



Lattice design of 250 MeV version of PERLE

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Motivation for 250 MeV version (pros and cons)

Lattice design (maximal compatibility with 500 MeV design prepared by Alex Bogacz)

Optics (comparison with 500 MeV version)

Filling patterns (optimal for lower energies)

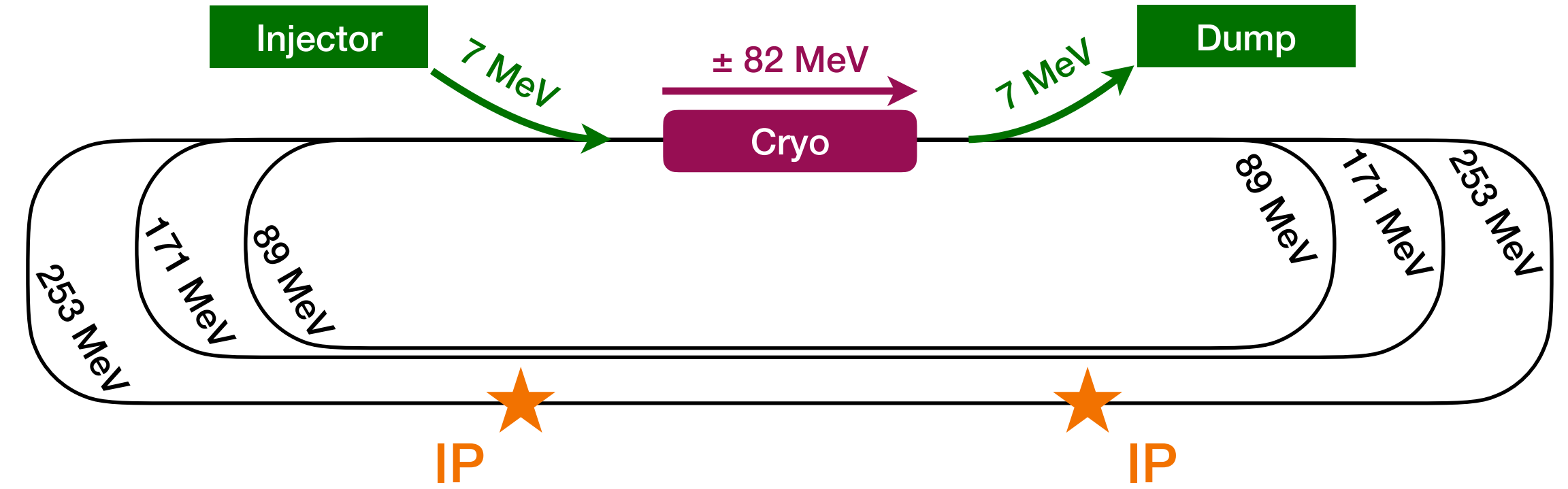
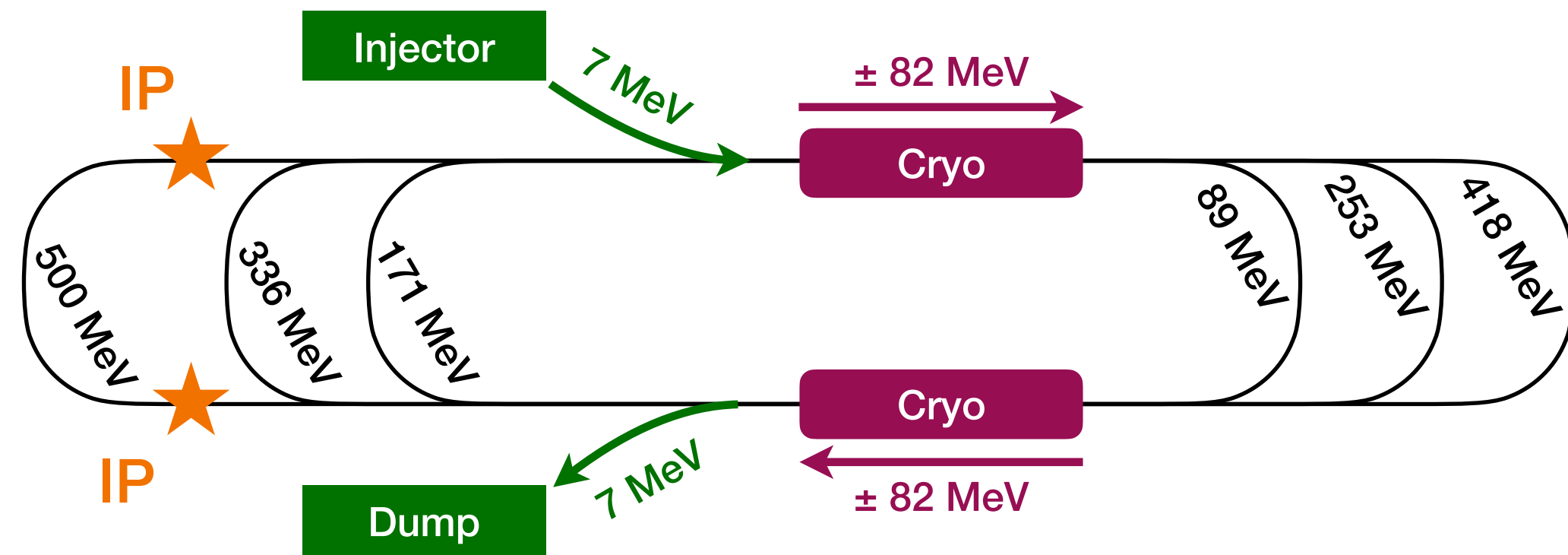
Conclusions



Motivation for one cryo-module phase (250 MeV versions)



250 MeV version features three Straight Sections replacing Recombiner, Common Section 2, and Spreader



Pros:

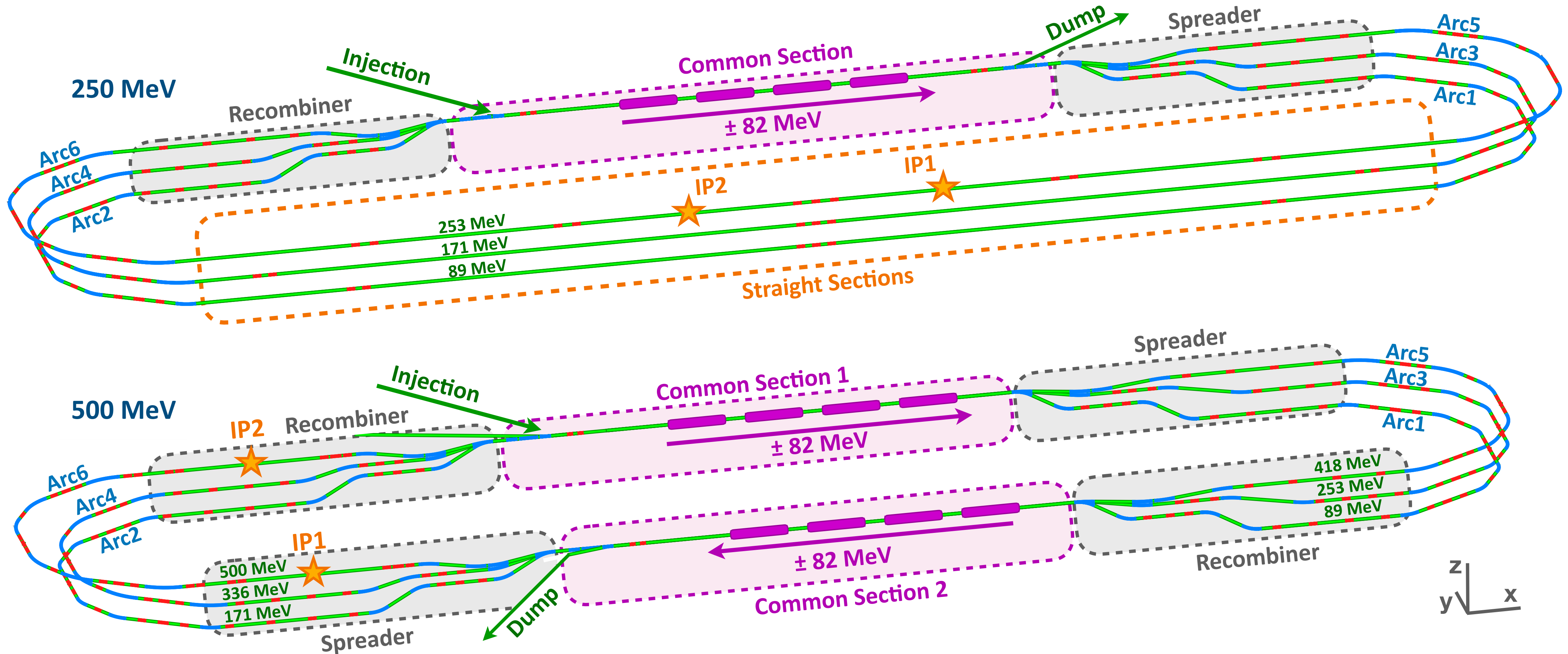
- **reduction of immediate expenses (time for the first results)** (second cryo-module and 18 dipoles can be purchased later)
- **demonstration of ERL with 6 paths at high current** (same as in 500 MeV version, but with half of the power)
- more space for experimental areas

Cons:

- **additional expenses / manpower / shutdown time** (rebuilding / recommissioning for the full power machine)
- about 30 meters of extra beam pipes (all other main elements are chosen to be compatible with both versions)
- a slightly larger footprint (28.6 m → 29.9 m)



Lattice design. 500 MeV vs 250 MeV versions



All elements are compatible with both versions !

250 MeV version features **three Straight Sections** replacing **Recombiner**, **Common Section 2**, and **Spreader**



Types of dipoles (optics v2.0 → 2.1) 250 MeV vs 500 MeV



The dimensions of dipoles were slightly adjusted in order to reduce the variety of magnets → In optics v2.1 there are 7 types of magnets

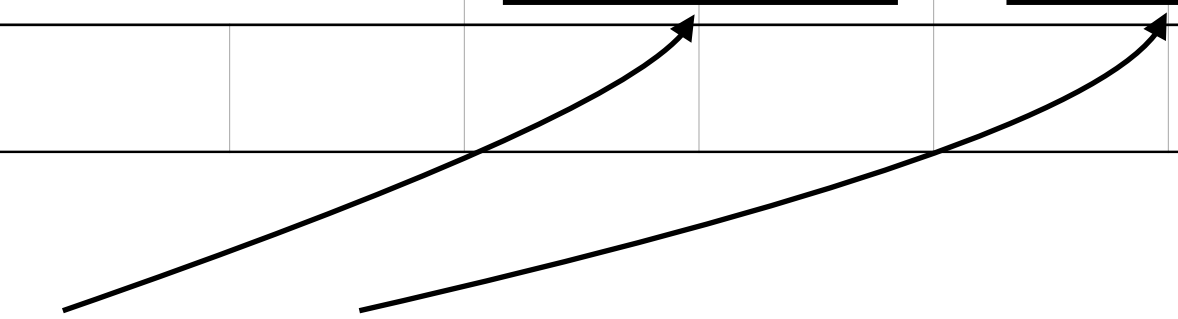
Type	Name	Plane	Number		Function	Geometry	L, cm	Deflection, deg		B , T		I, mA	
			v.250	v.500				min	max	min	max	min	max
1	Chicane 15cm	hor.	4		Injection and Dump /spreader/correctors/merger	R-Bend	15	0.2	15	0.040		100	120
2	Chicane 30cm	hor.	2		corrector with double length and inverted field (w.r.t. Type 1)	R-Bend	30	0.4	2.3	0.040		100	120
3	B-Com 3-lines	vert.	2	4	spreaders/recombiners for 3 energy lines (for all Arcs)	R-Bend	33	6.1	30	0.451	0.866	100	120
4	B-Com 2-lines	vert.	2	4	spreaders/recombiners for 2 energy lines (for Arcs 3, 5 & 4, 6)	R-Bend	33	6.1	15.1	0.451	0.866	60	80
5	R-Bend 33cm	vert.	8	16	spreaders (one energy line) for Arcs 3, 4, 5 & 6	R-Bend	33	6.1	15.1	0.451	0.873	20	40
6	S-Bend 33cm	vert.	6	12	spreaders (one energy line) for Arcs 1 & 2	S-Bend	33	30		0.472	0.907	40	
		hor.	18		180° turn of the Arc 1, 2, 3 (6 dipoles per Arc)	S-Bend	33	30		0.472	1.342	20	40
7	S-Bend 66cm	hor.	18		180° turn of the Arc 4, 5, 6	S-Bend	66	30		0.453	1.323	20	40
Total			60	78									

Total number of dipole (ERL only)

- 60 dipoles for 250 MeV version
- 78 dipoles for 500 MeV version

- the required magnetic field (and beam current) might vary by the factor 2—3 (and 2 respectively) within the same Type of dipole
- “S-Bend 33cm” at the Spreader/Recombiner sections is in **vertical** orientation and in **horizontal** at the Arcs

Is it possible to have the same dipole design?





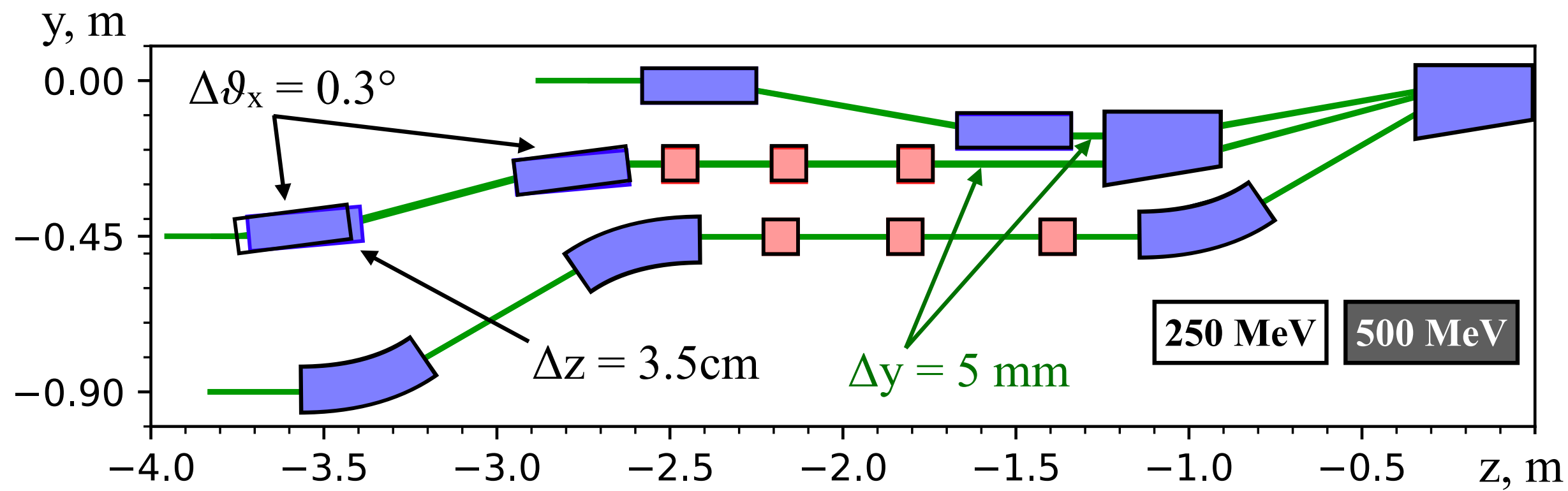
Spreaders / Recombiners / Arcs 250 MeV vs 500 MeV



The ratio of the energies in 250 MeV version is very close to the one in Arcs 2,4,6:

$$\Delta E \approx 82 \text{ MeV}$$

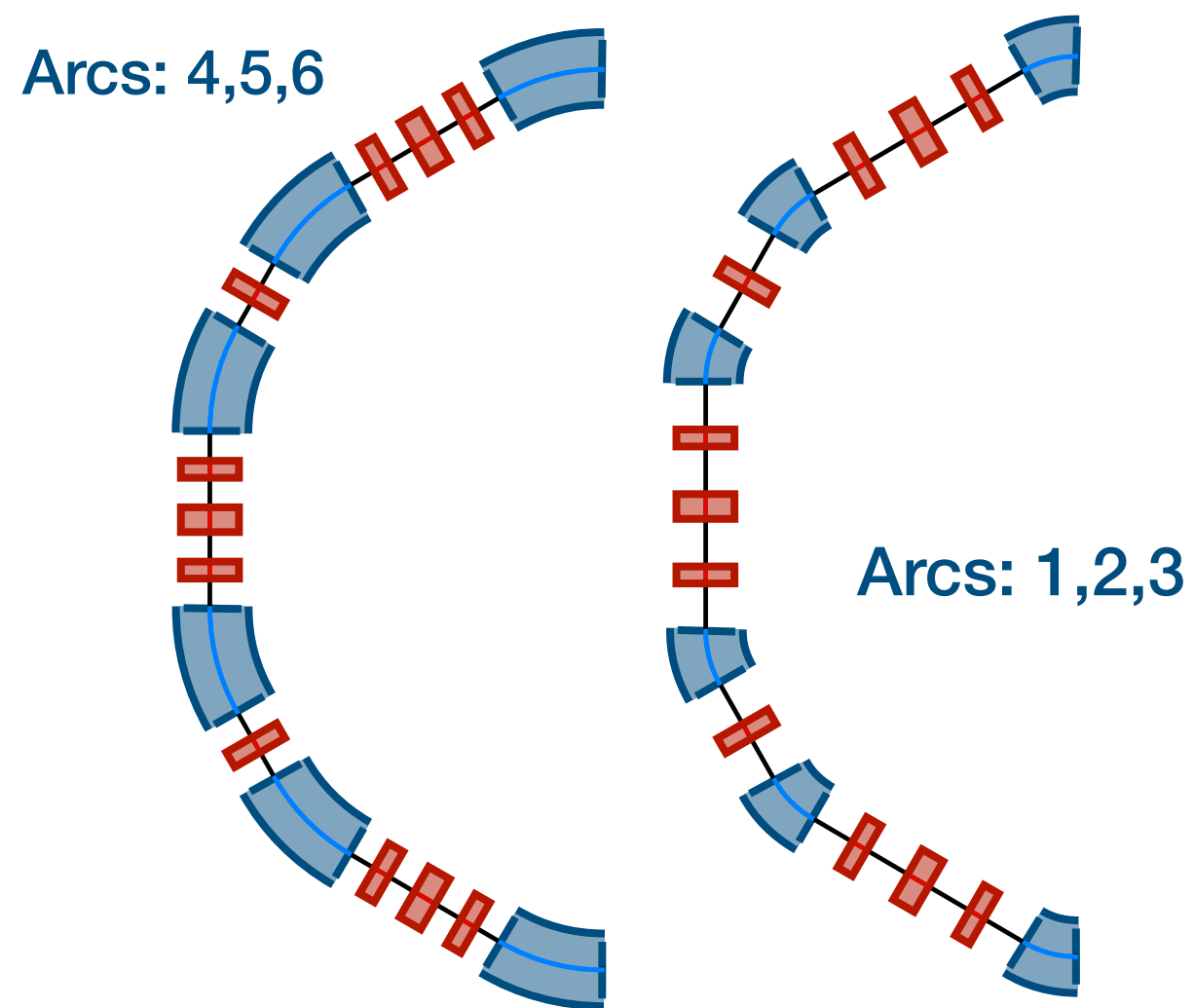
$$E_0 \approx 7 \text{ MeV}$$



$$\Delta E + E_0 : 2\Delta E + E_0 : 3\Delta E + E_0 \approx 1 : 1.92 : 2.84$$

$$2\Delta E + E_0 : 4\Delta E + E_0 : 6\Delta E + E_0 \approx 1 : 1.96 : 2.92$$

- we can use the same magnets,
- the lattice should be adjusted



All six arcs are chosen to be **the same** as in 500 MeV version (**for compatibility**)

- lengths of dipoles are 33 cm (at arcs 1, 2 & 3) and 66 cm (at arcs 4, 5 & 6)

If designing 250 MeV version **from scratch** (no compatibility with 500 MeV)

