

FCC-ee Monochromatization Updates

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Outline

- Transverse Monochromatization Principle
- FCC-ee Monochromatization Schemes
- FCC-ee Monochromatization Optics Design
- Summary and Outlook

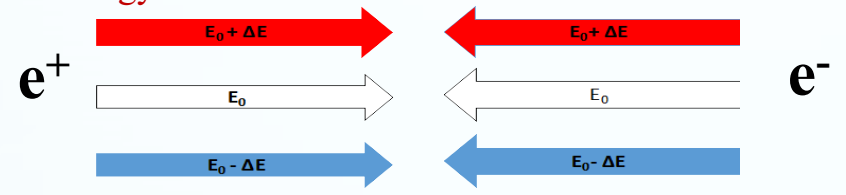
Transverse Monochromatization principle

Standard

$$D_{x,y}^* = 0$$

correlation between transverse spatial position and energy deviation

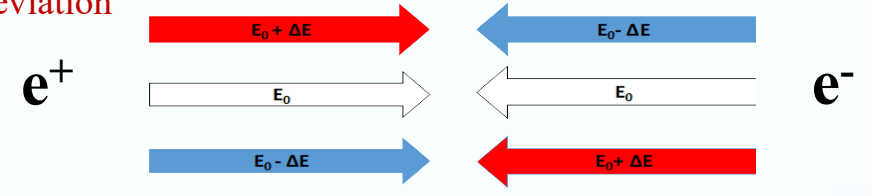
IP



Monochromatization

Opposite correlations between transverse spatial position and energy deviation

IP



$$D_{x+}^* = -D_{x-}^* = D_x^*$$

$$D_{y+}^* = -D_{y-}^* = D_y^*$$

Dispersion function at the IP created by bending dipoles, when different from zero contribute to the beam size

CM energy

$$w = 2(E_b + \Delta E)$$

$$w = 2E_b + O(\Delta E)^2$$

Monochromatization factor

$$\lambda = \left(1 + \sigma_\delta^2 \left(\frac{D_x^{*2}}{\sigma_{x\beta}^{*2}} + \frac{D_y^{*2}}{\sigma_{y\beta}^{*2}} \right) \right)^{1/2}$$

$$\sigma_w = \sqrt{2} E_b \sigma_\delta$$

$$\sigma_w = \frac{\sqrt{2} E_b \sigma_\delta}{\lambda}$$

Enhancement of energy resolution, and sometimes increase of the relative frequency of the events at the center of of the distribution but luminosity loss !!!!

Number of bunches k_b Revolution frequency f_r Particles per bunch $N_+ N_-$

$$L_0 = \frac{k_b f_r N_+ N_-}{4\pi \sigma_{x\beta}^* \sigma_{y\beta}^*}$$

betatronic beam sizes at the IP

$$L = \frac{L_0}{\lambda}$$

dispersive beam size at the IP

Transverse Monochromatization principle

According to the formula of monochromatization factor, we can choose to introduce horizontal dispersion or vertical dispersion to the IP. Because the vertical beam size at the IP is much smaller than horizontal beam size, about ten times smaller vertical dispersion is needed to get the same monochromatization factor compared with the horizontal one.

| Parameters | Unit | Horizontal Dispersion | Vertical Dispersion |
|---|---------------|-----------------------|---------------------|
| Beam energy(E) | GeV | 62.5 | |
| Horizontal, vertical emittance($\epsilon_{x,y}$) | nm | 0.51, 0.002 | |
| Energy spread(σ_δ) | % | 0.052 | |
| Beam length(σ_δ) | mm | 3.3 | |
| IP Beta function($\beta^*_{x,y}$) | mm | 90, 1 | |
| IP RMS beam size ($\sigma_{x,y}$) | μm | 55, 0.045 | |
| Crossing Angle(θ_c) | mrad | 30 | |
| Vertical beam-beam parameter(ξ_y) | / | 0.106 | |
| Beam current(I_0) | mA | 395 | |
| Bunch population(N_b) | 10^{11} | 0.6 | |
| Bunches per beam(n_b) | / | 13420 | |
| IP Dispersion ($D^*_{x,y}$) | m | 0.105 | 0.01 |
| Monochromatization factor (λ) | / | 8.1209 | 11.6705 |

