

PAUL SCHERRER INSTITUT



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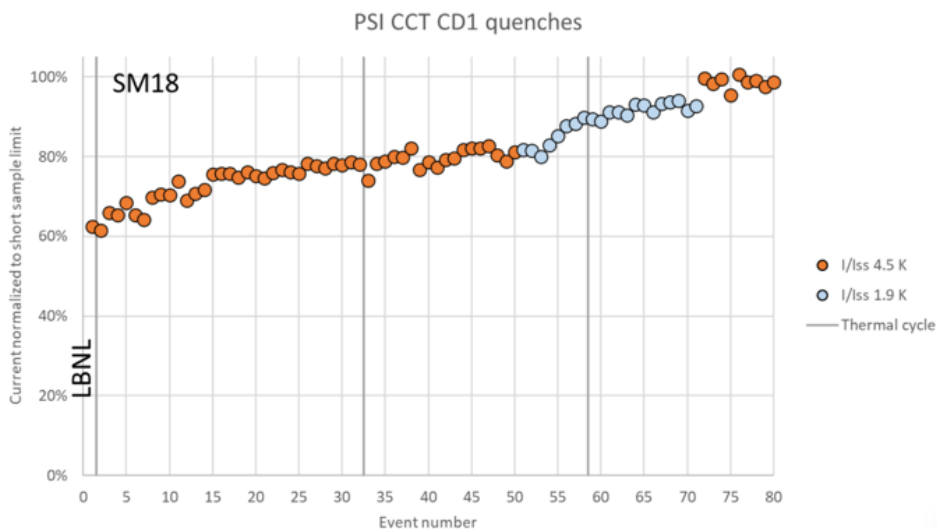
# Progress Report on the PSI CHART LTS and Hybrid HFM Roadmap

HFM annual meeting, 2023

Work supported by the Swiss State Secretariat for Education, Research and Innovation SERI.  
This work was performed under the auspices and with support from the Swiss Accelerator Research and Technology (CHART) program

# CD1 Testing Results and CCT Conclusions

- Canted-Cosine-Theta Magnet CD1 and Overview of the testing campaign of January 2023



### Training behavior:

the magnet trained a lot. How can we make it training less?

### Nb<sub>3</sub>Sn limit:

The magnet reached 100% of the maximum field at 4.5 K

### Degradation:

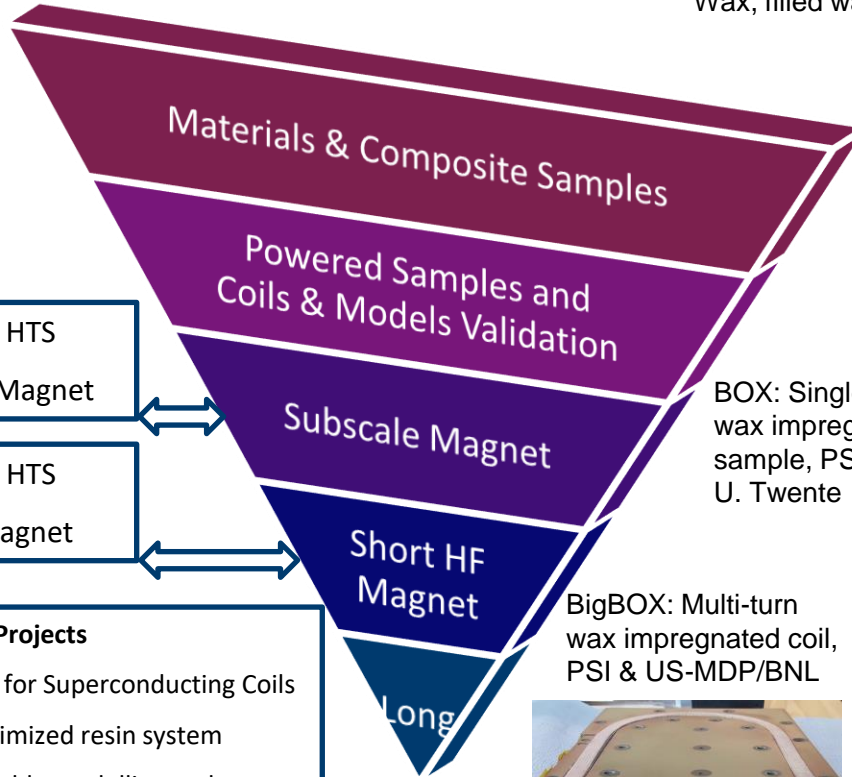
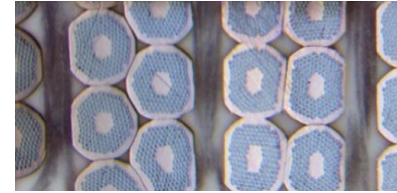
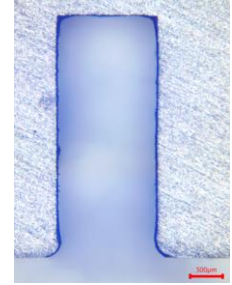
After 80 quenches and thermal cycles the magnet shows no degradation

**Stress-management works!**

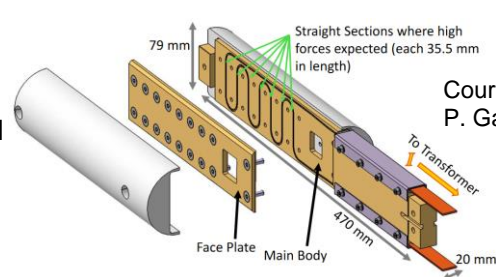
Courtesy F. Mangiarotti (CERN) and M. Daly (PSI).

# LTS and Hybrid LTS/HTS HFM Roadmap

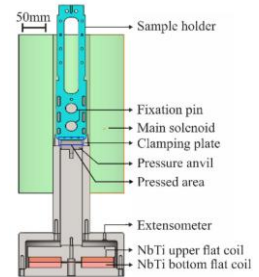
Wax, filled wax / epoxy process development, insulating ceramic coating, etc A. Brem



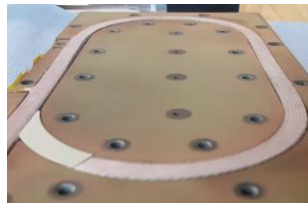
BOX: Single-turn wax impregnated sample, PSI & U. Twente



