

VACI Suite updates

FCC Booster and Main Ring optimization

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Rainer Wanzenberg (DESY), A Ghribi (CNRS), M. Migliorati (UniRoma)

HELMHOLTZ



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FUTURE
CIRCULAR
COLLIDER



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VACI Suite

Behind the scenes

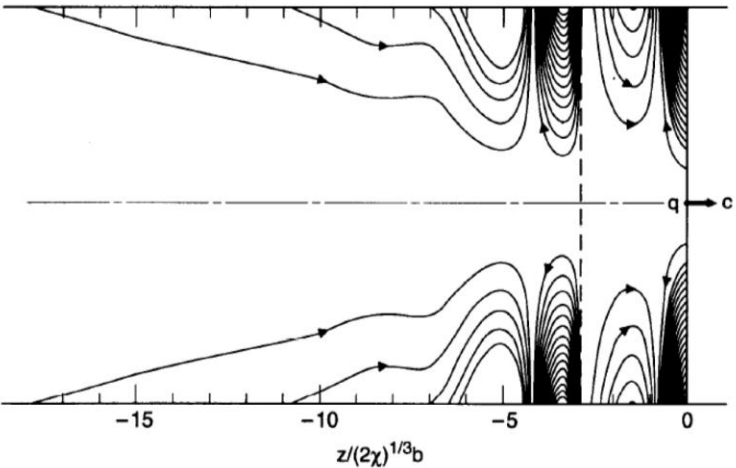
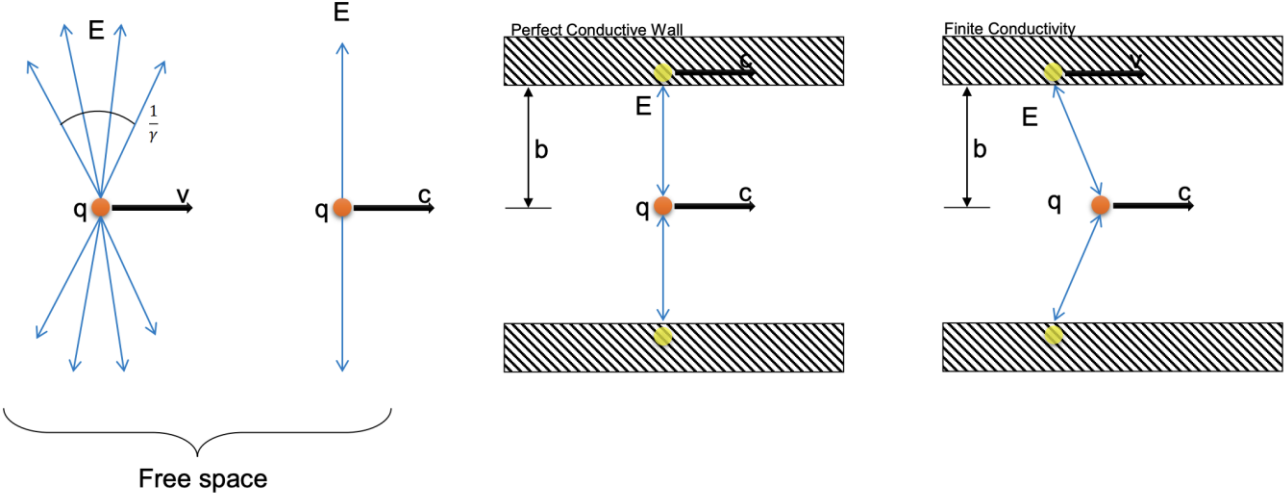
However difficult life may seem, there is always something you can do and succeed at.

Stephen Hawking

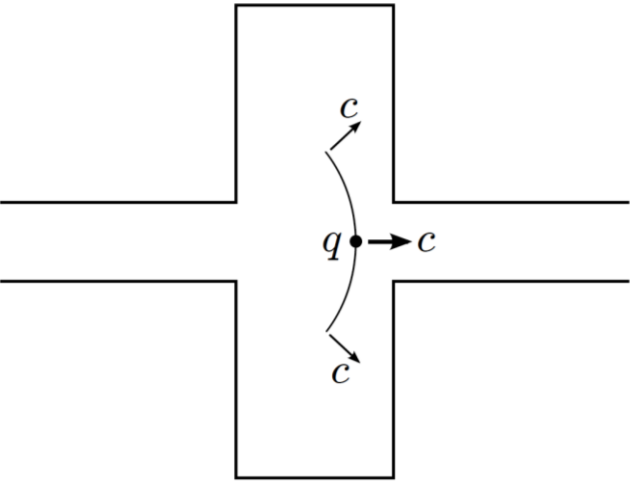
Introduction

What are collective effects?

- Interactions between particles within a beam are generally known as collective effects
 1. Incoherent
 - ❖ Space-charge
 - ❖ Scattering
 2. Coherent
 - ❖ Wake-fields



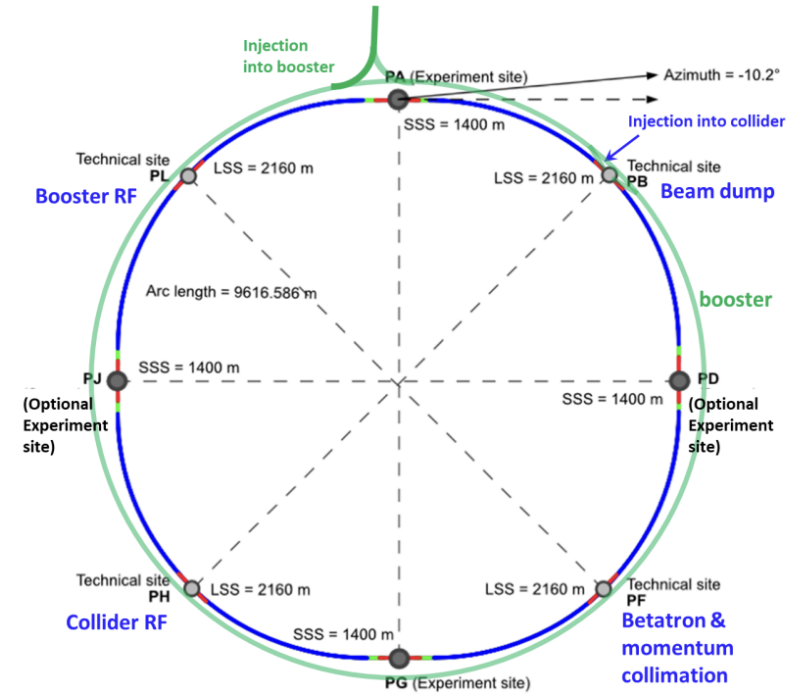
Wake fields following a point charge in a cylindrical beam pipe with resistive walls. (K. Bane)



Source of Impedance in the Ring

FCC Rings (old parameters, CDR)

- Beam pipes (Resistive Wall Impedance, ~ 90.7 km)
- RF Cavities (No. 48 in a 4-cell array)
- RF Cavity Tapers (No. 12 double tapers)
- Synchrotron Radiation Absorbers
- Collimators (No. 8)
- BPMs (No. 8000)
- Bellows (No. 12000)



Wake-field

Maxwell's equation

$$\begin{aligned}\operatorname{div} \vec{D} &= \rho_m, \\ \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}_m, \\ \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, \\ \operatorname{div} \vec{B} &= 0,\end{aligned}$$

$$\rho(r, z; \omega) = J_z(r, z; \omega)$$

$$J_n = \frac{Q_n}{A} \sigma(r; a, b) e^{in\theta} e^{-iks}$$

where:

$\sigma(r; a, b)$ means particles are in a ring with a thickness of (b-a)

A is the ring area

θ is the angle distribution of electrons around the ring

$$\vec{E} = -\vec{\nabla}\varphi - \frac{\partial}{\partial t} \vec{A} \quad \text{And} \quad \vec{B} = \vec{\nabla} \times \vec{A}$$

$$\vec{\nabla} \cdot \vec{A} = 0 \quad \text{Coulomb gauge}$$

$$\partial_t \Rightarrow -i\omega \quad \text{Fourier Transform}$$

$$\partial_z \Rightarrow -i\omega/v \quad \text{long pipe Appr.}$$

Boundary Condition

$$\begin{cases} \vec{\nabla} \cdot (\epsilon \vec{\nabla} \varphi) = \rho_m \\ \vec{\nabla} \times (1/\mu \vec{\nabla} \times \vec{A}) - \epsilon \omega^2 \vec{A} = -J_n \hat{e}_z + i\epsilon \omega \vec{\nabla} \varphi \end{cases}$$

Resistive wall wake-field

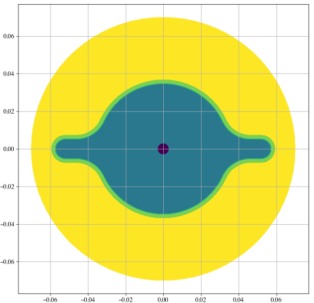
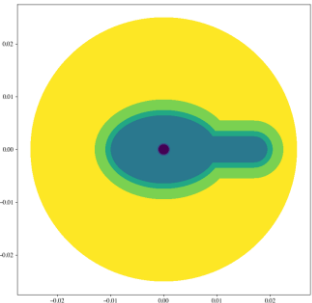
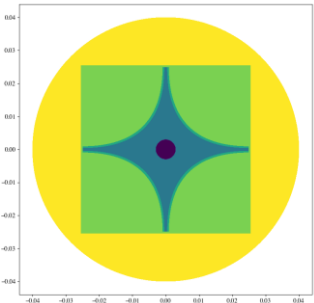
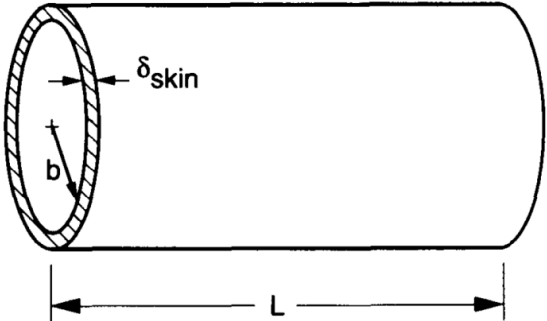
Simple Geometries

$$E_s = -\frac{16q}{4\pi\epsilon_0 b^2} \left(\frac{e^u}{3} \cos(\sqrt{3}u) - \frac{\sqrt{2}}{\pi} \int_0^\infty \frac{x^2 e^{ux^2}}{x^6 + 8} dx \right), \quad (14.114)$$

$$E_r = cB_\theta = \frac{8qr}{4\pi\epsilon_0 b^3 \xi^{2/3}} \times \left(\frac{e^u}{3} \cos(\sqrt{3}u) - \frac{e^u}{\sqrt{3}} \sin(\sqrt{3}u) - \frac{\sqrt{2}}{\pi} \int_0^\infty \frac{x^4 e^{ux^2}}{x^6 + 8} dx \right), \quad (14.115)$$

where:

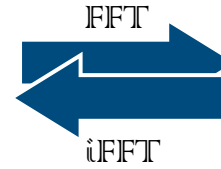
$$u = \frac{z}{b\xi^{2/3}}. \quad (14.116)$$



Resistive wall wake-field

How to calculate impedance

Wakefield



Impedance

Based on: *Robert L. Gluckstern and Uwe Niedermayer*

$$\underline{\vec{Z}}(\vec{r}_1^\perp, \vec{r}_2^\perp, \omega) = - \int_{-\infty}^{\infty} \vec{W}(\vec{r}_1^\perp, \vec{r}_2^\perp, s) e^{-i\omega s/v} \frac{ds}{v}. \quad \longrightarrow \quad \underline{\vec{Z}}(\vec{r}_1^\perp, \vec{r}_2^\perp, \omega) = - \frac{1}{q_1 q_2} \int_{-\infty}^{\infty} \vec{F}(\vec{r}_1^\perp, \vec{r}_2^\perp, z, \omega) e^{+i\omega z/v} dz,$$

Single particle

one should note that the integral is not a Fourier transform, but the wake integration in the frequency domain.

$$\left\{ \begin{array}{l} \vec{J}_s(\vec{r}_\perp, z, t) = q_1 \sigma(\vec{r}_\perp) \delta(z - vt) \vec{v} \\ \vec{J}_s(\vec{r}_\perp, z, \omega) = q_1 \sigma(\vec{r}_\perp) e^{-i\omega z/v} \vec{e}_z. \end{array} \right.$$

Integrating over the beam in FD
Like Convolution in TD

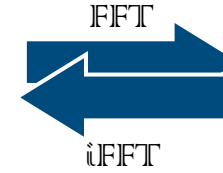
$$\underline{\vec{Z}}(\omega, \vec{r}_2^\perp) = - \frac{1}{q_1 q_2} \int_{\text{beam}} \vec{F}(\vec{r}_1^\perp, \vec{r}_2^\perp, z, \omega) e^{i\omega z/v} \sigma(\vec{r}_1^\perp) d\vec{r}_1^\perp dz.$$

$$\underline{Z}_{\parallel}(\omega) = - \frac{1}{q^2} \int_{\text{beam}} \vec{E} \cdot \vec{J}_s^* dV.$$

