

DC-DC Converter Development for the CMS Pixel Upgrade

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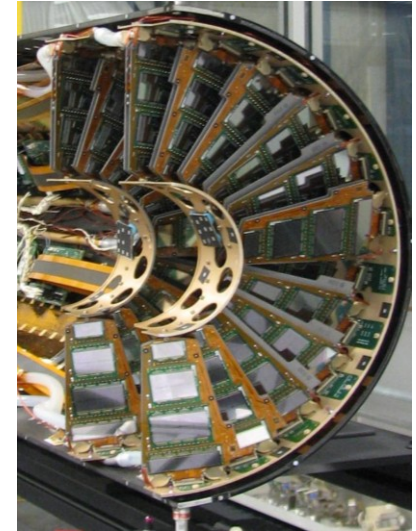
The CMS Tracker Upgrade



2017/2018: Exchange of the CMS pixel detector

- Less material, reduced data losses etc.
- Number of readout chips (ROCs) increases by factor 1.9
- Unacceptable power losses in cable trays
- Compatibility with existing power supply chain desirable

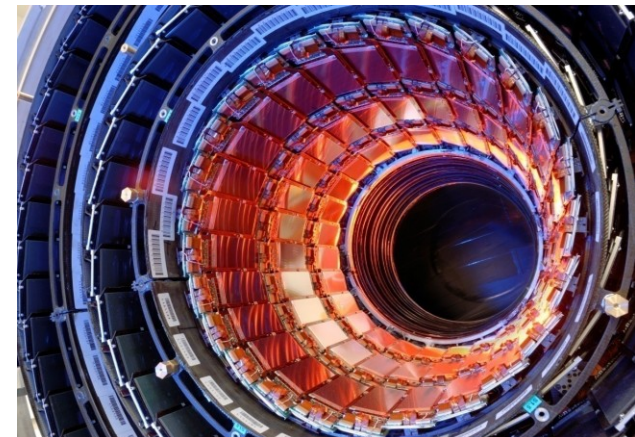
→ DC-DC buck converters with conversion ratio of 2-3



> 2020: Exchange of the CMS tracker

- Higher granularity → more readout channels
- Additional functionality (track trigger) needs power

→ DC-DC converters with conversion ratio of 8-10

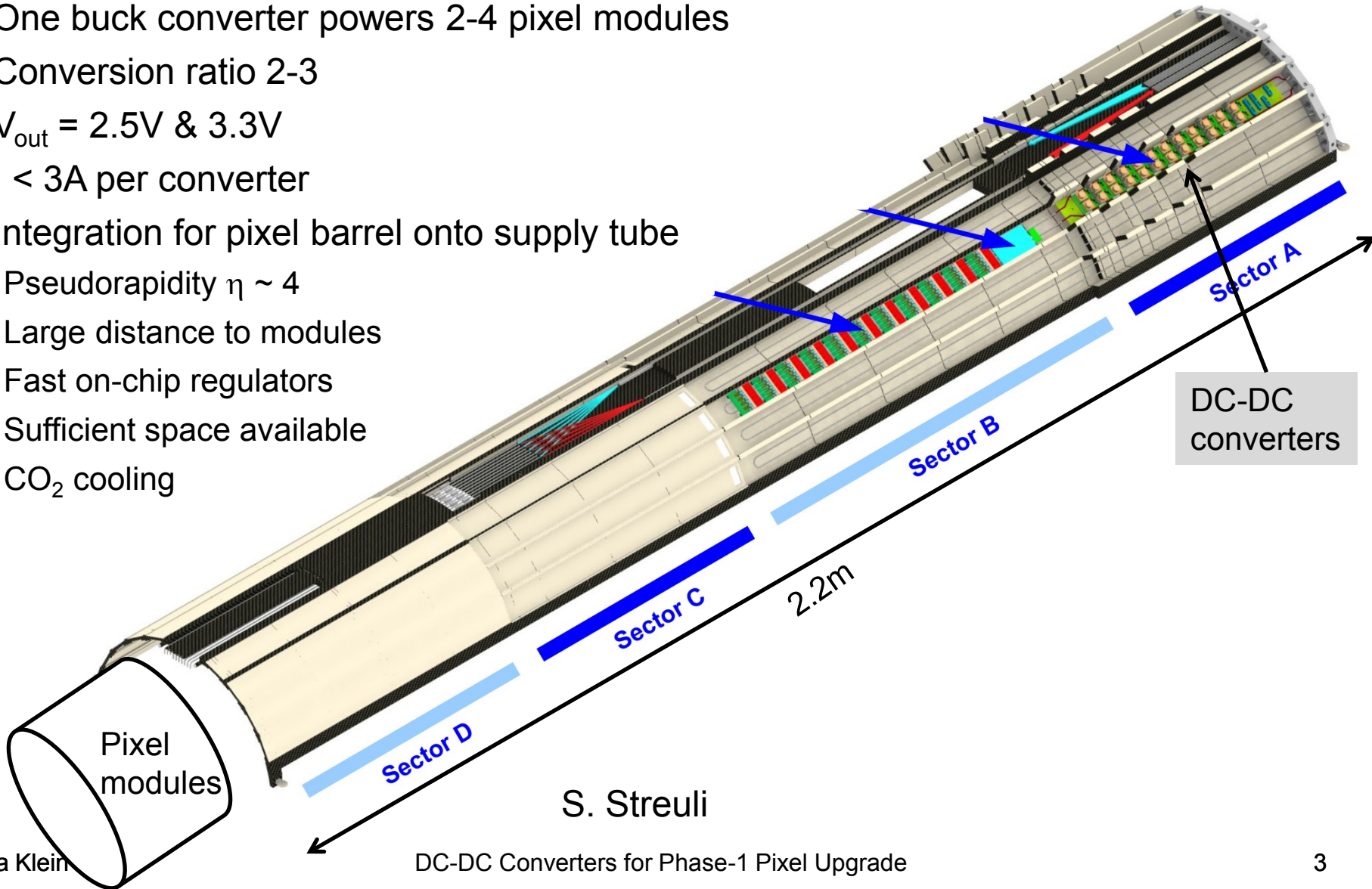




DC-DC Converters for the Pixel Upgrade

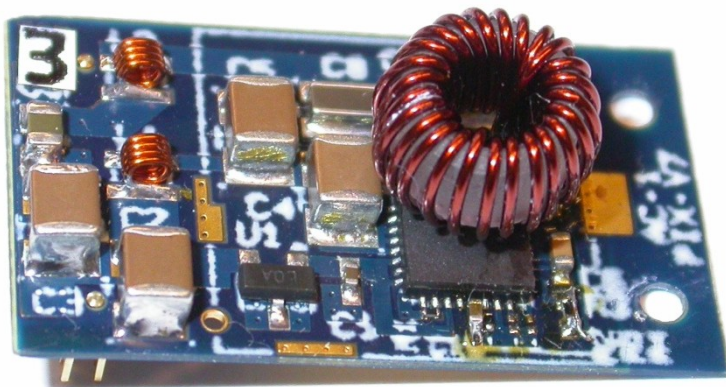


- One buck converter powers 2-4 pixel modules
- Conversion ratio 2-3
- $V_{out} = 2.5V$ & $3.3V$
- $I < 3A$ per converter
- Integration for pixel barrel onto supply tube
- ✓ Pseudorapidity $\eta \sim 4$
- ✓ Large distance to modules
- ✓ Fast on-chip regulators
- ✓ Sufficient space available
- ✓ CO_2 cooling





PIX_V7



$M = 2.3\text{g}$
 $A = 28 \times 16 \text{ mm}^2$

ASIC: AMIS2 by CERN

$I_{out} < 3\text{A}$
 $V_{in} < 12\text{V}$
 V_{out} configurable; 2.5V & 3.3V
 f_s configurable, e.g. 1.3MHz

PCB:

2 copper layers a 35 μm
 0.3mm thick
 Large metallic ground area on bottom
 for cooling

Toroidal inductor:

