



# Towards 20 T accelerator magnets: a road to super-high energy colliding beams

**A.V. Zlobin**

**Fermilab**





## *Outline*

- ❖ **Why do we need Higher Fields in accelerators and how to generate high fields?**
- ❖ **SC magnet possibilities and limitations**
- ❖ **SC material options**
- ❖ **20+ T HTS/LTS hybrid magnets**
- ❖ **Conclusions**



## *Why do we need higher field magnets?*

- ❖ **For a fixed size of a circular collider, its energy is limited by the strength of bending dipole magnets.**

$$E[GeV] = 0.3RB [m \cdot T]$$

- ❖ **For both linear and circular machines, their maximum luminosity is determined (among other factors) by the strength of quadrupole magnets used for the final beam focusing.**
- ❖ **We should not forget that our work inspires and fertilizes other fields of science and industry which need and use high field superconducting magnets and related technologies.**



## Accelerator Electromagnets

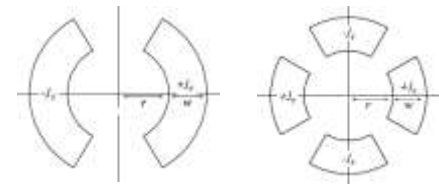
- ❖ Magnetic fields are generated by electrical currents (Bio-Savart law)

$$B_{\theta} = \frac{\mu_0 I}{2\pi r}$$



- ❖ There are current configurations which produce dipole, quadrupole and higher multipole fields

- Dipole configuration (60° coil)
- Quadrupole configuration (30° coil)



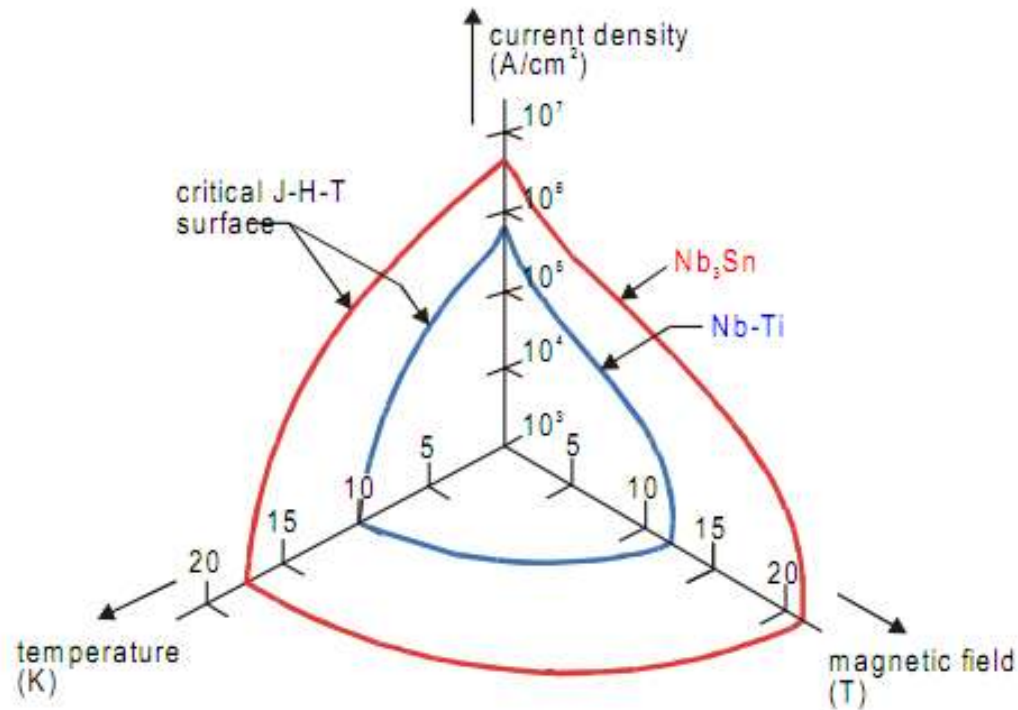
- ❖  $B_D$  and  $G_Q$  are proportional to current density  $J_e$  in coil and coil width  $w$

$$B_D = -\frac{\sqrt{3}\mu_0}{\pi} J_e w \quad G_Q = -\frac{\sqrt{3}\mu_0}{\pi} J_e \ln\left(1 + \frac{w}{r}\right)$$