Resistive wall wake-field

How to calculate impedance

Wakefield



Impedance

Based on: *Elias Métral*

- *Non axis-symmetric structures:*
 - A current density with some azimuthal Fourier component may create an electromagnetic field with various different azimuthal Fourier components
 - ✓ A more general beam coupling impedance is **REQUIRED** to treat coupling of different azimuthal Fourier components

$$Z_{m,n}(\omega) = \int dv E_m * J_n^* \quad \text{over the beam area}$$

$$J_n = \frac{Q}{2\pi a^{|n|+1}} \delta(r-a) e^{jn\theta} e^{-jks} \quad \text{and } m, n = 0, +1, +2, \dots$$

Considering $m \geq 0$ instead of $m = 0, +1, +2, \dots$:

$$\left. \begin{array}{l} \bar{J}_m = J_m + J_{-m} \\ \bar{E}_m = E_m + E_{-m} \end{array} \right\} \Rightarrow \bar{Z}_m(\omega) = -\frac{1}{Q^2} \int dV (E_m + E_{-m})(J_m^* + J_{-m}^*)$$

$$\left\{ \begin{array}{l} \text{For } m = 0 : \quad \bar{Z}_0 = Z_{0,0} \\ \text{For } m \geq 1 : \quad \bar{Z}_m = Z_{m,m} + Z_{m,-m} + Z_{-m,m} + Z_{-m,-m} \end{array} \right.$$

Resistive wall wake-field

How to calculate impedance

Based on: *Robert L. Gluckstern, Elias Métral, and Uwe Niedermayer*

$$Z_{\perp} = A(z) + x_1 Z_{\perp}^{dip} + x_2 Z_{\perp}^{det}$$

Applying Panofsky-Wenzel theorem:

$$k Z_m^{\perp} = \nabla_w^{\perp} Z_m^{\parallel}$$

$$k Z_x = (Z_{0,1} + Z_{0,-1}) + x_1 \bar{Z}_x + j y_1 (-Z_{1,-1} - Z_{1,1} + Z_{-1,-1} + Z_{-1,1})$$

$$+ 2(Z_{0,2} + Z_{0,-2}) x_2 + 2(Z_{0,2} - Z_{0,-2}) j y_2$$

$$k Z_y = j(Z_{0,1} - Z_{0,-1}) + y_1 \bar{Z}_y + j x_1 (-Z_{1,-1} + Z_{1,1} - Z_{-1,-1} + Z_{-1,1})$$

$$- 2(Z_{0,2} + Z_{0,-2}) y_2 + 2(Z_{0,2} - Z_{0,-2}) j x_2$$

$$Z_x^{\text{driving}} = \bar{Z}_x / k$$

$$Z_y^{\text{driving}} = \bar{Z}_y / k$$

$$Z^{\text{detuning}} = -2(Z_{0,2} + Z_{0,-2}) / k$$

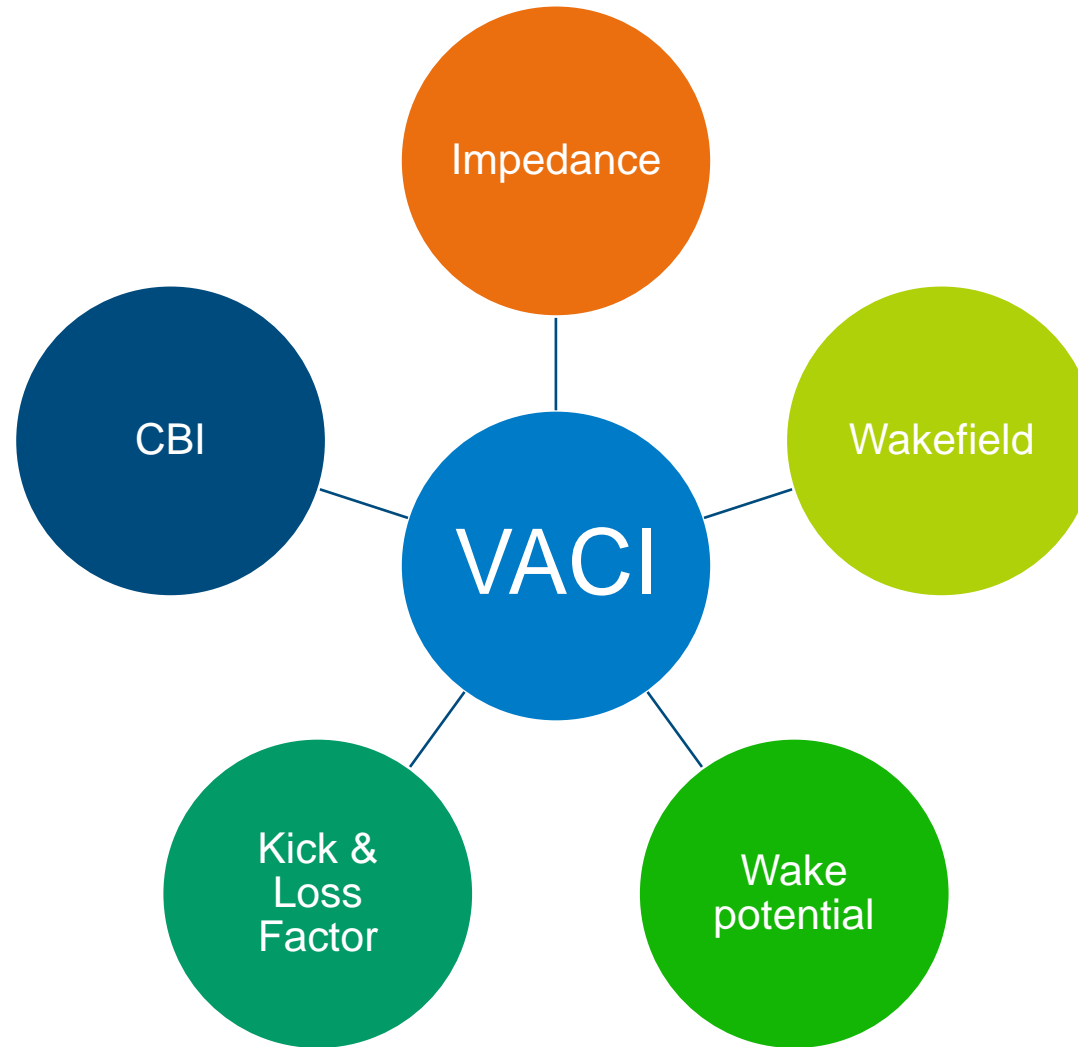


VACI Suite

A versatile tool for calculating the RW impedance in arbitrary pipe cross-sections

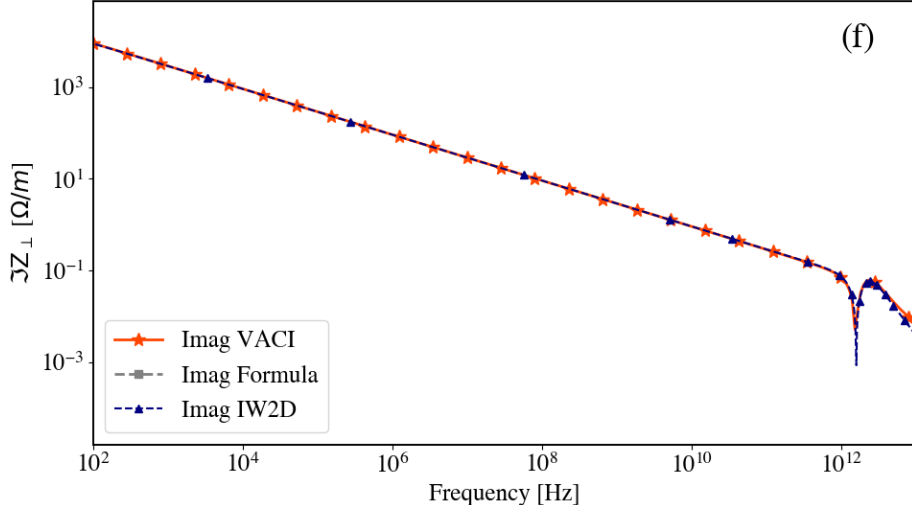
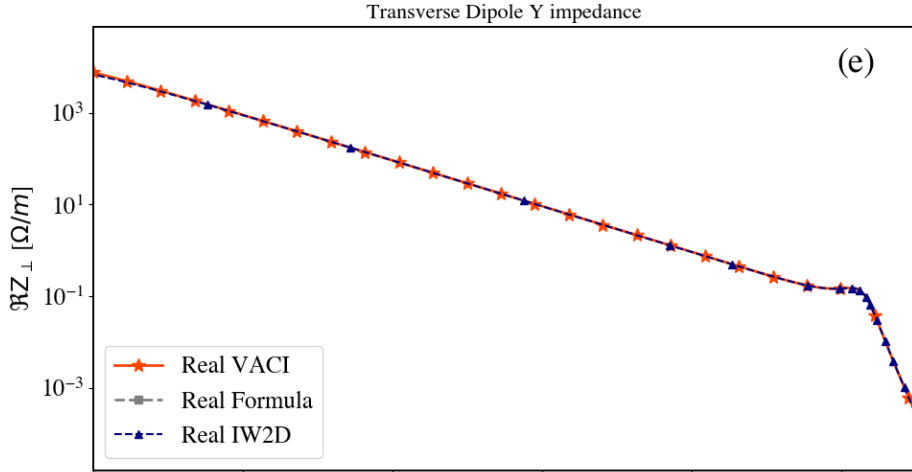
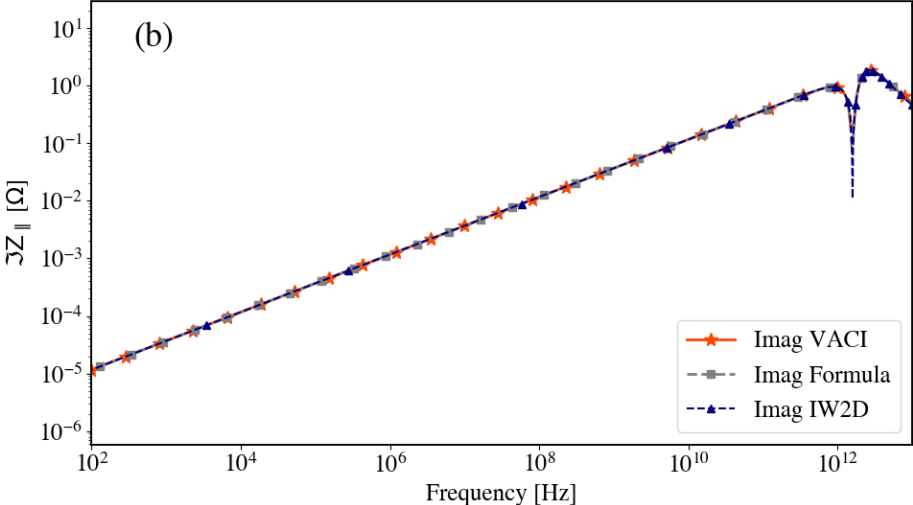
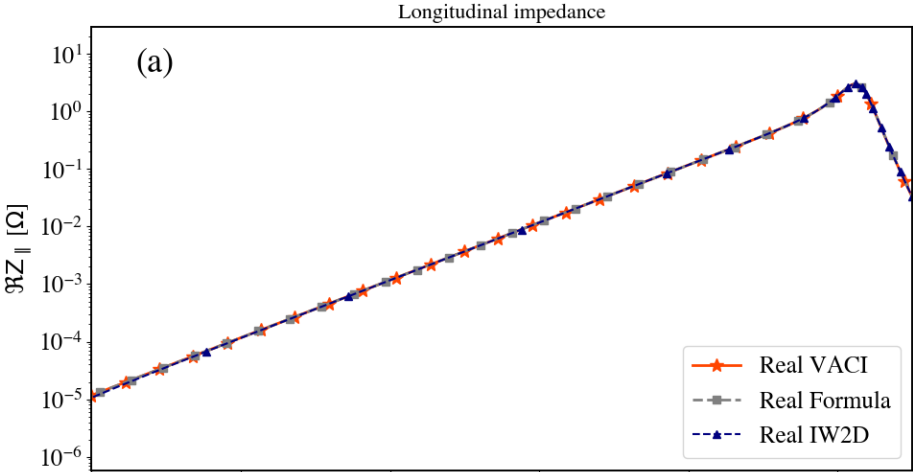
VACI Suite

