

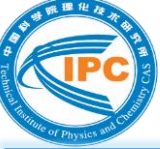
# Numerical investigation on transient sealing performance of square labyrinth seal in a liquid hydrogen piston pump

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## 2. Geometry Structure and Its Main Parameter

## 3. Simulated Results and Discussions

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# 1. Introduction

As a clean energy source, the future of hydrogen energy appears promising!

Numerous developments made in civilian hydrogen transports:



Hydrogen Powered Car



Hydrogen Powered Bus

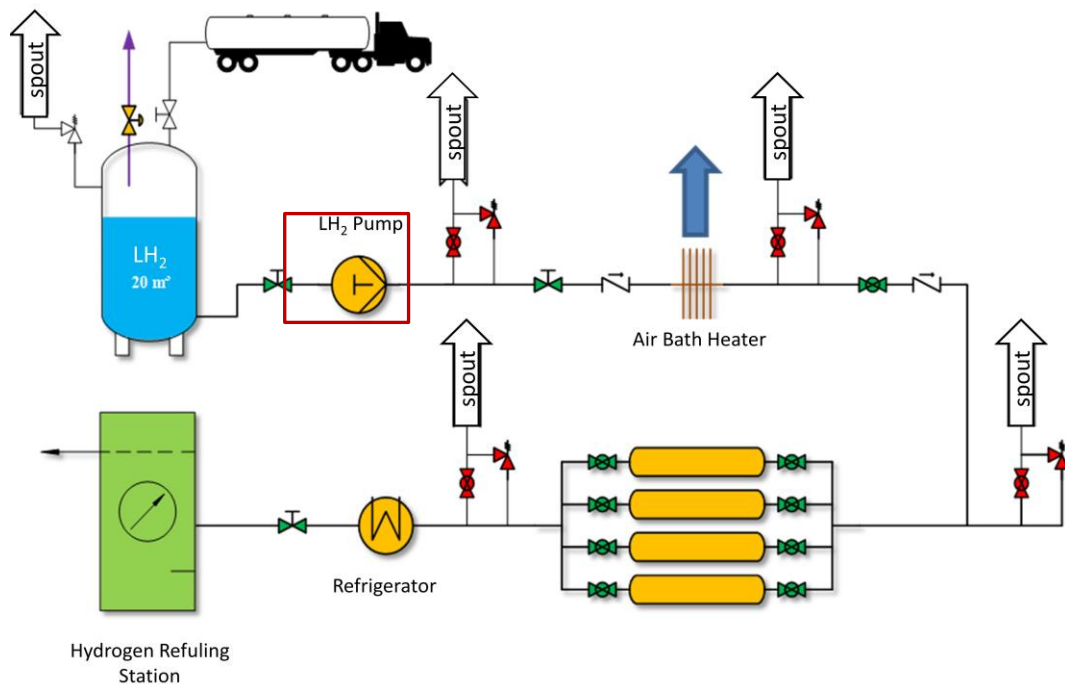


Hydrogen Powered plane

The potential application for hydrogen energy is substantial!

# 1. Introduction

**Liquid hydrogen refueling station** represents an efficient and cost-effective solution for the storage and refueling of hydrogen fuel.



## Liquid hydrogen piston pump:

- ❑ Core component of liquid hydrogen refueling station
- ❑ Liquid compression and lower cost
- ❑ Higher energy efficiency

# 1. Introduction

Effective Piston Sealing



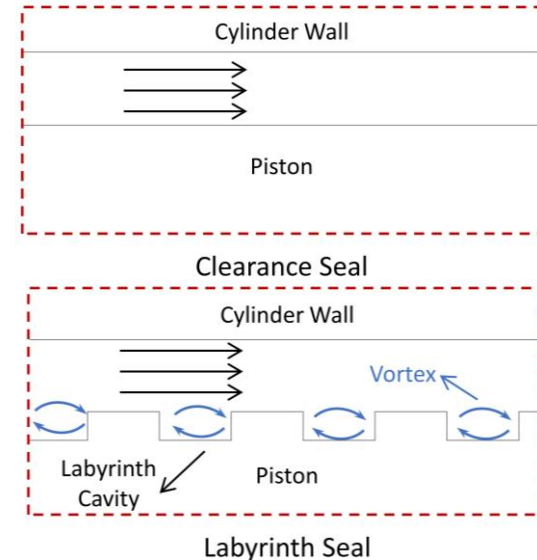
High Efficiency of LH<sub>2</sub> piston Pumps

## Clearance seal

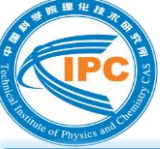
- Non-contact seal;
- Reduce the frictional resistance;
- Reduce the generation of frictional heat.