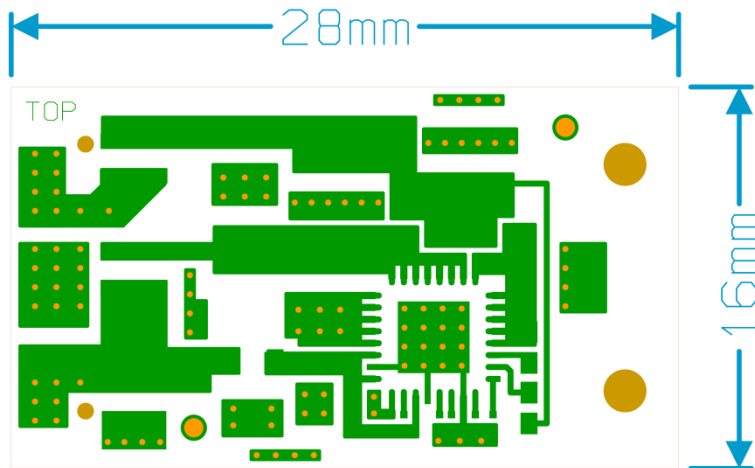
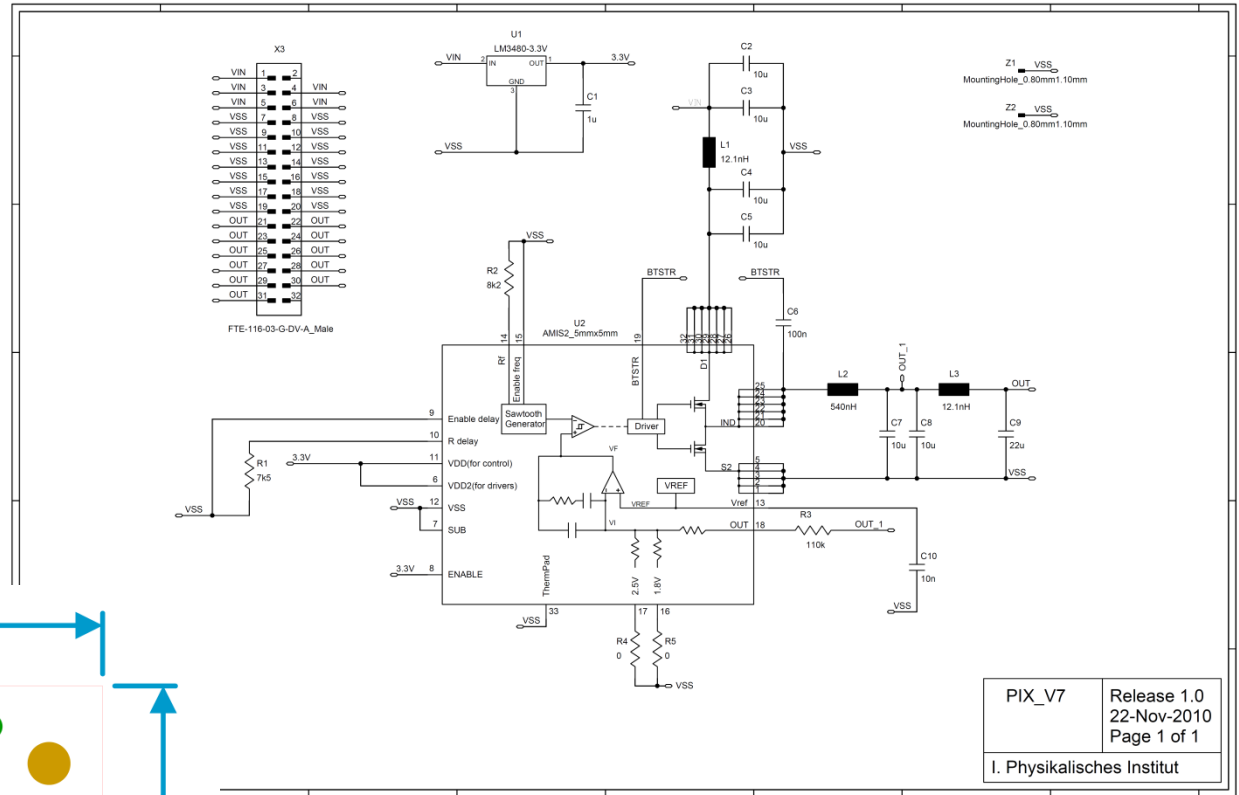
$L = 450\text{nH}$
 $R_{DC} = 40\text{m}\Omega$

Pi-filters at in- and output

Shield (soldered to GND pads of PCB):
 e.g. 150 μm Aluminium



DC-DC Buck Converter Development



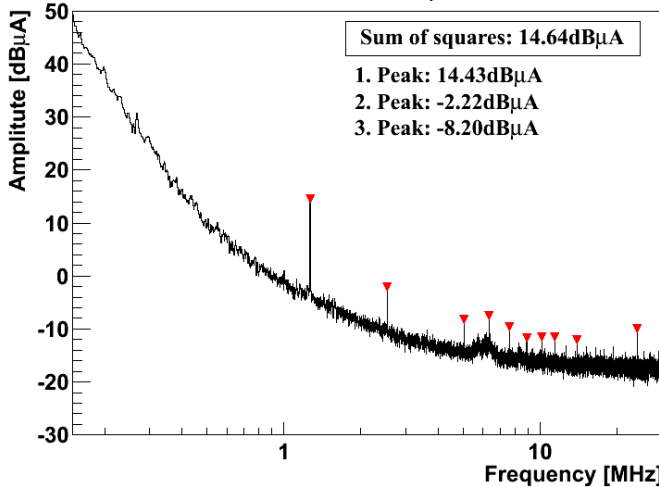
Design guidelines from CERN group have been followed.



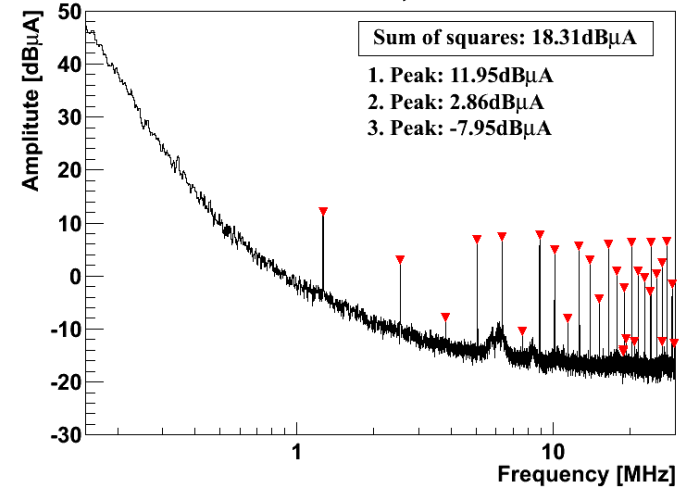
Conductive Noise at Converter Output



Differential Mode, no shield

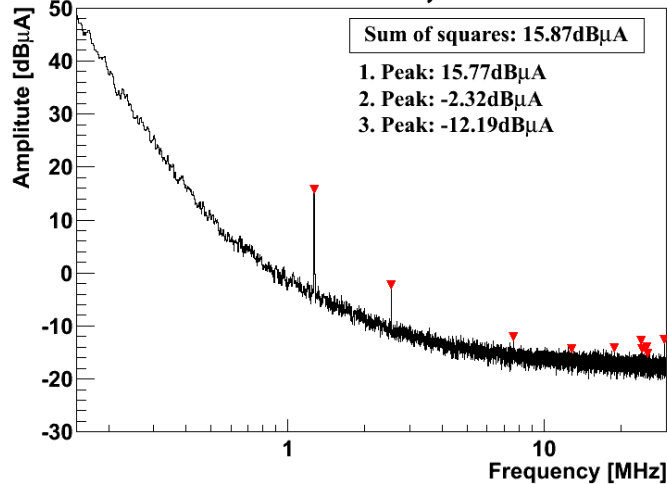


Common Mode, no shield

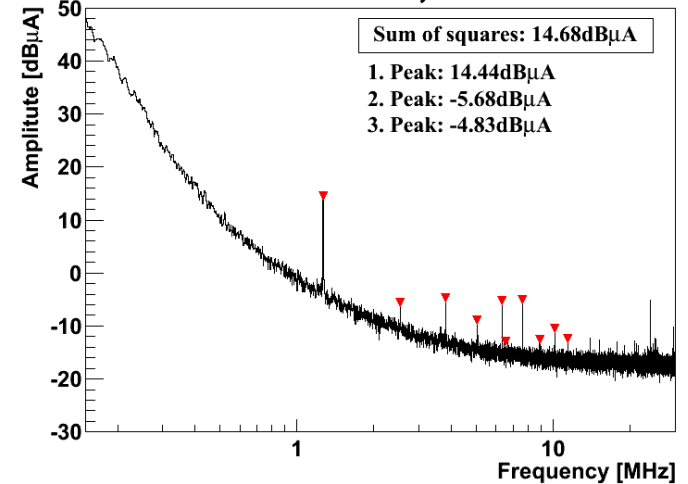


PIX_V7
Vout = 3.3V
Vin = 10V
fs = 1.3MHz
L = 450nH

Differential Mode, with shield



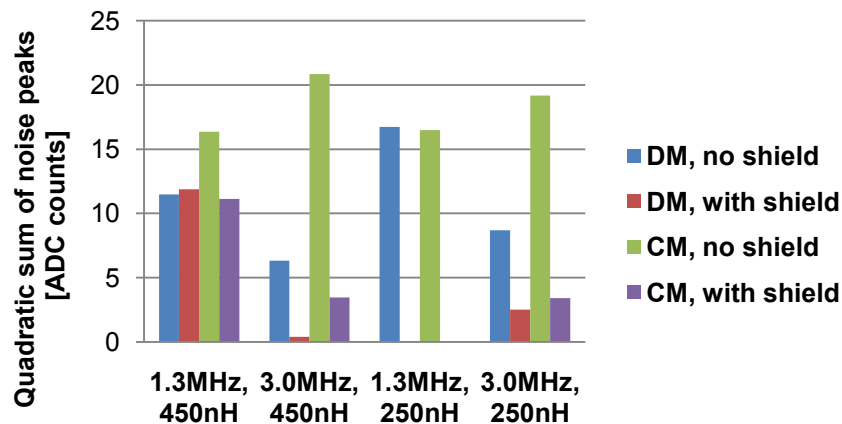
Common Mode, with shield



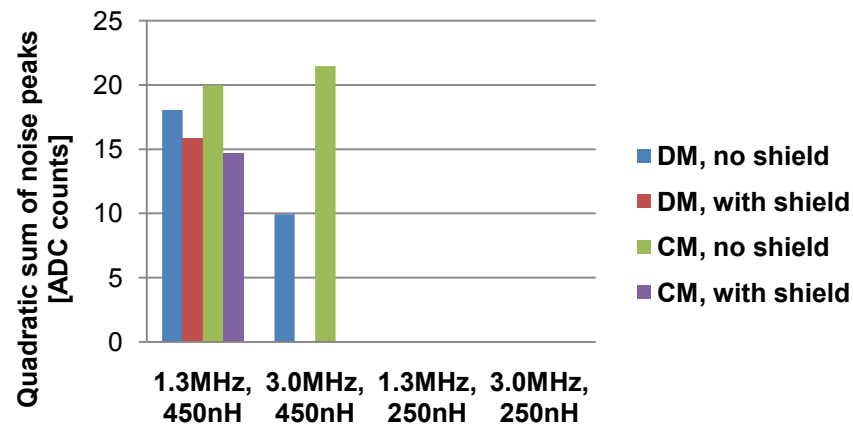
Shield most effective above \sim 2-3 MHz \rightarrow large reduction of CM, less red. for DM