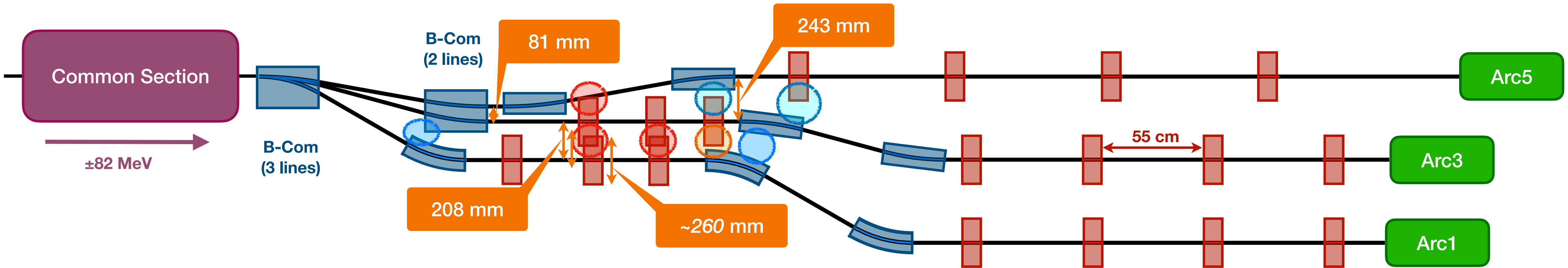
- all dipoles at arcs would be 33 cm (**18 shorter magnets**)
- arcs could be slightly shorter → **smaller footprint**

Distance between the Arcs and Spreaders should be adjustable

- to form an optimal filling pattern, i.e. placement of accelerated bunches between the injected bunches
- tune phase adjustment between accelerations at RF cavities



Spreaders / Recombiners — Space constrain

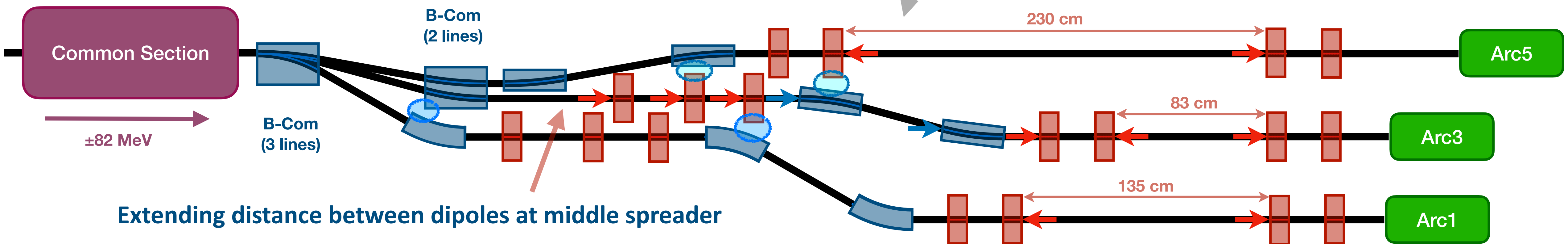


Two-step beam separation/recombining (proposed by A. Bogacz)

- reduction of dispersion (quadruple triplet between dipoles)
- distance between the beam pipes < size of the quadrupoles (current design)

Grouping into two doublets

- more space for instrumentation (if needed)
- possibility to host IRs at the spreader (like 500 MeV)
- not enough to install chicanes (phase adjustment for RF)



Extending distance between dipoles at middle spreader

- no overlap of quadrupoles

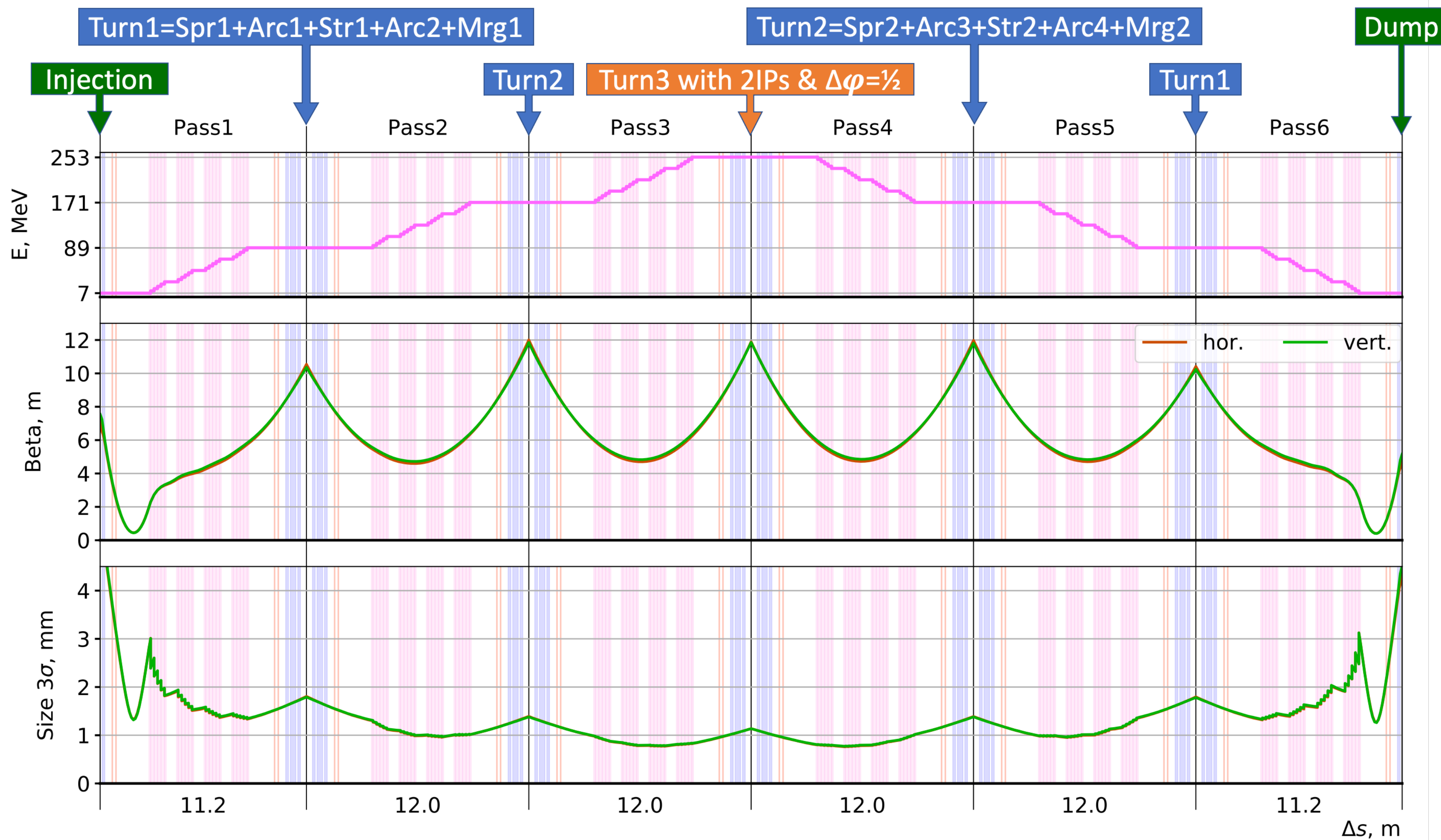


Optics

(comparison with 500 MeV version)



Optics comparison 250 & 500 MeV versions





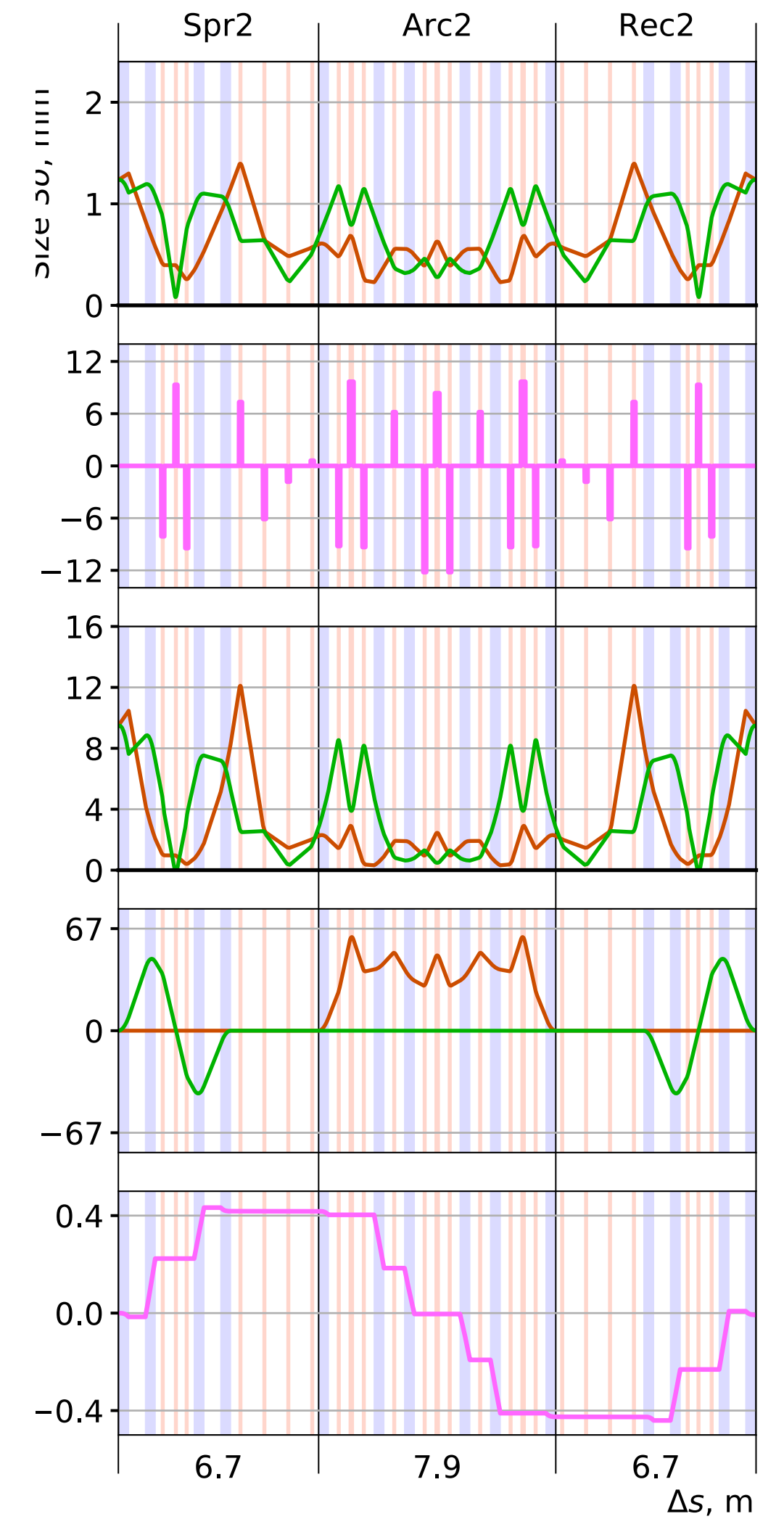
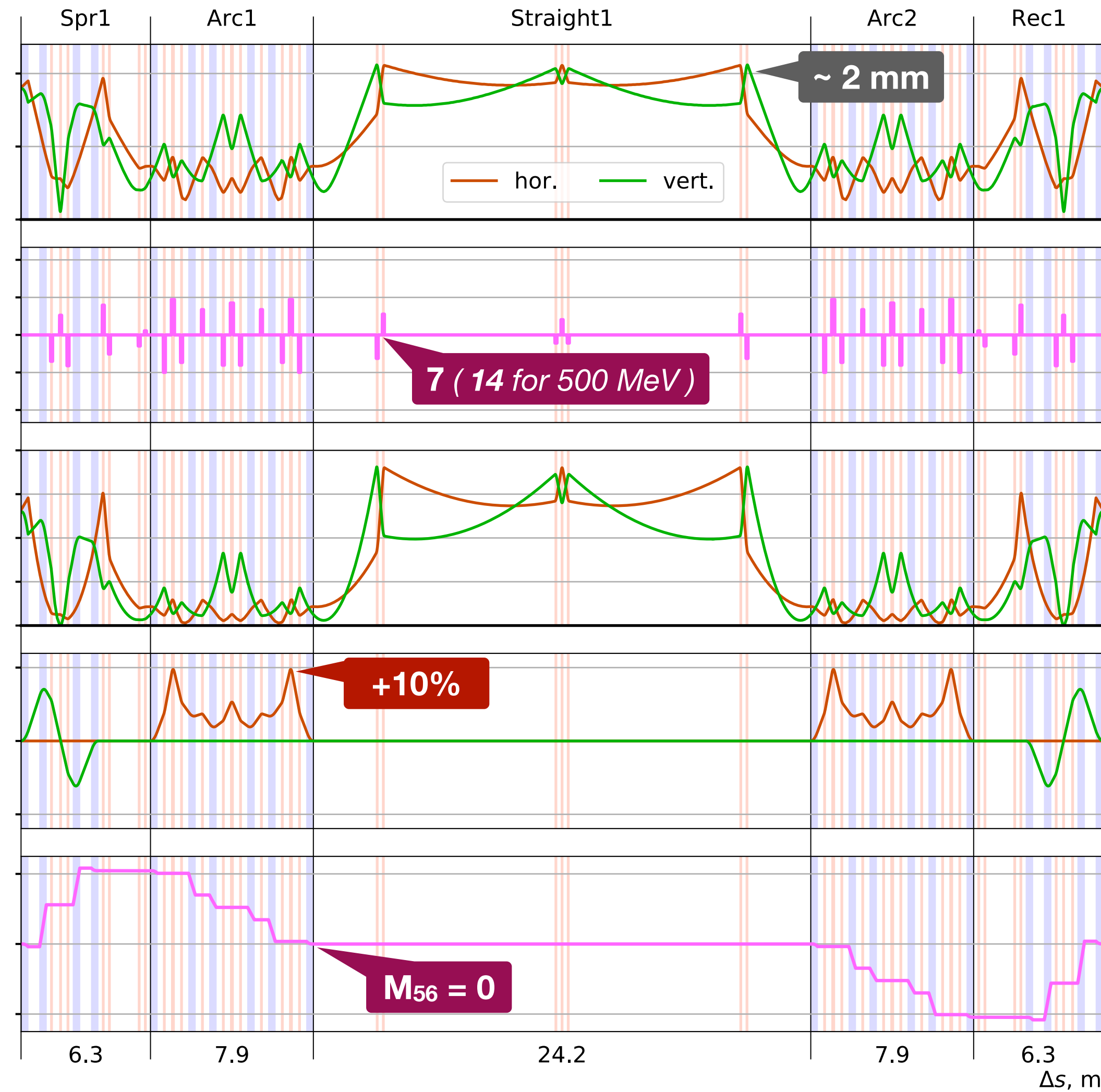
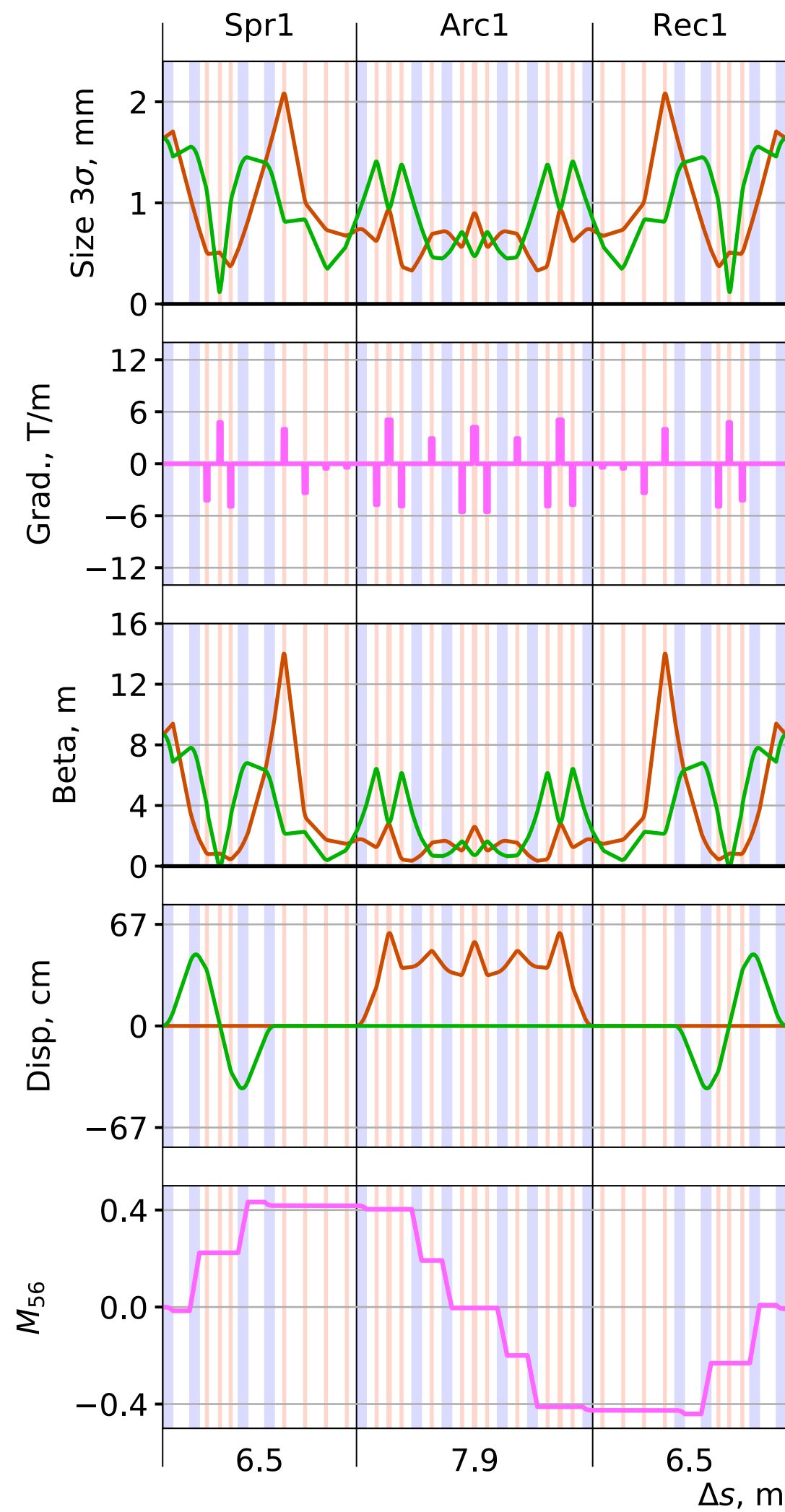
Optics comparison 250 & 500 MeV versions