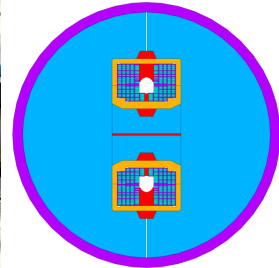
Courtesy P. Gao



BigBOX: Multi-turn wax impregnated coil, PSI & US-MDP/BNL



Subscale Stress-Managed Common-coils



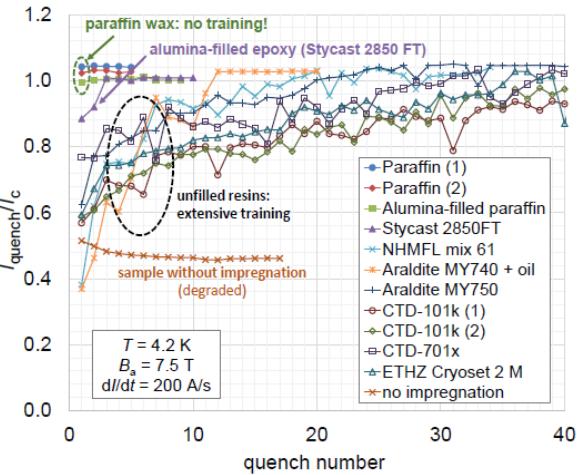
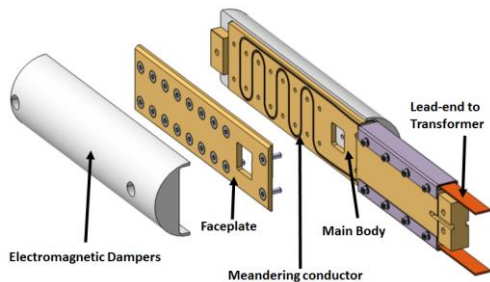
High-Field Stress-managed common coils

# HFM annual meeting

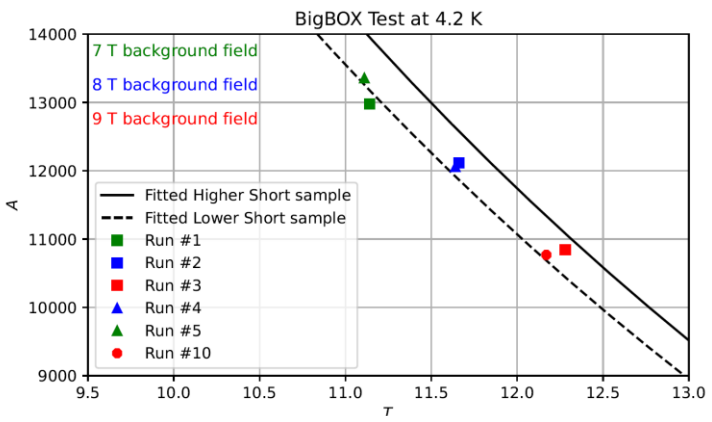
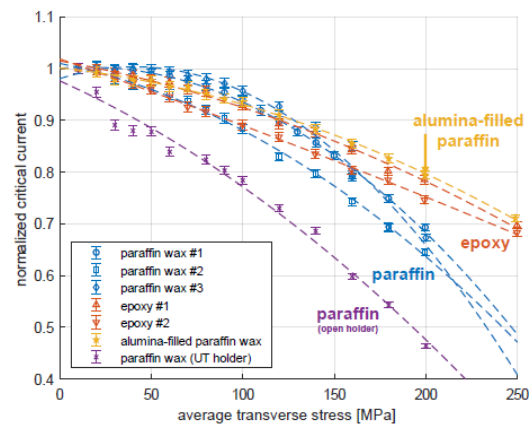
- Tuesday, 31 October: Transient effects in tape-stack cable and the PSI roadmap towards HTS HFMs – PSI, D. Sotnikov
- Wednesday, 1 November: Progress in materials and processes at PSI, A. Brem
- Wednesday, 1 November: WP4.4 - Determination of deformation via image-based measurements and design of epoxy systems for Nb<sub>3</sub>Sn Rutherford cables - ETHZ/CHART, P. Studer and X. Kong
- Thursday, 2 November: HFM infrastructure needs at PSI, B. Auchmann
- This presentation focus on the **subscale** and **14+ T Stress-Managed Common-Coils**



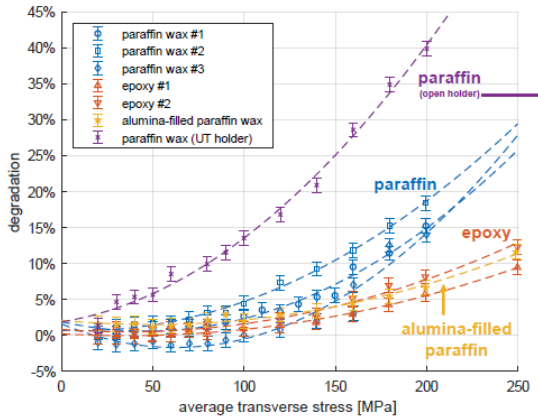
# BOX, Compression BOX and BigBOX



Normalized critical currents (11 T, 4.2 K)



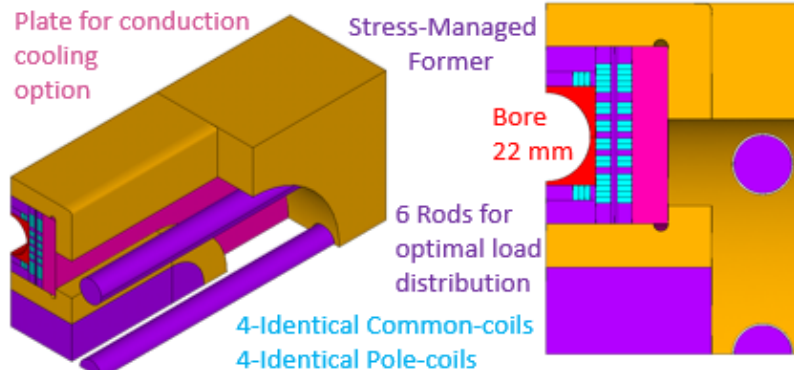
Degradation: Irreversible reduction in current after unloading to 10 MPa



"Influence of fillers and debonding layers on training of short Nb<sub>3</sub>Sn Rutherford cables studied in the BOX facility" & "Transverse pressure performance of paraffin-impregnated Nb<sub>3</sub>Sn Rutherford cables compared to epoxy-impregnated cables", S. Olten et al, MT-28

"Assessment of Training Performance, Degradation and Robustness of Paraffin-Wax Impregnated Nb<sub>3</sub>Sn Demonstrator under High Magnetic Field", D. Araujo et al, MT-28

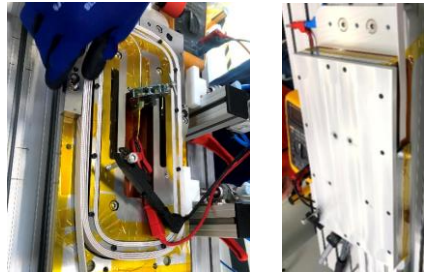
- Validating **manufacturing process** and introducing advanced concepts: **coil pre-load free**, at room temperature; stress-management structure and **splicing on the low-field region**.
- Fast turn-around platform for testing matrix systems; protection concepts and cooling options.
- Hybrid magnet with LTS Common-Coils and HTS racetracks
- LTS conductor manufactured by LBNL (cct subscale cable)



Magnet parameters for testing all coils or the common-coils. The coils straight section is 150 mm. The values refer to the fitted wire  $I_c$  curve at 4.2 K values.

