

# AN FCC-EE VIBRATIONS STUDY FOR ITS MDI

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*7<sup>th</sup> FCC Physics Workhsop*



# Outline

## Introduction and Context

- Our aims
- Interactions between beam physics and mechanical studies

**Mechanical studies: amplification of ground motion by the mechanical structure**

**Physics studies: a study of the ground vibrations**

- Simulation strategy
- Comparison with the analytical model
- A focus on the MDI region
- A specific use of the analytical model for the MDI region

**Conclusions and Perspectives**

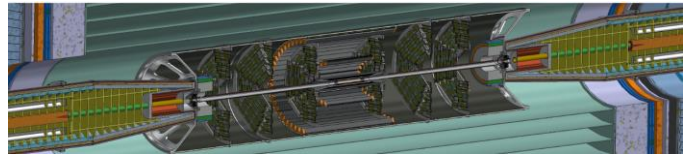


# INTRODUCTION

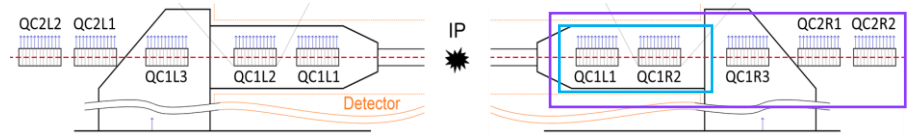
# Why studying vibrations in the MDI of FCC-ee?

## Aims:

- Guarantee a stable collision at the 4 Interaction Points
- Measure the impact of vibrations on luminosity and beam parameters



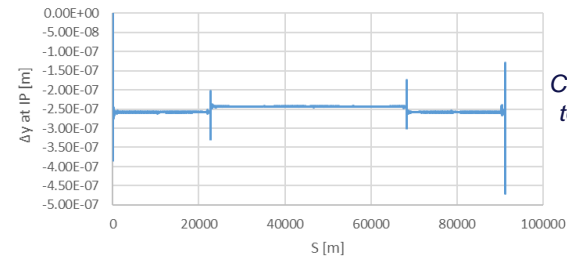
3D plan ongoing (F. Franesini, M. Boscolo et al.)



MDI schematics

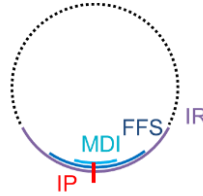
Main constraint: nanometer beam size in the vertical plane

- Quadrupoles in the MDI (even IR) with a very high magnetic field gradient



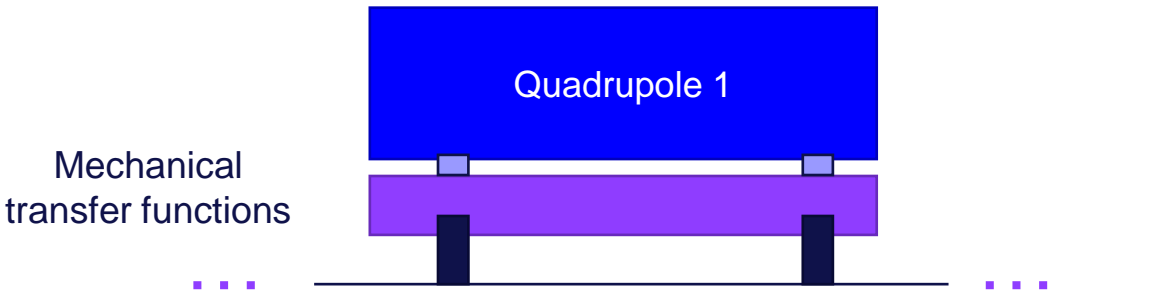
Cumulative vertical contribution to the IP.8 of the quadrupoles along FCC-ee

**In a collider:**  
 IR : Interaction Region  
 FFS : Final Focus System  
 MDI : Machine-Detector Interface  
 IP : Interaction Point



# Some definitions

Vibration: { ground motion amplified by the mechanical structure  
vary with time



Ground motion excitation, based on Plane Ground Waves + cultural noise, environment dependent

3 pillars in vibrations studies:

- Alignment
- Vibration
- Coherence

# Interactions between mechanics and beam physics

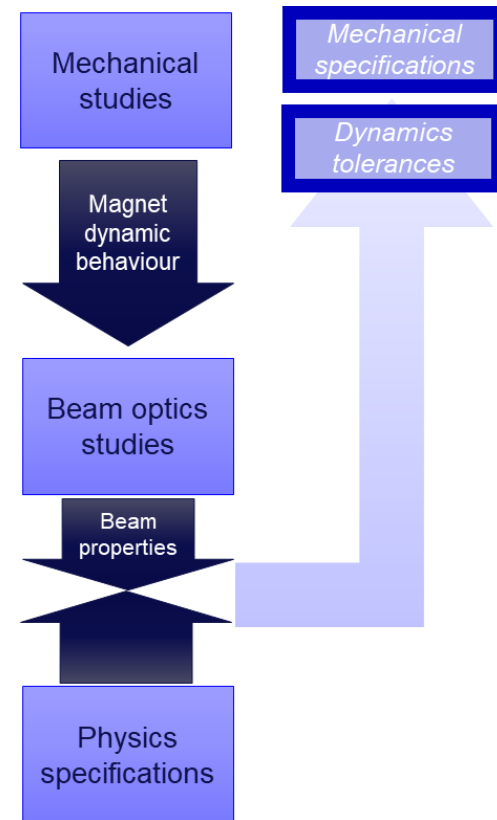
*Aims:* Define vibrations tolerances of magnets in the MDI

Two major contributions:

- Implementation of a **mechanical model** considering the mechanical behaviour (transfer functions) of each magnet
- **Physics simulations** (beam optics) to evaluate the impact of misalignments of these magnets

Iterative work:

- The result of the mechanical study will give input parameters for the physics study, and vice-versa.



# Mechanical studies

Mechanical design of the MDI ongoing



Access to SuperKEKB data, as vibrations sensors placed on the cryostat and the ground, near the Interaction Point



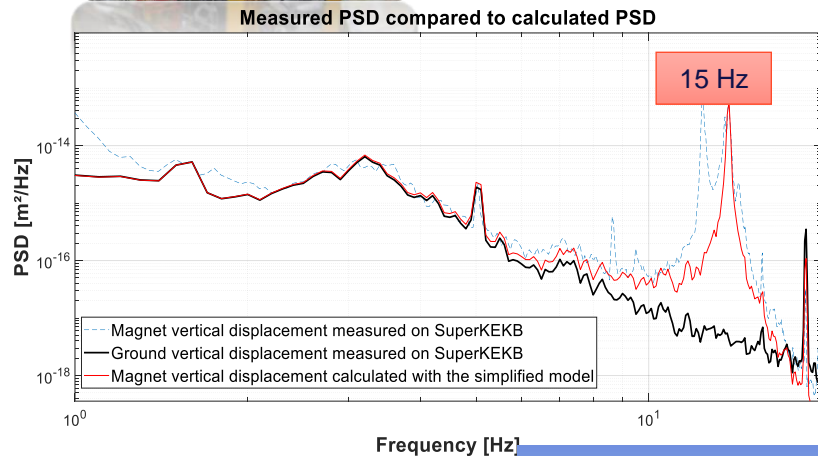
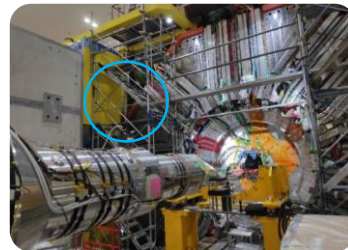
Evaluation of the resonance modes of the cryostat



Design of a simplified mechanical model

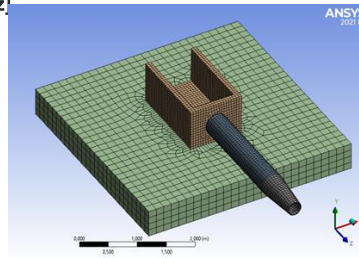


File containing, at MAD-X sampling frequency, the vertical displacements and rotations of the two quadrupoles embedded in the cryostat relative to time ( $\Leftrightarrow$  accelerator turn)



