

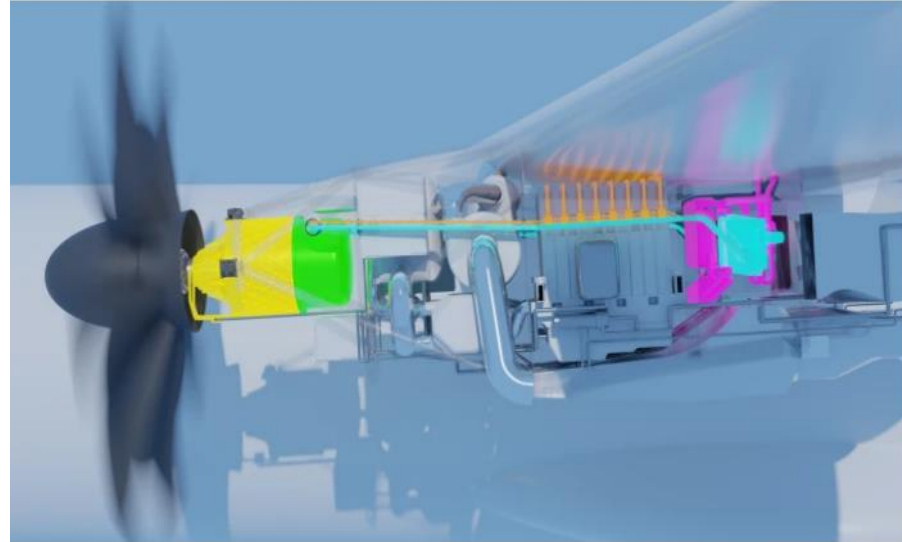
## **Modeling of Electro-Thermal Quench of a REBCO Superconducting Coil for Aircraft Propulsion Motors**

**Arif Hussain, Anang Dadhich, Enric Pardo\***

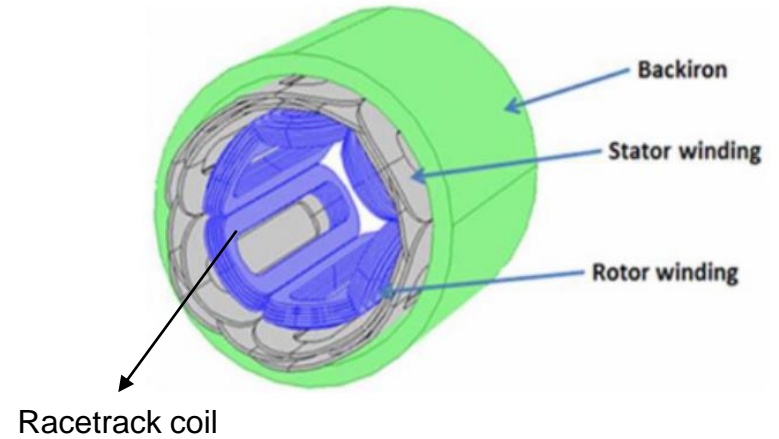
Institute of Electrical Engineering, Slovak Academy of Science, Bratislava

# HTS Motors for Aviation in Hydrogen Electric Aircrafts

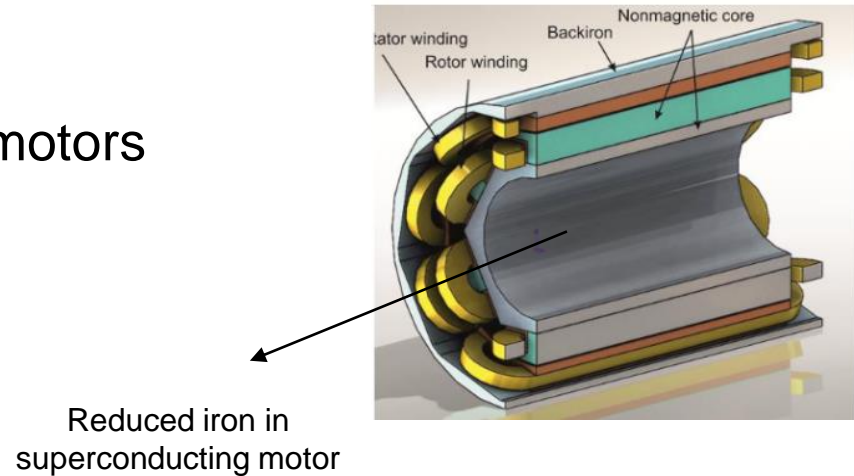
- High power-over-weight ratio
- Improved Efficiency
- Compact Size
- Higher Torque
- LH<sub>2</sub> is used as fuel and coolant



- Superconductor motors:  
racetrack coils



- Reduced Iron:  
compared to conventional motors



- Modeling methods
- Studied configuration
- Varying short-circuit voltages
- Conclusion

- **Modeling methods**
- Studied configuration
- Varying short-circuit voltages
- Conclusion

# Modeling Methods

## Minimum Electro-Magnetic Entropy Production (MEMEP)

- Electro-Magnetic behavior

$$\mathbf{E}(\mathbf{J}) = -\frac{\partial \mathbf{A}}{\partial t} - \nabla \varphi$$

Diagram illustrating the components of the electric field equation:

- A red arrow points from the term  $\frac{\partial \mathbf{A}}{\partial t}$  to the text "Vector potential".
- A red arrow points from the term  $\nabla \varphi$  to the text "Scalar potential".

$$\nabla \cdot \mathbf{A} = 0, \text{ also}$$
$$\mathbf{A} \rightarrow 0 \text{ at } \mathbf{r} \rightarrow \infty$$

Coulomb's gauge

# Electro-Magnetic Behavior

Solving the equation is same as minimizing the functional

$$L[\Delta\mathbf{J}] = \int_V dV \left[ \frac{1}{2} \Delta\vec{\mathbf{J}} \cdot \frac{\Delta\mathbf{A}_J}{\Delta t} + \Delta\mathbf{J} \cdot \frac{\Delta\mathbf{A}_a}{\Delta t} + U(\mathbf{J}) + \nabla\varphi \cdot (\mathbf{J}_0 + \Delta\mathbf{J}) \right]$$

Diagram illustrating the functional  $L[\Delta\mathbf{J}]$  and its components:

- Vector potential due to current density (points to  $\frac{\Delta\mathbf{A}_J}{\Delta t}$ )
- Vector potential due to applied field (points to  $\frac{\Delta\mathbf{A}_a}{\Delta t}$ )
- $\mathbf{J}$  at previous time step (points to  $\mathbf{J}_0 + \Delta\mathbf{J}$ )

# Electro-Magnetic Behavior

Solving the equation is same as minimizing the functional

$$L[\Delta\mathbf{J}] = \int_V dV \left[ \frac{1}{2} \Delta\vec{\mathbf{J}} \cdot \frac{\Delta\mathbf{A}_J}{\Delta t} + \Delta\mathbf{J} \cdot \frac{\Delta\mathbf{A}_a}{\Delta t} + U(\mathbf{J}) + \nabla\varphi \cdot (\mathbf{J}_0 + \Delta\mathbf{J}) \right]$$

Vector potential due to current density
Vector potential due to applied field

E(J) Power Law  
 $\mathbf{E}(\mathbf{J}) = E_c \left( \frac{|\mathbf{J}|}{J_c} \right)^n \frac{\mathbf{J}}{|\mathbf{J}|}$

$U(\mathbf{J}) = \int_0^{\mathbf{J}} \mathbf{E}(\mathbf{J}') \cdot d\mathbf{J}'$

J at previous time step



# Benefits of MEMEP

- Self-programmed software in C++
- Considers screening currents
- Easily take voltage input
- Highly efficient and robust
- Order of magnitude faster compared to commercial software

# Thermal Response

## Temperature dependent thermal parameters

$$C_{pv} \frac{\partial T}{\partial t} = \nabla \cdot (k(T) \cdot \nabla T) + p(\mathbf{J}) \quad \text{Thermal Diffusion Equation}$$

### Time Evolution using Finite Difference

$$T(t) = T(t - \Delta t) + \frac{\Delta t}{C_{pv}(T)} \nabla \cdot (k(T) \cdot \nabla T) + \frac{\Delta t p(\mathbf{J})}{C_{pv}(T)}$$