Finite Element PDE solver



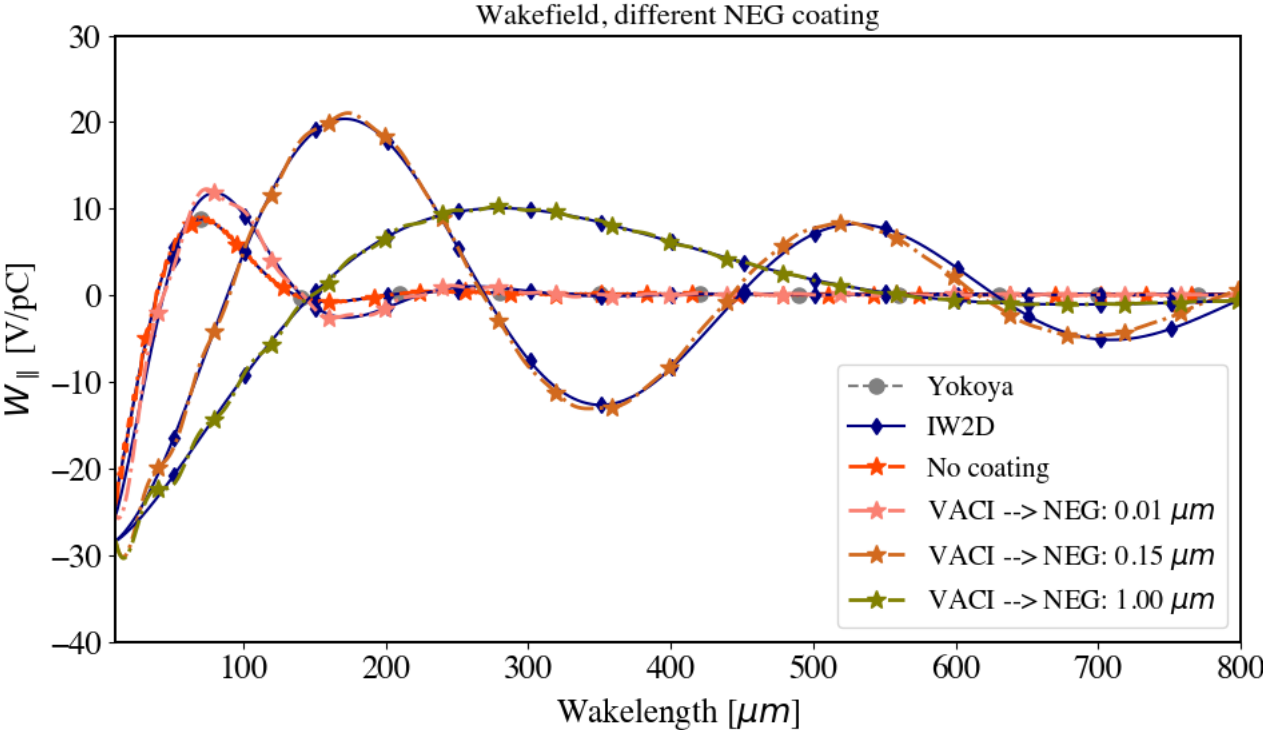
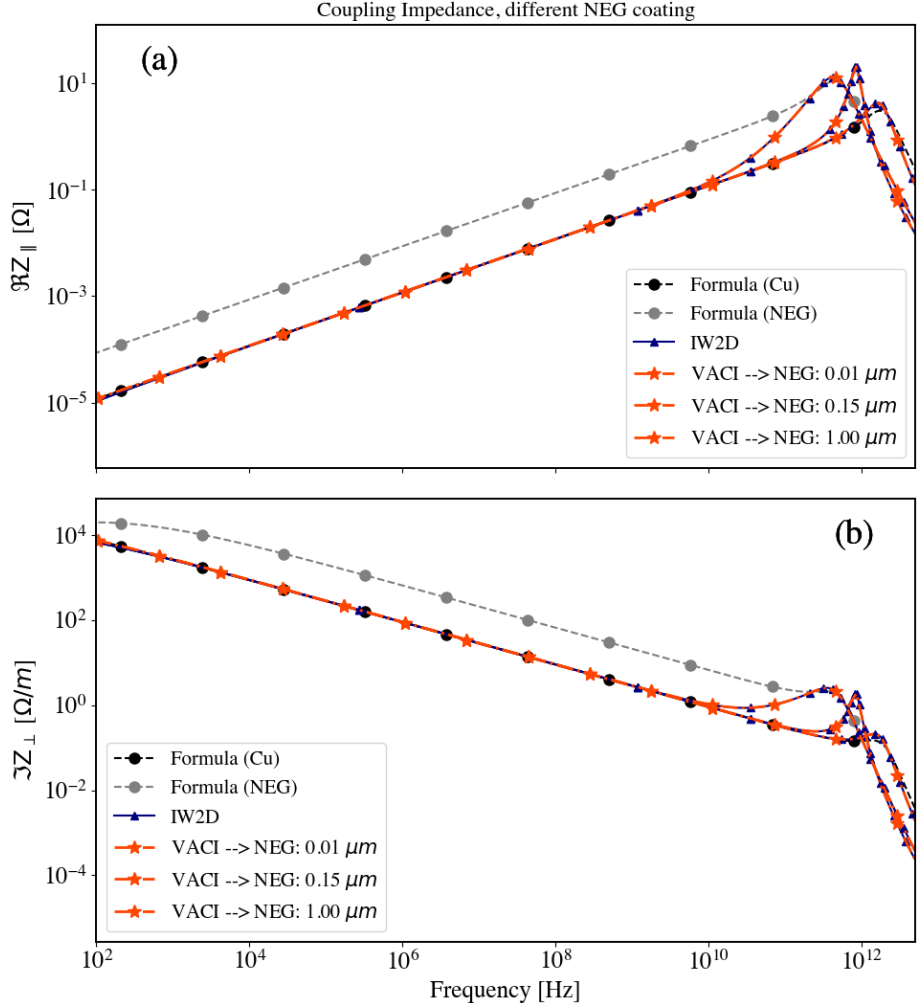
Round pipe

Impedance



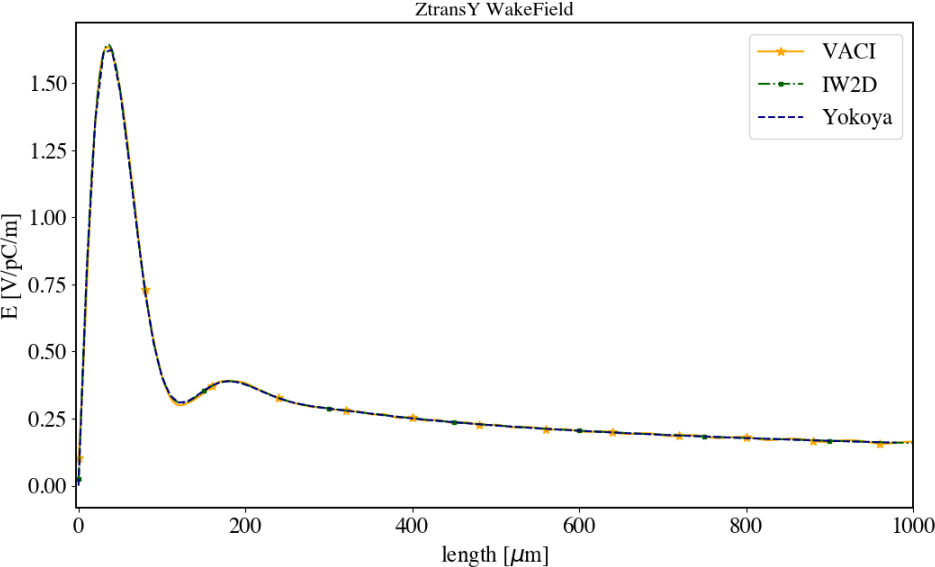
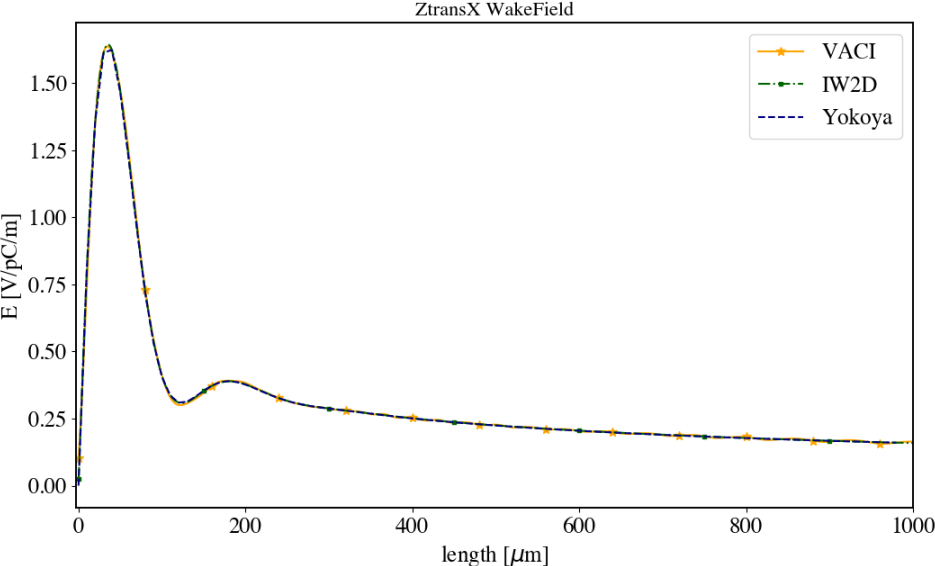
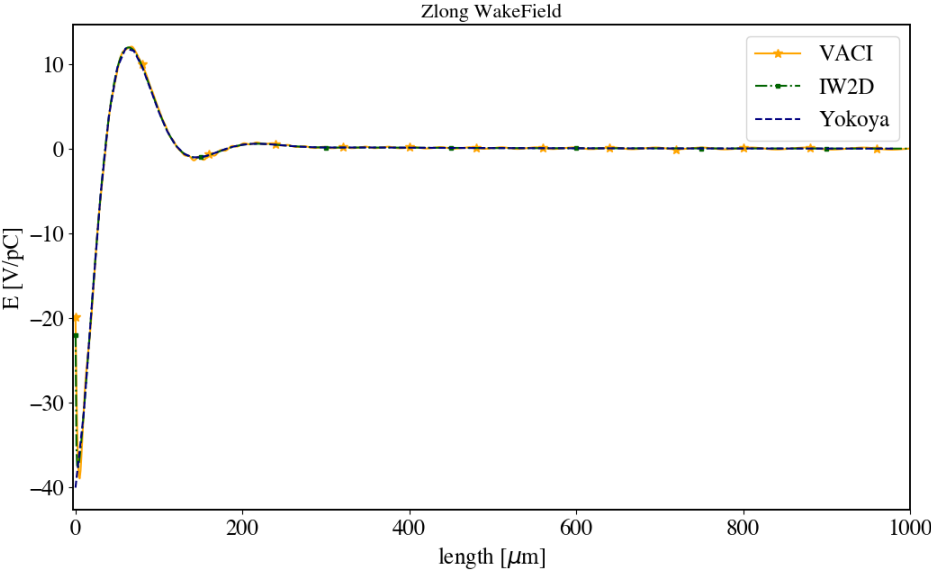
MultiLayer Pipes

NEG coating



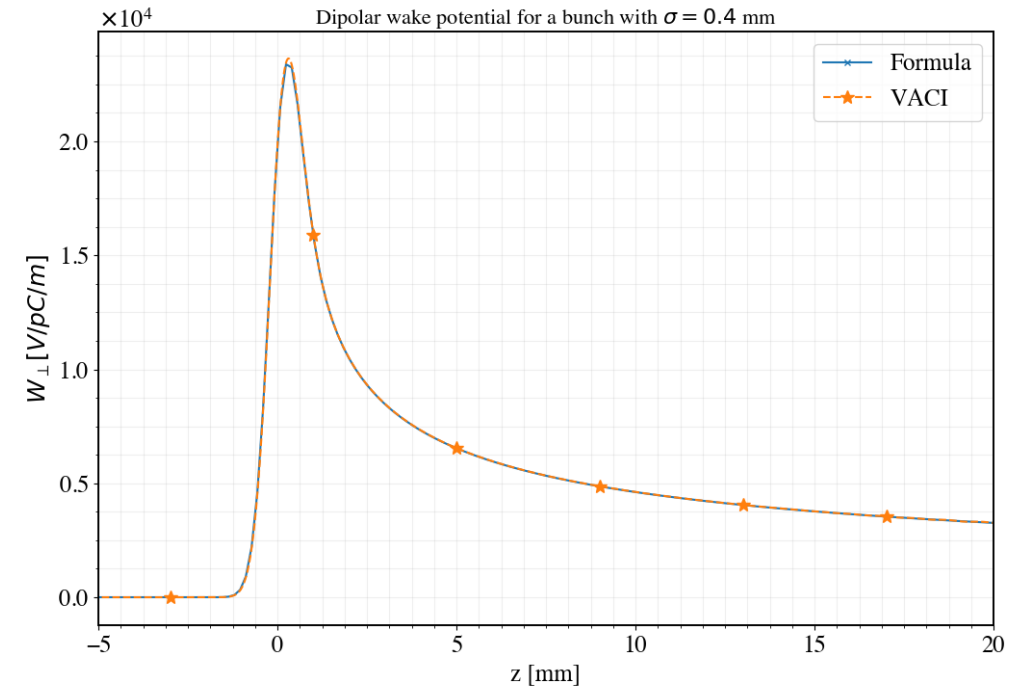
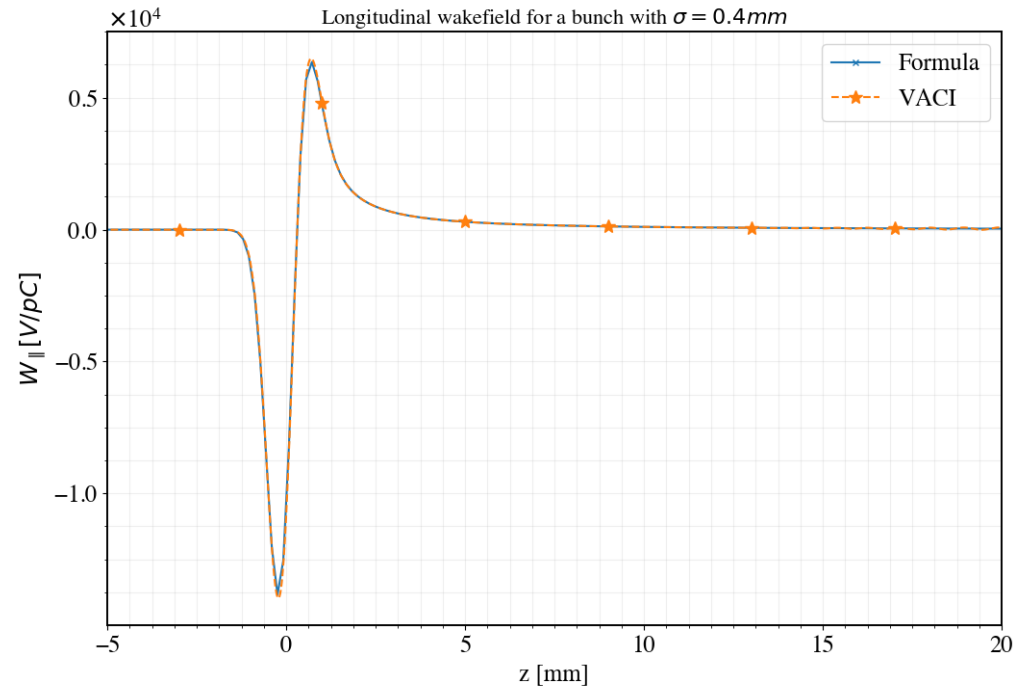
Round pipe