2.5V, output noise

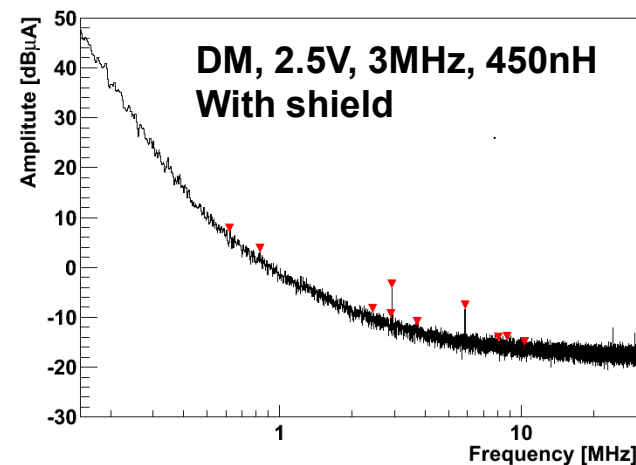


3.3V, output noise



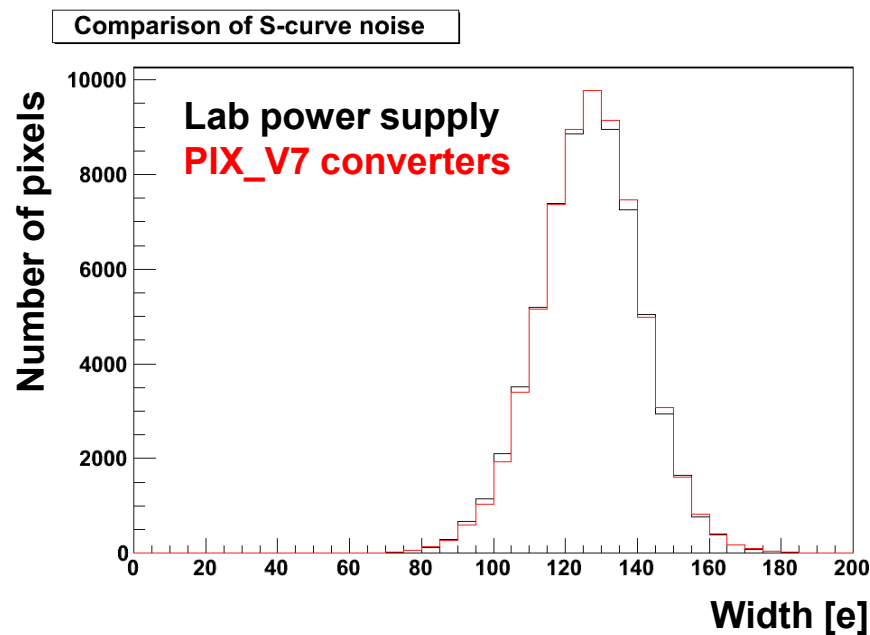
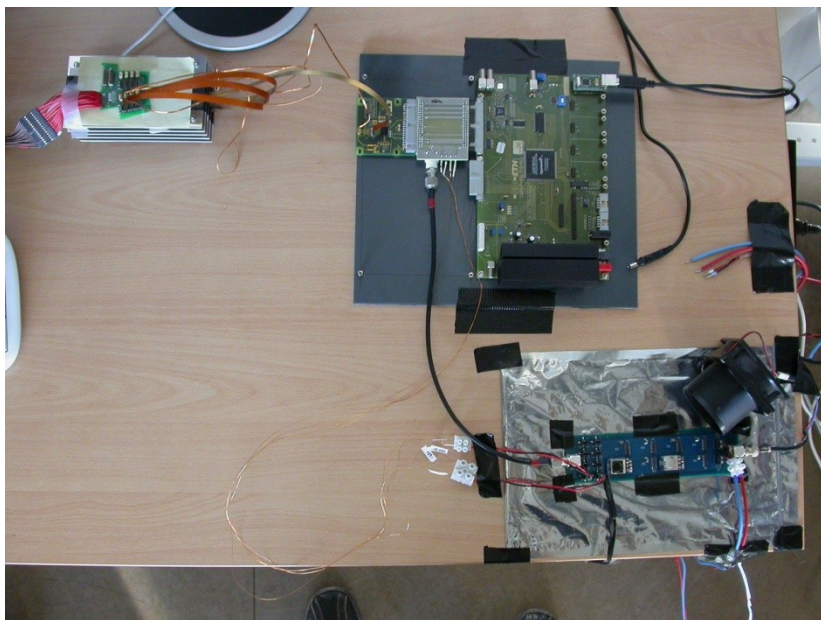
The conductive noise at the input and output has been studied under various conditions:

- Shield is more effective for switching frequency of (e.g.) 3MHz
- Larger DM noise for lower inductance





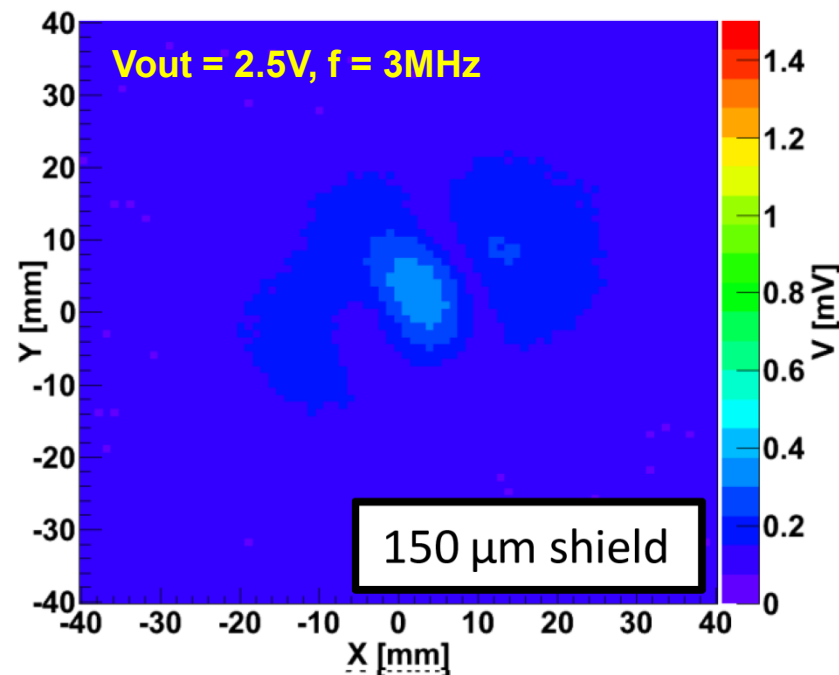
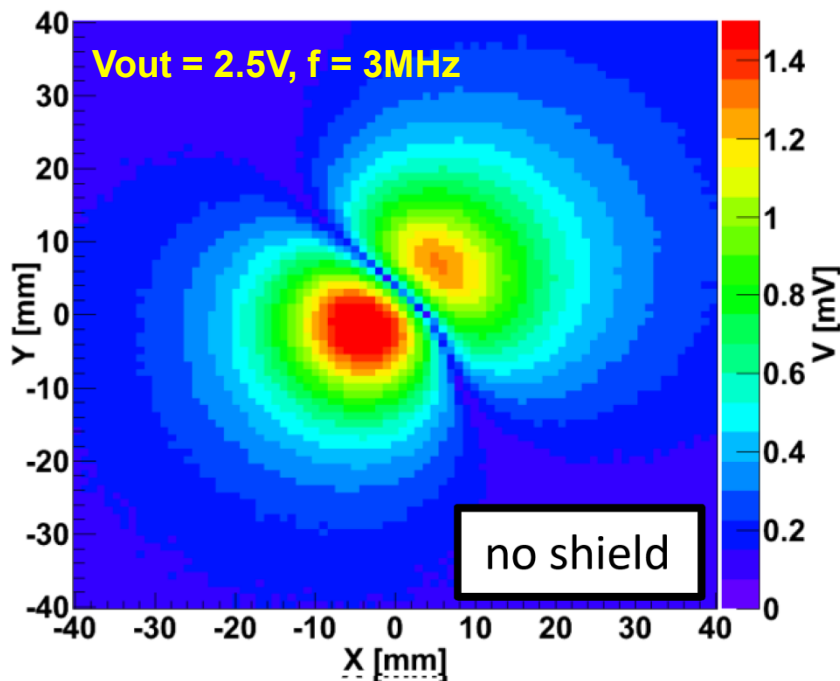
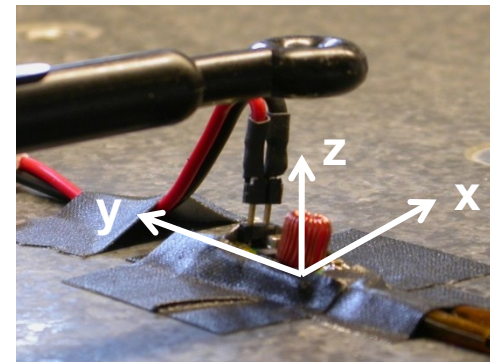
- Tests with pixel modules have to tell if noise is acceptable & what frequency is preferred!
- Measurement of S-curve with and without DC-DC converters
- Width of S-curve is taken as noise figure
- Pixel modules seem to be rather insensitive to ripple from V7 converters
- Work in progress ...