MAD-X Tracking

Ground motion **amplified** by the **mechanical structure**



# Physics studies

**Ground motion** excitation **without** amplification of the mechanical structure (transfer functions = 1)

*Plane Ground Wave model:*

- Vertical misalignment attributed to each beam element  $j$  along the accelerator ring, in terms of **harmonic number**, to be fully independent from the wave velocity:

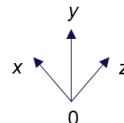
$$\varepsilon(j) = A \sin \left( \frac{2\pi h}{C} (X(j) \times \cos(\alpha) - Z(j) \times \sin(\alpha)) + \varphi \right)$$

- A: amplitude of oscillation
- h: harmonic number
- C: circumference of FCC-ee
- $\alpha$ : wavefront tilt angle
- $\varphi$ : phasing advance

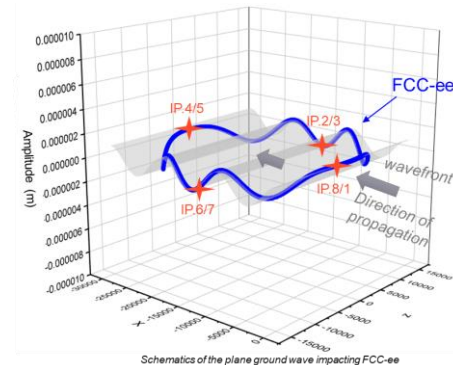
$$h = \frac{cf}{v_{wave}}$$

*In the study,  $f$  varies and:*

- $A_0 = 5 \cdot 10^{-7}$  m
- $C = 91172$  m
- $\alpha_0 = 0$  rad
- $\varphi_0 = \pi/2$  rad



*N.B.:* (0, 0, 0) is taken as IP.8/1.





# Pros and cons of this study

## *Benefits:*

- Study the impact of ground-motion induced vibrations on the whole accelerator
  - With a special highlight put on the MDI area
- Simulate spatial coherence along the ring to quantify the impact on FCC-ee performances
  - So far, impact of these waves never estimated for FCC-ee
- Comparison to SPS, LEP, LHC and HL-LHC possible thanks to previous works
- Help to design building constraints (magnets, supports, hall)

## *Limitations :*

- Beam made out of only one particle, placed on the ideal closed orbit
- Only one beam considered: no beam-beam effect introduced in the simulations
- No multi-turn tracking
- No local nor global correction, as starting from a perfectly aligned lattice
- Sinusoidal plane ground wave

# Simulations procedure

## Computer tools:

- Optics simulations carried out with MAD-X (5.09.00)
- Post-treatment held with Python, thanks to cpyrad module (3.6.9)

## Optics-related matters:

- Z lattice (V22)
- Start of the sequence at IP.1

## Process:

Photography of the accelerator, completely misaligned by the wave  No temporal study

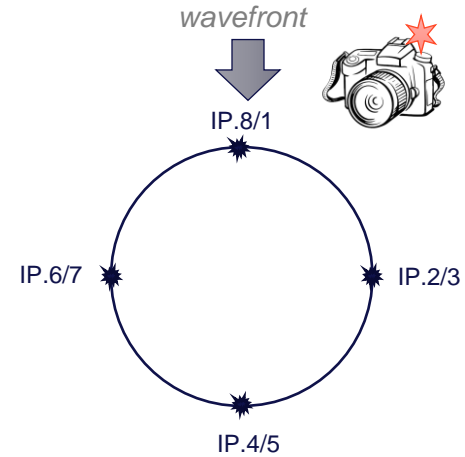
TWISS of the nominal  
sequence



Assigning vertical  
displacements of all elements  
relative to plane ground wave



