



Field emission assisted heating of Cs₂Te photocathode: Implication toward mesoscale surface breakdown

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LANL Mentors: Danny Perez, Soumendu Bagchi

MSU Advisor: Sergey Baryshev

CARIE Project team: Evgenya Simakov, Chengkun Huang, etc.

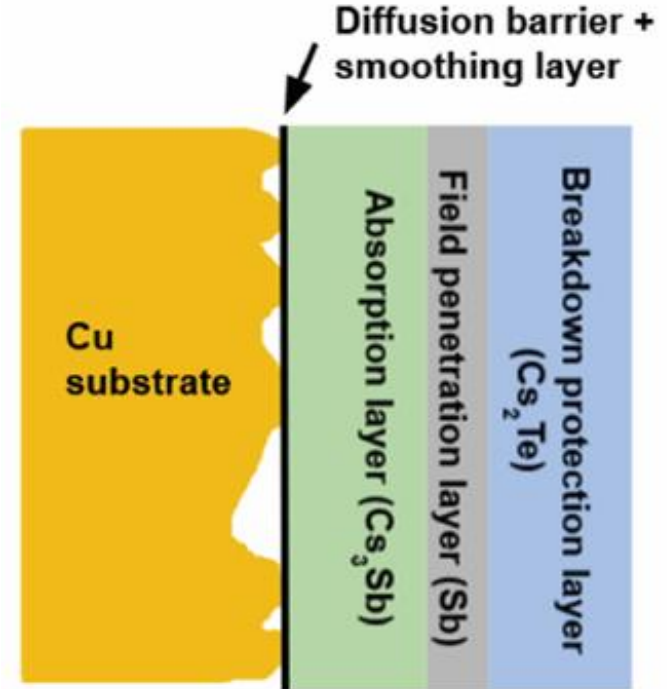
Overview

- **CARIE Project**
 - Theory effort
- Mesoscale Surface Diffusion Model
- Field Emission Modeling
- Result
- Conclusion / Future Work

CARIE: Cathodes And Rf Interactions in Extremes

A new three-year project was funded at LANL to demonstrate operation of high-quantum-efficiency cathodes in a high-gradient RF injector.

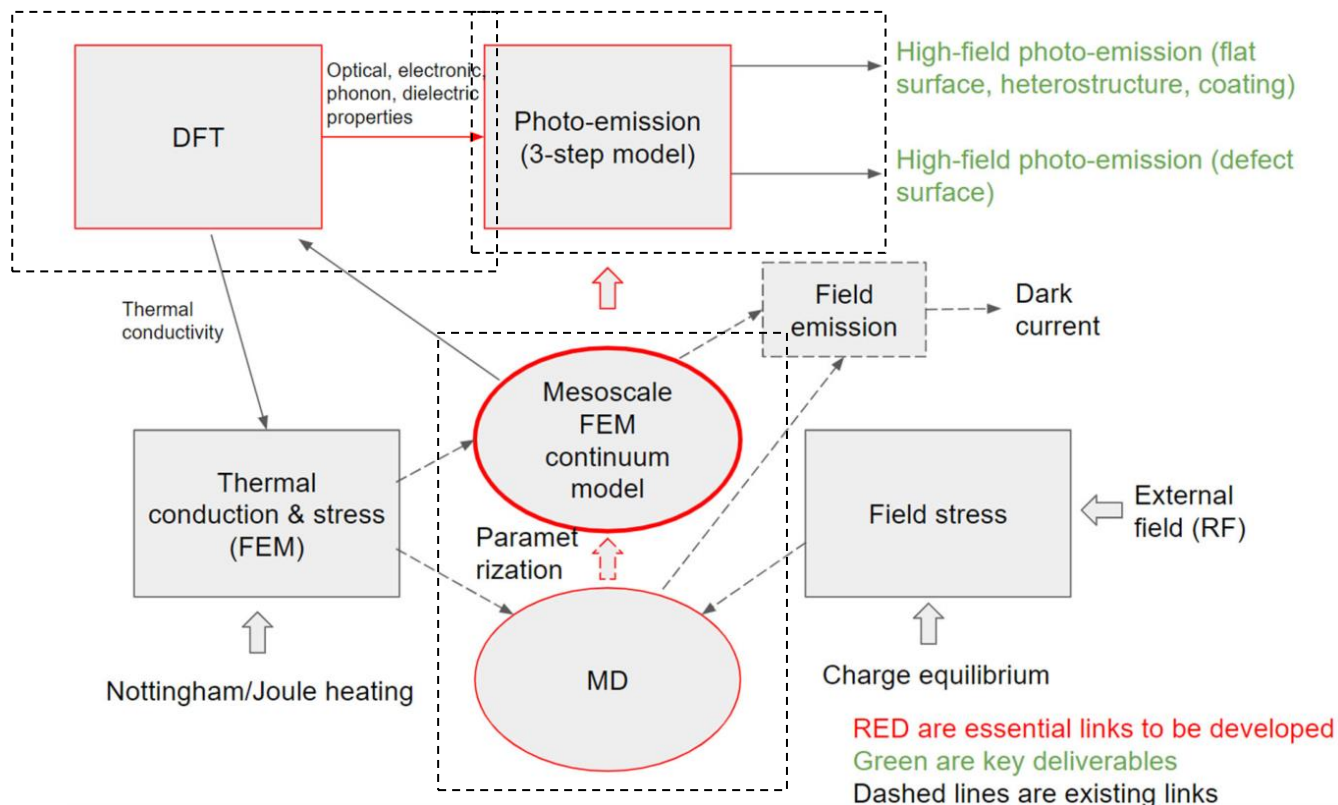
- Project builds upon LANL's expertise in high-gradient C-band and high-QE photocathodes.
- The proposed heterostructured cathode will include multiple layers to ensure atomic flatness of the surface, high QE, and the ability to withstand high electric fields with no breakdown.
- Target beam parameters: 250 pC, 0.1 $\mu\text{m}\cdot\text{rad}$, $B_{5D} = 10^{16} \text{ A/m}^2$.
- The project started in October of 2022.



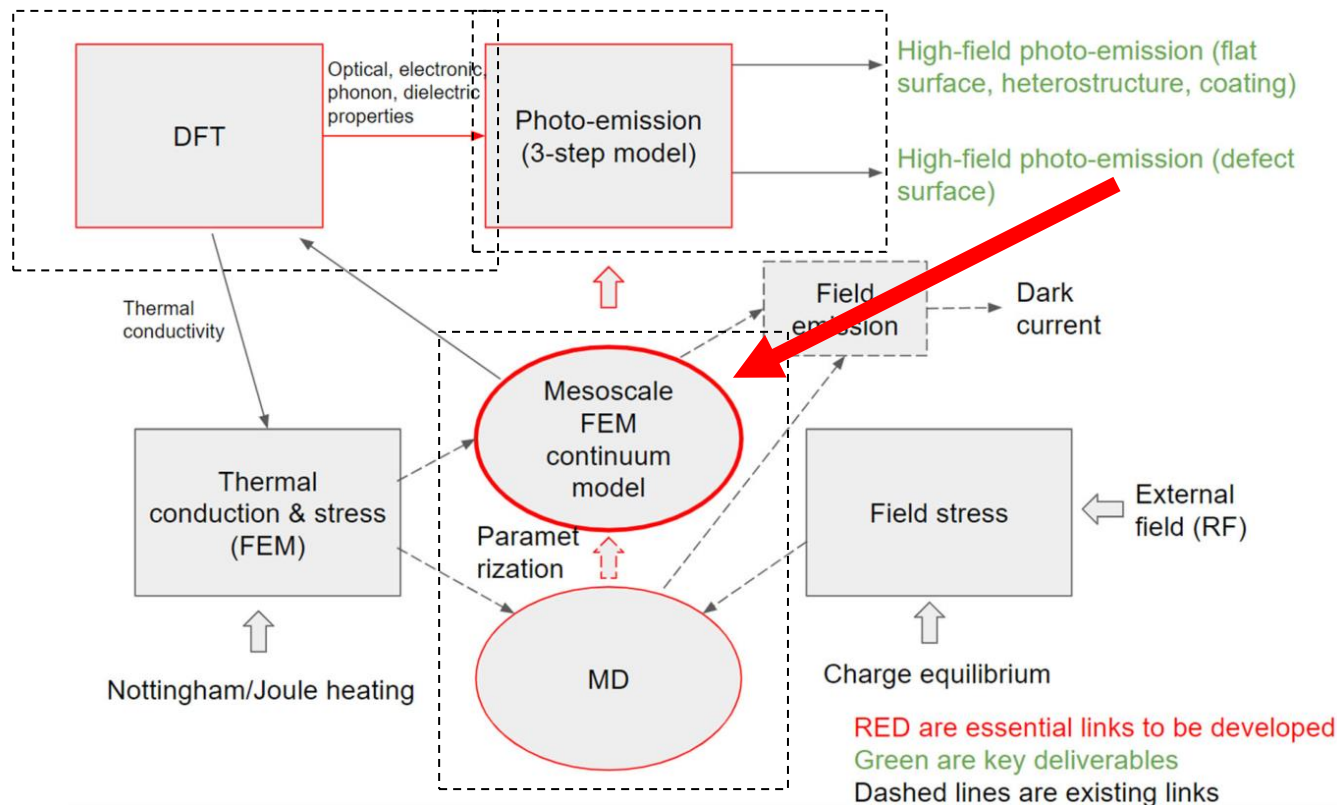
Theory efforts: thrusts and the team

- New photoemission model for thin-film semiconductor cathodes (D. Dimitrov)
- DFT modeling of cathode materials (Cs_2Te and Cs/alkaline antimonides) (G. Wang)
 - Bulk properties (structure, optical, electronic, photon, and atomic potential)
 - Surface properties (work function, electronic properties)
- Monte-Carlo (MC) high-field transport modeling (C. Huang, D. Dimitrov)
- Molecular Dynamics (MD) models for cathode materials (S. Bagchi, D. Perez)
 - Beyond standard charge equilibration approach for high-field operation
 - Data-driven parametrization of interatomic potentials
- **Meso-scale surface breakdown modeling** (S. Bagchi, R. Shinohara - MSU)
- Integration of the nano/meso-scale models

Overview of our models and the integrated modeling approach for semiconductor cathodes



Overview of our models and the integrated modeling approach for semiconductor cathodes

