

PAUL SCHERRER INSTITUT



UNIVERSITY OF  
CAMBRIDGE



Fermilab



WIR SCHAFFEN WISSEN – HEUTE FÜR MORGEN

Marco Calvi :: Photon Science Division :: Paul Scherrer Institute

# A GdBCO Undulator for Tomographic Microscopy at the new Swiss Light Source, SLS2.0

TE-MSc Seminar

Feb 1<sup>st</sup> 2024, CERN via Zoom

LEAPS  
INNOVATION

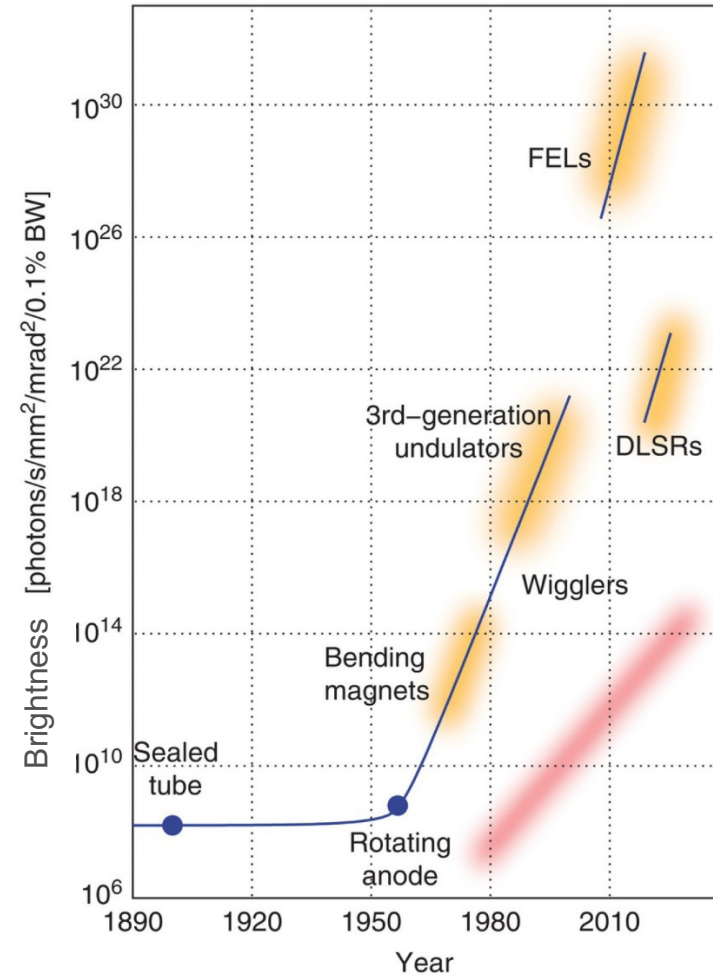
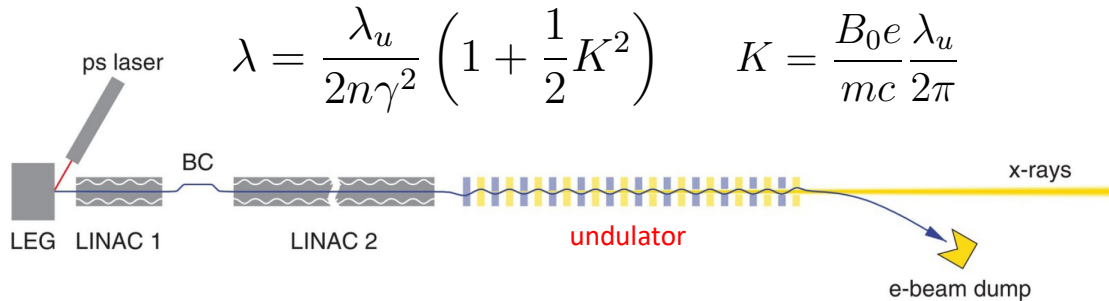
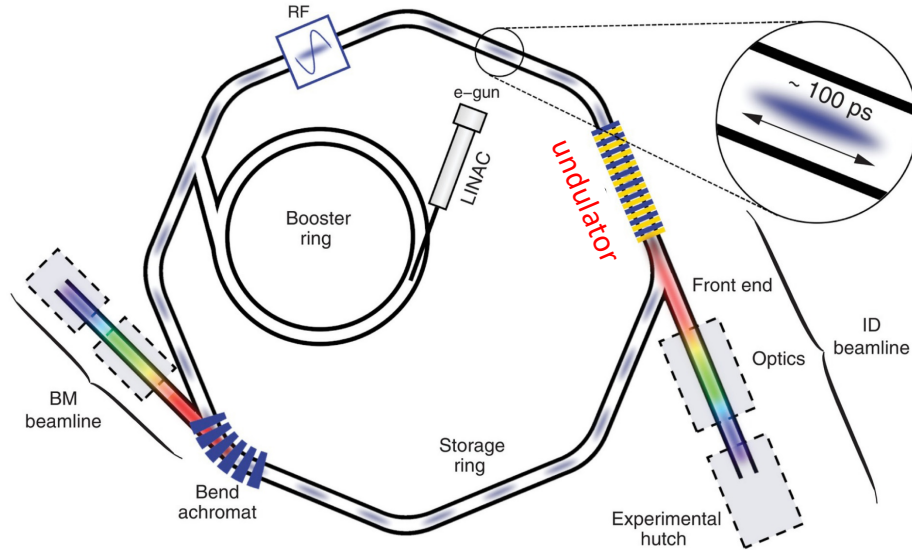
SLS2.0



Swiss Accelerator  
Research and  
Technology

- Brief introduction to accelerator based light sources
- The tomographic microscopy beamline: TOMCAT → I-TOMCAT
- The HTS (REBCO) bulk staggered array undulator
- The results on short samples:
  - Bulks & Tape-Stacks
- The status of the meter long HTS undulator prototype
- Conclusions

# Introduction

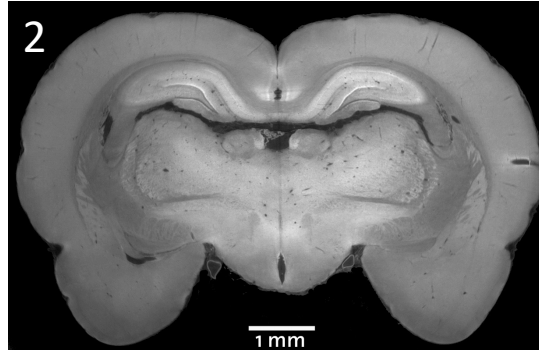


Non-destructive, high-throughput, high-resolution, 3D imaging technique:

1. Wide spatial resolution: nano-micro-meso scales (0.1-10  $\mu\text{m}$ )
2. High density resolution enhanced by phase contrast
3. Broad range of sample sizes (10  $\mu\text{m}$  – 20 mm)
4. High temporal resolution: 3D data acquisition in less than 1 s
5. In-situ, operando, in-vivo investigations



