

Accelerator Physics Lecture 9: Momentum Effects

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Curvilinear Co-ordinates

- (x, y, s) , often called the standard co-ordinate system in accelerator physics
- The origin is defined by the vector $\vec{S}(s)$ following the ideal reference path
- $x = r \rho$ $s = \rho \theta$
- $X = r \sin \theta = (\rho + x) \sin \theta$, $Y = y$, $Z = r \cos \theta = (\rho + x) \cos \theta$

Transverse Equation of Motion - 1

• Start with the basics

$$
F_x = m \frac{d^2 r}{dt^2} - \frac{m v^2}{r}
$$

= $m \frac{d^2 (x + \rho)}{dt^2} - \frac{m v^2}{x + \rho} = -eB_y v$ (1)

• Factorise the equation

$$
m\frac{\mathrm{d}^2x}{\mathrm{d}t^2} - \frac{mv^2}{\rho} \left(1 + \frac{x}{\rho}\right)^{-1} = -eB_yv\tag{2}
$$

• Utilise the binomial approximation

$$
m\frac{\mathrm{d}^2x}{\mathrm{d}t^2} - \frac{mv^2}{\rho} \left(1 - \frac{x}{\rho}\right) = -eB_yv\tag{3}
$$

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Transverse Equation of Motion - 2

• Replace t with s and rearrange

$$
mv^{2}\frac{d^{2}x}{ds^{2}} - \frac{mv^{2}}{\rho}\left(1 - \frac{x}{\rho}\right) = -eB_{y}v
$$
 (4)

$$
\frac{d^{2}x}{ds^{2}} - \frac{1}{\rho}\left(1 - \frac{x}{\rho}\right) = -\frac{eB_{y}}{mv}
$$
 (5)

• Consider small displacements in x

$$
\frac{\mathrm{d}^2 x}{\mathrm{d}s^2} - \frac{1}{\rho} \left(1 - \frac{x}{\rho} \right) = -\frac{e}{mv} \left(B_0 + x \frac{\partial B_y}{\partial x} \right) \tag{6}
$$

Transverse Equation of Motion - 3

• Set field gradient,
$$
g = \frac{\partial B_y}{\partial x}
$$

$$
\frac{\mathrm{d}^2x}{\mathrm{d}s^2} - \frac{1}{\rho} \left(1 - \frac{x}{\rho} \right) = -\frac{eB_0}{mv} - \frac{exg}{mv} \tag{7}
$$

This is a modified Hill's equation

• Consider small momentum offsets $\Delta p = p - p_0 \ll p_0$

$$
\frac{1}{p_0 + \Delta p} = \frac{1}{p_0} \left(1 + \frac{\Delta p}{p_0} \right)^{-1}
$$

$$
\approx \frac{1}{p_0} - \frac{\Delta p}{p_0^2}
$$
(8)

Transverse Equation of Motion - 4

• Insert equation [8](#page-5-0) into modified Hill's equation [7](#page-5-1)

$$
\frac{d^2x}{ds^2} - \frac{1}{\rho} \left(1 - \frac{x}{\rho} \right) = -\frac{eB_0}{p} - \frac{e x g}{p}
$$

$$
\frac{d^2x}{ds^2} - \frac{1}{\rho} \left(1 - \frac{x}{\rho} \right) = -\frac{eB_0}{p_0} + \frac{eB_0 \Delta p}{p_0^2} - \frac{e x g}{p_0} + \frac{e x g \Delta p}{p_0^2} \tag{9}
$$

• Remember magnetic rigidity??, $B\rho = p/e$

$$
\frac{\mathrm{d}^2x}{\mathrm{d}s^2} + \frac{x}{\rho^2} = \frac{1}{\rho} \frac{\Delta p}{p_0} + kx \tag{10}
$$

where $k = \frac{eg}{p_0}$ and the last term is the product of two small terms (≈ 0)

Transverse Equation of Motion - 5

• Finally a new **modified Hill's equation**

$$
\frac{\mathrm{d}^2 x}{\mathrm{d}s^2} + \left(\frac{1}{\rho^2} - k\right)x = \frac{1}{\rho} \frac{\Delta p}{p_0} \tag{11}
$$

• Compare to the original Hill's equation from transverse lectures

$$
\frac{\mathrm{d}^2x}{\mathrm{d}s^2} + \left(\frac{1}{\rho^2} - k\right)x = 0\tag{12}
$$

• Particles with different momenta/energy have different orbits

Dispersion

- General solution will be of the form $x(s) = x_h(s) + x_i(s)$
- From previous lecture, dispersion is defined as

$$
D(s) = \frac{x_i(s)}{\Delta p/p_0} \qquad (13)
$$

- It is just another orbit and is subject to the focusing properties of the lattice
- The orbit of any particle is the sum of the well-known x_h and dispersion