Heat capacity per  
unit volume

Thermal  
conductivity

$$p = \mathbf{J} \cdot \mathbf{E}(\mathbf{J}, T)$$

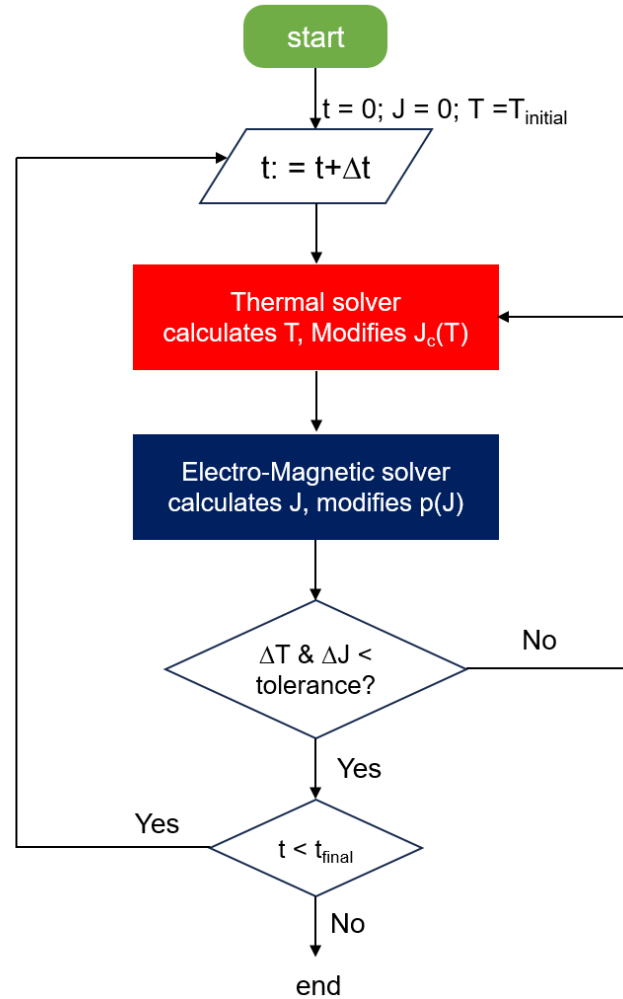
Power loss per  
unit volume

# Finite Difference Approximation

- Explicit discretization
- Stability condition

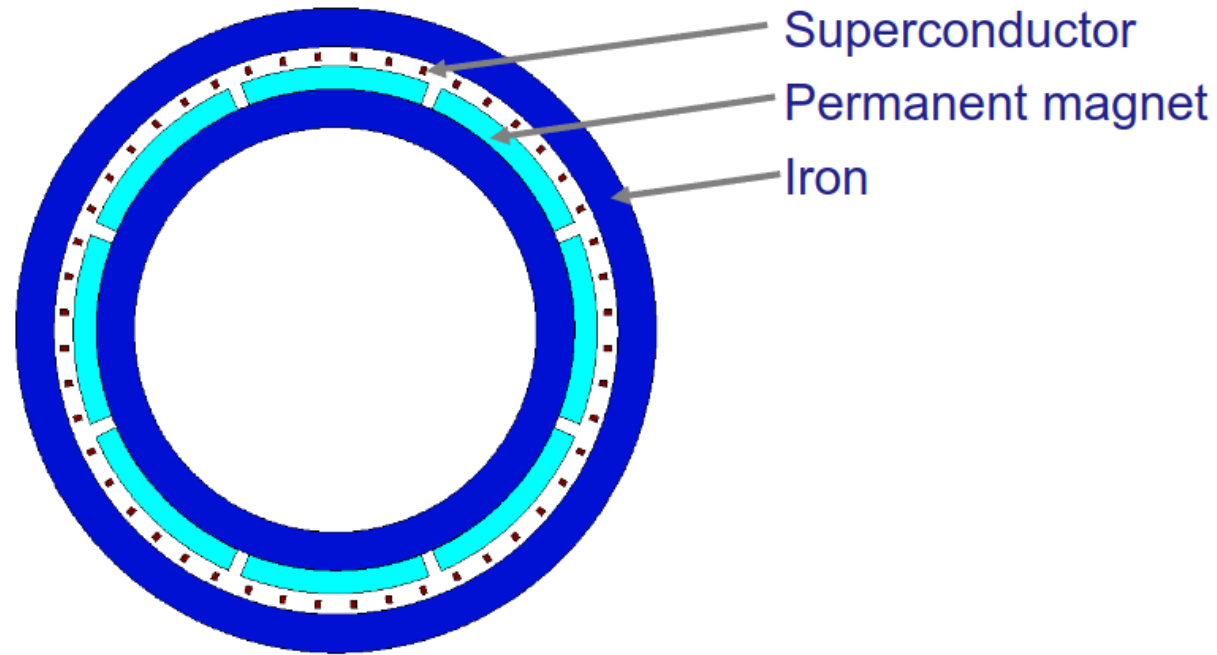
$$\Delta t \leq \frac{1}{2} \cdot \frac{C_{pv}(T) \cdot \min(\Delta x^2, \Delta y^2)}{k(T)}$$

# Coupling Electro-Magnetic and Electro-Thermal Models

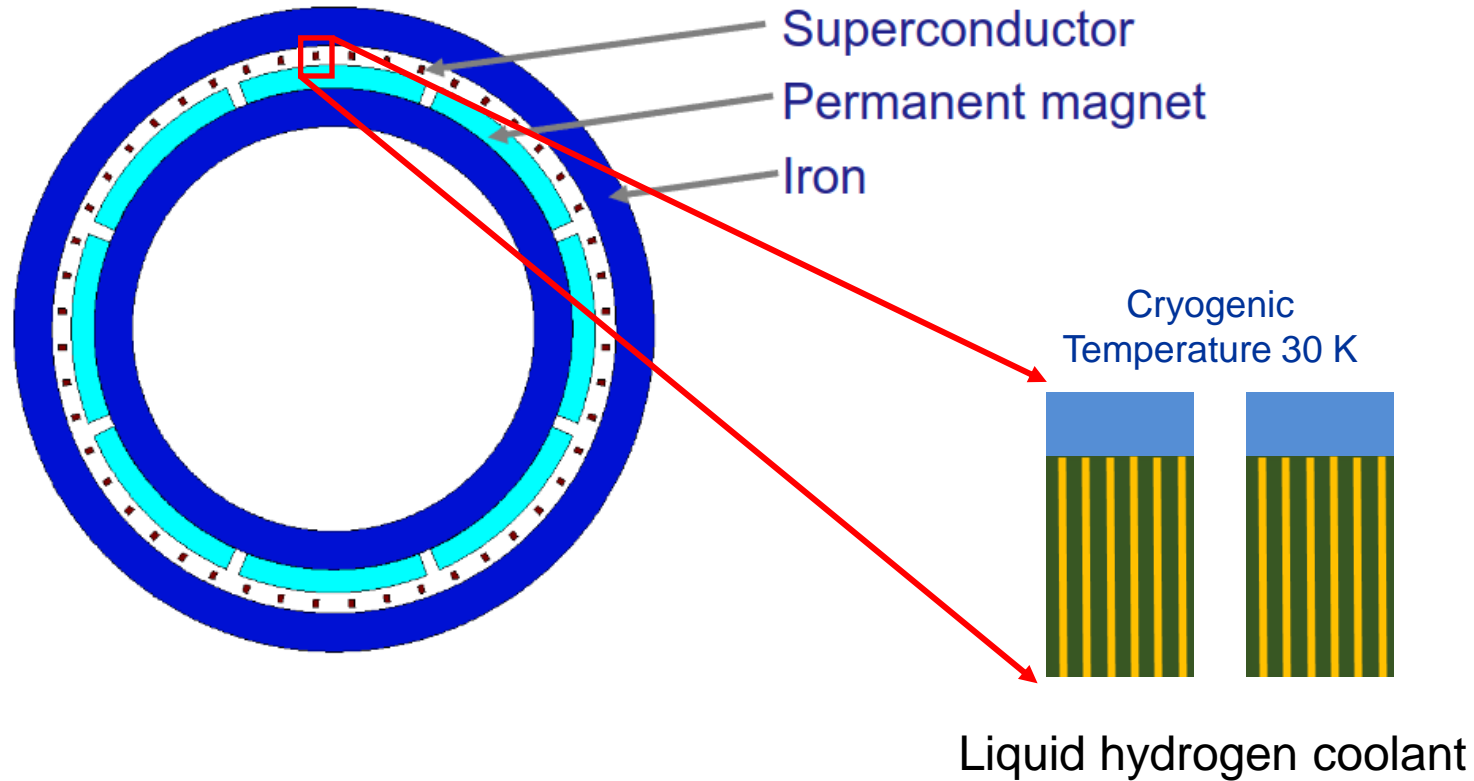


- Modeling methods
- **Studied configuration**
- Varying short-circuit voltages
- Conclusion