500 MeV (Arc1, 89 MeV)

250 MeV (Arc1+Arc2, 89 MeV)

500 MeV (Arc2, 171 MeV)





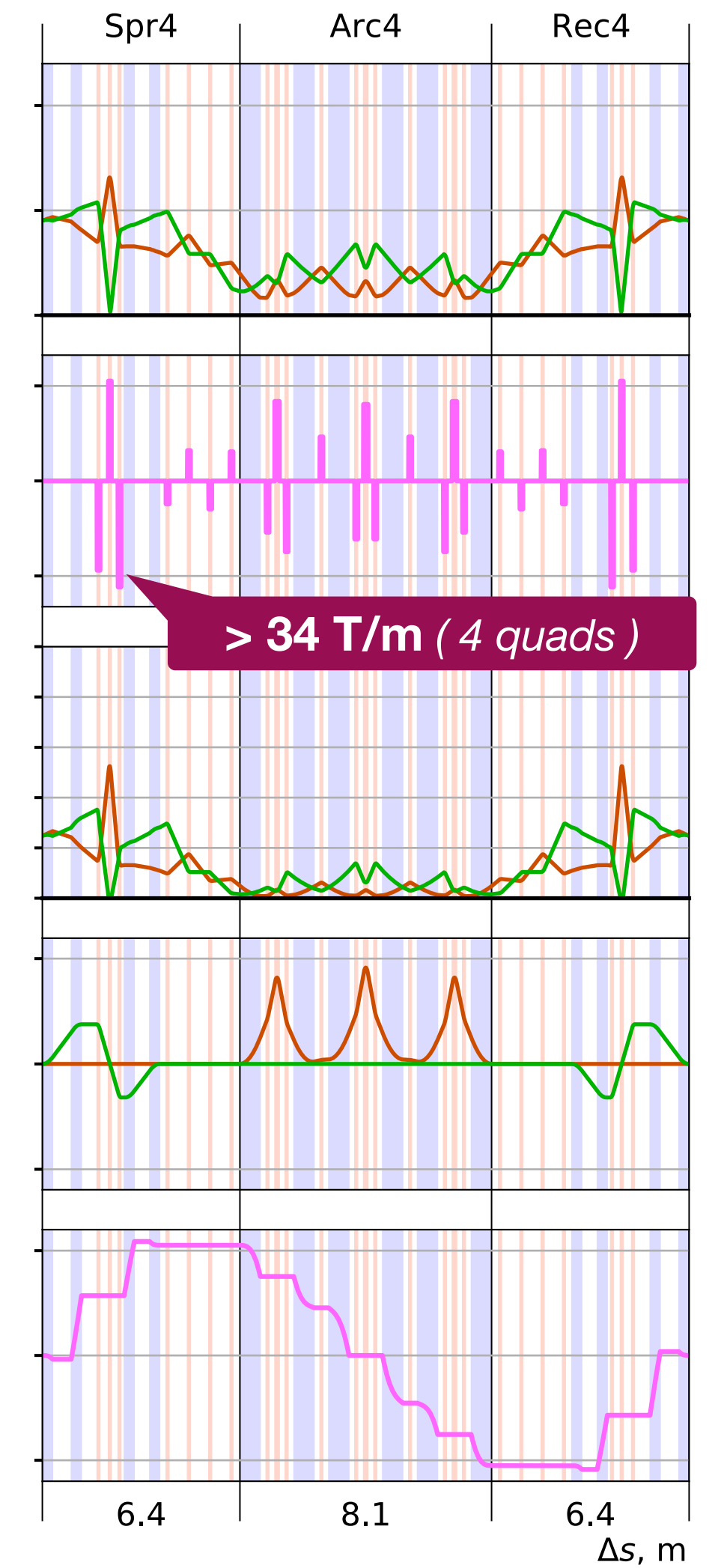
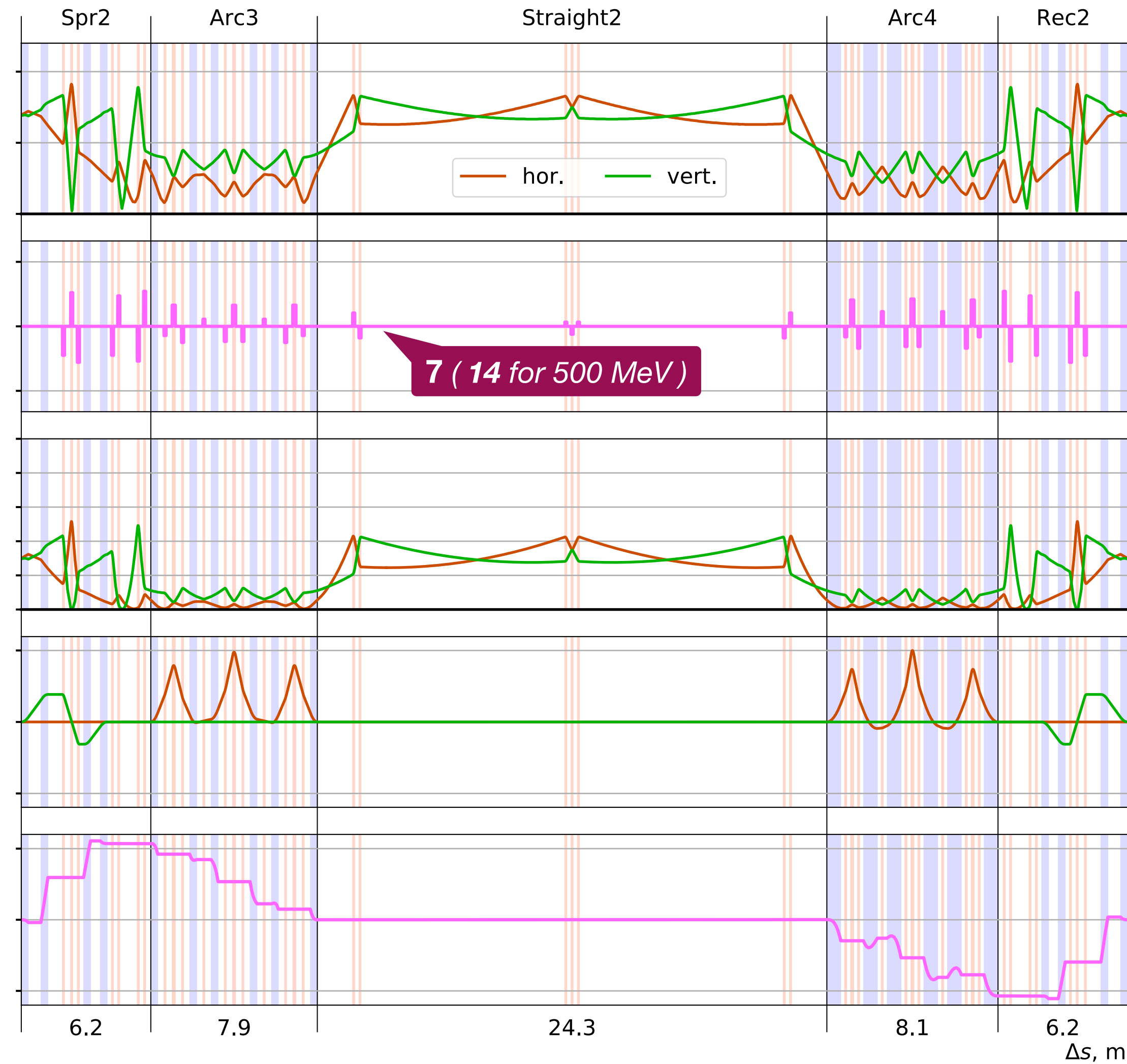
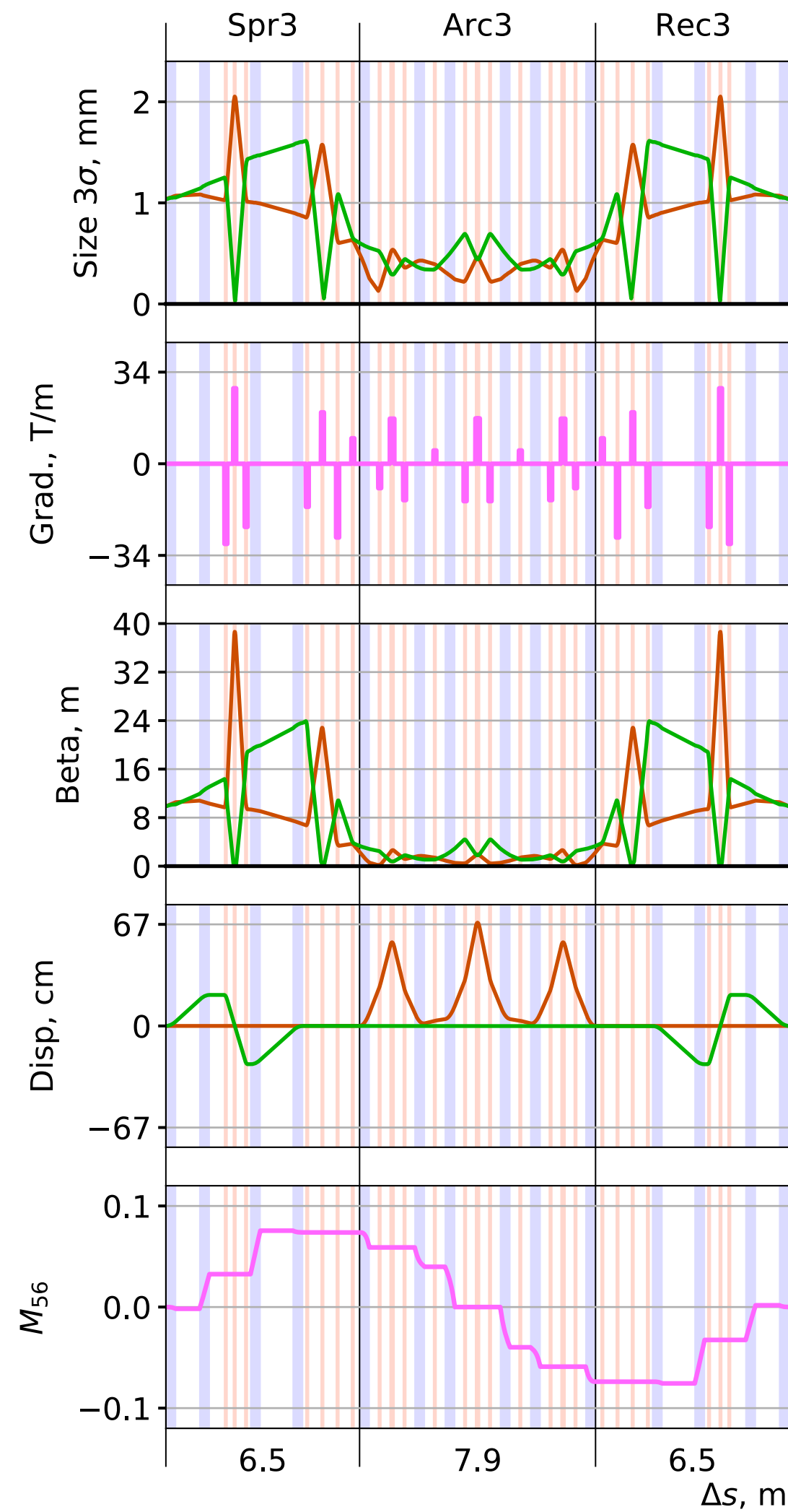
Optics comparison 250 & 500 MeV versions



500 MeV (Arc3, 253 MeV)

250 MeV (Arc3+Arc4, 171 MeV)

500 MeV (Arc4, 336 MeV)





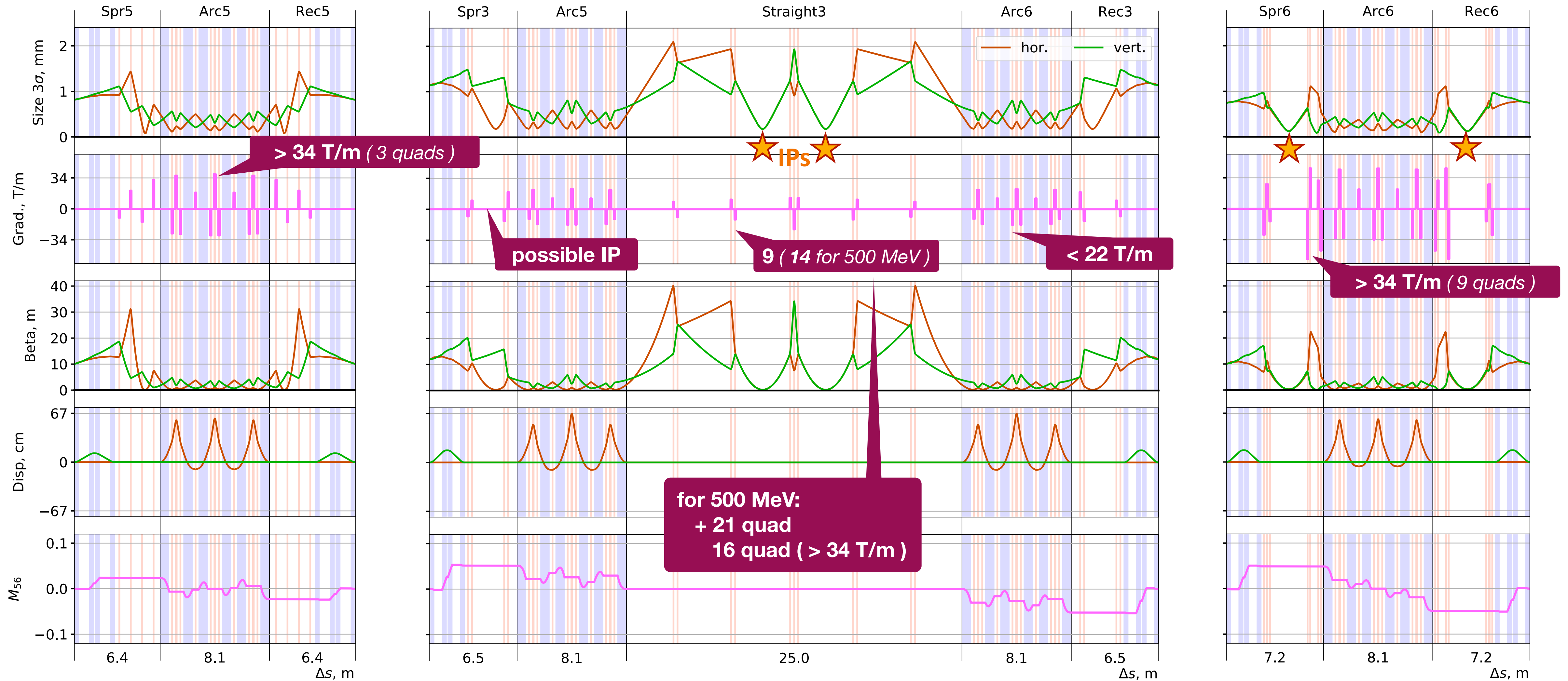
Optics comparison 250 & 500 MeV versions



500 MeV (Arc5, 418 MeV)

250 MeV (Arc5+Arc6, 253 MeV)

500 MeV (Arc6, 500 MeV)





Filling pattern

(size of the Arcs)



Forming the Filling Pattern. Injection and Pass 1



Pass 1

Injection

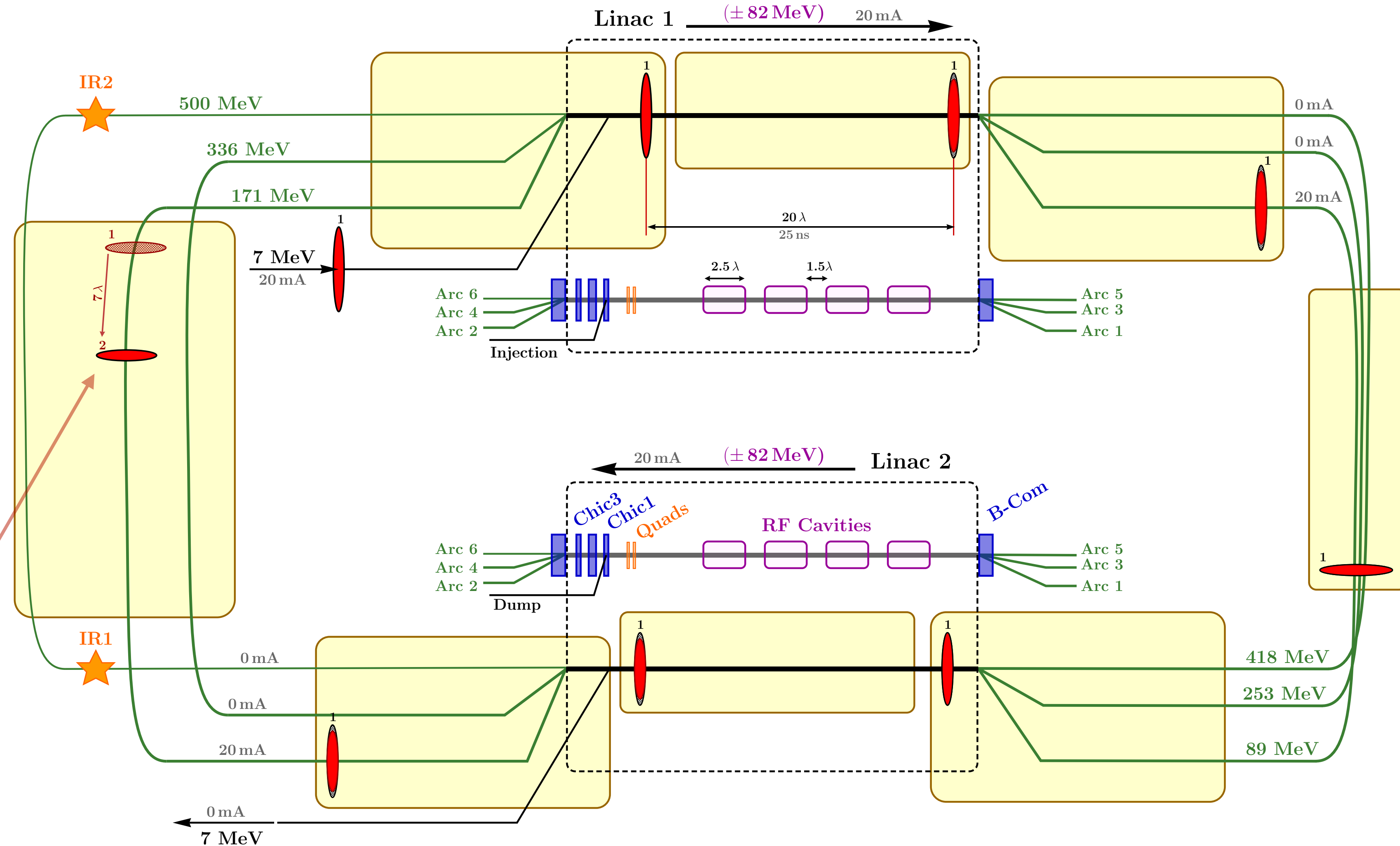
7 MeV bunches are injected at Linac 1 section
 at the rate of $\nu_{inj} \approx 40$ MHz (every $t_{inj} = 25$ ns)
 target current is $I = 20$ mA
 → charge of one bunch $Q \approx 500$ pC ($3 \times 10^9 e^-$)

RF Cavity ($V_{RF} = 801.58$ MHz)

→ spacing between injections $L_{inj} = 20 \lambda_{RF}$
 $V_{RF} / V_{inj} = 20$, $\lambda_{RF} \approx 34.7$ cm

Pass 1 Linac 1 → Arc 1 → Linac 2 → Arc 2
 7 → 89 MeV 89 → 171 MeV

Pass 1 length (Arc1 + Arc2 + 2 Linac) $L_{Pass 1} = 167 \lambda_{RF}$
 → the 9th injected bunch is followed by the accelerated bunch shifted by $7 \lambda_{RF}$





Forming the Filling Pattern. Passes 1 & 2



Passes 1-2

Injection

7 MeV bunches are injected at Linac 1 section at the rate of $\nu_{inj} \approx 40$ MHz (every $t_{inj} = 25$ ns) target current is $I = 20$ mA
 → charge of one bunch $Q \approx 500$ pC ($3 \times 10^9 e^-$)