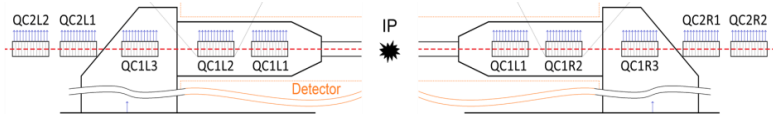
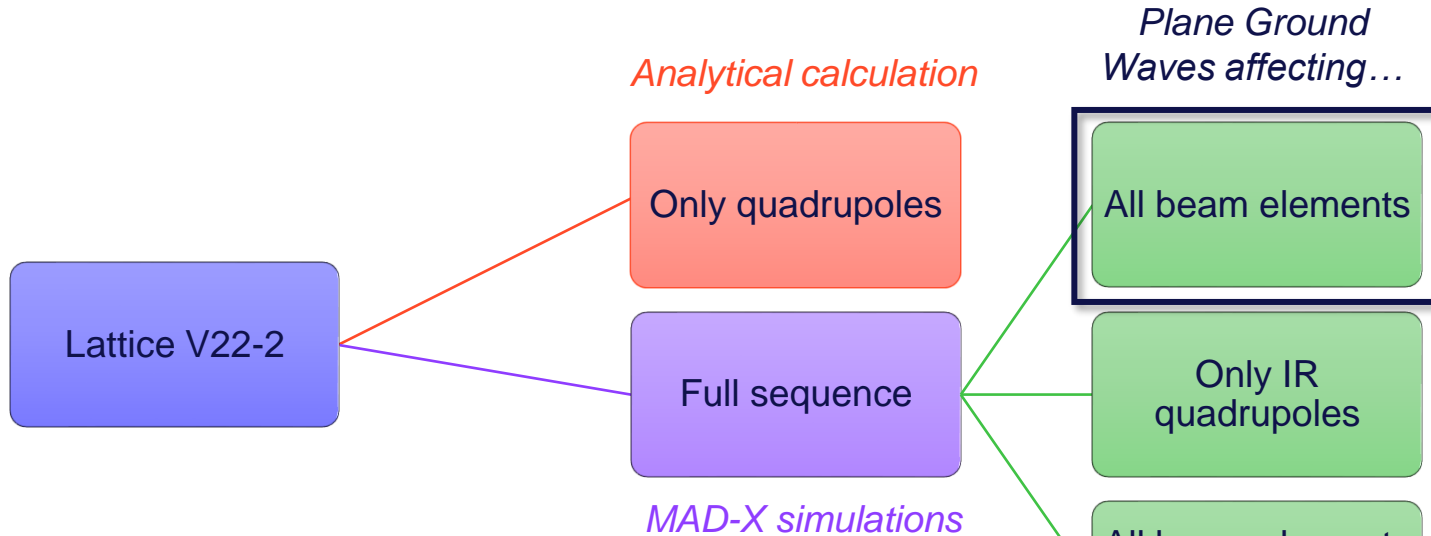
Evaluation of the vertical  
position of the orbit referred to  
the ideal orbit:  $y_{co}$





# STRATEGY OF THE WORK

# Strategy of our work



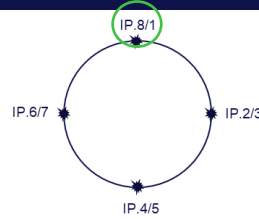
- 5 quadrupoles at each IP side
  - 4 IPs
- } 40 IR quadrupoles



# SIMULATIONS RESULTS

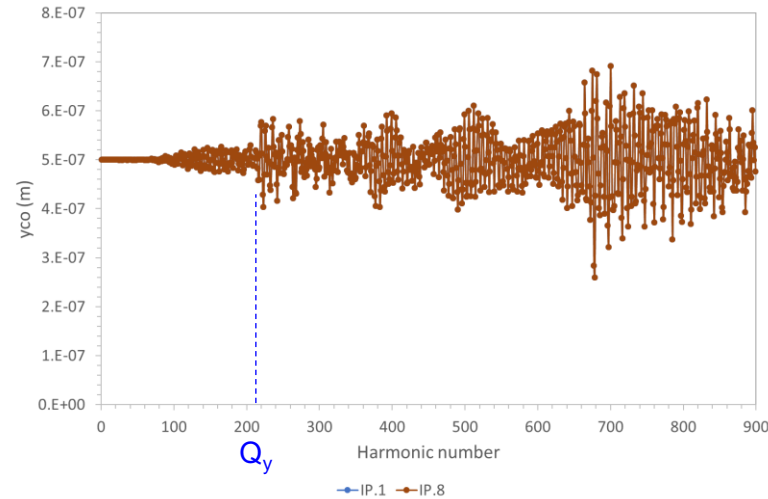
*How does  $y_{co}$  at the distinct IPs look like  
relative to the harmonic number?*

