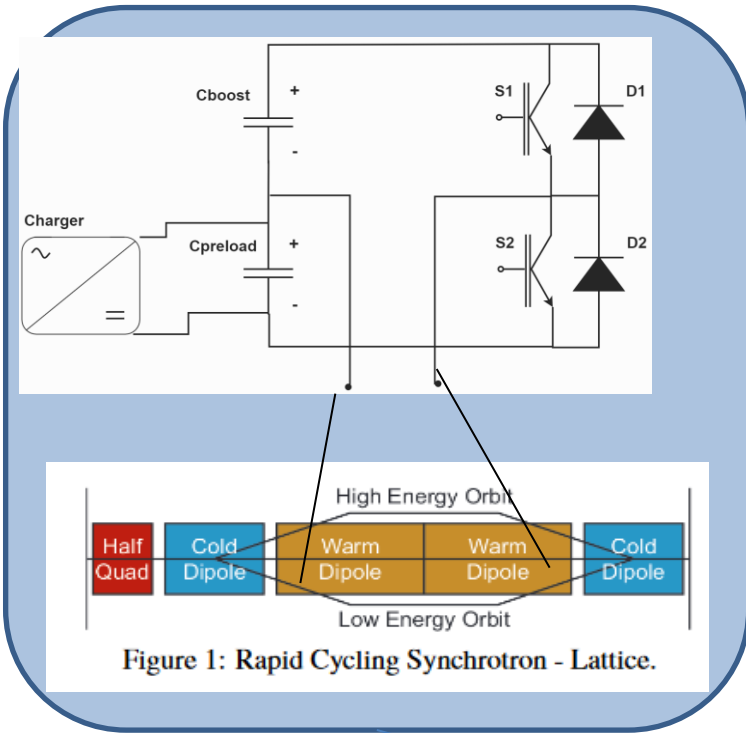


International
UON Collider
Collaboration

Technology options for the accelerator powering

F. Boattini D. Aguglia
21.June.23

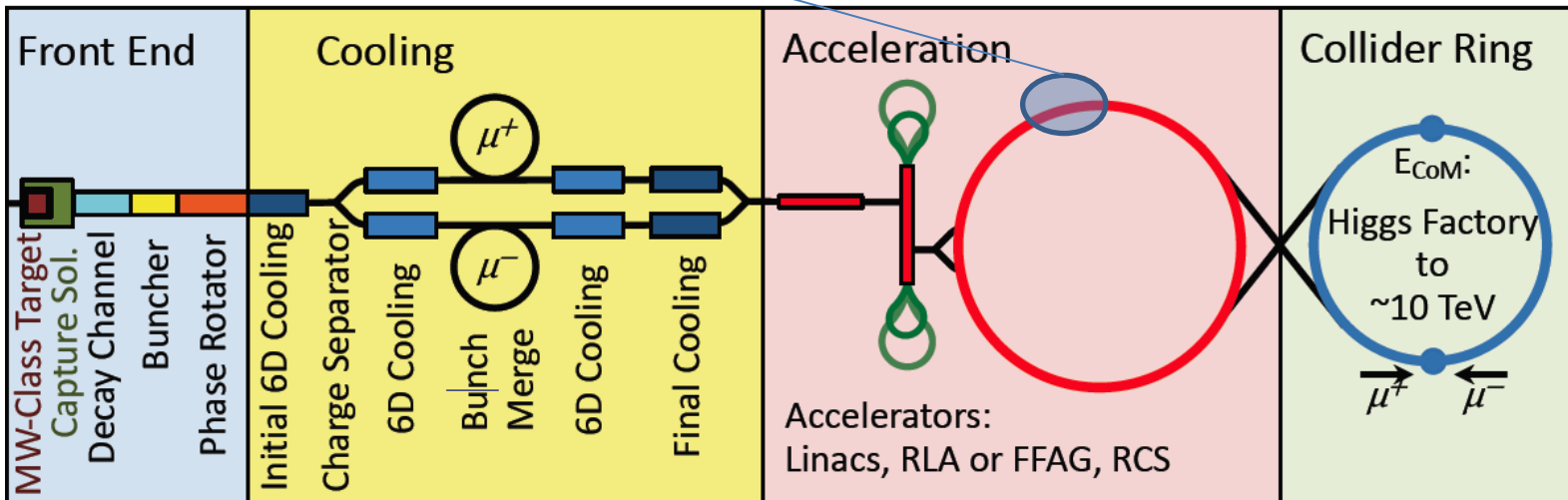
Critical systems and main- specifications