Wakefield, Green Function



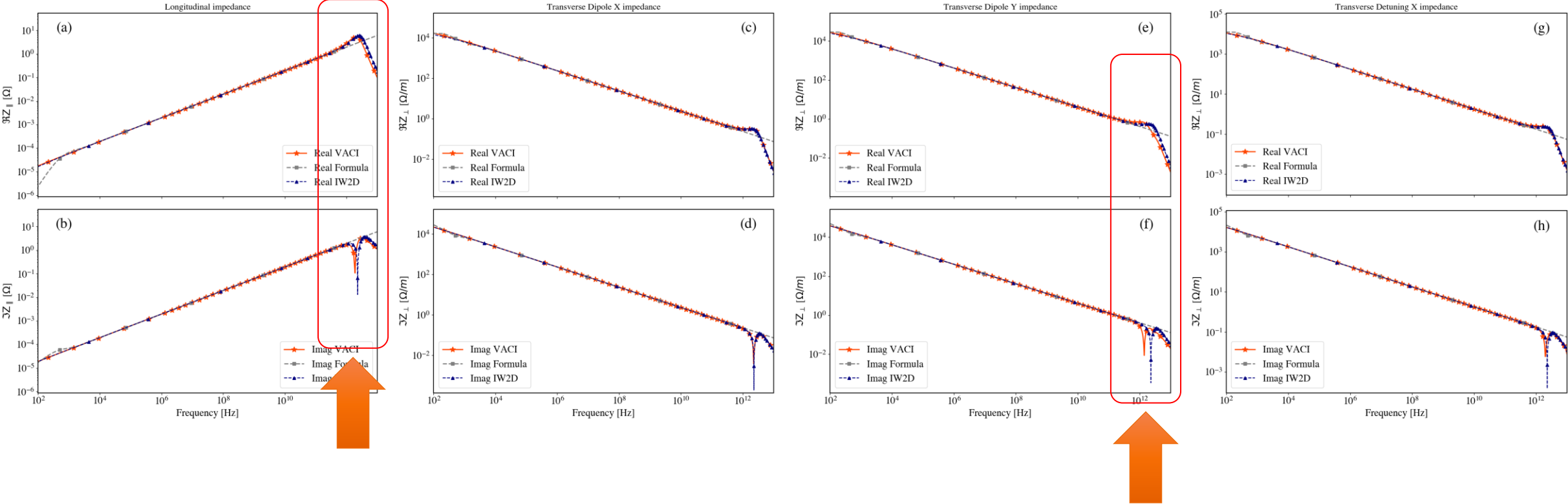
Round pipe

WakePotential $\sigma = 0.4 \text{ mm}$



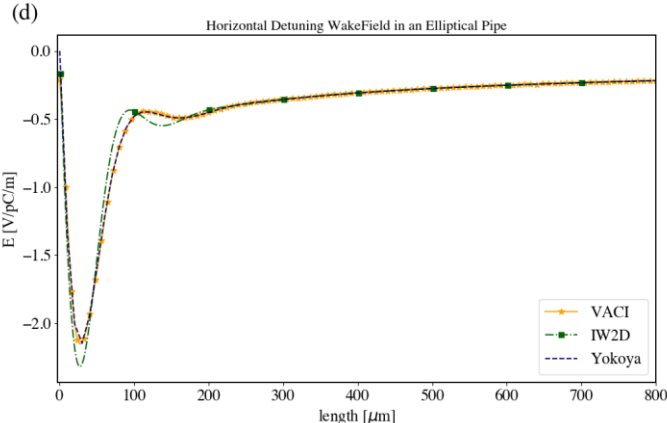
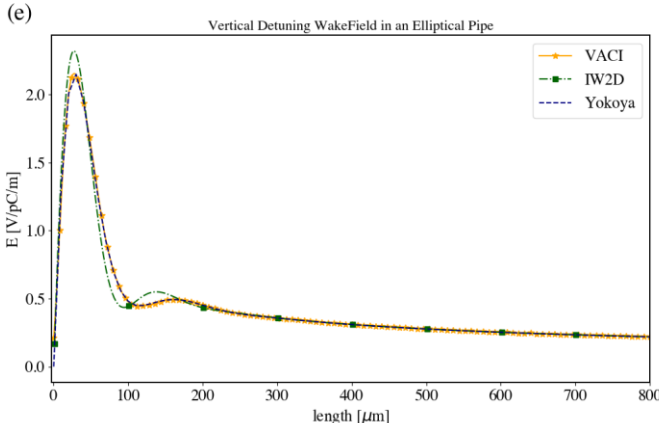
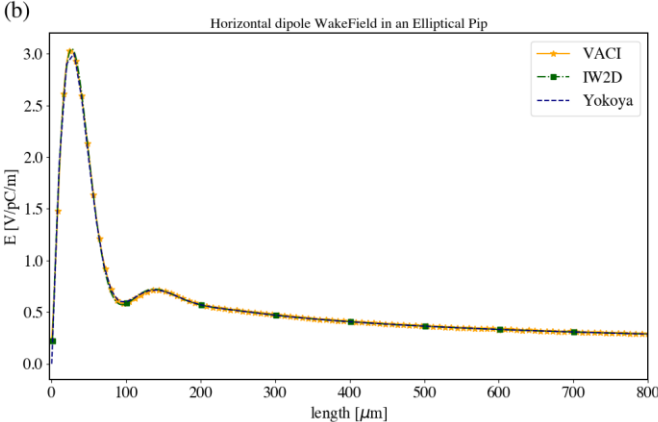
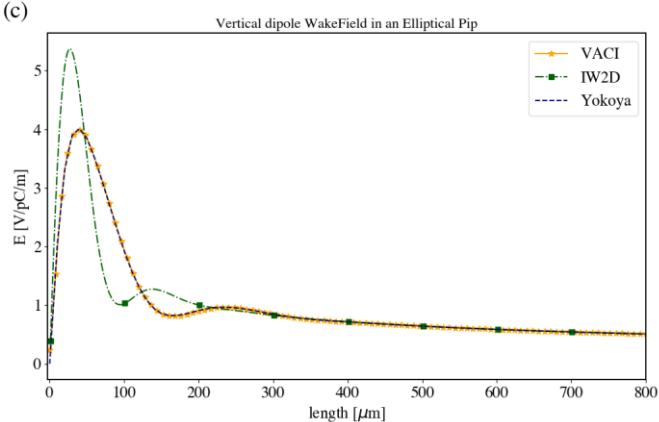
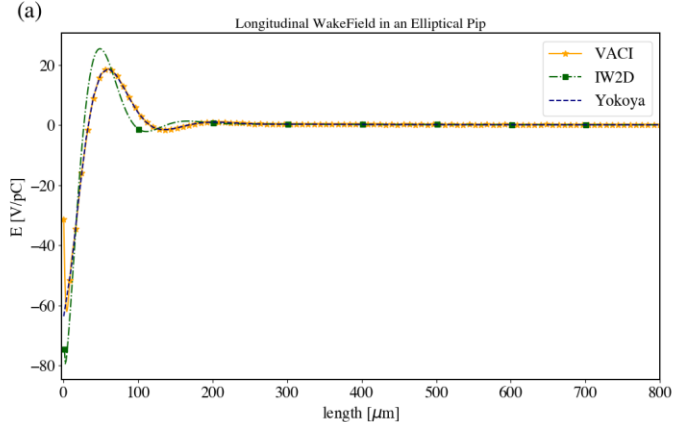
Elliptical pipe

Compare with IW2D and Analytical Formula



Elliptical pipe

Compare to IW2D and Yokoya's Code



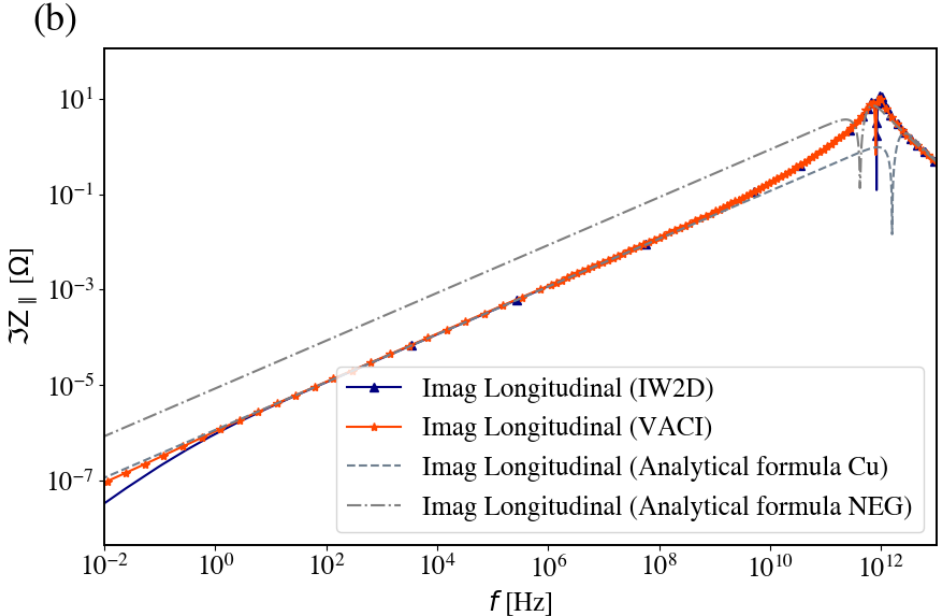
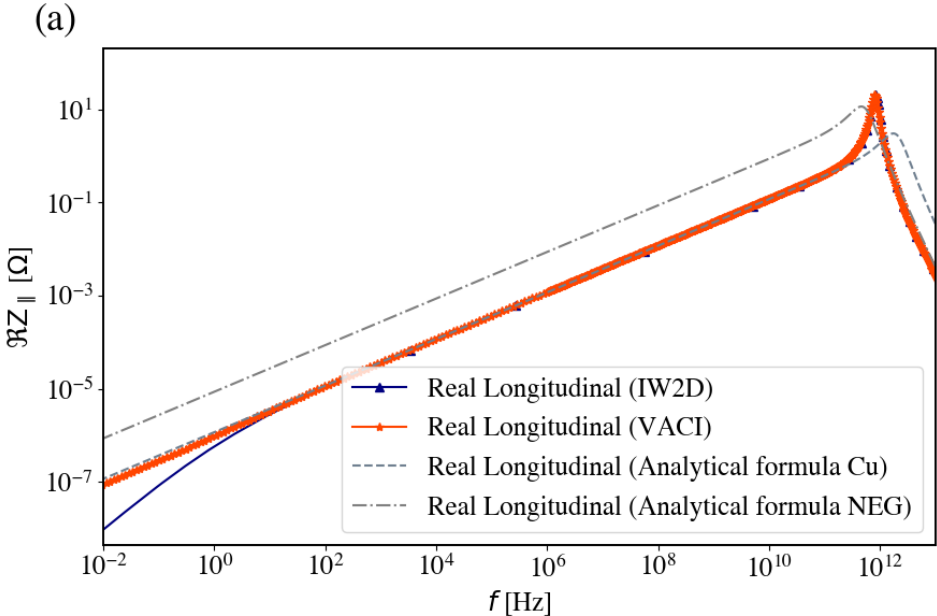
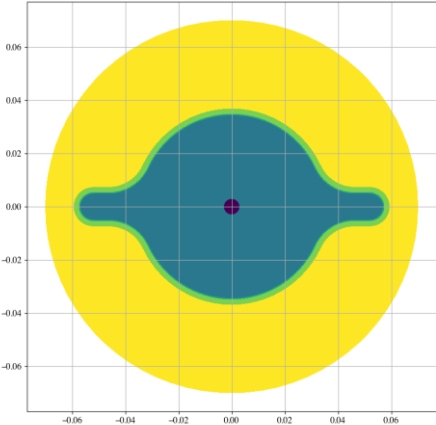
FCC Main Ring