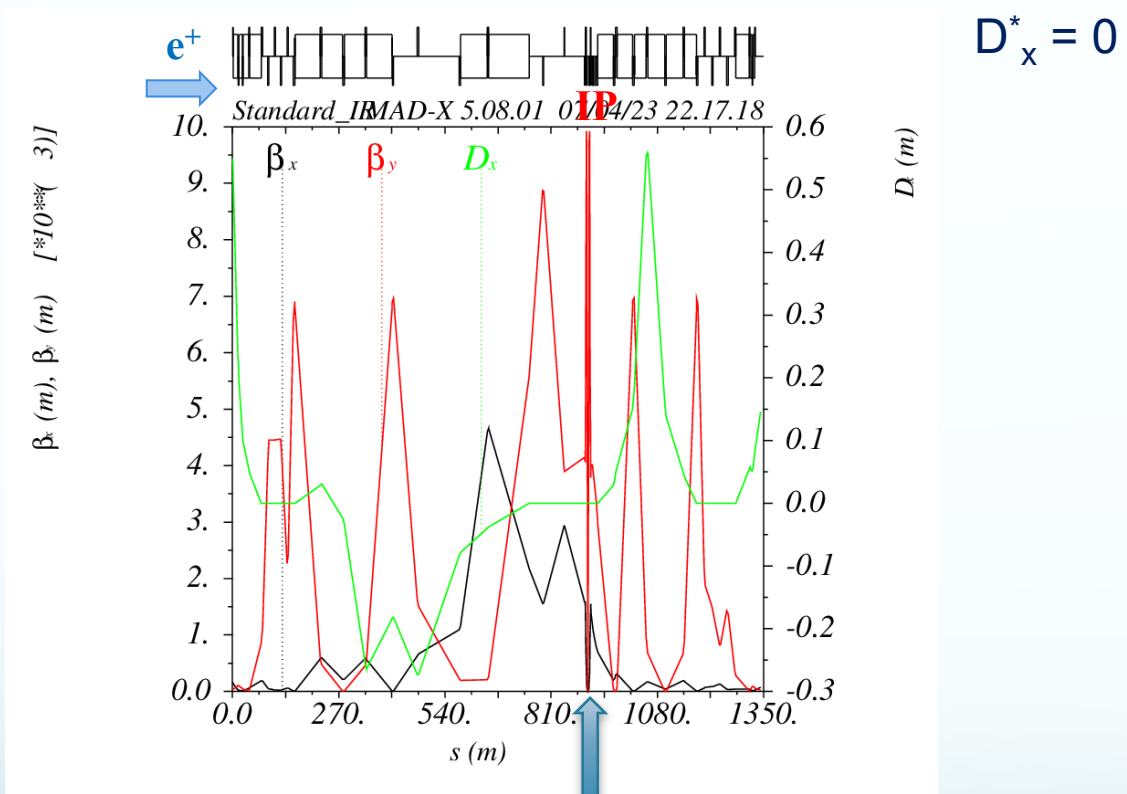
Monochromatization factor

$$\lambda = \left(1 + \sigma_\delta^2 \left(\frac{D_x^{*2}}{\sigma_{x\beta}^{*2}} + \frac{D_y^{*2}}{\sigma_{y\beta}^{*2}} \right) \right)^{1/2}$$

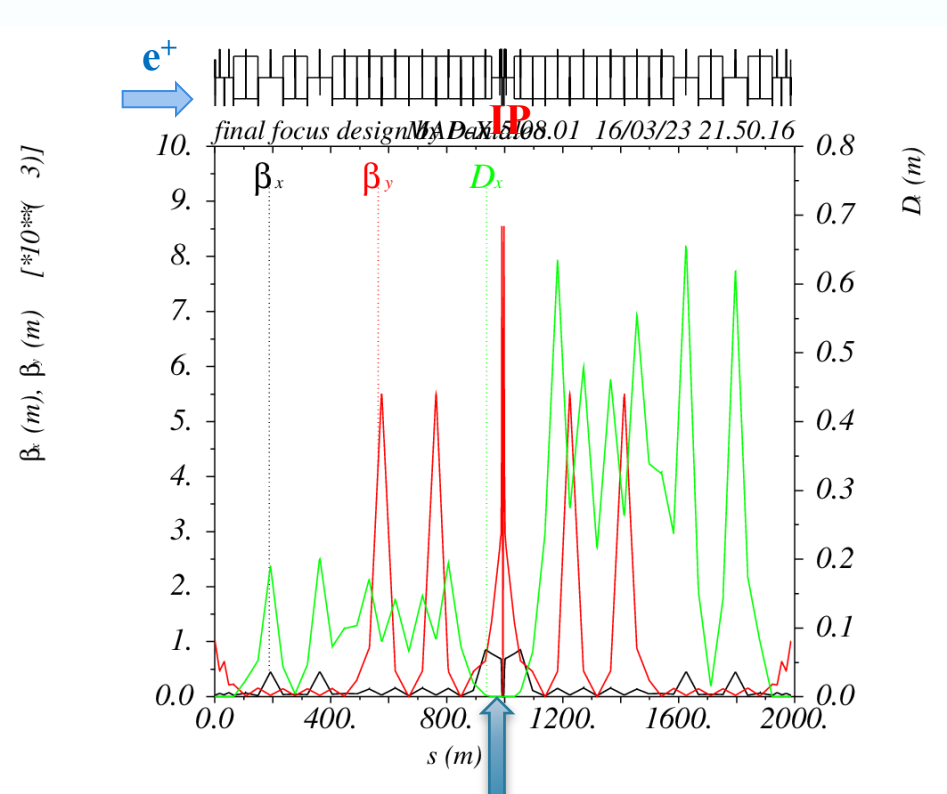
Parameters checked in Mathematica

FCC-ee Monochromatization Scheme Implementation

Scheme for Asymmetrical Standard IR Optics



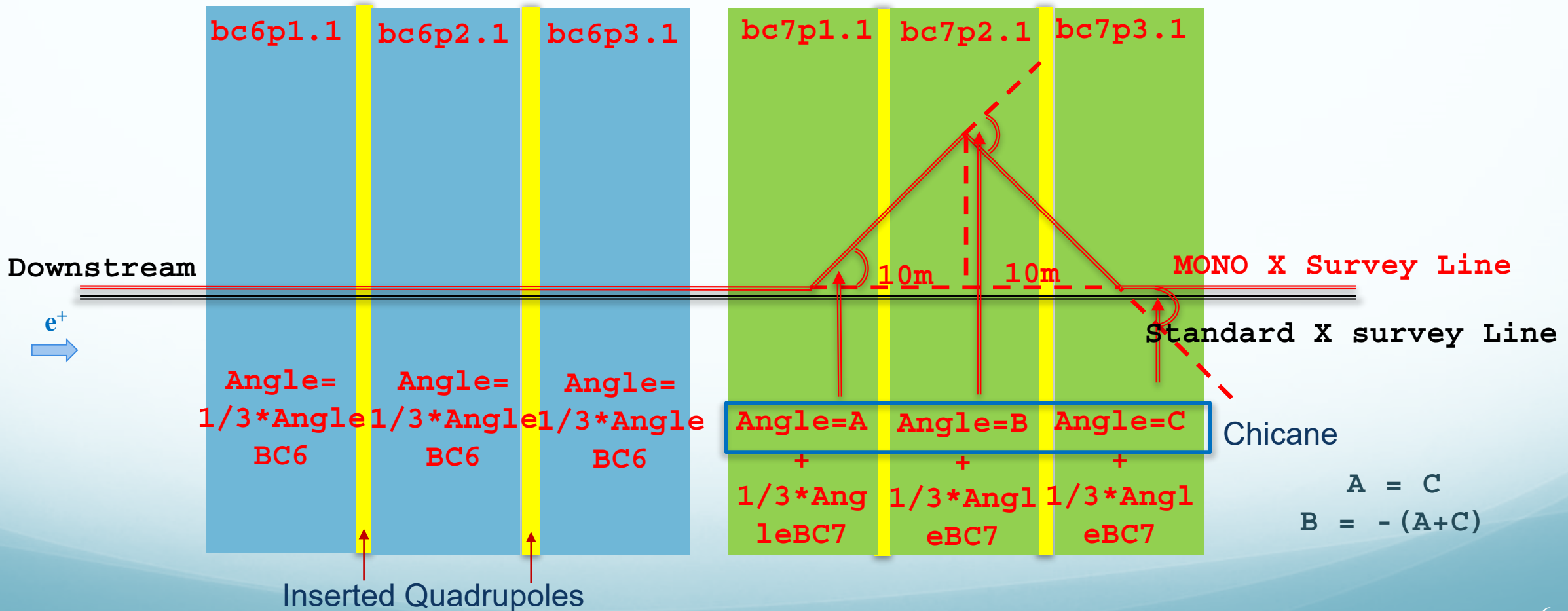
Scheme for Symmetrical Standard IR Optics