# All beam elements affected by the Plane Ground Wave model



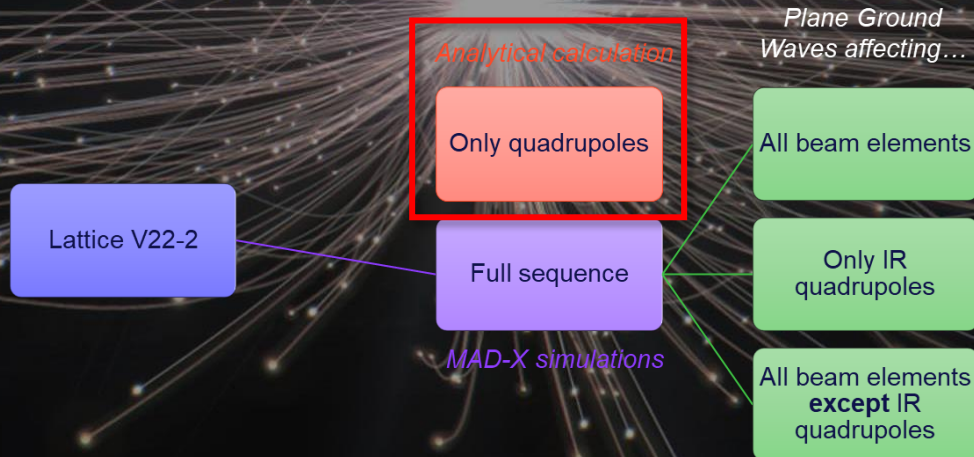
- Yco is evaluated at IP.8, equivalent to IP.1 after one accelerator turn.
- Yco at IP.8 is made out of resonance nodes and antinodes with:
  - a baseline at  $y = A = 0.5 \mu\text{m}$
  - a first oscillation at  $h = Q_y \approx 214$
  - a maximum amplitude of  $0.7 \mu\text{m}$

$$\varepsilon(j) = A \sin\left(\frac{2\pi h}{C}(X(j) \times \cos(\alpha) - Z(j) \times \sin(\alpha)) + \varphi\right)$$



Study **dependent** of the **wavefront** location and inclination angle, as considered in the equation  
The work here focuses on yco @ IP.8.

# COMPARISON TO THE ANALYTICAL MODEL



# Definitions of the analytical model

- The sequence used to solve analytically the Plane Ground Waves study **only** considers **quadrupoles** (1856 in total).
- Each misalignment of quadrupole  $\varepsilon$  generates a dipole kick  $\delta$ :

$$\delta = kl\varepsilon$$

$k_i$ : normal quadrupole coefficient ( $\text{m}^{-2}$ )  
 $l$ : effective length of the quadrupole (m)

- The  $i^{\text{th}}$  dipole kick creates a vertical perturbation  $yco_i$  of the closed orbit:

$$yco_i = - \sum_{j=0}^n \frac{\sqrt{\beta_i \beta_j}}{2 \sin(\pi Q_y)} \cos(\pi Q_y - 2\pi \Delta \mu_{ij}) \times \delta_j$$

