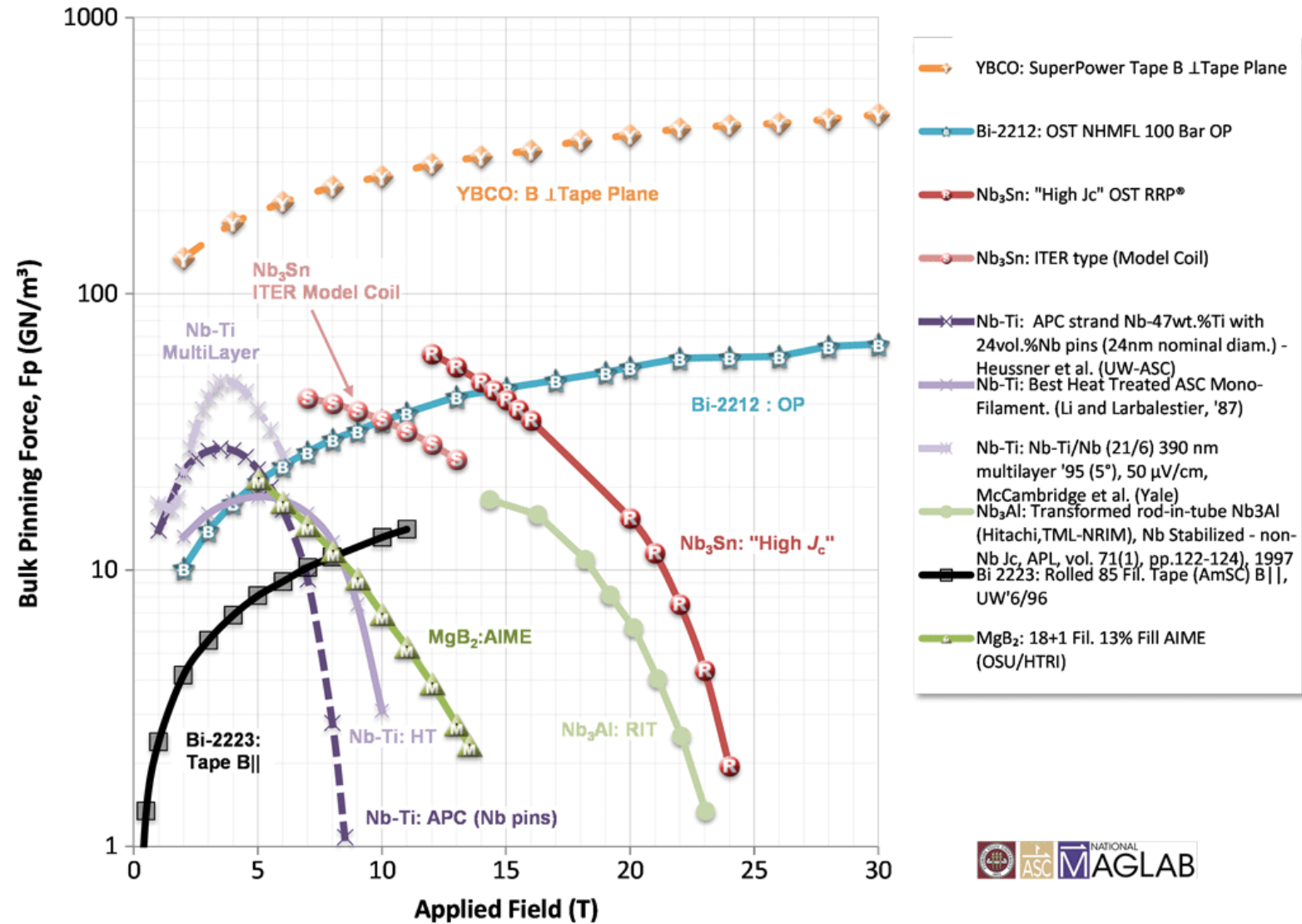
How to make it in practice ?