Field measured with pick-up probe $\sim 1.5\text{mm}$ above coil

- Both $150\mu\text{m}$ & $50\mu\text{m}$ Aluminium shields are very effective
- Plastic shields coated with $\sim 20\mu\text{m}$ Alu or Cu less effective
- Larger emissions for lower inductance (250nH)
- Larger emissions with higher switching frequency (but can be shielded)





More on Shields

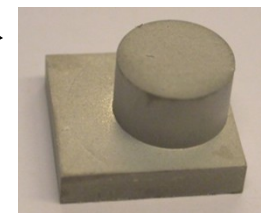
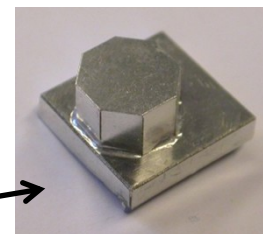


The shield has three functions:

- 1) to shield radiated emissions
- 2) to reduce conducted noise by means of segregation between noisy and quiet parts of board
- 3) to provide cooling contact for coil through its solder connection to PCB, since cooling through contact wires not sufficient (see later)

We are currently investigating several technologies:

- Aluminium shields of various thicknesses
- Plastic shields (PEEK) coated with a metall layer (outside, inside & outside)
 - Aluminium sputtered (5 or 10 μ m)
 - Copper/tin sputtered (5 or 10 μ m)
 - Copper, galvanic deposition (20 μ m)
 - Parylene coating of whole PCB ...

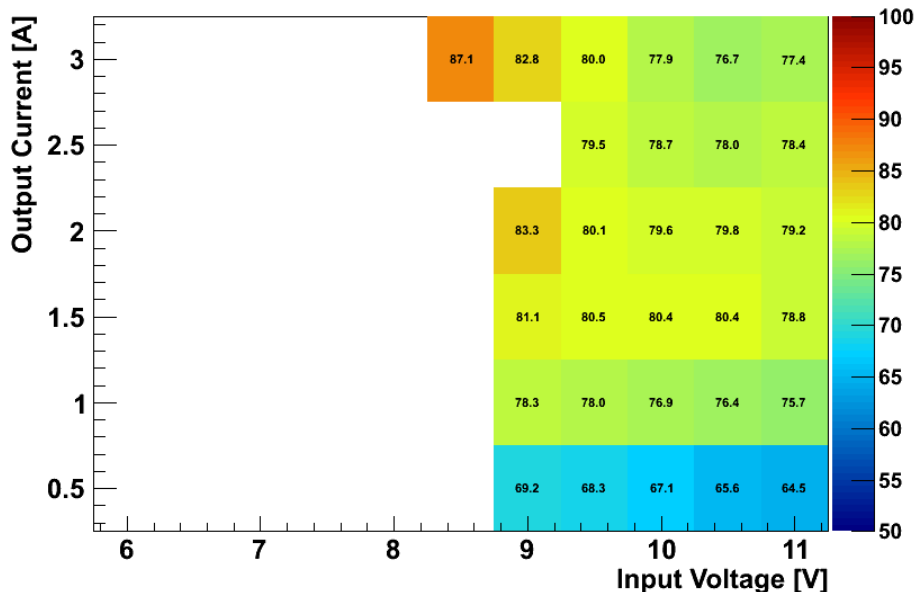


We are also in contact with industry to find industrial affordable solutions
(deep drawing, forming with water pressure, ...)



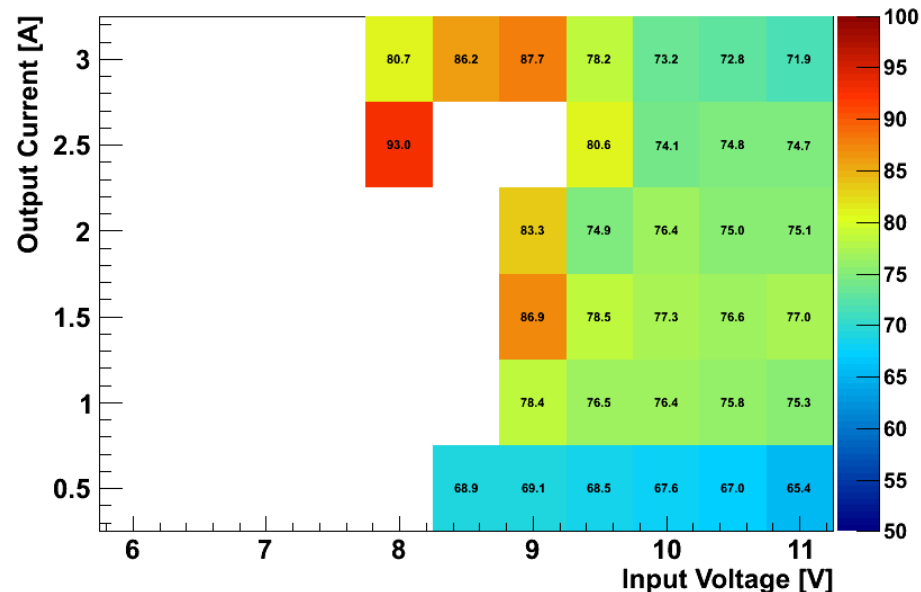
Vout = 3.2V, 1.3MHz, 437nH

Efficiency [%]



Vout = 2.5V, 1.3MHz, 450nH

Efficiency [%]

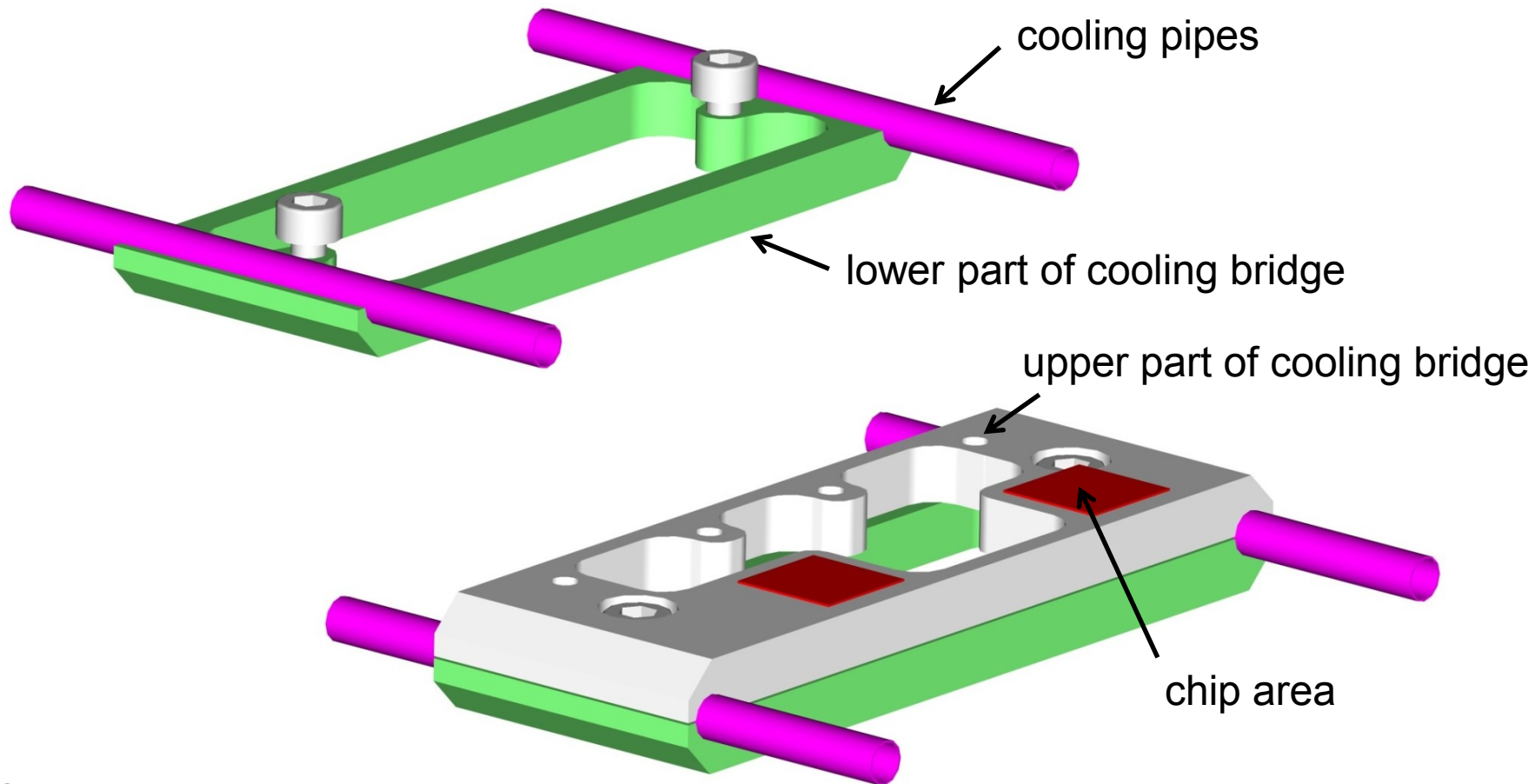


→ **Efficiencies are around 75%** (expected to increase for AMIS4 ASIC)