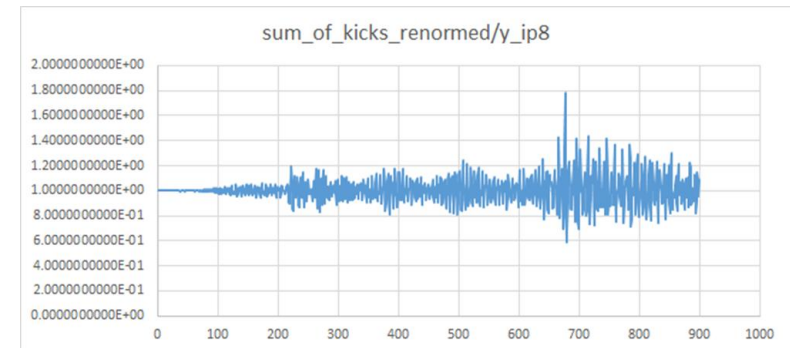
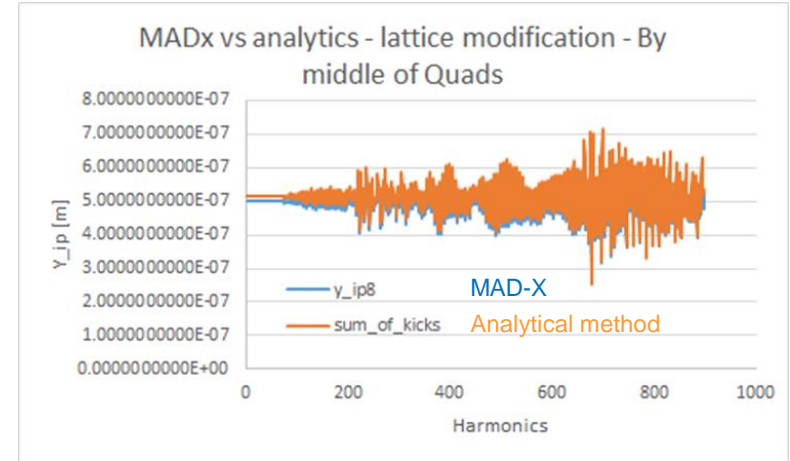


# Comparison between MAD-X and the analytical method

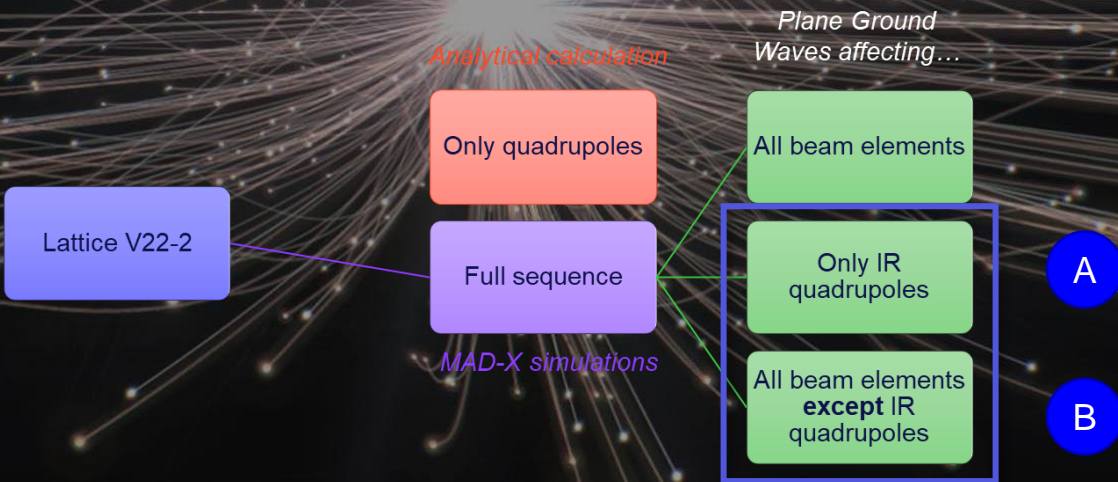
- The two methods are **very consistent**.
- The first oscillation at  $h=214$  corresponds to the FCC-ee vertical tune.
- There is a small **offset**:
  - At  $h = 1$ : 2,8 % of difference
  - Offset not constant relative to  $h$

## ➡ Slight difference of **definitions**

- $\beta$  functions used in the analytical method are defined at the centre of each quadrupole, and thus are higher than defined at the exit of the beam elements (MAD-X)
- It has been checked that other beam elements than quadrupoles do not contribute to this offset