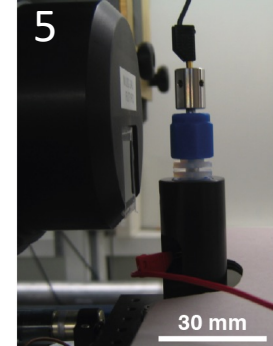
**Spatial Resolution**  
10 microns – 0.1 microns



**Density Resolution**  
Phase contrast imaging

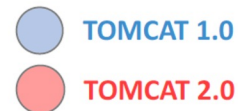
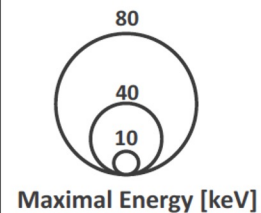
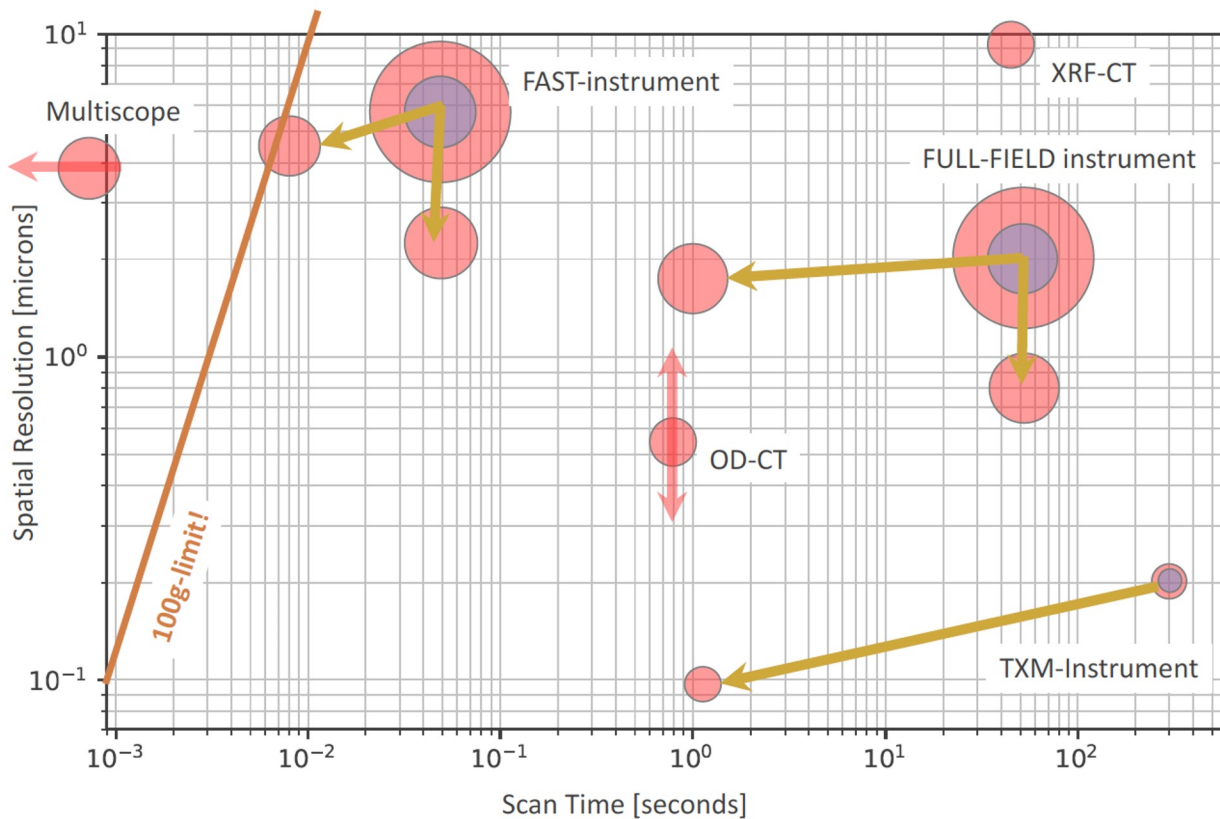


**Ultra-fast tomography**  
Living fly



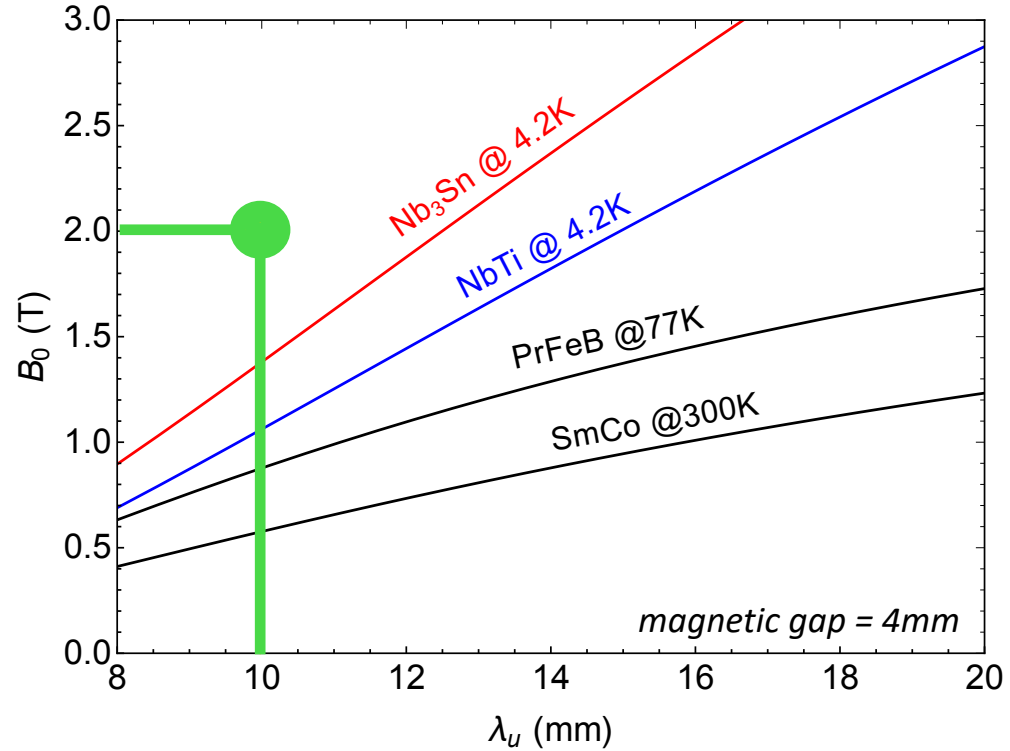
**In-situ capabilities**  
Furnace/Cryo/Traction  
Electrochemistry