# Tentative design of motor for aviation



# Tentative design of motor for aviation



# Studied Configuration

## Racetrack coil in superconducting motors

No. of turns: 30

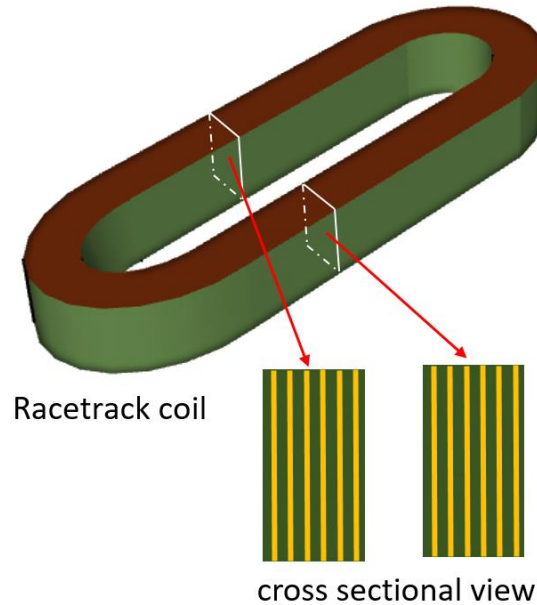
Length: 20 cm

Width: 4 mm

Airgap: 50 mm

$I_c$ : 470 A

$T_c$ : 92 K





# Dimensions of superconducting tape

Silver: 2  $\mu\text{m}$

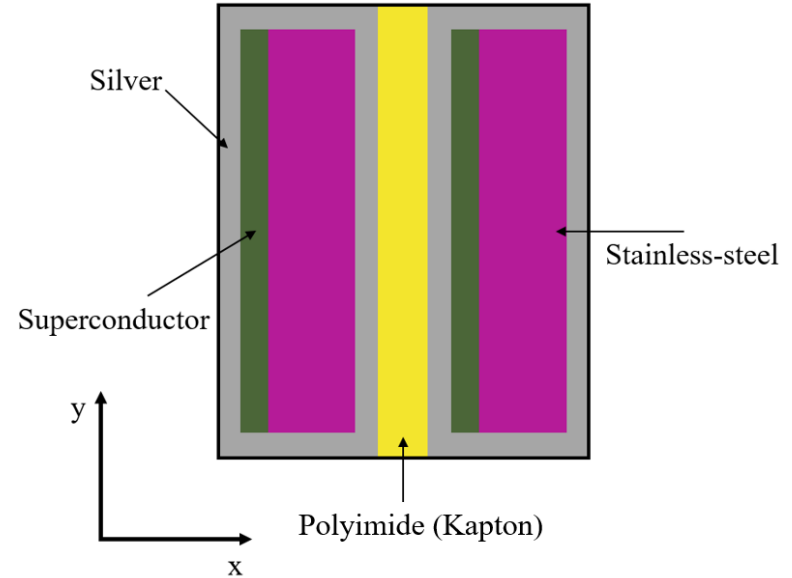
REBCO superconductor: 2  $\mu\text{m}$

Polyamide: 20  $\mu\text{m}$

Stainless steel: 100  $\mu\text{m}$

**$k(T)$  for each material**

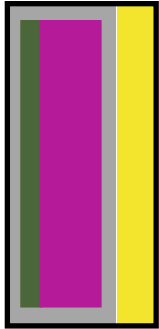
**$C_v(T)$  for each material**



Material properties from NIST database:

<https://trc.nist.gov/cryogenics/materials/materialproperties.htm>

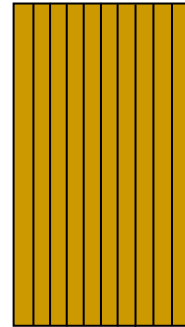
# Homogenization Approximation



Single Tape

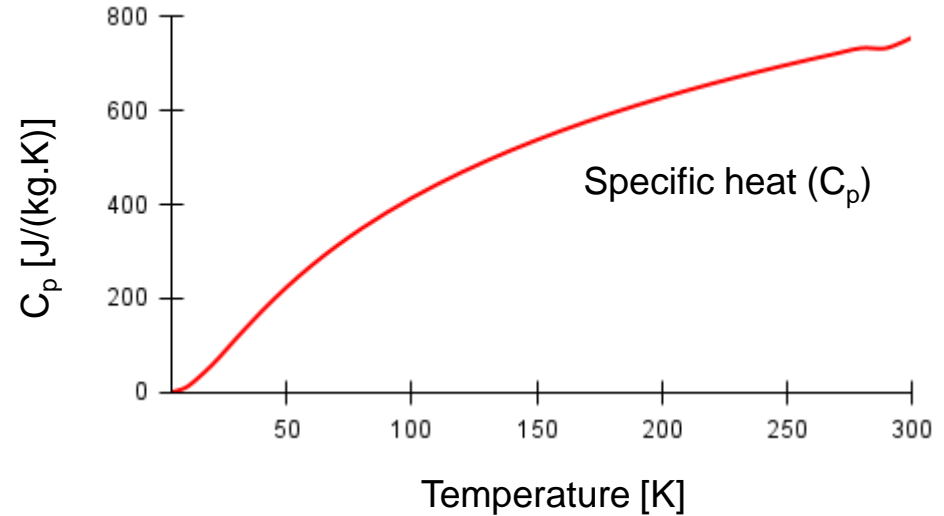
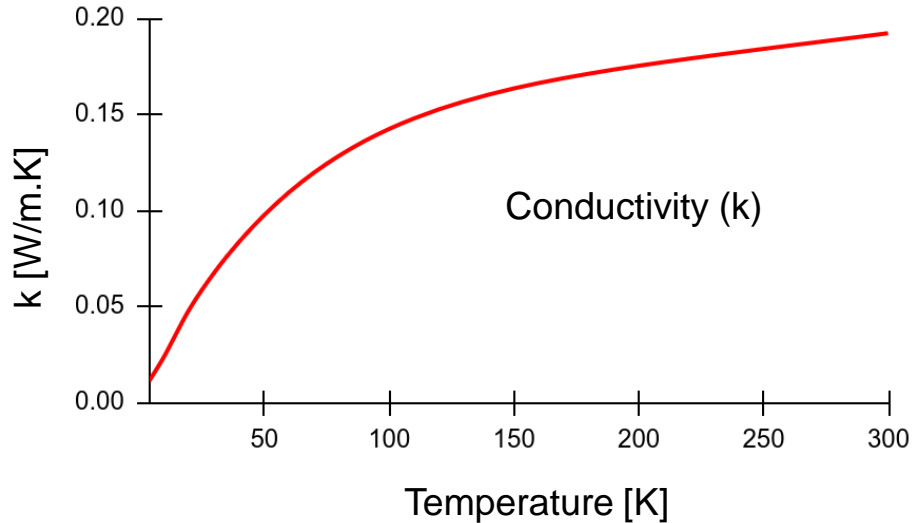