## Labyrinth seal

- A special form of clearance seal;
- To reduce the leakage rate by the throttle effect in teeth clearances and the vortex dissipation effect in cavities.



- ❑ A **two-dimensional transient labyrinth seal model** of a liquid hydrogen piston pump
- ❑ The effects of **piston motion, compression chamber pressure and labyrinth seal geometries** on the leakage rate



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## 1. Introduction

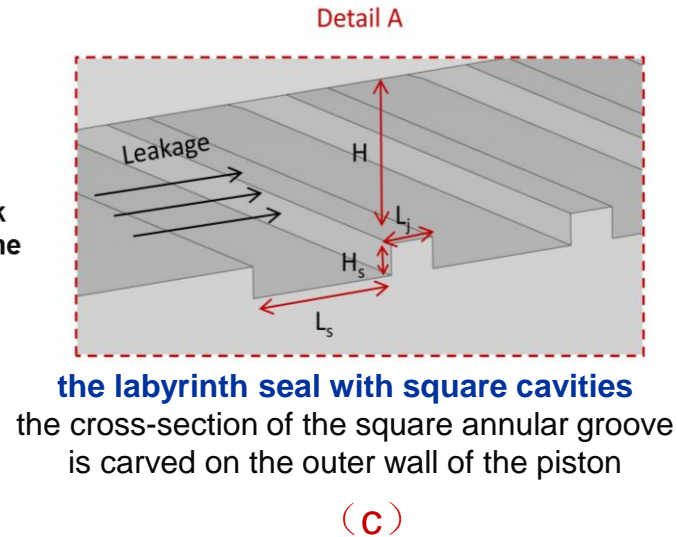
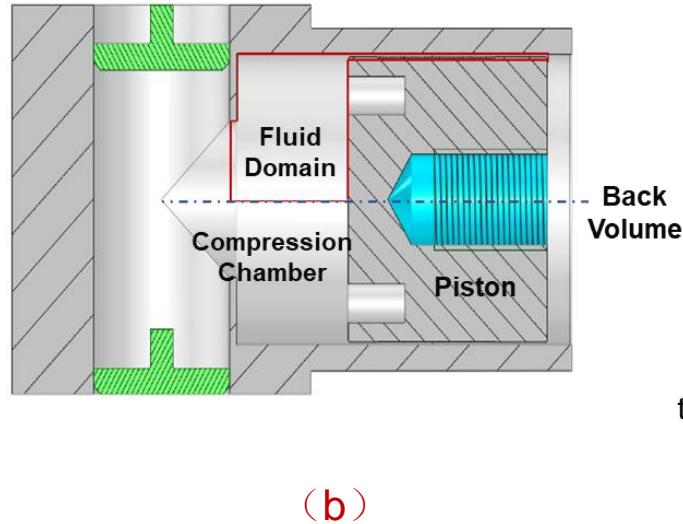
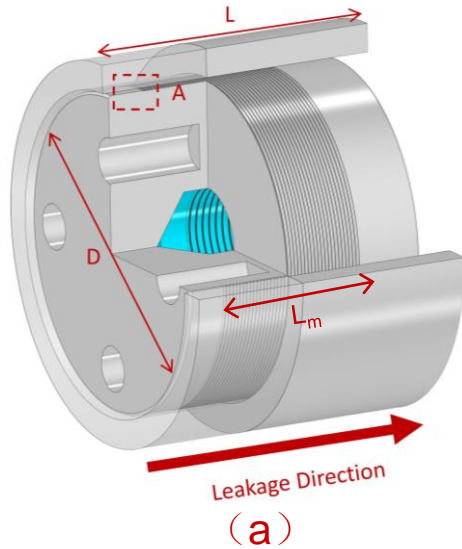
## 2. Geometry Structure and Its Main Parameter

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## 2. Geometry Structure and Its Main Parameter

- The pump chamber is divided into a compression chamber and a back pressure chamber by the piston.
- The piston is driven by the piston rod to perform a reciprocating motion within the pump chamber.
- The pressure differential between two chambers leads to the leakage through the labyrinth or clearance seal.