Parameter	All coils	CCs
$B_0$ in T	5.15	5.1
$B_{peak}$ in T	6.45	6.3
$I_{op}$ in kA	8.25	9.2
$E_{mag}$ in kJ	15.2	16.4

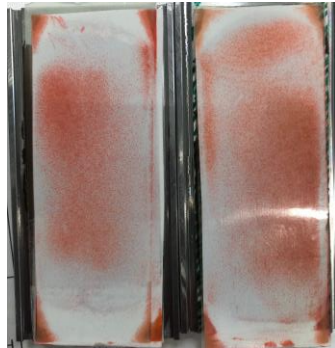
- Progress on R&D and engineering design (testing in Q2/2024)



Winding method validation

Instrumented mock-up for  
assembling validation

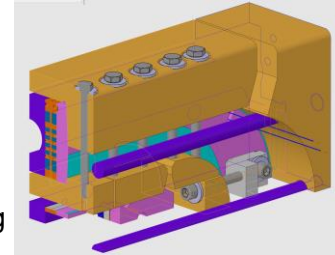
Pre-scaled paper after  
disassembling the Mock-up



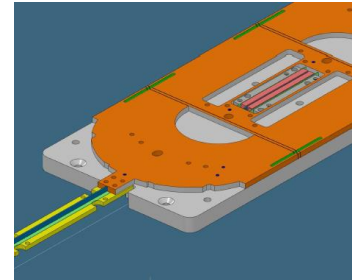
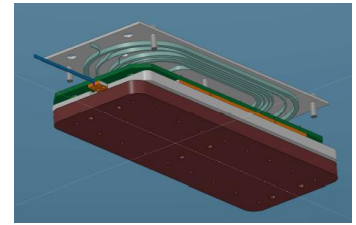
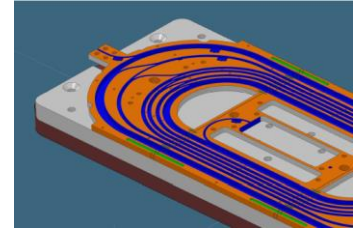
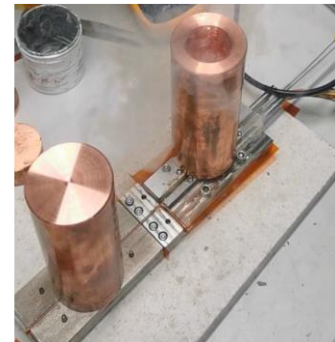
Mock-up for axial pre-  
load

Low-temperature  
splicing process trials

Completed engineering  
design



T. Michlmayr

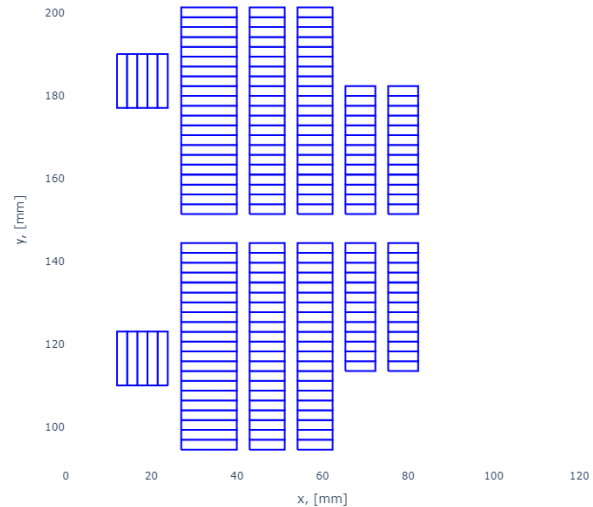


# Stress-Managed Asymmetric Common-Coils 1/2

In respect to a standard common-coils magnet, we would like to explore solutions on how to:

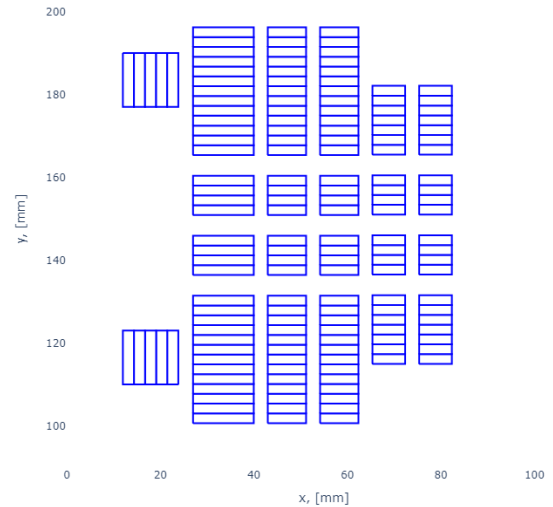
- deal with high **Lorentz forces**
- **simplify the common-coils architecture** for accelerator magnets
- allowing a full common coils architecture and eventually **reacting & winding**