Homogenized  
tape



Homogenized  
coil

# Temperature dependent thermal parameters for polyimide (Kapton)



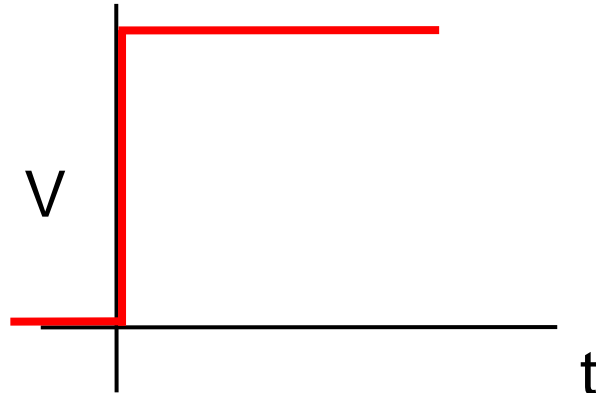
Material properties from NIST database:

<https://trc.nist.gov/cryogenics/materials/materialproperties.htm>

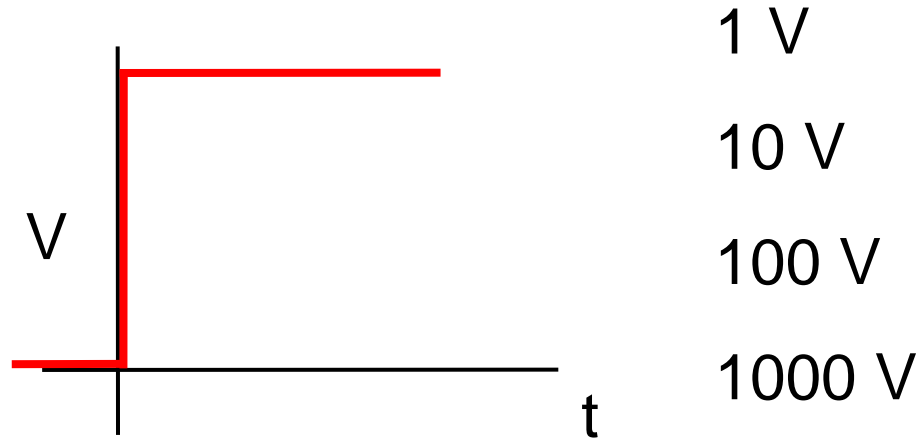
- Modeling methods
- Studied configuration
- **Varying voltage cases**
- Conclusion

# Short-Circuit DC Voltage

- Insulation damage
- Over voltage or lightning strike
- Fault in power source

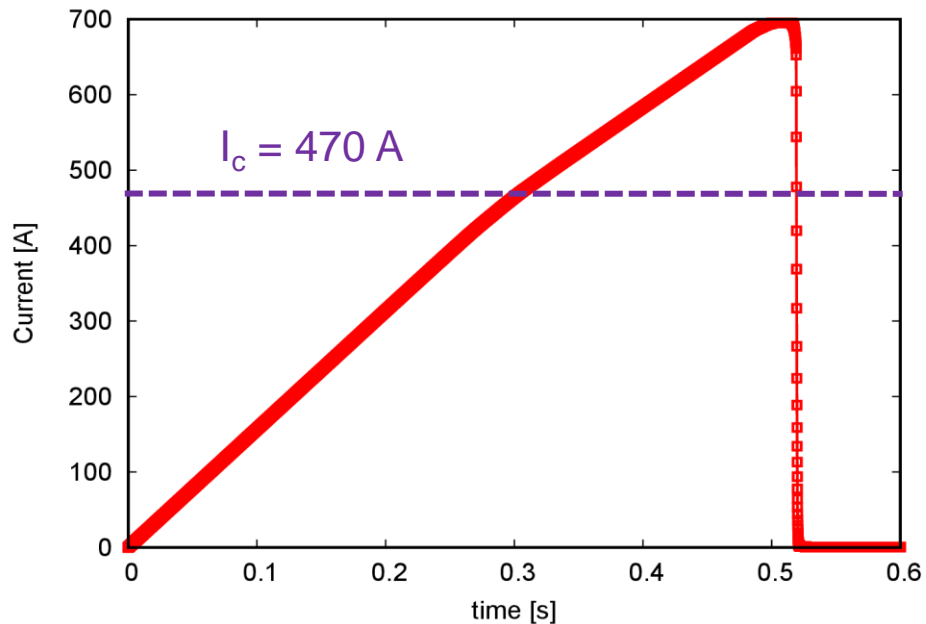


# Short-Circuit DC Voltage



# Short-Circuit DC Voltage

1 V DC

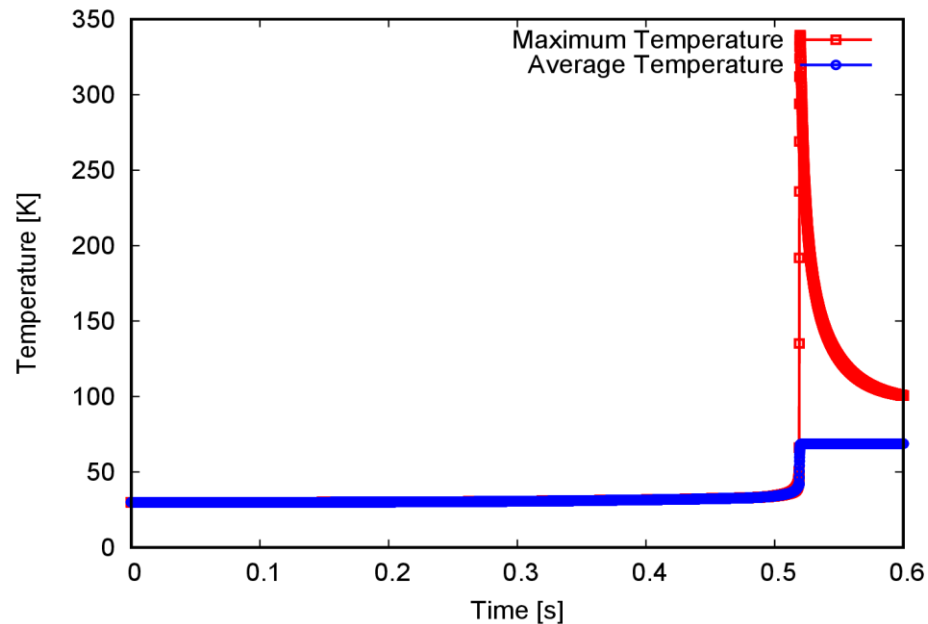
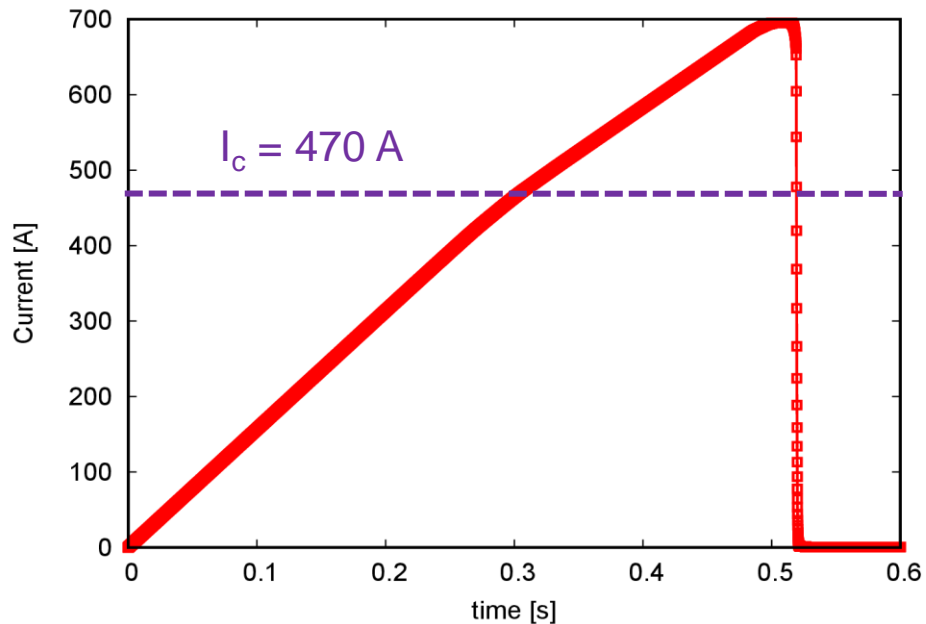


Estimated  $I_c$  from the load-line technique

Data for SuperOx REBCO tape from VUW database.