# TOMCAT → I-TOMCAT @ SLS2.0

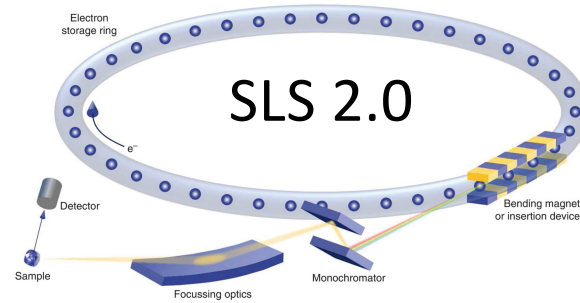
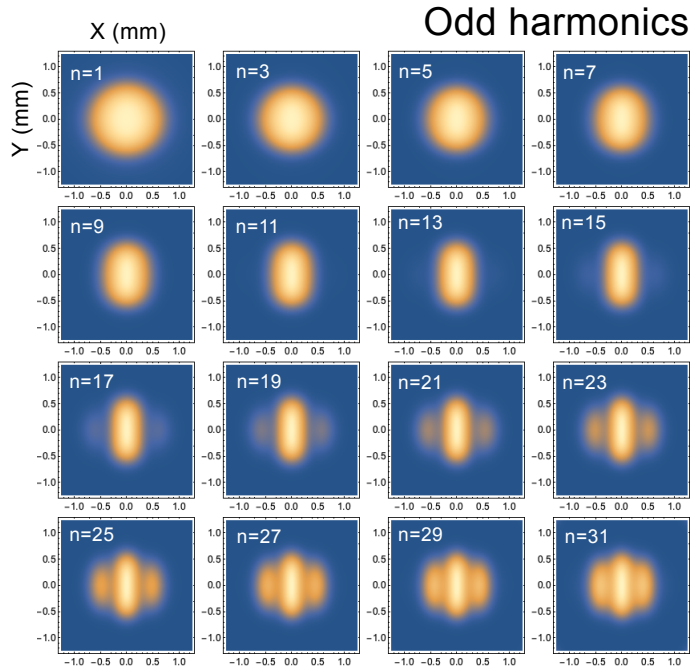


- Higher spatial and temporal resolution
- Larger samples, denser material
- More chemical information

# The new $\mu$ -Tomography beamline of SLS2.0

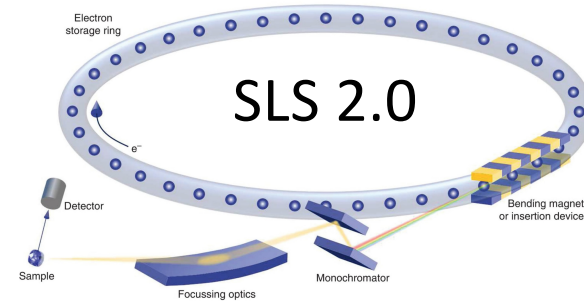
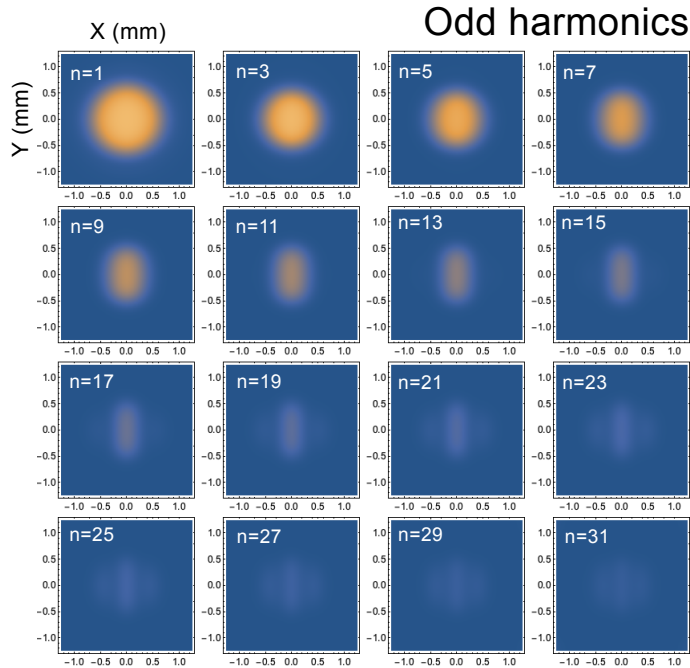


[Scaling laws: E.R. Moog, R.J. Dejus, and S. Sasaki , Light Source Note: ANL/APS/LS-348  
James Clarke, FLS 2012, March 2012, Ryota Kinjo Physical Review Special Topics, Accelerator  
and Beams 17, 022401 (2014)]



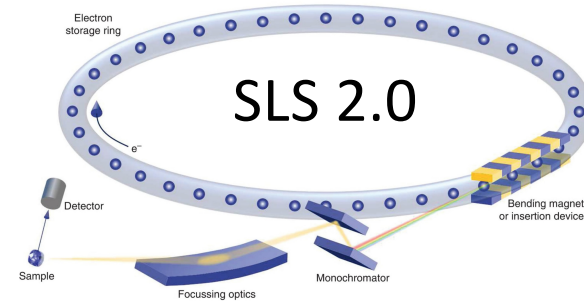
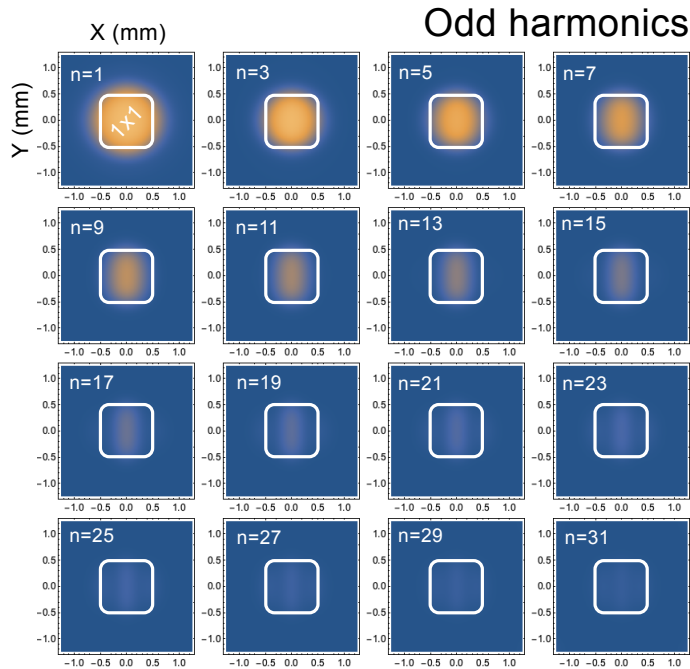
Calculations done for the future  
**iTOMCAT beamline**, dedicated to  
tomographic microscopy