Matrix formalism

• Recall transfer matricies from transverse lectures and add dispersion

$$
\begin{pmatrix} x \\ x' \end{pmatrix}_1 = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}_0 + \frac{\Delta p}{p_0} \begin{pmatrix} D \\ D' \end{pmatrix} \tag{14}
$$

where $C = \cos \sqrt{|k|} s$, $S = \frac{1}{\sqrt{k}}$ $\frac{1}{k}$ sin $\sqrt{|k|}s$, $C' = \frac{dC}{ds}$ $\frac{\mathrm{d}C}{\mathrm{d}s}$, $S' = \frac{\mathrm{d}S}{\mathrm{d}s}$ $_{\rm ds}$ and $D'(s) = \frac{x'_i(s)}{\Delta n/n}$ $\Delta p/p_0$

• One can show that

$$
D(s) = S(s) \int_{s_0}^{s_1} \frac{1}{\rho} C(s) \, ds - C(s) \int_{s_0}^{s_1} \frac{1}{\rho} S(s) \, ds \tag{15}
$$

Examples of Dispersion - 1

• Start with something simple, a drift!

$$
M_{\text{drift}} = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix}, \qquad C(s) = 1, S(s) = l \tag{16}
$$

- Importantly $\rho = \infty$ so immediately $D_{\text{drift}} = 0$
- OK, how about a **pure sector dipole**?

$$
M_{\text{dipole}} = \begin{pmatrix} \cos\frac{l}{\rho} & \rho\sin\frac{l}{\rho} \\ -\frac{1}{\rho}\sin\frac{l}{\rho} & \cos\frac{l}{\rho} \end{pmatrix}
$$

$$
C(s) = \cos\frac{l}{\rho}, \ S(s) = \rho\sin\frac{l}{\rho} \qquad (17)
$$

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Examples of Dispersion - 2

• Putting this in the equation for dispersion

$$
D_{\text{dipole}}(s) = \sin\frac{l}{\rho} \int_0^l \cos\frac{s}{\rho} ds - \cos\frac{l}{\rho} \int_0^l \sin\frac{s}{\rho} ds
$$

$$
= \sin\frac{l}{\rho} \left[\rho \sin\frac{s}{\rho} \right]_0^l - \cos\frac{l}{\rho} \left[-\rho \cos\frac{s}{\rho} \right]_0^l
$$

$$
= \rho \sin^2\frac{l}{\rho} + \rho \cos\frac{l}{\rho} \left(\cos\frac{l}{\rho} - 1 \right)
$$

$$
= \rho \left(1 - \cos\frac{l}{\rho} \right) \tag{18}
$$

• And $D'_{\text{dipole}}(s) = \sin \frac{l}{\rho}$

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Examples of Dispersion - 3

• Assuming θ is small we can expand this

$$
D(s)_{\text{dipole}} = \rho \left(1 - \cos \frac{l}{\rho} \right)
$$

\n
$$
\approx \rho \left(1 - \left[1 - \frac{1}{2} \left(\frac{l}{\rho} \right)^2 \right] \right)
$$

\n
$$
\approx \frac{\rho}{2} \left(\frac{l}{\rho} \right)^2 = \frac{\rho \theta^2}{2} \tag{19}
$$

Matrix formalism continued

• Can now expand the transfer matrix to include dispersion

$$
\begin{pmatrix} x \\ x' \\ \Delta p/p \end{pmatrix}_1 = \begin{pmatrix} C & S & D \\ C' & S' & D' \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x \\ x' \\ \Delta p/p \end{pmatrix}_0 \tag{20}
$$

- Dispersion can be calculated by an optics code for a real machine
- $D(s)$ is created by the **dipoles**...
- ... and focused by the **quadrupoles**
- Diamond DBA example \Rightarrow

- These are 2D ellipses defining the beam
- The central and extreme momenta are shown (there is a distribution in between)
- The vacuum chamber must accommodate the full spread
- With dispersion the **dispersed closed orbit** for a given particle is (assuming $D_u = 0$)

$$
y(s) = y_{\beta_y}(s), \qquad x = x_{\beta_x}(s) + D(s)\frac{\Delta p}{p} \tag{21}
$$

Dispersed Beam Size

- Dispersion also contributes to the beam size
- Therefore we can **measure the dispersion** by measuring beam sizes at different locations with different amounts of dispersion and different β s

Dispersion Suppression

- Given a periodic lattice what can we do about dispersion?
- We can't get rid of it completely as it's produced by the dipoles
- Answer . . . suppress the dispersion elsewhere

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Dispersion Suppression: Easy option

- Use extra quadrupoles to match $D(s)$ and $D'(s)$
- Given an optical solution in the arc, suppressing dispersion can be achieved with 2 additional quadrupoles
- But that's not enough! Need to match the Twiss, optical parameters too
- An extra 4 quadrupoles are needed to match α and β

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Dispersion Suppression: Easy option

Advantages:

- Straight forward
- Works for any phase advance per cell
- Ring geometry is unchanged
- Flexible! Can match between different lattice structures

Disadvantages:

- Additional quadrupole magnets and power supplies required
- The extra quadrupoles are, in general stronger
- The β function increases so the aperture increases