a: racetracks / clover-leaf coils and wide blocks



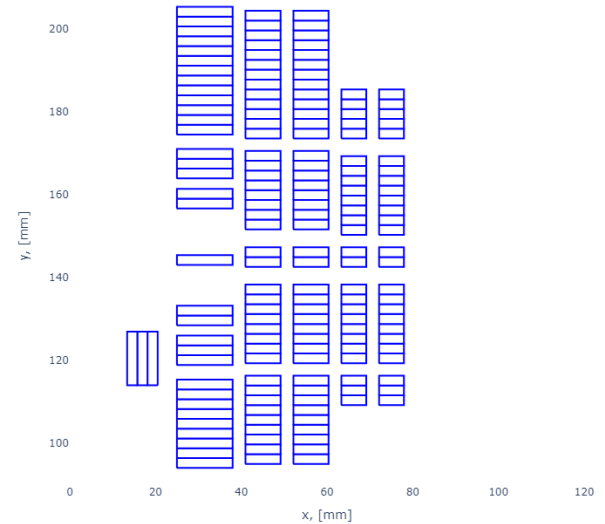
Stress-management with spars

b: racetracks / clover-leaf coils and thin blocks



Stress-management with spars and ribs

c: only common-coils and thin blocks



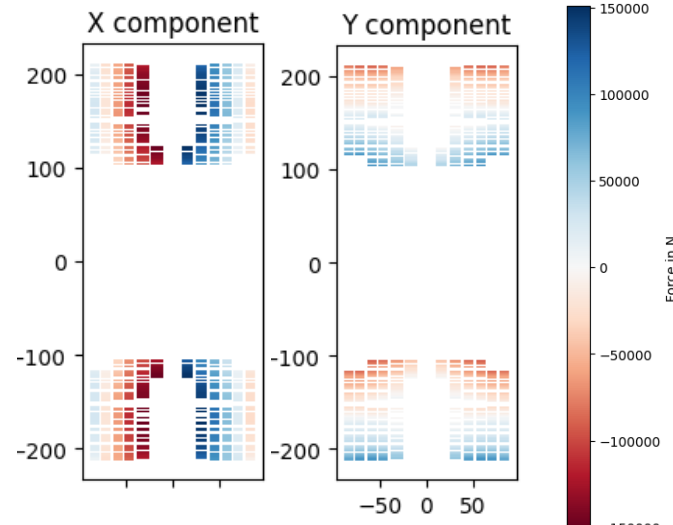
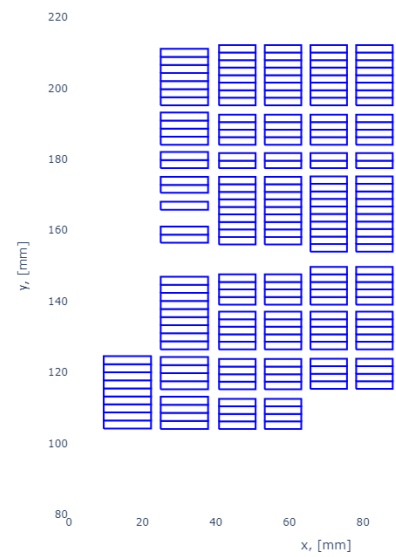
Asymmetric design



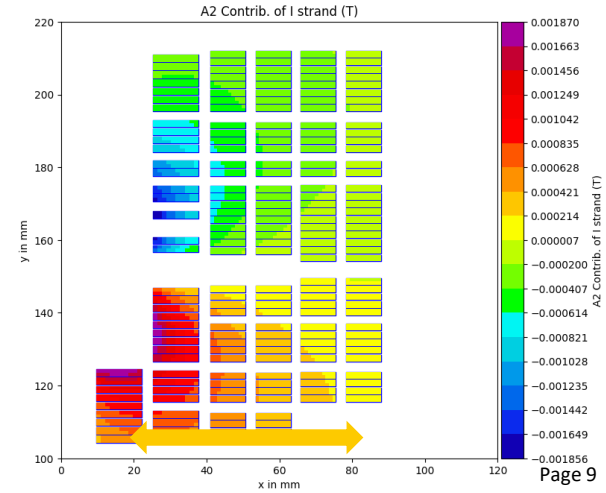
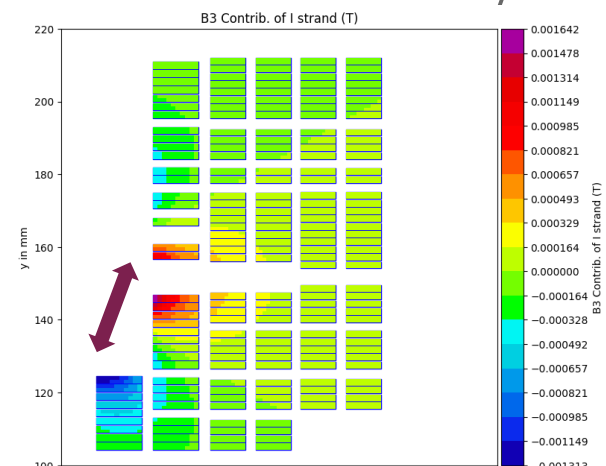
# Stress-Managed Asymmetric Common-Coils 2/2

We can further simply option C, by having **only easy-way bend coils**  
**Ribs and spar thickness** were optimized for mechanics  
 Compensation example on **b3** and **a2**

Layers: 1 2 3 4 5 6



D. Araujo



# SMACC: Cross-Section

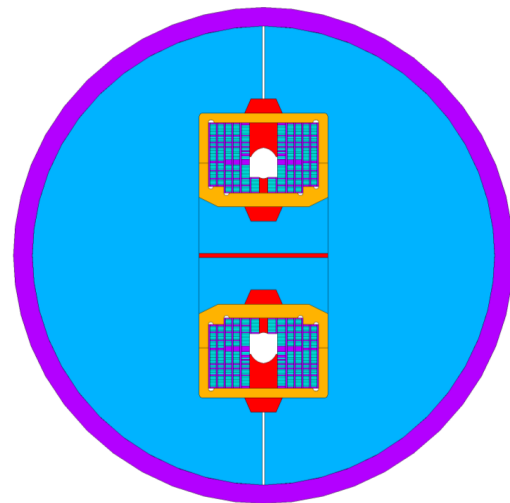
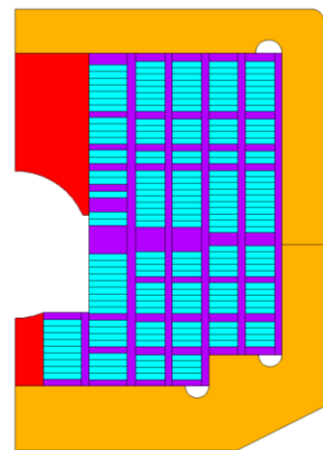
The asymmetric common-coils magnet was designed with a intra-beam distance of 300 mm, 50 mm **bore**, **yoke** diameter of 740 mm and 30 mm thick stainless steel **shell**.

The magnet has 4 different types of coils (layer 1, layer 2, layer 3,4 and layer 5,6) and **12 coils in total (for a double aperture magnet)**. The coils are placed in the stress-management **formers**. The preload is transferred towards the inner-most layers through the **ribs**.

The massive **iron pole**, combined with the asymmetric concept, helps on the balance vertical force balance.

The load, due to Lorentz forces, is distributed between **pads** and **shell**, which limits the thickness of the **shell**.

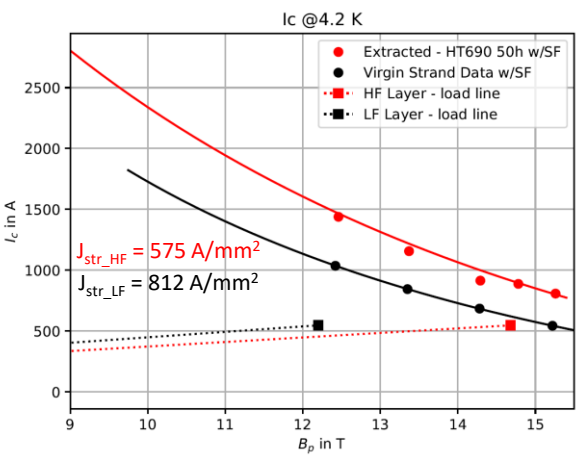
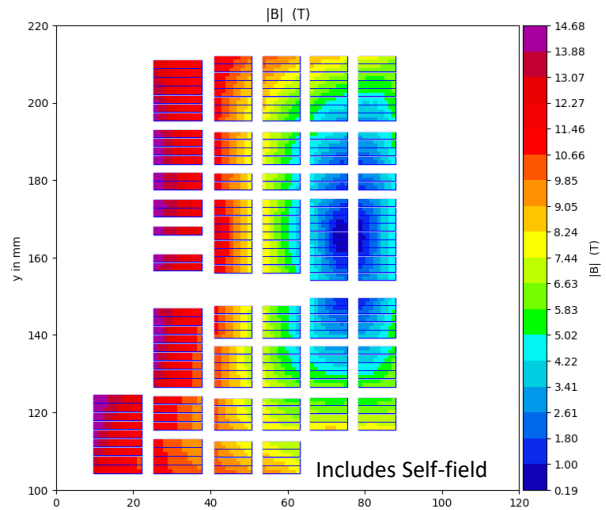
The magnet concept is based on **bladder & keys technology** for room temperature preload. The structure is loaded, but thanks to the stress-management formers, **the coil stress after loading and after cooling is < 40 MPa**.