# Short-Circuit DC Voltage

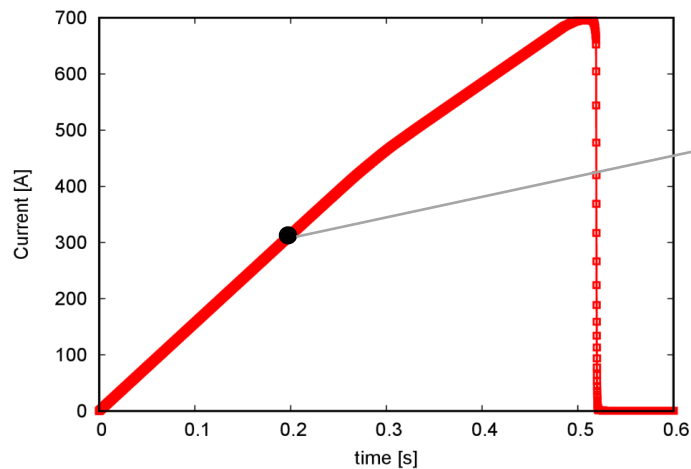
1 V DC



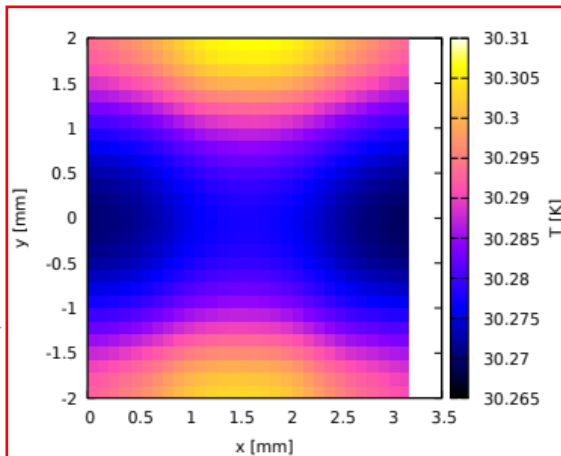


# Short-Circuit DC Voltage

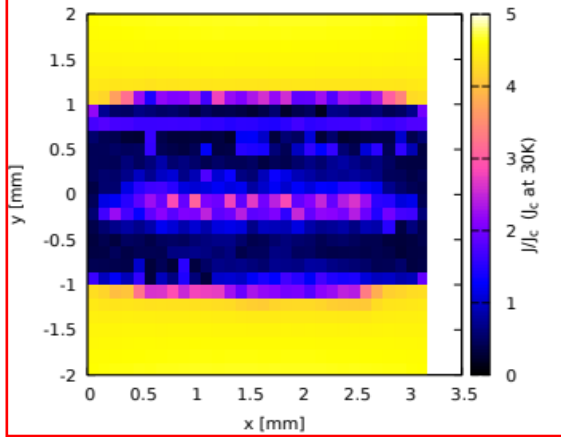
1 V DC



Temperature [K]



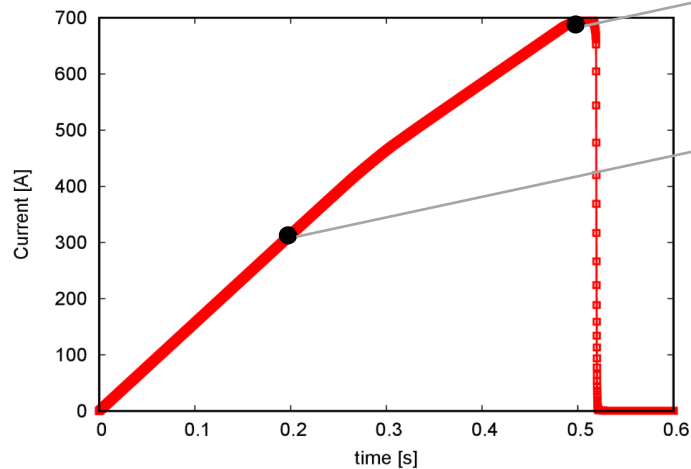
Normalized current density



- Small Temperature rise

# Short-Circuit DC Voltage

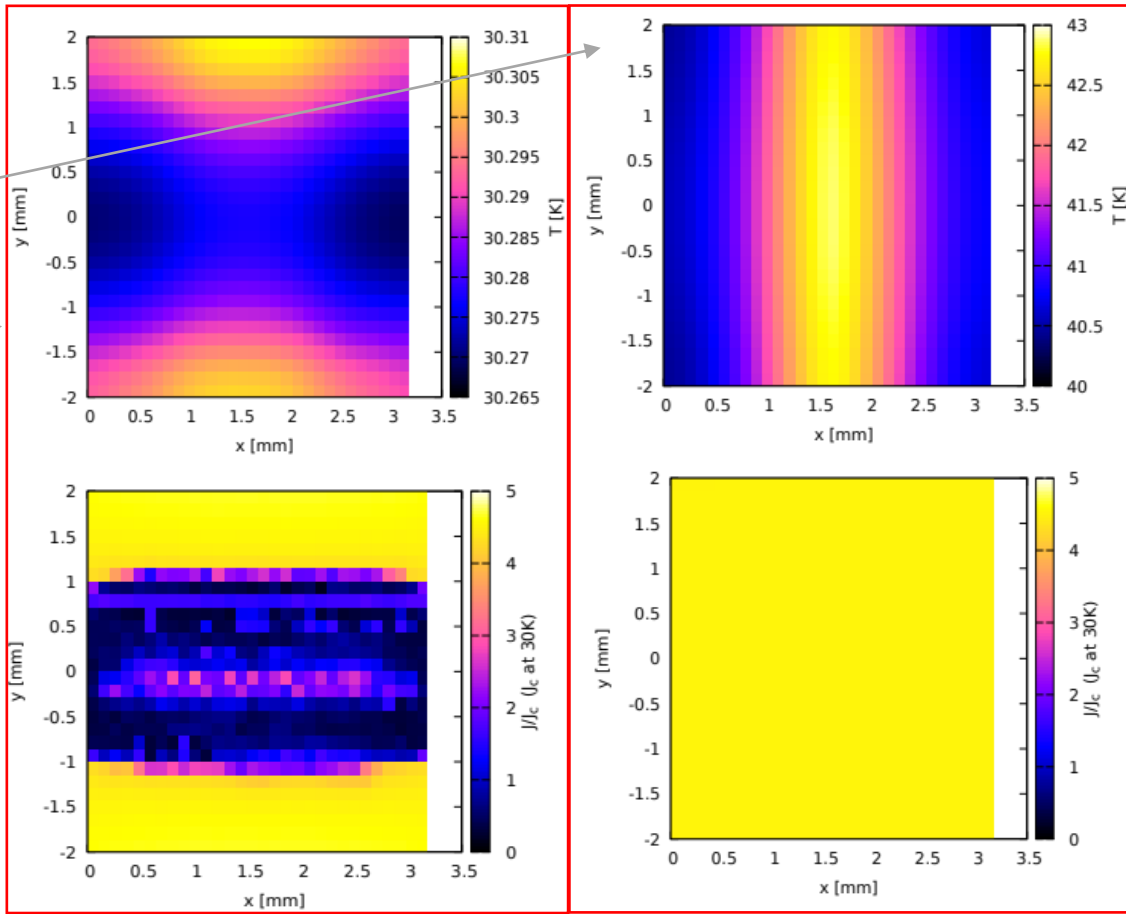
1 V DC



- Significant Temperature rise
- Uniform current density

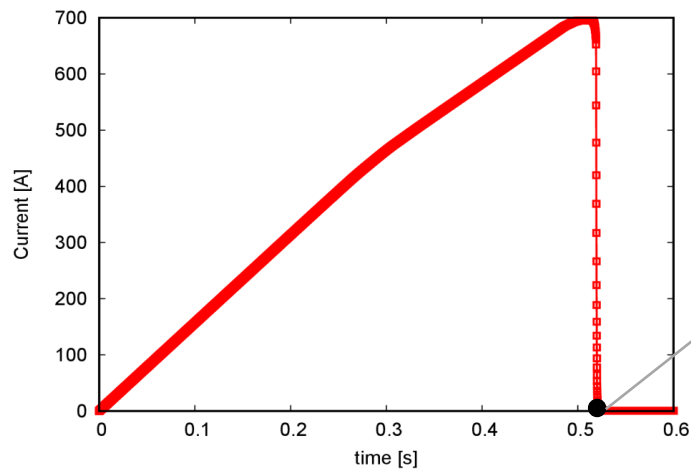
Temperature [K]