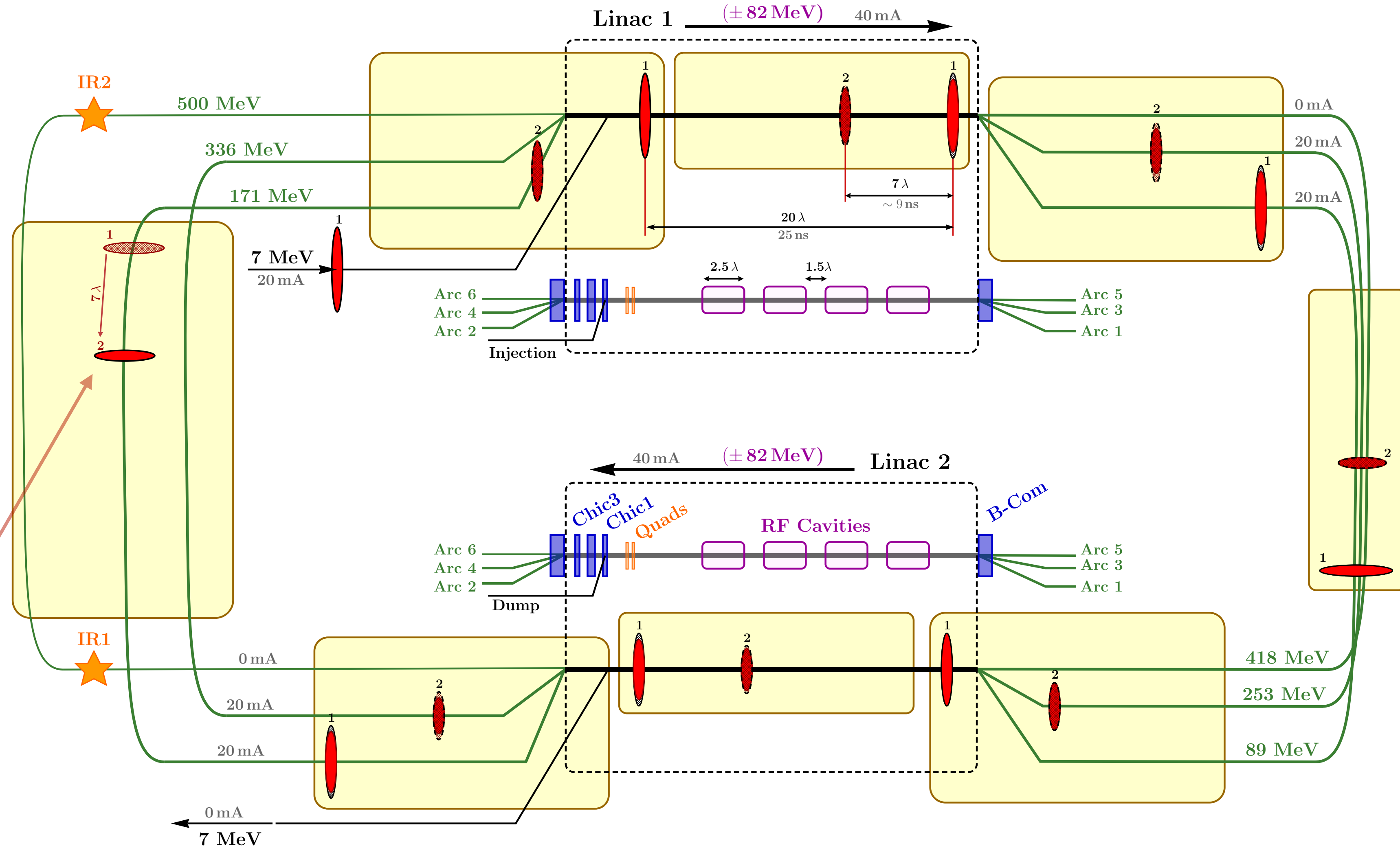
RF Cavity ($V_{RF} = 801.58$ MHz)

→ spacing between injections $L_{inj} = 20 \lambda_{RF}$
 $V_{RF} / V_{inj} = 20$, $\lambda_{RF} \approx 34.7$ cm

Pass 1 Linac 1 → Arc 1 → Linac 2 → Arc 2
 7 → 89 MeV 89 → 171 MeV

Pass 1 length (Arc1 + Arc2 + 2 Linac) $L_{Pass 1} = 167 \lambda_{RF}$
 → the 9th injected bunch is followed by the accelerated bunch shifted by $7 \lambda_{RF}$

Pass 2 Linac 1 → Arc 3 → Linac 2 → Arc 4
 171 → 253 MeV 253 → 336 MeV





Forming the Filling Pattern. Passes 1–3



Passes 1–3

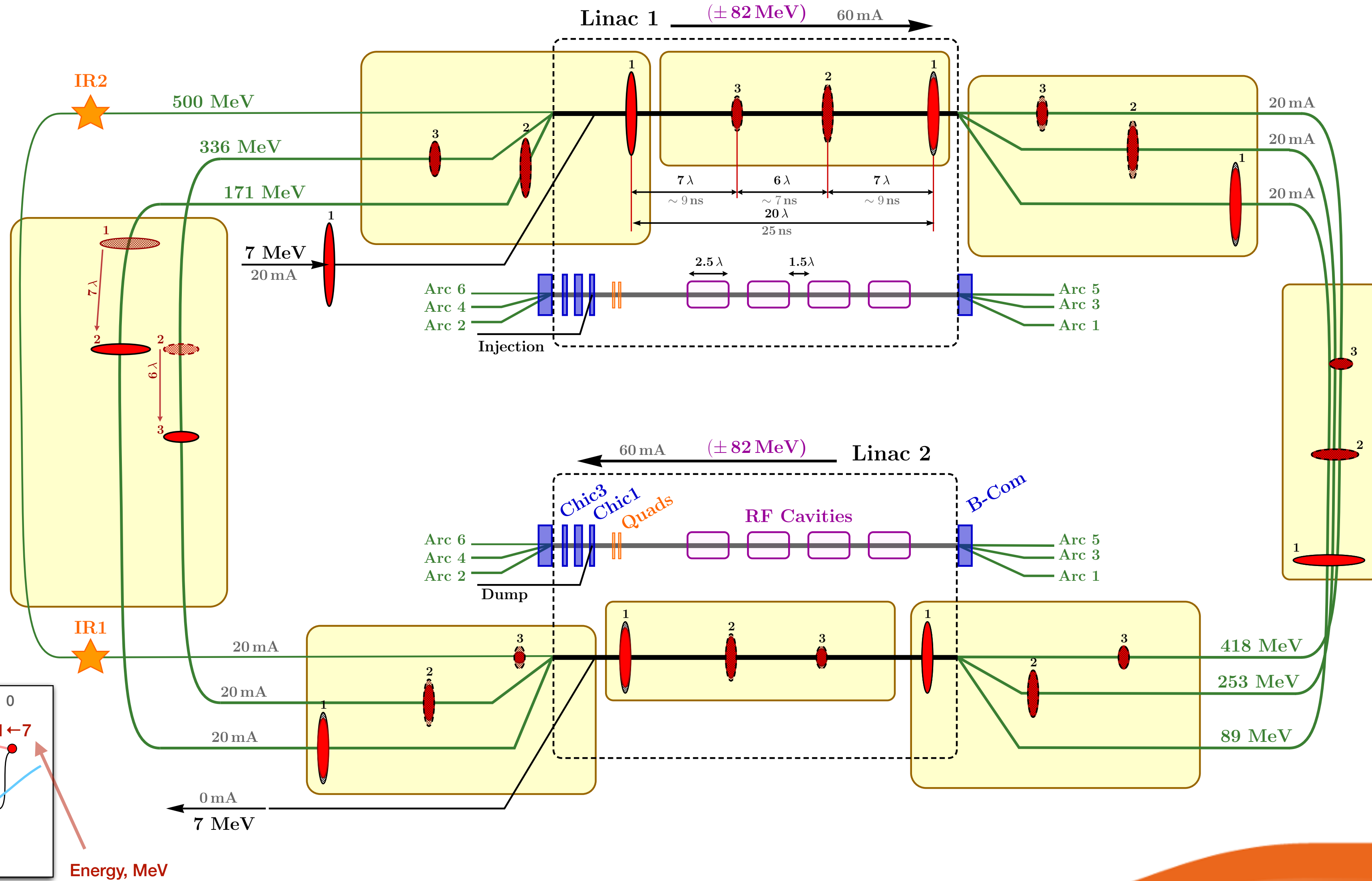
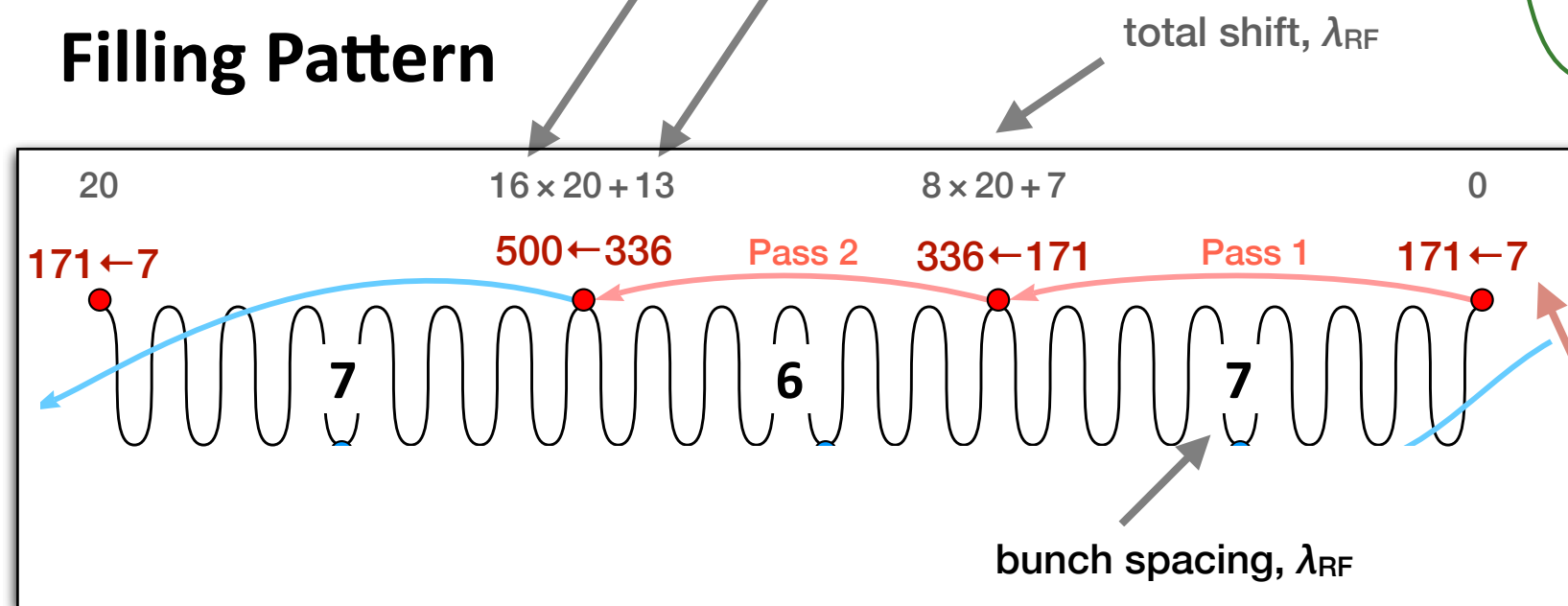
Injection ($v_{inj} \approx 40$ MHz) $I = 20$ mA ($Q \approx 500$ pC, $t_{inj} = 25$ ns)

RF Cavity ($v_{RF} = 801.58$ MHz) $L_{inj} = 20 \lambda_{RF}$ ($\lambda_{RF} \approx 34.7$ cm)

Pass Lengths Linac 1 + Arc j + Linac 2 + Arc k

Pass	Arcs	L_{Arcs}, λ_{RF}	L_{Pass}, λ_{RF}	n_{inj}	Δ, λ_{RF}	$\Delta t, \mu s$
1	1+2	56 + 57	167	8	7	0.209
2	3+4	56 + 56	166	16	13	0.416
3						

Filling Pattern





Forming the Filling Pattern. Passes 1–4



Passes 1–4

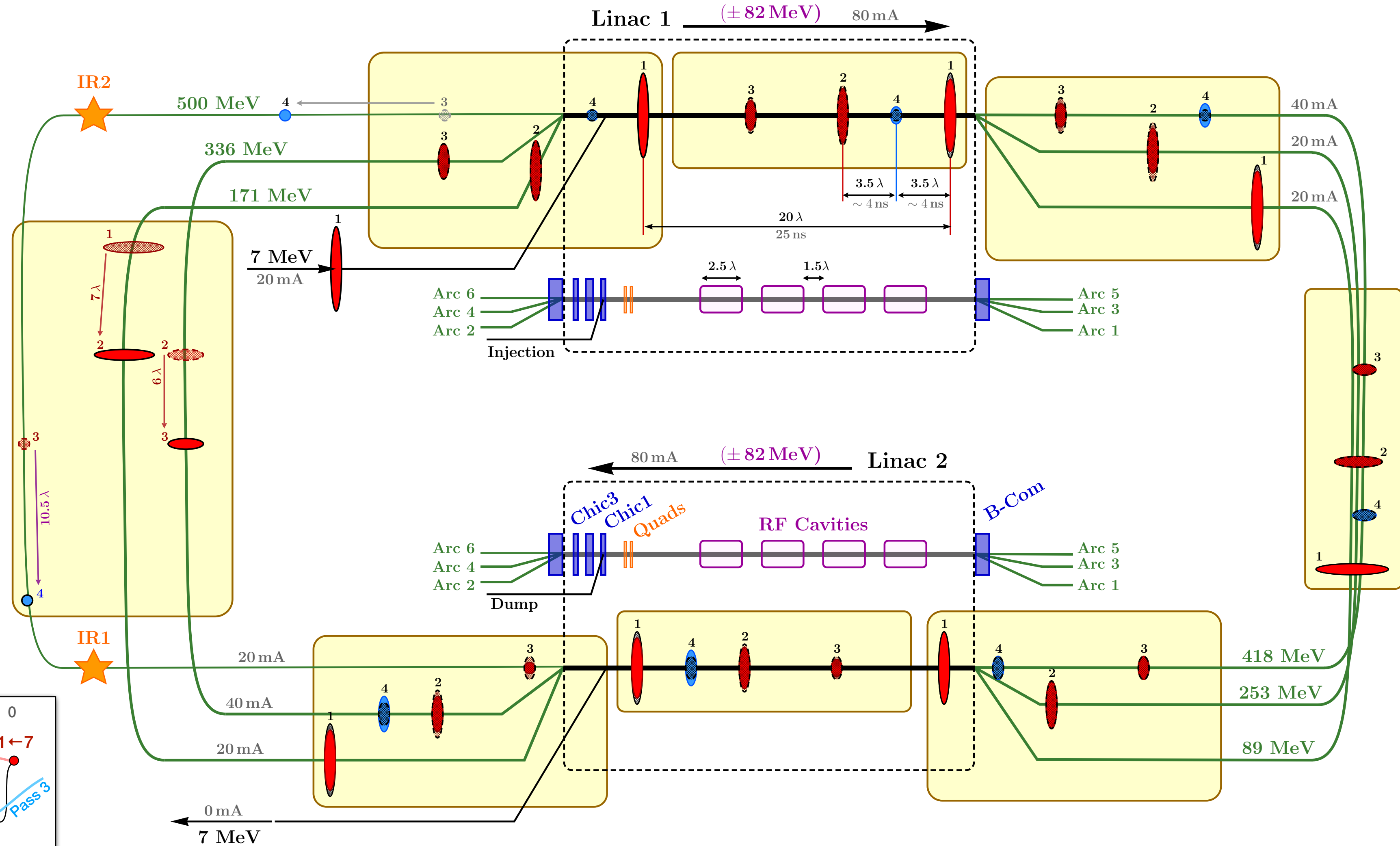
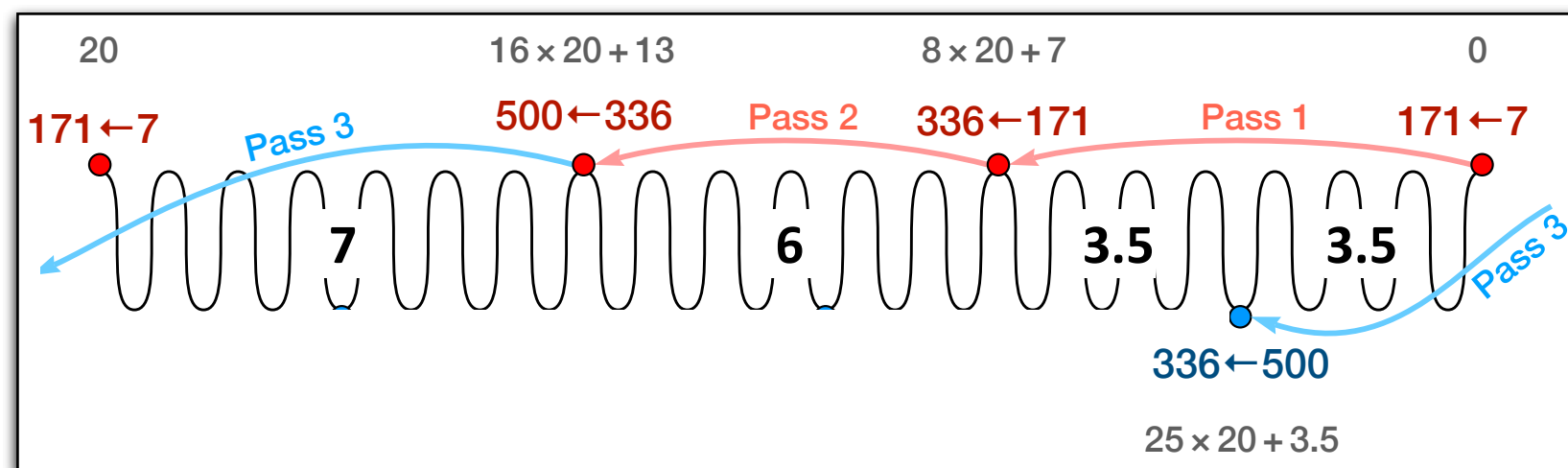
Injection ($v_{inj} \approx 40$ MHz) $I = 20$ mA ($Q \approx 500$ pC, $t_{inj} = 25$ ns)

RF Cavity ($V_{RF} = 801.58$ MHz) $L_{inj} = 20 \lambda_{RF}$ ($\lambda_{RF} \approx 34.7$ cm)

Pass Lengths Linac 1 + Arc j + Linac 2 + Arc k

Pass	Arcs	L_{Arcs}, λ_{RF}	L_{Pass}, λ_{RF}	n_{inj}	Δ, λ_{RF}	$\Delta t, \mu s$
1	1+2	56 + 57	167	8	7	0.209
2	3+4	56 + 56	166	16	13	0.416
3	5+6	56 + 60.5	170.5	25	3.5	0.629
4						