# SMACC: Magnet Parameters

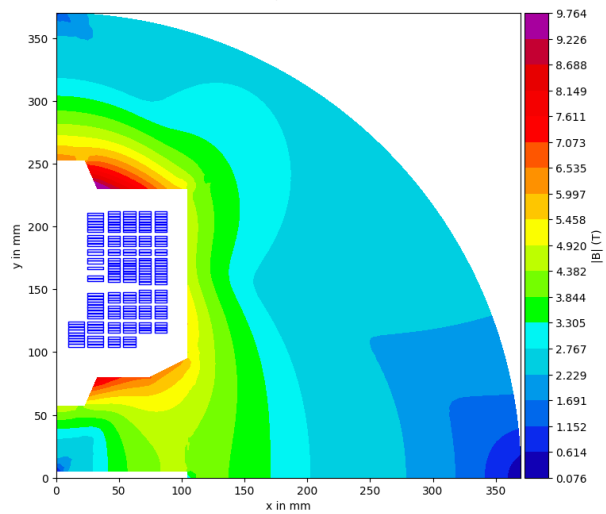
Layers 1 and 2 with 21 x 1.1 mm RRP® 162/169 strand cu/n\_Cu 0.9 and layers 3 to 6 with 18 x 1.0 mm RRP® 132/169 strand cu/n\_Cu 1.3.

Field quality is < 15 units spread between injection and 14 T nominal field operation and < 15 units at nominal (to be further optimized after decision on LF cable).



parameter	value		
Op. temperature	$T_{op}$	4.2	K
Op. current	$I_{op}$	11.48	kA
Central field	$B_0$	13.98	T
Peak field w/sf	$B_p$	14.68	T
Eng. margin		10	%
Inductance	$L$	41	mH/m
Magnetic energy	$E_{mag}$	2.7	MJ/m

High-Field and Low-Field strand experimental data, fitting and load lines



# SMACC: Mechanical Analysis

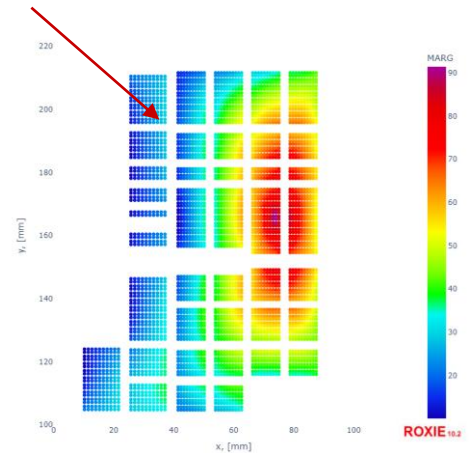
Pre-load with 0.5 mm interference on the keys.

Low-stress on coils after loading and

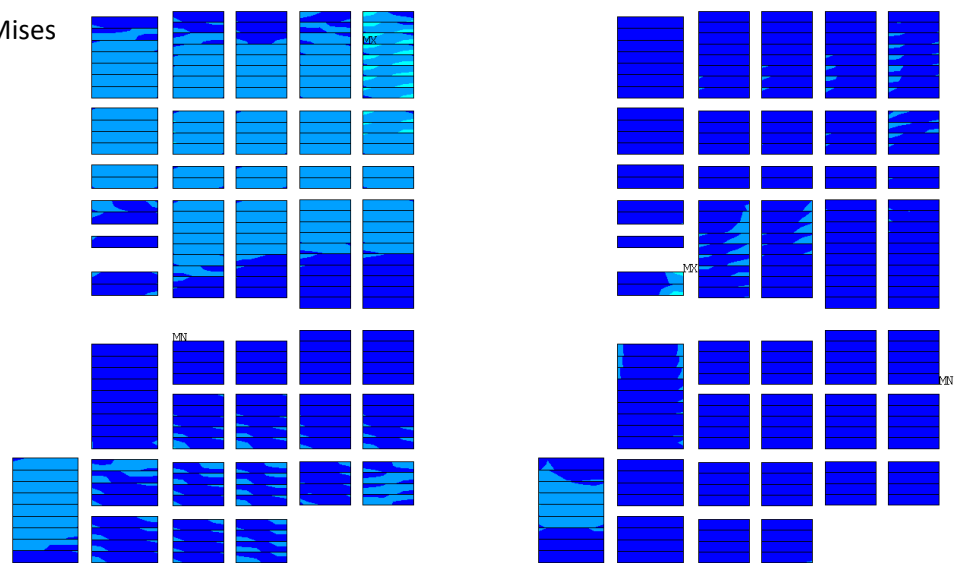
Cooling-down: **37 MPa**

Peak of stress on the low-field side of layers

All magnet components respect material limits



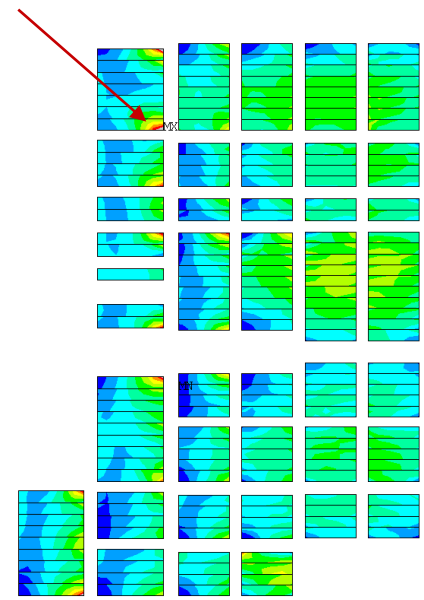
Von-Mises



Keys

Cool-down

Nominal field



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Build 21.1
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NODAL SOLUTION
STEP=3
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SEQV (AVG)
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EFACET=1
AVRES=Mat
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SMN =492913
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0
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.444E+08
.556E+08
.667E+08
.778E+08
.889E+08
.100E+09
    
