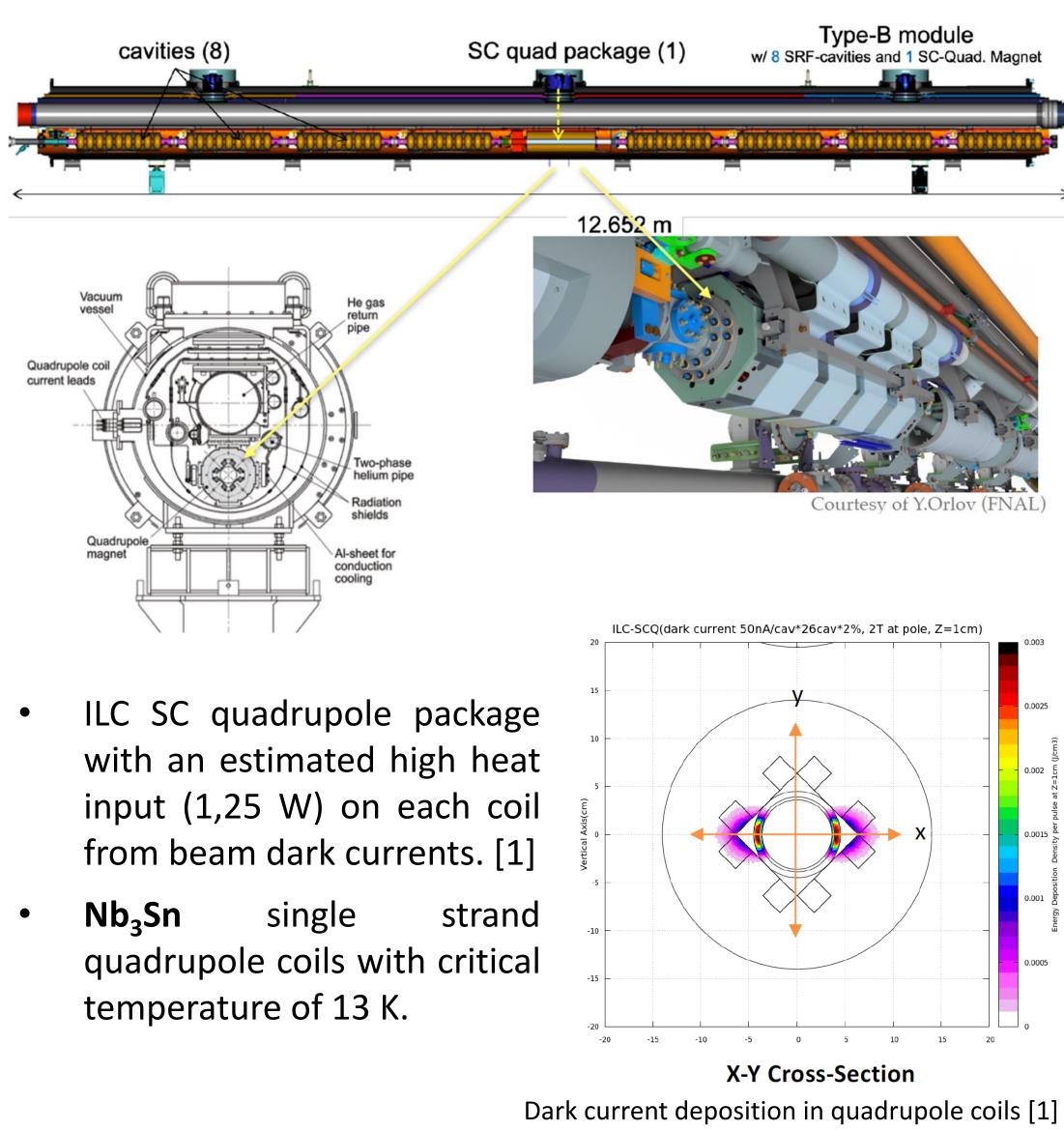
Thermal analysis of a conduction-cooled superconducting quadrupole for ILC Main Linac with large temperature margin

Supported by the Spanish Ministry of Science, Innovation and Universities under 2020 R&D Program, project PID2020-120582GB-I00

Abstract: The Main Linac of the International Linear Collider (ILC) includes superconducting quadrupole (SCQ) packages that are located between the superconducting RF cavities, with one SCQ within each of the Type-B cryomodules. This combined-functioned, splittable superconducting magnet focus and steer the electrons and positrons. The magnet is required to be cryogen free, and conductively cooled down via thermal links. This links should be connected to the outer surface of the transfer line that supplies liquid helium to the RF cavities. Additionally, to address the large heat deposition expected in the superconducting coils due to beam-induced dark currents, the use of Nb₃Sn strand is advocated for the coil, given their superior thermal margin related to NbTi.