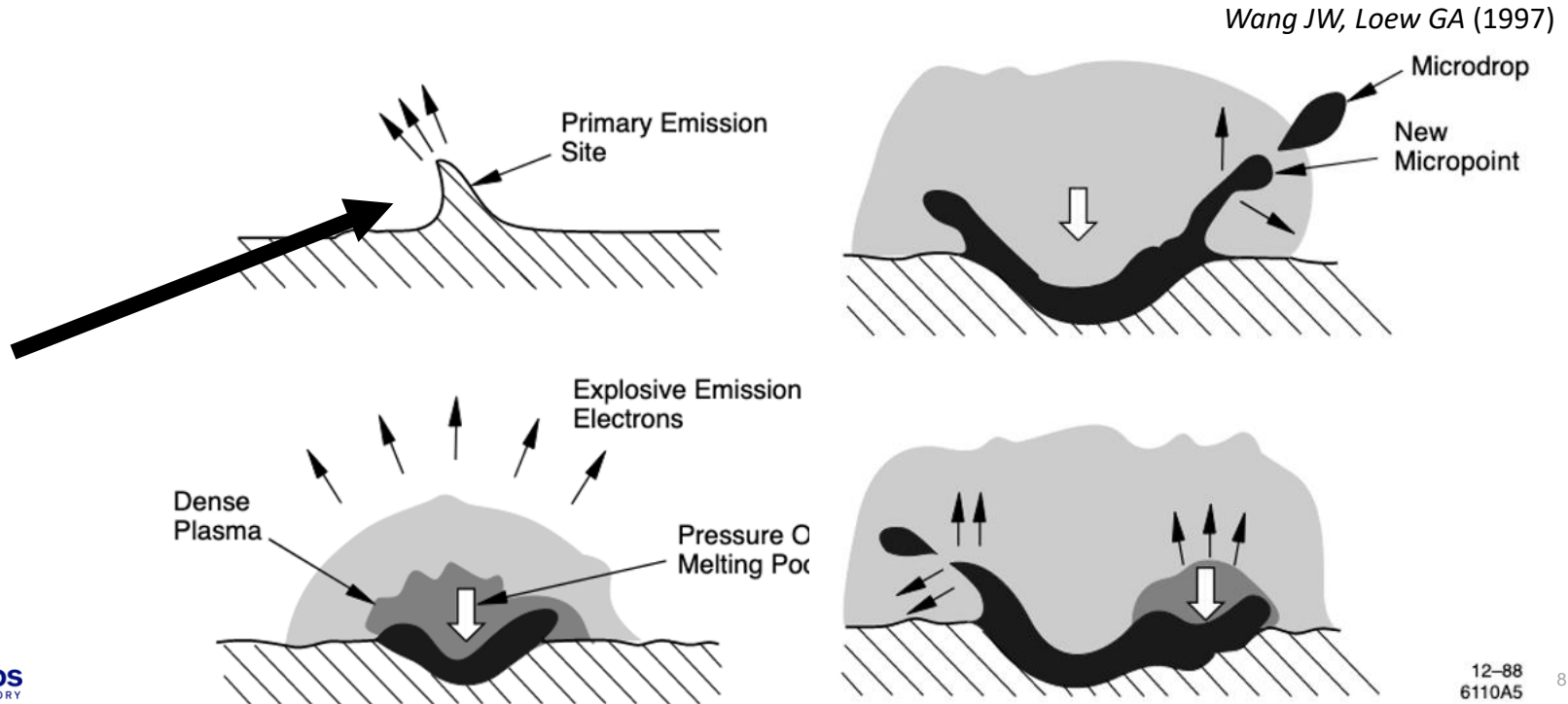


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Breakdown Under High Field Environment

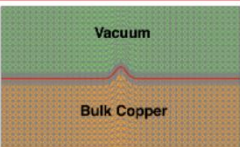
- Triggered from primary emission site



Mesoscale Surface Diffusion Model

1

Finite Element Method



Vacuum
Bulk Copper

1. Local field distribution is solved on the vacuum mesh
2. Linear Thermoelasticity is solved on the copper mesh

2 & 3

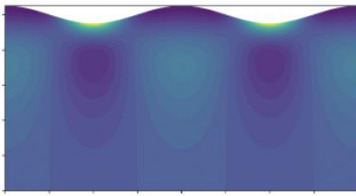
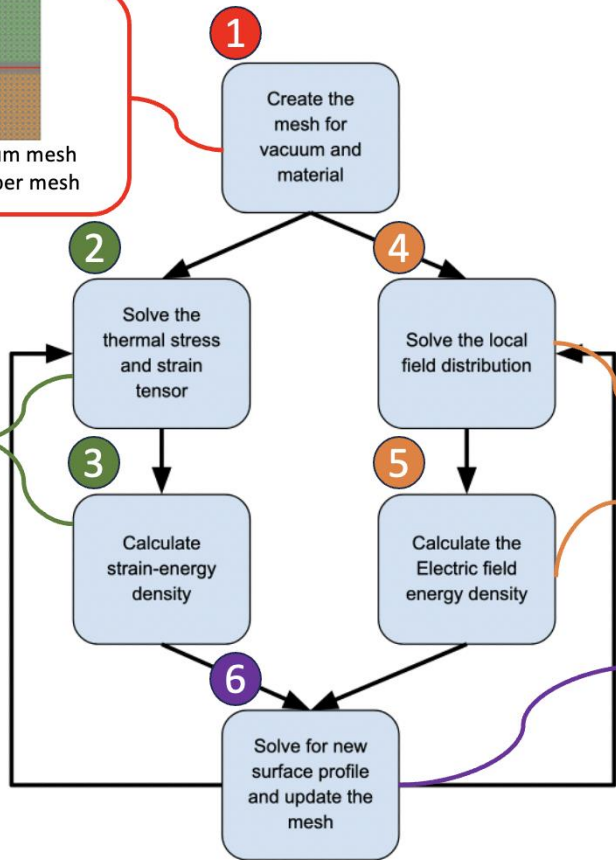
Linear Thermoelasticity

$$-\nabla \cdot \sigma(u) = 0$$

$$\sigma(u) = \lambda \text{tr}(\epsilon(u)) \mathbb{1} + 2\mu \epsilon(u) - \frac{\alpha Y}{1-2\nu} \Delta T \mathbb{1}$$

$$\epsilon(u) = \frac{1}{2} (\nabla u + (\nabla u)^T)$$

Strain-Energy Density

$$\omega_T = \frac{1}{2} \sum_i \sum_j \sigma_{ij} \epsilon_{ij} = \frac{1}{2} (\sigma_{11} \epsilon_{11} + \sigma_{22} \epsilon_{22} + \sigma_{12} \epsilon_{12} + \sigma_{21} \epsilon_{21})$$



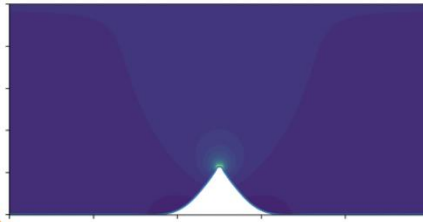
4 & 5

Electrostatic

$$\nabla \cdot (\nabla \phi) = 0$$

$$E = -\nabla \phi$$

Field Energy Density

$$U_E = \frac{1}{2} \epsilon_0 E^2$$


6

Surface Diffusion

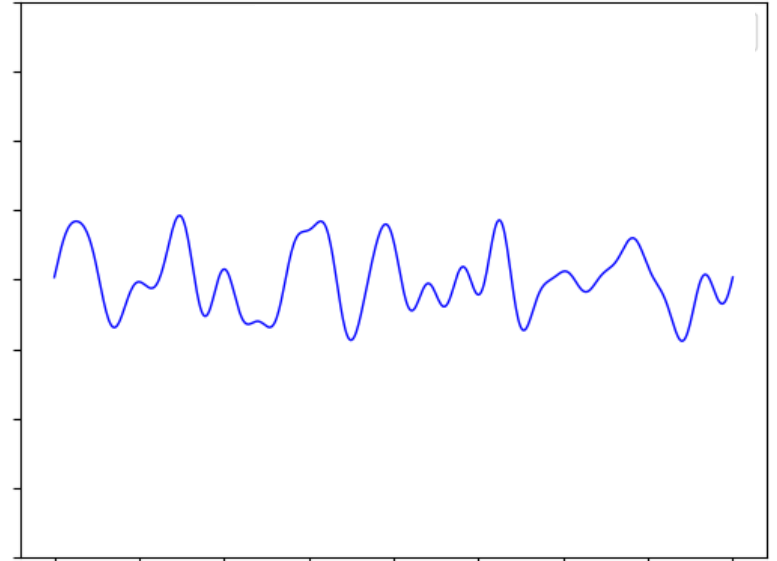
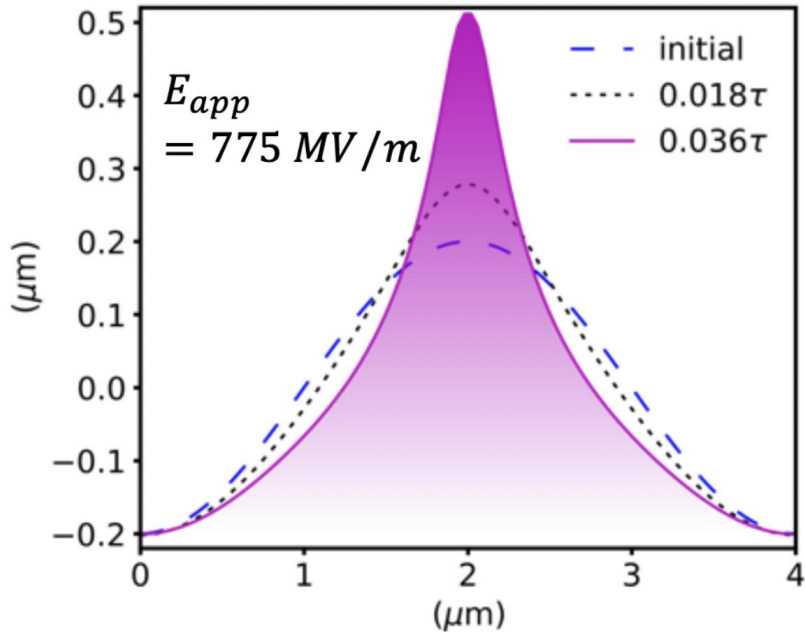
$$V_n = \frac{D_s \Omega v_s}{k_B T} \frac{\partial^2 \mu_c}{\partial s^2}$$

$$\frac{\partial h}{\partial t} = \frac{D_s v_s \Omega}{k_B T} \frac{\partial}{\partial x} \left[(1 + h'_x)^{-1/2} \frac{\partial}{\partial x} (\mu_c) \right]$$

$$\mu_c = \Omega (\gamma k - U_E + \omega_T)$$

Chemical potential = surface tension + electrostatic energy + strain energy density