Creating horizontal dispersion ($D_x^* = 0.105$ m)

Creating vertical dispersion ($D_y^* = 0.01$ m)

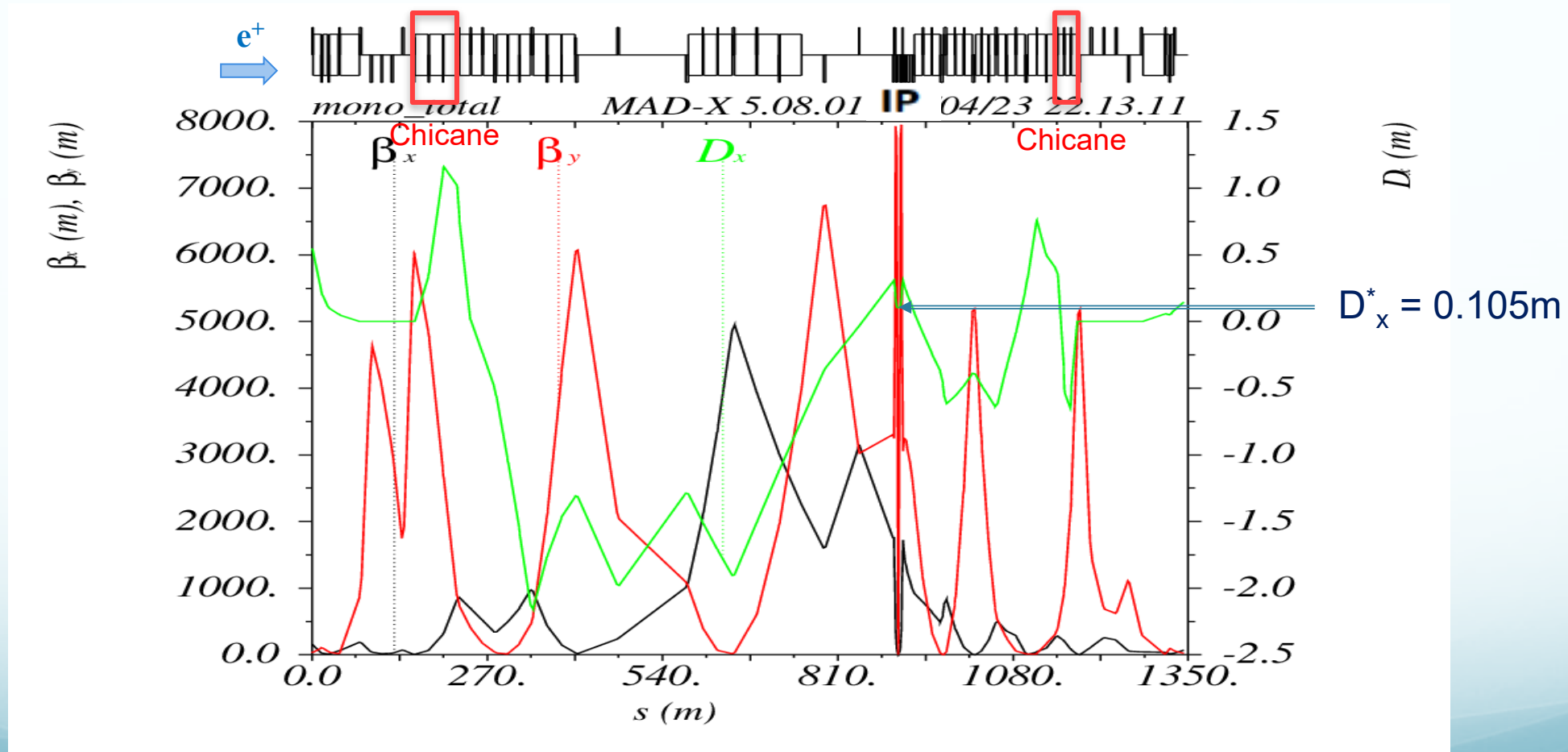
All local vertical chromaticity dipoles in standard IR Optics are cut into three pieces and quadrupoles are inserted between them. One Chicane is implemented in the last dipole in each upstream and downstream to create the dispersion in the IP and to match the dispersion in the arcs while keeping the orbit.