Manufacture the screen using REBCO tapes soldered to the screen

Coat the inside of the screen with TI-1223 films



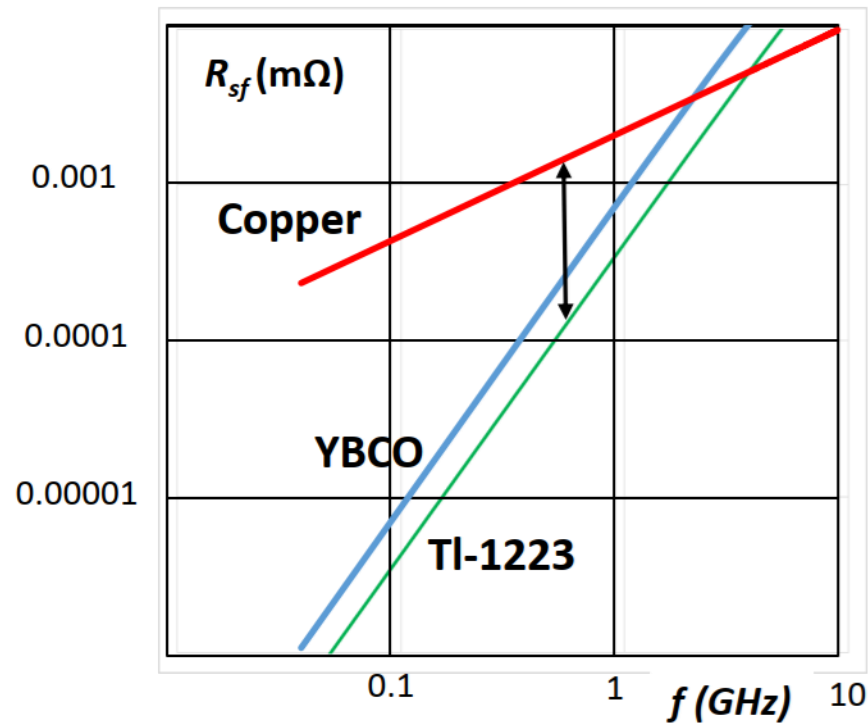
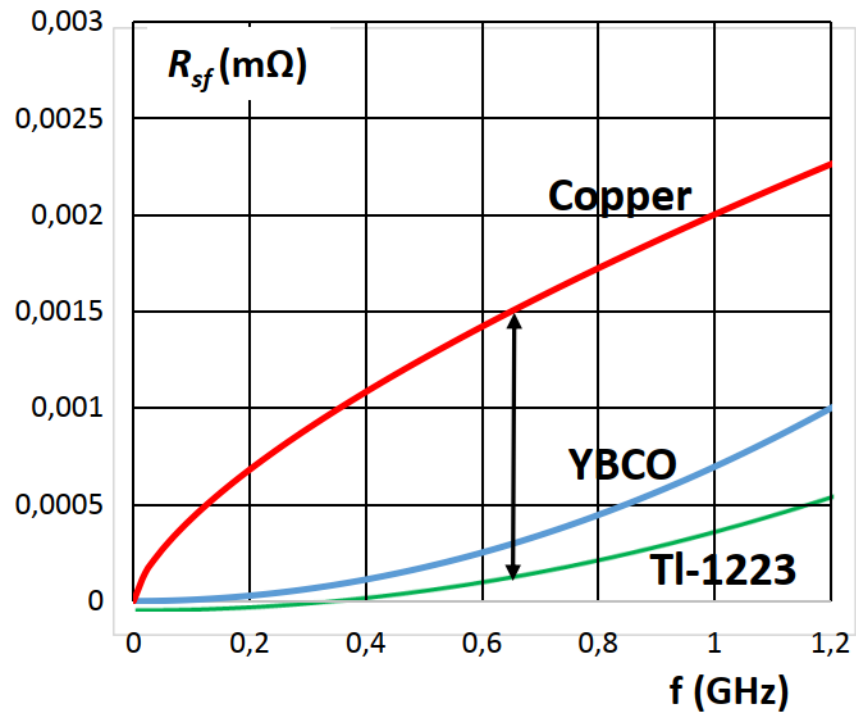
Pinning force



<https://nationalmaglab.org/magnet-development/applied-superconductivity-center/plots>