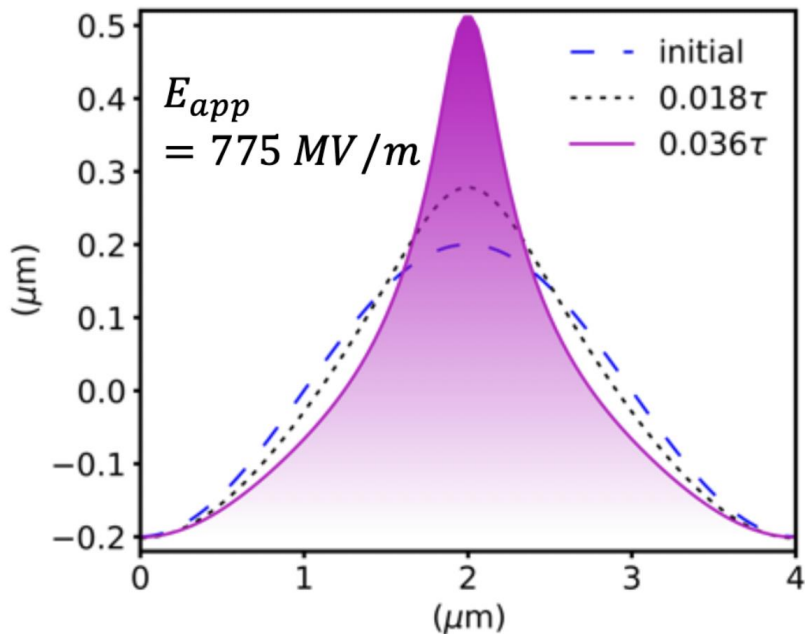
Mesoscale surface diffusion model



<https://arxiv.org/pdf/2311.06624.pdf>

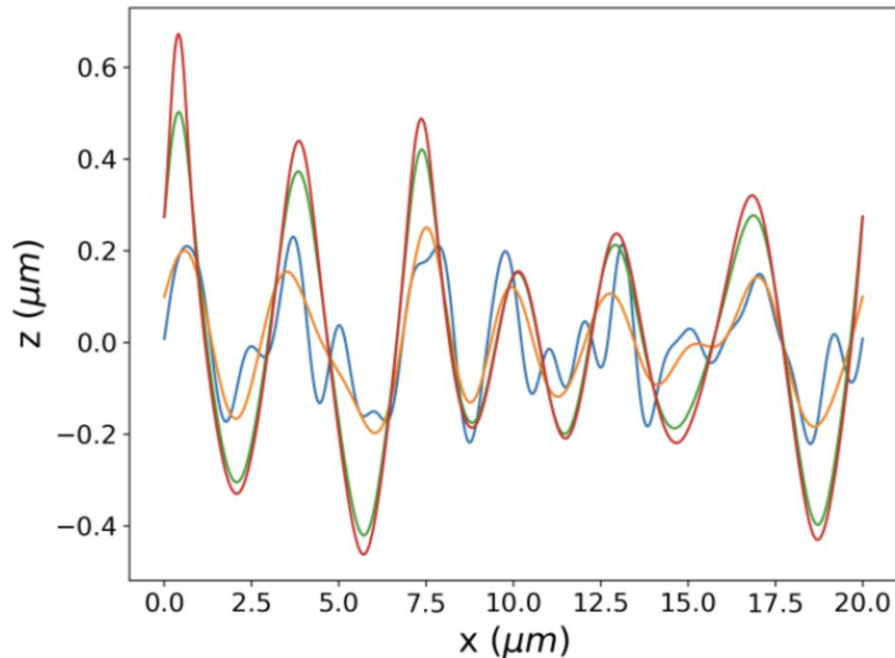
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Overview

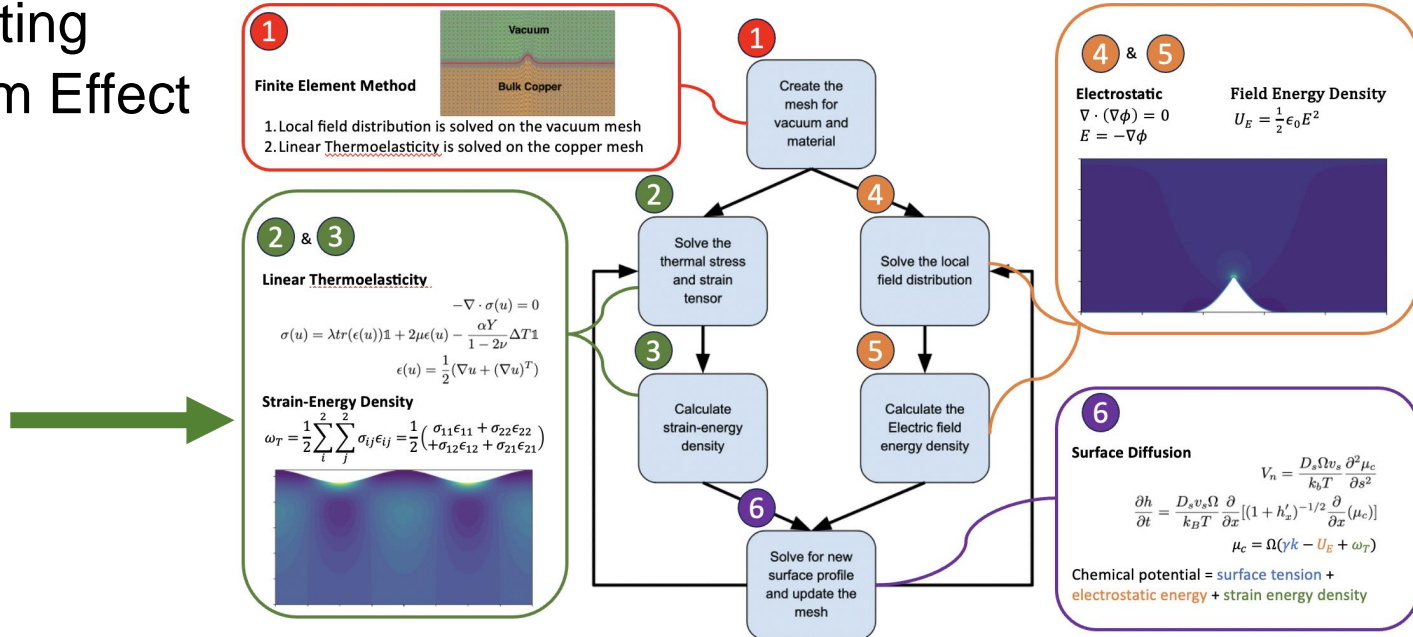
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Semiconductor Breakdown: Field Emission

- Field Emission

- Source → Current Density

- Joule Heating
- Nottingham Effect



Field Emission Current & Heating

- Field Emission Calculated through Fowler-Nordheim equation

$$- J_{FN} = 1.54 * 10^6 * 10^{4.53\phi^{-0.5}} [E_{local}]^2 \text{Exp}\left(\frac{-6.53*10^9*\phi^{1.5}}{E_{local}}\right)$$

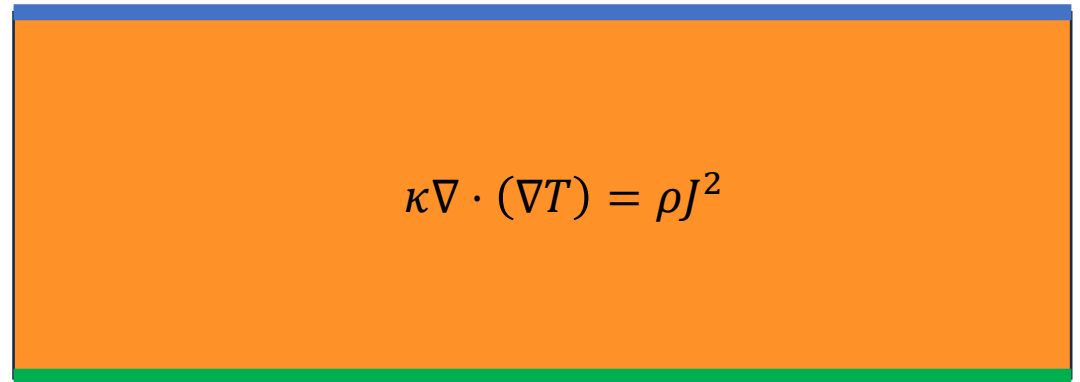
- Joule heating:

$$- \frac{\partial T}{\partial t} = \rho J_{bulk}^2$$

- Nottingham Heating:

$$- \nabla T \cdot \vec{n} = \frac{J_{FN} \Delta U_e}{q_e \kappa}$$

$$\nabla T = \frac{J_{FN} \Delta U_e}{q_e \kappa} \text{ at } \partial\Omega_V$$

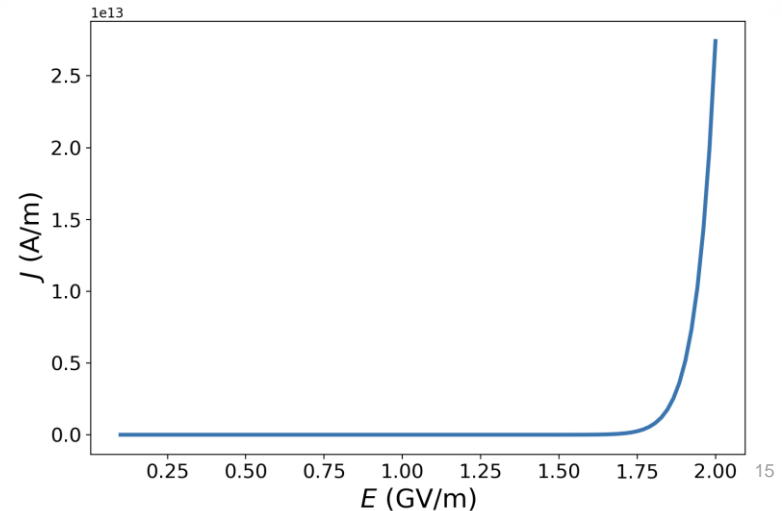
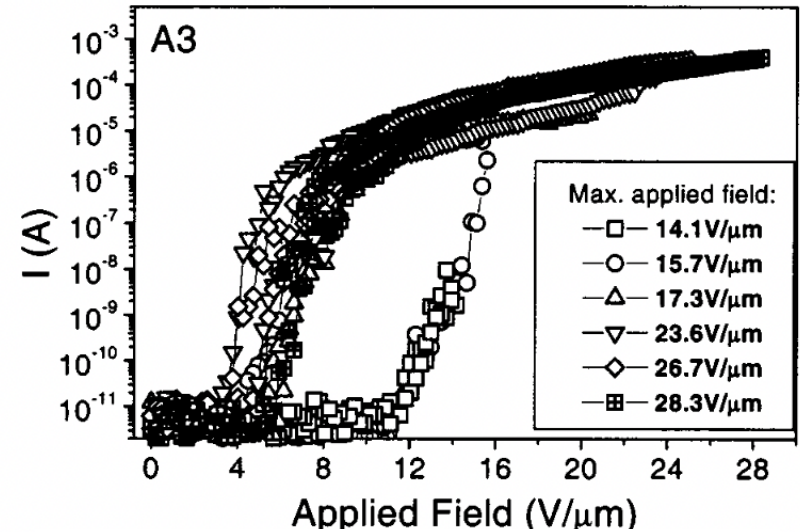


$$\kappa \nabla \cdot (\nabla T) = \rho J^2$$

$$T = 300 \text{ K at } \partial\Omega_C$$

Deviation from FN equation for semiconductor

- Current-density Saturation in semiconductor
- Strong Deviation from classical FN equation in high-field regime
 - $1.54 * 10^6 * 10^{4.53\phi^{-0.5}} [E_{local}]^2 Exp(-\frac{6.53*10^9*\phi^{1.5}}{E_{local}})$
 - FN equation predicts that current increases exponentially with surface field