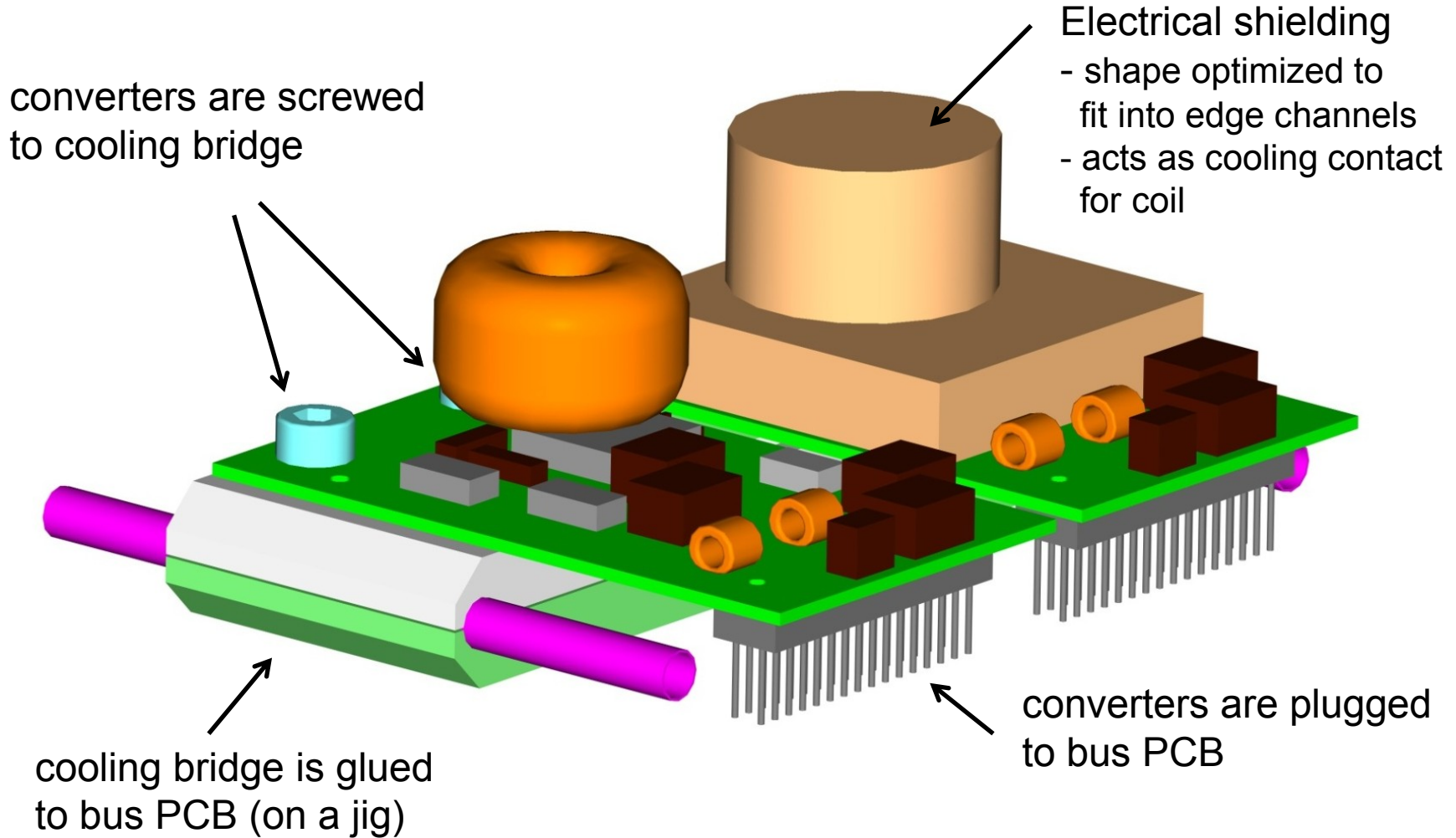
→ 5 -10% higher efficiency with 1.3MHz wrt 3MHz (for 450nH)

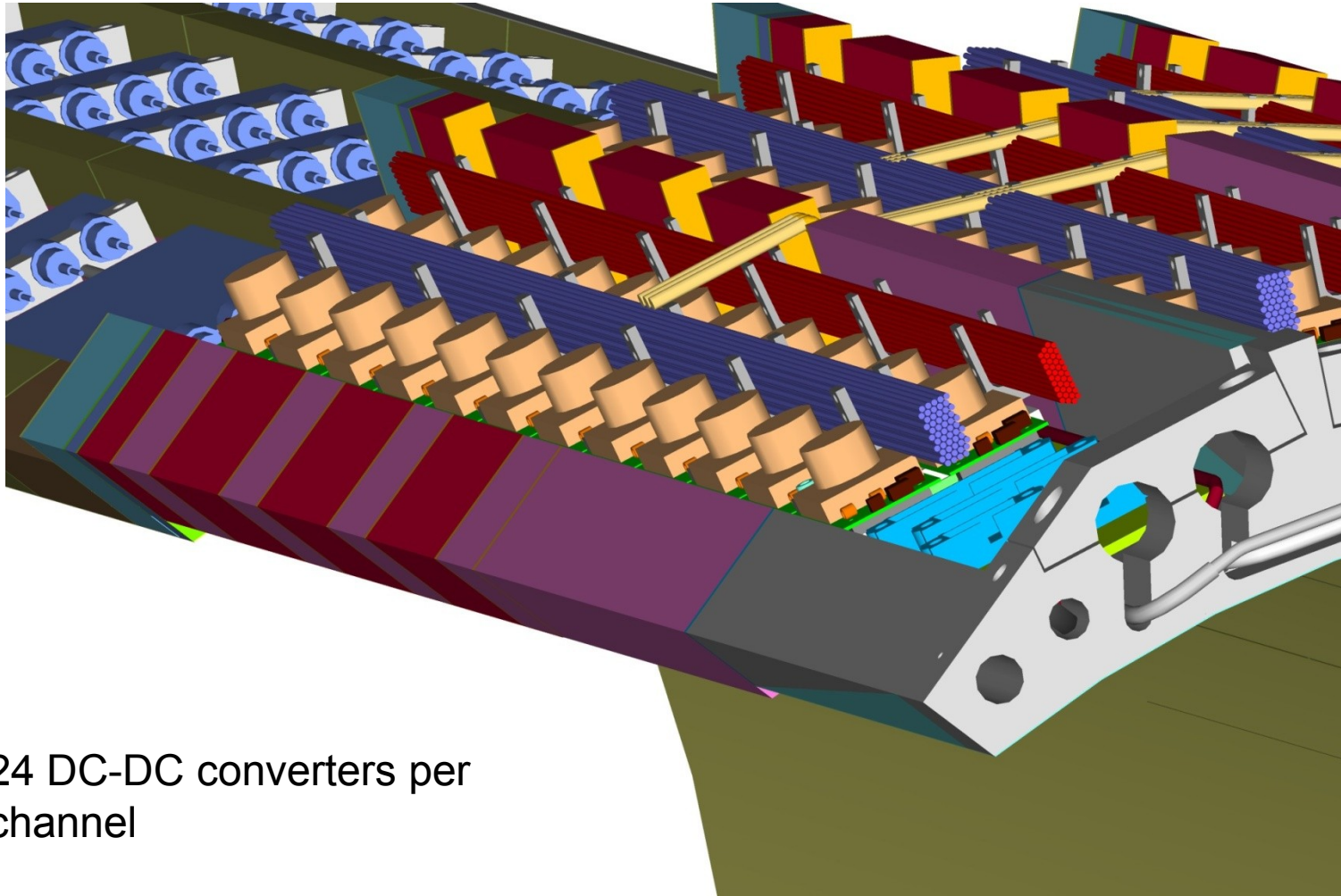
→ For lower inductance (250nH), 5-30% lower for 1.3MHz, 0-10% lower for 3MHz

→ suggests to stay with 1.3MHz if noise acceptable to pixel system; to be studied again with AMIS4



- Cooling bridge clamps around pipe
- Area reduced to reduce material
- Aluminium (could be Graphite, but gain for material budget is low)