Filling Pattern





Forming the Filling Pattern. Passes 1–5



Passes 1–5

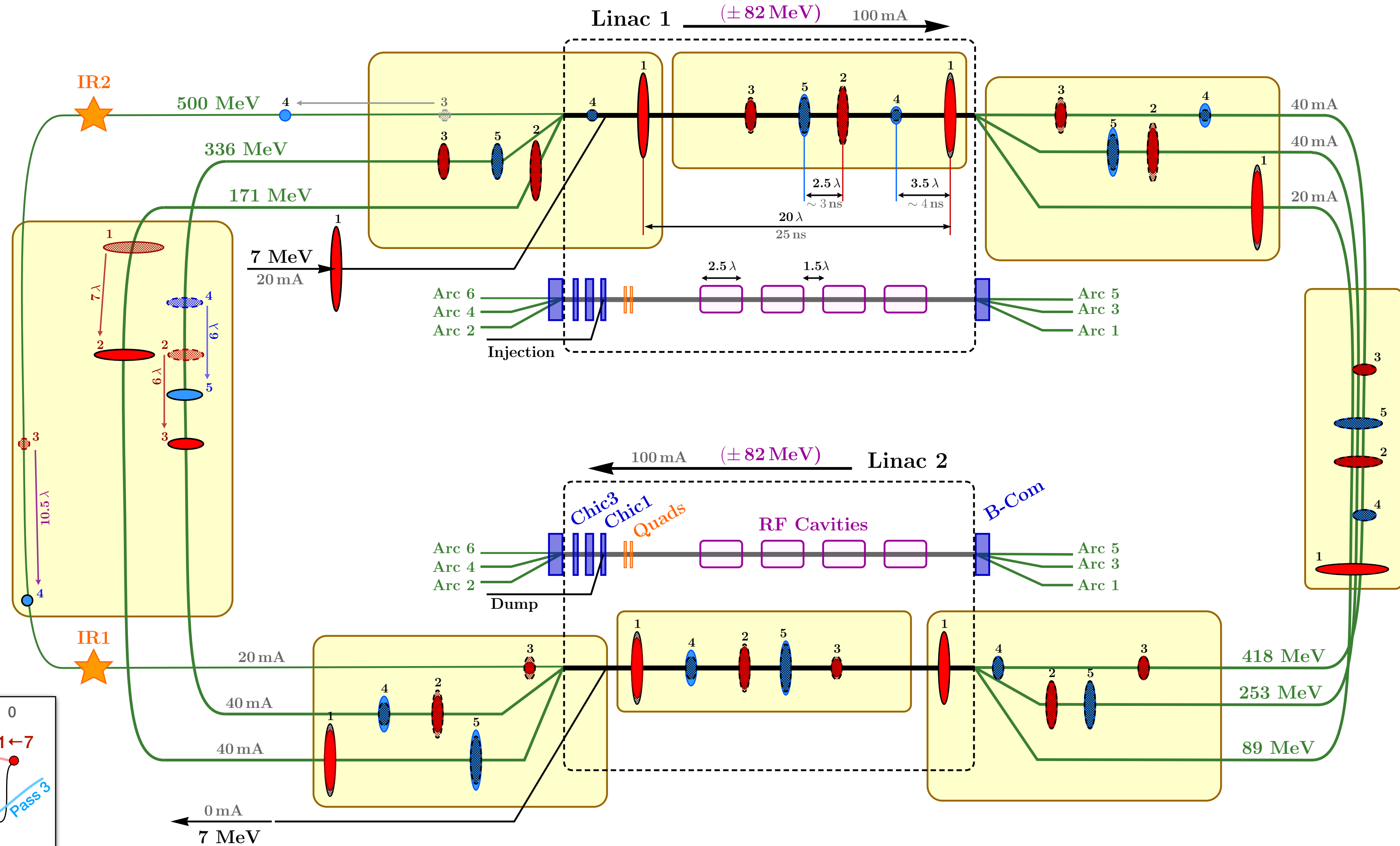
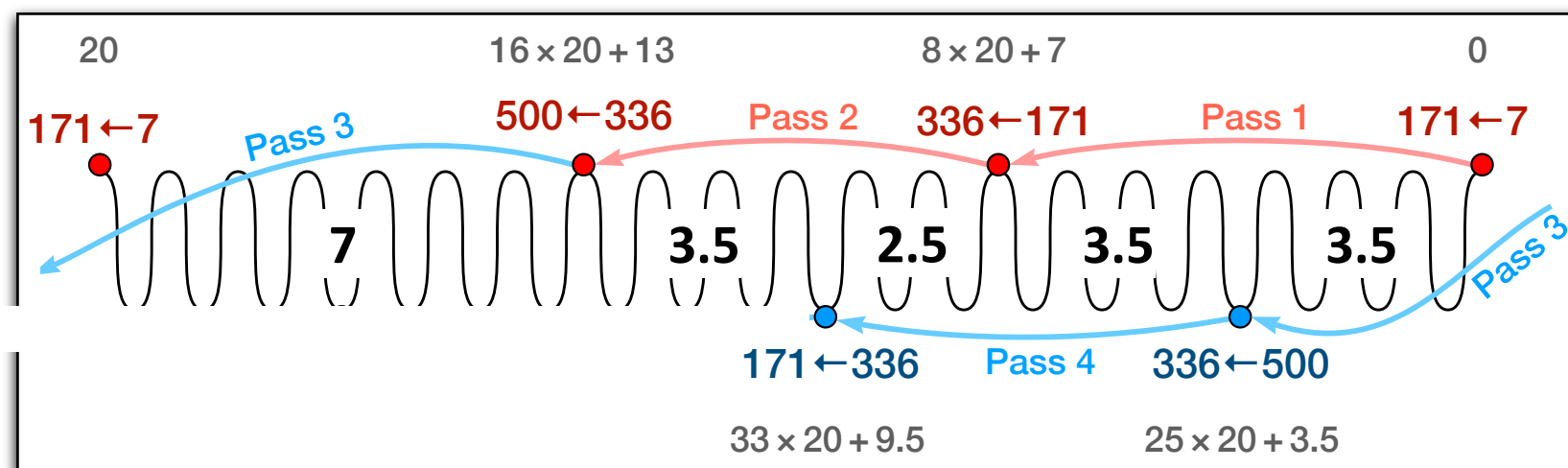
Injection ($v_{inj} \approx 40$ MHz) $I = 20$ mA ($Q \approx 500$ pC, $t_{inj} = 25$ ns)

RF Cavity ($v_{RF} = 801.58$ MHz) $L_{inj} = 20 \lambda_{RF}$ ($\lambda_{RF} \approx 34.7$ cm)

Pass Lengths Linac 1 + Arc j + Linac 2 + Arc k

Pass	Arcs	L_{Arcs}, λ_{RF}	L_{Pass}, λ_{RF}	n_{inj}	Δ, λ_{RF}	$\Delta t, \mu s$
1	1+2	56 + 57	167	8	7	0.209
2	3+4	56 + 56	166	16	13	0.416
3	5+6	56 + 60.5	170.5	25	3.5	0.629
4	5+4	56 + 56	166	33	9.5	0.837
5						

Filling Pattern





Forming the Filling Pattern. Continues cycle



Passes 1-6

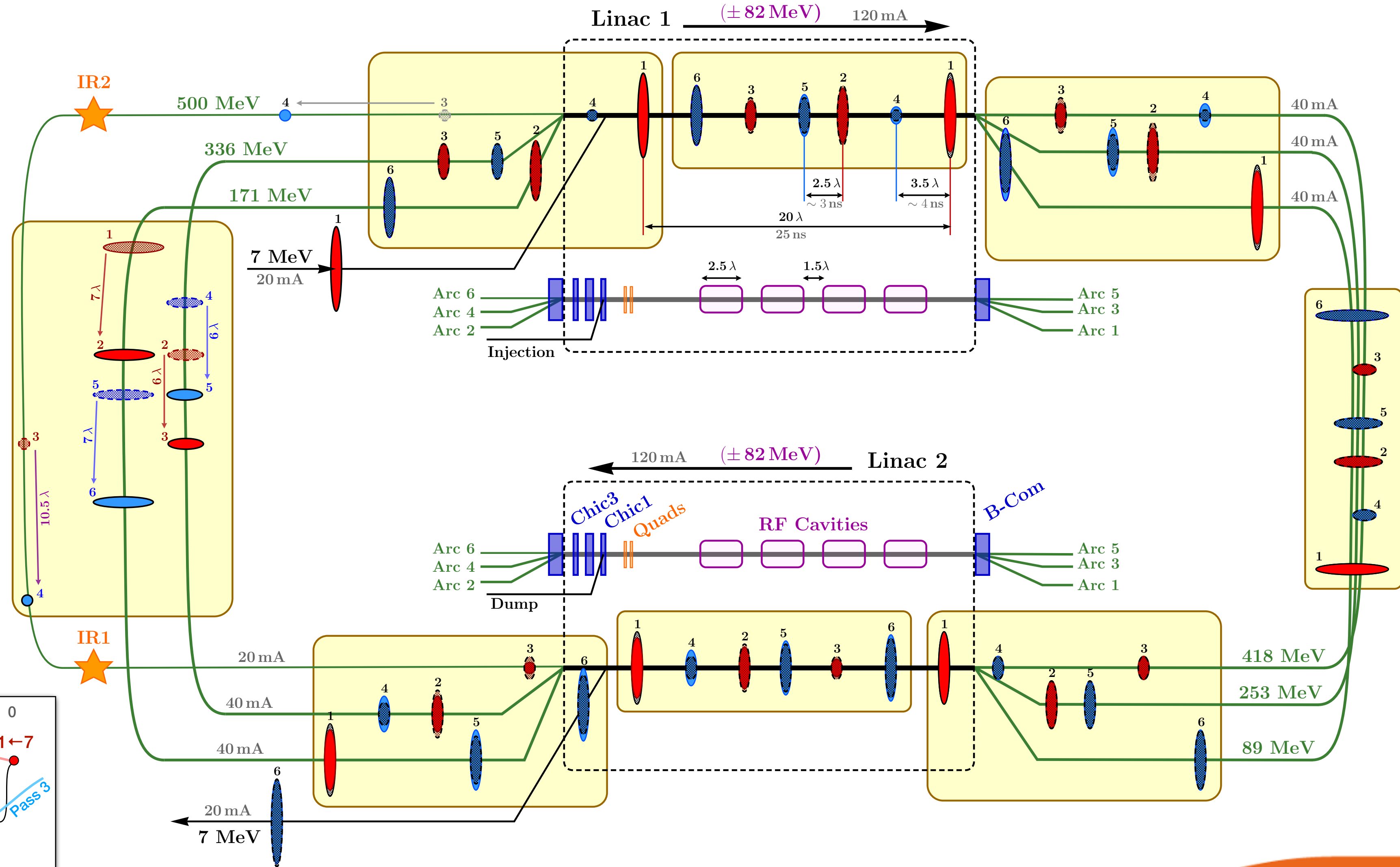
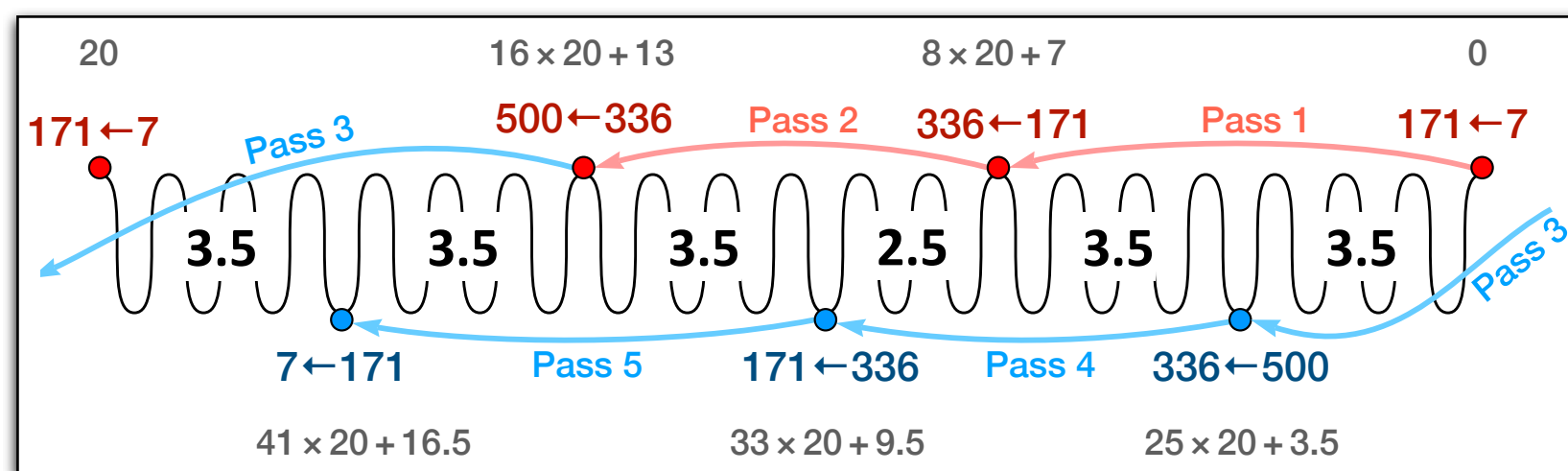
Injection ($v_{inj} \approx 40$ MHz) $I = 20$ mA ($Q \approx 500$ pC, $t_{inj} = 25$ ns)

RF Cavity ($v_{RF} = 801.58$ MHz) $L_{inj} = 20 \lambda_{RF}$ ($\lambda_{RF} \approx 34.7$ cm)

Pass Lengths Linac 1 + Arc j + Linac 2 + Arc k

Pass	Arcs	L_{Arcs}, λ_{RF}	L_{Pass}, λ_{RF}	n_{inj}	Δ, λ_{RF}	$\Delta t, \mu s$
1	1+2	56 + 57	167	8	7	0.209
2	3+4	56 + 56	166	16	13	0.416
3	5+6	56 + 60.5	170.5	25	3.5	0.629
4	5+4	56 + 56	166	33	9.5	0.837
5	3+2	56 + 57	167	41	16.5	1.046
6	1	56	—	—	—	—

Filling Pattern





Filling pattern for 250 MeV version



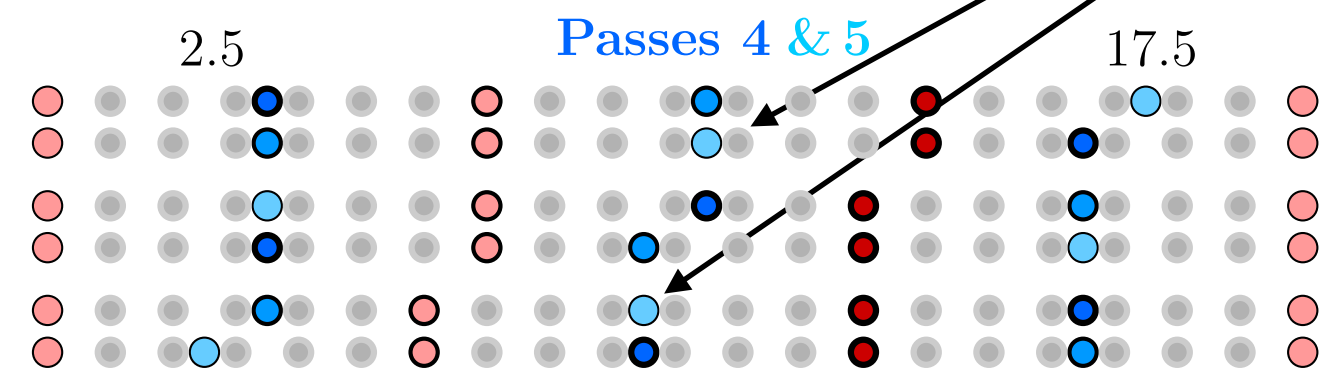
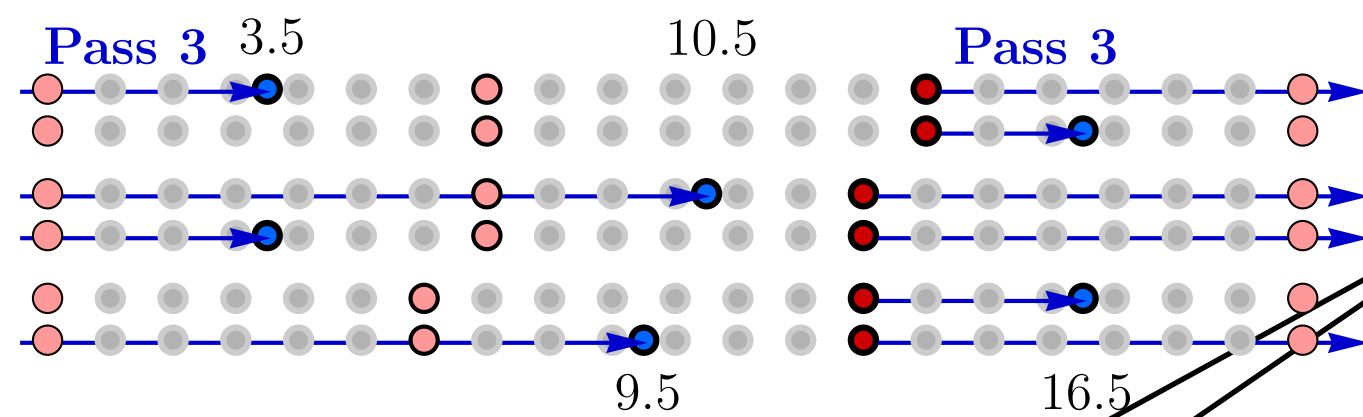
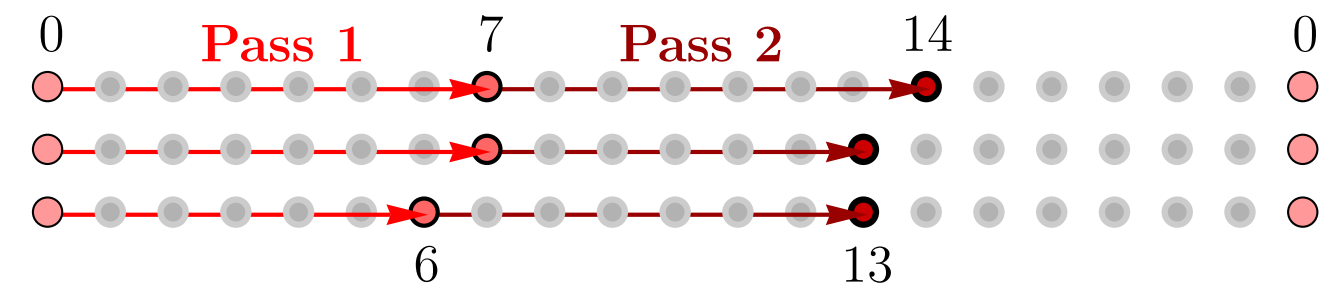
Consecutive injections ($v_{inj} = 40$ MHz), RF cavity ($v_{RF} = 801.58$ MHz) \rightarrow spacing between injections $20 \times \lambda_{RF}$

$$v_{RF} / v_{inj} \approx 20, \lambda_{RF} = 37.4 \text{ cm}$$

Distance between the arcs \rightarrow path length of the bunch between consecutive passes \rightarrow form the filling pattern (placement of accelerated bunches between the injected bunches)

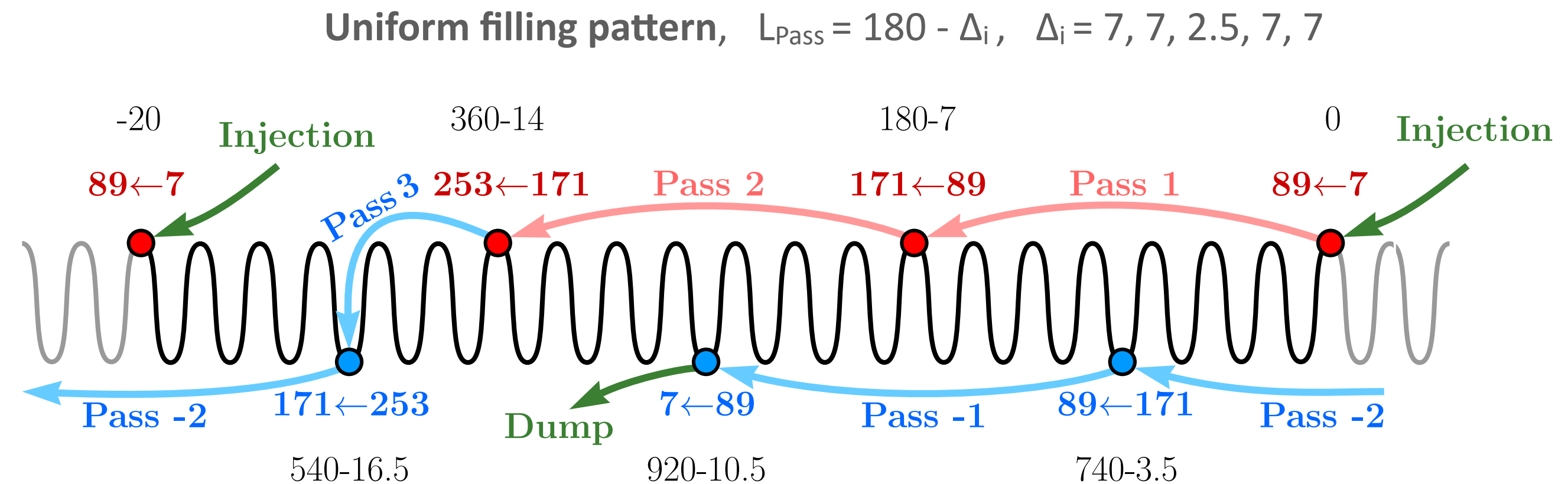
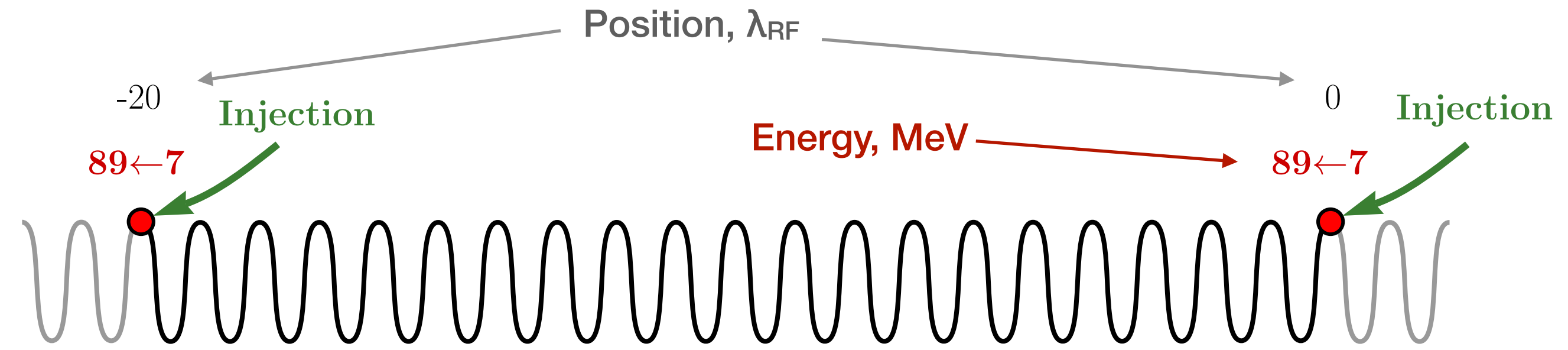
To reduce the risk of beam break-ups \rightarrow uniform filling pattern