Predicted surface resistance of HTS in 16 T field

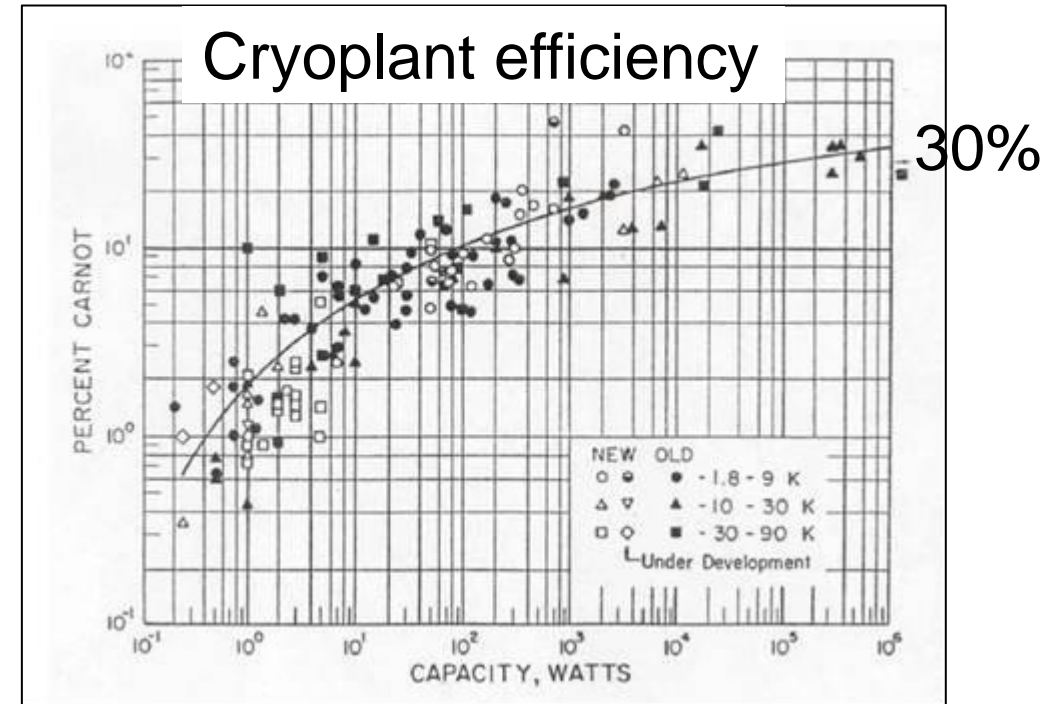
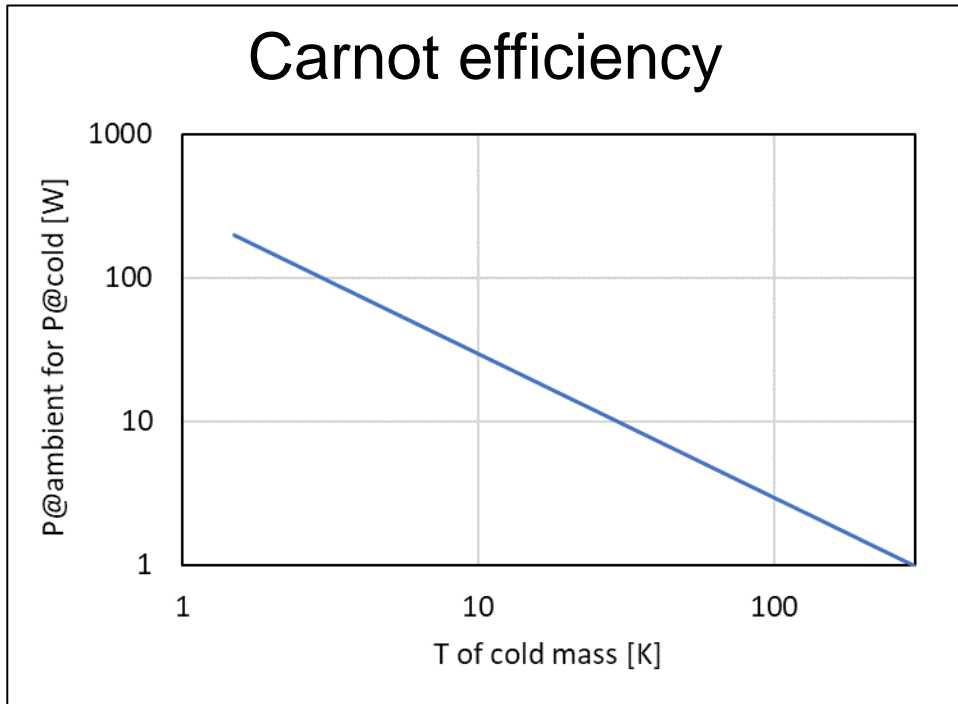
YBCO	$T_c=92\text{K}$	$T=50\text{K}$	$B_0=16\text{T}$	$J_c(50,16)=7.5 \times 10^9 \text{Am}^{-2}$	$B_{c2}(50)=40\text{T}$	$\rho_n=60 \mu\Omega\text{cm}$	$f_0=10\text{GHz}$
Tl-1223	$T_c=125\text{K}$	$T=50\text{K}$	$B_0=16\text{T}$	$J_c(50,16)=1 \times 10^{10} \text{Am}^{-2}$	$B_{c2}(50)=80\text{T}$	$\rho_n=80 \mu\Omega\text{cm}$	$f_0=14\text{GHz}$