```

# SMACC: Protection 1/2

- Re-use of tooling for several coils
- Optimized Electrical order for CLIQ protection
- Same side Magnet & CLIQ leads
- Study for 15 m long magnet

## CLIQ optimization study

- 25 CLIQ configurations studied
- 5 CLIQ unit types studied
- Optimized coil electrical order

### LF Cable Outer Coils:

layers 5, 6, 11, 12

### LF Cable Intermediate Coils:

layers 3, 4, 9, 10

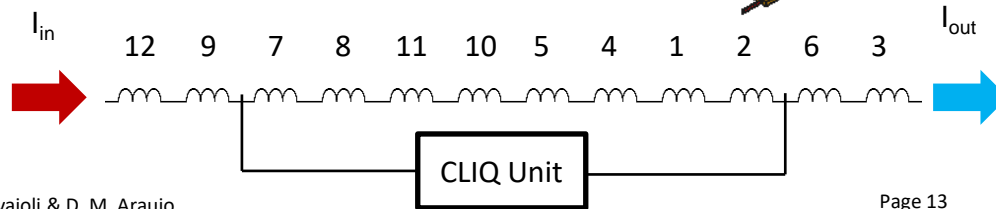
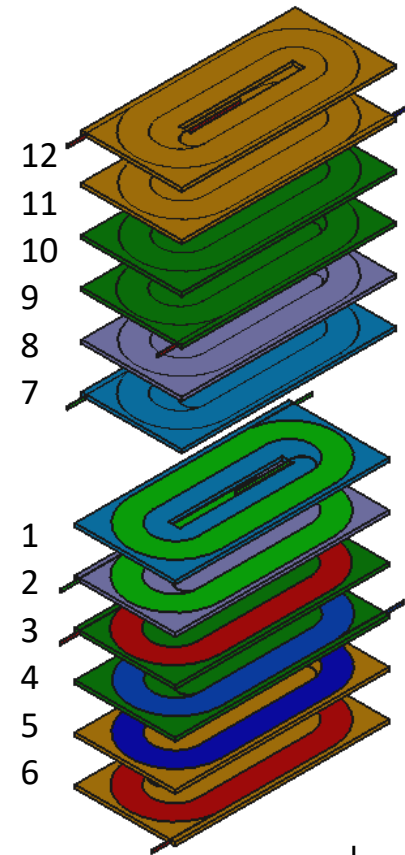
**HF Cable Inner Coils:** layers 1, 7

**HF Cable Inner Coils:** layers 2, 8

**Intra-layer splice:** layers 1-2 and 7-8

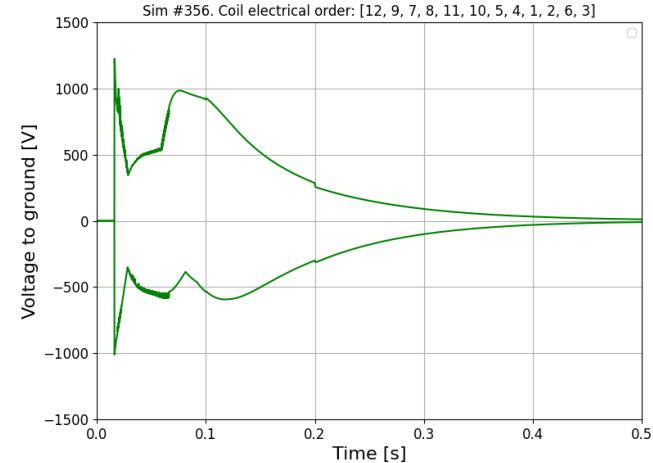
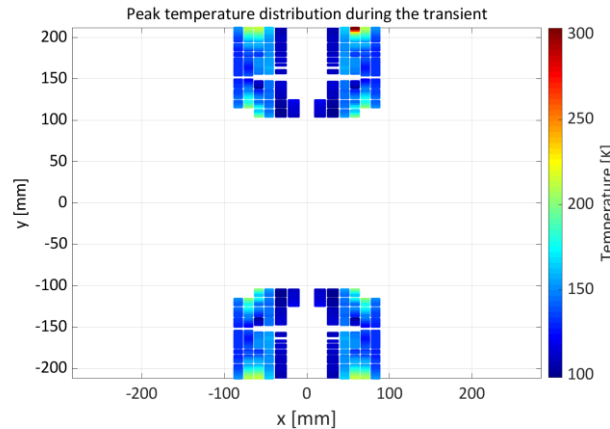
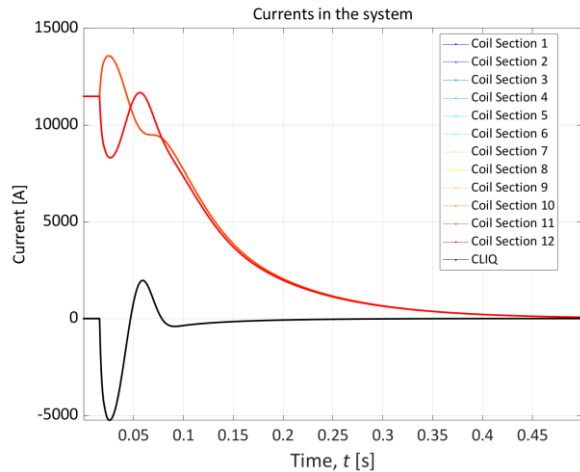
**Intra-layer splice:** layers 3-6 and 9-12

**Intra-layer splice:** layers 4-5 and 10-11





One 50 mF, 2 kV CLIQ unit can effectively protect a 15 m long SMACC magnet.  
Further optimization of the quench protection system in progress.  
All simulations performed with the STEAM-LEDET program.



Peak CLIQ current  
~5 kA

Hot-spot temperature  
~300 K

Peak voltage to ground  
~1250 V

## Progress on the roadmap:

- ... BOX impregnated with filled-wax -> no training