Six possible options of uniform filling patterns



option 2 & 5 have bunches of lowest energies separated

option 5 is chosen for 250 MeV version (more detailed studies will follow)





Filling pattern 500 vs 250 MeV versions



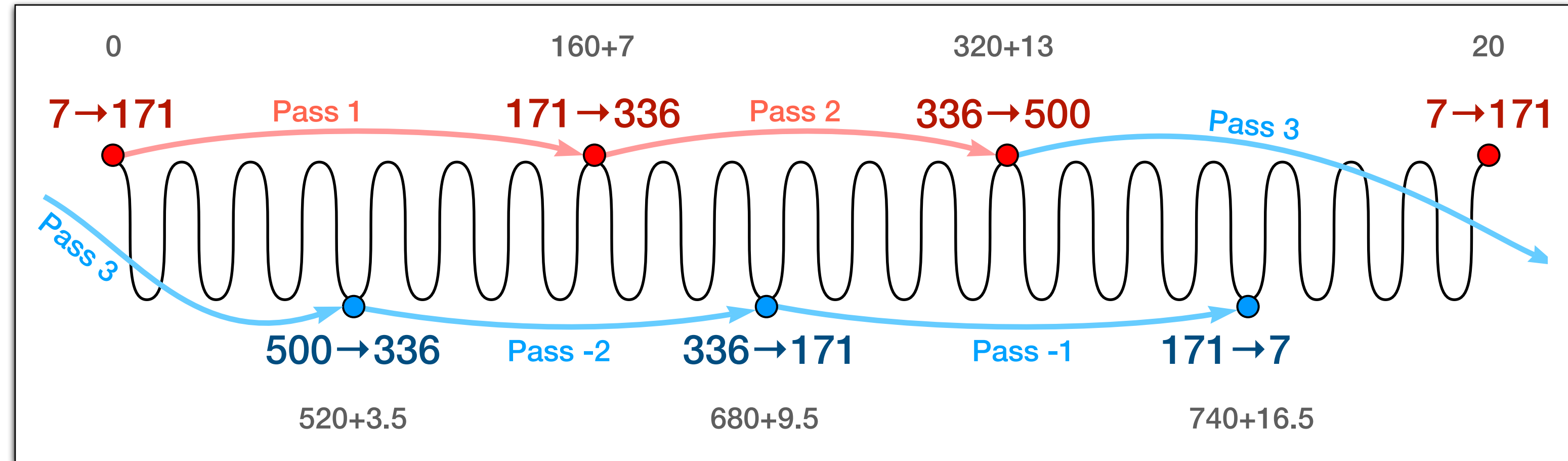
500 MeV

Full length of one turn: $(160 + \Delta) \lambda_{RF}$

chosen shift: $\Delta = 7, 6, 10.5, 6, 7$

→ 2.7 m at IPs (28.6 m total)

studies by A. Bogacz, P. Williams, R. Apsimon, and K. Andre



250 MeV

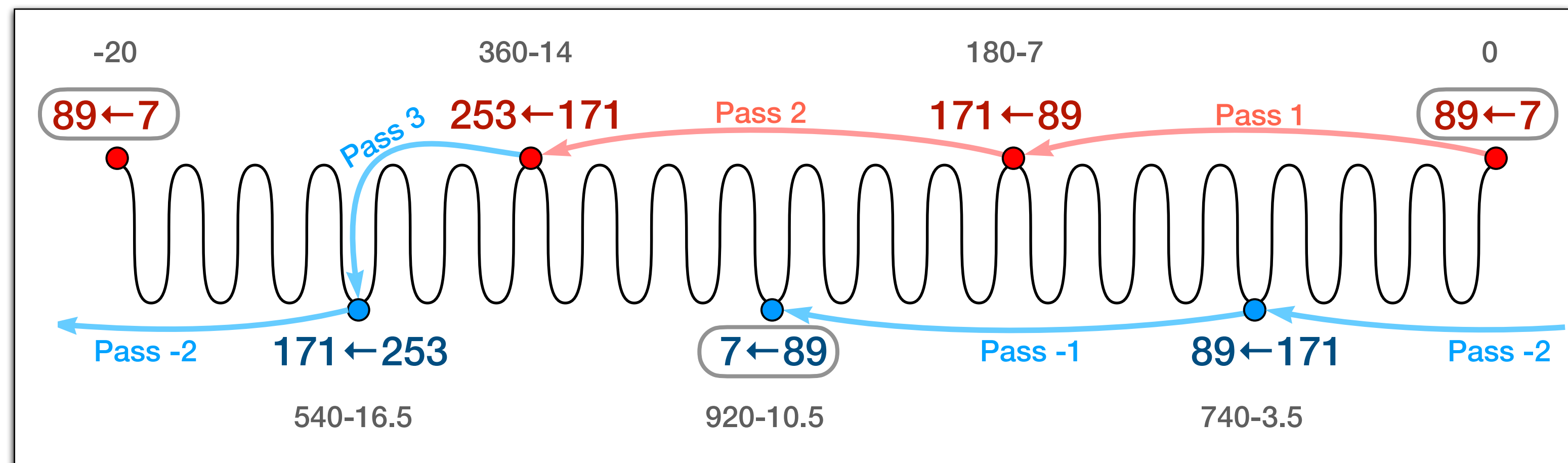
Full length of one turn: $(180 - \Delta) \lambda_{RF}$

optimal shift: $\Delta = 7, 7, 2.5, 7, 7$

→ bunches of lowest energies are separated (more important than for 500 MeV version)

→ more detailed studies will follow)

→ 29.9 m of total length



$$(177.5 - 170.5) \lambda_{RF} / 2 = 3.5 \lambda_{RF} \approx 1.3 \text{ m} \quad (\lambda_{RF} = 37.4 \text{ cm})$$



Motivation of 250 MeV version of PERLE

- **compatible with the upgrade to 500 MeV version** (the same elements used, only about 30 meters of extra beam pipes)
- **reduced immediate expenses** (second cryo-module, 18 dipoles and 21 quads can be purchased later)
- **demonstration of ERL with 6 paths at high current** (same as in 500 MeV version, but with half of the power)
- more space for experimental areas
- **additional expenses / manpower / shutdown time** (rebuilding / recommissioning for the full power machine)

Main differences of 250 MeV

- a slightly larger footprint (28.6 m \rightarrow 29.9 m) shorter Arc6, but longer common section
- different filling pattern (optimal for low energies) — more detailed studies will follow
- less quadrupole magnets — all compatible with current design (< 22 T/m < 34 T/m)

Benchmarking codes for lattice design and beam dynamics simulation

- small difference between Optim6 and MadX calculations of dipole fringe field effect ($\sim 1\%$ correction of the quad field)
- longitudinal beam dynamic from 7MeV to 82MeV with field-map & calculation tool (work of Coline Guyot)



Thank you



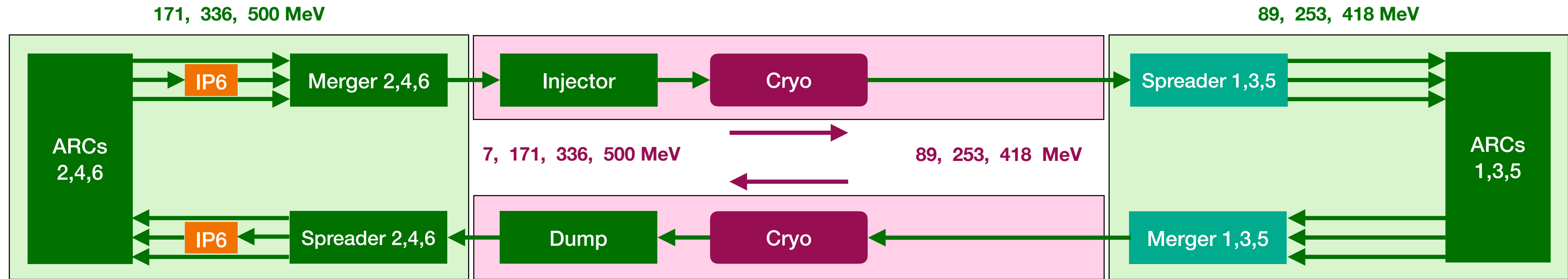
Lattice design. 500 MeV vs 250 MeV versions



500 MeV

Shorter **common area**

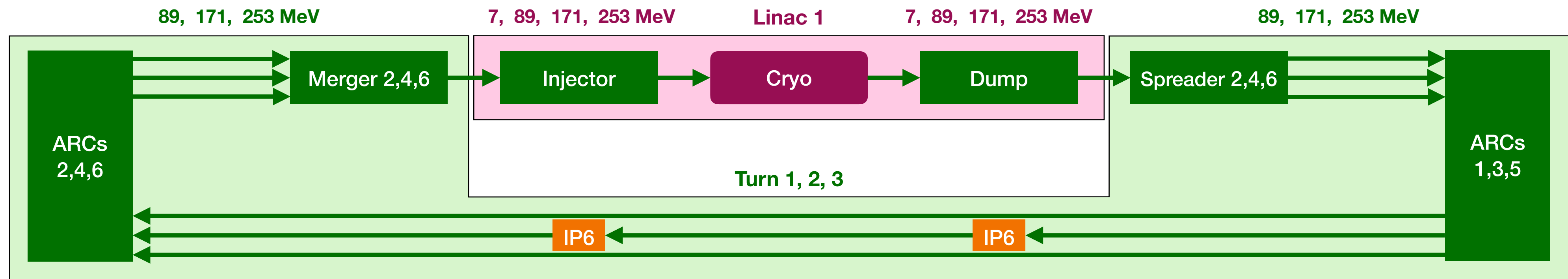
→ 28.6 m total length



250 MeV

Shorter **Arc 6**

→ 29.4 m total length



Two cryo-modules (500 MeV)

- two common sections: Injector+Cryo and Cryo+Dump (~10m)
- two Spreader and two Merger sections
- extended Arc6 (hosting low-beta IRs)

One cryo-module (250 MeV)

- one common sections: Injector+Cryo+Dump (~12m)
- one Spreader and one Merger section
- low-beta IRs at the straight line (between Arcs 5 & 6)

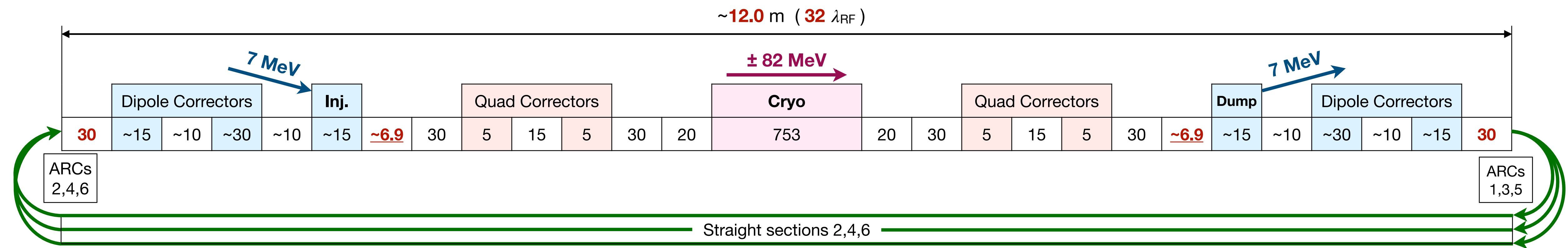
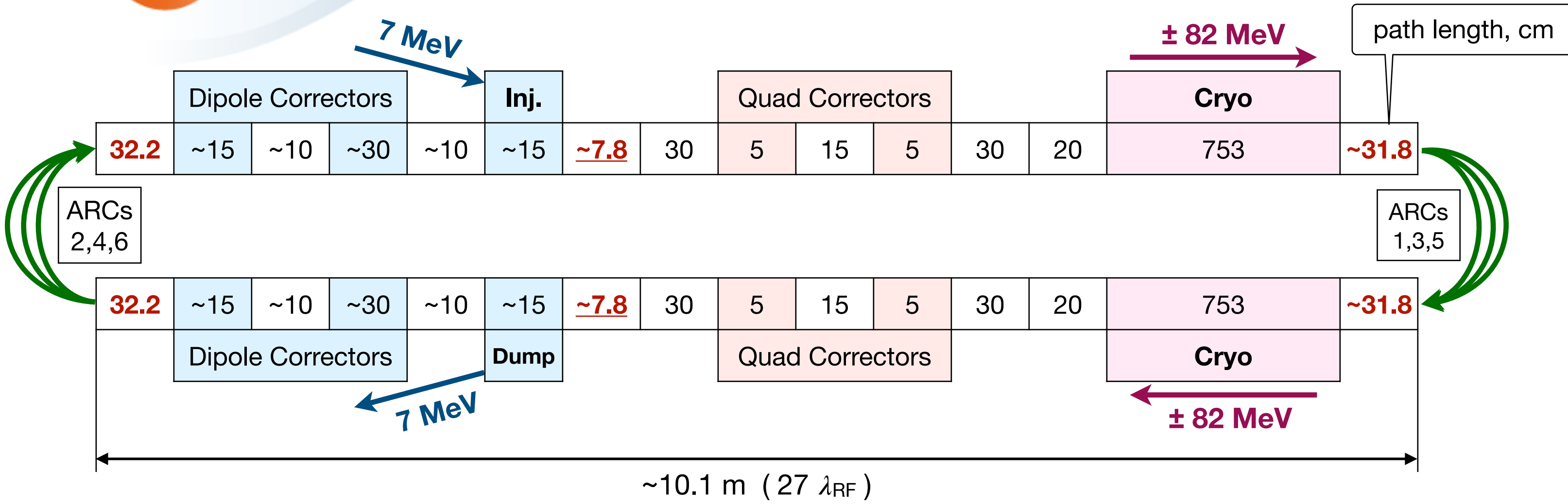


Section(s) with common beam pipe



500 MeV → 250 MeV

- **Injection and Dump** are on the same side
- Drifts around **Dipole Correctors** shortened by **1-2 cm**
- Length of the straight section
 $27\lambda \rightarrow 32\lambda$ ($\lambda = 37.4$ cm)
 10.1 m \rightarrow 12.0 m





Spreader / Mergers

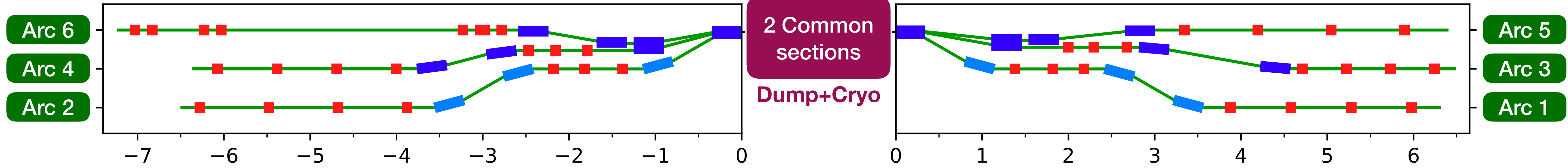


500 MeV

Merger + Spreader

Injection+Cryo

Spreader + Merger

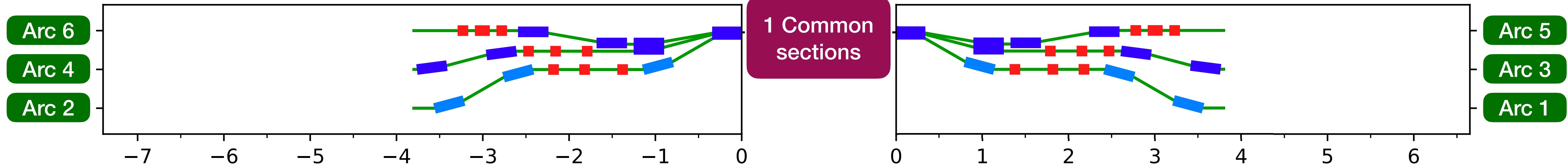


250 MeV

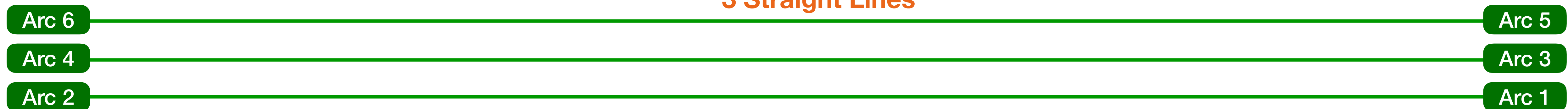
Merger

Injection+Cryo+Dump

Spreader



3 Straight Lines

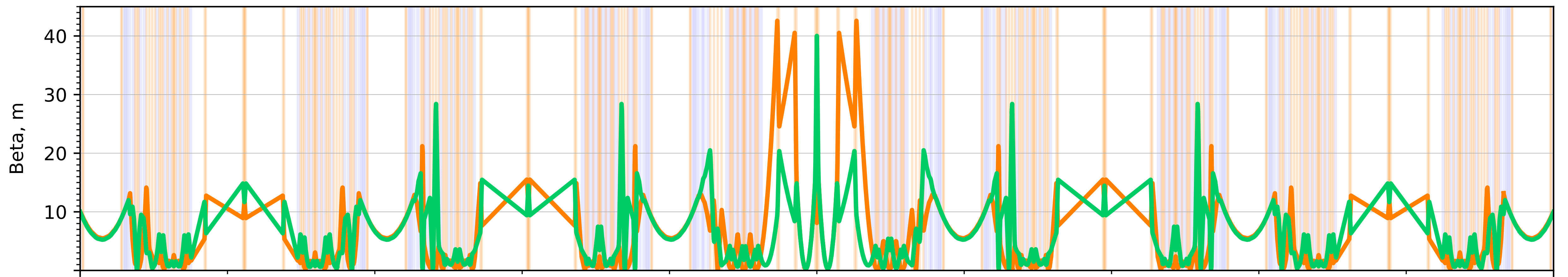
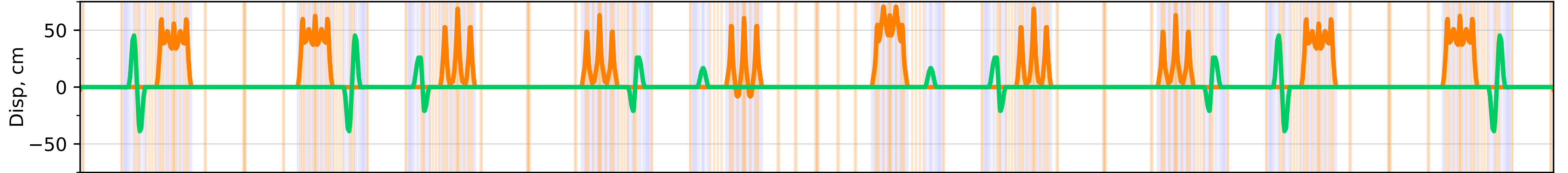




Optics for 250 MeV version (preliminary)



Injection
Acceleration 1
Spr1
Arc1
Arc2
Mirg1
Acceleration 2
Spr2
Arc3
Arc4
Mirg2
Acceleration 3
Spr3
Arc5
IRs ($\beta_{x,y}=30\text{cm}$)
Arc6
Mirg3
Deceleration 1
Spr2
Arc3
Arc4
Mirg2
Deceleration 2
Spr1
Arc1
Arc2
Mirg1
Deceler. 3
Dump