For HTS the R_s scales as f^2

For Cu the R_s scales as $f^{1/2}$

Cryogenic losses: SRF aimed at energy saving compared to NRF



Power consumption for 1 W @ 77 K	13 W
Power consumption for 1 W @ 20 K	50 W
Power consumption for 1 W @ 4.2 K	230 W
Power consumption for 1 W @ 1.9 K	920 W

Thanks to T. Koettig, CERN

Surface Impedance Measurements on Nb₃Sn in High Magnetic Fields

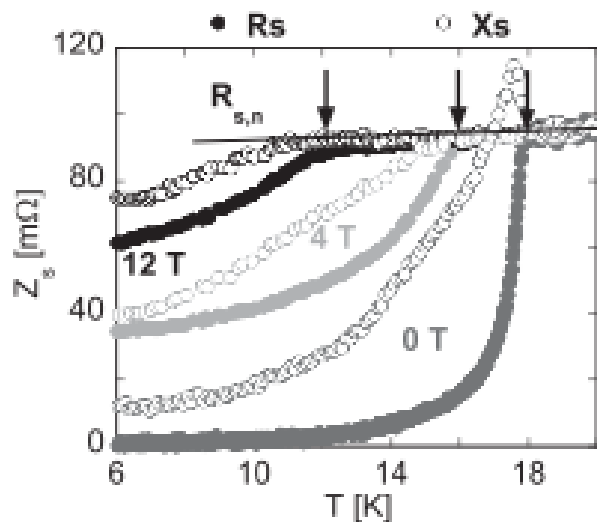


Fig. 2. Z_s measured at fixed $\mu_0 H$, depicted in the figure, and varying T . Full circles: R_s ; empty circles: X_s . Colors: black, $\mu_0 H = 12$ T; light gray, $\mu_0 H = 4$ T; dark gray, $\mu_0 H = 0$ T. Vertical arrows indicate $T_{c2}(H)$.

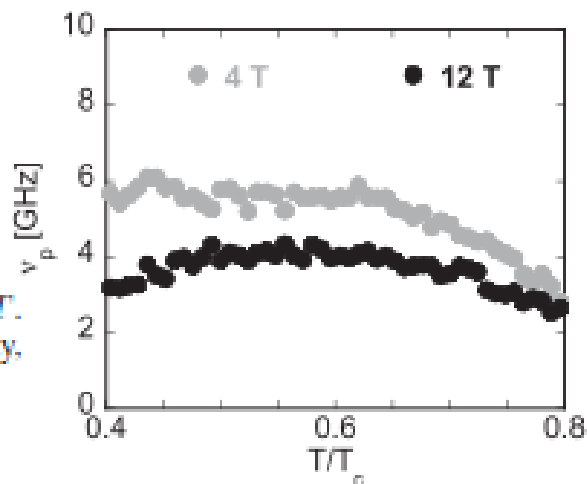
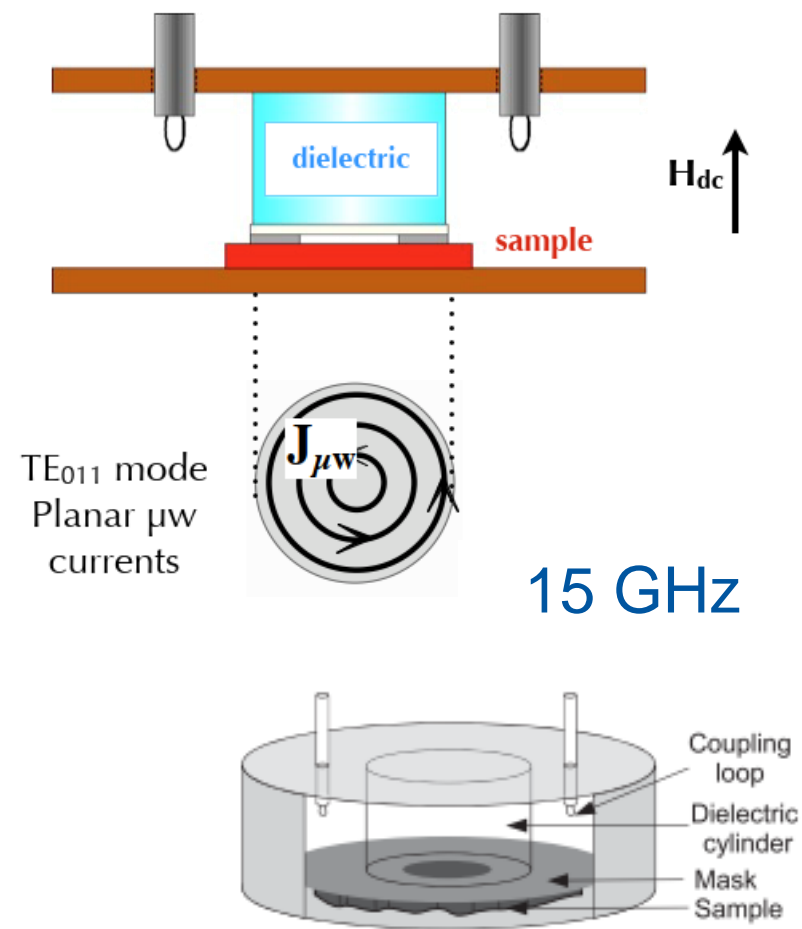