Flux at 30m from the source  
to illuminate a sample of about  $1\text{mm}^2$

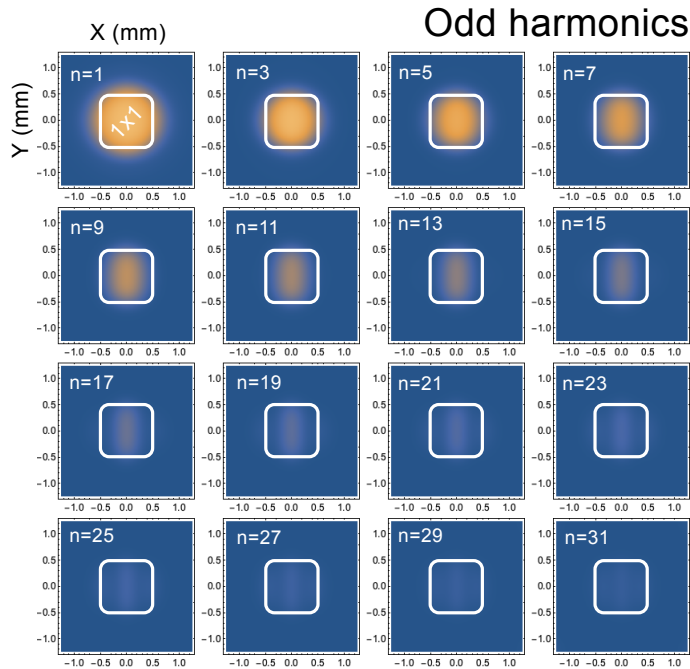
CPMU14 with  $B_0=1.3$  T – ABSOLUTE SCALE

Calculations done for the future  
**iTOMCAT beamline**, dedicated to  
tomographic microscopy

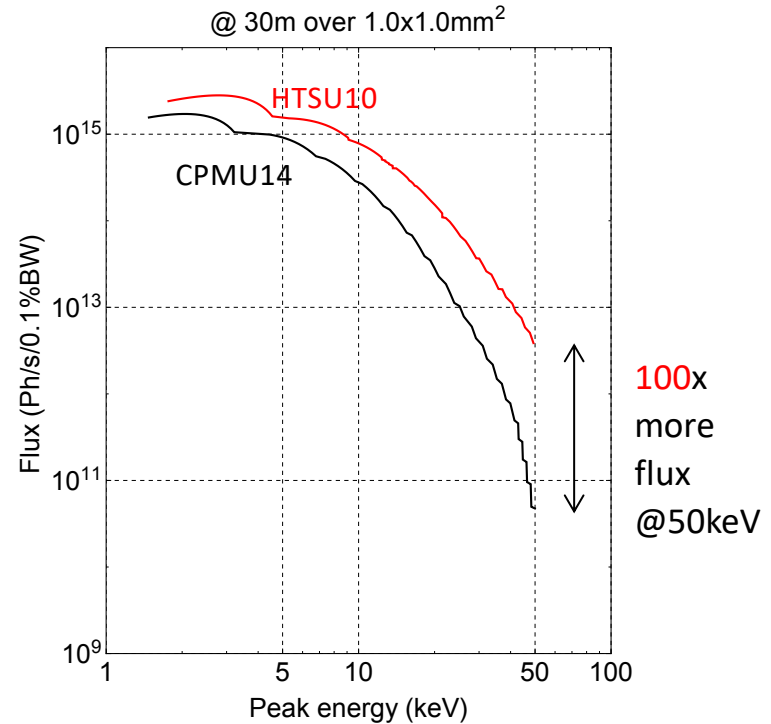


CPMU14 with  $B_0=1.3$  T – ABSOLUTE SCALE

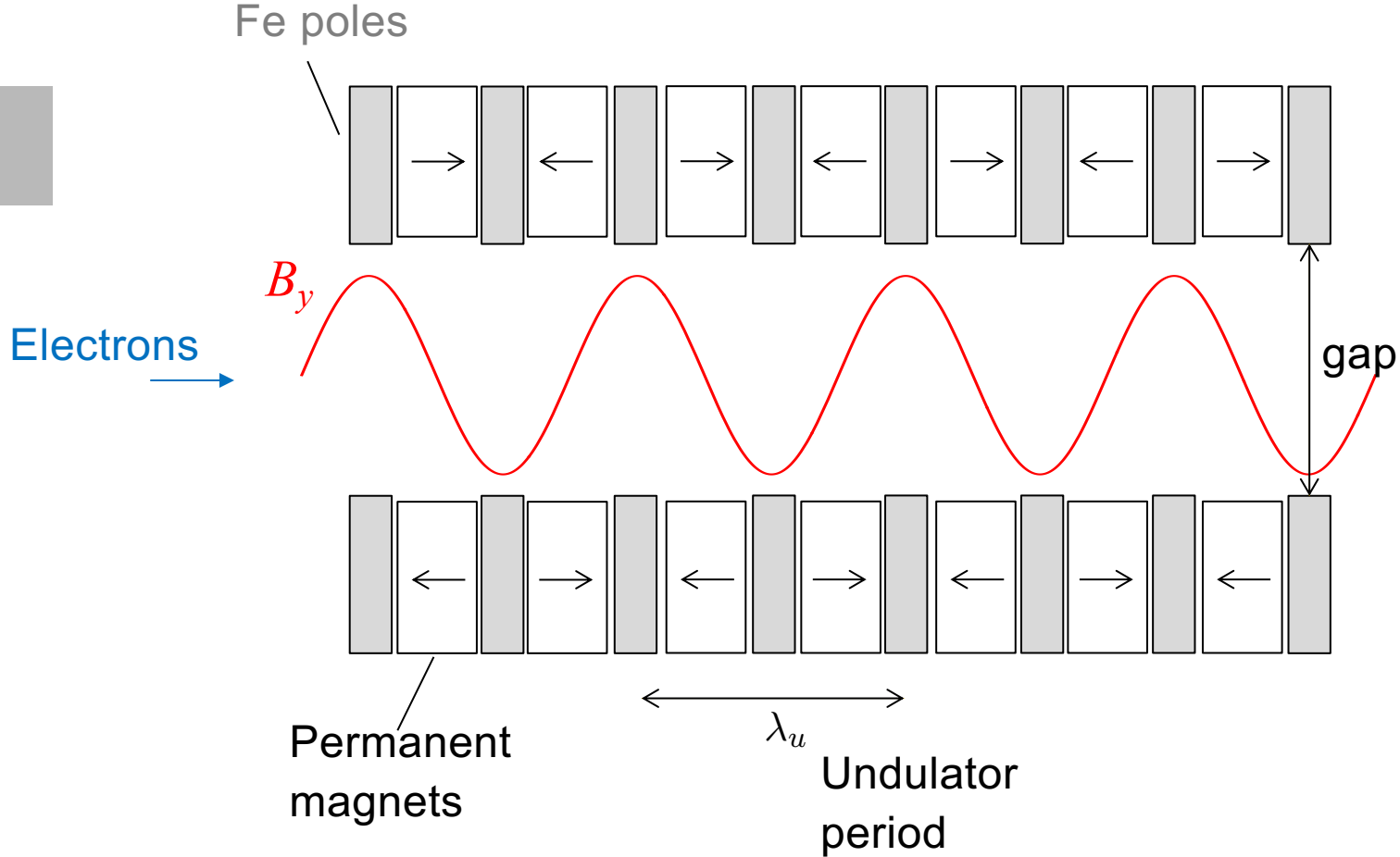
Calculations done for the future  
**iTOMCAT beamline**, dedicated to  
tomographic microscopy