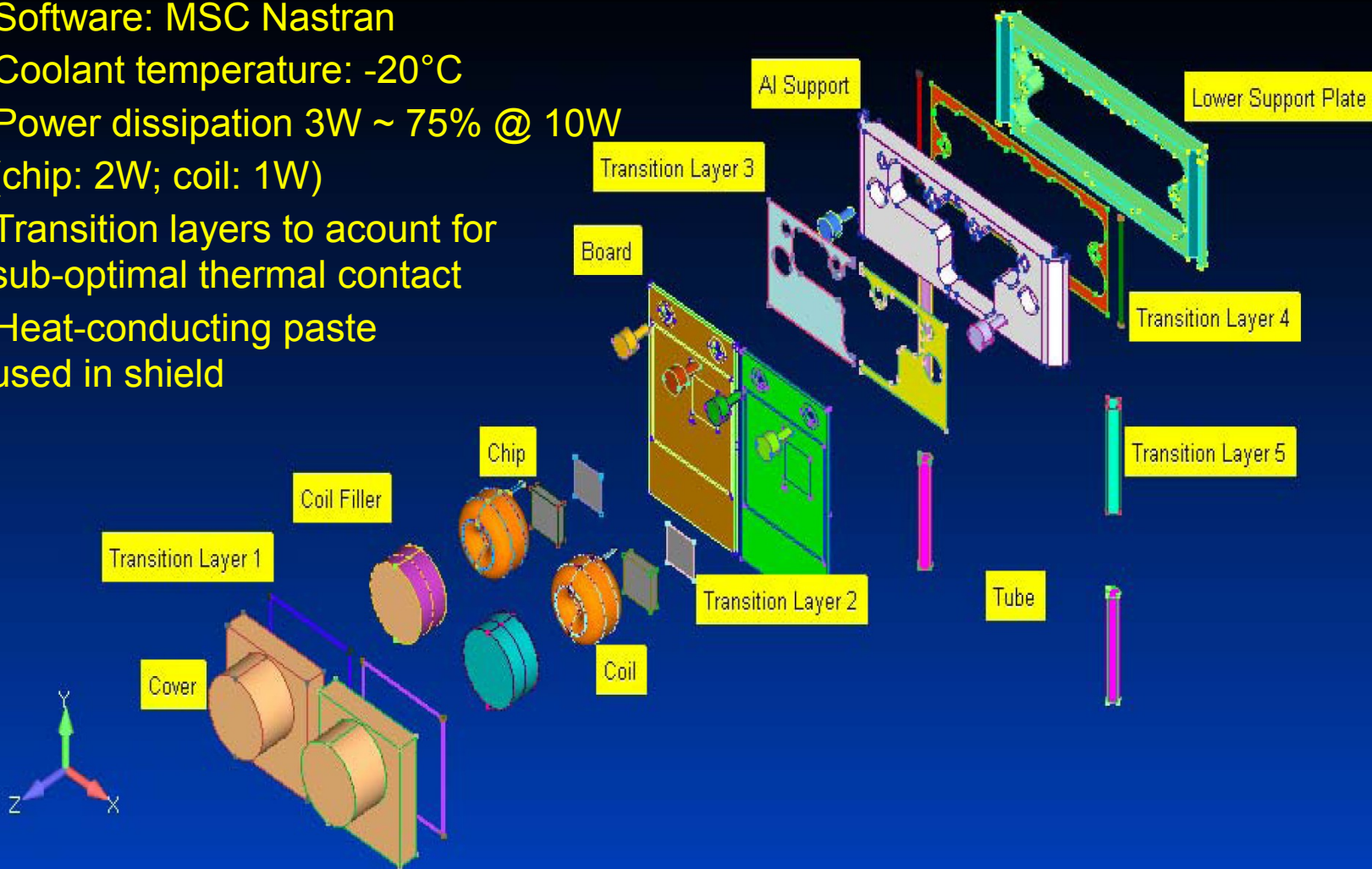


24 DC-DC converters per channel



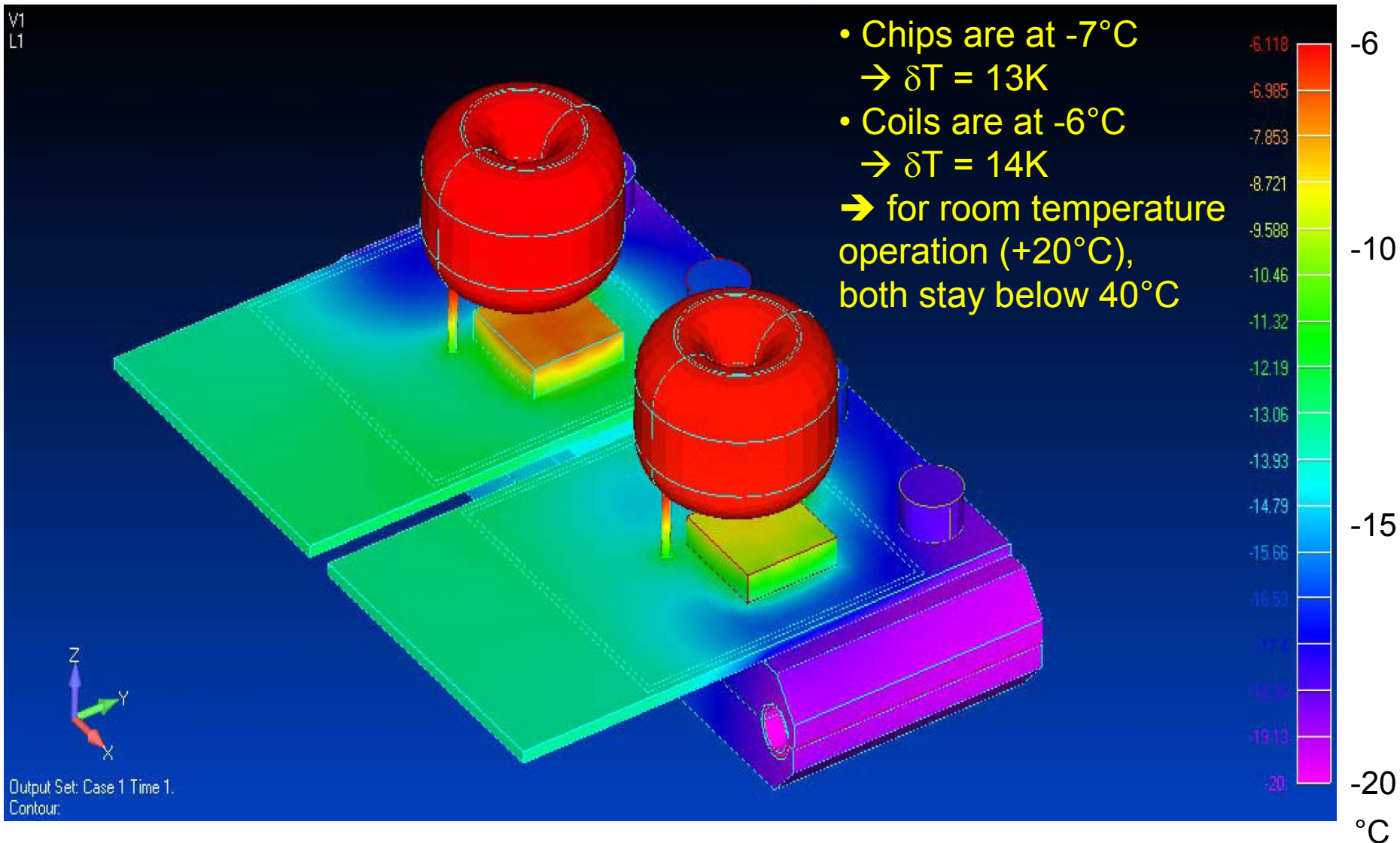
v1

- Software: MSC Nastran
- Coolant temperature: -20°C
- Power dissipation $3\text{W} \sim 75\%$ @ 10W
(chip: 2W ; coil: 1W)
- Transition layers to account for sub-optimal thermal contact
- Heat-conducting paste used in shield