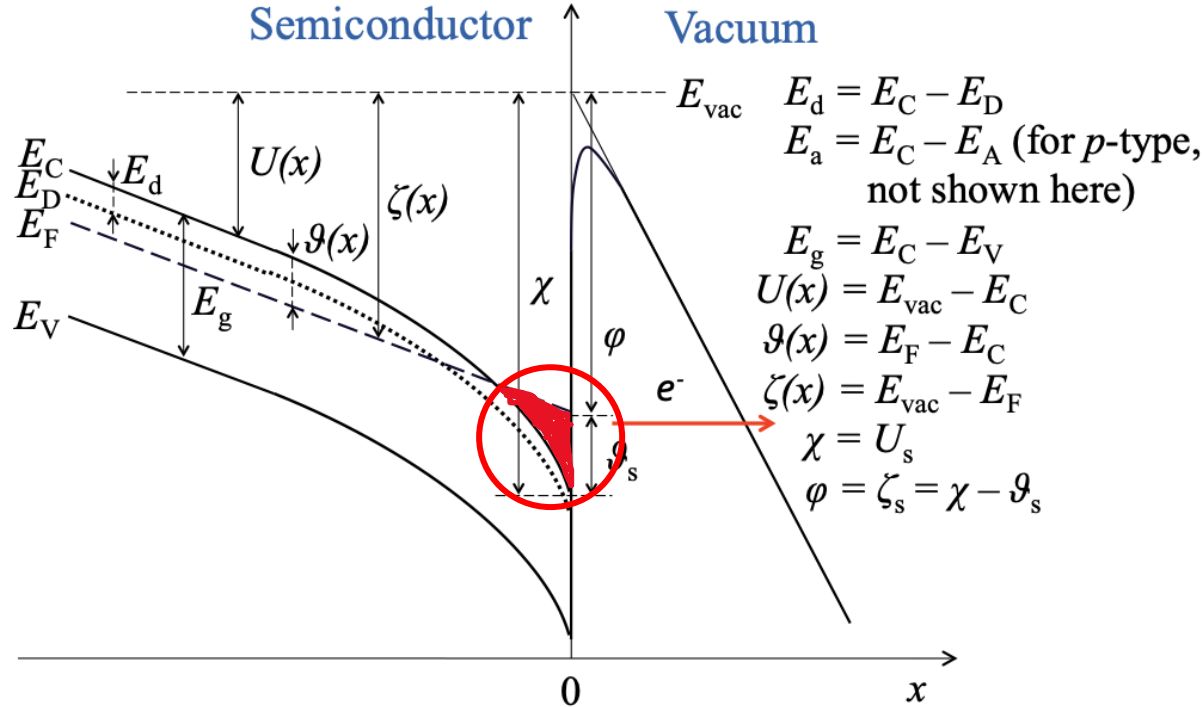


Un-physical results with FN equation

- Temperature Rise per Applied Field for Joule Heating:
 - 100MV/m: $\sim 0^{\circ}K$
 - 125MV/m $\sim 0^{\circ}K$
 - **150MV/m: $\sim 12^{\circ}K$**
 - **175MV/m: $\sim 14000^{\circ}K$**
- Temperature Rise per Applied Field for Nottingham
 - 50MV/m: $\sim 0^{\circ}K$
 - 55MV/m $\sim 1^{\circ}K$
 - **60MV/m: $\sim 180^{\circ}K$**
 - **65MV/m: $\sim 16000^{\circ}K$**

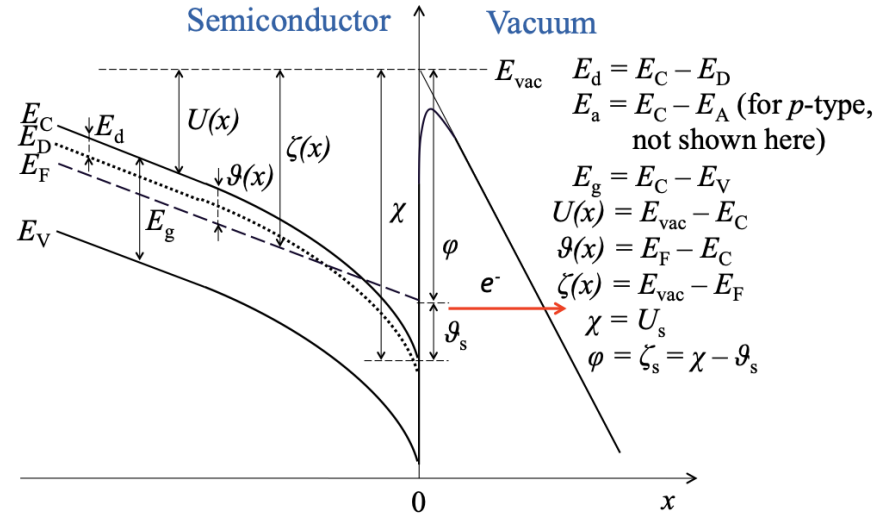
**Unrealistic
Temperature Spike**

Stratton-Baskin-Lvov-Fursey Formalism, Oksana Chubenko



Stratton-Baskin-Lvov-Fursey Formalism, Oksana Chubenko

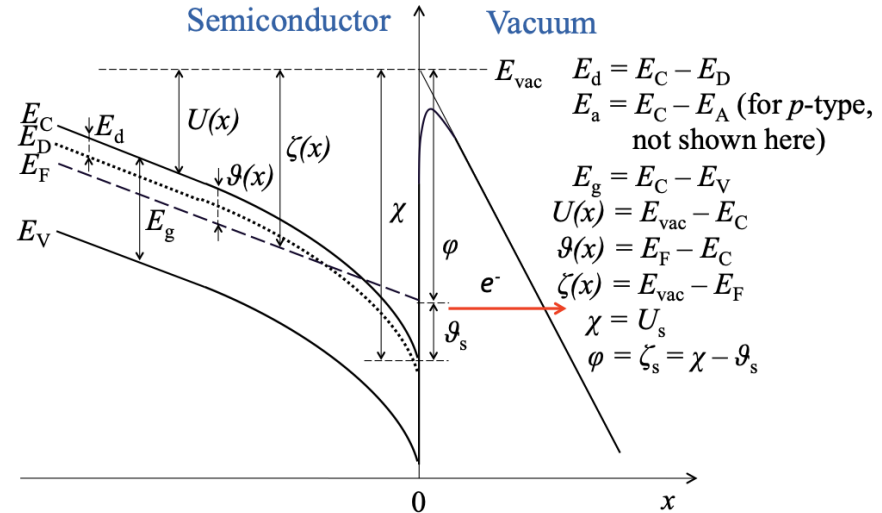
- **Low-field Regime**
 - Limited by tunneling probability
 - → Act metal like (follows FN)
- **High-field Regime (saturation)**
 - Limited by electron supply in the space-charge (band-bending) region
- Formalism takes into account the band-bending



Journal of Applied Physics **125**, 205303 (2019); <https://doi.org/10.1063/1.5085679>