- ❖ The current density in coil  $J_e$  is a key parameter
  - Resistive magnets with Cu or Al cable -  $J_e \sim 5-50 \text{ A/mm}^2$
  - Superconducting magnets -  $J_e \sim 500-1000 \text{ A/mm}^2$
- ❖ SC magnets are more compact and have lower operational costs (only power consumption is to keep them cold)



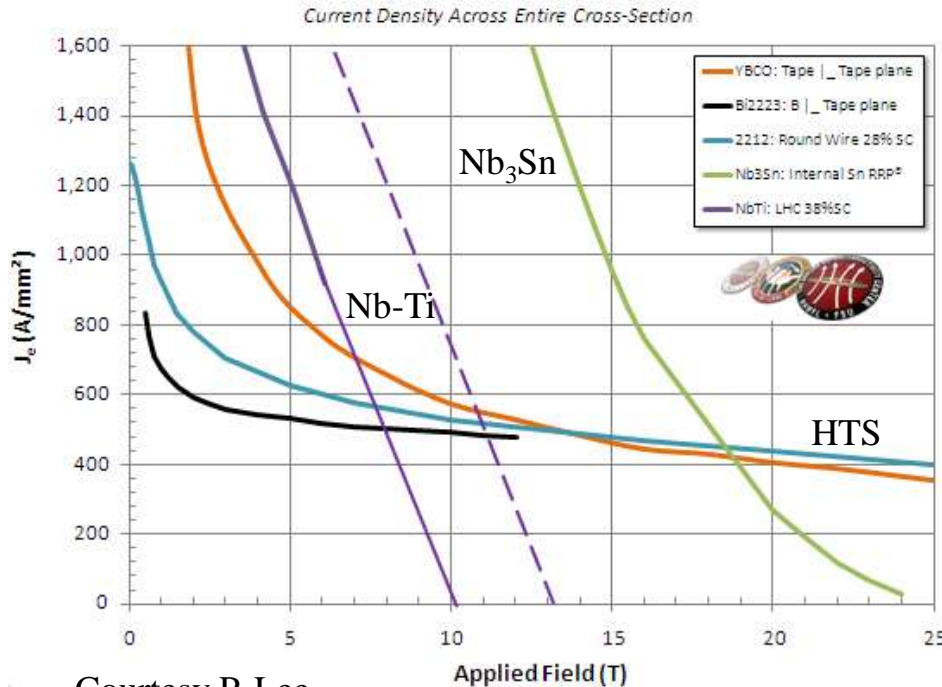
## *$J_e$ Limit in SC Magnets*



- ❖ The highest fields in accelerator magnets have been achieved using SC magnets.
- ❖ However, superconductivity exists inside the critical surface in ( $J$ ,  $B$ ,  $T$ ) space.
- ❖  $J_e$  (and  $B$ ) in SC magnets is limited by the superconductor  $J_c(B, T)$ .



# HTS Accelerator Magnets



❖ The materials are produced by industry in long length (~1 km)