Normalized current density



# Short-Circuit DC Voltage

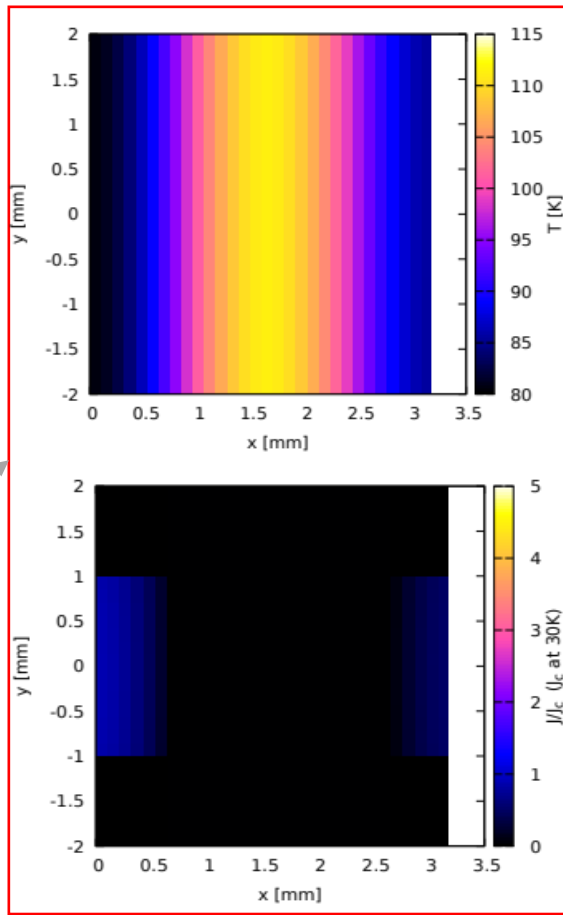
1 V DC



- $T > T_c$  in the middle turns
- Current density reduces

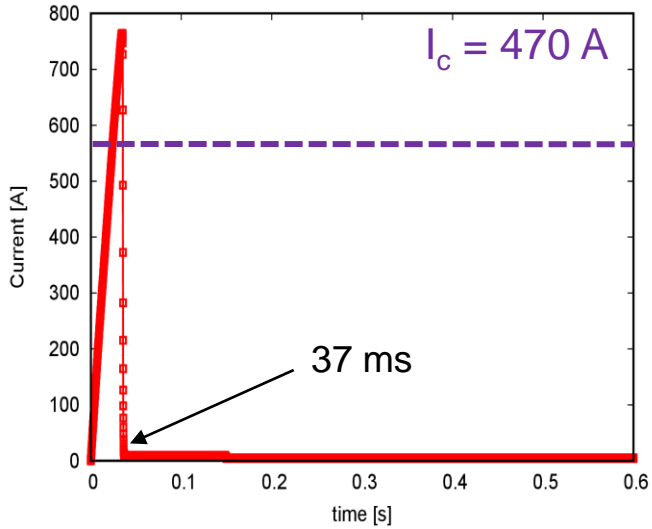
Temperature [K]