This poster depicts a numerical analysis of the thermal behaviour of the impregnated Nb₃Sn quadrupole coils and proposes a conduction-cooling strategy for these coils. The anisotropic behaviour of the coil has been thoroughly examined. A highly conductive casing for the coil has been designed and high purity aluminium sheets have been integrated to significantly improve thermal management.

Introduction



[1] A. Yamamoto et al., "Dark Current Electrons and Irradiation Heating of Superconducting Magnets for High-Gradient SRF Linacs", presented at TTC-2021, DESY (online), 20 Jan. 2020

^aÓ. Durán (CIEMAT and UPM), L. García-Tabarés, L. González, F. Toral (CIEMAT), Y. Arimoto, T. Yamada, A. Yamamoto (KEK).

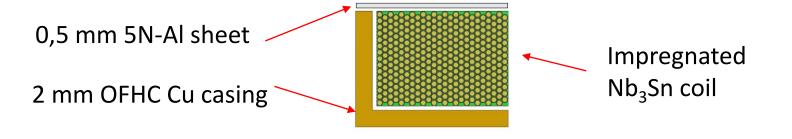
Materials

Highly conductive materials around the coil to extract dark current heat deposition.

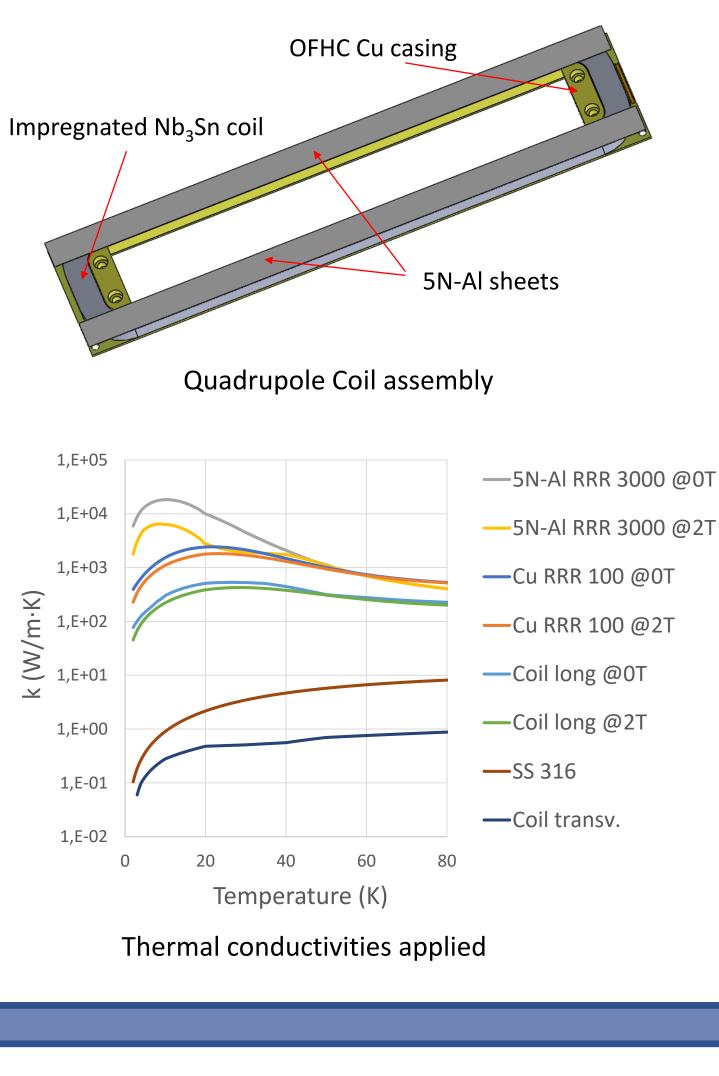
- OFHC Copper for the casing on the bottom and lateral of the coil.
- Al 5N Sheets on top of the coil.