Fig. 4. The depinning frequency ν_p at $\mu_0 H = 12$ T (black points) and at $\mu_0 H = 4$ T (gray points). The ν_p is almost constant up to $0.65 T_c$.



HTS coating technologies

						
$ReBa_2Cu_3O_7$	Y	Gd Eu	Gd	Gd Y	{ Y,Gd }	Gd
Thickness [μm]	1.6	1.8 2.5	1.6	0.9 3.0	1.5	3.0
Nano-inclusion	BaZrO ₃	none BaHfO ₃	none	none Y ₂ O ₃	BaZrO ₃	none
Technology	PLD	PLD	RCE	PLD	MOVCD	EB-PVD
Substrate	Stainless Steel	Hastelloy C276	Hastelloy C276	Hastelloy C276	Hastelloy C276	Hastelloy C276
Thickness [μm]	100	75 50	100	60 40	50	100
Stabilizer [μm]	e.p. 25	lam. 75	e.p. 20	e.p. 10	e.p. 20	e.p. 20
T_C [K]	85	94 92	94	94	91	92

Patrick Krkotic, PhD dissertation, UPC Barcelona 2022

Microwave Losses in a DC Magnetic Field in Superconducting Cavities for Axion Studies

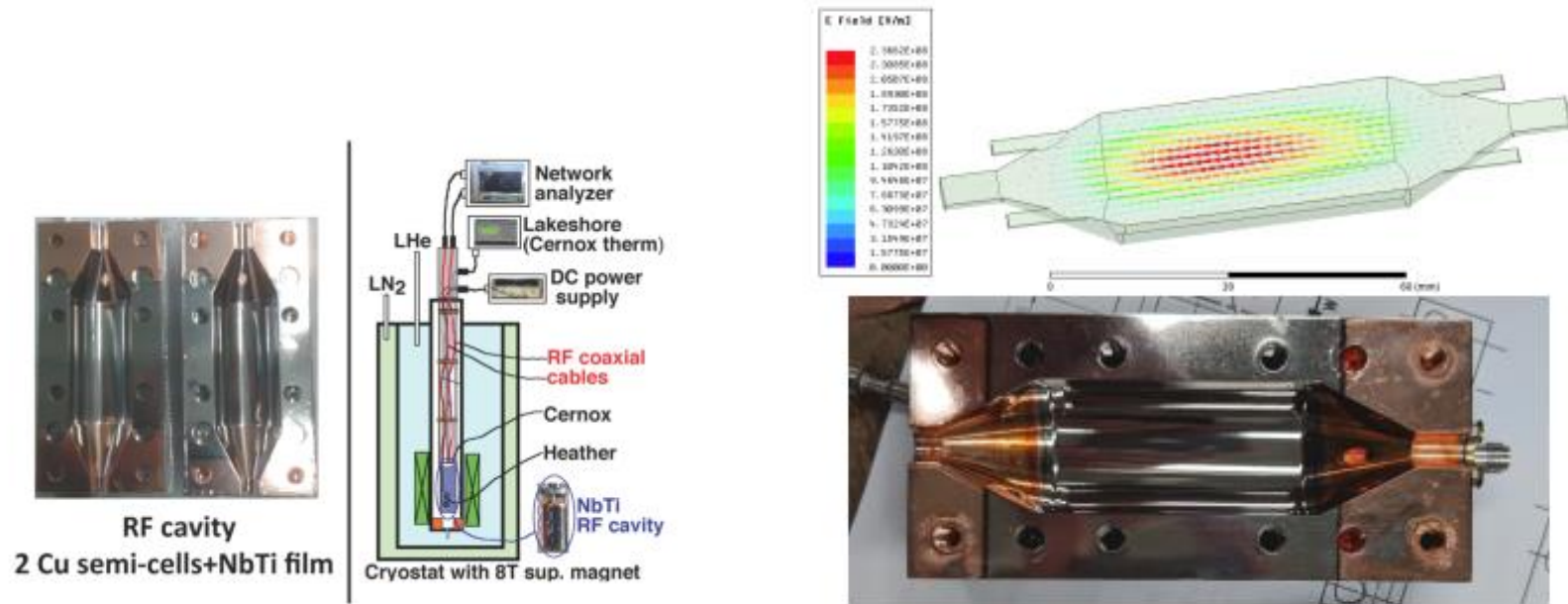
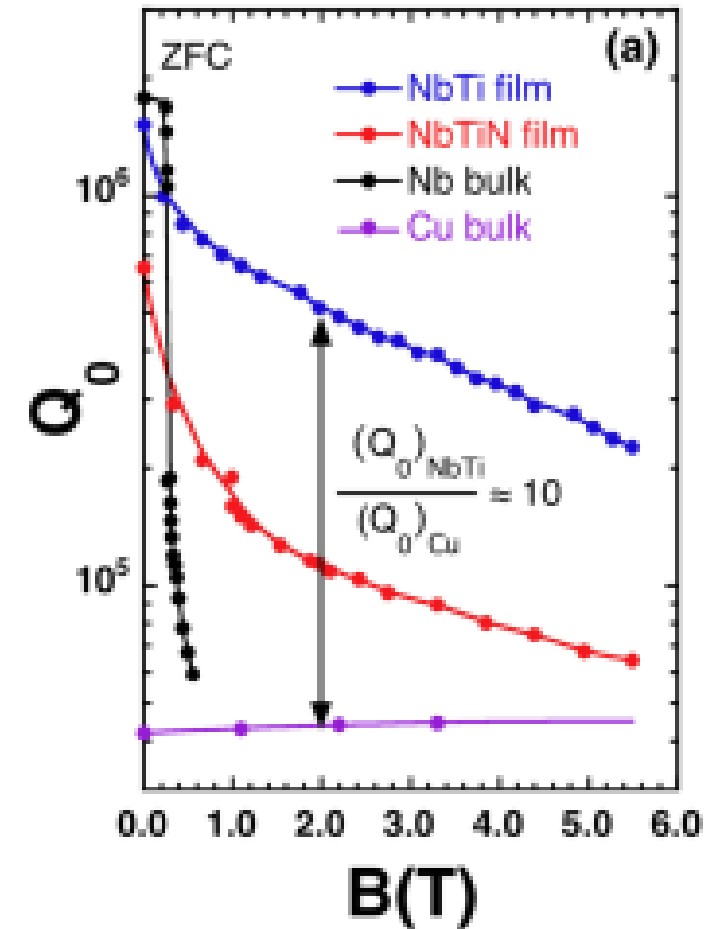


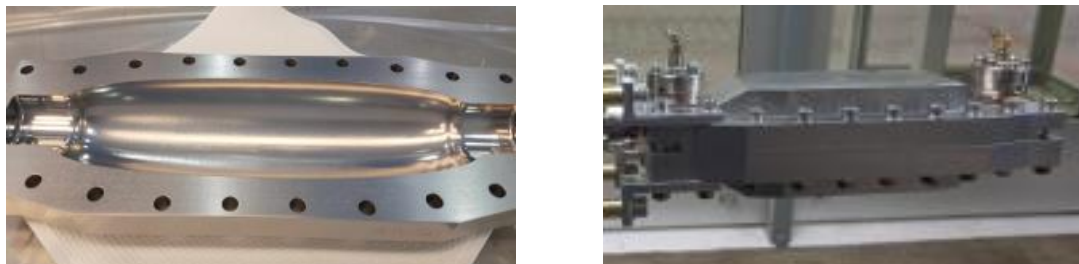
FIG. 1: The upper image represents the electric field of 9.08 GHz TM₀₁₀ mode in arbitrary amplitude units, while the lower photo is one of the two halves of the superconducting cavity.



