

# The Influence of Filling Ratio and Number of Turns on the Heat Transfer Performance of Nitrogen Pulsating Heat Pipe

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## ICEC/ICMC

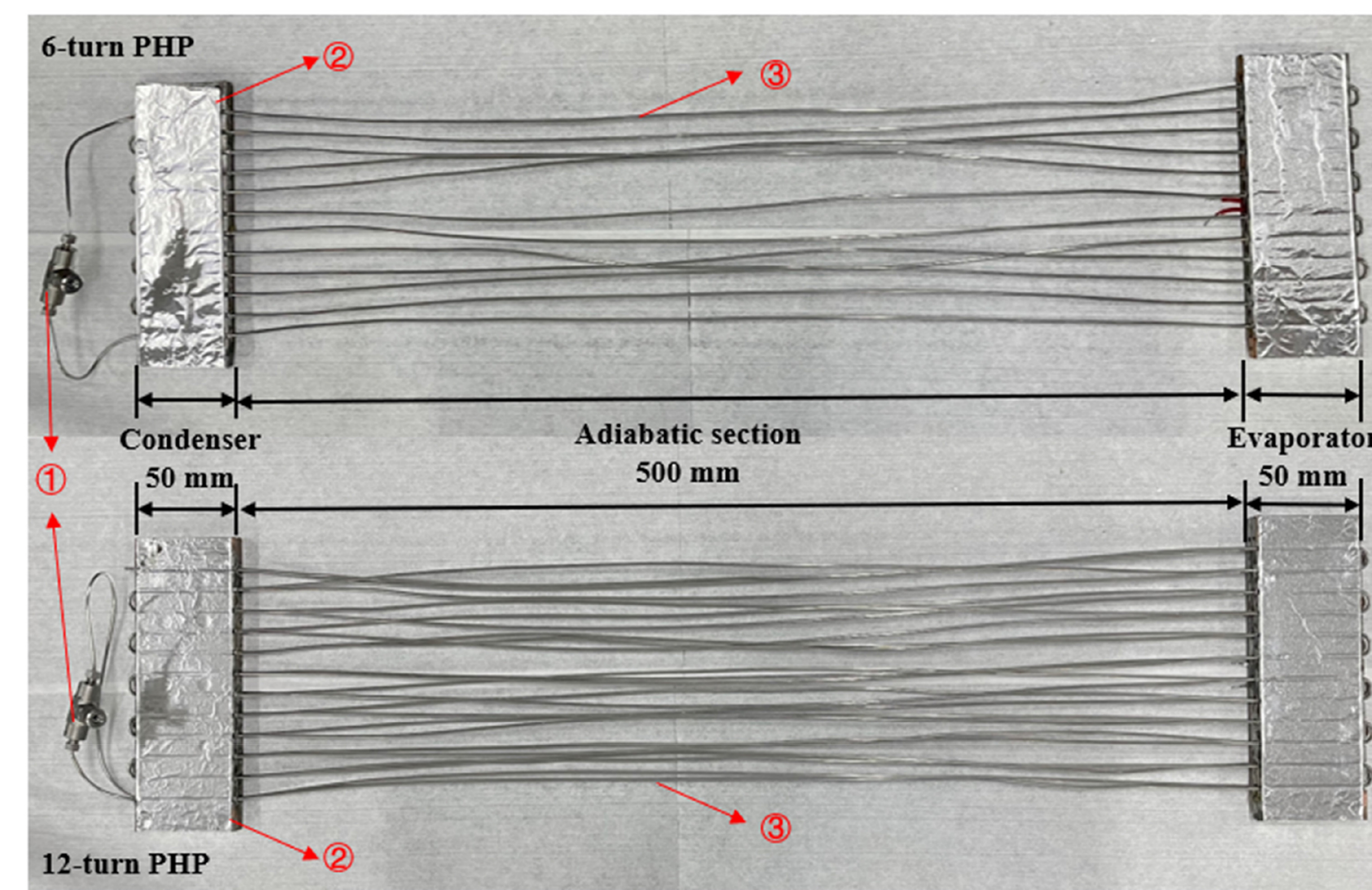
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### 1. Introduction

- Pulsating heat pipes (PHPs) are promising high-efficiency heat transfer devices with high cost-effectiveness and flexibility.
- The heat transfer performance of PHPs with long distances, which are more valuable for practical applications, requires further investigation under different structural and operational parameters.
- In the present work, the impacts of **filling ratios (15%~95%)** and **number of turns (6 and 12)** on the heat transfer performance of nitrogen PHPs, each with a total length of 0.6 m, was experimentally tested.