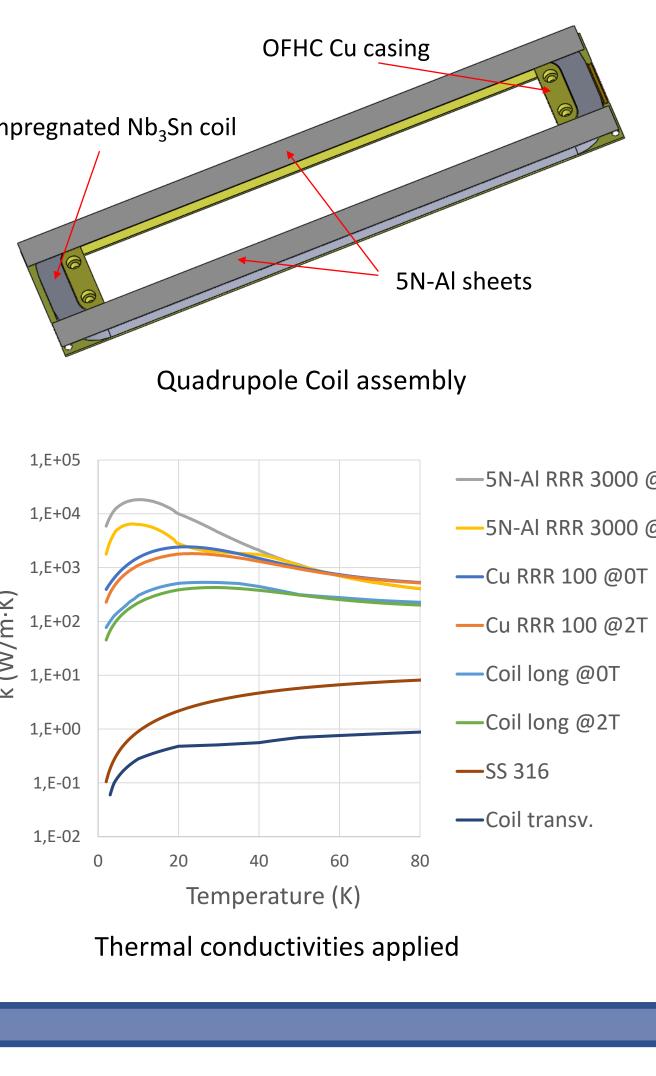
Anisotropy of the impregnated, fiberglass insulated, Nb₃Sn Coil is considered in the thermal conductivity estimations:

- Cross-section: Layers of **resin** in series with layers of copper. Cu as perfect conductor.
- Longitudinally: **Copper + bronze** + SC + charged resin + uncharged resin in parallel. SC and resin assumed non-conductor.



Quadrupole coil assembly cross-section





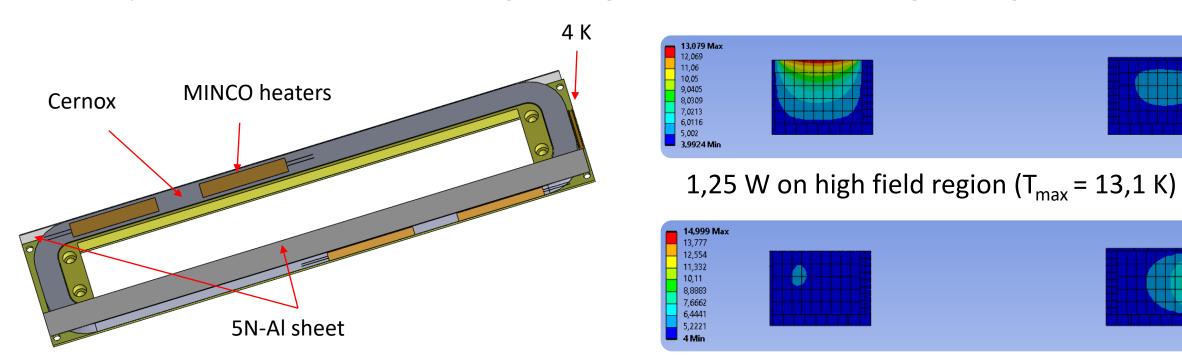
FEM approach (ANSYS)

- 3-D evaluation of coil, Cu casing and Al sheet heat extraction.
- Steady state 1,25 W internally generated in 1/8 of the coil and 4 K in the extremity.

Maximum temperature in coil (K)				
Analytical 1-D	FEM 3-D			
13,4 K	11,5 K			
9,2 K	7,7 K			
11,504 Max 10,67 9,8363 9,0025 8,1688 7,335 6,5013				
	Analytical 1-D 13,4 K 9,2 K			

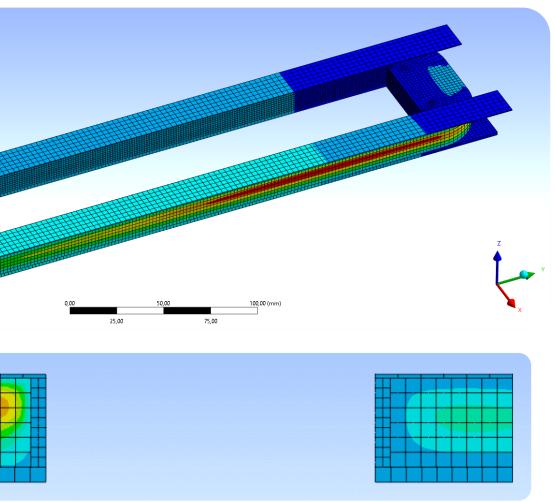
Test coil:

Superficial heaters heating in regions of low and high magnetic field in the coil.

