

Status of the development of miniHV at Nikhef

Small HV modules dedicated to gaseous detectors for laboratory use



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Why developing HV power supplies?

- Getting a HV supply that is dedicated for gaseous detectors
 - Fast trip in nA region
 - Accurate current measurement in nA region
 - Small unit, not too expensive
 - Fast remote control
 - Gently ramping to target voltage
- In addition, for large scale HEP experiments, one would like having these units close to the detectors in the hot region
 - Non-magnetic
 - Minimal mass
 - Radhard
 - Low noise emittance



Aiming for two designs

1. MiniHV for use in the lab, testbeams etc

- Practical in use, relatively small, not completely antimagnetic
 - But **NO** inductors, transformers

2. MicroHV for use near the detectors in a big experiment

• Very low mass, non-magnetic, radhard (until 1000 Mrad/ 10⁷ Gy)



Philosophy of Nikhef miniHV

- Generally HV power supplies make use of feedback by voltage divider circuit
 - => quiescent current of $10 100 \,\mu A$
- With Nikhef miniHV no feedback by voltage divider
 - But by dummy Cockcroft-Walton cell
 - Additional compensation from measured output current
- => trip and output current measurement in nA region
- Bleeder circuit using high ohmic resistors (180 GΩ total) for HV signaling
 - => $I_{\text{quiescent}} < 6 \text{ nA}$
 - Used for HV indication by an LED
 - (Not suited for voltage regulation)

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Fred Haı

Voltage regulation

- Regulation by analogue input voltage (0 60V)
- Voltage feedback
 - Via single Cockroft Walton circuit
 - Current compensation by local microprocessor



Configuration

- Up to 10 HV units connected to single power supply unit
- Only connected by CAN bus
 - Power supply lines incorporated (+/- 12 V; 60 V)
- CAN interface needed (National Instruments or KVASER)
- CAN bus ends in passive terminator



Specs of miniHV, version 2





- Completely controlled by local microprocessor
- Initially linear, followed by exponential approach to target voltage, fully configurable
- Containing minor magnetic parts from electronics
 - expected to operate in magnetic field
 - Supply box is NOT antimagnetic





Ramping scheme

Ramp-up at speed=500 for different linear/exponential percentages





Two different trip actions

• Warning limit (nA) in $0 - 65 \mu A$

Action: warning message is sent

- **Trip** limit (nA) in $0 65 \mu$ A
 - Actual trip only after certain number of overcurrent events (0 – 255)
 - => reaction time depends on frequency of the control loop of the local processor
 - Example: $2 \text{ Hz} \Rightarrow 0.5 128 \text{ s}$

Action: HV supply current is set to zero

(no active pull down to zero, the pull down current has to be provided by the detector itself)

Manufacturer-Specific Profile Area							
Index (hex)	Sub Index	Description	Data/ Object	Attr	Default	Comment	

2001		High-Voltage control loop	Record			
		parameters				
	0	Number of entries	U8	RO	7	
	1	Control loop enabled	Bool	RW	0	= 1 at power-up if module is
		_				calibrated
*	2	Control loop interval	U8	RW	50	In units of 10 ms, must be > 10
*	3	Output current warning limit	U16	RW	0	In nA $(0 = not enabled)$
*	4	Output current trip limit	U16	RW	0	In nA $(0 = not enabled)$
*	5	Current limit count	U8	RW	1	If number of consecutive samples
						exceeding the limit reaches this
						count action is taken
						(e.g. Emergency message, trip),
						must be > 0
*	6	Constant p in logarithmic	U8	RW	20	Factor is elog(1+Iadc/p)[V]
		factor for current compensa-				
		tion				
	7	Constant q	U8	RW	0	Currently not used
		-				
	1					

CANopen Object Dictionary prepared

v1.0 17-Feb-2011 miniHV software Software for miniHV a high-voltage powersupply module with CANopen interface user manual & reference version 1.0 NI Henk Boterenbrood NIKHEF, Amsterdam 17 February 2011 1