Fcc-ee Monochromatization optics design

Monochromatization optics design base on the asymmetrical standard IR optics

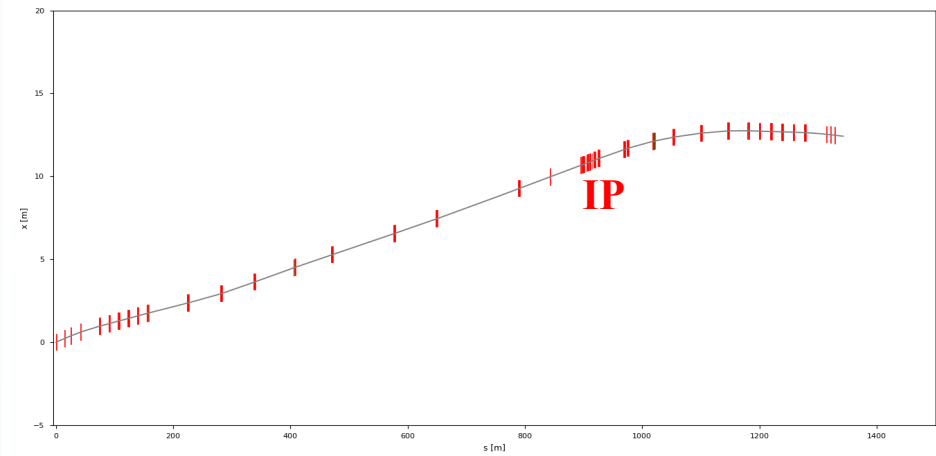
- Monochrom Optics



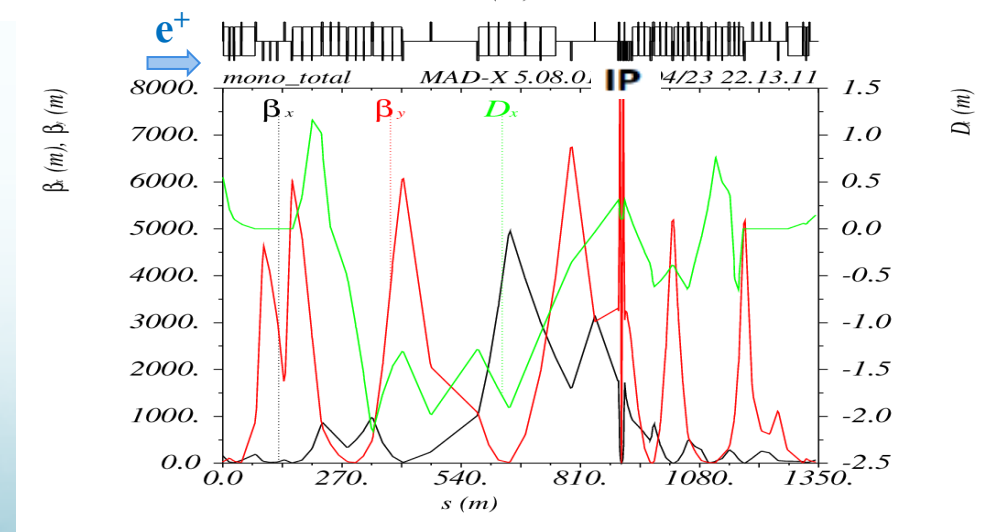
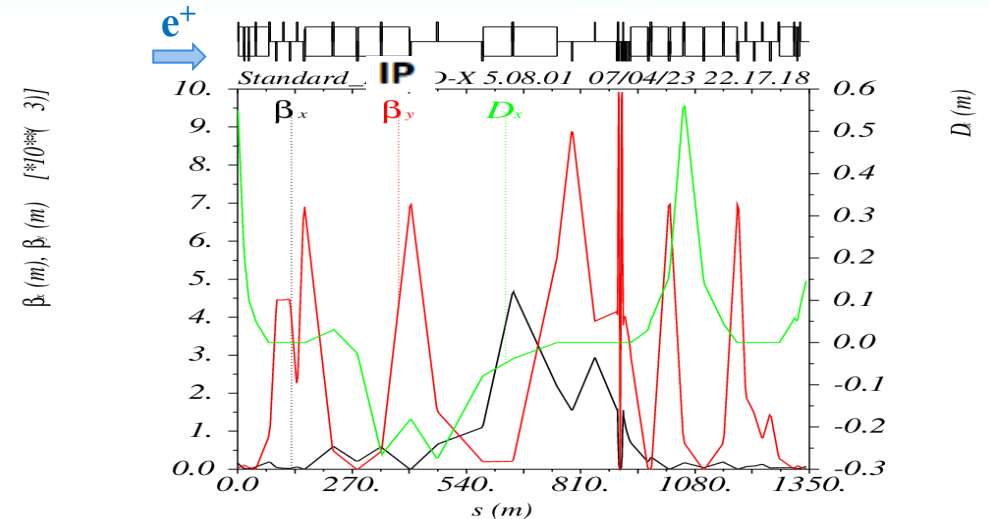
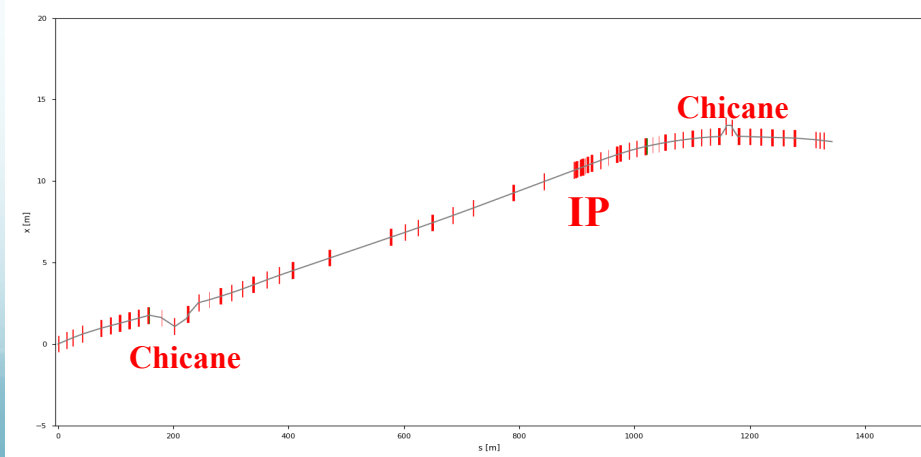
Fcc-ee Monochromatization optic design