- Round pipe with Winglets

FCC main Ring

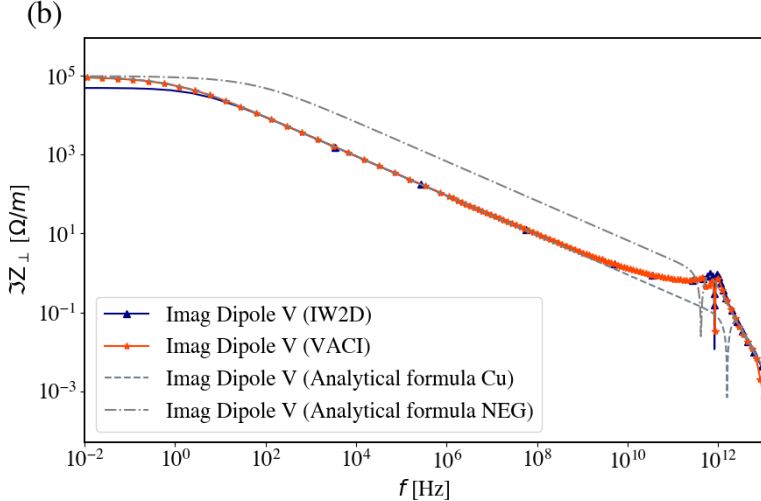
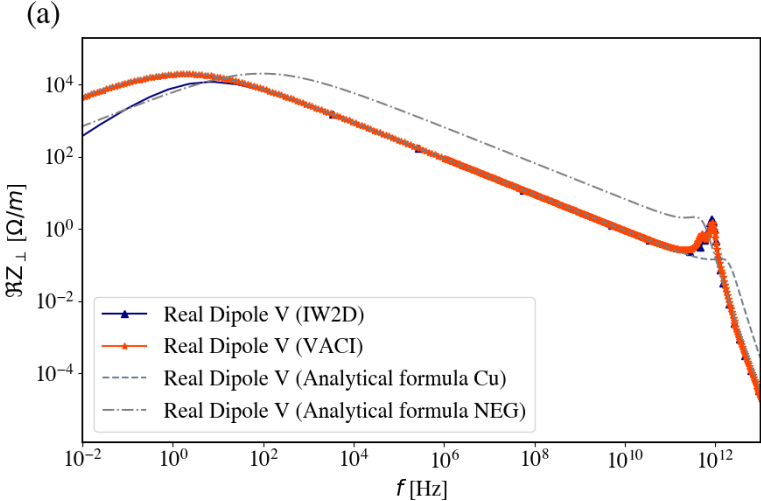
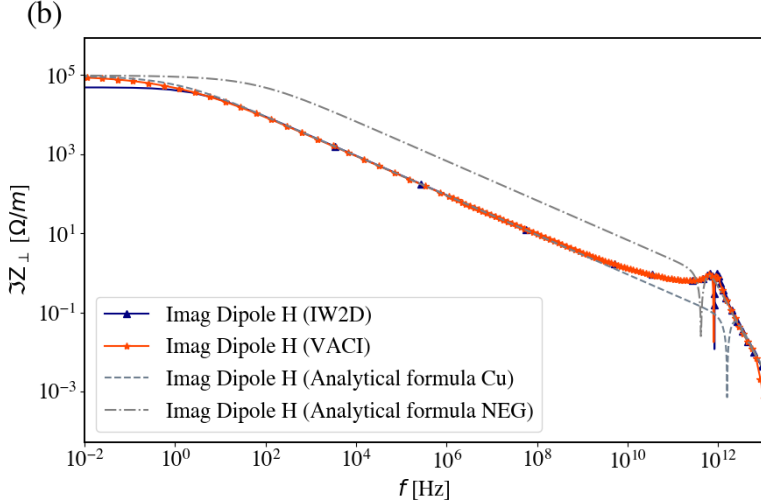
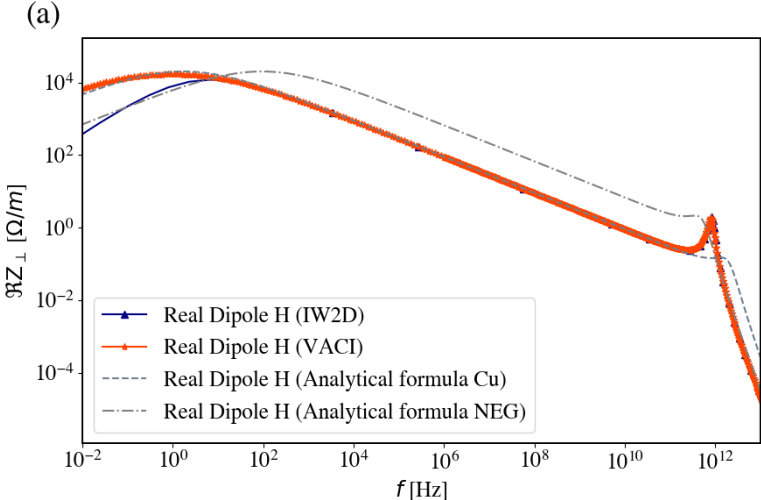
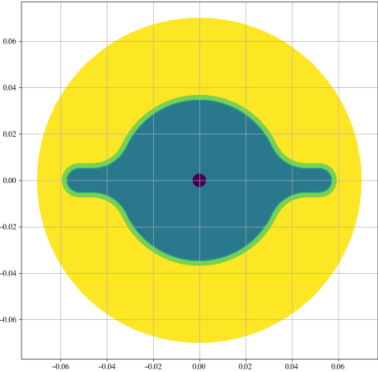
Monopolar Impedance

E -> 45.6 GeV
Pipe -> Cu (5.96e7 S/m)
NEG -> 1e6 (S/m)
R -> 35 mm



FCC main Ring

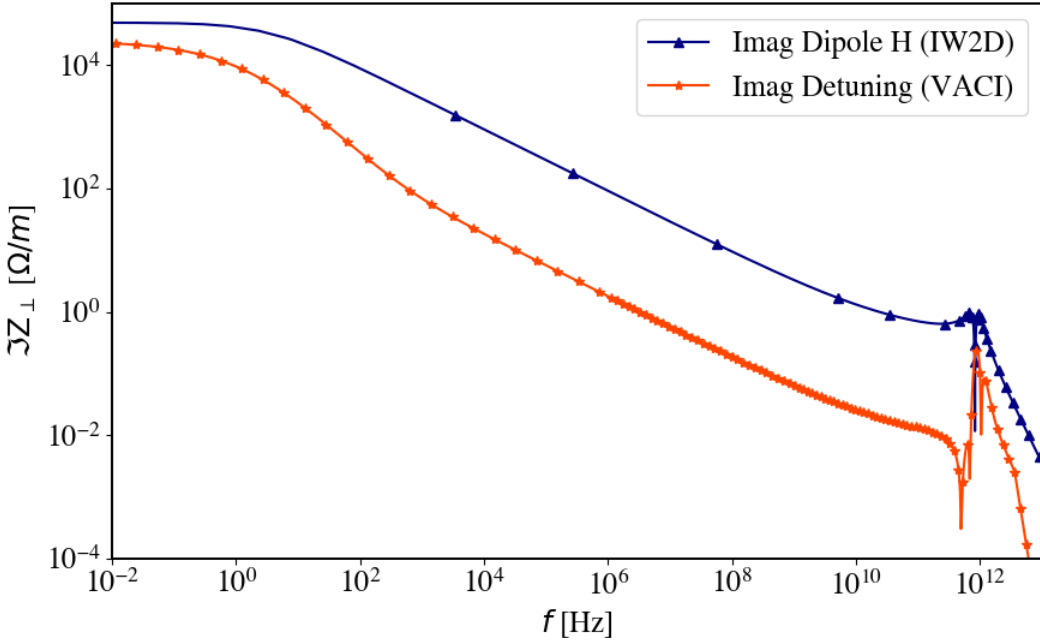
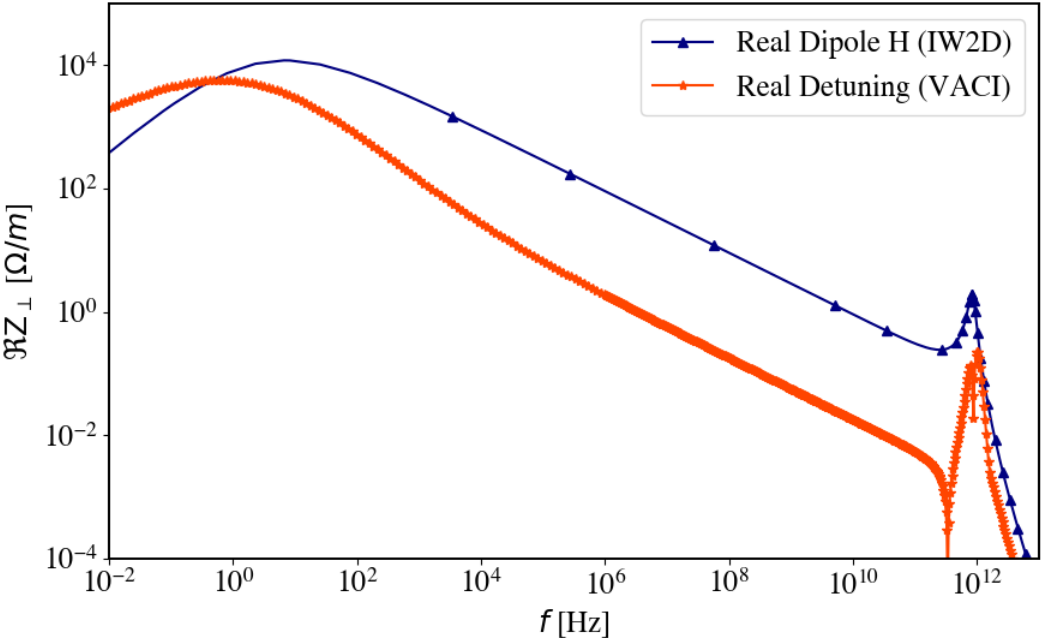
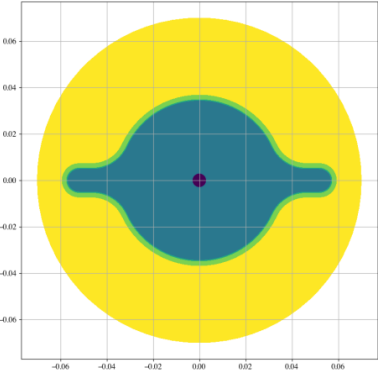
Dipolar Impedance



FCC main Ring

Detuning Impedance

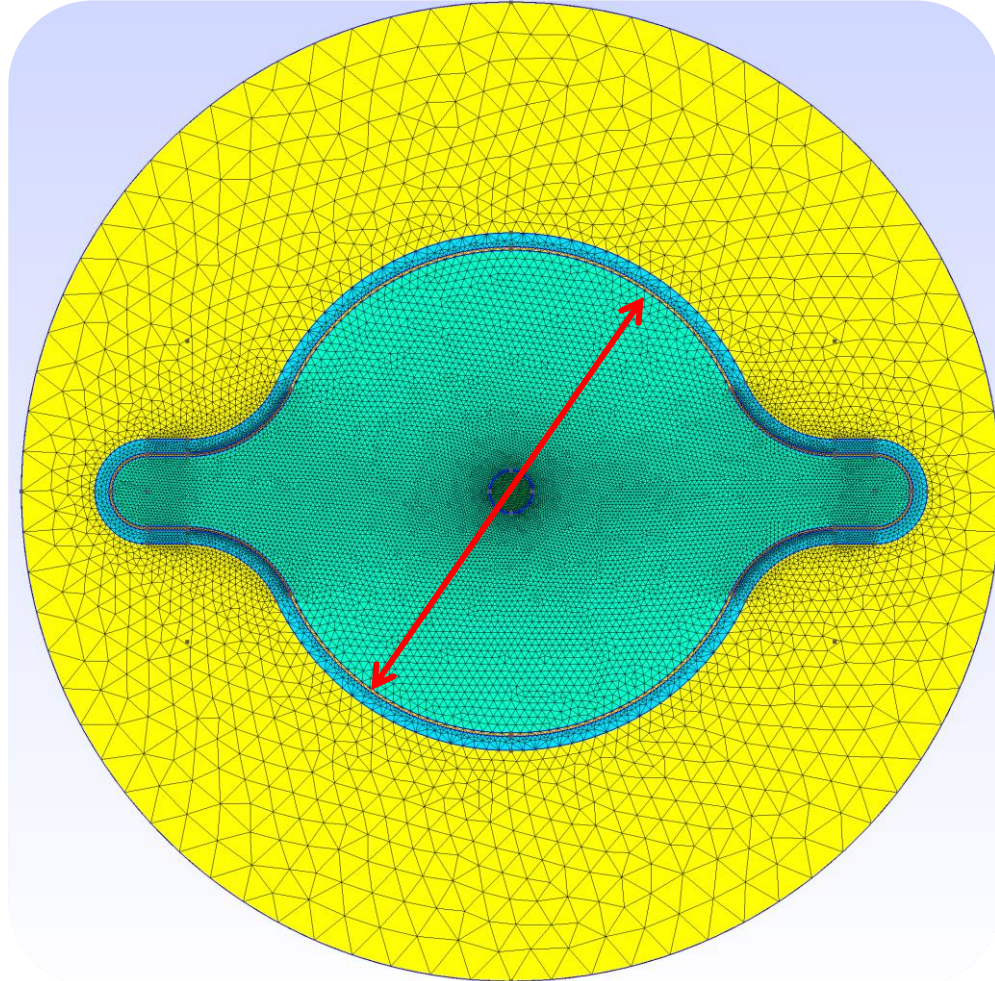
$$W_x = A(z) + x_s W_x^{dip} + x_w W_x^{det}$$