Stratton-Baskin-Lvov-Fursey Formalism, Oksana Chubenko

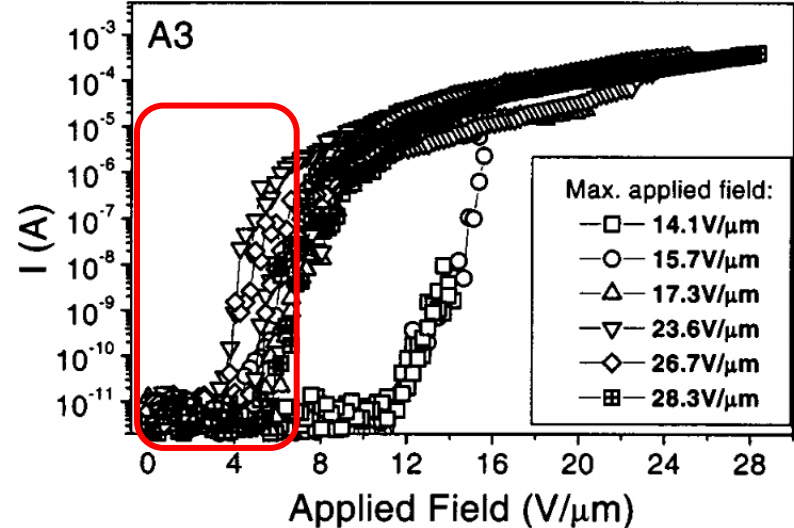
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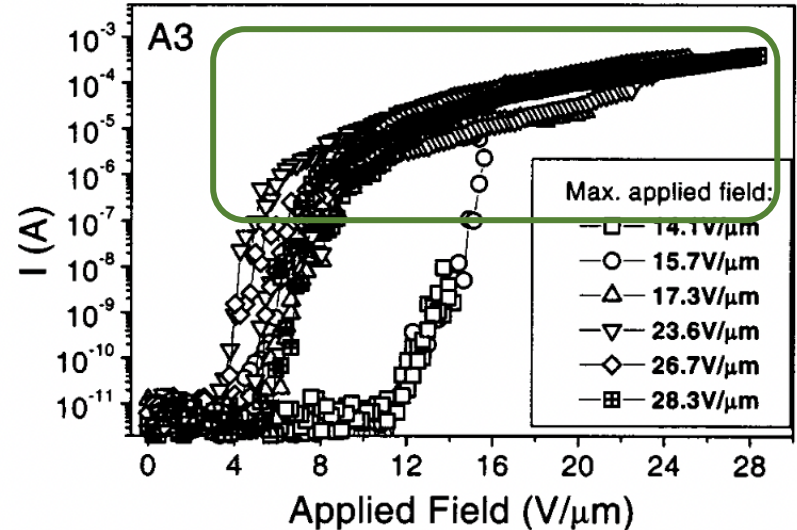
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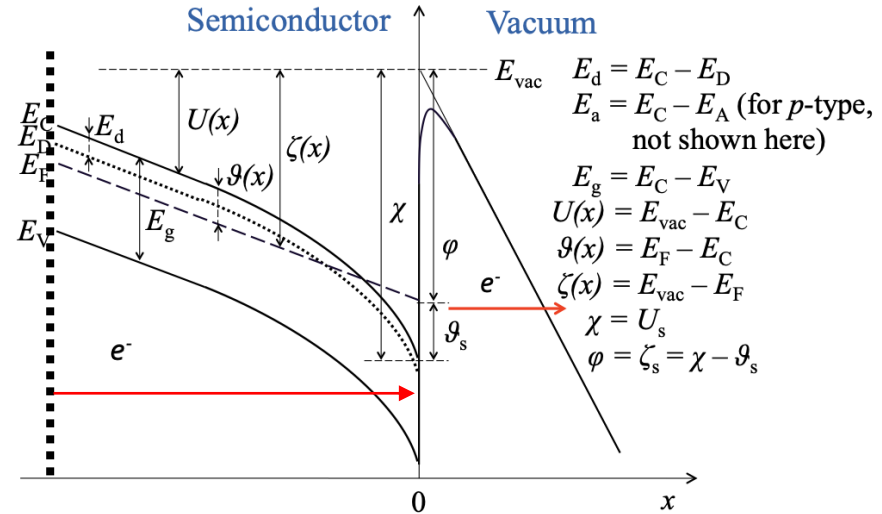
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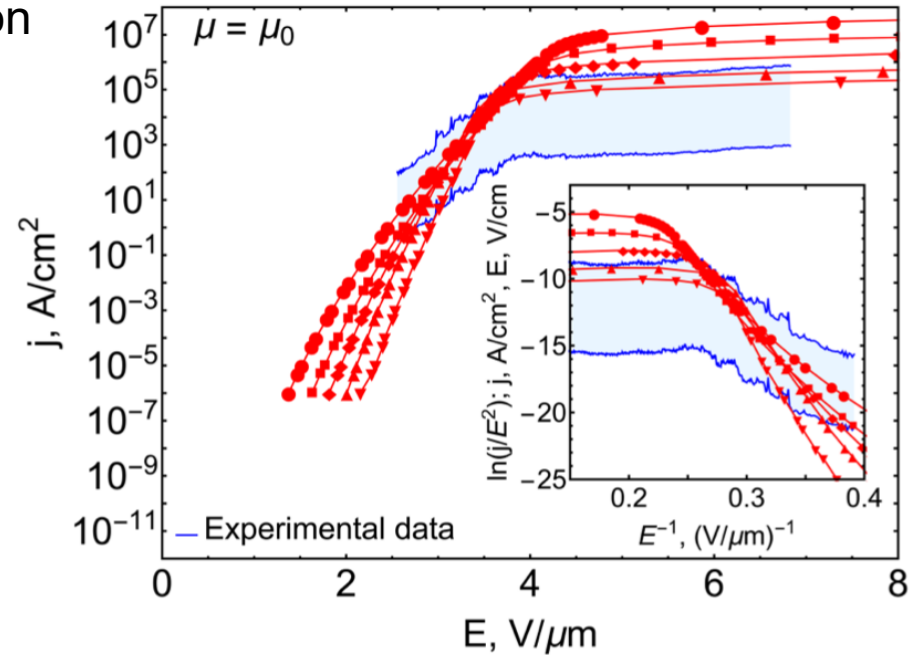
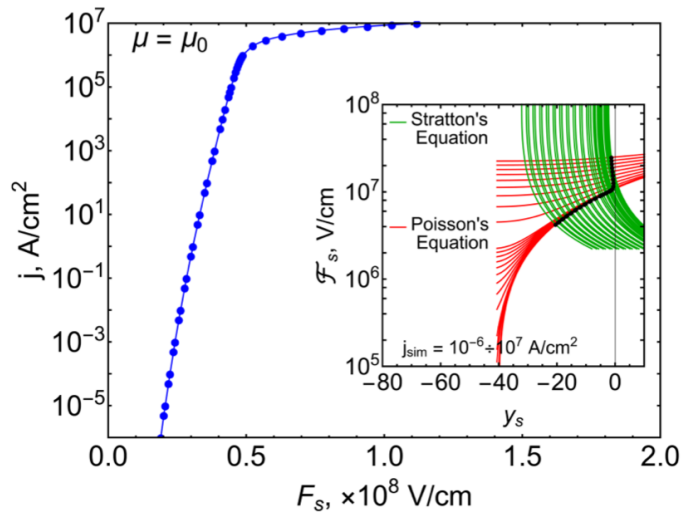
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Stratton-Baskin-Lvov-Fursey Formalism

- Find the simultaneous solution of the Poisson equation and Stratton's equation
- Oksana Chubenko studied (N)UNCD



Poisson Equation

- Solve

$$-\frac{d^2V}{dx^2} = -\frac{\rho}{\kappa\epsilon_0}, \rho = -q(n - p + N_a^- - N_d^+)$$

Concentration
Densities

$$\left\{ \begin{array}{l} n = N_C F_{1/2}[(E_F - E_C)/k_B T], \\ p = N_V F_{1/2}[(E_V - E_F)/k_B T], \\ N_a^- = \frac{N_a}{1 + 2 \exp[(E_A - E_F)/k_B T]}, \\ N_d^+ = \frac{N_d}{1 + 2 \exp[(E_F - E_D)/k_B T]}, \end{array} \right.$$

$$y(x) \equiv \frac{\mathcal{V}(x)}{k_B T} = \frac{E_F - E_C}{k_B T}.$$

$$\left\{ \begin{array}{l} n(y) = N_C F_{1/2}(y), \\ p(y) = N_V F_{1/2}(-E_g/k_B T - y), \\ N_a^-(y) = \frac{N_a}{1 + 2 \exp(-E_a/k_B T - y)}, \\ N_d^+(y) = \frac{N_d}{1 + 2 \exp(E_d/k_B T + y)}. \end{array} \right.$$

Stratton's Equation

- $$j_{\text{em}}^-(F_s, y_s) = A_1 \exp\left[-B_1 \frac{\chi^{3/2}}{F_s} \nu(Y_1)\right] \exp(y_s)$$
- $$\times \left[1 - C_1 \frac{\chi^{1/2}}{F_s} t(Y_1) k_B T\right]^{-1},$$
- $$j_{\text{em}}^+(F_s, y_s) = \frac{A_2}{t^2(Y_2)} \frac{F_s^2}{\varphi(y_s)} \exp\left[-B_1 \frac{\varphi^{3/2}(y_s)}{F_s} \nu(Y_2)\right]$$

$$\times \left\{1 - \exp\left[-B_2 \frac{\varphi^{1/2}(y_s)}{F_s} y_s t(Y_2)\right]\right.$$

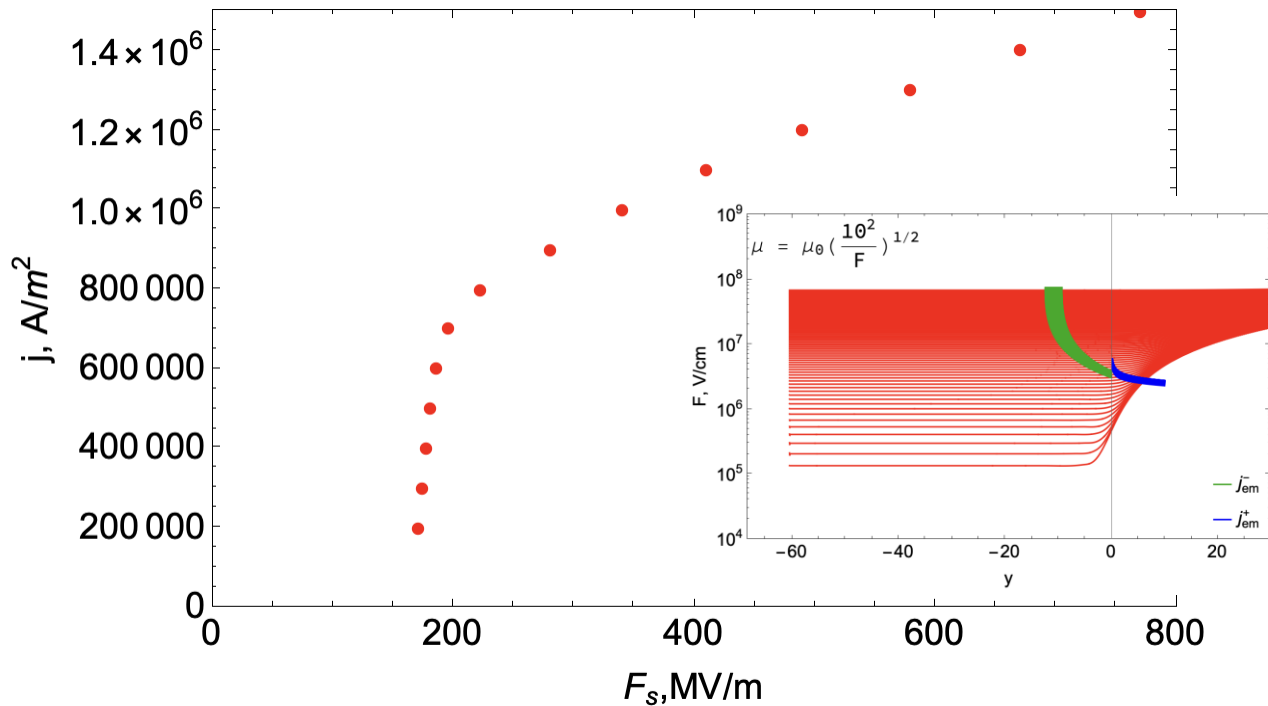
$$\left. \times \left[1 + B_2 \frac{\varphi^{1/2}(y_s)}{F_s} y_s t(Y_2)\right]\right\},$$

Parameters	Expression
A_1	$4\pi m_0 q (k_B T)^2 / h^3$
B_1	$8\pi \sqrt{2m_0} / (3qh)$
C_1	$4\pi \sqrt{2m_0} / (qh)$
A_2	$q^3 / (8\pi h)$
B_2	$4\pi \sqrt{2m_0} k_B T / (qh)$