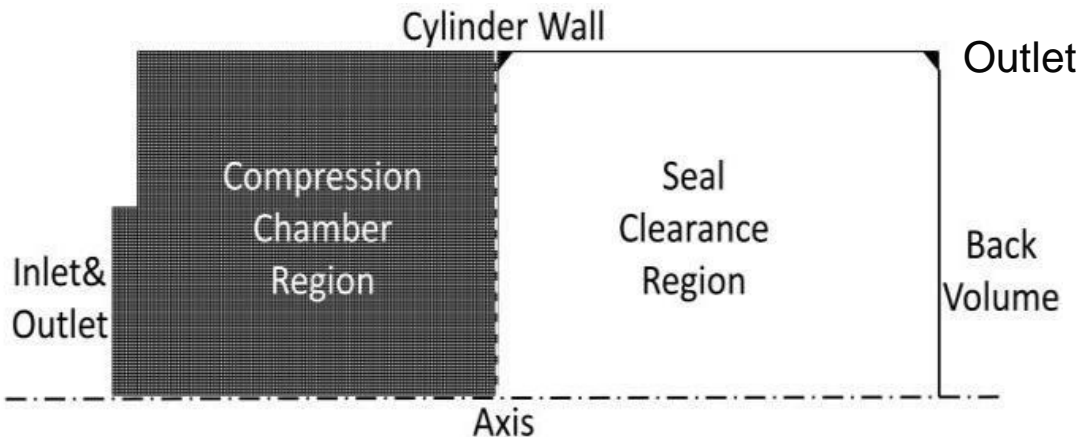


**D**: piston diameter, **L**: length of the piston, **H**: clearance height, **L<sub>s</sub>**: square cavity length, **H<sub>s</sub>**: square cavity depth, **L<sub>j</sub>**: cavity interval, **L<sub>m</sub>**: labyrinth section length.

**Figure 1: Structure schematic diagram of the liquid hydrogen piston pump**

## 2. Geometry Structure and Its Main Parameter

- A **two-dimensional axisymmetric transient clearance seal model**
- The fluid domain is divided into two distinct regions: **Compression chamber region & Seal clearance region**, which are discretized into **a quadrilateral structural mesh**
- The interface between the two regions: an internal surface, thereby establishing a connection between the two fluid regions



- The fluid : a dynamic mesh using the layering method
- The sealing clearance: rigid body motion
- The wall: as a non-slip & adiabatic wall

Figure 2: Fluid domain mesh and boundary conditions



## 2. Geometry Structure and Its Main Parameter

### Independence validation of mesh number:

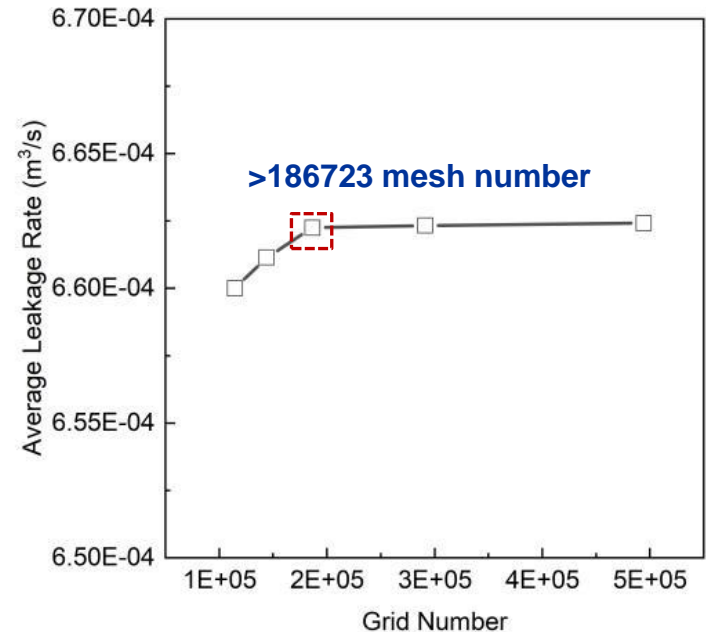
#### □ Seal structure parameters:

- The length of the compression chamber is set to 82 mm.
- $D = 110$  mm,  $L = 88$  mm ,  $H = 50$   $\mu\text{m}$ ,
- $L_s = 1.0$  mm,  $H_s = 0.2$  mm,  $L_j = 0.3$  mm, and  $L_m = 60$  mm.

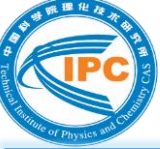
#### □ Pressure boundry conditions:

- The outlet pressure of the discharge stroke: 0.6 MPa,
- The inlet pressure of the suction stroke: 0.3 MPa.
- The back volume pressure: 0 MPa.