Dispersion Suppression: Missing Bend

- Start with $D = D' = 0$ and create dispersion such that the conditions are matched in the first regular quadrupoles
- Utilise *n* cells **without dipole magnets** at the end of an arc, followed by m arc cells
- ... hence "missing bend" dispersion suppression
- Condition:

$$
\frac{2m+n}{2}\Phi_C = (2k+1)\frac{\pi}{2} \quad (22)
$$

where
$$
\Phi_C
$$
 = cell phase advance,
\nsin $\frac{m\Phi_C}{2} = \frac{1}{2}$, $k = 0, 2, ...$ or
\nsin $\frac{m\Phi_C}{2} = -\frac{1}{2}$, $k = 1, 3, ...$

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ISIS Neutron and Dispersion Suppression: Missing Bend **Muon Source**

Advantages:

- No additional quadrupoles or new power supplies
- Aperture requirements are the same as those in the arc as β is unchanged

Disadvantages:

- Only works for certain phase advances restricting optics options in the arc
- The geometry of the ring is changed

Dispersion Suppression: Half Bend

- How about inserting different strength dipoles? Does it help?
- Assume you have a FODO arc cell, a lattice insertion and then a dispersion free section without dipoles
- Condition for vanishing disperion can be calculated for n cells with dipole strength $\delta_{\rm sun}$

$$
2\delta_{\rm sup} \sin^2\left(\frac{n\Phi_C}{2}\right) = \delta_{\rm arc} \tag{23}
$$

• So if we require $\delta_{\text{sup}} = \frac{1}{2}$ $\frac{1}{2}\delta_{\text{arc}}$ we get

$$
\sin^2\left(\frac{n\Phi_C}{2}\right) = 1 \Rightarrow \sin(n\Phi_C) = 0
$$

$$
\Rightarrow n\Phi_C = k\pi, \quad k = 1, 3, ...
$$
 (24)

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Dispersion Suppression: Half Bend

Advantages and Disadvantages are the same as for the missing bend only there is an extra **disadvantage**:

A special half strength dipole is required which may add extra cost to the design

N.B. This is not an exhaustive list of dispersion suppression techniques, just a taster! Dr Rob Williamson 23/30

Chromaticity - 1

- What about off-momentum effects through quadrupoles?
- The focusing strength of a quadrupole depends on the momentum of the particle $1/f \propto 1/p$

- Particles with $\Delta p > 0$, $\Delta p < 0$, ideal momentum
- Off-momentum particles oscillate around a **chromatic** closed orbit NOT the design orbit

Chromaticity - 2

- Normalised quadrupole strength $k = \frac{g}{p}$ p/e
- In case of a momentum spread

$$
k = \frac{eg}{p_0 + \Delta p} \approx \frac{eg}{p_0} \left(1 - \frac{\Delta p}{p_0} \right) = k_0 + \Delta k \qquad (25)
$$

$$
\Delta k = -\frac{\Delta p}{p_0} k_0 \qquad (26)
$$

• This acts like a quadrupole error in the machine and leads to a tune spread

$$
\Delta Q = \frac{1}{4\pi} \int \Delta k(s)\beta(s) \, \mathrm{d}s = -\frac{1}{4\pi} \frac{\Delta p}{p_0} \int k_0(s)\beta(s) \, \mathrm{d}s \tag{27}
$$

Chromaticity - 3

• This spread in tune is expressed via **chromaticity**, Q' or the normalised chromaticity, ξ

$$
Q' = \frac{\Delta Q}{\Delta p/p_0}, \qquad \xi = \frac{\Delta Q/Q}{\Delta p/p_0} \tag{28}
$$

- Note that chromaticity is produced by the lattice itself
- It is determined by the focusing strength of all the quadrupoles
- The "natural" chromaticity is negative and can lead to a large tune spread and consequent instabilities
- For example, for a FODO lattice $\xi \approx -1$

Correcting Chromaticity - 1

- Want to "sort" the particles by their momentum
- Utilise dispersive trajectory! Apply magnetic field that is zero at small amplitudes and rises quickly outward
- Use sextupoles!

$$
B_x = \tilde{g}xy
$$
, $B_y = \frac{1}{2}\tilde{g}(x^2 - y^2)$ (29)

- This results in a linear gradient in x , $\frac{\partial B_x}{\partial y} = \frac{\partial B_y}{\partial x} = \tilde{g}x$
- And a normalised quadrupole strength $k_{\rm sext} = \frac{\tilde{g}x}{p/e} = m_{\rm sext}x = m_{\rm sext}D\Delta p/p$

Correcting Chromaticity - 2

• This all results in a corrected chromaticity

$$
Q' = -\frac{1}{4\pi} \oint \beta(s) \left[k(s) - mD(s) \right] ds \tag{30}
$$

- Chromatic sextupoles: Sextupoles at nonzero dispersion can correct natural chromaticity
- Usually 2 families, one horizontal and one vertical
- Place where $\beta_{x/y}D$ is large to minimise their strength Dr Rob Williamson 28/30

- Reminder of co-ordinate system
- Transverse equation of motion: **modified Hill's equation** with momentum spread
- **Dispersion** revisited in matrix form
- Effect of dispersion on beam orbit and beam size
- Dispersion suppression
- Chromaticity and chromatic tune spread
- Chromatic sextupoles and **chromaticity correction**

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