Overview

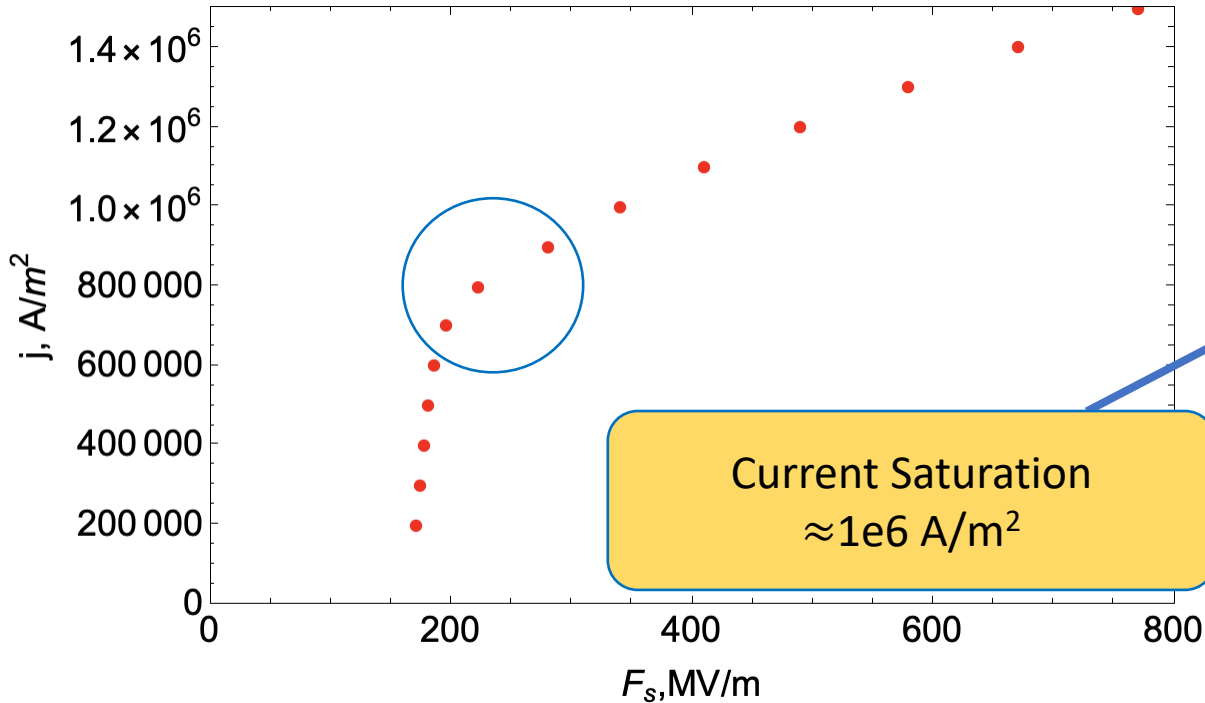
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Current vs Field: Current Saturation



MV / m	A/m ²
171.522	200 000.
174.772	300 000.
177.454	400 000.
180.912	500 000.
185.53	600 000.
195.323	700 000.
222.762	800 000.
280.	900 000.
340.	$1. \times 10^6$
410.	1.1×10^6
490.	1.2×10^6
580.	1.3×10^6
670.	1.4×10^6
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880.	1.6×10^6
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Current vs Field: Current Saturation



Current Saturation
 $\approx 1e6 \text{ A/m}^2$

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Simple heating test with the solved current

- 50nm thin coat
- Solving for **Stationary Heat Equation**

- $\kappa \nabla \cdot (\nabla T) = f$

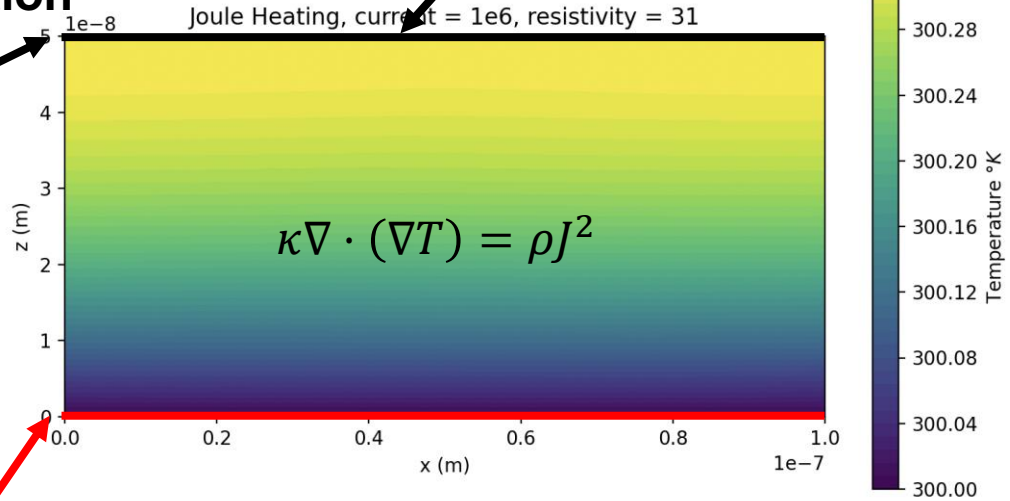
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- Nottingham Heating:

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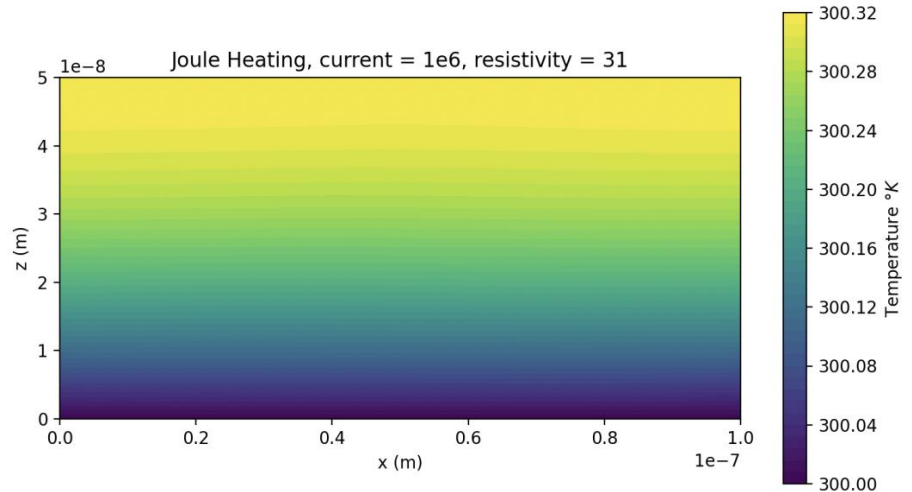
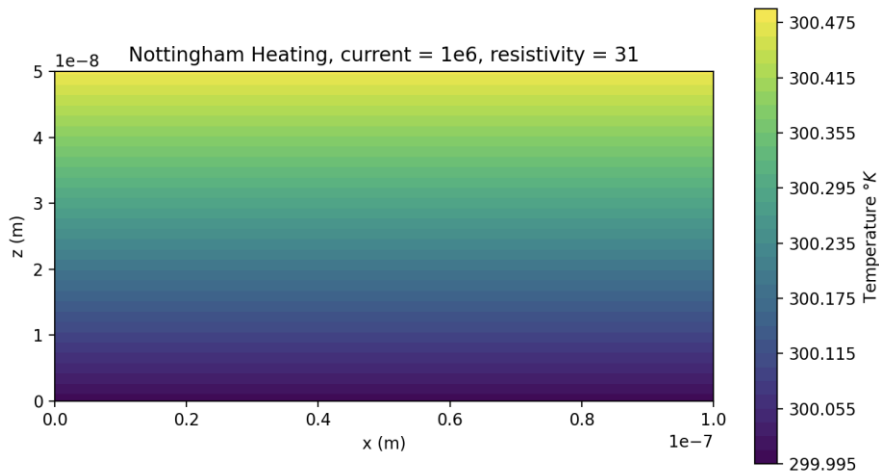
- $f = \nabla \cdot (\kappa \Delta T)$



Copper semiconductor boundary: $T = 300 \text{ K}$ on $\partial\Omega_C$

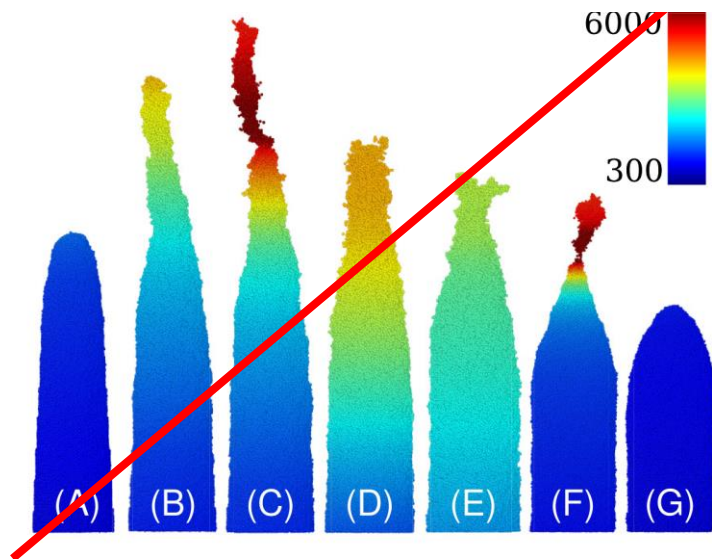
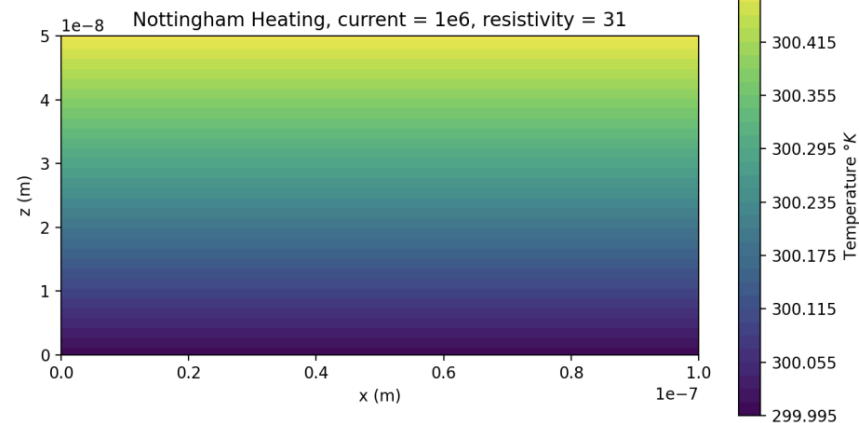
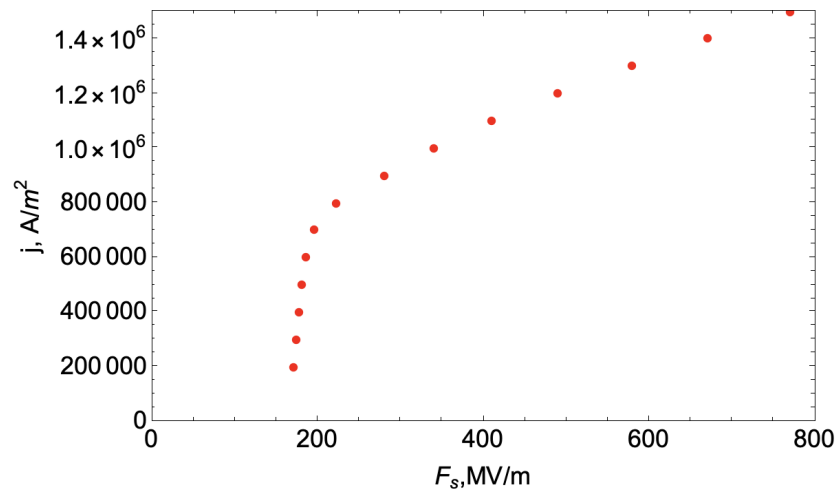
Heating: max ΔT

- Joule Heating ΔT : 0.32 K
- Nottingham Effect ΔT : 0.47 K



Conclusion

- Current Saturation
- Insufficient current for meaningful heating to take place
 - Max ΔT of 0.8 K
- Thermal Runaway will (likely) to not take place