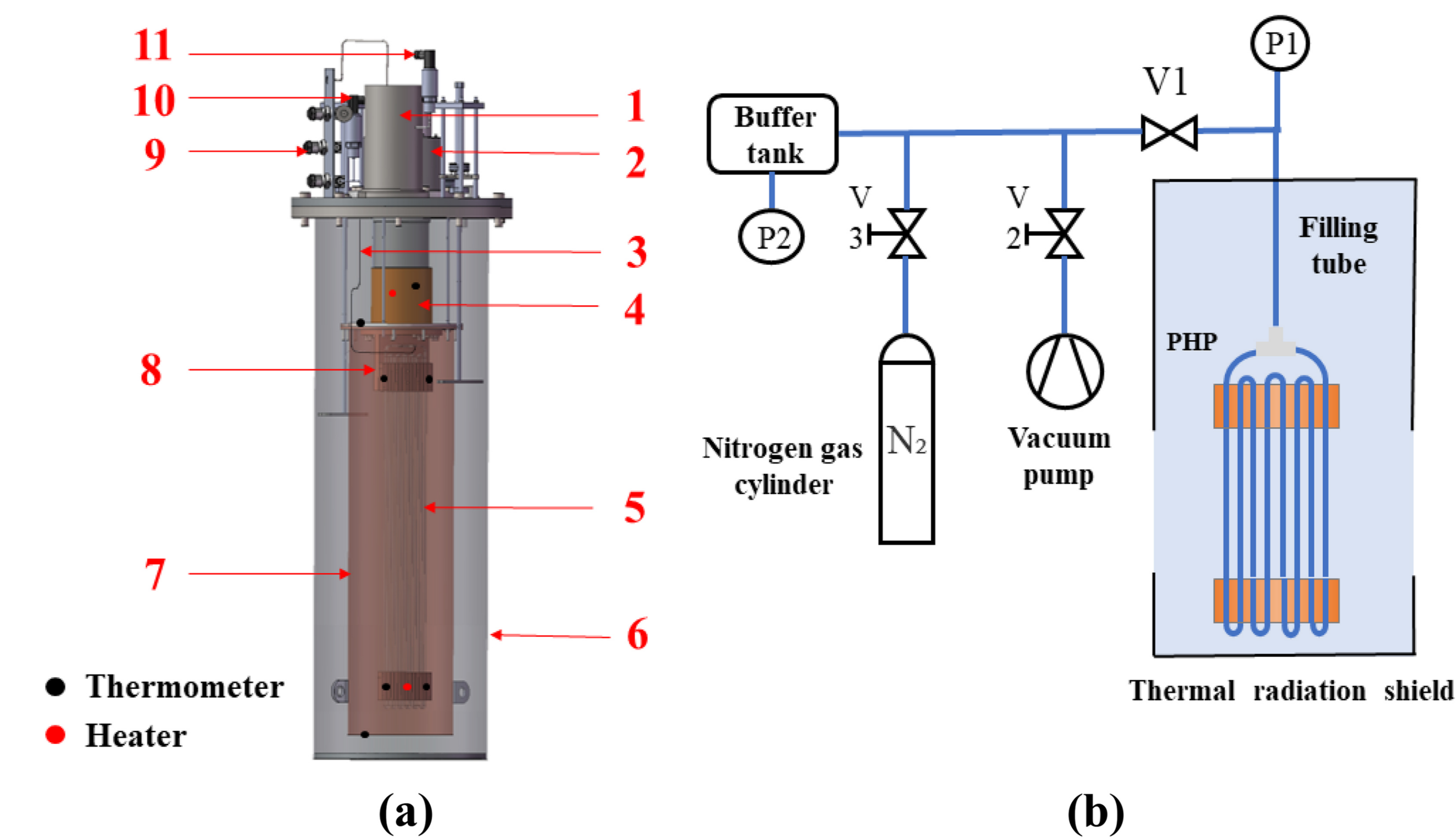
### ➤ PHP prototype



**Fig. 1** Schematic diagrams and photos of PHP prototypes with 6-turn and 12-turn: (1) three-pass junction; (2) copper plate; (3) stainless-steel tube (with an inner diameter of 1 mm and an outer diameter of 1/16 inch)

### 2. Experiment

### ➤ Experimental setup and procedure



**Fig. 2** Schematic diagrams of (a) the experimental setup and (b) filling system: (1) buffer tank; (2) GM cryocooler; (3) filling tube; (4) cold head; (5) nitrogen