Comparison between standard survey and MonochromM survey

- $D_x^* = 0$ Standard Survey



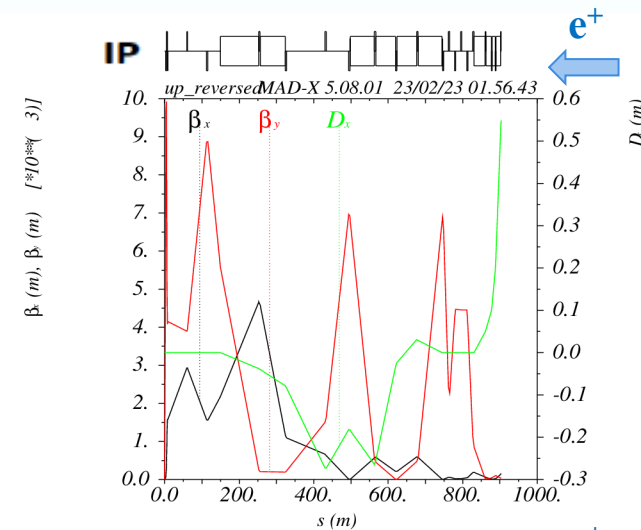
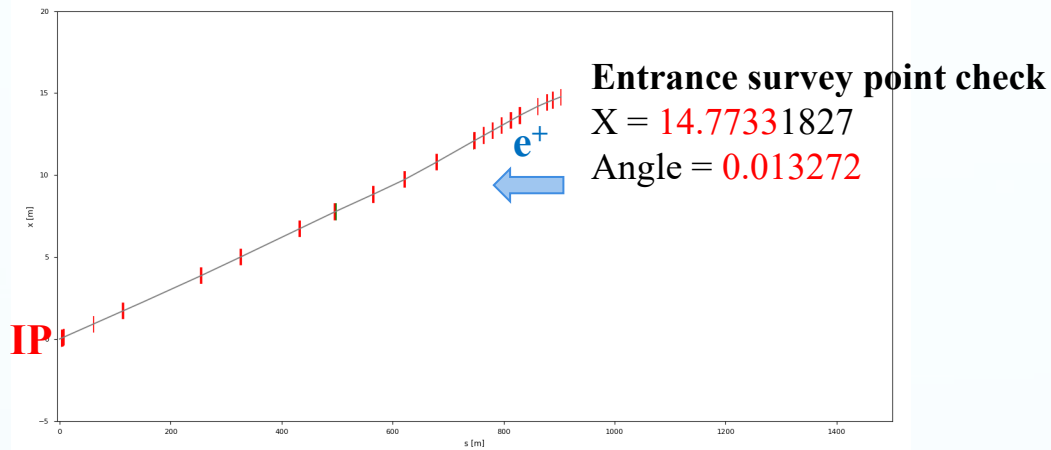
- $D_x^* = 0.1$ m Monochromatization Survey



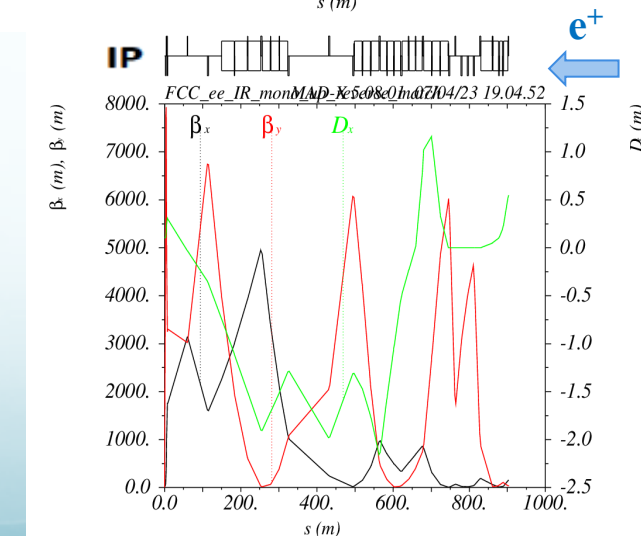
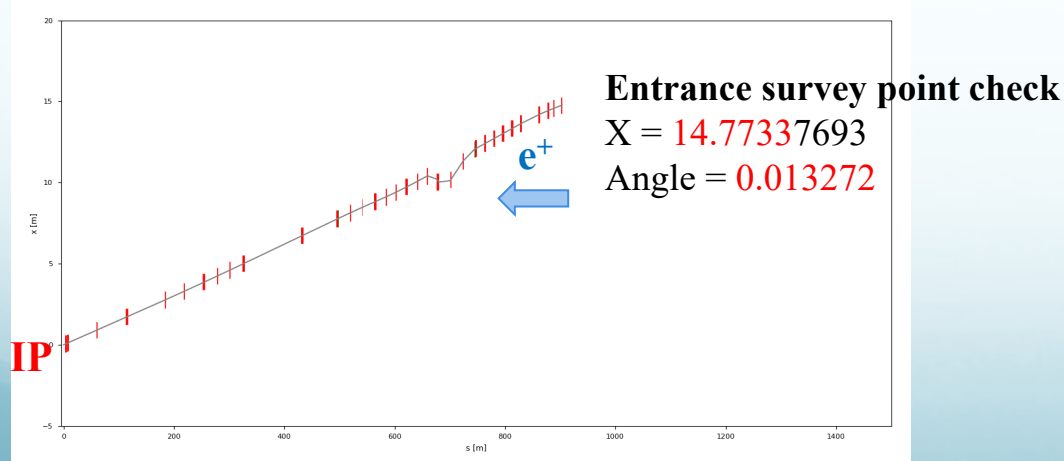
Fcc-ee Monochromatization optic design