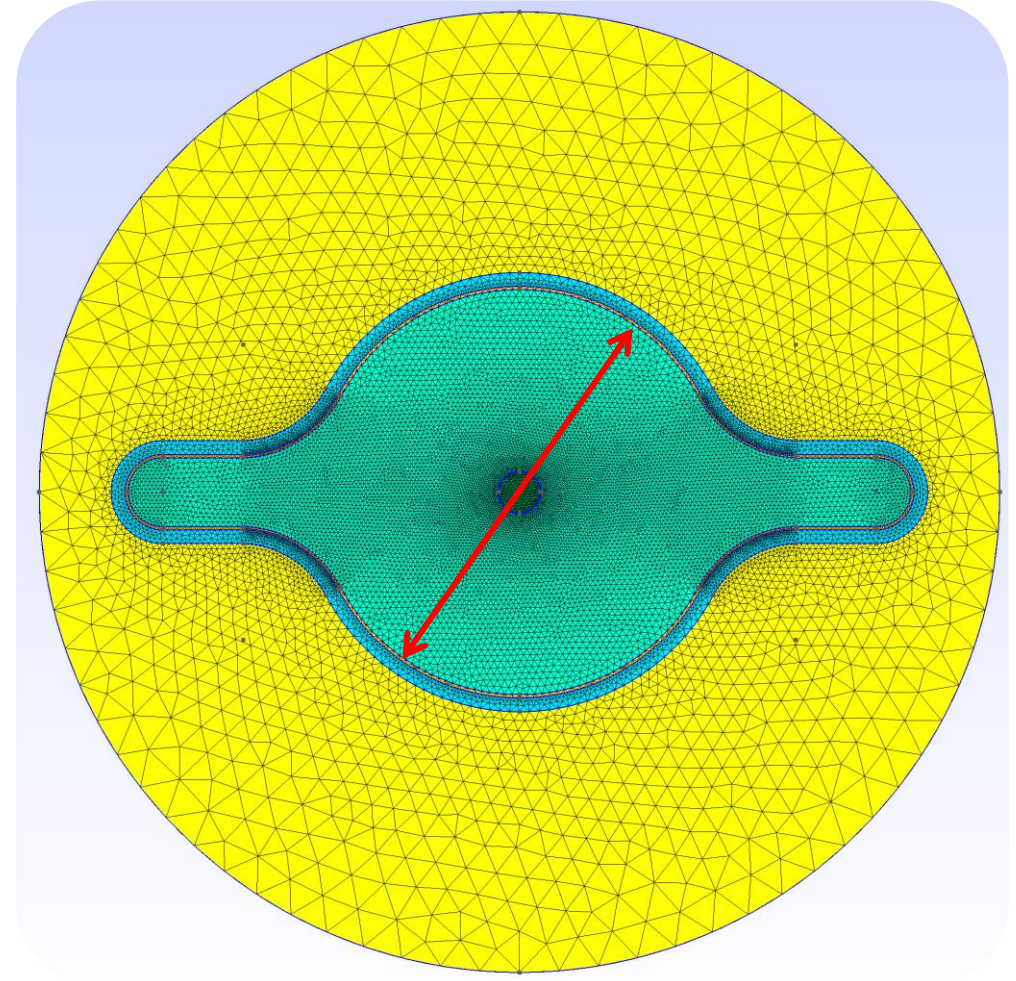
FCC main Ring

Changing Radius

35 mm

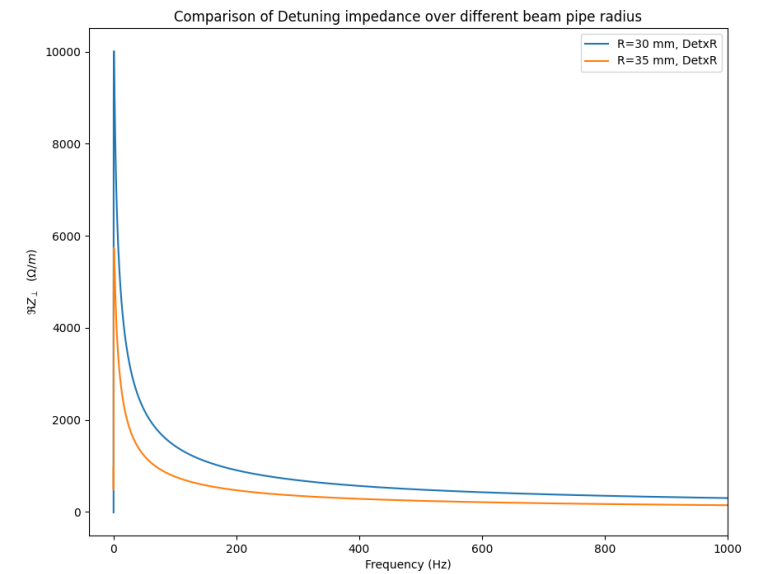
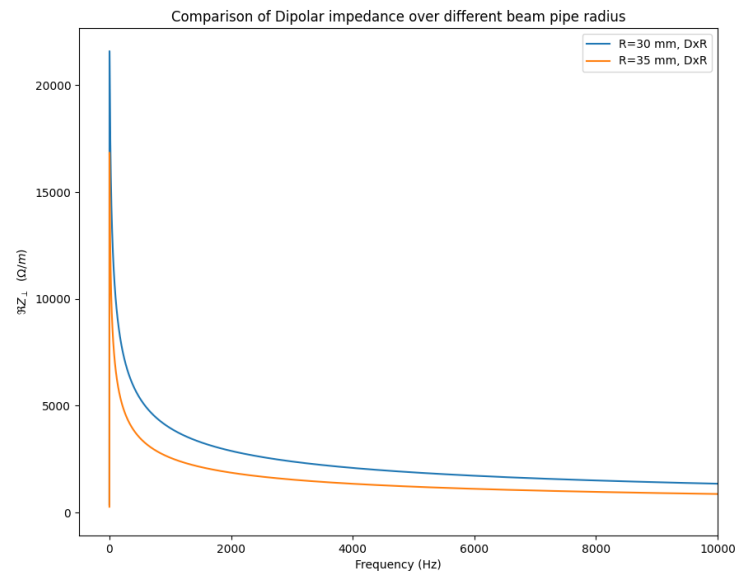
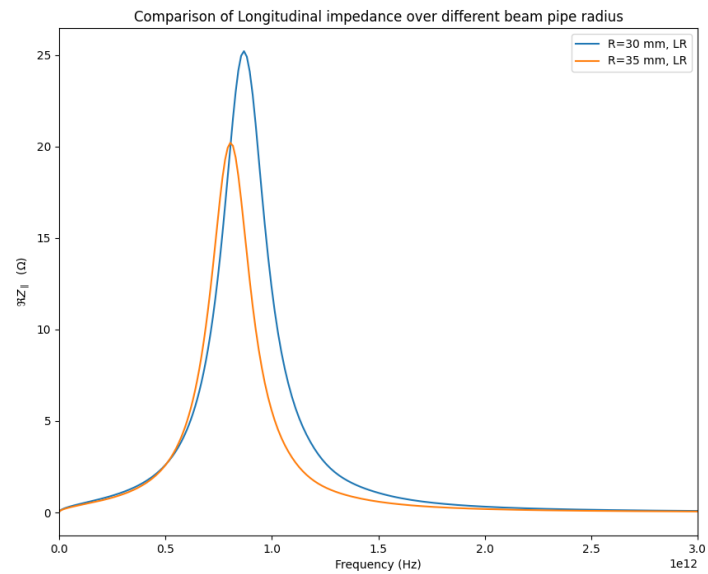