The powering system is very interlinked with the resistive magnets design

| | RCS1 | RCS2 | RCS3 | RCS4 |
|------------------------|------|------|------|-------|
| Inj Energy [GeV] | 63 | 314 | 750 | 1500 |
| Acc. length [km] | 5.99 | 5.99 | 10.7 | 35.0 |
| Res. mags Lm [km] | 3.65 | 2.54 | 4.37 | 20.38 |
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| Dipoles Gap w [mm] | 100 | 100 | 100 | 100 |
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| Dipoles Pmax [GW] | 111 | 54 | 43 | 74 |

The key performance drivers are directly related to the total energy and power to be delivered to the magnets, but also to the tracking accuracy that will have to be guaranteed. This input should come from the beam studies

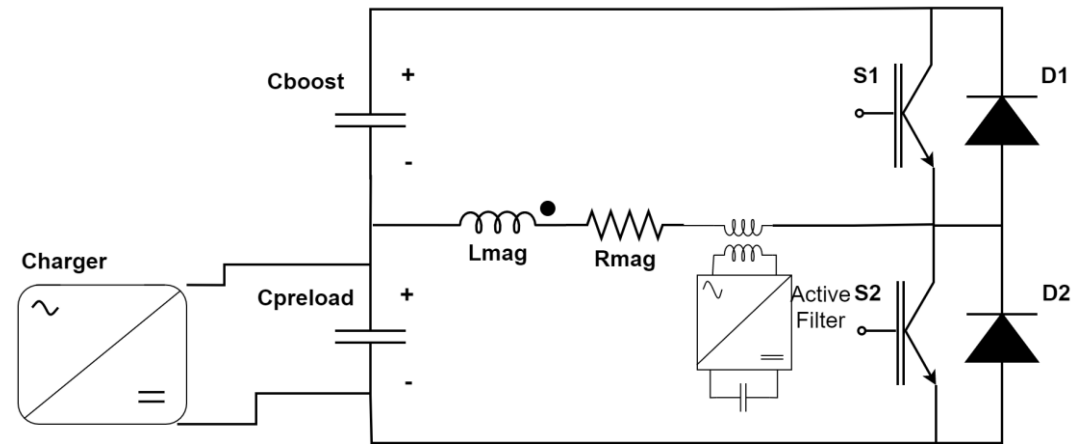
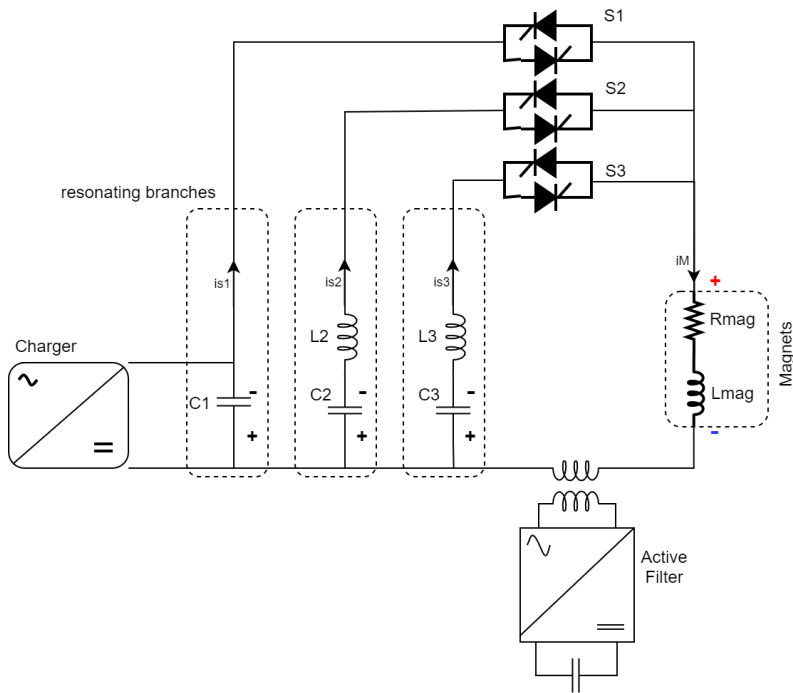