❖ **Nb-Ti**

- $B_{c2}(0) \sim 14$  T
- $T_c(0) \sim 9$  K
- => 10 T magnets

❖ **Nb<sub>3</sub>Sn**

- $B_{c2}(0) \sim 27$  T
- $T_c(0) \sim 18$  K
- => 16-17 T magnets

❖ **BSCCO/YBCO**

- $B_{c2}(4.2 \text{ K}) > 50$  T
- $T_c(0) \sim 110/90$  K

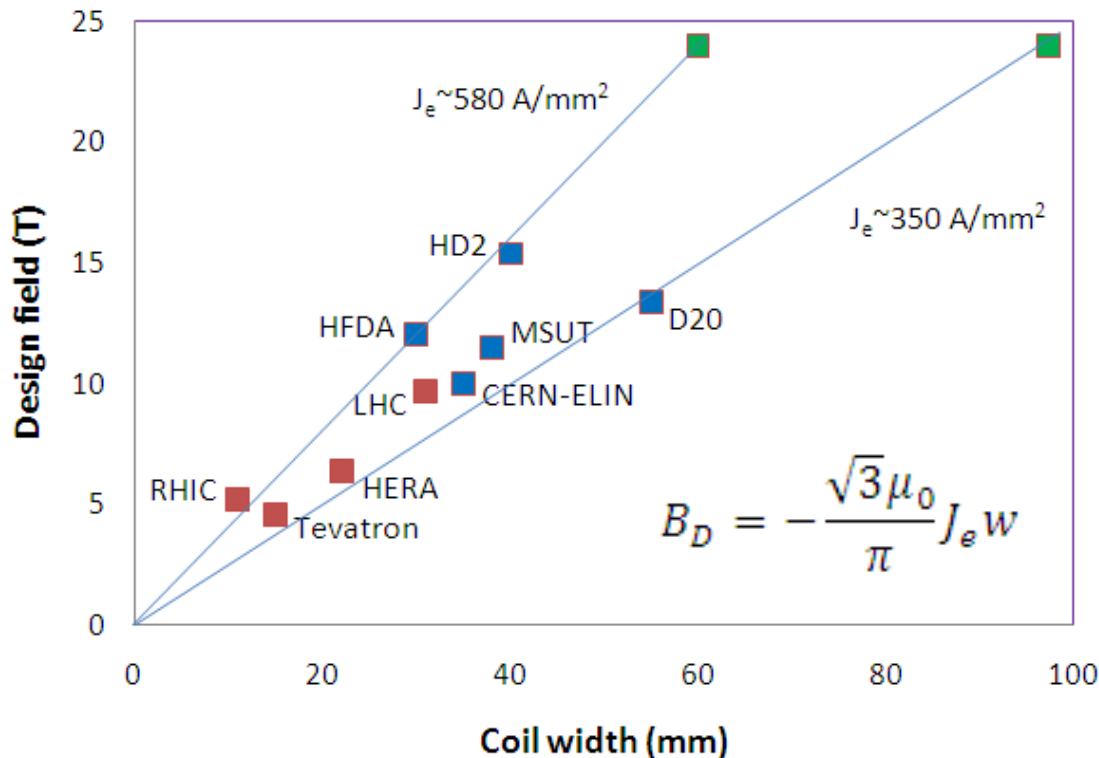
❖ High-field high-temperature superconductors open the possibility of accelerator magnets with  $B_{nom} > 15$  T

- $B_{des} > 18$  T assuming typical 20% margin

❖ Due to the lower  $J_c$  @  $B < 18$  T (and higher cost) for HTS, a hybrid approach with Nb<sub>3</sub>Sn coils in fields < 15 T is an attractive option