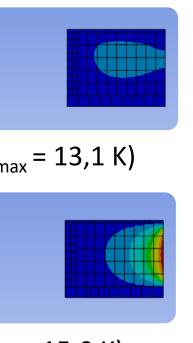


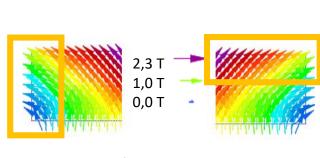
1,25 W on low field region ($T_{max} = 15,0$ K)





to high purity 5N Al sheets on top of the coil

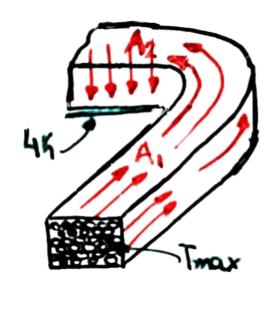


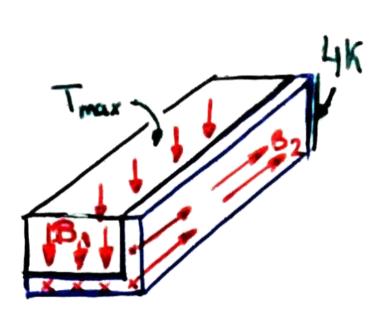


Magnetic field seen by the coil: Q@40T/m + D@0,10T

Analytical approach

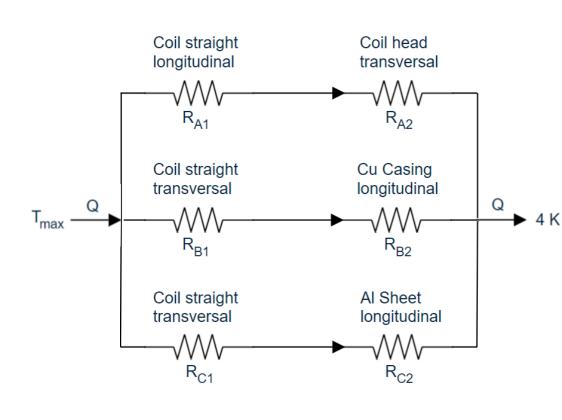
1-D model analyzing the contribution of the three parallel thermal paths, evaluated with the conduction heat transfer equation and the equivalent circuit of the system:





A. Longitudinally via strand + transversally via coil head.

 $\dot{Q} = \frac{\Delta T}{D} = \Delta T \cdot \frac{k_m \cdot A}{T}$



Conclusions

- understanding of the coil assembly heat transfer.

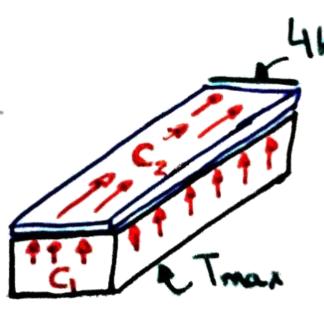
- quadrupole coil in the ILC SC magnet.
- Next steps:

 - Fabrication and test of the proposed test coil.





B. Transversally via coil section + longitudinally via Cu Casing.



C. Transversally via coil section + longitudinally via Al sheet.

		A/L (m)	k _m (W/m∙K)	R _k (K/W)		
	R _{A1}	1e-3	256	3,9	R _A	22,8
	R_{A2}	2e-1	0,25	18,9		
	$R_{\mathtt{B1}}$	3e-1	0,31	11,3	D	17.0
	R_{B2}	3e-4	566	5,7	R _B	17,0
	R_{C1}	9e-1	0,32	3,6	D	7 2
	R_{C2}	5e-5	5350	3,7	R _C	7,3

Analytical and FEM models offer a complete and complementary

Impregnated bronze-route Nb₃Sn anisotropy and magnetoresistance influence the materials considerations for the calculations.

Conduction through coil resin is the bottle neck of the heat transfer chain. A test coil configuration is identified to simulate the requirements of the

Design and fabricate a test station. See poster Thu-Po-3.5.