# HIGHLIGHT ON IR QUADRUPOLES



# Case A:

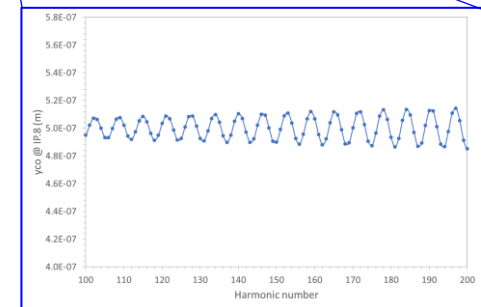
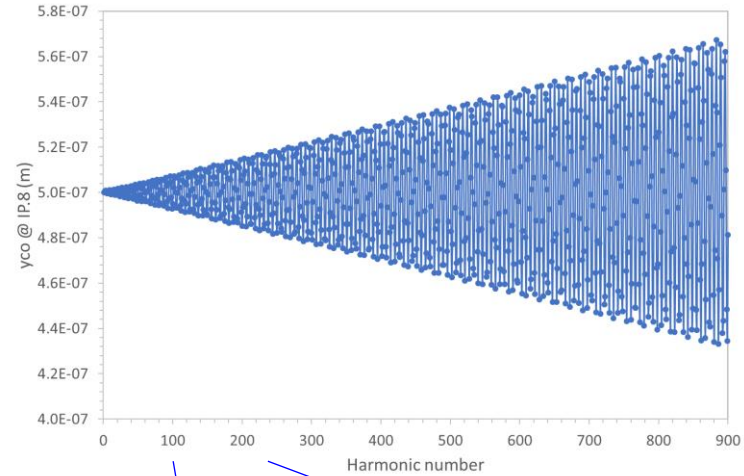
*If only IR quadrupoles were affected by the wave*

Definition of IR quadrupoles:

- 5 quadrupoles at each IP side
  - 4 IPs
- } 40 quadrupoles

- Yco at IP.8 has the following parameters:
  - Baseline at  $y = A = 0.5 \mu\text{m}$
  - Periodic structure relative to  $h$ :  $T_{yco} = 7 [h]$
  - No specific contribution at  $h = Q_y$