Normalized current density



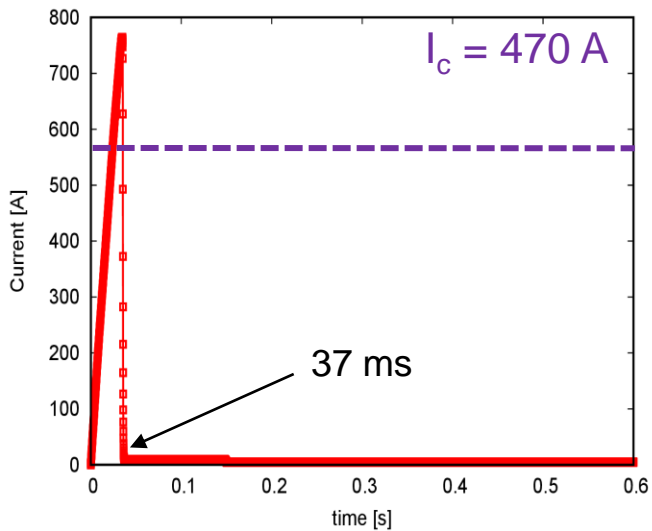
# Short-Circuit DC Voltage

10 V DC

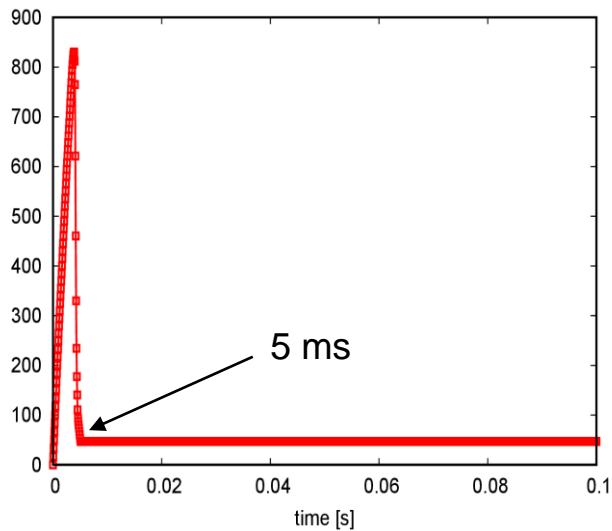


# Short-Circuit DC Voltage

10 V DC

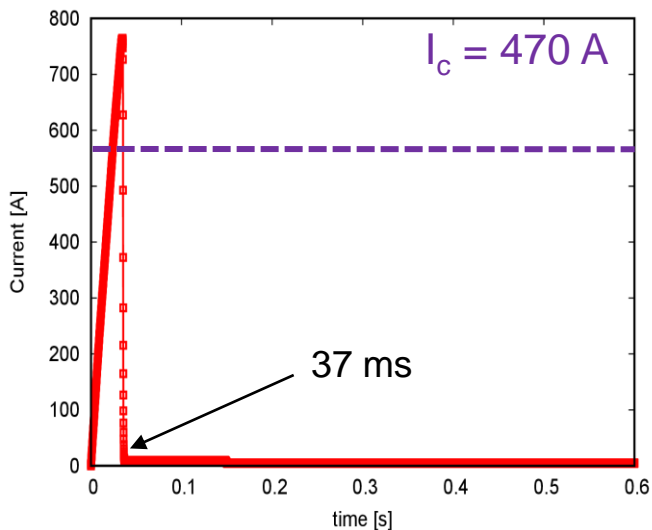


100 V DC

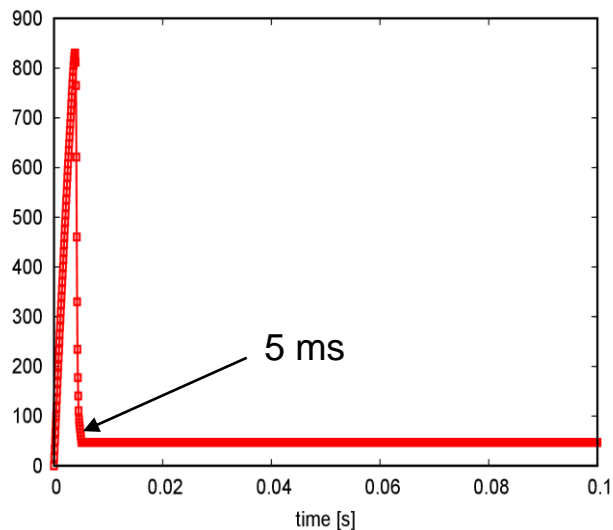


# Short-Circuit DC Voltage

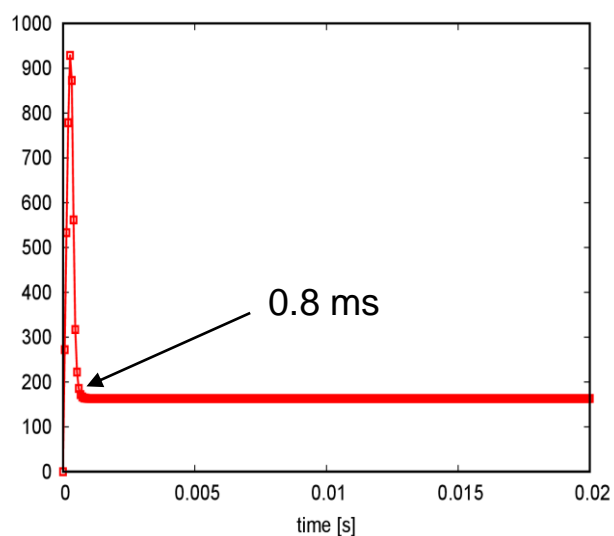
10 V DC



100 V DC



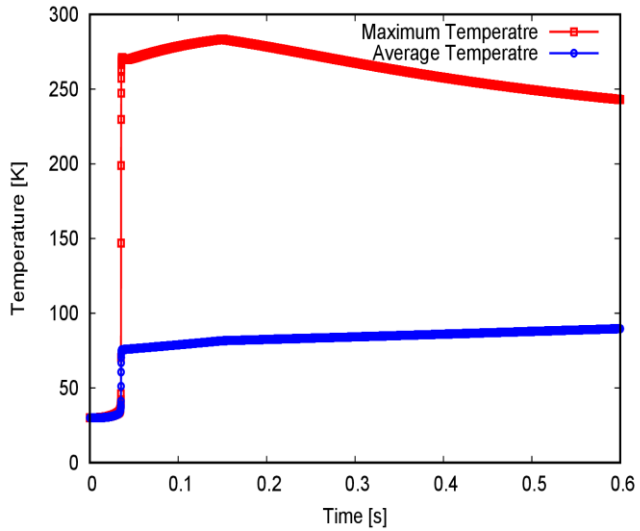
1000 V DC



Quench occurs earlier for higher amplitude of short-circuit DC voltage

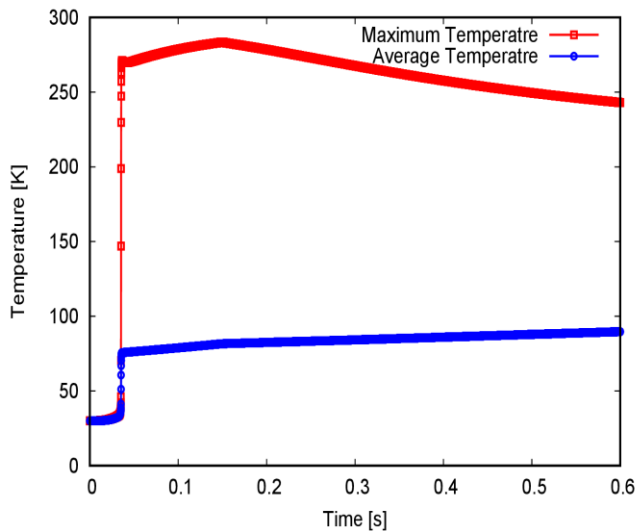
# Short-Circuit DC Voltage

10 V DC

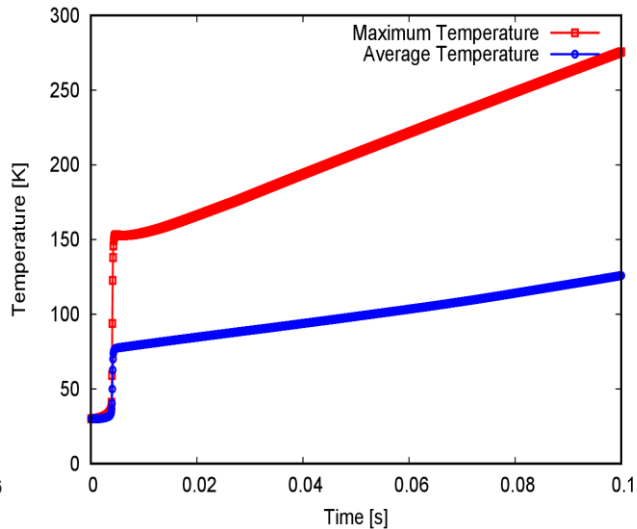


# Short-Circuit DC Voltage

## 10 V DC



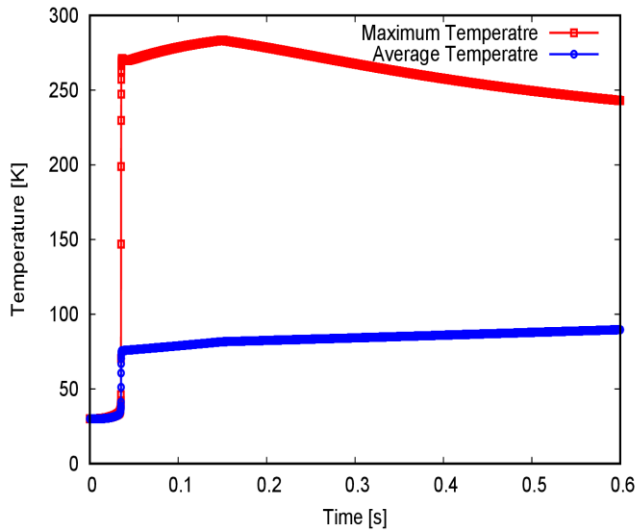
## 100 V DC



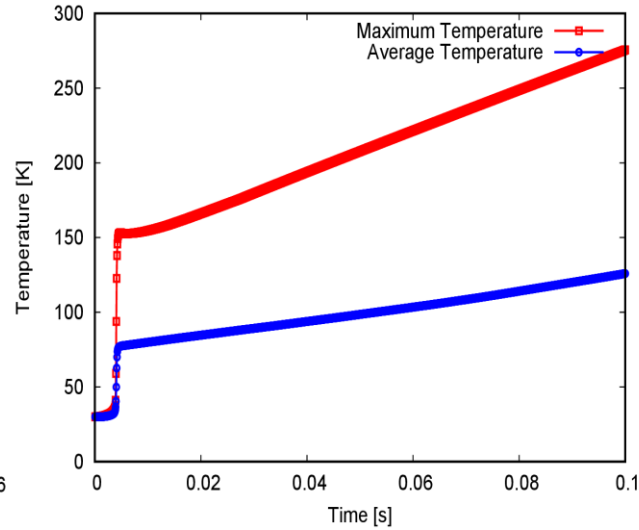


# Short-Circuit DC Voltage

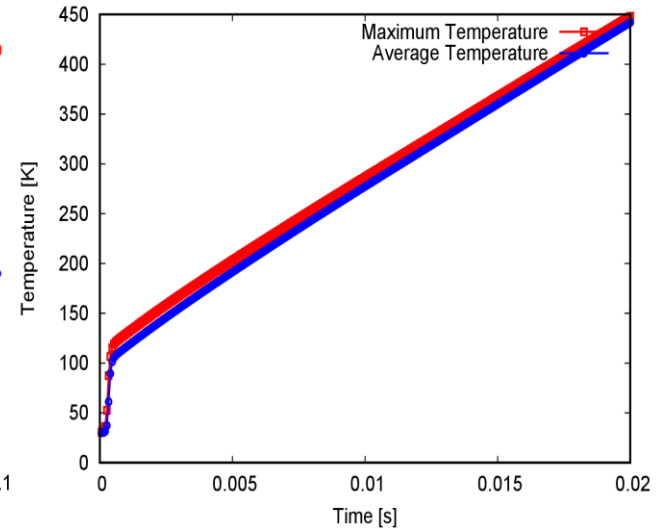
10 V DC



100 V DC



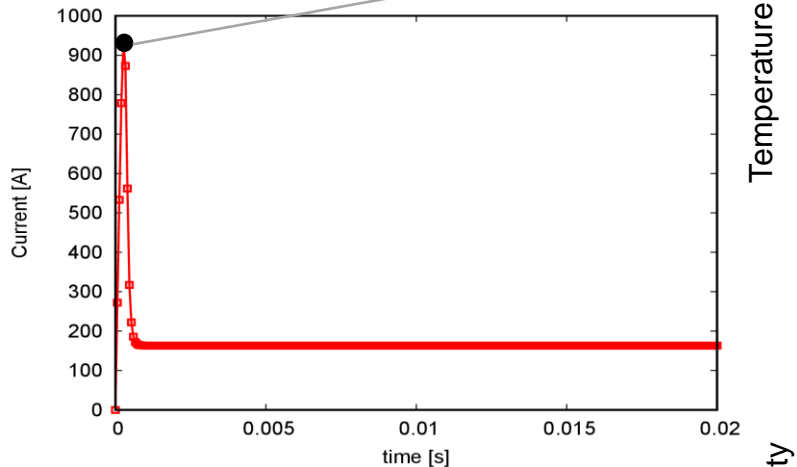
1000 V DC



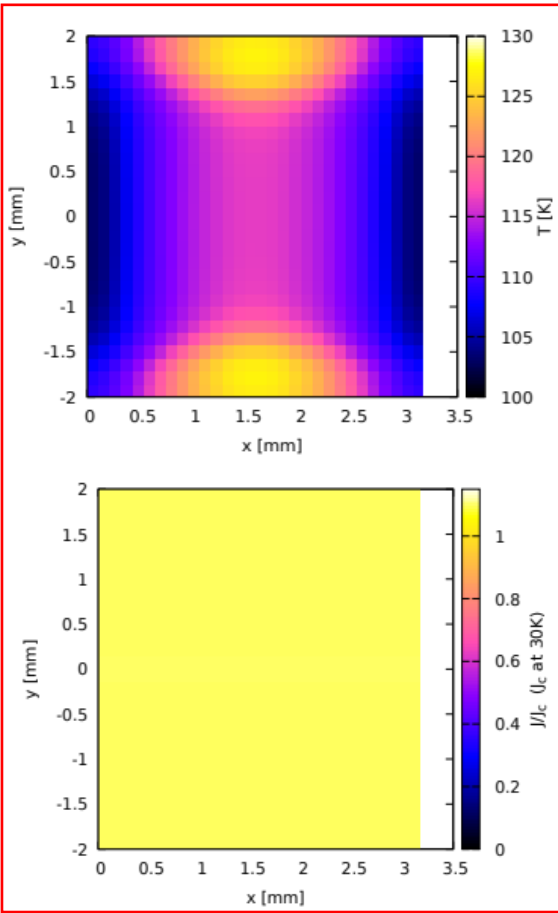
Sharp temperature rise occur for higher amplitude of short-circuit DC voltage

# Short-Circuit DC Voltage

1000 V DC



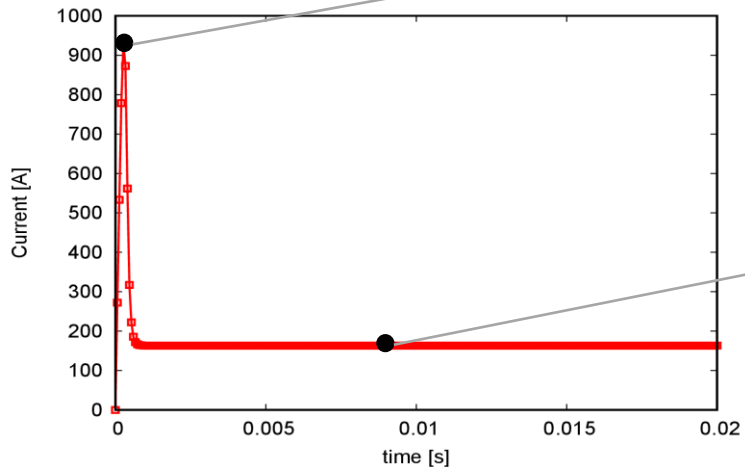
Temperature [K]  
Normalized current density



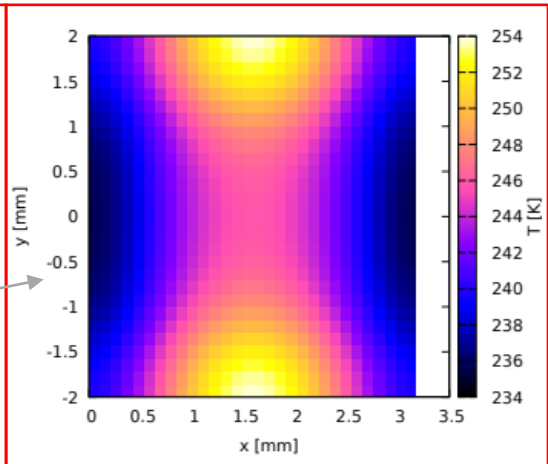
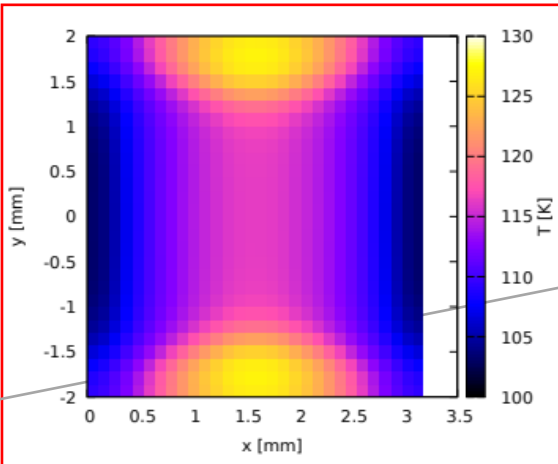
- Significant Temperature rise