## Towards 20+ T Magnets



### **Nb<sub>3</sub>Sn section:**

$$B_{\text{des}} = 13\text{T} + 20\% = 15.6\text{T}$$

$$J_{e\_coil}(16\text{T}) = 580\text{A/mm}^2$$

$$J_{e\_sc}(16\text{T}) = 800\text{A/mm}^2$$

$$\Rightarrow w \sim 45\text{ mm}$$

### **HTS section:**

$$B_{\text{des}} = 7\text{T} + 4\text{T} = 11\text{T}$$

$$J_{e\_coil}(24\text{T}) = 350\text{A/mm}^2$$

$$J_{e\_sc}(24\text{T}) = 700\text{A/mm}^2$$

$$\Rightarrow w \sim 40\text{ mm}$$

**Total coil width  $w_{\text{tot}} \sim 85\text{ mm}$  with  $J_{e\_sc}(24\text{T}) = 700\text{A/mm}^2$**

o **Now  $J_{e\_sc}(24\text{T}) \sim 400\text{A/mm}^2$**

**To reduce the coil width to 60 mm  $J_{e\_sc}(24\text{T}) \sim 1200\text{A/mm}^2$**

**Nb<sub>3</sub>Sn section: dipole aperture  $> 120\text{ mm}$  and  $B_{\text{max}} \sim 16\text{ T}$**

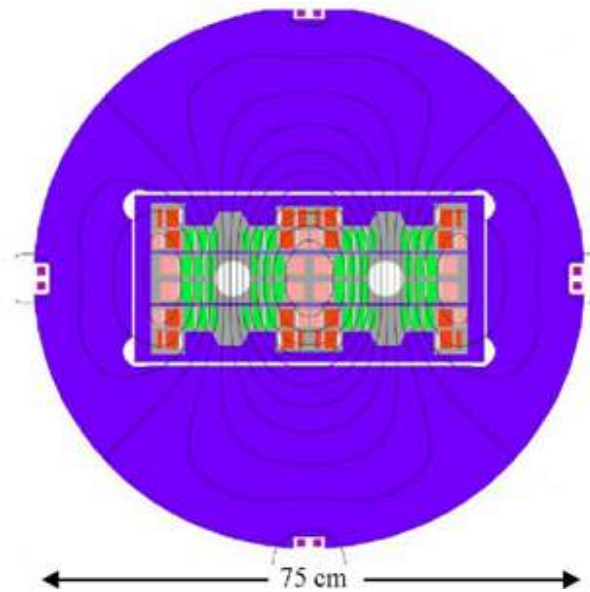
o **New challenging R&D goal for Nb<sub>3</sub>Sn dipole magnets**



# 24 T Dipoles for LHC Energy Upgrade

P. McIntyre et al.(TAMU), PAC'2005

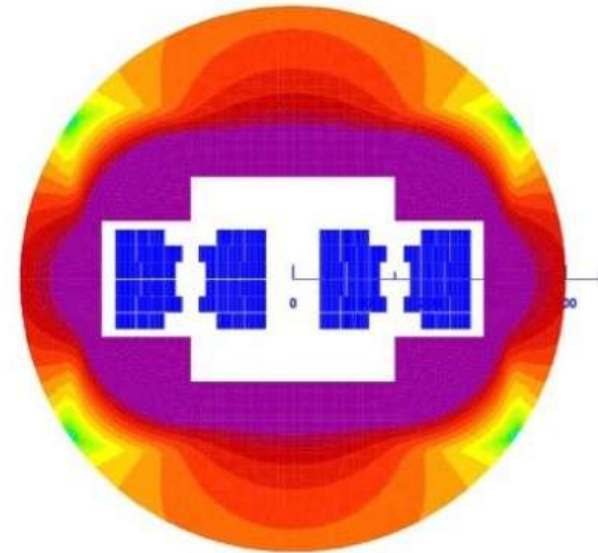
L. Rossi, E. Todesco (CERN), HE-LHC'2010



Bi2212 + Nb<sub>3</sub>Sn

Table 1. Main parameters of the 24 T hybrid dipole.

Dipole dimensions:	
length	30 m
cold mass diameter	80 cm
Beam tube diameter	40 mm
Operating temperature	4.5 K
Coil current	33 KA
Maximum stress in windings	150 MPa
Stored energy/bore	5 MJ/m
Total horizontal Lorentz force/bore	40 MN/m



Bi-2212+Nb<sub>3</sub>Sn+Nb-Ti

Table : Main parameters of the HE-LHC and LHC dipole

		HE-LHC	LHC
Operational field	(T)	20.0	8.3
Operational current	(kA)	13.8/6.9	11.8
Operational margin	(%)	20	14
Magnetic length	(m)	14.3	14.3
Total stored energy	(MJ)	100	7.0
Distance between beams	(mm)	300	194
Maximum coil thickness	(mm)	97.3	31
Cold mass diameter	(mm)	800	570