pulsating heat pipe; (6) vacuum chamber; (7) thermal radiation shield; (8) conduction cooling plate; (9) valve panel; (10) pressure transducer P1; (11) pressure transducer P2.

- The **filling ratio (FR)** was calculated by
 
$$\frac{P_0 V_{\text{Buffer tank}}}{R_g T_{\text{amb}}} = \frac{P_f V_{\text{Buffer tank}}}{R_g T_{\text{amb}}} + \frac{P_f V_{\text{filling tube}}}{R_g T_{\text{filling tube}}} + m_t$$

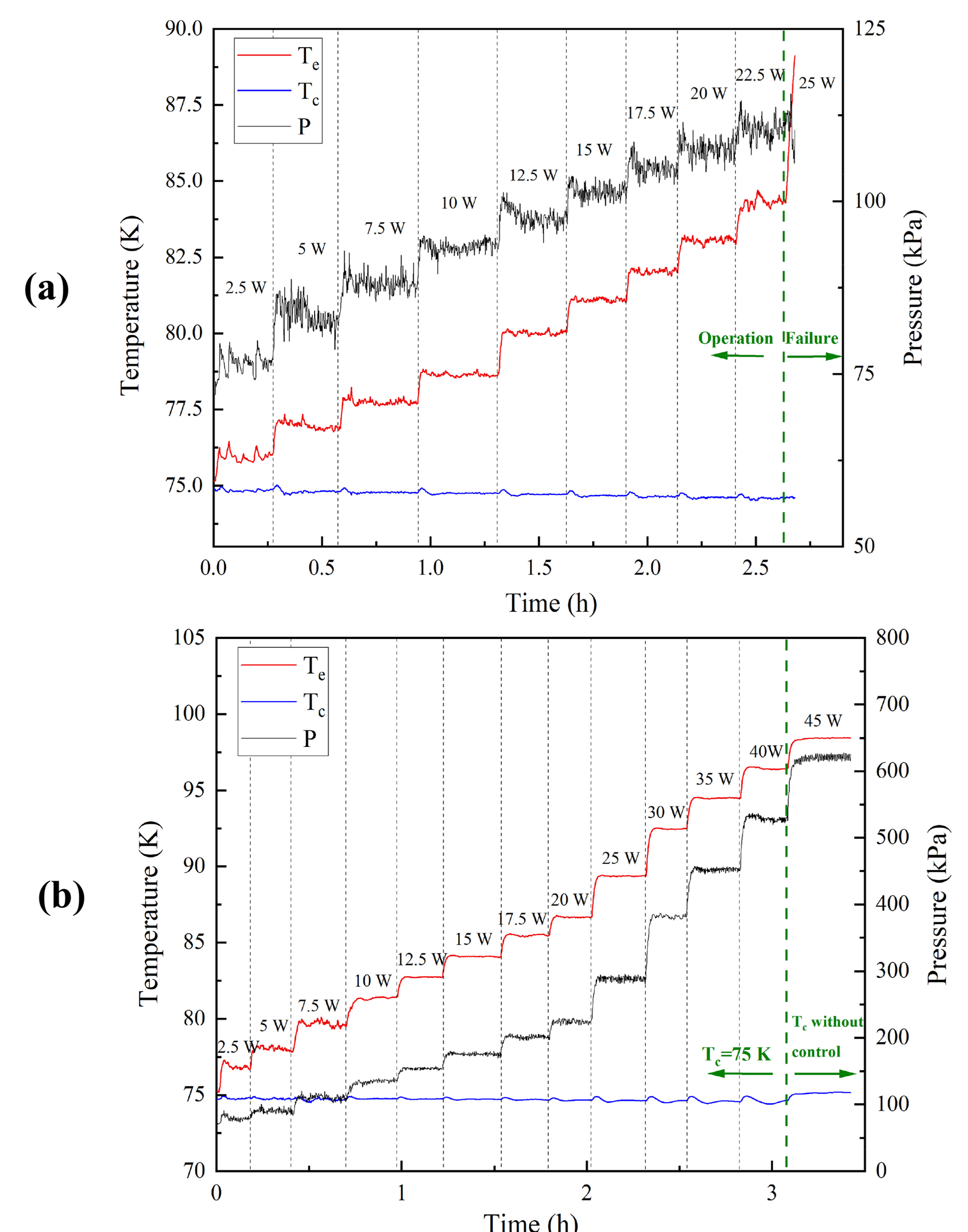
$$m_t = \rho_l V_l + \rho_v (V_{\text{PHP}} - V_l)$$