89 MeV 171 MeV s, m 171 MeV 89 MeV 335

253 MeV

— Horizontal plane — Vertical plane



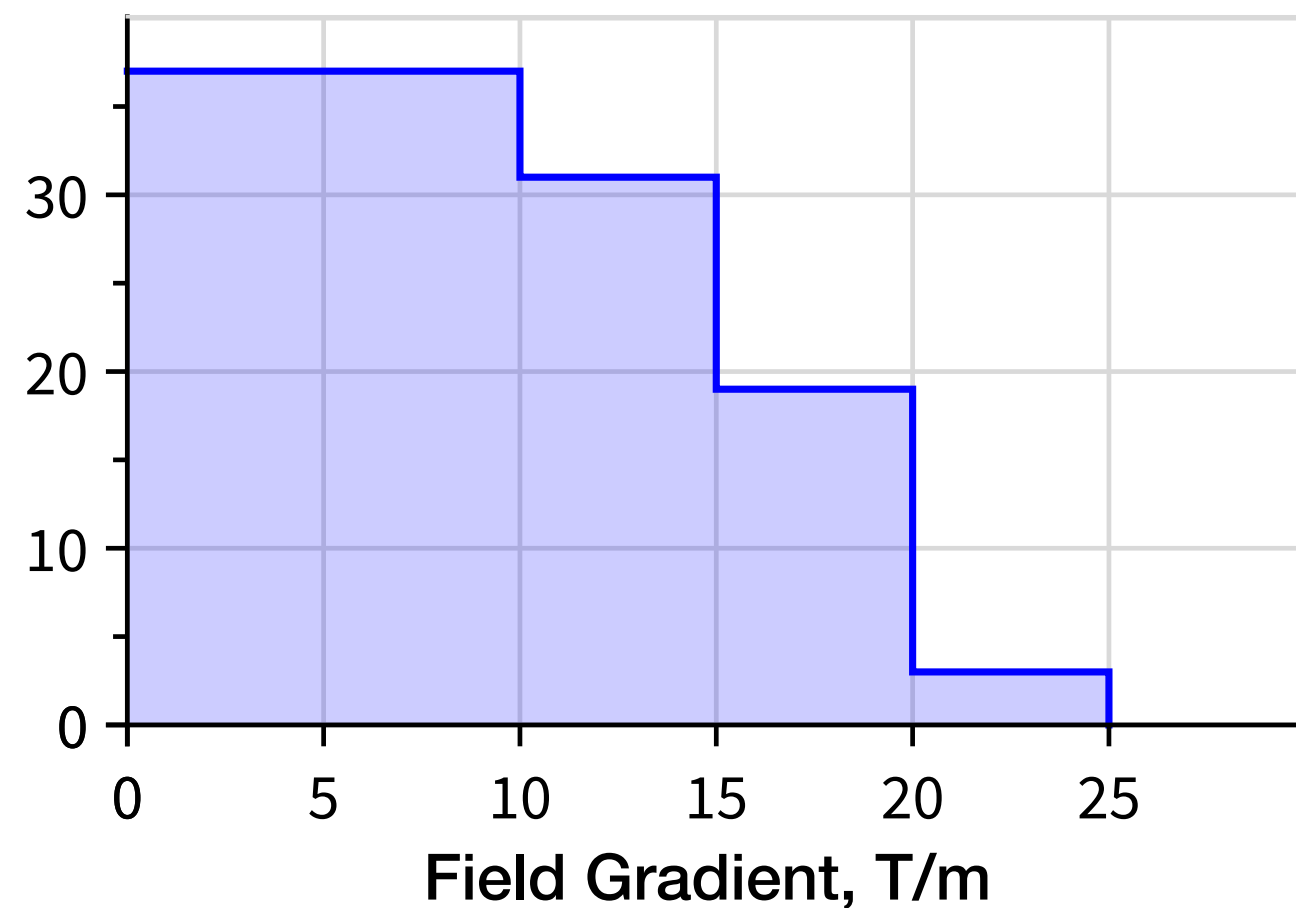
Quadrupole Magnets



Field, T and Field Gradient, T/m (500 MeV)

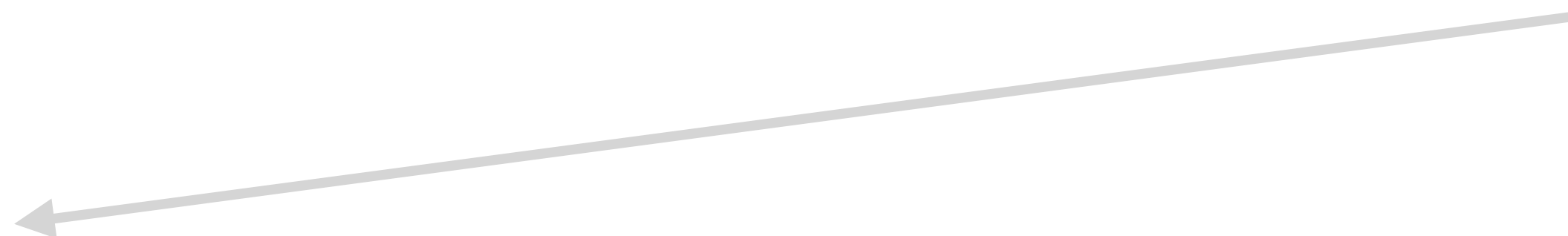
	Spreaders												Arcs								
	10 cm	15 cm	10 cm	10 cm	10 cm	10 cm	10 cm	10 cm	10 cm	10 cm	10 cm	10 cm	15 cm	10 cm	10 cm	10 cm	15 cm	10 cm	10 cm	15 cm	
1	-0.45	0.47	-4.3	4.9	-5.0	-0.47	0.47		4.0	-3.4	-0.53	-0.42	0.48	-4.7	5.1	-4.9	0.48	2.9	0.48	-5.3	4.1
2	-0.87	0.9	-8.2	9.5	-9.5	-0.9	0.9		7.3	-6.1	-1.8	0.61	0.92	-9.2	9.7	-9.3	0.92	6.2	0.92	-11.2	7.8
3	-0.45	0.45	-29.7	28.0	-23.4	-0.45	0.45		-16.0	19.0	-27.2	9.6	1.36	-9.2	16.7	-13.5	1.36	4.5	1.36	-14.1	16.9
4	-0.87	0.87	-32.0	35.7	-37.9	-0.87	0.87		-7.6	10.6	-10.8	10.2	0.9	-18.6	28.4	-25.3	0.9	15.7	0.9	-20.1	27.0
5	-0.45	0.45	0.45	-0.45	10 cm	15 cm	10 cm		-9.5	20.0	-14.8	31.9	1.12	-27.2	36.4	-27.5	1.12	17.9	1.12	-29.2	37.8
6	-0.87	0.87	0.87	-0.87	-28.1	27.7	-16.4	iIR	-54.9	44.4	30.9	-46.2	1.34	-32.6	43.0	-32.5	1.34	21.2	1.34	-34.1	44.1

Number of quadrupoles vs gradient (250 MeV)



500 MeV: 144 quadrupoles (**16 at saturation**)

250 MeV: 127 quadrupoles (17 quads less) **all are below the saturation** (34.15 T/m)



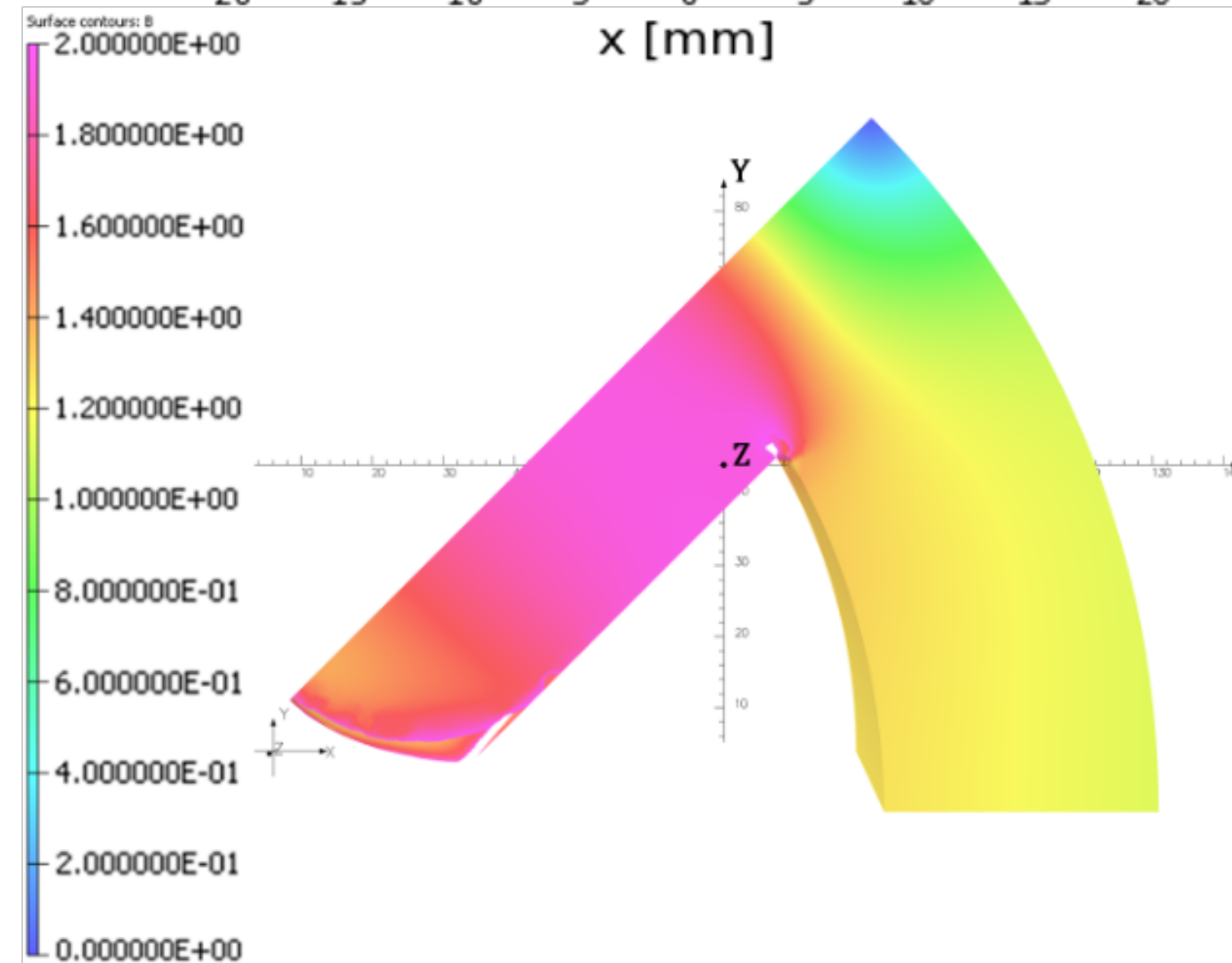
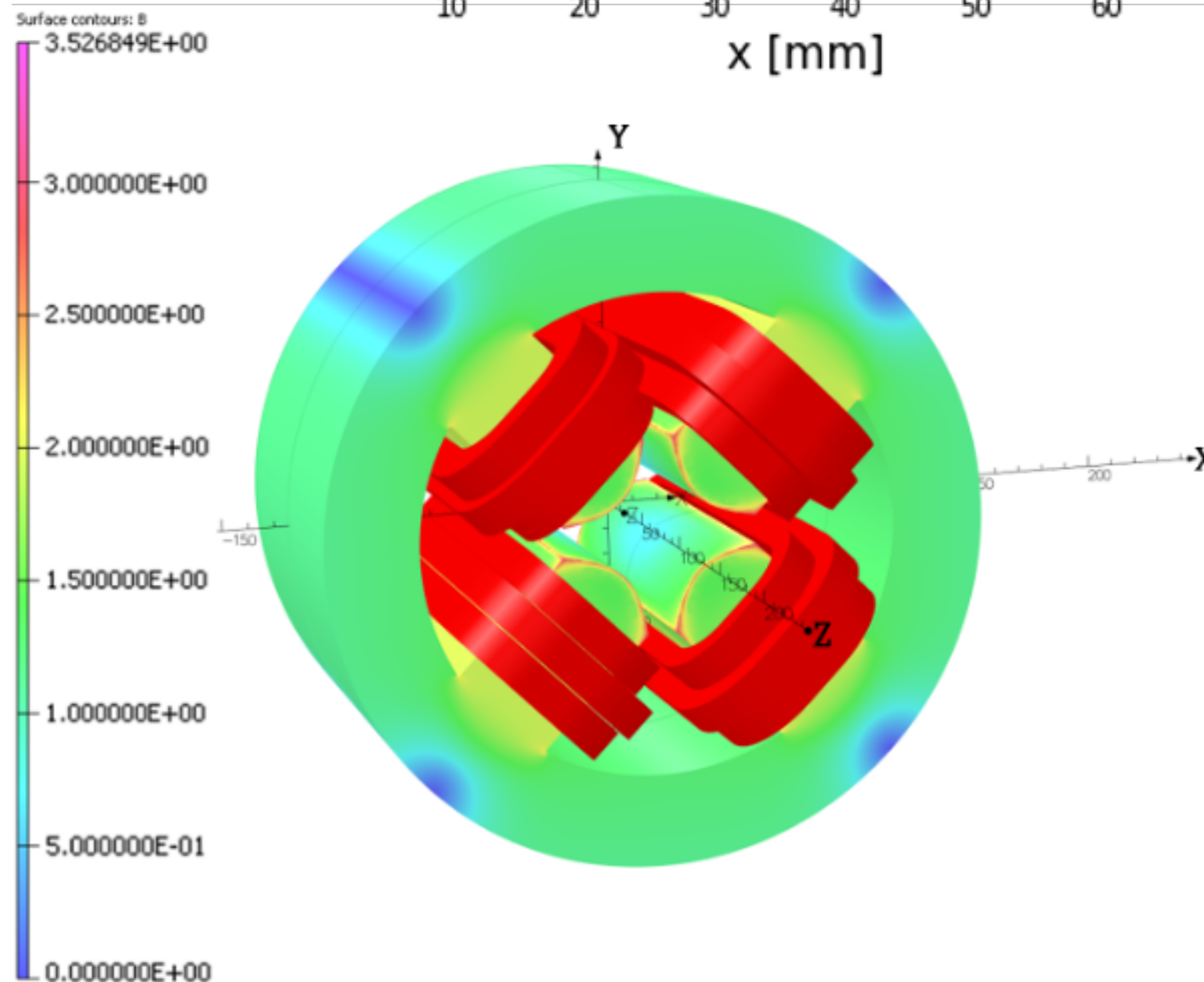
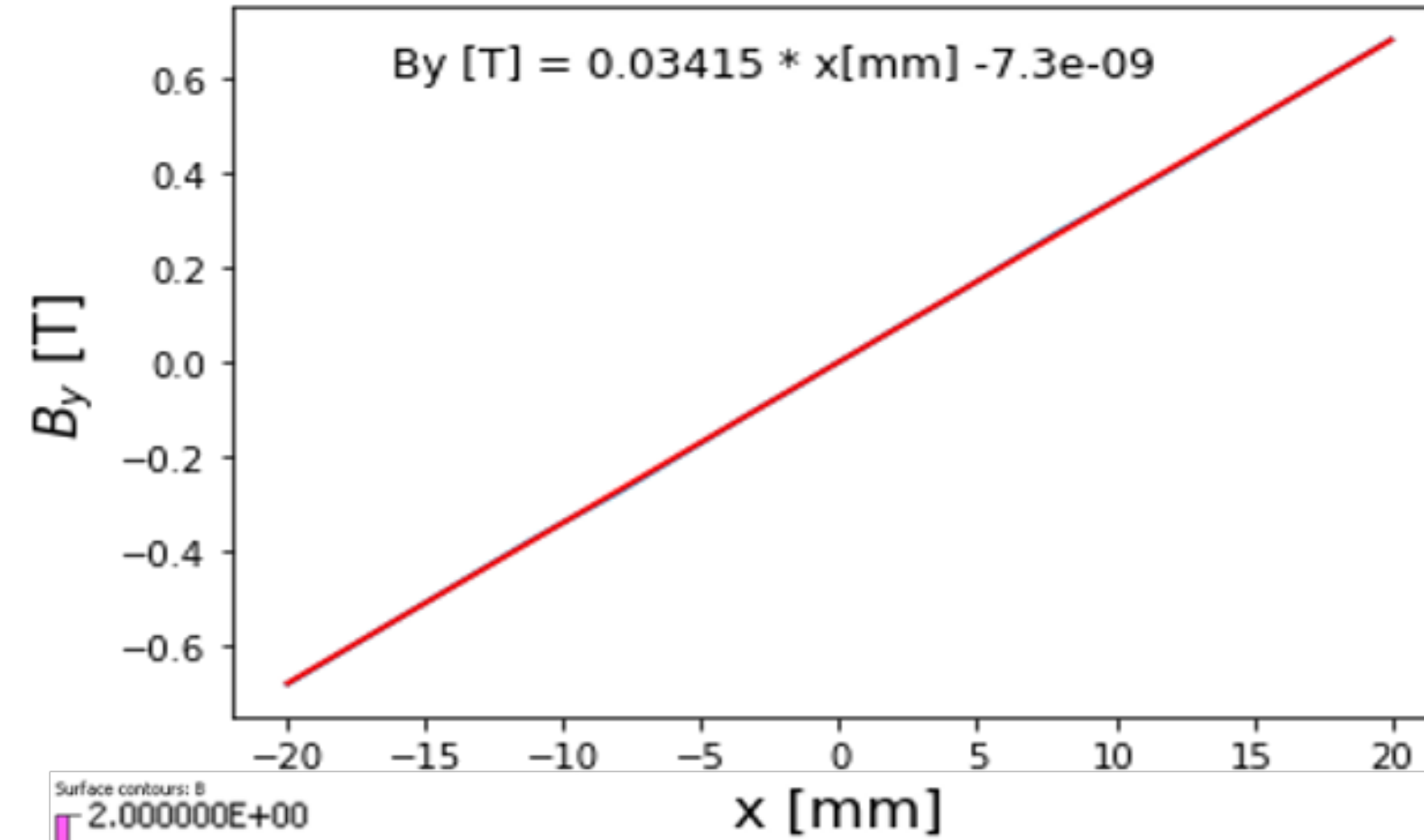
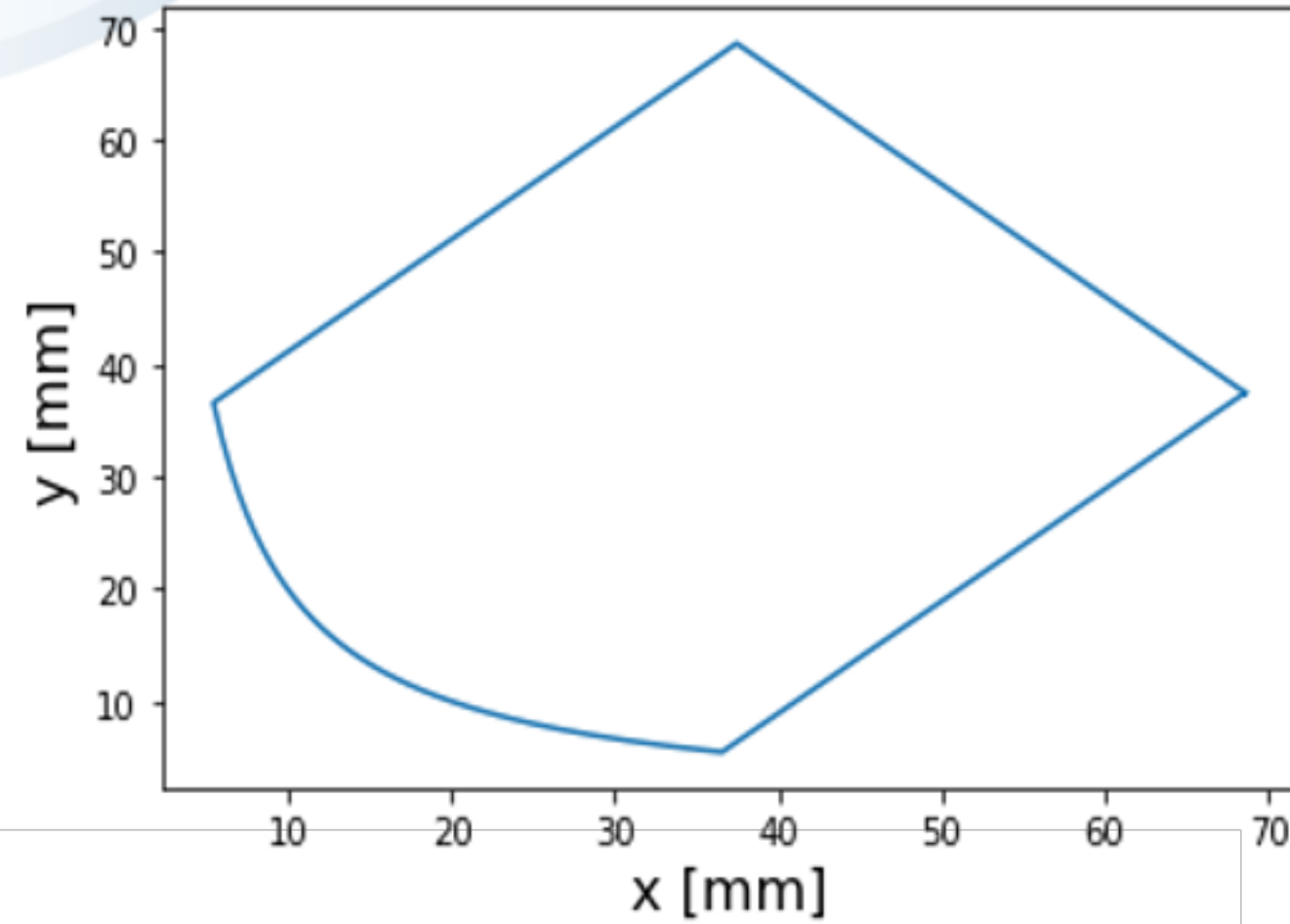


Quadrupole Magnet (work by Rasha Abukeshek)



Multi-coil design

$$G = 34.15 \text{ T/m}$$



Parameters	Value
Height	250 mm
Yoke thickness	35 mm
Length	150 mm
Aperture radius	20 mm
Pole width	44 mm
Max. gradient	44.1 T/m
NI per coil	1750.7 A.turn
Pole tip field	0.685 T

- ✓ 15 cm quadrupole: design is ready up to the 4th arc.
- ✓ arcs 5 and 6: design saturation.