Evaluation of technology options

| Technology | Pro's | Con's |
|--------------------------------------|---|---|
| Full Wave resonance powering scheme | <p>Minimization of storage energy</p> <p>Power electronics based on thyristors.</p> <p>Example (with smaller power) available in the literature.</p> | <p>Low energy density in capacitor dimensioning</p> <p>Low versatility towards changing of the operating conditions.</p> <p>The control of the inter-sector tracking is more complicated.</p> <p>Higher saturation of magnet is in general required</p> |
| Commutated resonance powering scheme | <p>Unipolar only capacitor excitation.</p> <p>Higher energy density</p> <p>More versatile schema with possibility to modify the Bref shape within a range.</p> <p>No inductive energy store components are required</p> | <p>Important R&D for the development of an IGBT/IGCT based switching leg.</p> <p>Possibly higher losses on magnets (depending upon final layout)</p> |
| Capacitor as storage elements | <p>Very fast discharge and very high current peaks are possible, particularly in plastic capacitors</p> | <p>Particularly with voltage polarity reversal, the correct energy density is difficult to estimate.</p> |
| Spatial harmonic distribution | <p>Simpler pure sinusoidal discharge</p> | <p>Not clear how we should consider the integral field at different harmonics</p> |

Selected options and priorities ranking

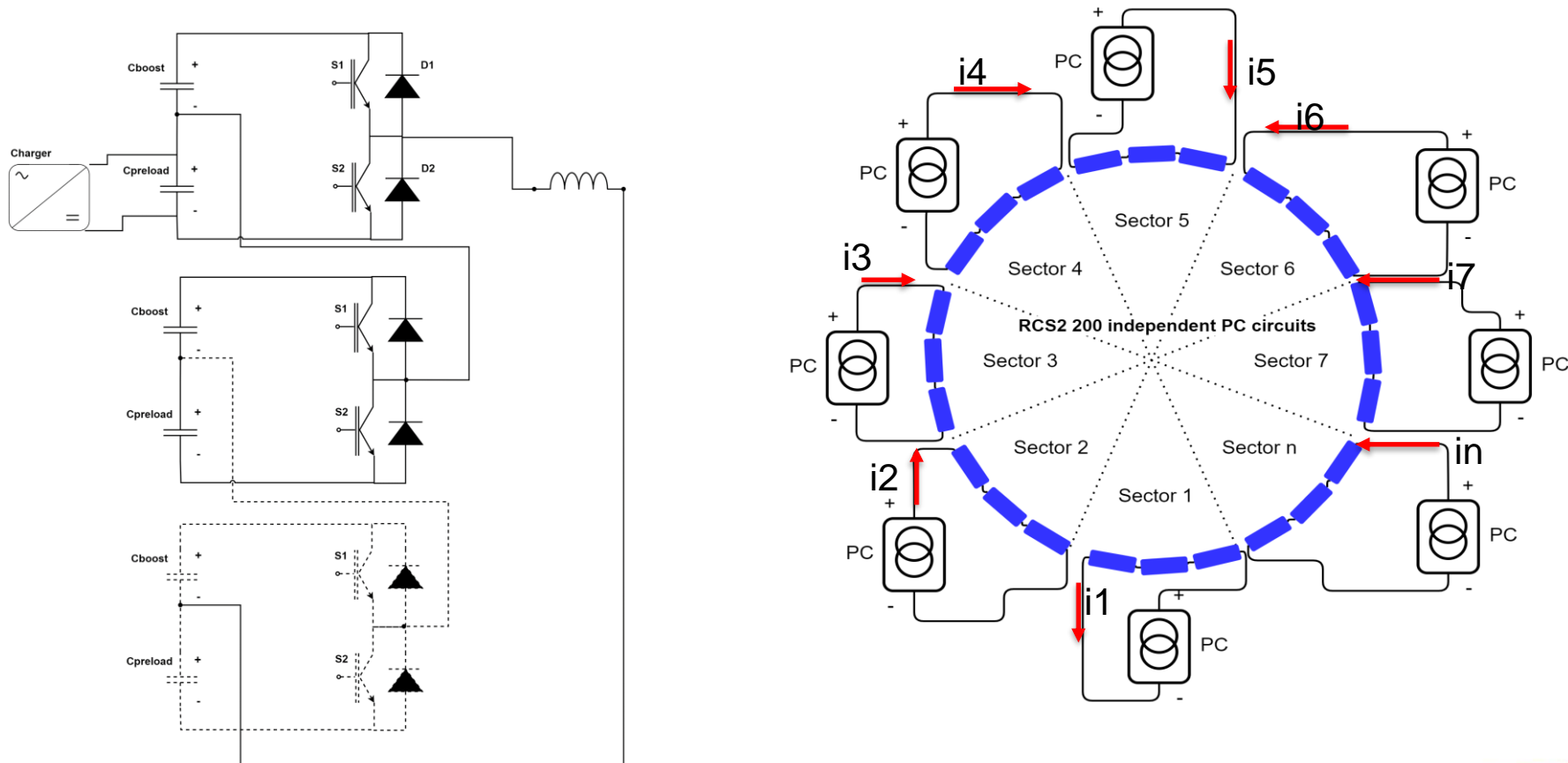
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Circuit simulation will be carried on to better frame the control problem. To this goal it is of paramount importance to have an idea of the accuracy that will be required. This input should come from the physics studies.