$$FR = \frac{V_l}{V_{\text{PHP}}} \times 100\%$$
- The heat transfer performance was evaluated using the heat transfer limit  $Q_{\text{max}}$  (the maximum heat input that the PHP can load) and the effective thermal conductivity  $K_{\text{eff}}$ .
- The  $K_{\text{eff}}$  was calculated by
 
$$K_{\text{eff}} = \frac{4QL_a}{n\pi d_i^2 (T_e - T_c)}$$

### 3. Results and discussion

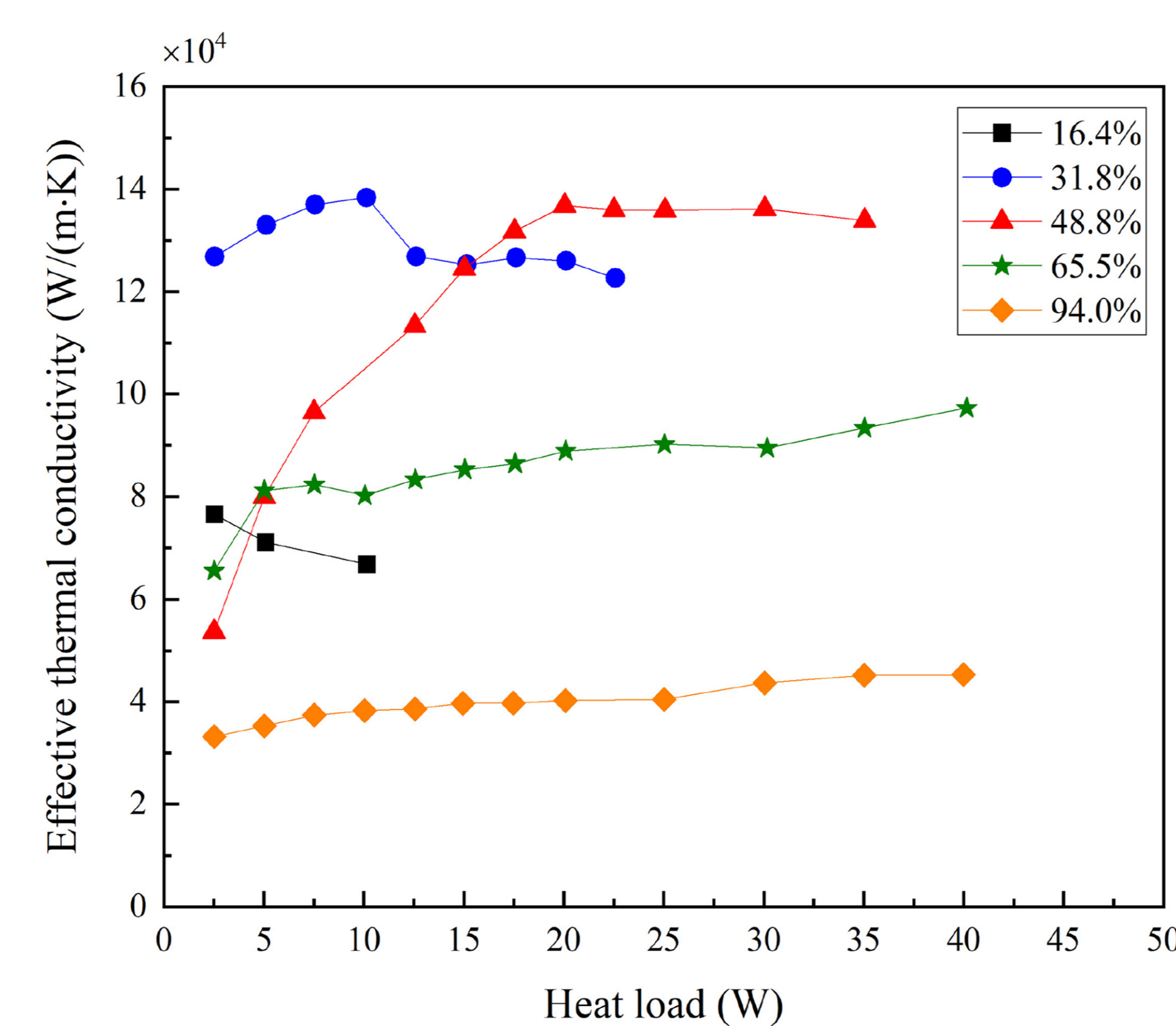
### 4. Conclusion

### ➤ Temperature and pressure response under different head loads



**Fig. 3** The temperature and pressure variations of the 6-turn PHP: (a) FR=31.8% and (b) FR=48.8%.

### ➤ Effect of the filling ratios



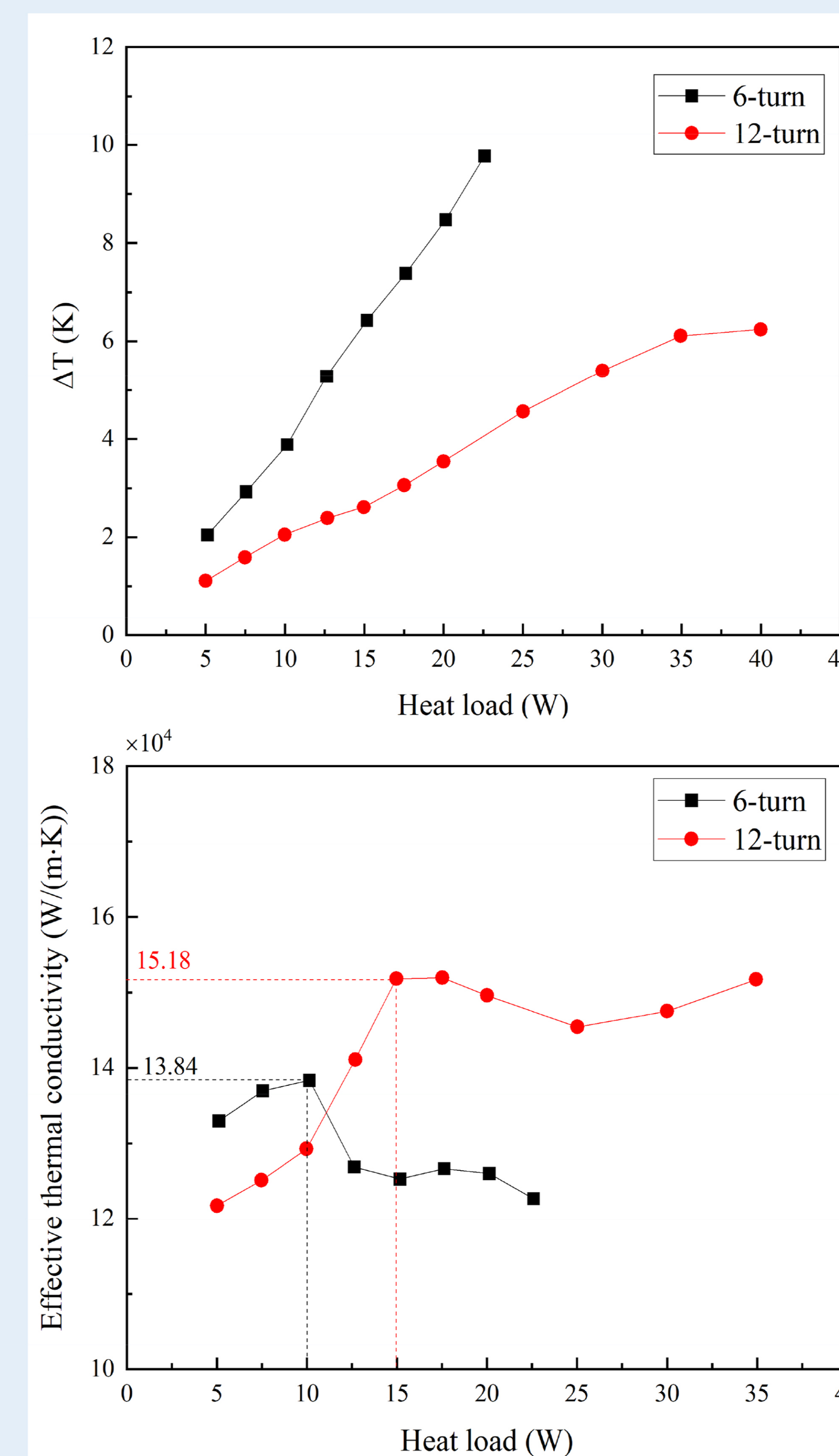
**Table 1** The heat transfer limit of 6-turn PHP.

FR (%)	$Q_{\text{max}}$ (W)
16.4	10
31.8	22.5
48.8	35
65.5	> 40
94.0	> 40