- The 186723 mesh number is chosen for the subsequent calculations after the **Independence validation of mesh number**



**Figure 3. average leakage rate of different grid numbers under the entire cycle**



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# 3. Simulated Results and Discussions

## The leakage rate of the clearance and labyrinth seal during the entire cycle

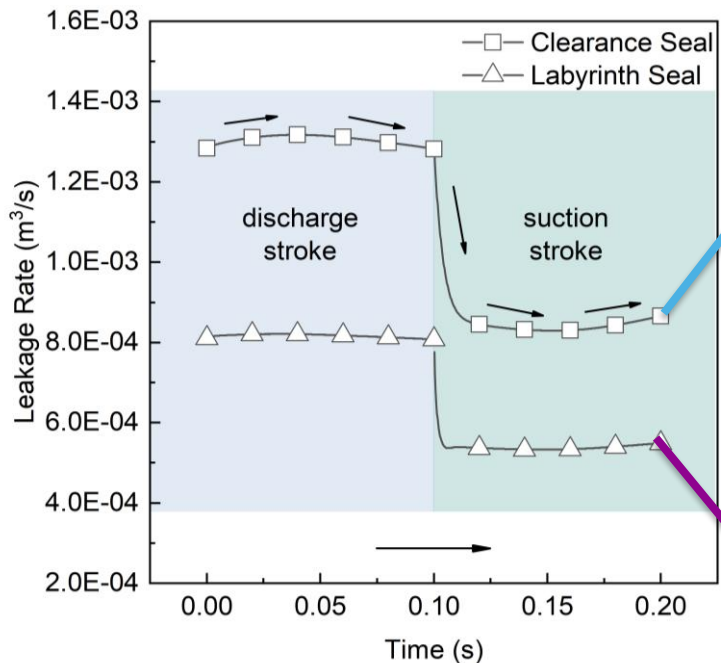
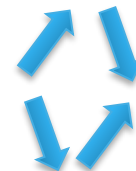


Figure 4.

### Clearance seal

- During the **discharge stroke**: the leakage rate
- During the **suction stroke**: the leakage rate

**due to the piston's inward extrusion**



### Labyrinth seal

- To simultaneously reduce the leakage rate and the fluctuations, thereby attenuate the impact of piston motion in comparison to the clearance seal

# 3. Simulated Results and Discussions

## The leakage rate under different discharge stroke pressures in the entire cycle

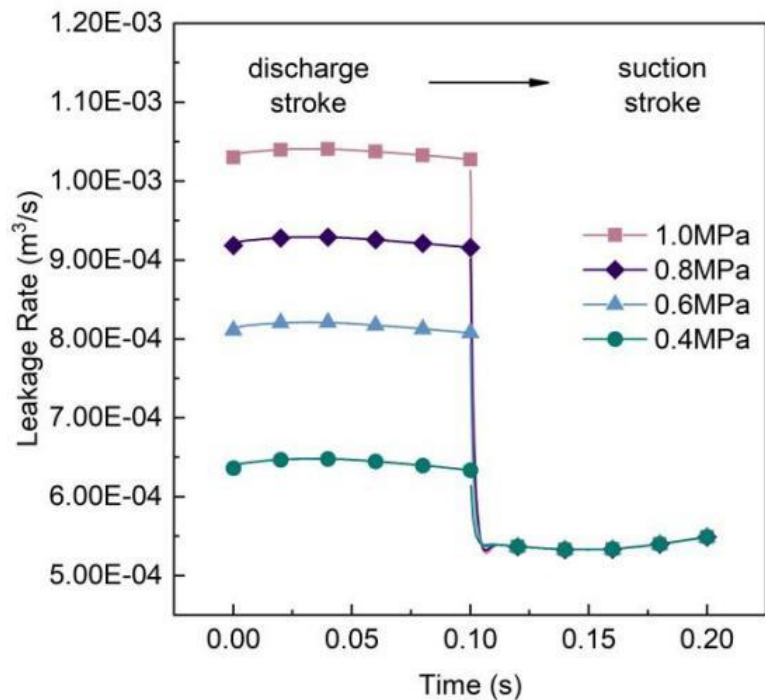


Figure 5

discharge stroke pressures



pressure differential between the compression chamber and the back pressure chamber



the leakage rate

- the leakage rate exhibits an initial increase and a subsequent reduction during the discharge stroke