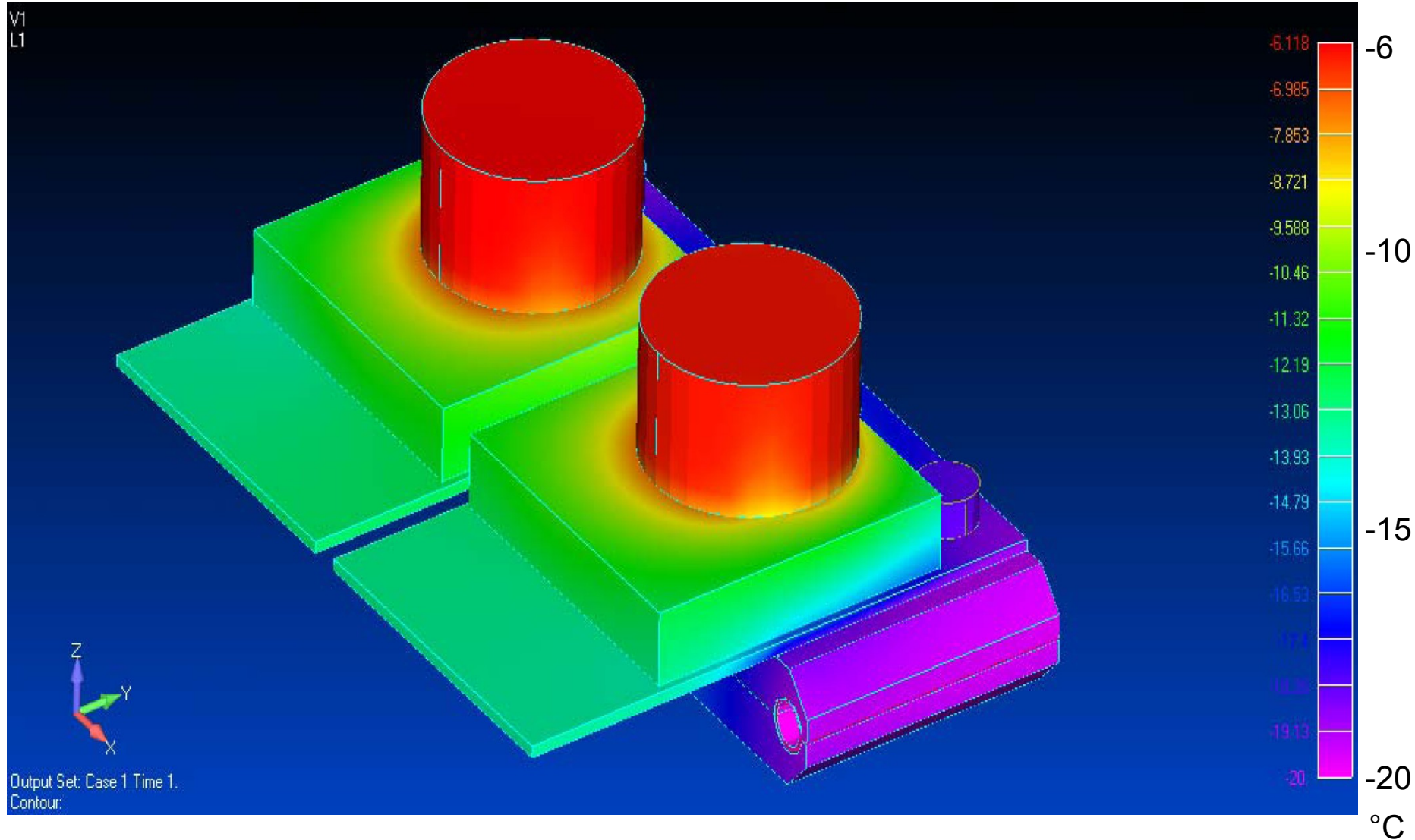


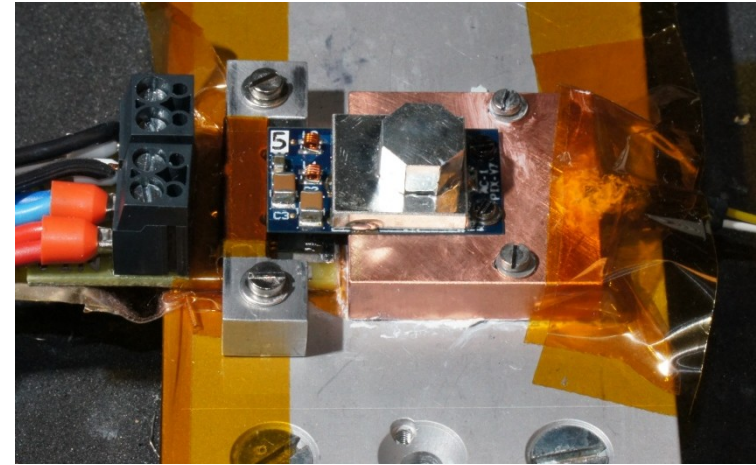
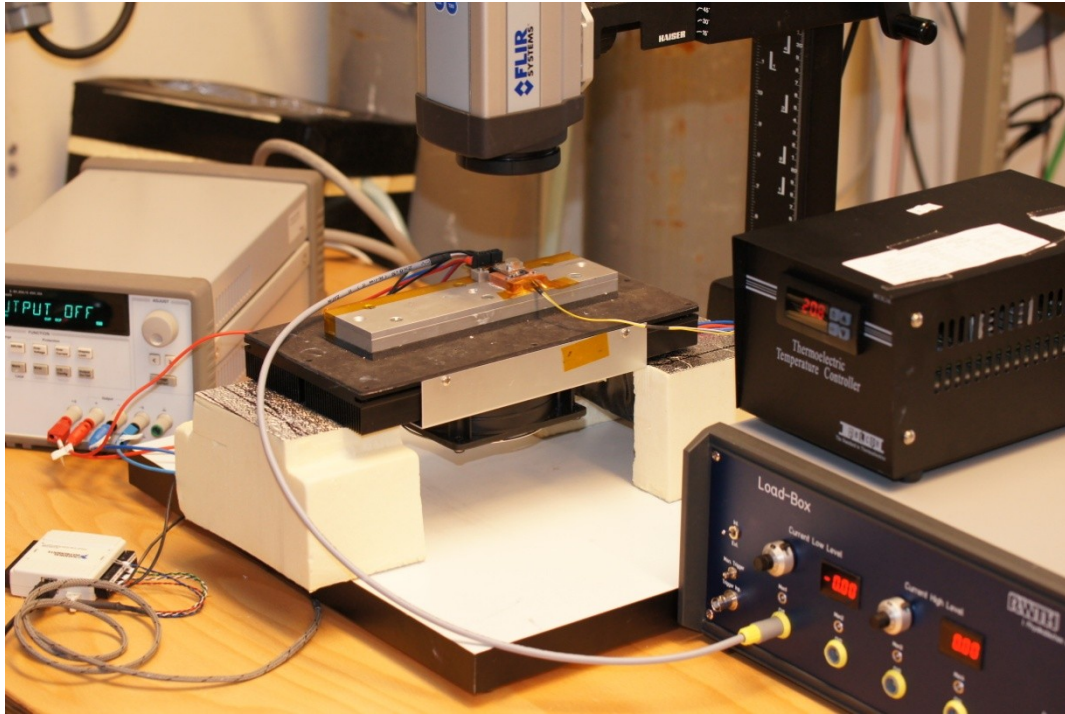


V1
L1



- Chips are at -7°C
→ $\delta T = 13\text{K}$
- Coils are at -6°C
→ $\delta T = 14\text{K}$
- for room temperature operation ($+20^{\circ}\text{C}$), both stay below 40°C





- To cross-check simulations
- Peltier element set to $+20^{\circ}\text{C}$
- Peltier regulates on external sensor that is fixed to copper block

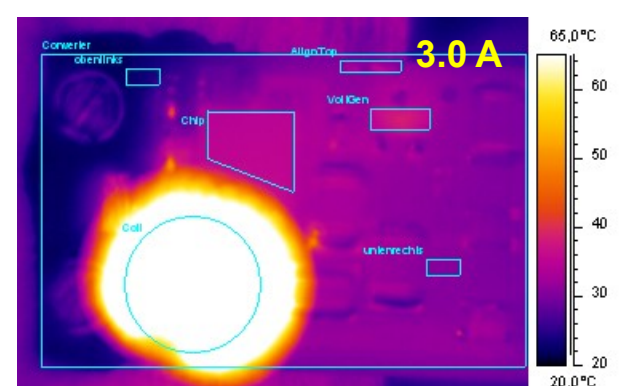
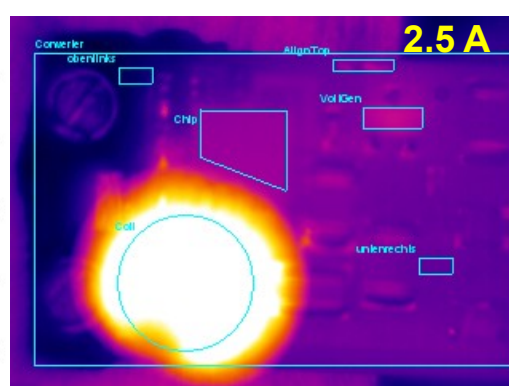
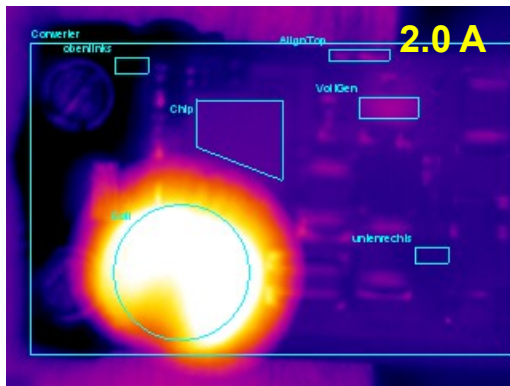
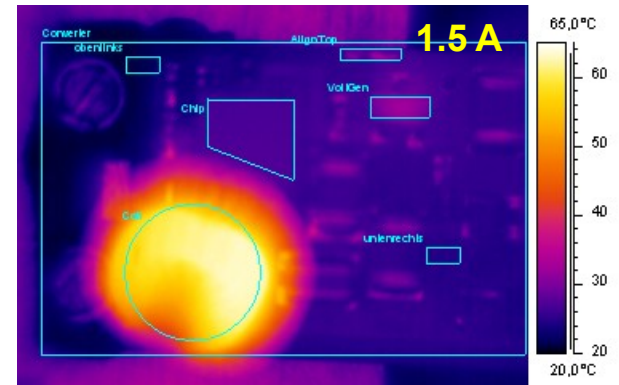
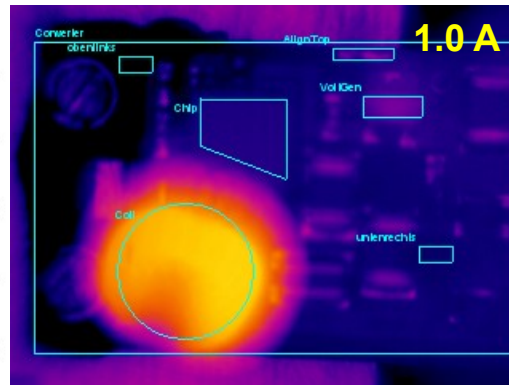
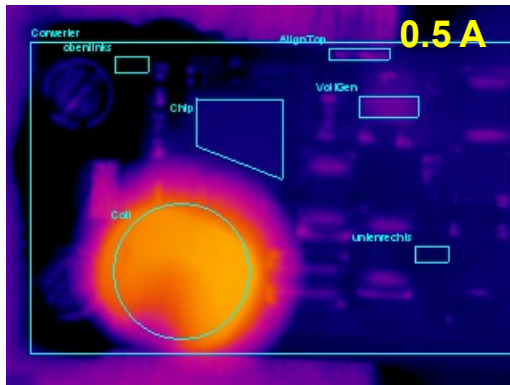
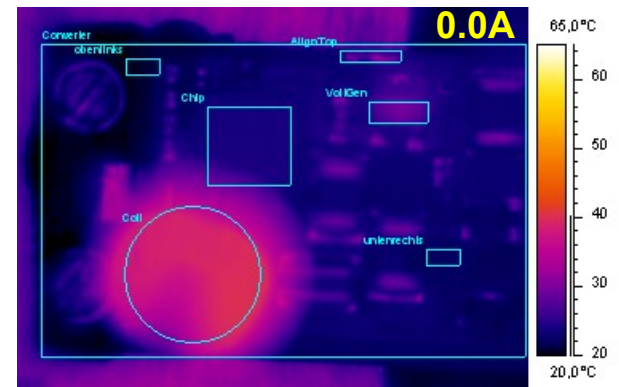
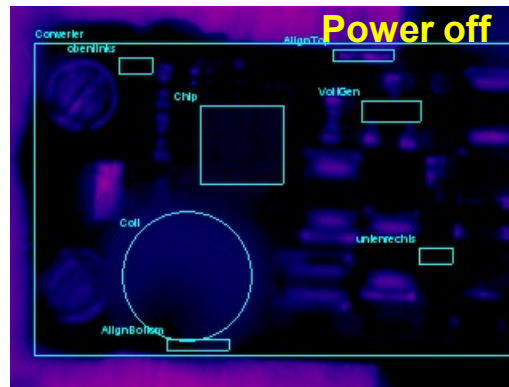