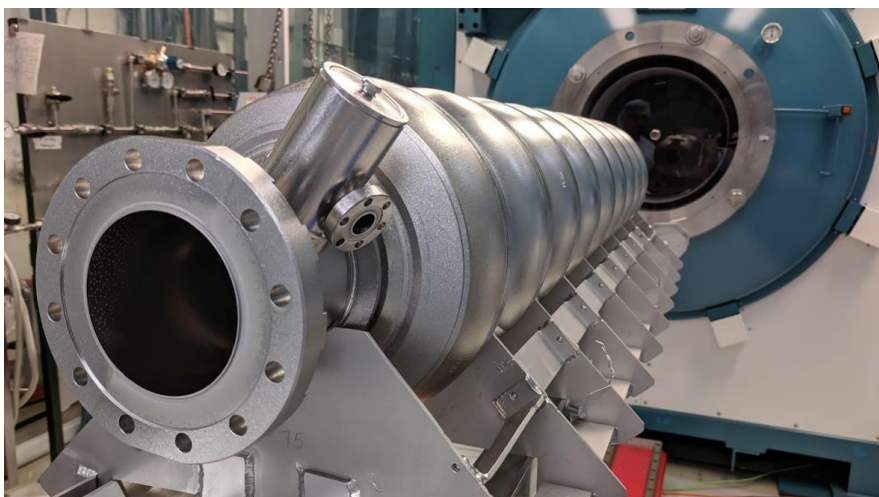
x10 improvement over copper at 4.2 K

Nb₃Sn @ 3.9 GHz in strong magnetic field: FNAL results

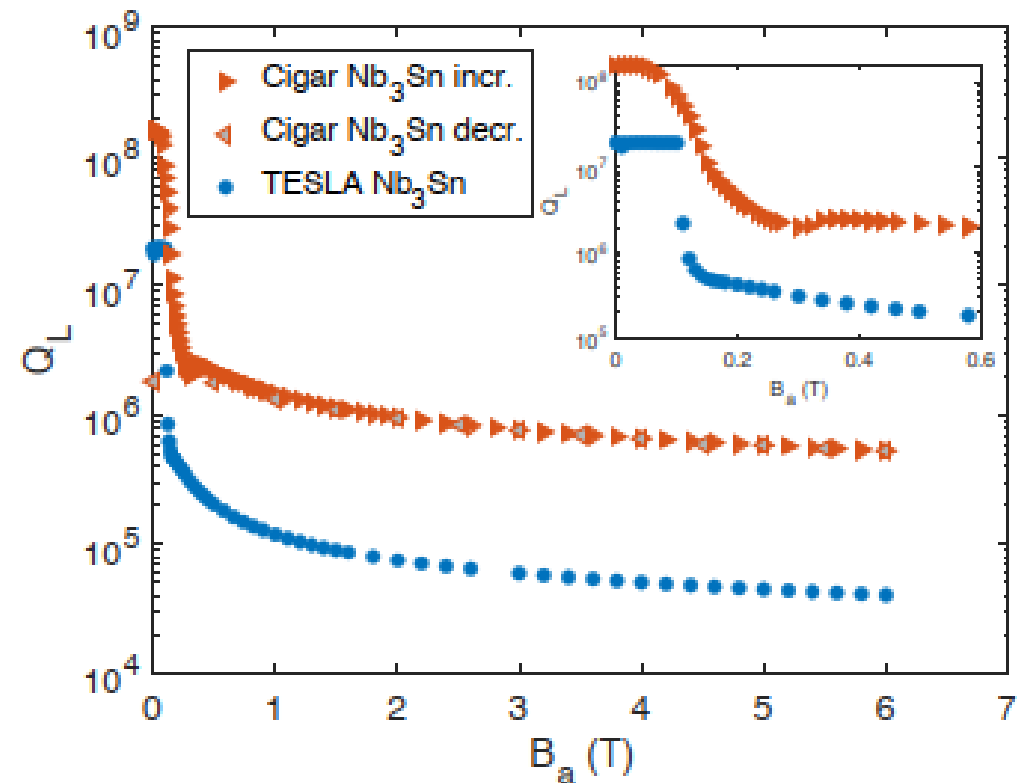
Cigar-shaped cavity 3.9 GHz



1-cell ILC type 3.9 GHz



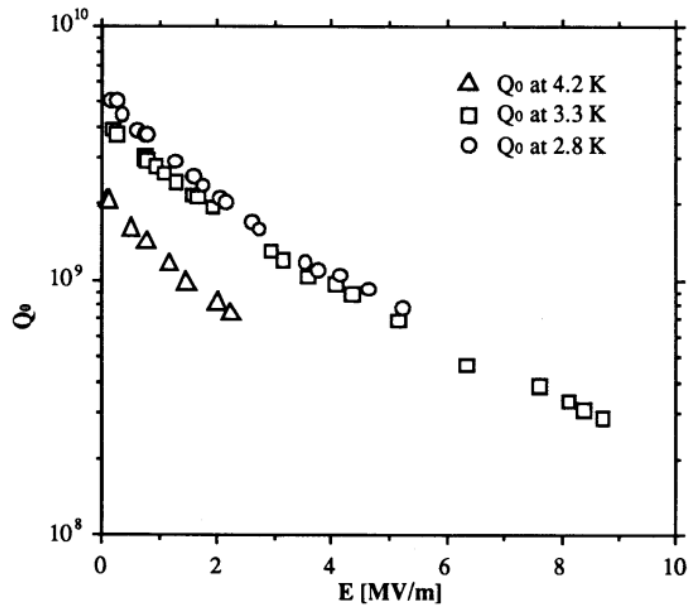
S. Posen et al. ArXiv 2201.10733