CPMU14 with  $B_0=1.3$  T – ABSOLUTE SCALE

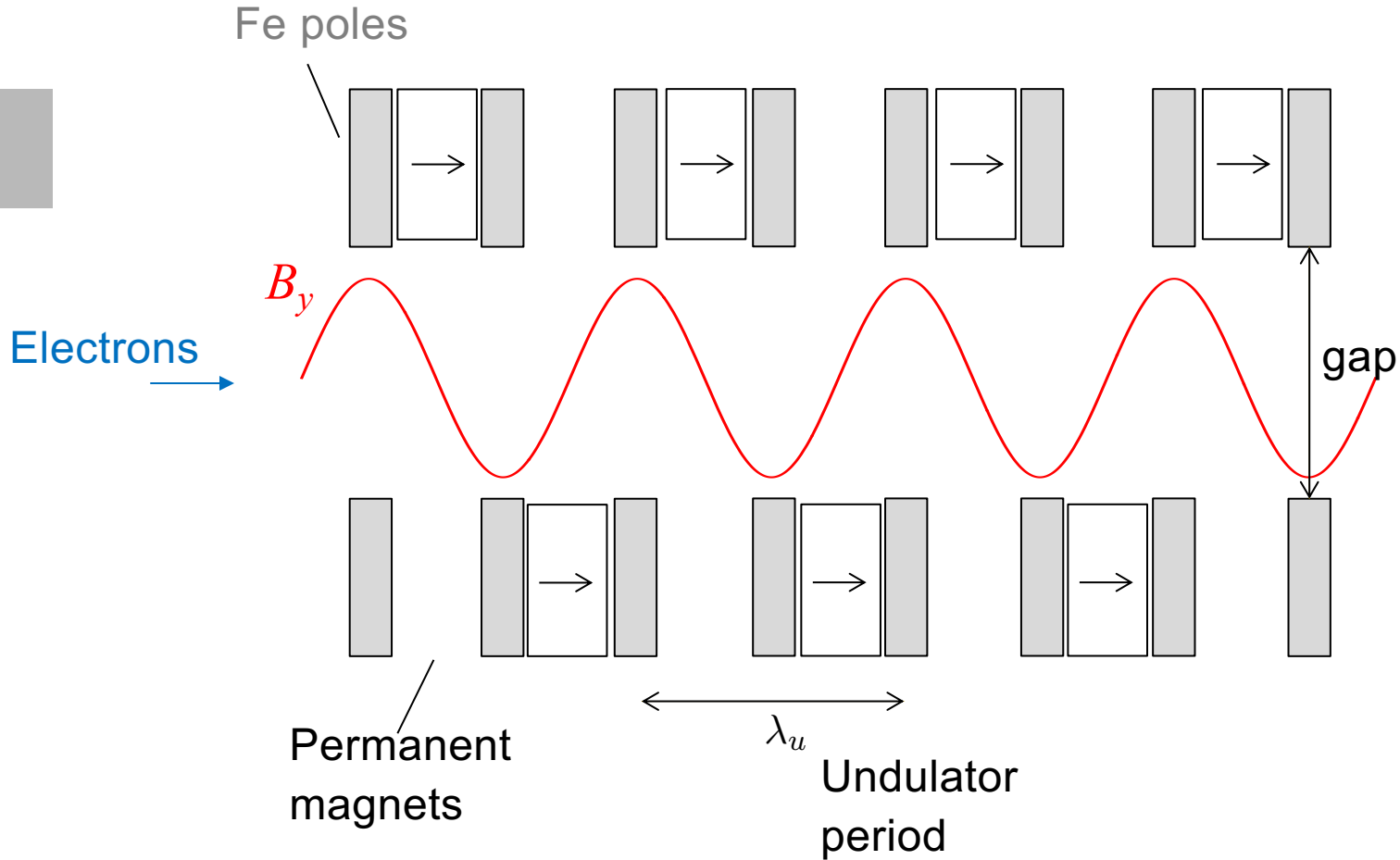
Flux at 30m from the source  
to illuminate a sample of about  $1\text{mm}^2$



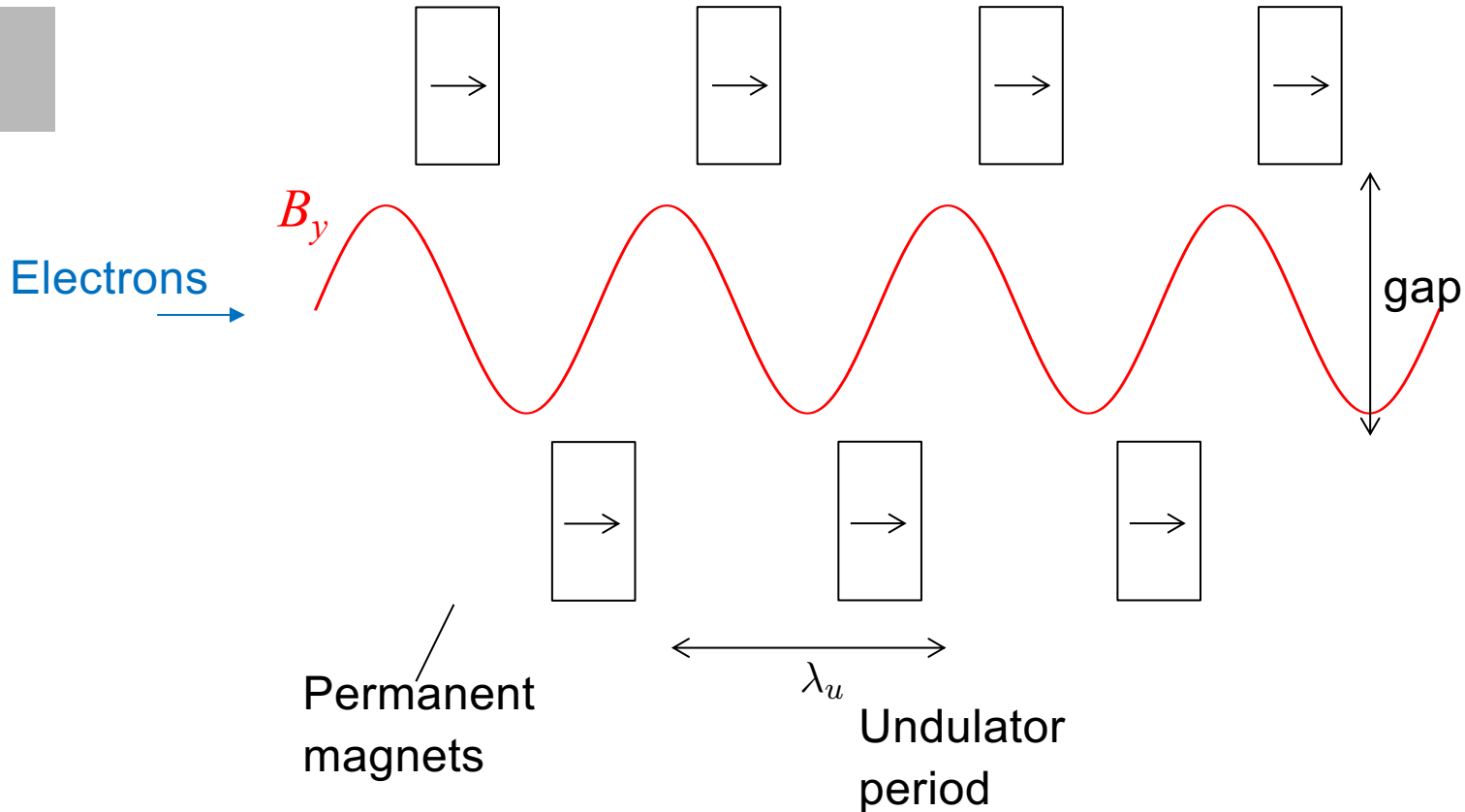
# Permanent Magnet Undulator with Fe poles