Manufacturer-Specific Profile Area						
Index (hex)	Sub Index	Description	Data/ Object	Attr	Default	Comment
		-				
2000		High-Voltage parameters	Record			
	0	Number of entries	U8	RO	13	
	1	Set output voltage [V]	U16	RW	0	Maximum possible is set in Object 2000, sub 8
	2	Set output voltage [V] directly	U16	RW	0	No ramping done if setting is lower than current setting (e.g. for fast HV switch-off)
	3	Output voltage [V]	U16	RO	0	Vout = $((a/100)*V_{adc} + b - c*I_{adc} - log(1+I_{adc}/p))/1000$
	4	Output current [pA]	I32	RO	0	Iout = $e^*I_{adc} + f - I_{bleeder}$
	5	Bleeder voltage [V]	U16	RO	0	High-voltage output according to bleeder resistance and current, Ob- jects 2000, sub 6 and 2010, sub 8
	6	Bleeder current [pA]	U16	RO	0	
*	7	Ramp speed [mV/s]	U32	RW	0	If != 0 ramp speed is taken into account; in mV per second, as- suming Vout = (m/100)*DAC + n Equivalent to Object 2500, sub 2
*	8	Maximum allowed output voltage [V]	U16	RW	1020	Maximum high-voltage output allowed (must be ≤ fullscale in OD 2020)
	9	HV voltage calibrated	Bool	RO	0	= 1 if voltage output has been cali- brated
	10	HV current calibrated	Bool	RO	0	= 1 if current output has been calibrated
*	11	Bleeder resistor installed	Bool	RW	1	
	12	Temperature sensor reading [°mC]	I32	RO		The ADC input connected to the onboard temperature sensor is read out and converted to mil- lidegrees centigrade
*	13	T-sensor data in TPDO	Bool	RW	0	If = 1, DAC value in TPDO1 replaced by temperature

Existing control software



Preliminary performance

Actual voltage measured with electrostatic voltmeter (readout lc 1 V)

Voltage stability $(0 - 5 \mu A)$: ~ 5 V

Output voltage vs output current of Nikhef MiniHV version 2 Feedback loop active



Output voltage vs output current of Nikhef MiniHV version 2 Feedback loop active



• 5 miniHVs are operational

- Only for Nikhef use
- 20 miniHVs in preparation
 - Expected to be finished mid May 2011
 - Partly for Nikhef use
 - Price not yet fixed, but ~ € 1200
 + 19% VAT (Europe)
- 10 modified power supply units in development (connected to line ground)
 - Expected to be finished July 2011
 - Price not yet fixed, but ~ € 400
 + 19% VAT (Europe)
- In addition a CAN interface is needed (National Instruments or KVASER)
 - ~ € 300

Send me an email if you're interested

F.Hartjes@nikhef.nl

Prices, availability



Ideas for other miniHV modules

- 1. -2000 V version
 - Different CW PCB but same housing
- 2. Single MiniHV with ~ 7 outputs (-6000 V?) from Cockroft Walton circuit for triple GEM
 - Regulating GEM voltages by selecting the desired CW stage
 - steps of $\sim 50V$
 - But whole chain may be finely tuned
 - Advantage
 - Getting rid of voltage divider chains or multiple cascaded HV units
 - Low trip levels possible (nA region)
 - No current from voltage divider chain
 - **Problem**: how to handle possible **pull up currents**

Send me an email if you're interested in one of these ideas F.Hartjes@nikhef.nl



Conclusions

5 units Mini HV version 2 (-1000V) now completed and operating well

20 units + power supplies available after summer, partly for groups outside Nikhef
 But a new series can be started at sufficient interest

Positive output possible but needs additinal work (modified cascade board)

-2 kV version well possible but also new cascade PCB required
 Not yet designed, will only be considered at sufficient interest

Possible future developments

More outputs and higher voltage (-6 kV)

• GEM grids

■ => bit larger housing

Not yet designed, will only be considered at sufficient interest

More info about mini HV on web page

http://www.nikhef.nl/pub/departments/et/high_voltage/index.html