Suggested solution: pole tapering



Filling pattern



	Two Cryomodules (500 MeV)		One Cryomodule (253 MeV)		Filling Pattern
After	E, MeV		E, MeV		
Pass 0	7		7		
Pass 1	171		89		
Pass 2	336		171		
Pass 3	500		253		
Pass -2	336		171		
Pass -1	171		89		
Dump	7		7		



Filling pattern



Chosen for 500 MeV

- shifts after each turn: $\Delta = 7, 6, 10.5, 6, 7$
 → 2.7 m free space at IPs
 → total length 28.6 m

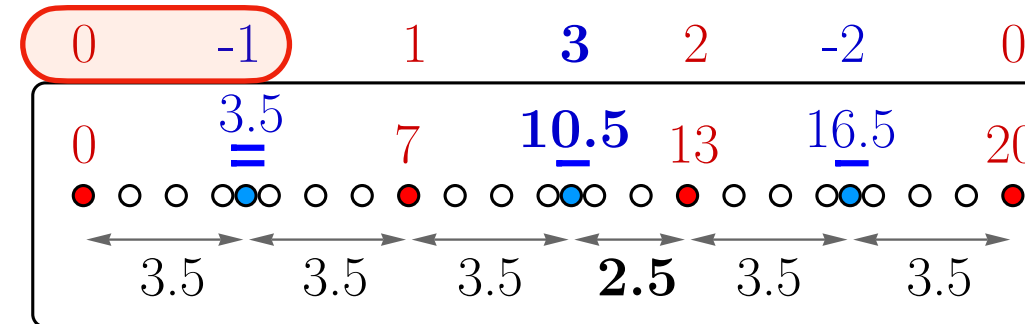
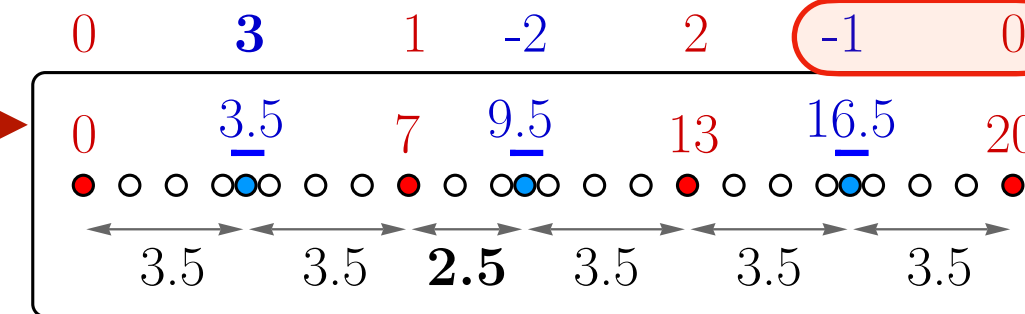
Optimal filling pattern

- shifts after each turn: $\Delta = 7, 7, 2.5, 7, 7$
 → separation of lowest energies bunches
 → more important for 250 MeV version

Possible adjustments

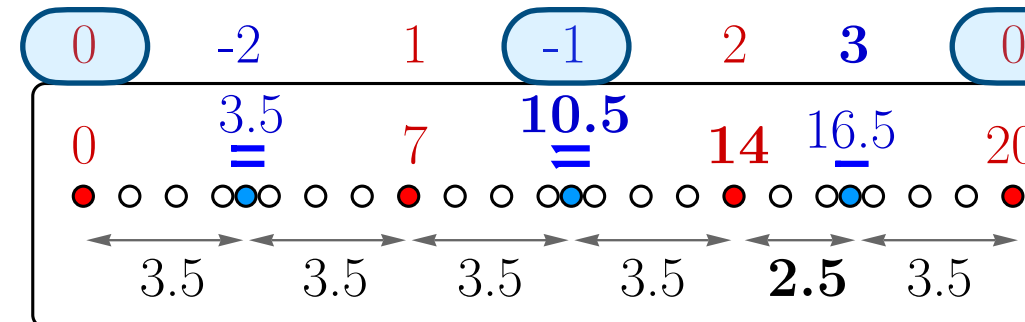
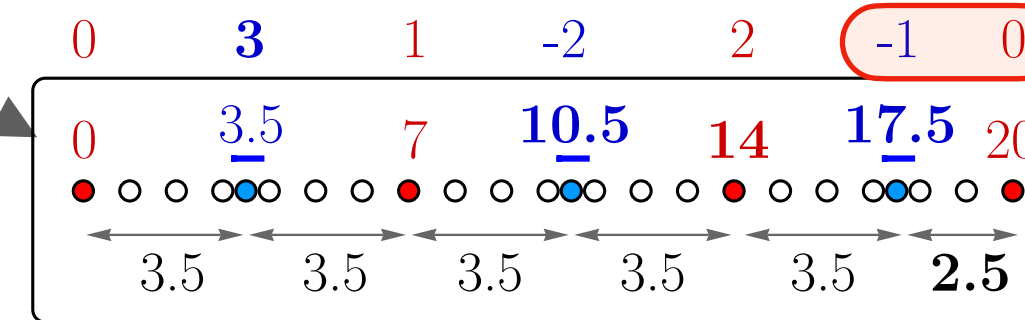
- the lengths of each even Arcs can be reduced by the same value as each of all odd Arcs increased (and vice versa)
- length of any Arc can be adjusted by integer number of 20 ($\Delta \rightarrow \Delta \pm 20n$)
- all shifts can be inverted ($\Delta \rightarrow -\Delta$)

A1	57	4	7		7	
A2	56	3		7		+20
A3	57	4	6		13	+20
A4	55	2		6		9.5
A5	57	4	10.5		3.5	
A6	59.5	6.5				



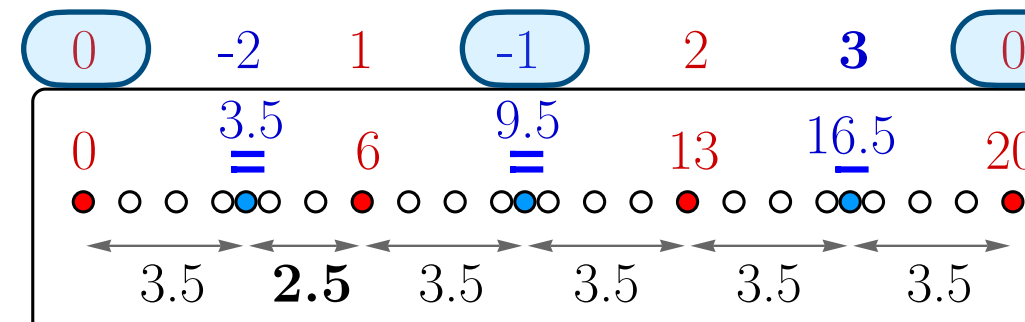
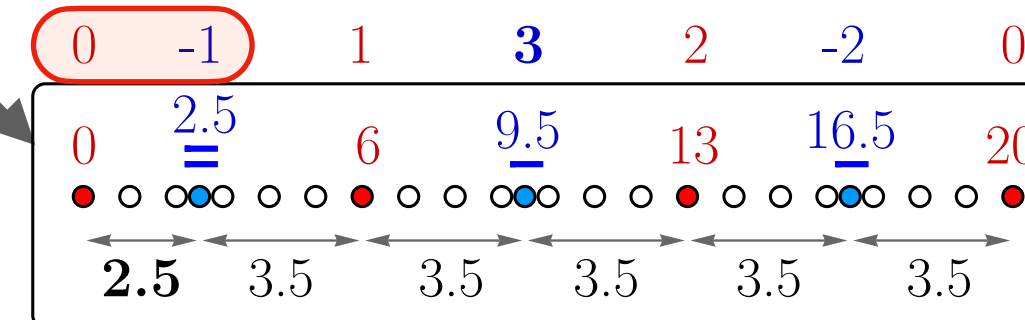
A1	57	4	7		7	
A2	56	3		7		+40
A3	57	4	6		13	+20
A4	55	2		6		16.5
A5	57	4	17.5		10.5	
A6	66.5	13.5				

A1	57	4	7		7	+20
A2	56	3		7		17.5
A3	57	4	7		14	+20
A4	56	3		7		10.5
A5	57	4	9.5		3.5	
A6	58.5	5.5				



A1	57	4	7		7	+40
A2	56	3		7		10.5
A3	57	4	7		14	+40
A4	56	3		7		3.5
A5	57	4	22.5		16.5	
A6	78.5	18.5				

A1	57	4	6		6	+40
A2	55	2		6		2.5
A3	57	4	7		13	+20
A4	56	3		7		16.5
A5	57	4	16.5		9.5	
A6	72.5	12.5				



A1	57	4	6		6	+40
A2	55	2		6		9.5
A3	57	4	7		13	+40
A4	56	3		7		3.5
A5	57	4	23.5		16.5	
A6	79.5	19.5				



Transition between Optim6 and MadX



Optim6

```
g1S01 B[kG]=-4.506411 Angle[deg]=0   EffLen[cm]=2
b1S01 L[cm]=34.55752  B[kG]=-4.506411 G[kG/cm]=0
G1S01 B[kG]=-4.506411 Angle[deg]=30  EffLen[cm]=3.849
```

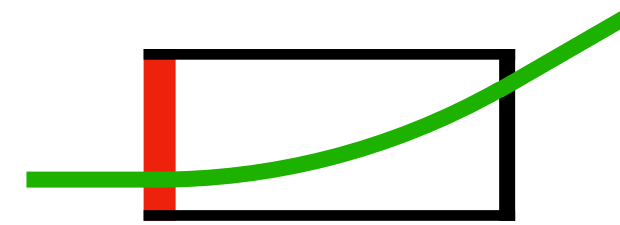
(all in vertical plane: TILT = $\pi/2$)

MadX

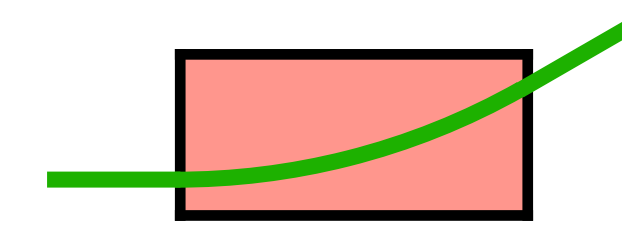
```
b1S01a: DIPEDGE, H=1.515151, E1=0,      FINT=0.5, HGAP=0.02;
b1S01b: SBEND,   L=0.3455752, ANGLE=- $\pi/6$ ;
b1S01c: DIPEDGE, H=1.515151, E1=- $\pi/6$ ,  FINT=0.5, HGAP=0.02;
```

Matching

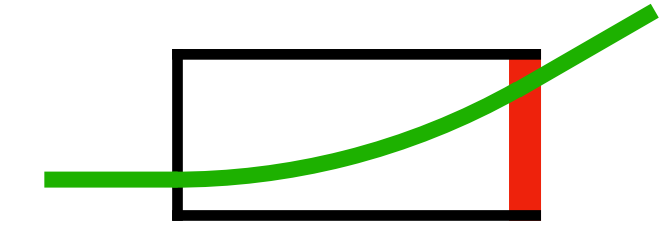
	Place	Initial	Matched
Field gradient, T/m	qq1s01	-4.26551	-4.265 82
	qq1s02	4.87074	4. 92812
	qq1s03	-4.96549	-4.96547
	qq1s04	-5.28356	-5.28 686
	qq1s05	4.07249	4.07 428
α_x	center	-0.0 14401	0
α_y	center	0.000 17	0



1					
0.0459 1	1				
		1			
			1		
				1	
					1



1	0.34558				
0	1				
		0.86603	0.33	-0.08842	
		-0.75758	0.86603	-0.5000 0	
		-0.5000 0	0.08842	1	-0.01556
					1



1					
-0.78 64	1				
		1			
		0.87477	1		
				1	
					1

1					
0.0459 3	1				
		1			
			1		
				1	
					1

1	0.34558				
0	1				
		0.86603	0.33	-0.08842	
		-0.75758	0.86603	-0.5000 1	
		-0.5000 1	0.08842	1	-0.01556
					1

1					
-0.78 85	1				
		1			
		0.87477	1		
				1	
					1

The edge focusing of a dipole is not identical in two codes
 With a small correction (~1%) of the filed gradient
 in quadrupoles the lattice can be symmetrized



Transition between Optim6 and MadX



Optim6

```
g1S01 B[kG]=-4.506411 Angle[deg]=0   EffLen[cm]=2
b1S01 L[cm]=34.55752  B[kG]=-4.506411 G[kG/cm]=0
G1S01 B[kG]=-4.506411 Angle[deg]=30  EffLen[cm]=3.849
```

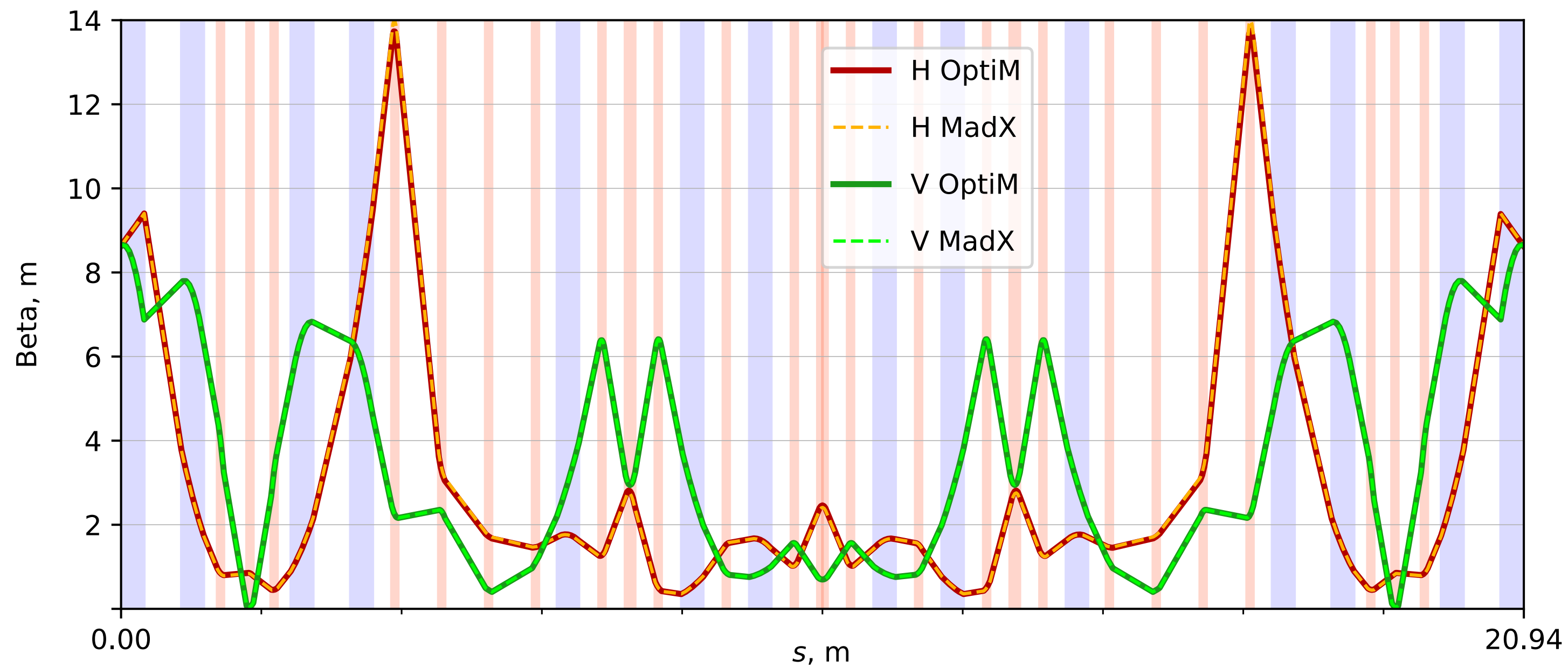
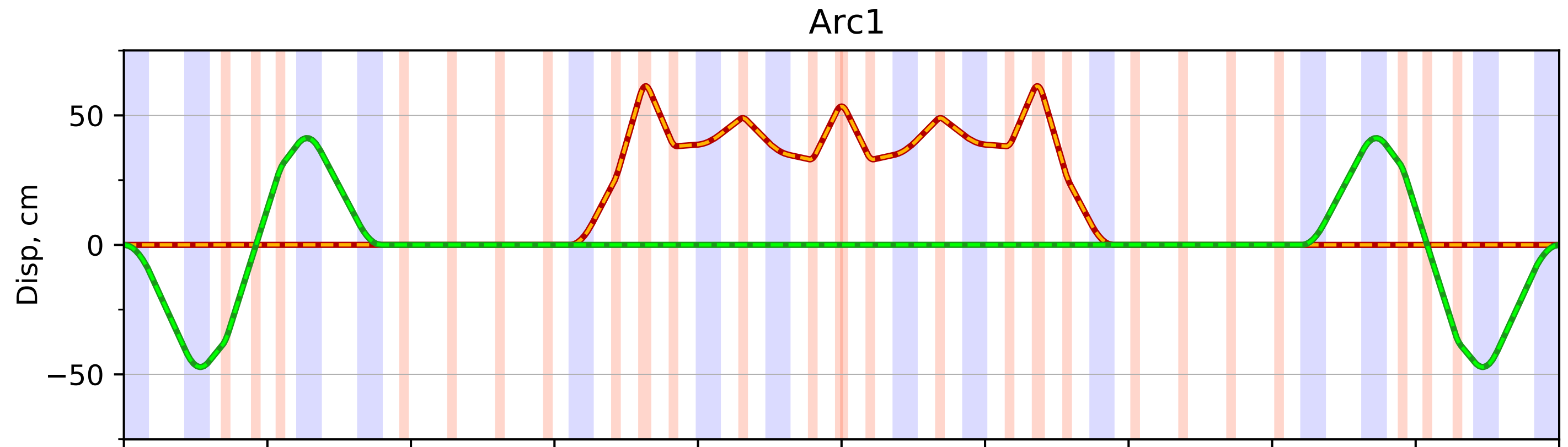
MadX

(all in vertical plane: TILT = $\pi/2$)

```
b1S01a: DIPEDGE, H=1.5151515, E1=0,      FINT=0.5, HGAP=0.02;
b1S01b: SBEND,    L=0.3455752, ANGLE=- $\pi/6$ ;
b1S01c: DIPEDGE, H=1.5151515, E1=- $\pi/6$ ,  FINT=0.5, HGAP=0.02;
```

Matching

	Place	Inital	Matched
Field gradient, T/m	qq1s01	-4.26551	-4.265 82
	qq1s02	4.87074	4. 92812
	qq1s03	-4.96549	-4.9654 7
	qq1s04	-5.28356	-5.28 686
	qq1s05	4.07249	4.07 428
α_x	center	-0.01 4401	0
α_y	center	0.000 17	0



also benchmarked with CODAL (Coline Guyot)