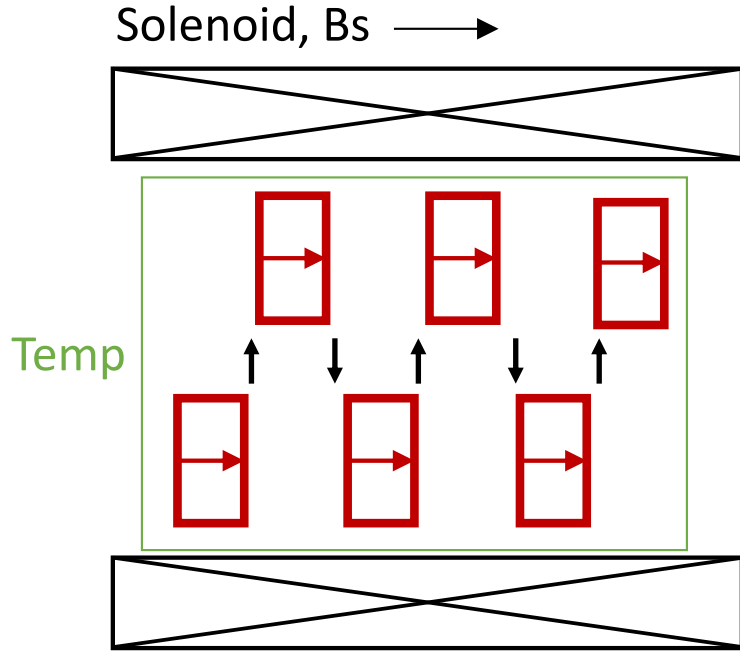
## Permanent Magnet Undulator with Fe poles



# Permanent Magnet Undulator with Fe poles

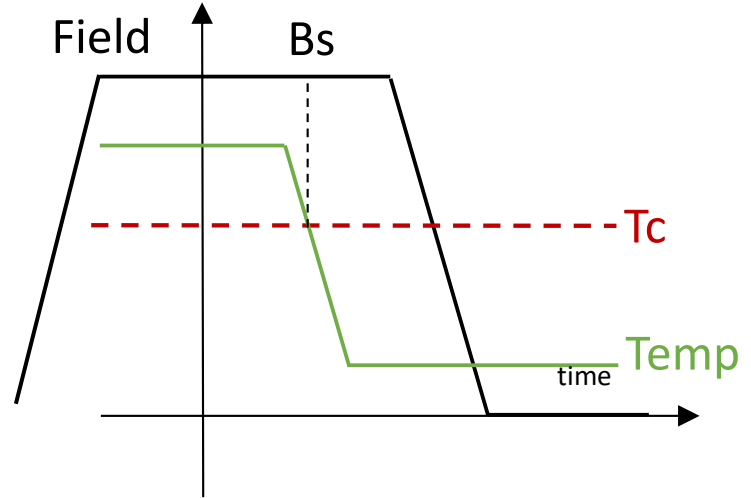


# Superconducting Staggered Array Undulator

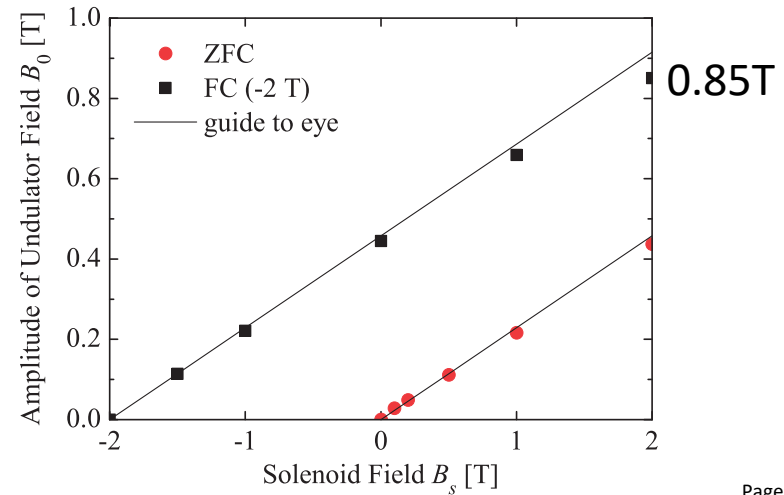
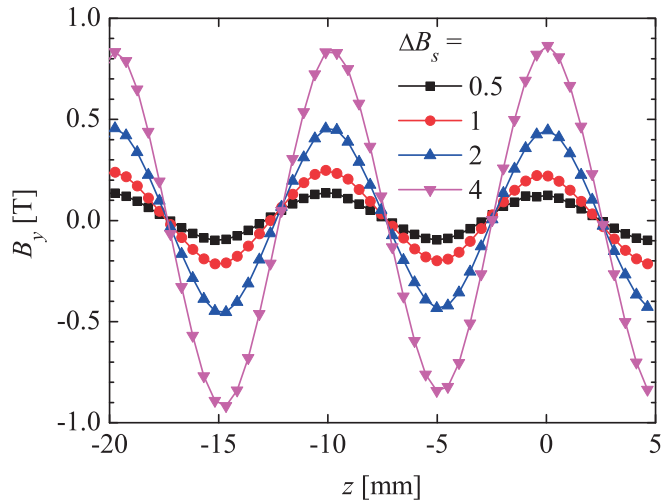
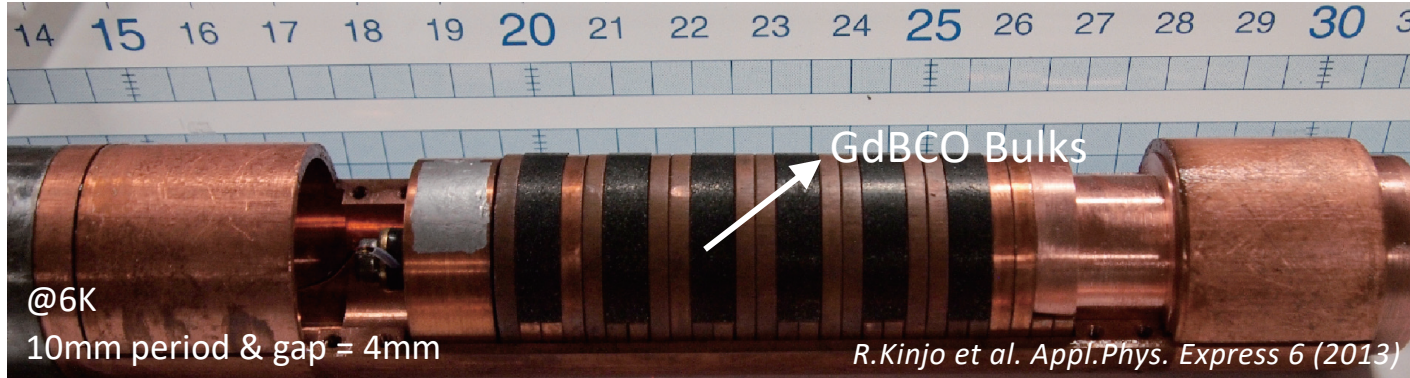


