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Technical requirements

and engineering design

of the RF structures

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> Two-beam acceleration:

- which components are needed and what do they stand for.

> The main requirements:

- beam requirements;
- RF design.
- shape accuracy;
- tolerances and surface quality;
- systems

Mechanical design:

- RF structures prototypes;
- engineering issues
- what will be required for the final CLIC RF structures









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The CLIC two-beam RF network includes the standard X-band rectangular waveguides connecting PETS, AS and other supplementary devices such as choke-mode flange (CMF), Hybrid, high-power load, splitter and WFM.



Waveguide length optimization is based on losses, phase advance and RF to beam timing considerations.

The power transmission without electrical contact between two beams, and also MB and DB independent alignment is getting possible with CMF. The Hybrid provides the power to two adjacent AS. The RF load is attached to one of the hybrid ports to avoid the RF reflection to the corresponding PETS. The RF splitters are used to equally feed the AS.

Requirements:

tolerance on RF phase change between DB and MB: **± 0.12 deg**

WG interconnections between PETS and AS via CMF:

X – shift: ± 0.25 mm, Y ± 0.5 mm, Z ± 0.5 mm, Twist: < 5°







The micrometer tolerance level is required for the structure components production and a few micrometers for the structure assembly in order to fulfil very stringent beam dynamics requirements.

Phasing: an error in the cell shape determines a wrong phase advance \rightarrow inefficiency in acceleration

Mismatching: a geometrical error introduces a power reflection \rightarrow lower efficiency.

Assembly: bookshelf \rightarrow introduces the transverse kick which is proportional to the accelerating gradient; longitudinal misalignment of half-structure



Structure in disks. Problem mainly for the brazing/bonding (assembly)



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Tolerances study. Summary table.



			Cause								
Item	Effect of the item	Performance	Mach.	Assem.	Align.	Oper.	Solution	Magnitude of tolerance	Criticality	Comments	Scheme
SHAPE											
Shape of an Iris	dephasing	lower efficiency	x				Tuning	± 0.001 mm	\mathbf{V}_{high}	local	1
Shape of the matching Iris	mismatching	lower efficiency	x				Tuning	± 0.001 mm	V high	local	2
LONGITUDINAL											
Expansion due to heat dissipation	dephasing	lower efficiency				x	Thermal elongation compensated (isotropic)	± 0.005 mm	low	thermal elongation	3
Tilt of the disks (Bookshelf)	transverse kick	RF induced transverse kick	x	x			Vertical V- block assembly	± 18 mrad **	$\checkmark_{\scriptscriptstyle \mathrm{high}}$	bookshelf	4
TRANSVERSE											
Relative position of disks	wakefield	beam induced transverse kick	x	x			V-block assembly	± 0.005 mm **	1ow	alignment problem	6
Peak of magnetic field on surface	magnetic field *	local temperature rising	x	x			***	***	low	local	
Expansion due to unsymmetrical heat dissipation	wakefield	beam induced transverse kick				x	Symmetric deformation design	± 0.005 mm	$\checkmark_{\scriptscriptstyle \mathrm{high}}$	bending	5
Thermal isotropic expansion	dephasing	lower efficiency				x	Very accurate water temperature control	± 0.1 ° C	$\checkmark_{\scriptscriptstyle \mathrm{high}}$	variation of the structures	10
Supporting of accelerating structure	wakefield	beam induced transverse kick	x	x	x		Accurate reference interfaces in structures	± 0.005 mm	low	structure axis w 1to beam axis	9
TILT											
Tilt of the full structure	transverse kick	RF induced transverse kick			x		Reference points in the structures	± 0.03 mrad	low	tilt of full structure	7
Deformation of support	transverse kick	RF induced transverse kick				x	Active cooling system	± 0.03 mrad	low	support interference	8

Courtesy of R. Zennaro

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Iris shape description

Iris parameters			Cell parameters0.5					Other parameters:
Iris#	a [mm]	d [mm]	Cell #	b [mm]	c [mm]	l [mm]	eow	r pipe = 1 mm
1	3.15	1.67	0		0.65	6.66	3.4	r_pipe = 4 mm
2	3.1192	1.6442	1	8.6154	0.6269	6.6749	3.3962	l pipe > 10 mm
3	3.0885	1.6185	2	8.6035	0.6208	6.7007	3.3885	N = 26 – regular cell numbe
4	3.0577	1.5927	3	8.5917	0.6146	6.7264	3.3808	h = 8.332 mm - period
5	3.0269	1.5669	4	8.5801	0.6085	6.7522	3.3731	r = 0.5 mm
6	2.9962	1.5412	5	8.5687	0.6023	6.778	3.3654	s = 0.1 *d
7	2.9654	1.5154	6	8.5575	0.5962	6.8037	3.3577	e = 1+(d/h)/(a/2.625mm)
8	2.9346	1.4896	7	8.5465	0.59	6.8295	3.35	idw = 8 mm
9	2.9038	1.4638	8	8.5357	0.5838	6.8553	3.3423	adw = 11 mm
10	2 8731	1 //381	9	R 2221	0 5777	6 881	3 33/16	ldw = 40 mm