- ... Compression BOX impregnated with filled-wax -> degradation behaviour similar to epoxy
- ... BigBOX, wax impregnated multi-turn coil under background field -> no training
- ... Subscale Stress-Managed Common-Coils (LTS) -> engineering design finalized, procuring the parts

## Introduction of

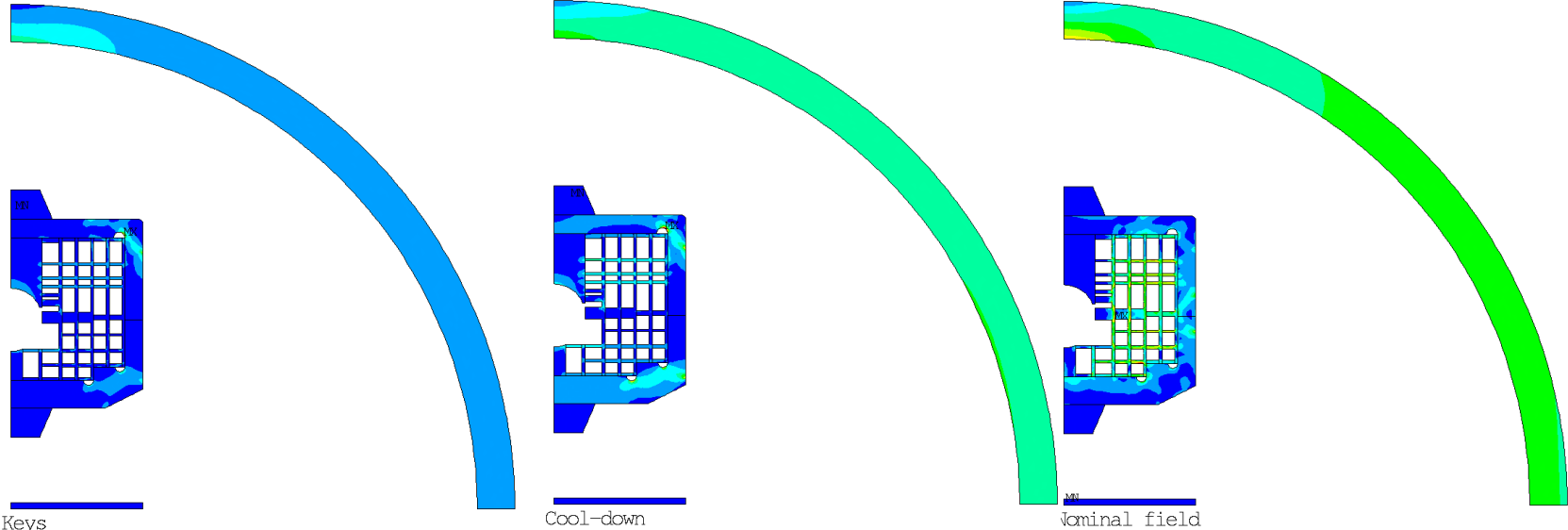
- ... Stress-Managed Common-Coils Concept
- ... Asymmetric Common-Coils Concept

## Interesting SMACC features

- ... Simple geometry (no pole coils) for fully automated coil winding and reduced number of manufacturing steps
- ... Splices on the low-field region -> facilitating grading
- ... Possibly easily implementation of Reaction & Winding technique
- ... Possibly lower-margin operation due to the low stress on high-field regions

## Stainless-steel 316-L components

Von-Mises

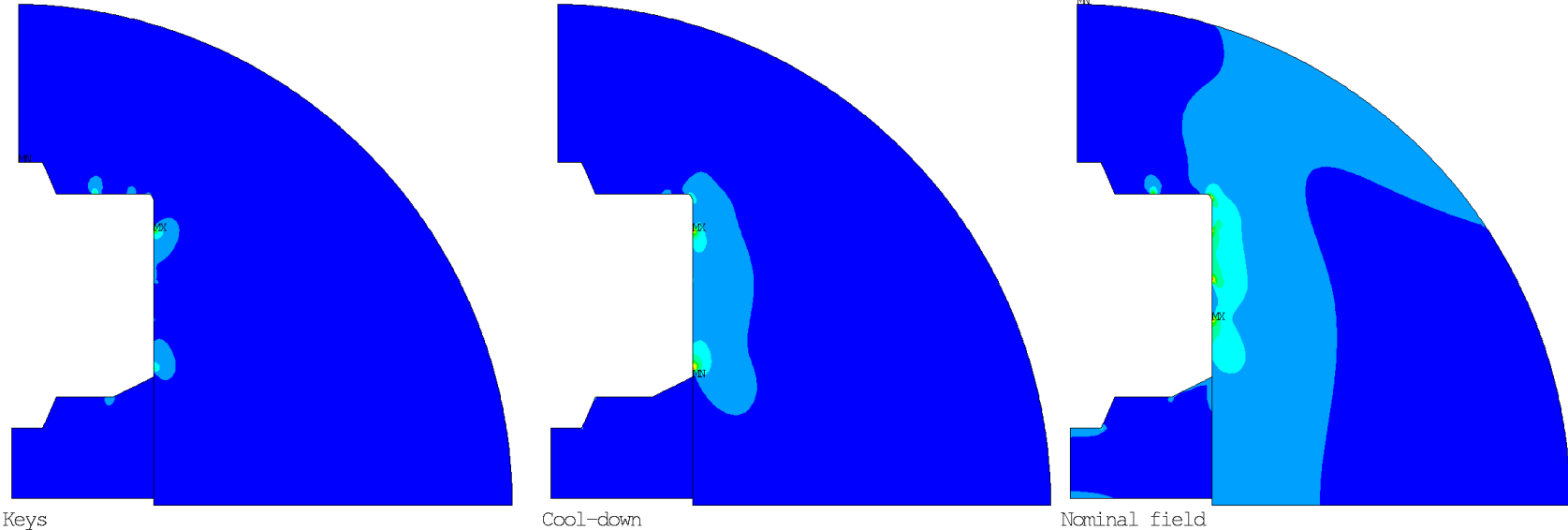


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SMX =.594E+09
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.333E+09
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```

## Magnetic yoke and pole

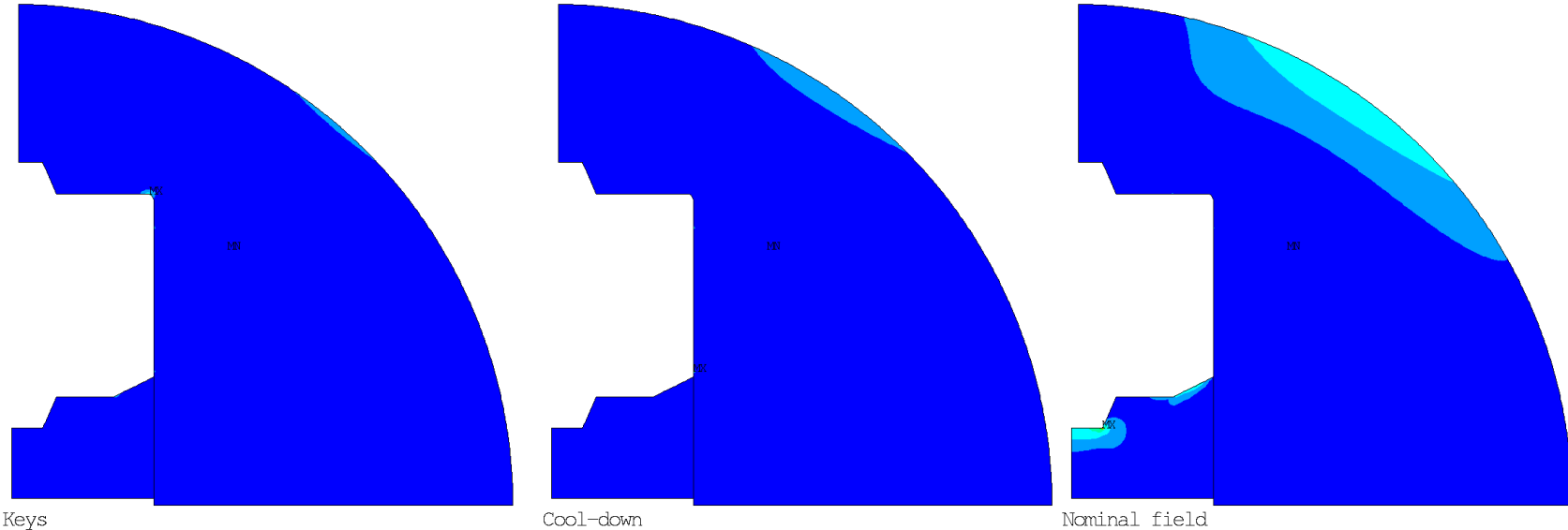
Von-Mises



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.430E+09
```