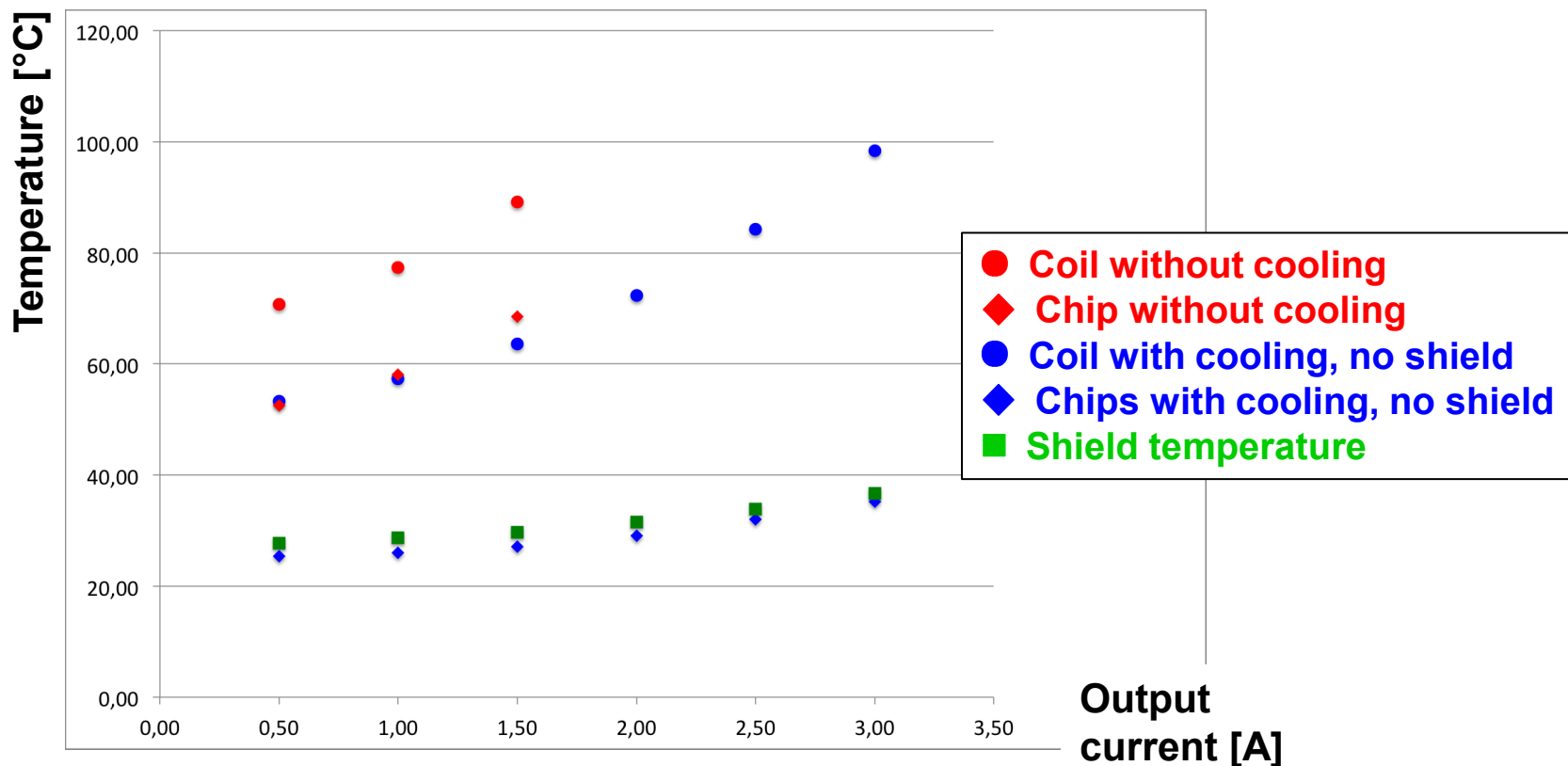
Thermal Measurements



Temperature of coil, chip and PCB versus output current

PIX_V7, 450nH, 1.3MHz
 $V_{in} = 10V$, $V_{out} = 3.3V$





- Converters need to be cooled
- Cooling of chips via backside of PCB is very effective
- Coil needs to be connected to cooling contact (shield)
- Temperature of coil inside shield measured with thermistor → very similar to shield temp.
- Good agreement with FE-simulations



Summary & Outlook



- Low noise converters with reasonable efficiency in hands
- Large progress with mechanical, electrical and thermal integration
- Cooling of converters (chip and coil) under control

- Industrialization of coil and shield production
- Further study of sensitivity of pixel modules to ripple from DC-DC converters
- Production and test of bus PCB, thermal tests with cooling bridge,
- Turn next ASICs (AMIS3, AMIS4) into converters

Back-up Slides



Thermal FE-Simulation



- Support Plates: Aluminum 200 W/m/K
- Tubes: Stainless Steel (316L) 18.8 W/m/K
- Coils: Copper 390 W/m/K
- Chips: Silicon 20 W/m/K
- Screws: Stainless Steel 13 W/m/K
- Coil Filler: Conductive Glue: 22 W/m/K

- Transition Layer Between Support Plates: Assumed 50 % Contact 100 W/m/K
- Transition Layer Around Tubes: Assumed 95 % Contact 190 W/m/K
- Transition Layer Underneath Boards: Some Conductive Plastic 20 W/m/K
- Transition Layer Underneath Chips: 32 Contacting Strips (0.25 mm Dia) and a $\emptyset 2 \text{ mm}$ Solder Patch resulting in 4.1 W/m/K
- Transition Layer Underneath Cover: At 4 Locations Solder 3 mm Wide, 1.5 mm High, 1.4 W/m/K

- Boards:
The Board Consists of a Glass Fiber Composite Coated with two Layers of Copper Foil. The Thickness of the Composite is 0.3 mm and of the Foil 0.035 mm . At Several Locations there are Feedthroughs from the Upper to the Lower Foils. The Upper Foil covers 70 % of the Total Area and the Lower 100 %. The Fraction of the Feedthroughs is 1 % of the Total Area.

in plane: 63 W/m/K
across plane: 5 W/m/K

- Plastic Cover:
The Cover Consists of a Plastic Body coated with Layers of Aluminum Foil. The Thickness of the Plastic is 0.3 mm and of the Foil 0.05 mm . The Foils Cover the Plastic Totally. This leads to
- i in plane: 55 W/m/K
across plane: 0.2 W/m/K



Thermal Measurements



Temperature of shield;
temperature of coil inside
shield measured with
thermistor