GdBCO  $T_c=92\text{K}$

Example of *field cooling* magnetisation



# Superconducting Staggered Array Undulator



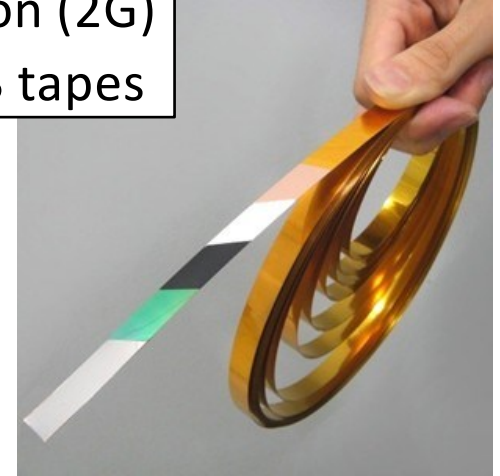
# HTS → REBCO

REBCO Bulks



- • CAN Superconductor
- • Adelwitz Technologiezentrum
- • Nippon Steel

2nd generation (2G)  
thin-film HTS tapes



- Fujikura
- SuperPower
- • THEVA
- SuNAM
- AMSC
- Deutsche Nanoschicht/BASF
- • SuperOX
- BRUKER

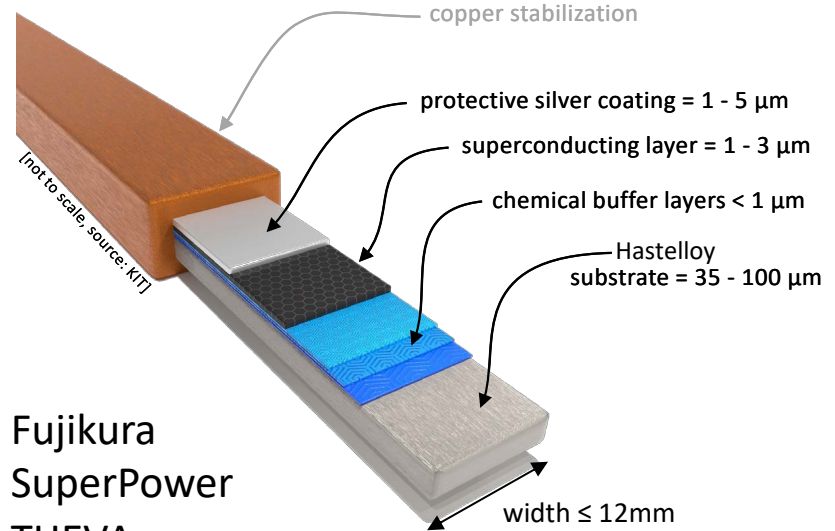


# HTS → REBCO



- ➔ • CAN Superconductor
- ➔ • Adelwitz Technologiezentrum
- ➔ • Nippon Steel

## 2nd generation (2G) thin-film HTS tapes



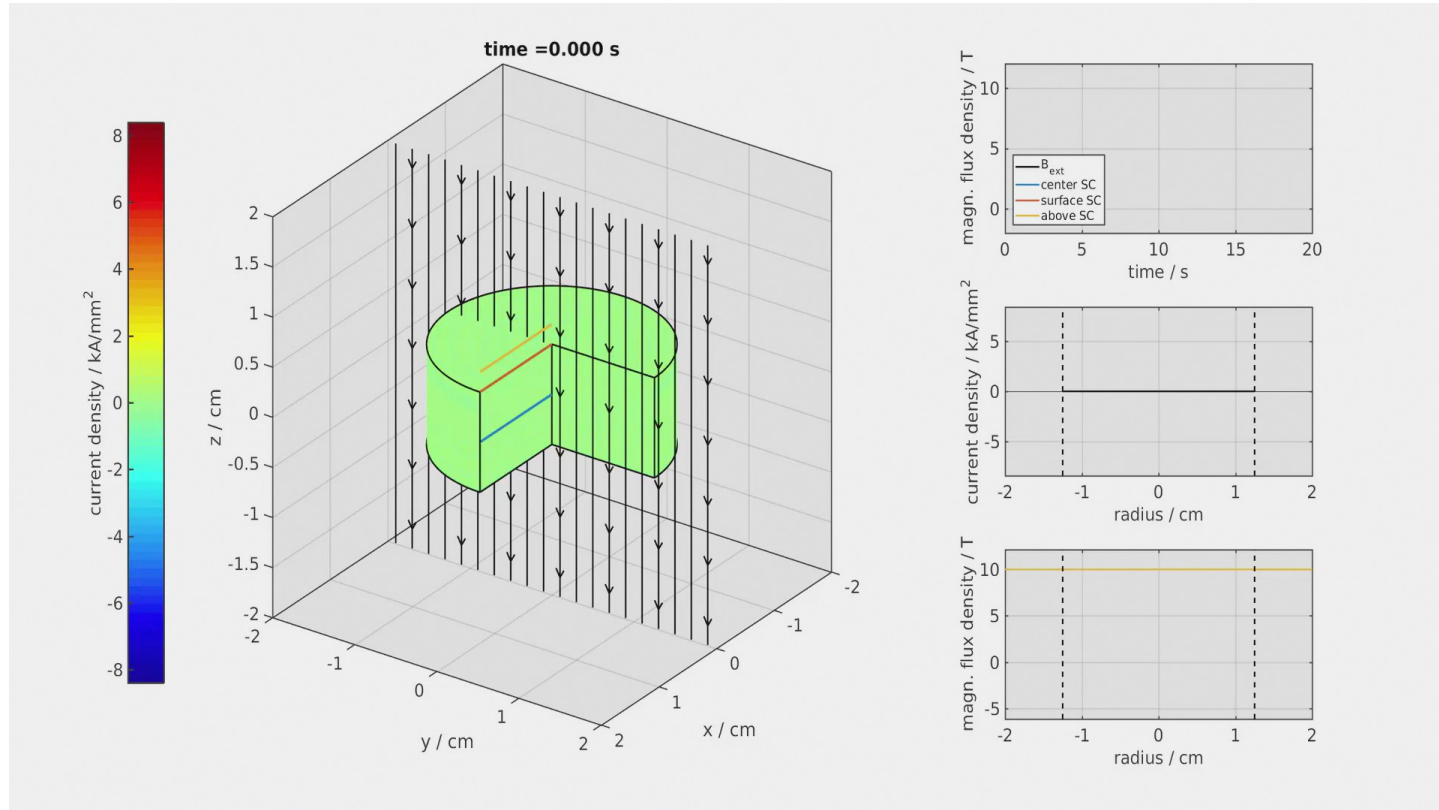
- Fujikura
- SuperPower
- ➔ • THEVA
- SuNAM
- AMSC
- Deutsche Nanoschicht/BASF
- ➔ • SuperOX
- BRUKER