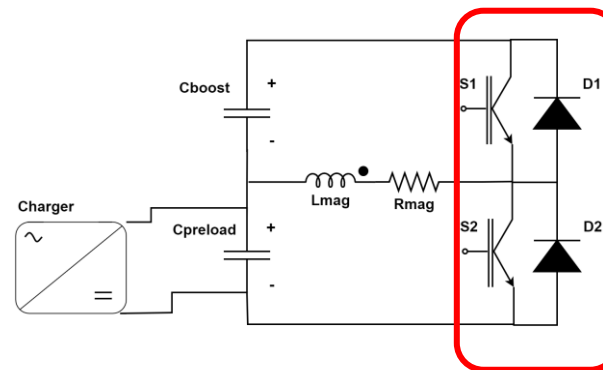
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Simplified magnet models for the calculation of the losses and the electric equivalents are under design. The use of machine learning techniques are under discussion as a mean to determine losses model of the magnets. Magnet models will be progressively employed in powering-magnets optimizers that will guide the final technical choices for both the systems.

Design of the IGCT/Thyristors switch shall proceed as the final power scheme layout becomes better defined



Selected options and priorities ranking

A zoo of test benches - 3

- Custom-winding permeameter



Vitroperm500F. Non-standard dimensions and very-high permeability (about 80,000)

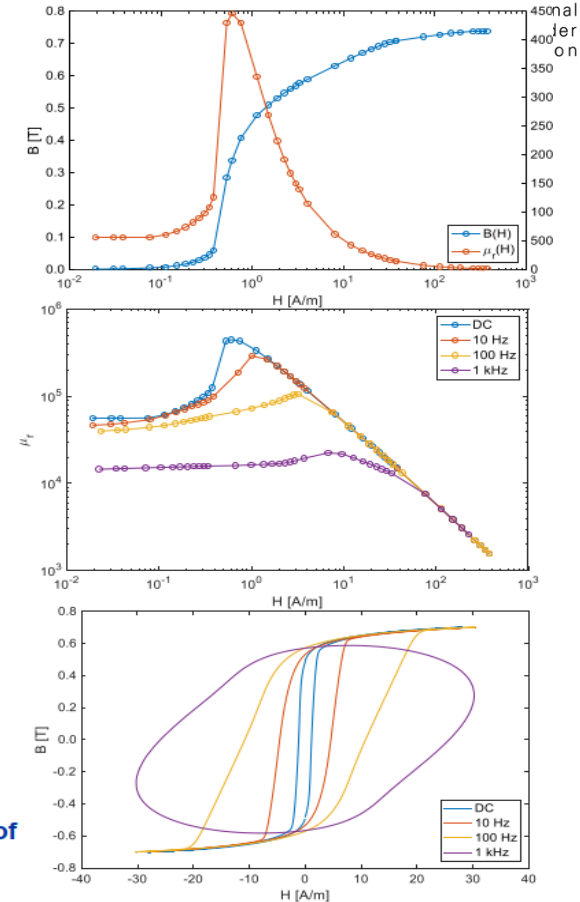


Mu-metal sample in the holder

- Manual winding of the coils allows to cover what the split-coil permeameter can't do
 - **Very-high permeability materials (i.e. mu-metals)**
 - Fewer excitation turns can be used to measure low magnetic fields (<10 A/m) by using conveniently high currents.
 - Dynamic characterization possible up to 1 kHz for some materials
 - **Non-standard sized toroids**
- **It works at cryogenic temperatures!**