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UNDAMPED WG DAMPING **RADIAL CHOKE DAMPING** DISK DISK QUADRANT (HALF) HALF (QUADRANT)





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AS cell iris - the most critical area





 \star - Evaluation length is equal to (d-2 \star be) mm Roughness is according to ISO 1302

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MeChanlCs Meeting

tolerances & surface quality



Test structures



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Different mechanical design approaches



The design of AS is driven by extreme performance requirements. The assembly accuracy is $\pm 5 \ \mu m$. Many features of different systems, such as vacuum, cooling, WFM as well as damping waveguide absorbers are incorporated into design.



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COMPLEXITY

Brazed disks with "compact" coupler & vacuum system, micro-precision assembly, cooling circuits (~400 W per AS), wakefield monitor (1 WFM per SAS), interconnection to MB Q (stabilization!), structure support (alignment), output WG with RF components (e.g. loads), RF distribution (WGs & splitters)





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Assembly of AS (3/3)







Two AS (~250 mm) form one Super-AS (~500 mm)



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CLIC PETS is one of the key components in the CLIC two-beam acceleration scheme. It is a passive microwave device, in which bunches of the DB interact with the impedance of the periodically loaded waveguide and generate RF power for the AS (MB).







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PETS body is composed of eight identical parts, octants. The copper octant has a wedge-shaped cross-section profile, while the narrow side of octant has the corrugated RF geometry. Each octant is damped with SiC shim attached to the lateral surfaces.

The compact coupler combines three functions: transferring RF power to the AS, connecting two PETS and cutting the produced power by means of integrated "On-Off" mechanism, momentary (<20ms) changes which the geometry of the waveguide.





PETS octant



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Shape accuracy 15 μm Roughness Ra 100 nm







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Mechanical design must take into account all requirements of beam physics, RF design, production and assembly methods, as well as installation and operation.

Stringent tolerances imply the precise and ultra-precise machining procedures, including also special pre- and intermediate heat treatments.

CLIC structures combine many features of different technical systems, so lots of additional engineering issues have to be solved.

Industrialization studies are going in parallel in collaboration with manufacturers and modifications expected to be implemented "on fly".

Specific requirements for packaging, transport and for the control procedures

CLIC at 3 TeV (20924 modules) would require:

- \rightarrow 142812 Accelerating structures;
- \rightarrow 71406 PETS, and
- ightarrow about 400000 RF components







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Many thanks to all mechanical designers and CLIC Module Working Group members !









Due to the very large amount of structures the implementation of tuning in the final design is not suitable, for this reasons the tolerances are defined on the assumption to avoid any possible tuning. A detailed study of the required machining and assembly tolerances has been performed [8] which is summarized below.

•Systematic errors: Inefficiency in acceleration due to rf de-phasing is mainly caused by systematic errors in the cell dimensions since it is a coherent effect. The most sensitive dimension is the transverse size of the cell 2b where 1 micrometer systematic error causes ~2% reduction in the structure acceleration.

• Random errors: Cell to cell frequency error due to random errors in cell dimensions causes mismatch, reflections and appearance of field enhancement due standing wave. Limiting the mismatch to < -40dB results in the same tolerance on the most critical dimension 2b of ~1 micrometer.

• "Bookshelfing": Systematic tilt of the disks introduces the transverse kick which is proportional to the accelerating gradient. Keeping ratio of the transverse kick to the acceleration dVt/dVz <10e-4 (see, BD section) requires the tilt to be below 180 micro-radian.

•WFM: The required WFM accuracy must be below 3.5 micrometers. This sets the limit on the cell shape accuracy such that the transverse alignment of the axis of the iris aperture (source of the short range wakes) with respect to the axis of the cell and damping waveguides (measuring the wakes) must be at least better than 3.5 micrometers.

In summary, micrometer tolerance level is required in cell disk fabrication and several micrometers in the structure assembly in order to satisfy stringent beam dynamics requirements without additional tuning.







Machining and joining



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Turning vs. milling







Diffusion bonding (vacuum vs. hydrogen environment)

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