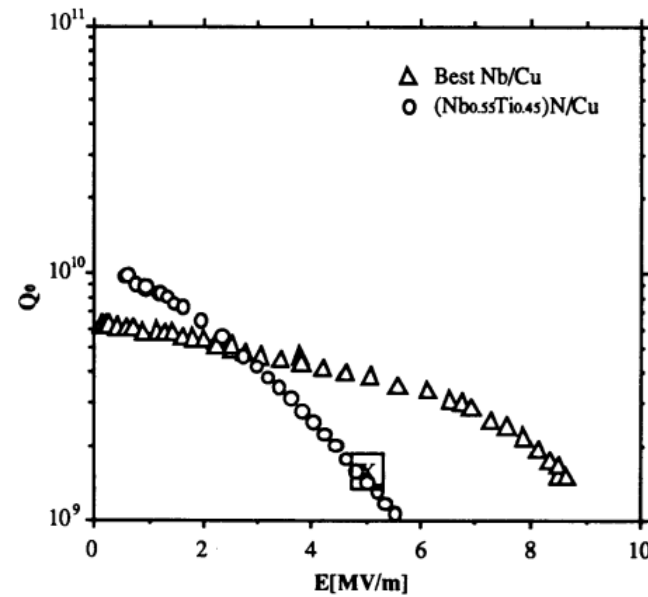
Ideally, Nb₃Sn from vapor tin diffusion should then be compared to Nb₃Sn from sputtering

NbTi / NbTiN and Nb₃Sn at high RF field

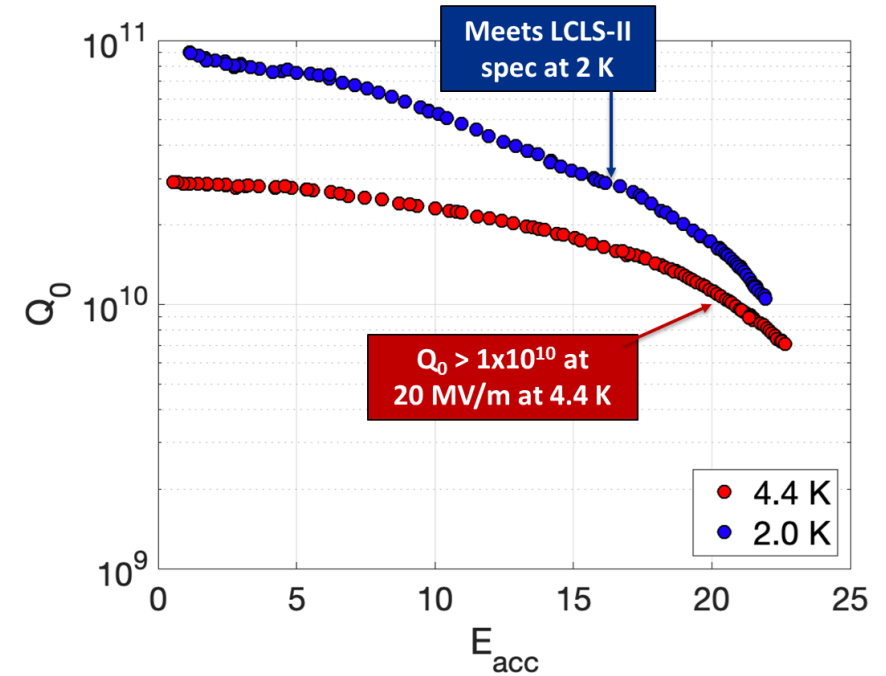
NbTi 500 MHz



NbTiN 500 MHz, 4.2 K



S. Calatroni et al., Proc of the SRF 91



S. Posen – FNAL (TTC 2019 talk)