Upstream entrance survey point check and beam parameter check

- $D_x^* = 0$ Standard



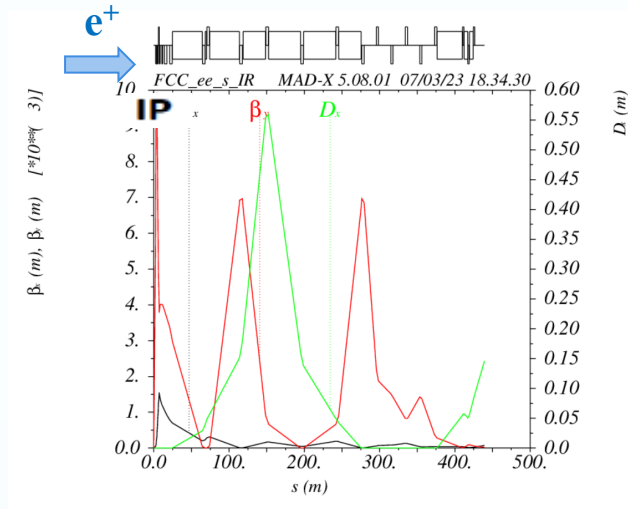
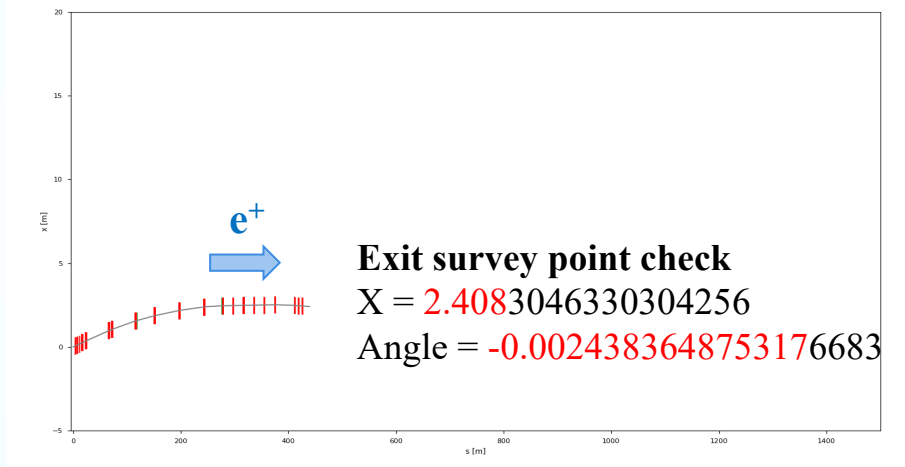
- $D_x^* = 0.1$ m Monochromatization



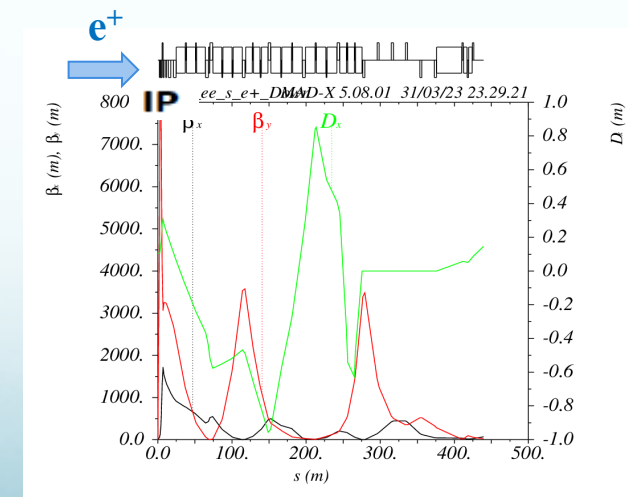
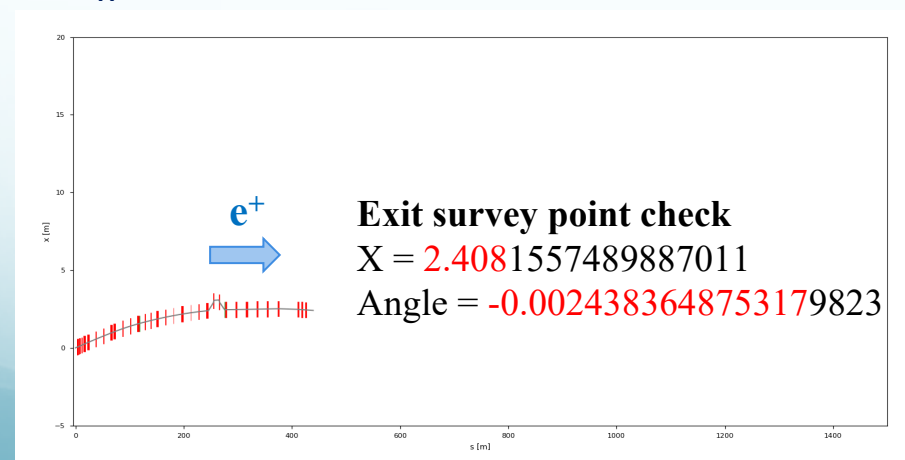
Fcc-ee Monochromatization optic design