➔ **Linear contribution** of IR quadrupoles

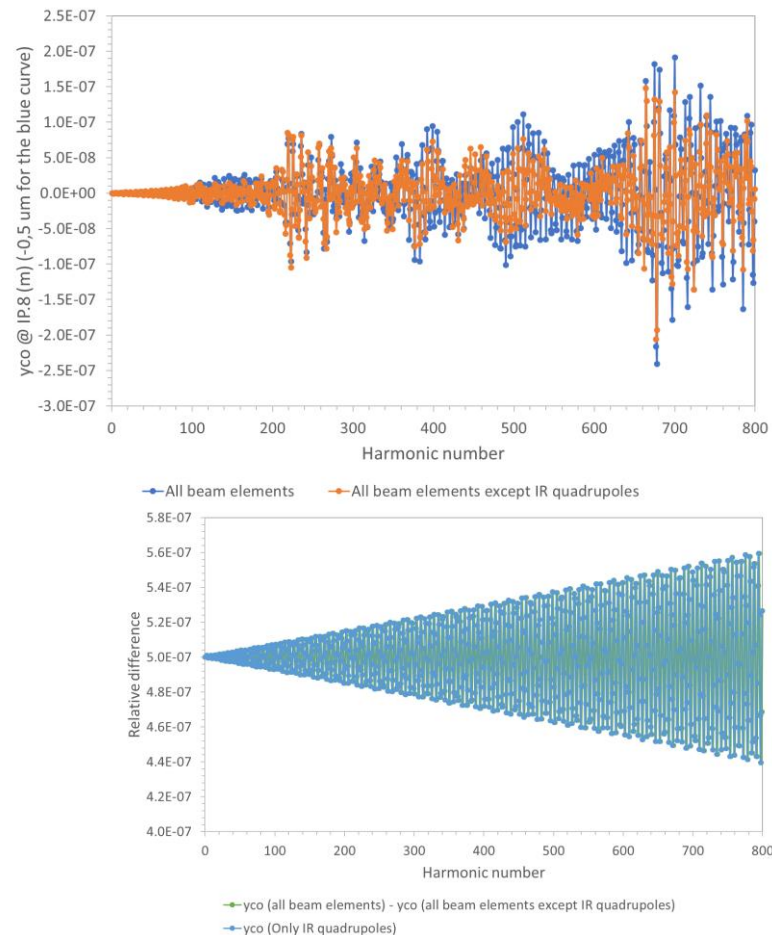


## Case B:

*If all beam elements except IR quadrupoles were affected by the wave*

- Yco @ IP.8 is similar to the case where all beam elements are impacted by the wave:
  - Correction by the maximum amplitude of the wave
  - Contribution of IR quadrupoles is the difference between the two plots (*green plot*)
- **Exact same values** as in the case where only IR quadrupoles are affected by the wave

➡ Estimate of **spatial coherence** (wavelengths longer than the MDI total length), not a study of vibrations impact



# To go beyond the Plane Ground Wave model

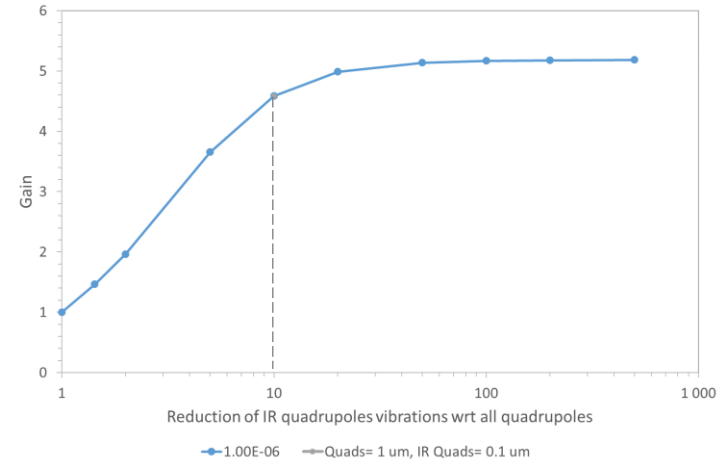
- No plane wave in this case!
- Analytical method:
- “Vibrations” model:
  - Random vertical displacements of the quadrupoles, following a gaussian distribution
  - 1000 seeds

$$yco_i = - \sum_{j=0}^n \frac{\sqrt{\beta_i \beta_j}}{2 \sin(\pi Q)} \cos(\pi Q - 2\pi \Delta \mu_{ij}) \times \delta_j$$

$$Gain = \frac{\sigma_{y_{o\_m d i}}}{\sigma_{y_{o\_a l l}}}$$

$\sigma_{y_{o\_m d i}}$  Corresponds to the std of the vertical position of the beam at IP8 when the IR quads vibrate less (by a reduction factor)

$\sigma_{y_{o\_a l l}}$  Corresponds to the std of the vertical position of the beam at IP8 when the vibration is the same for all quads (here taken as the reference)  $1 \mu\text{m}$



➔ If the “vibrations” in the IR region are reduced by a factor 10 compared to the rest of FCC-ee, the vertical closed orbit is **≈ 5 times closer** to the nominal one. It **tends** to this numerical value, even though the IR vibrations are lowered. In the case of QC1 vibrations (3 quadrupoles), the maximum gain is equal to 2.

➔ First answers given to a vibrations model regarding the **intrinsic optics** functions of FCC-ee ( **$\beta$  functions**)



# CONCLUSIONS AND PERSPECTIVES

# First conclusions and outlook

- Investigation of the effect of a plane ground wave on the whole FCC-ee accelerator
  - Photography of the misalignments taken, no tracking yet
- MAD-X simulations and the analytical method are giving the same results
  - Checks done to establish the reliability of the method
- The analytical method can be used as a fast scanner
- Flexible, adaptable and tunable methodology, to highlight:
  - The Machine Detector Interface,
  - But as well, other parts of the accelerator, such as the arc-cells

## *Perspectives:*

- Parametric study to test the influence of all definition parameters (inclination, phase advance)
- Comparison with other FCC-ee lattices (V23, LCCO)
- Towards more realistic waves models:
  - Injection of coherence measurements made at other accelerators (SuperKEKB,...)
  - Wave speed(s) definition



Thank you  
for your attention!





# APPENDICES