Courtesy of Marco Buzio and his team

Characterization of Mu-Metal for CLIC



In parallel to all above, magnetic material characterization tests should be organized. Methodology under discussion

Selected options and priorities ranking



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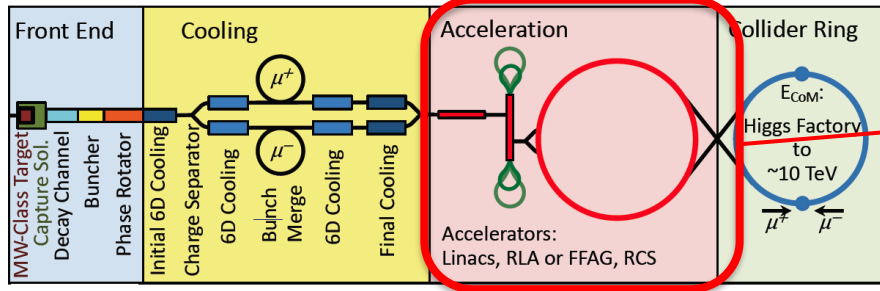
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Task3 working plan

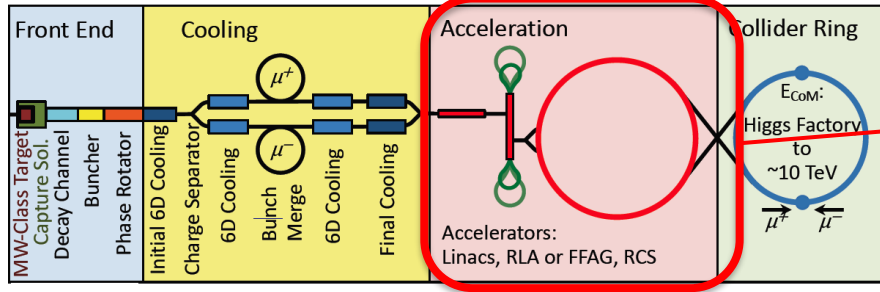


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Task3.1: Resistive magnets and power system

- Optimal design of resistive dipoles and quadrupole with emphasis on minimization of energy content and losses. Basic effect of the vacuum chamber should be considered. Simplified analytical model will also be developed to be used within the full optimization
 - Who: (UNIBO: M. Breschi). When: first version January 2024; draft final version September 2025; final study results September 2026
- Analysis of magnet optimized designs with 2D and 3D time dependent FEM simulations. These models will focus on most promising design options and address important calculations as losses, field quality, electrodynamic effects, saturation effects etc...
 - Who (TUDa H. De Gersem). When: first version January 2024; draft final version September 2025; final study results September 2026
- Integrated power system / magnets optimization to minimize the total power requirements / cost and land occupation (CERN, LNCMI). Evaluation of different powering concepts based on full wave and/or switched resonance.
 - Who: F. Boattini (CERN), J. Beard (LNCMI). When: first version mid 2024; updated version mid 2025; final study results September 2026
- Cost and power estimate
 - Who: F. Boattini (CERN), M. Breschi (UNIBO), H. De Gersem (TUDa), L. Bottura (CERN), S. Fabbri (CERN), L. Quettier (CEA). When: draft version June 2025; final version June 2027
- Testing of soft magnetic material at high frequency and high magnetic field. The study will help modelling the resistive magnets
 - Who: The team is under formation

Task3 working plan



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Task3.2: Superconducting magnets

- Study suitable geometries and materials for fields in the hypothesis of magnetic fields in the range of 8...10T. Look at impact on accelerator layout (e.g. limiting maximum to 8 T), aperture and winding options (e.g. rectangular vs. round aperture). Basic 2D electromagnetic design
Who: L. Bottura (CERN), S. Fabbri (CERN), M. Breschi (UNIBO)
- HTS option for fast pulsed dipoles. Scoping studies for dB/dt in the range of 300T/s and Bgap > 2T
Who: A. Kario, H. Ten Kate (TWENTE), FNAL cooperation
When: to be defined. Possibly for the next IMCC?