# HTS Magnet Cost Expectation

L.Rossi, E.Todesco (CERN), HE-LHC'2010

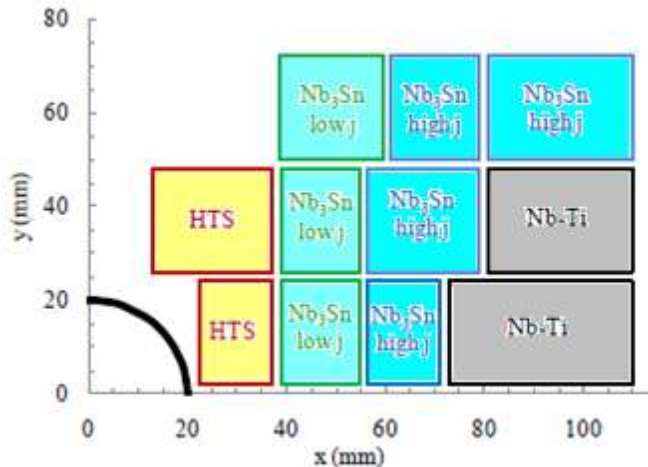


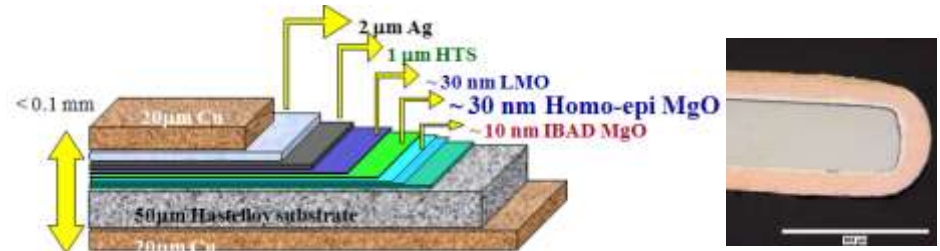
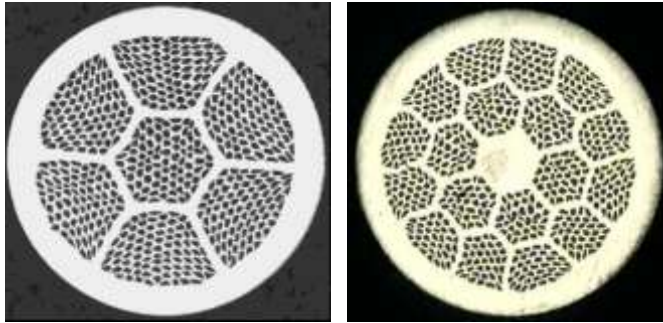
Table : Estimate of the cost of the conductor for a 14.3 m coil length two-in-one dipole.

	(\$/kg)	m <sup>3</sup>	Kg	M\$	%	Field (T)
Nb-Ti	200	0.12	960	0.19	5%	8
Nb <sub>3</sub> Sn - h	800	0.16	1300	1.0	28%	13
Nb <sub>3</sub> Sn - l	800	0.10	850	0.7	18%	15
HTS	3000	0.07	620	1.9	49%	20
<b>Total</b>		<b>0.45</b>	<b>3730</b>	<b>3.8</b>		

- ❖ **Cost estimate for the generic shell-type hybrid HTS/Nb<sub>3</sub>Sn 20 T magnet gives comparable numbers**
- ❖ **Taking into account the cost of conductor, components and assembly labor the magnet cost per T\*m (w/o cryostat):**
  - **8.3 T LHC NbTi dipole – 7-8 k\$/T/m**
  - **20 T HTS/LTS dipole – 16-17 k\$/T/m**
- ❖ **The possibility of operation of 20 T magnets at 4.5 K instead of 1.9 K (LHC) reduces the cost difference**



## Practical HTS Strands



- ❖  $\text{Bi}_2\text{Sr}_2\text{CaCu}_2\text{O}_x \Rightarrow \text{Bi-2212}$
- ❖ Multifilament round 0.7-1.0 mm wire with Ag matrix
- ❖ SC fraction ~25-30%
- ❖ Traditional PIT process (OST)
  - Unit length >1 km
- ❖ Complex high-temperature final heat treatment in  $\text{O}_2$
- ❖ Brittle after heat treatment, sensitive to longitudinal and transverse load
- ❖ Isotropic properties
- ❖  $\text{YBa}_2\text{Cu}_3\text{O}_y \Rightarrow \text{YBCO-123}$
- ❖ 4-12 mm wide tape, 50% is high strength superalloy (Hastelloy) and ~40% is Cu coating
- ❖ YBCO fraction ~1%
- ❖ Complex multilayer deposition process and final Cu electroplating (SP)
  - Unit length ~500-1000 m
- ❖ No final heat treatment
- ❖ Brittle but can withstand substantial load
- ❖ Large  $I_c$  variation along the tape
  - limit unit length to 50-200 m
- ❖ Highly anisotropic

**Present  $J_e(24\text{T})$  is  $\sim 400\text{A}/\text{mm}^2$  for both materials. It needs to be increased by a factor of 2-3 for 20 T accelerator magnets.**