30 mm



FCC main Ring

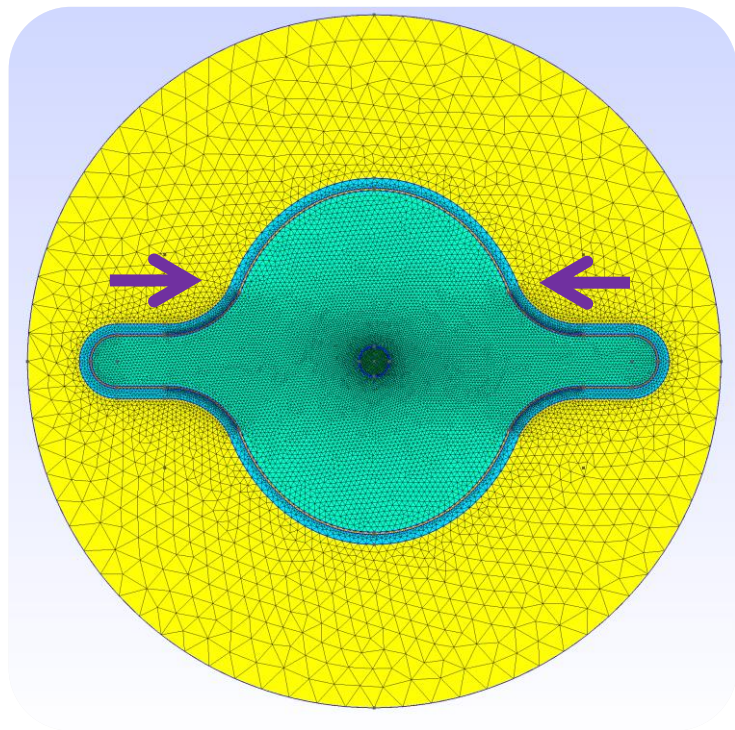
Changing Radius



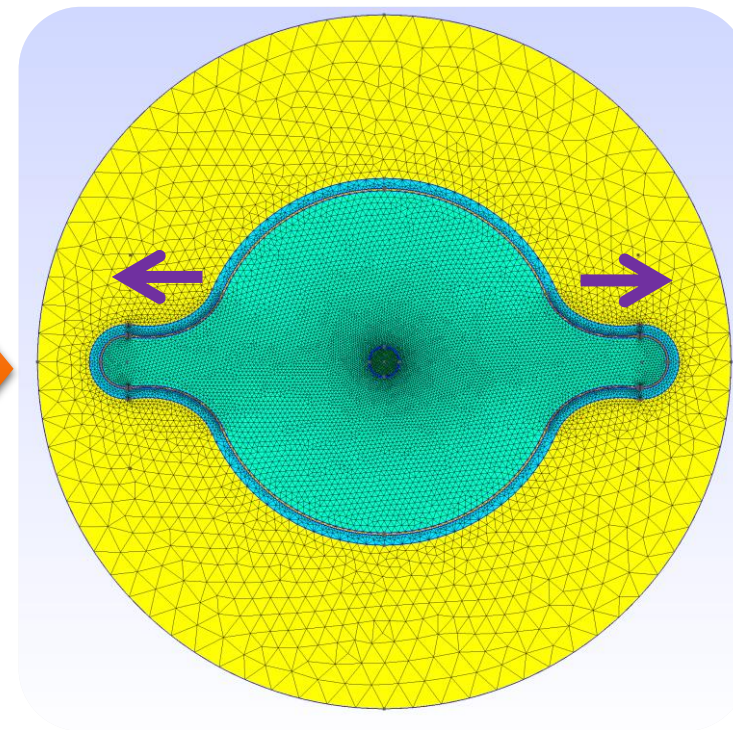
FCC main Ring

Minimizing Detuning impedance

-5 mm

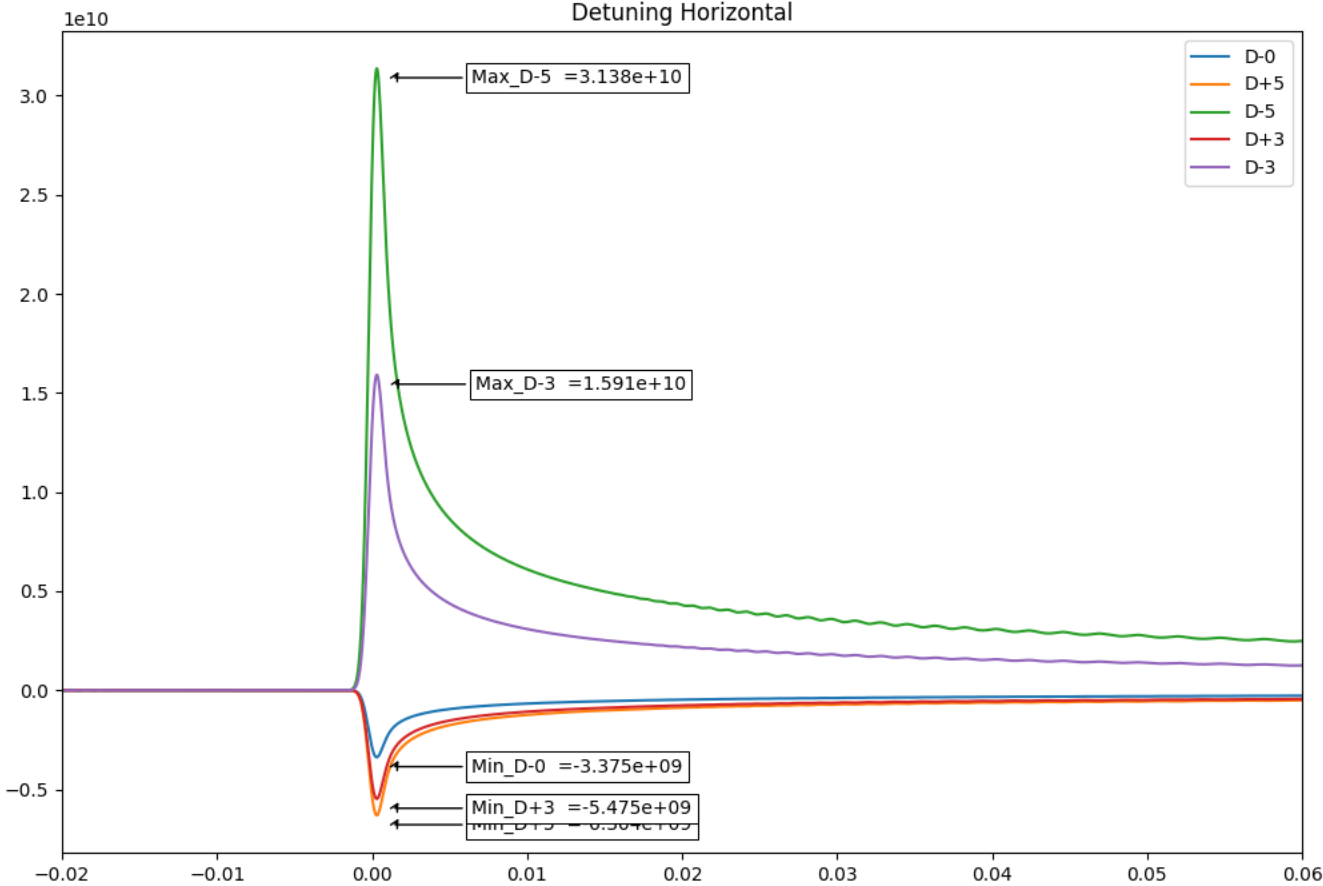


+5 mm



FCC main Ring

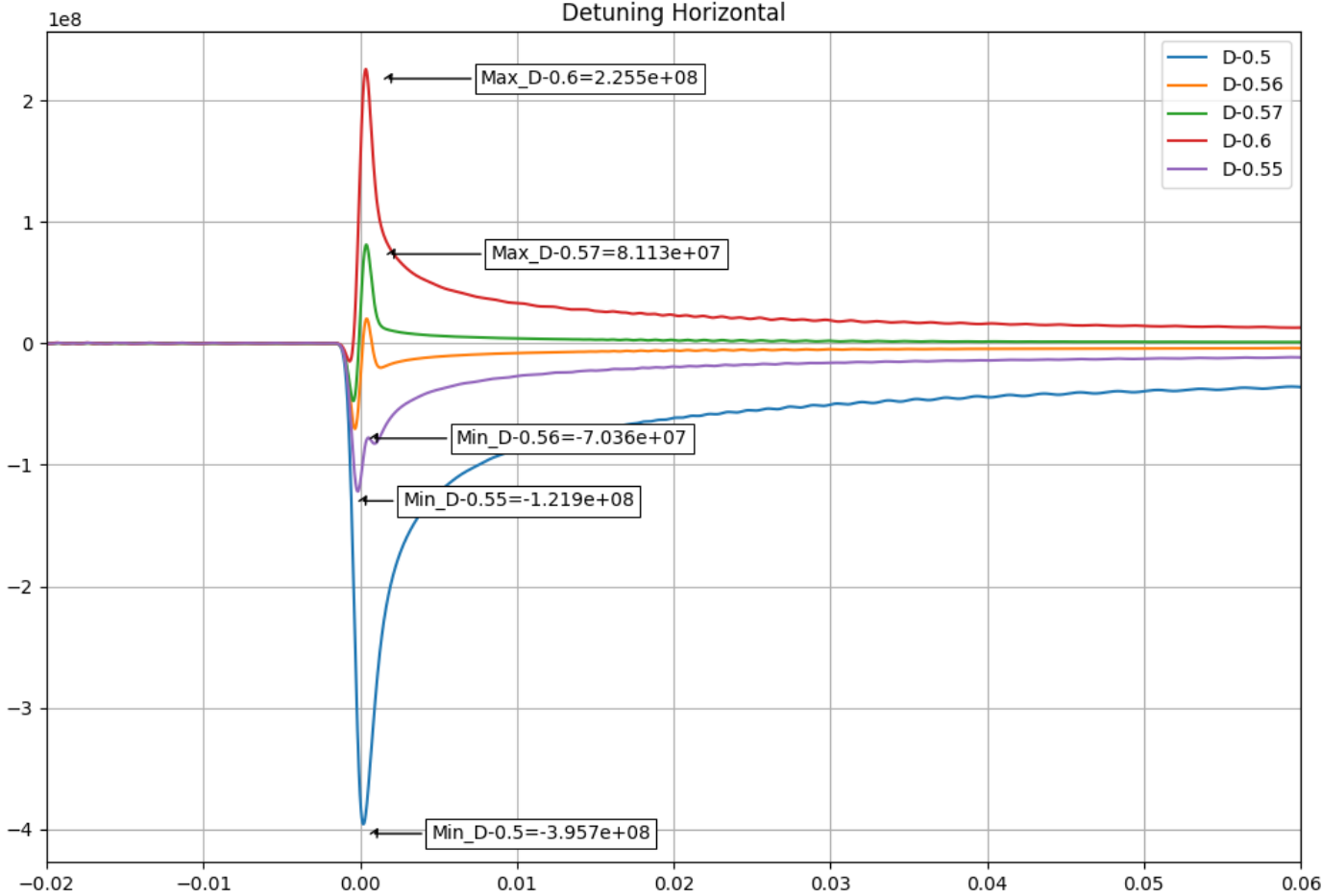
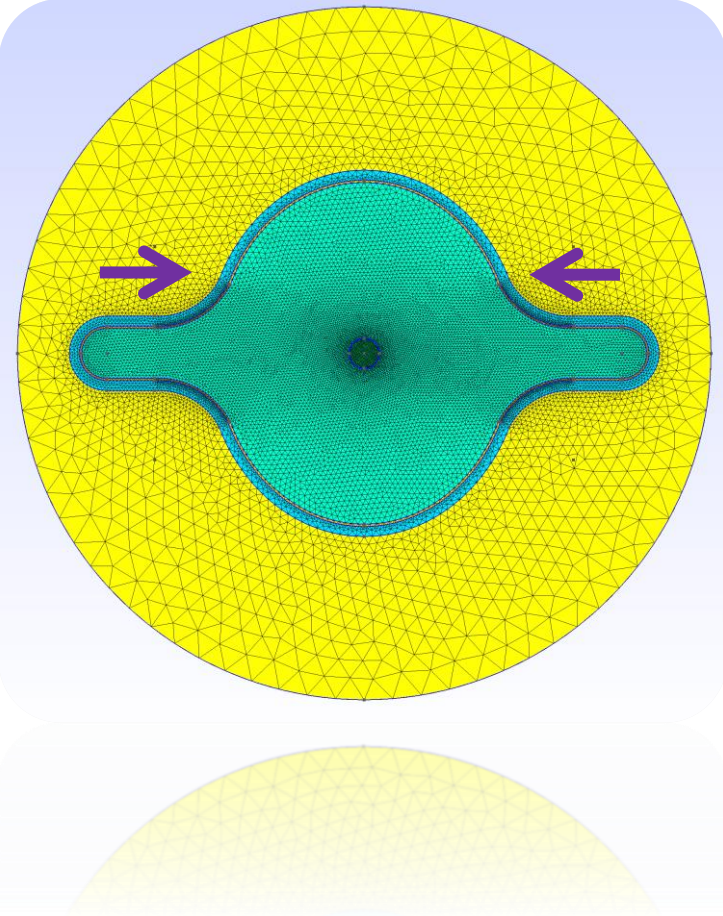
Minimizing Detuning impedance



FCC main Ring

Minimizing Detuning impedance

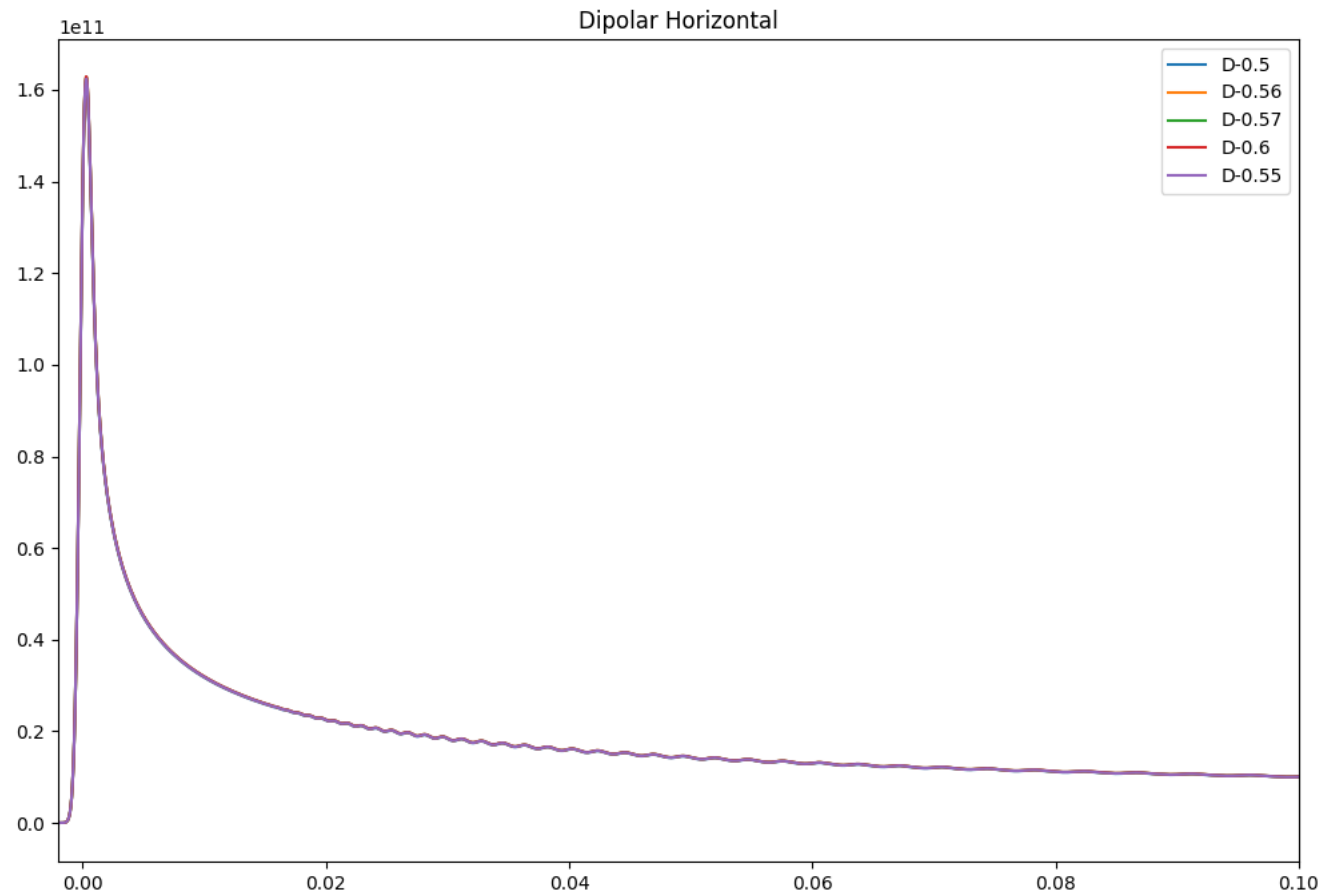
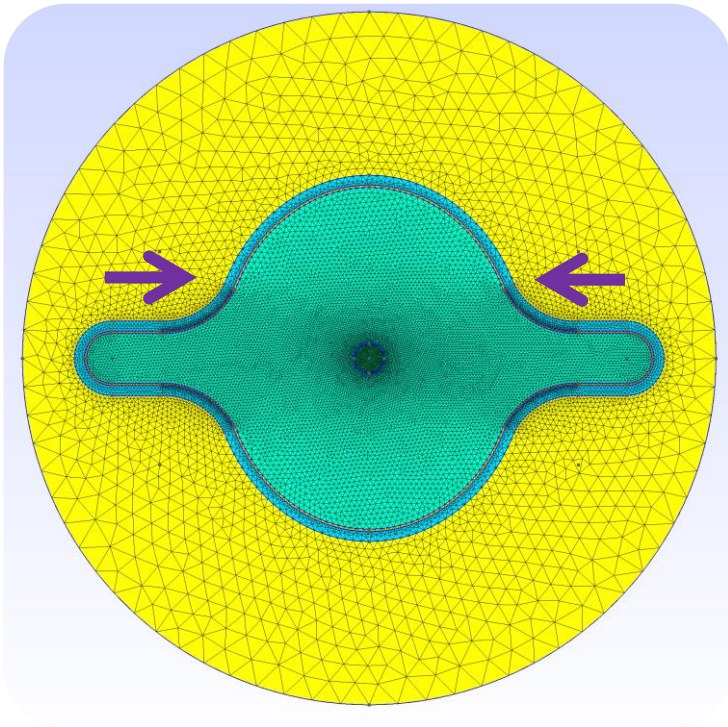
Best ~ 560 – 570 μm (each side)