# Short-Circuit DC Voltage

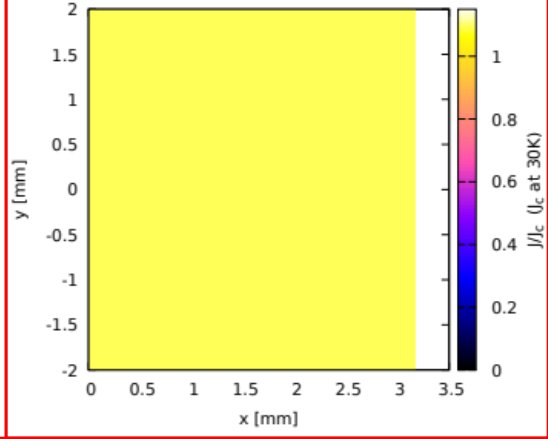
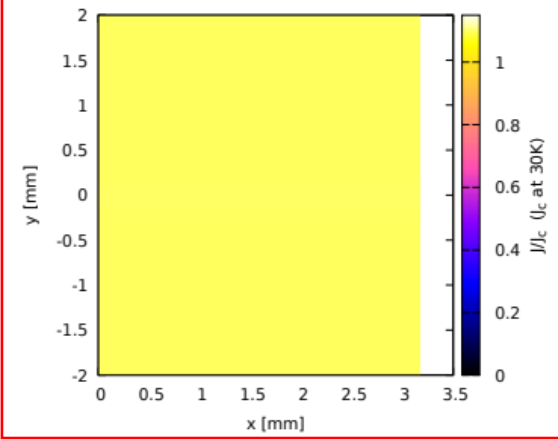
1000 V DC



Temperature [K]



Normalized current density



- $T > T_c$
- $J > J_c$  (Overcritical state)

- Modeling methods
- Studied configuration
- Varying voltage cases
- **Conclusion**

# Conclusion

- Multiphysics electromagnetic and thermal modeling of racetrack coil in motor for aviation

# Conclusion

- Multiphysics electromagnetic and thermal modeling of racetrack coil in motor for aviation
- Electrothermal modeling with temperature dependent thermal variables

# Conclusion

- Multiphysics electromagnetic and thermal modeling of racetrack coil in motor for aviation
- Electrothermal modeling with temperature dependent thermal variables
- For both 1 V DC and 10 V DC, at 30 K, temperature does not exceed the maximum limit to damage the superconductor

# Conclusion

- Multiphysics electromagnetic and thermal modeling of racetrack coil in motor for aviation
- Electrothermal modeling with temperature dependent thermal variables
- For both 1 V DC and 10 V DC, at 30 K, temperature does not exceed the maximum limit to damage the superconductor
- For both 100 and 1000 V DC, maximum temperature could damage the superconductor



**Thank you for your attention!**