### 3. Simulated Results and Discussions

#### The Effect of labyrinth section length ( $L_m$ ) on Average Leakage Rate

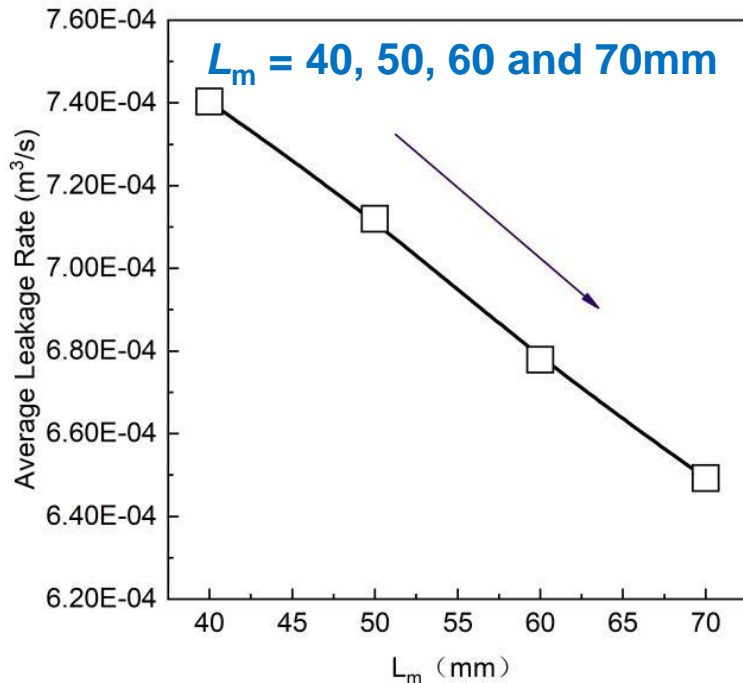


Figure 6

- The longer  $L_m$ , the lower the average leakage rate.
- As  $L_m$  increases, the number of square labyrinth cavities also rises, accompanied by an increase in flow resistance, intensified kinetic energy dissipation and a reduction in leakage rate.

### 3. Simulated Results and Discussions

#### Average leakage rate at various square cavity depth $H_s$ in different square cavity length $L_s$

- ❑ The average leakage rate corresponding to different  $H_s$  is calculated for  $L_s$  at 0.5 mm, 0.7 mm, 1.0 mm, 1.2 mm, and 1.5 mm, respectively.
- ❑ The average leakage rate reduces with  $L_s$ .
- ❑ In the same  $L_s$ , with the increase of  $H_s$ , the average leakage rate initially decreases and then increases.
- ❑ When length-to-height ratio ( $L_s/H_s$ ) is approximately 5.0, the sealing effect is the most effective.

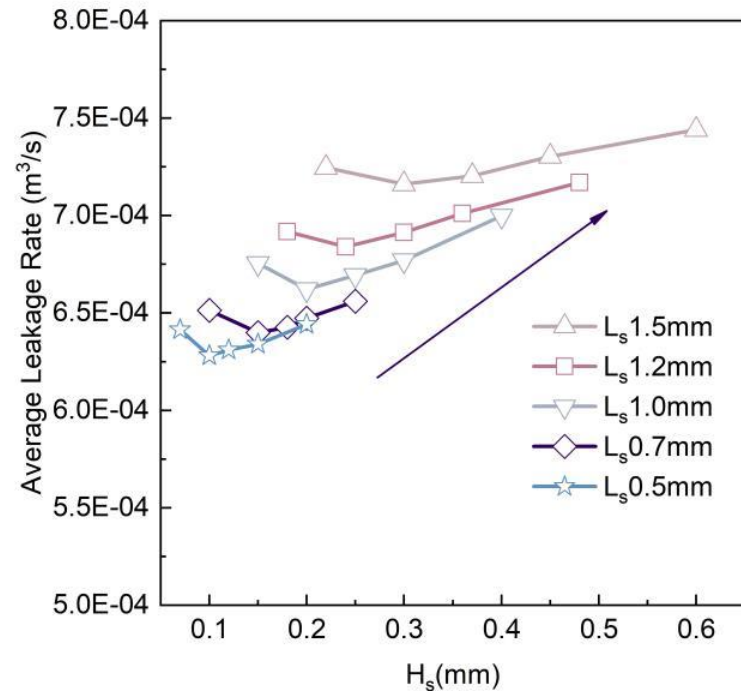
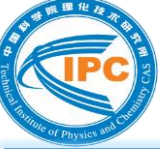


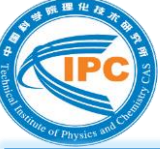
Figure 7



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## 4. Conclusions

- 1) The reciprocating motion of the piston results in fluctuations in sealing effect, which are synchronized with the change in piston speed over time.
- 2) The square cavity labyrinth seal significantly reduces average leakage rate in comparison to a clearance seal, and mitigates the impact of reciprocating piston movement.
- 3) As the compression chamber pressure increases, the average leakage rate will increase in magnitude. The trend of the leakage rate maintains consistent.
- 4) Average leakage rate decreases with an increase of the labyrinth section length. There is an optimum square cavity length-to-height ratio of 5.0 to minimize the average leakage rate.



***Thank you for your  
attention!***

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