Downstream exit survey point check and beam parameter check

- $D_x^* = 0$ Standard



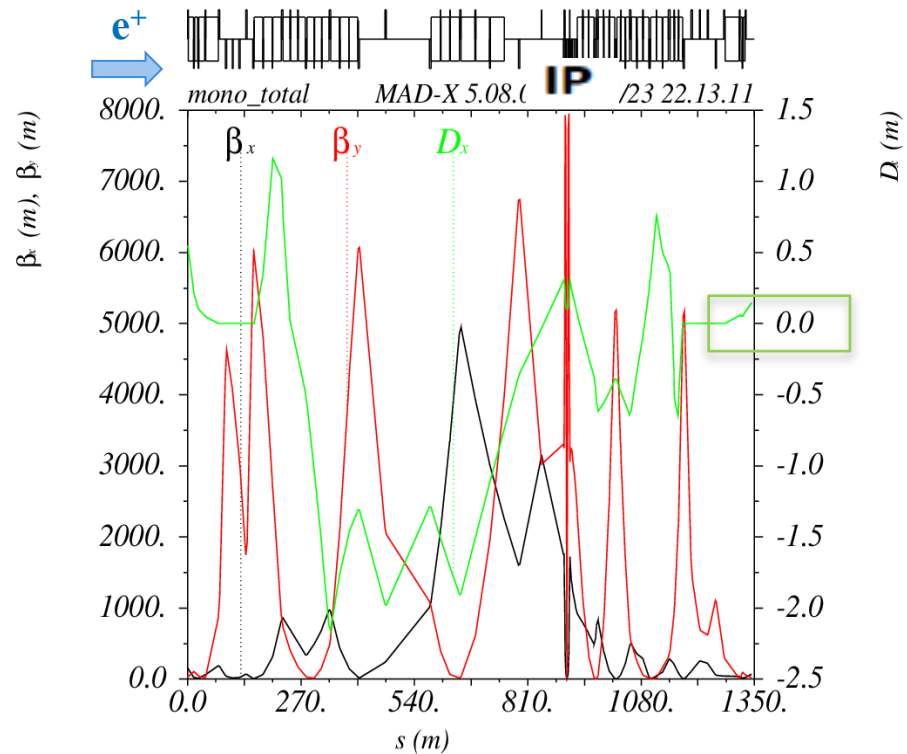
- $D_x^* = 0.1$ m Monochromatization



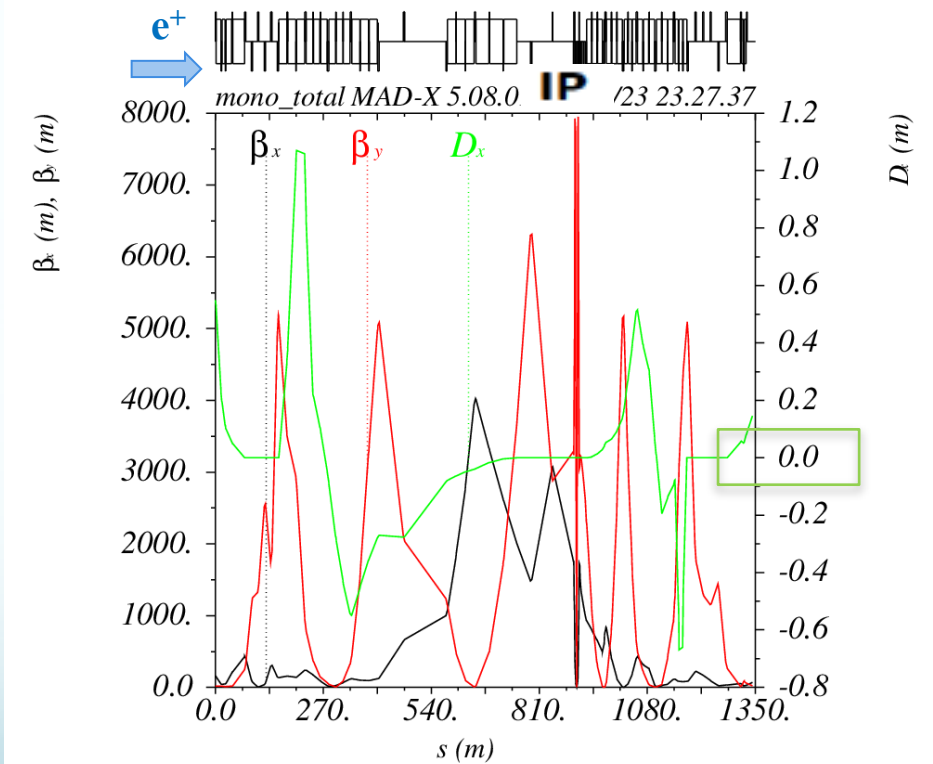
Standard Mode with monochromatization orbit

Frozen the angle of all the dipoles of monochromatization optics (keeping the monochromatization orbit), matching only with the strength of all the quadrupoles to get the dispersion at the IP back to zero.

- $D_x^* = 0.1$ m Monochrom Optics

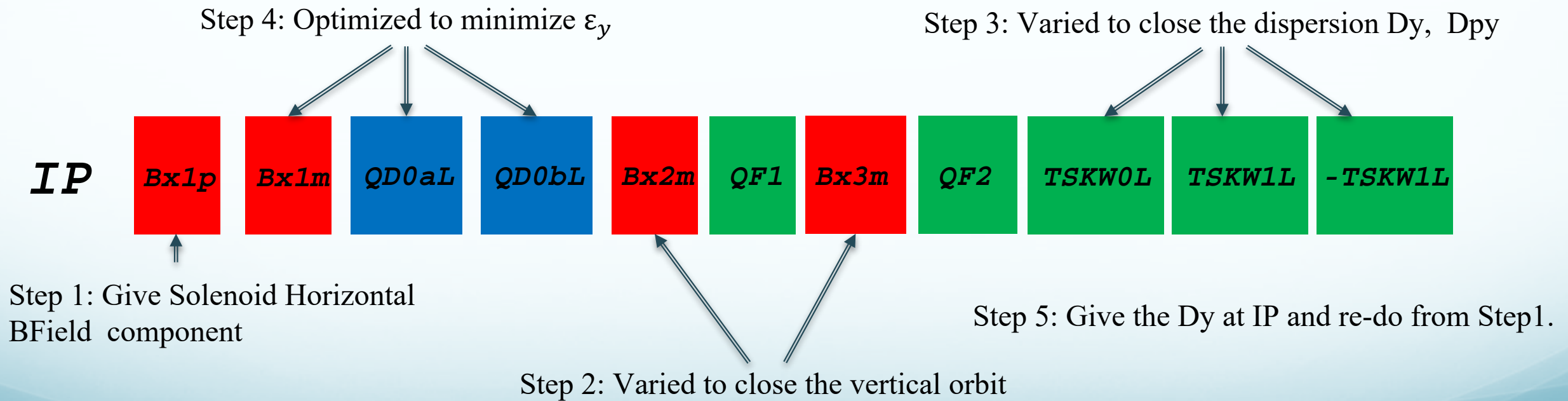


- $D_x^* = 0$ Monochrom Optics



Scheme for Symmetrical Standard IR Optics

Creating the vertical dispersion by adjusting the correctors and skew quadrupoles around the IP solenoid. It will take the following five steps to get the vertical dispersion at the IP.