**Fig. 4** Effect of the filling ratio on the effective thermal conductivity of 6-turn PHP.

- The  $Q_{\text{max}}$  **increased** with the increasing filling ratio.
- The high FR led to a **sharp decrease** in  $K_{\text{eff}}$ .
- The **optimal FR** range was between **30%~50%**.
- Different heat load ranges corresponded to **different optimum FRs** within 30%~50%.
- The  $\Delta T$  was **reduced** proportionally by doubling the number of turns.
- At  $Q < 10$  W, the **6-turn PHP** performed **better**.
- As  $Q$  increased, **degradation** occurred **earlier** in **6-turn PHP**.

### ➤ Effect of the number of turns



**Fig. 5** Effect of the number of turns on (a) the  $\Delta T$  and (b)  $K_{\text{eff}}$ .

- The heat transfer performance of the nitrogen PHP was significantly affected by the FR. The  $Q_{\text{max}}$  could be **enhanced** by increasing the FR. However, the high FR led to a **sharp decrease** in  $K_{\text{eff}}$ . The recommended FR was between **30% and 50%**.
- For the 6-turn PHP, the best heat transfer performance was achieved at a FR of 31.8% at a heat load less than 15 W whereas the optimal FR was 48.8% at a heat load exceeding 15 W. The maximum  $K_{\text{eff}}$  of **138.4 kW/(m·K)** and **136 kW/(m·K)** were achieved at FRs of 31.8% and 48.8%, respectively.
- The  $\Delta T$  between the evaporator and condenser was significantly **reduced** and the **maximum  $K_{\text{eff}}$**  was **increased** by increasing the number of turns from 6 to 12. Notably, at higher heat loads, the **12-turn PHP** exhibited better heat transfer performance compared to the 6-turn PHP, achieving a maximum effective thermal conductivity of **151.8 kW/(m·K)** at a heat load of 15 W.