## Magnetic yoke and pole

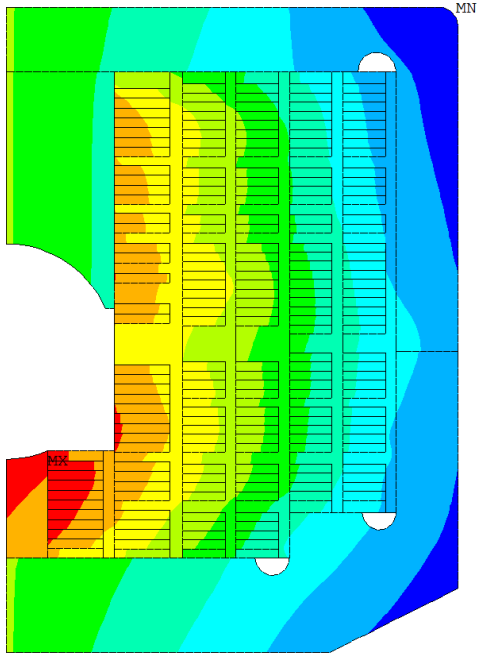
S1



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SMX =.188E+09  
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.222E+08  
.444E+08  
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.133E+09  
.156E+09  
.178E+09  
.200E+09
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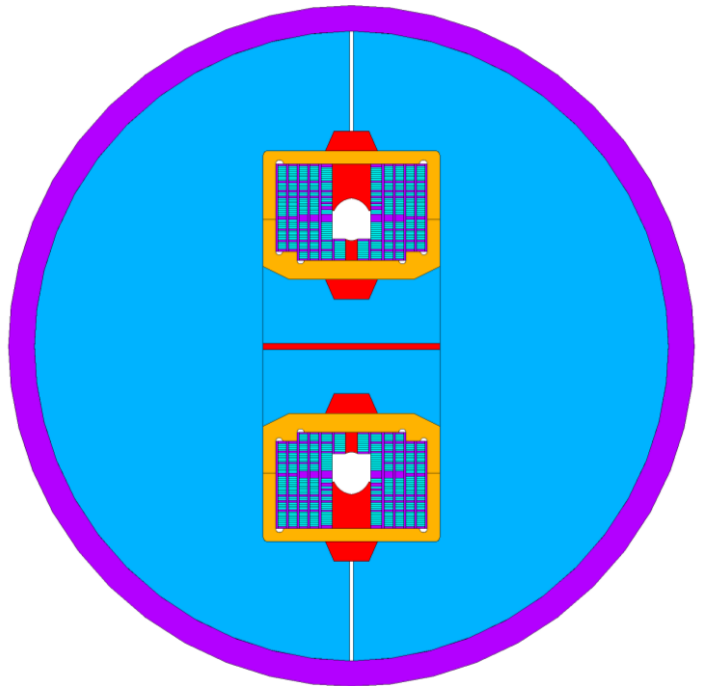
# Displacement at nominal field operation



Nominal field

0.2 mm

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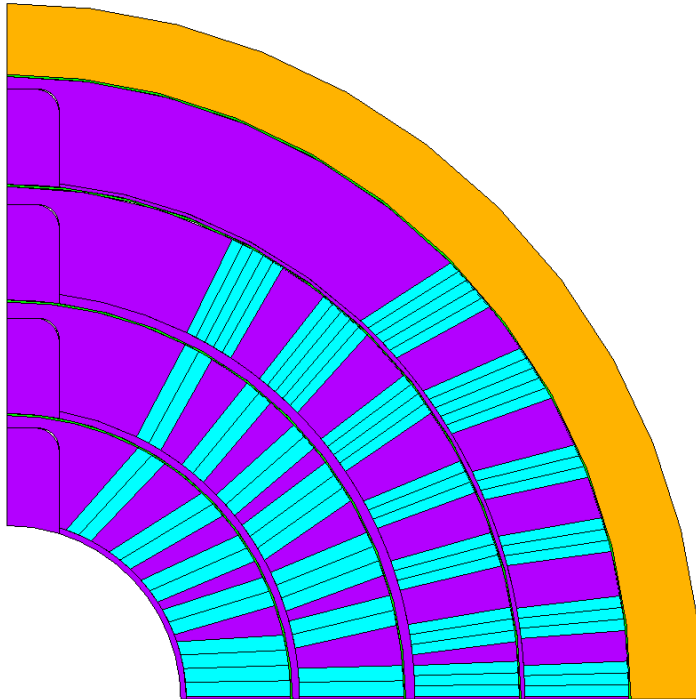


# SM-CT vs SM-CC 1/2: Cable Properties

- **High-field cable** (common coil first layer and pole coils)
  - 28 strands
  - 1 mm strand RRP-150/169
  - Cooper% = 48%
  - Width 14.7 mm and Thickness of 1.8 mm
  - Insulation thickness 155  $\mu\text{m}$
- **Low-field cable** (common coil second layer)
  - 40 strands
  - 0.7 mm strand RRP-108/127
  - Cooper% = 53%
  - Width 14.7 mm and Thickness of 1.27 mm
  - Insulation thickness 155  $\mu\text{m}$
- **Low-field cable** (common coil third and fourth layer)
  - 30 strands
  - 0.7 mm strand RRP-108/127
  - Cooper% = 53%
  - Width 11.02 mm and Thickness of 1.27 mm
  - Insulation thickness 155  $\mu\text{m}$

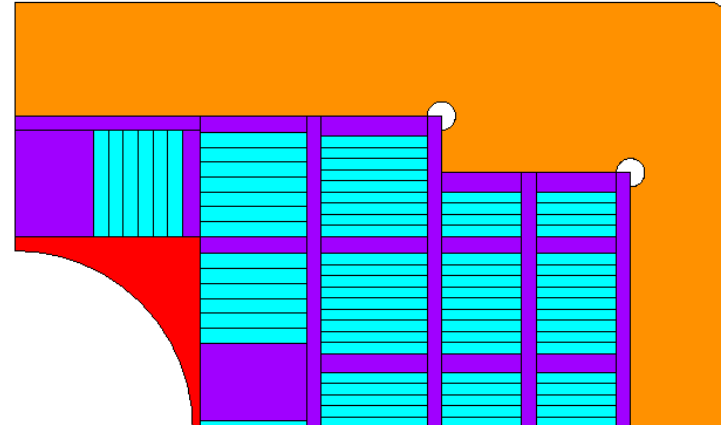
# SM-CT vs SM-CC 1/2: Geometry Comparison

- Stress-Managed Cosine-Theta



- Stress-Managed Common coils

Solution	N turns HF	N turns LF	Total Strand Area
SM-CT	28	48	1355 mm <sup>2</sup> (+ 13.1%)
SM-CC	19.5	53.5	1198 mm <sup>2</sup>



<https://chart.ch/chart-projects/>

ETH zürich

- MagRes
- WireChar
- MagComp
- MagAM
- MagNum