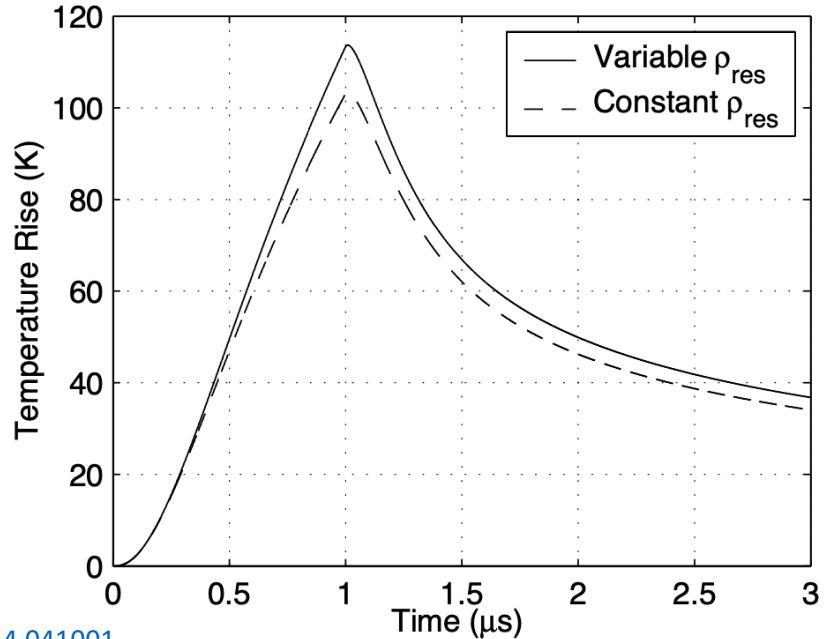
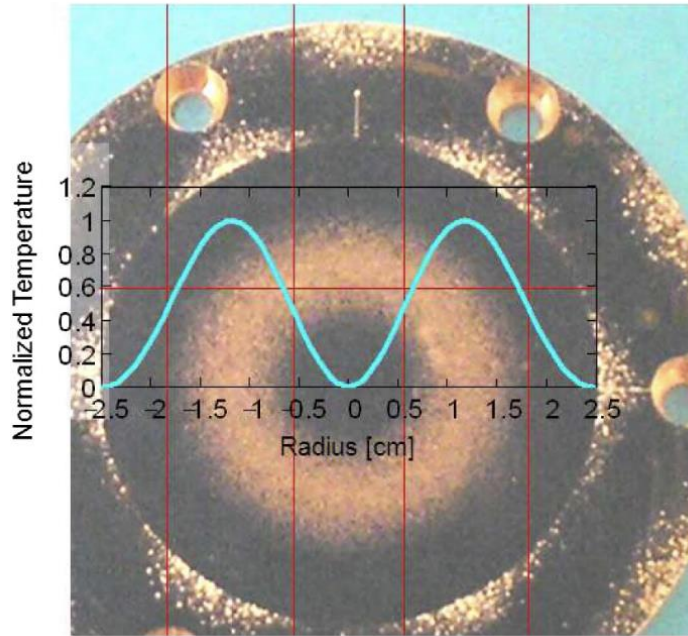


Moving Forward

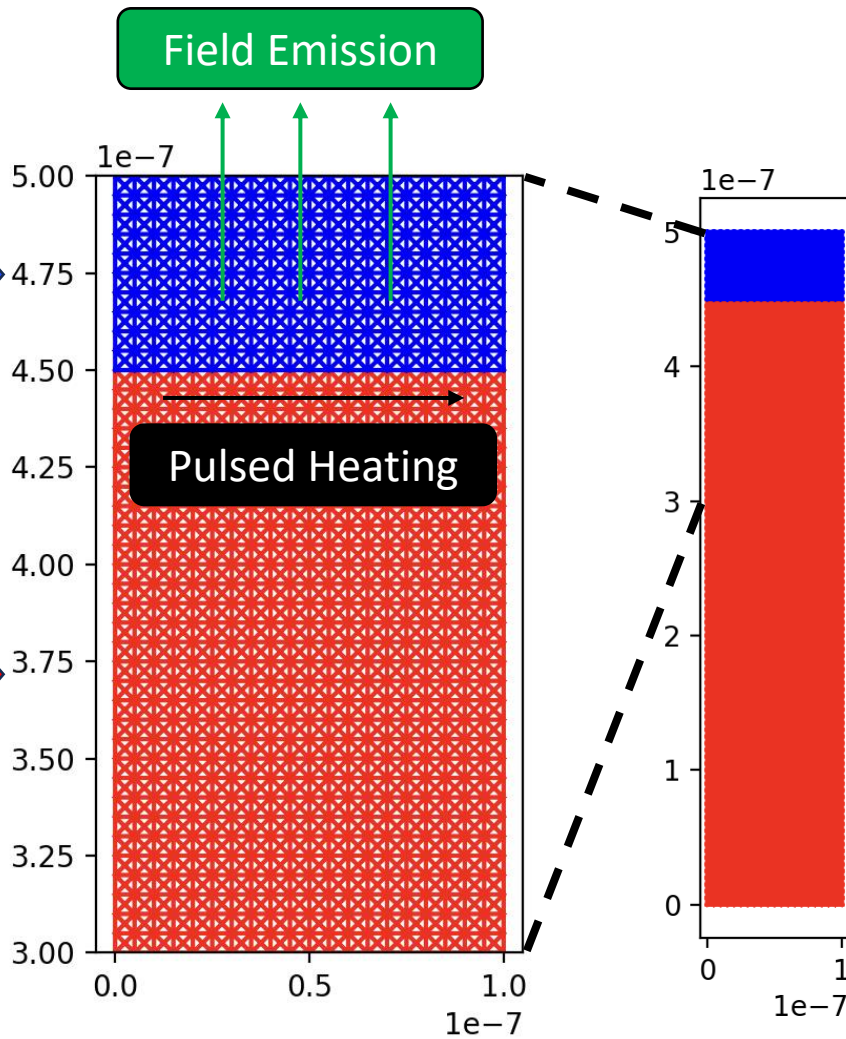
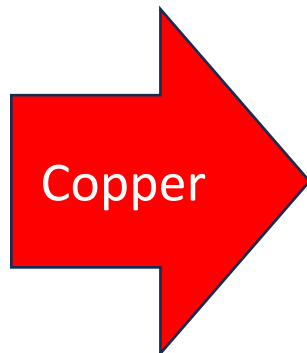
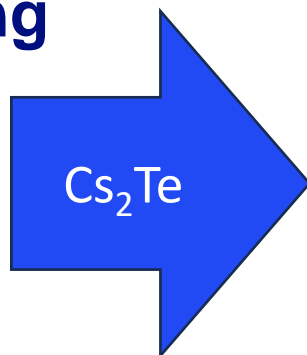
Pulsed Heating

- Without proper cooling temperature rise of ~ 100 K is expected

David Pritzkau <https://www.slac.stanford.edu/grp/arb/tn/arbvol3/ARDB271.pdf>



Pulsed Heating



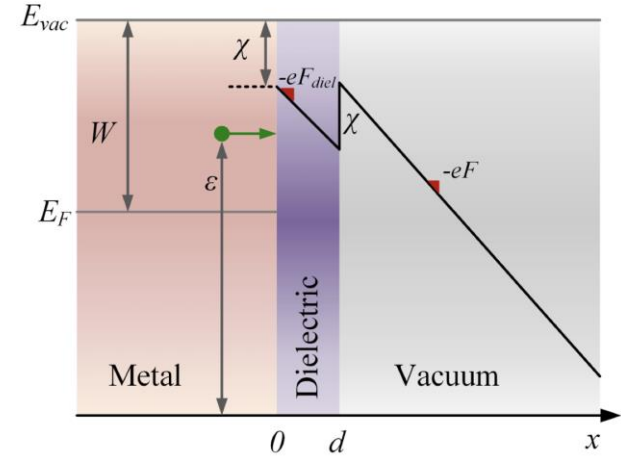
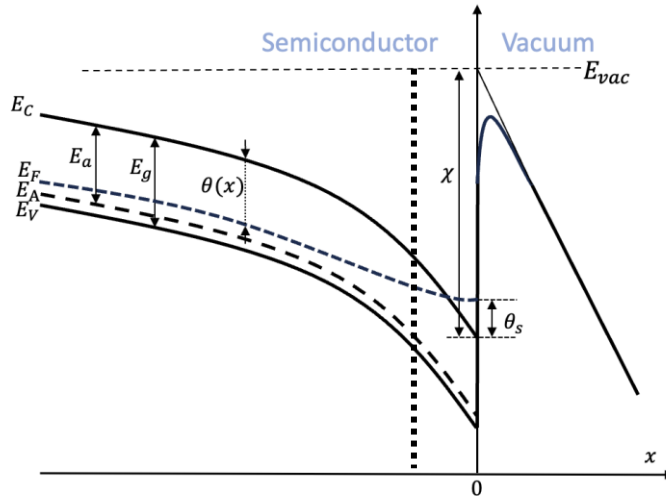
Acknowledgement