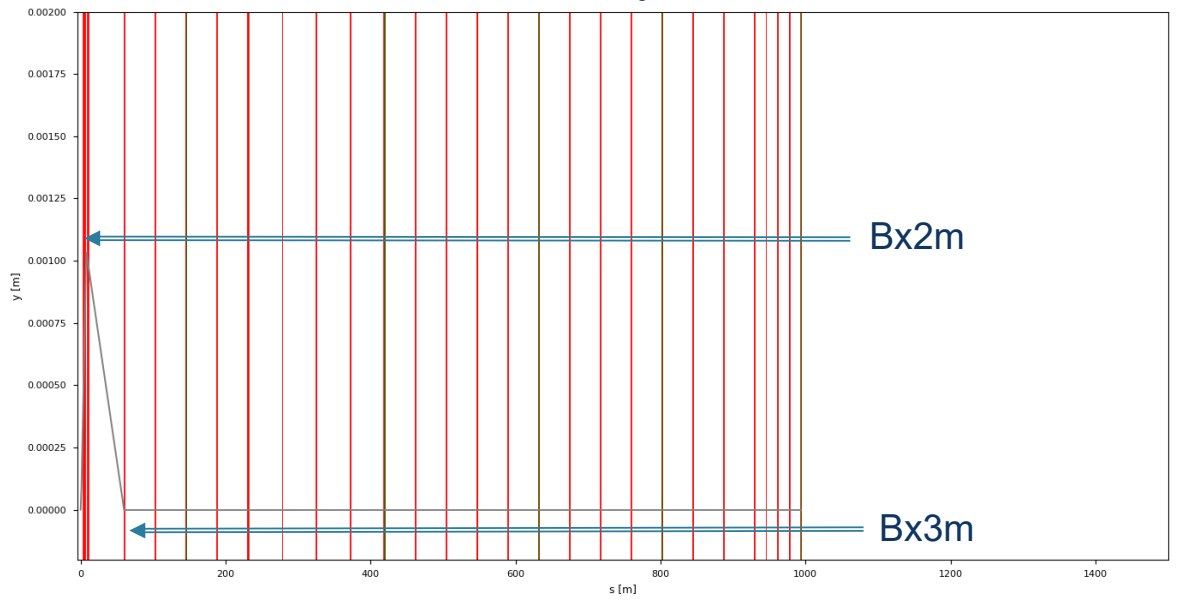


Symmetrical Standard IR Optics

Solenoid implementation

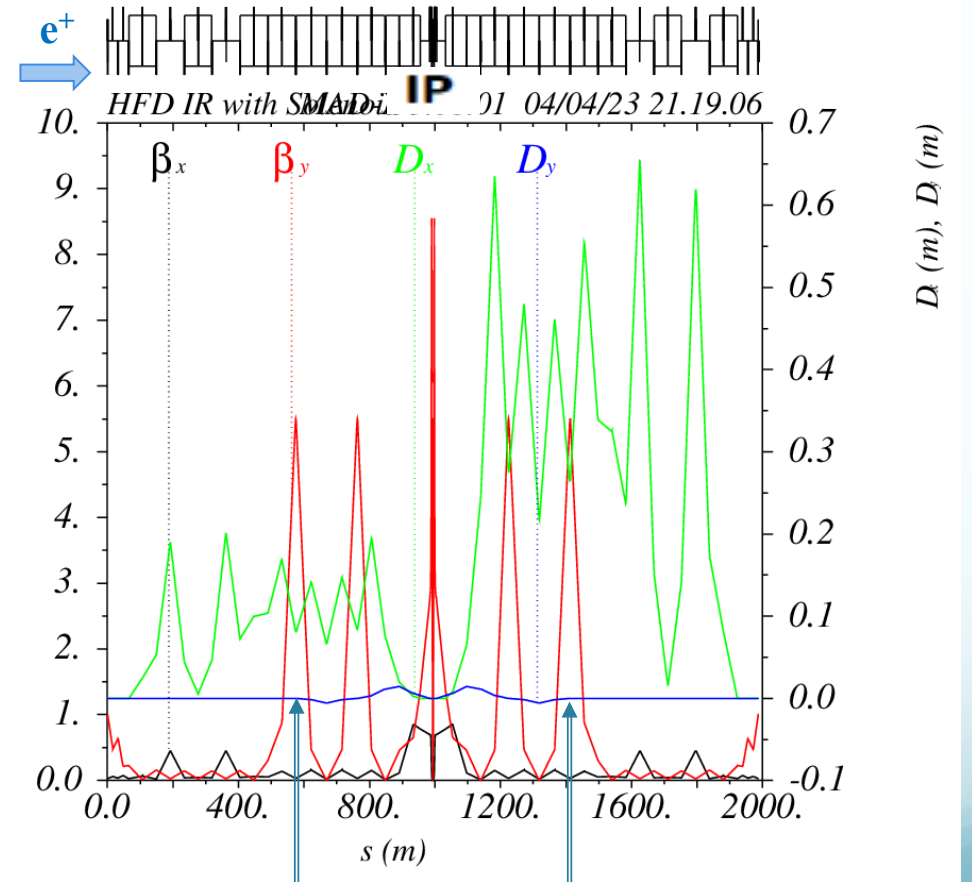
Vertical orbit and vertical dispersion was closed after implementing the solenoid.

Downstream Vertical Survey Plot



Vertical orbit back to 0 after Bx3m

Next step: calculating and minimizing the vertical emittance.



Vertical dispersion closed.

- **Asymmetrical IR Monochromatization Optics design**

- ✓ The monochromatization optics design for positron
- ✓ Survey plot and beam parameters check
- ✓ Standard Mode with monochromatization orbit
- Try to insert the monochromatization IR optics to the ring

- **Symmetrical IR Monochromatization Optics design**

- ✓ Solenoid implement
- ✓ Closing vertical orbit and vertical dispersion
- Calculate and minimize the vertical emittance

Thanks for you attention!