## HTS cables



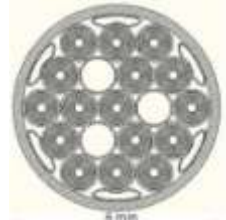
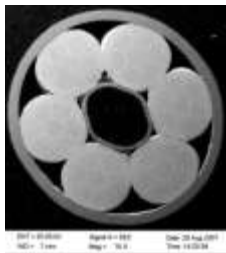
E. Barzi et al., Fermilab

### ❖ Rutherford cable works well for round Bi-2212 wire

- High packing factor ~85%
- $I_c$  degradation after cabling <20%
- Sensitive to transverse pressure
- R&D at Fermilab and LBNL

### ❖ Alternative option

- Round cable inside metal tube to reduce transverse and axial load on Bi-2212 strands
- Low packing factor



P. McIntyre et al., TAMU

### ❖ YBCO tape cannot be cabled using the Roebel method

- Large packing factor
- $I_c$  degradation and sensitivity to transverse pressure are being studied
- Under development by Karlsruhe (Germany) and General Cable and Industrial Research, Ltd (NZ)
  - 15/5 YBCO Roebel cable self-field  $I_c > 10$  kA



**10-kA HTS cable R&D is critical for 20 T accelerator magnets.**



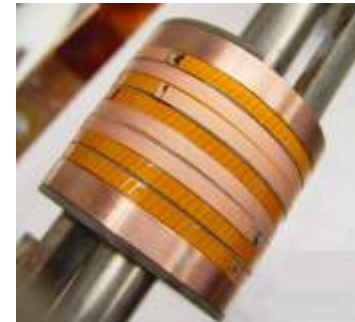
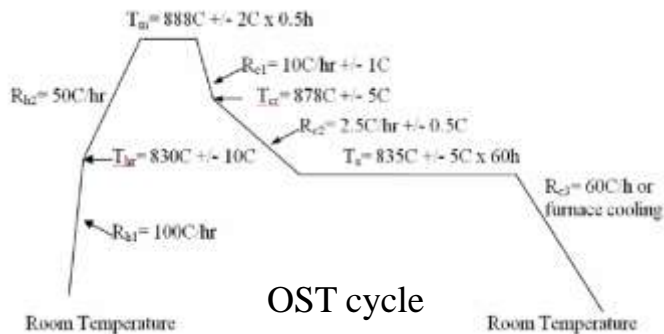
# HTS Coil technology

## Bi-2212 coils:

- ❖ **Cos-theta and block-type coil geometry possible**
  - **R&D using solenoids and small racetrack coils made of single strand and Rutherford cables**
- ❖ **W&R approach**
- ❖ **Complicate multi-step HT cycle**
  - **Temperature variations  $\pm 1-2$  C**
- ❖ **Liquid BSCCO can leak through the Ag matrix during reaction**
  - **Coil performance is  $\sim 50-70\%$  of short sample limit**
- ❖ **Insulation/structure/conductor chemical compatibility**

## YBCO coils:

- ❖ **Block-type coil geometry with relatively small bending radii**
  - ❖ **R&D using solenoids and small racetrack coils based on single tapes so far**
- ❖ **R&W approach**
- ❖ **Coil performance is  $\sim 80-90\%$  of short sample limit**
  - **Tape splicing may degrade the coil performance**



A. Godeke et al., LBNL

V. Lombardo et al., Fermilab

**The key step is HTS Coil technology R&D based on high-current HTS cables and realistic mechanical structures.**



## *Conclusions*

- ❖ **Accelerator magnets with nominal fields of 20+ T look feasible (technically and economically) thanks to recent progress with HTS materials.**
- ❖ **Focused and well coordinated R&D efforts are needed to develop and demonstrate this technology including**
  - **HTS conductor properties (BSCCO, YBCO) and processing**
  - **high-current HTS cables compatible with accelerator magnet operating conditions**
  - **robust coils and mechanical structures capable to generate accelerator field quality under high Lorentz forces**
  - **Short and long magnet performance**
- ❖ **Nb<sub>3</sub>Sn accelerator magnet R&D is still important**
  - **Nb<sub>3</sub>Sn coil will generate ~70% of the total field and play an important role in magnet quench protection and cost**
  - **focus on large aperture (>130 mm) 15-16 T magnets**
- ❖ **If successful, these technology will provide excellent opportunities for HE-LHC and especially for Muon Collider.**



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