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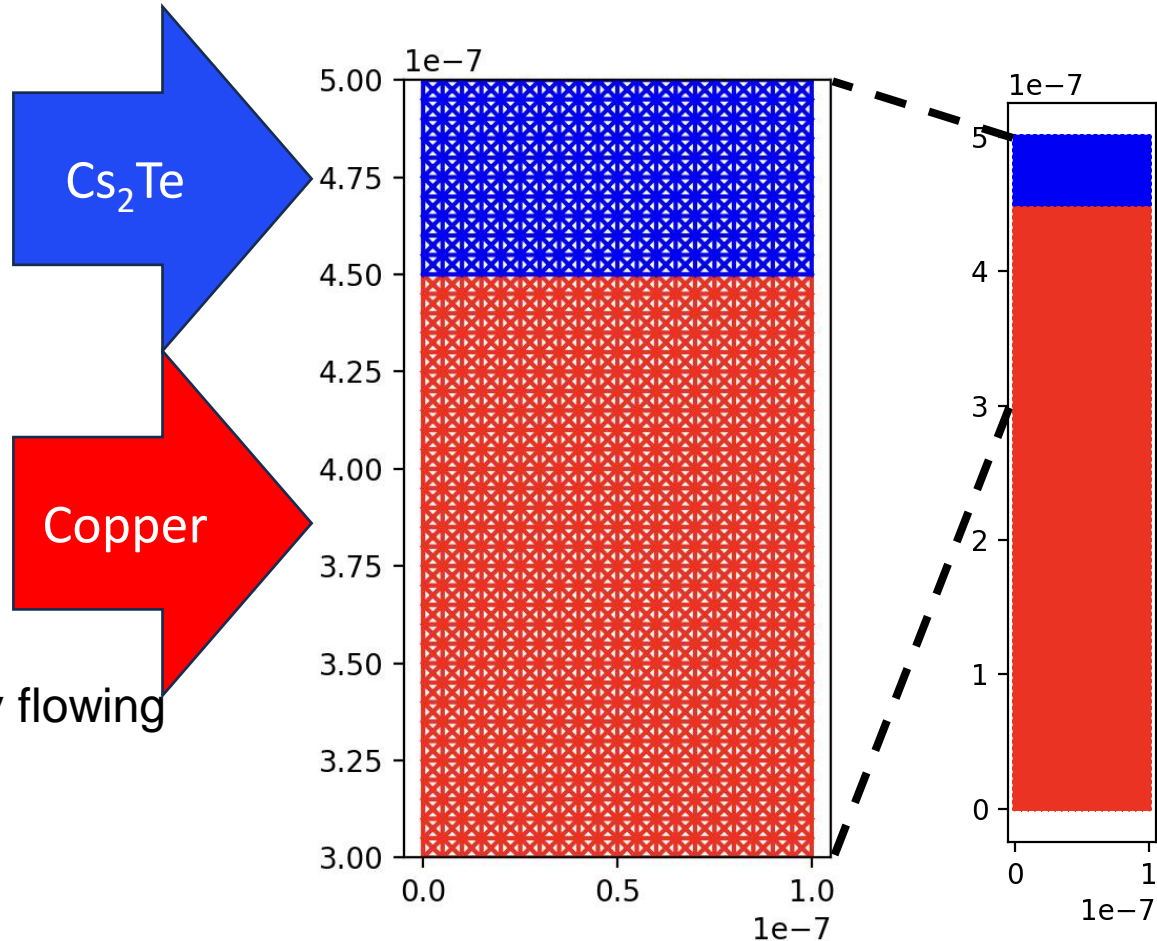
Assuming Double Triangle Energy Barrier

- Conduction-band near in the thin film follows the slope $-eF_{\text{vacuum}}$
- fermi level follows the slope $-eF_{\text{diel}}$
- linear relationship between $E_c(x)$ and $E_f(x)$ in the thin film



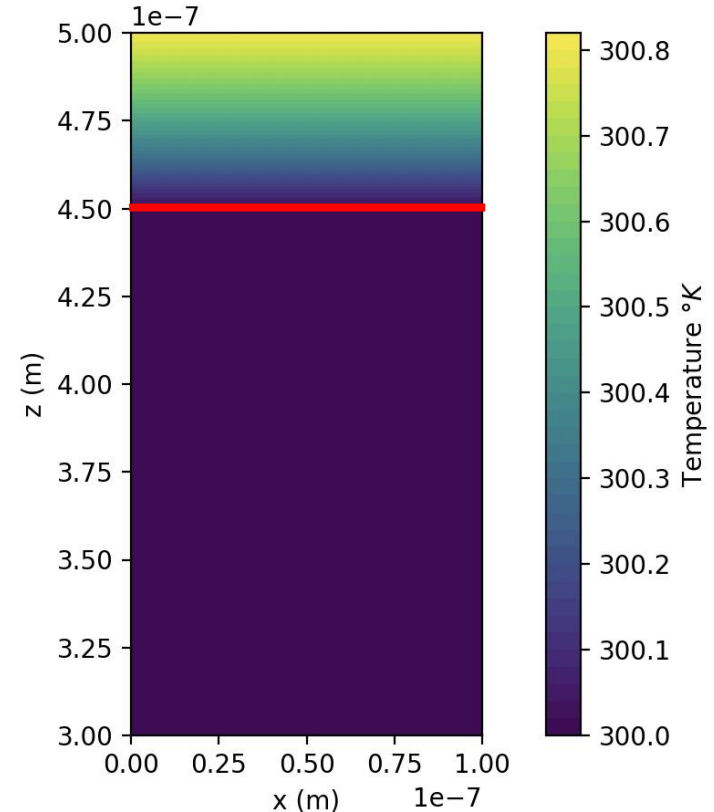
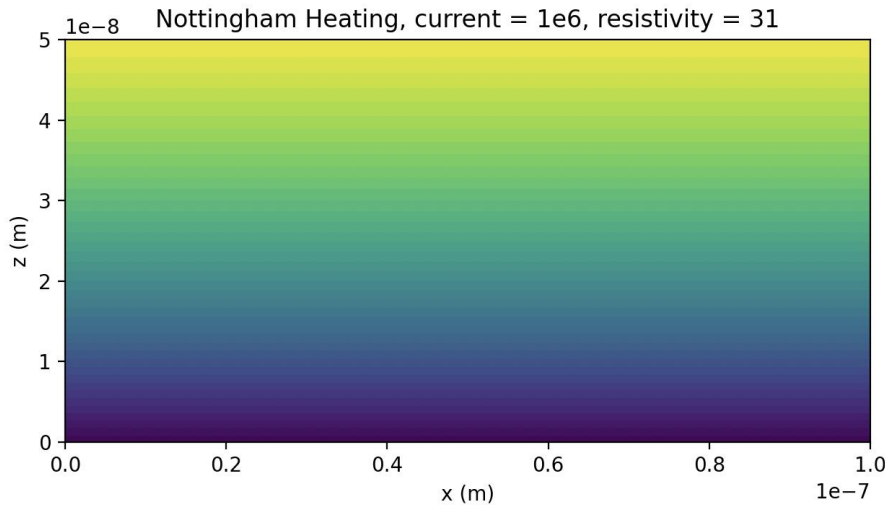
Simulation setup with copper layer

- 50 nm layer width
- Electrical Resistivity =
 - Cs₂Te: $31 \Omega \cdot m$
 - Copper: $1.68e-8 \Omega \cdot m$
- Thermal Conductivity =
 - Cs₂Te: $0.12 \frac{W \cdot m}{K}$
 - Copper: $386 \frac{W \cdot m}{K}$
- $1e6 A/m^2$ current density flowing through Cs₂Te



With Cs2te on top of copper layer

- Result is (basically) equivalent to boundary condition case ↓



Charge Density near surface

- $y(x) = \frac{E_F(x) - E_C(x)}{k_B T / q}$
- Linear relation with x vs y
- Can calculate charge density near surface

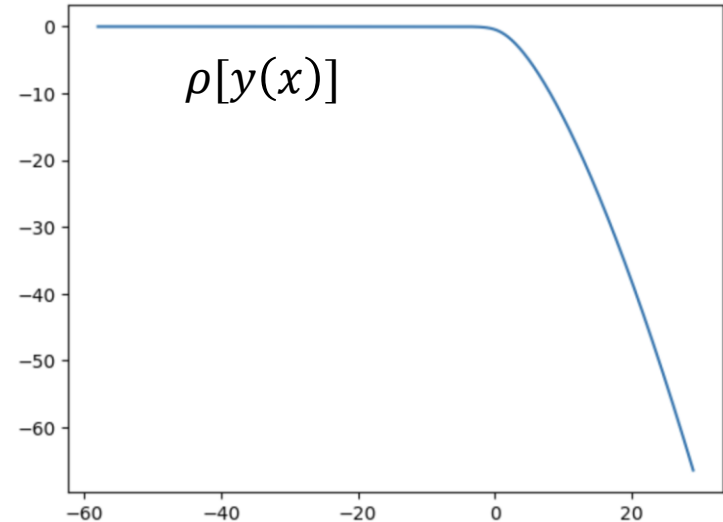
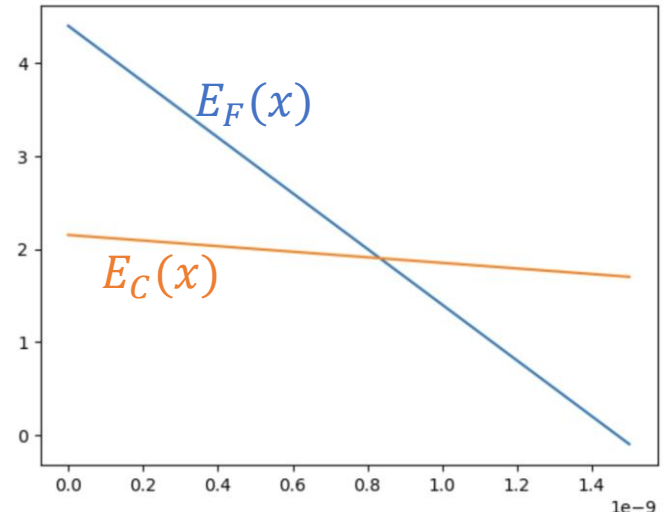
$$n(y) = N_C F_{1/2}(y),$$

$$p(y) = N_V F_{1/2}(-E_g / k_B T - y),$$

$$N_a^-(y) = \frac{N_a}{1 + 2 \exp(-E_a / k_B T - y)},$$

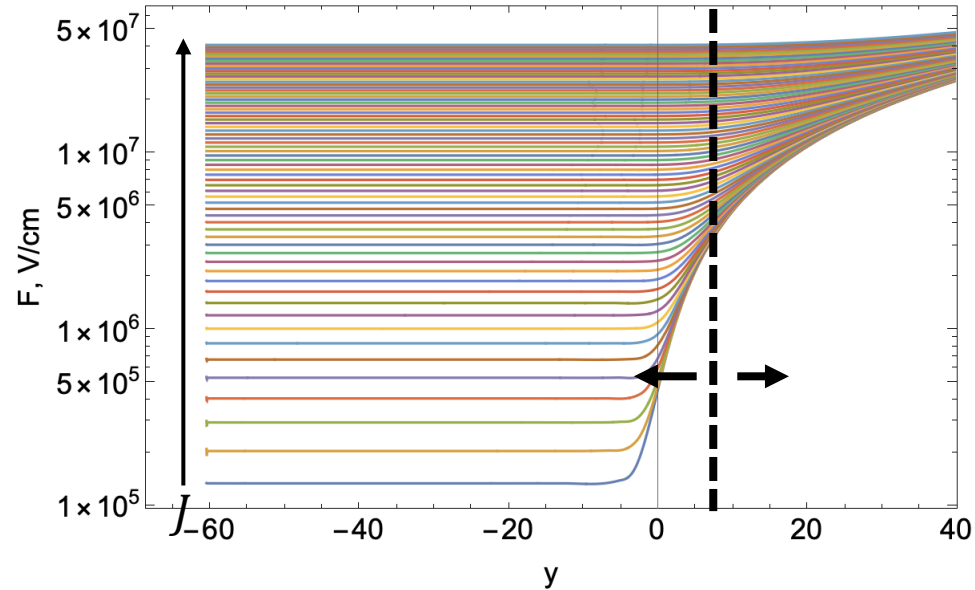
$$N_d^+(y) = \frac{N_d}{1 + 2 \exp(E_d / k_B T + y)}.$$

$$\rho = -q(n - p + N_a^- - N_d^+).$$



Result

- Each colored line represents a different current.
- Surface field/current can be determined by the assumed y (surface)



Current vs Field Preliminary Result