FCC main Ring

Minimizing Detuning impedance

Best ~ 560 – 570 μm (each side)



FCC Booster Ring

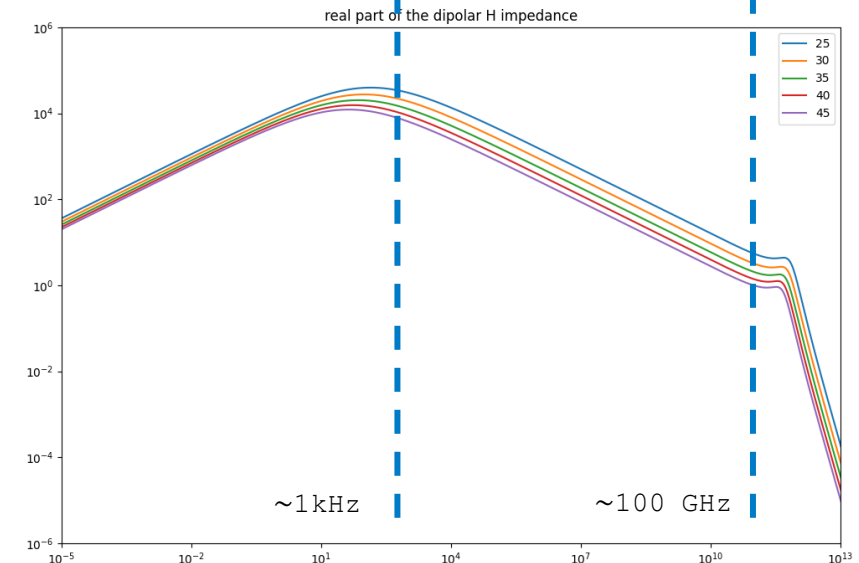
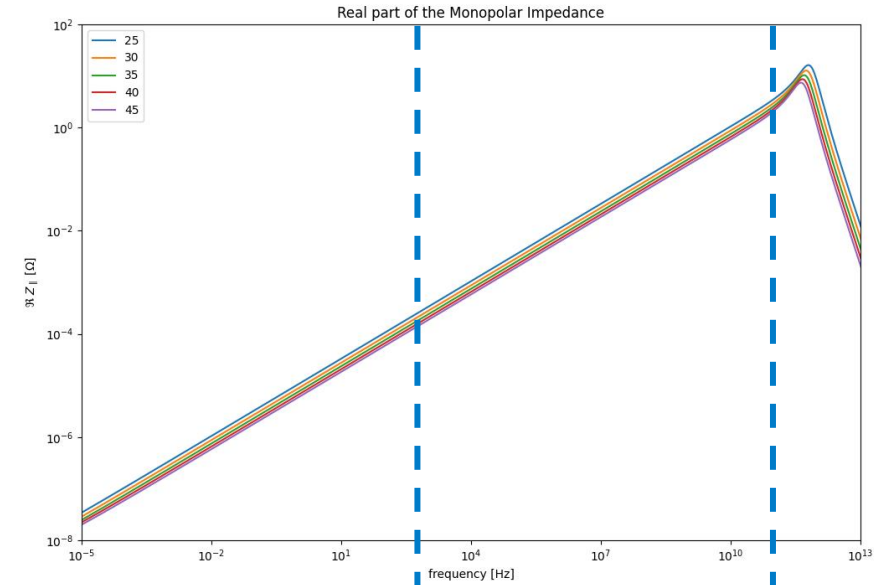
Different Senarios

FCC Booster Ring

Impedance, Stainless Steel, different radius

$$Z_{\parallel}(\omega) \equiv Z_0^{\parallel}(\omega) \approx (1 - i \operatorname{sgn}(\omega)) \frac{L}{2bc} \sqrt{\left(\frac{Z_0 c}{4\pi}\right) \frac{2|\omega|}{\pi\sigma}},$$

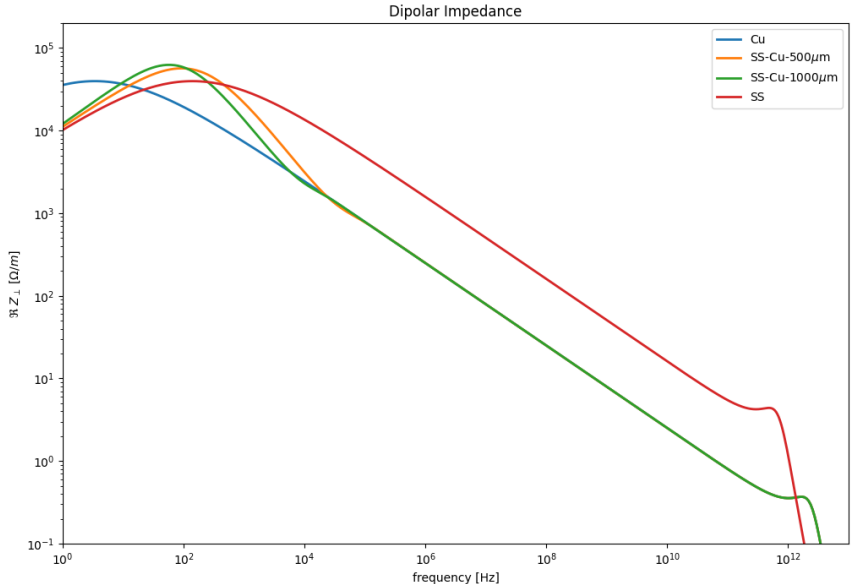
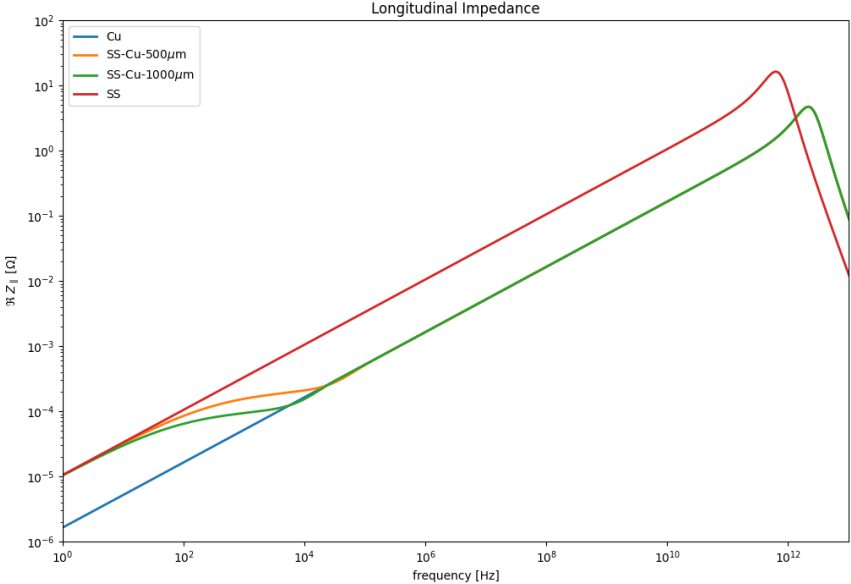
$$Z_{\perp}(\omega) \equiv Z_1^{\perp}(\omega) \approx (1 - i \operatorname{sgn}(\omega)) \frac{c L}{\omega b^3 c} \sqrt{\left(\frac{Z_0 c}{4\pi}\right) \frac{2|\omega|}{\pi\sigma}}.$$



Booster Ring

Different scenarios

- 1. Stainless Steel
- 2. Stainless Steel + 500 μm Copper
- 3. Stainless Steel + 1000 μm Copper
- 4. Copper

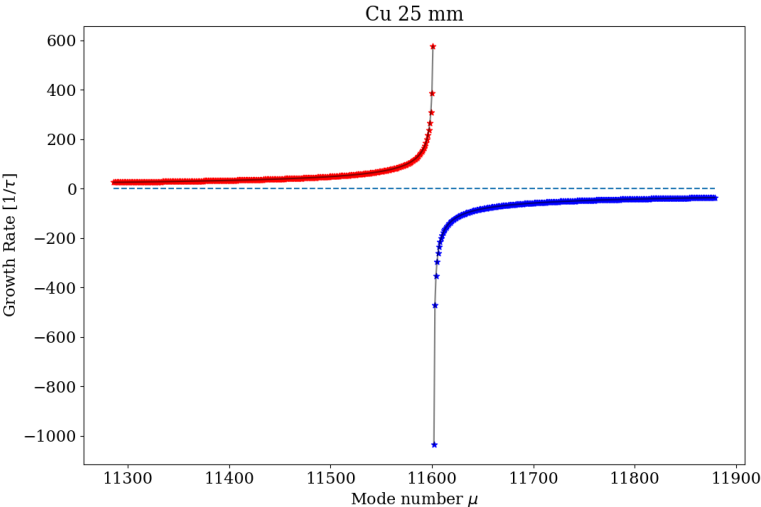


Booster Ring

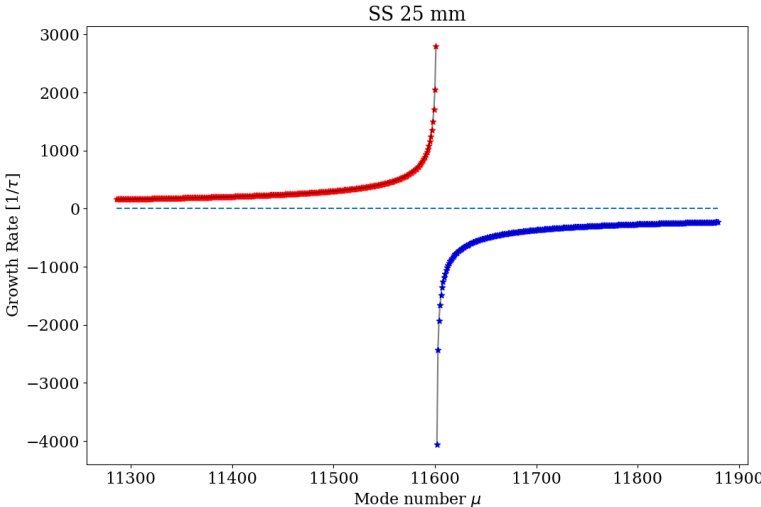
Different scenarios, CBI

Parameters	Value
Intensity	2.14e11
N Bunch	11200
σ_z	5.6 mm
α	28.6 e-6
Q_x	222.2

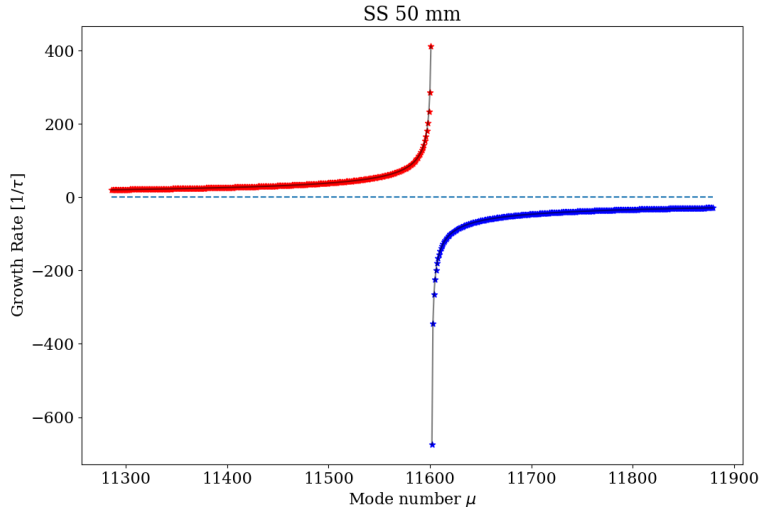
Copper R = 25 mm



Stainless Steel R = 25 mm



Stainless Steel R = 50 mm



Outlooks and Conclusion

A conclusion is the place where you got tired thinking. Martin H. Fischer

- VACI suite is a versatile tool for calculating resistive wall impedance in arbitrary beam pipe cross sections.
- Benchmarked against IW2D, analytical formulas, and Yokoya's code:
 - Demonstrated accuracy and reliability.
- Calculation of resistive wall impedance for the FCC main ring.
 - Omitted detuning impedance.
- Capabilities of VACI suite include:
 1. Impedance calculation
 2. Wakefield analysis
 3. Wake potential computation
 4. Kick and loss factor calculation
 5. Coupled-bunch instability (CBI) analysis
- Results are easily integrated with XSuite.
- VACI suite will be freely available after the publication of my paper. "<https://github.com/alirajabi87/VACI>"

Thank you

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