REBCO Bulks



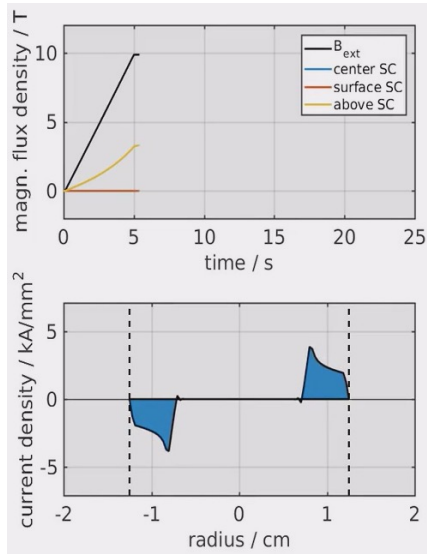
- • CAN Superconductor
- • Adelwitz Technologiezentrum
- • Nippon Steel

# Example of Field Cooling (FC)

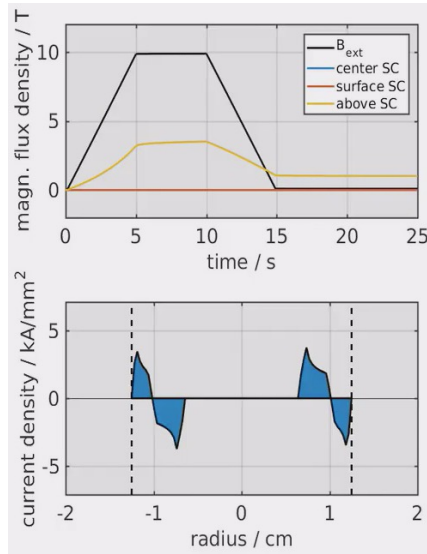


# ZFC versus FC

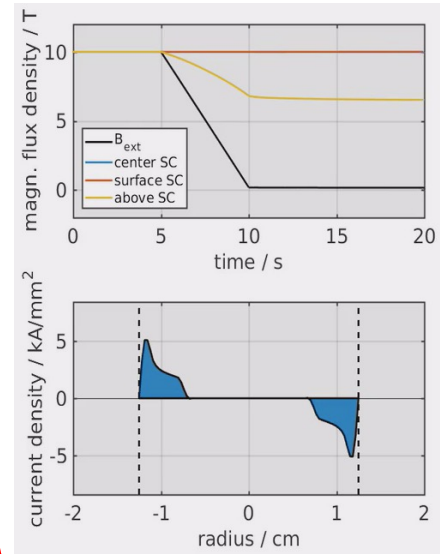
## ZFC - 1



## ZFC - 2

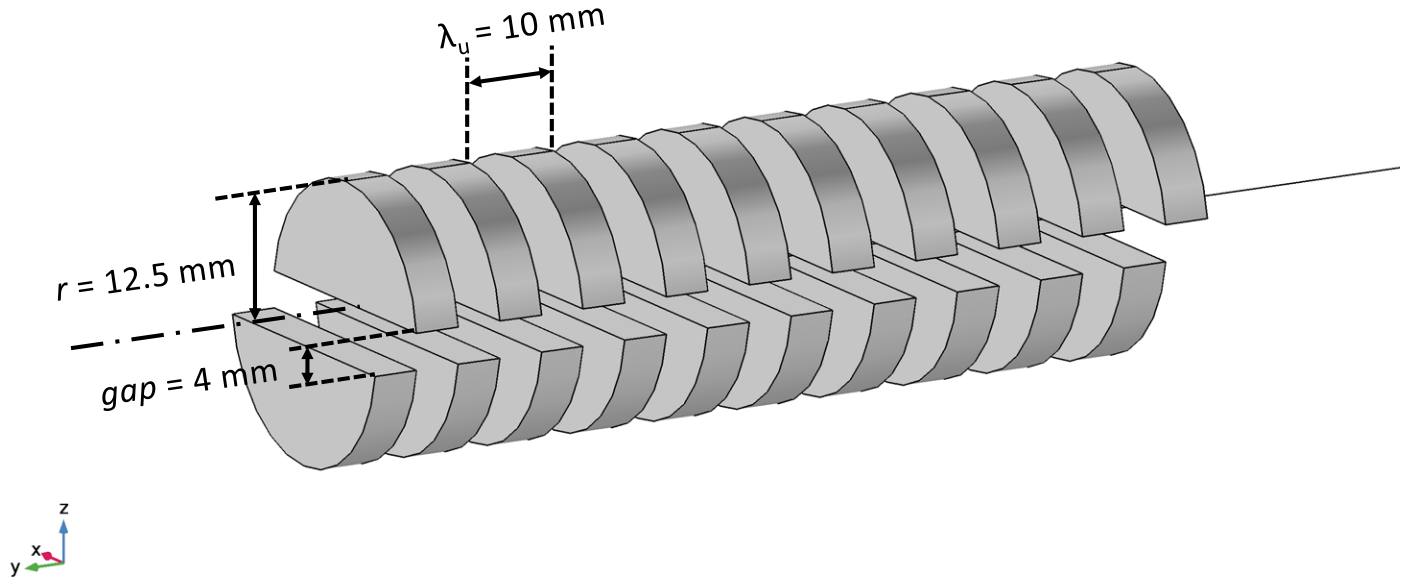


## Field Cooling



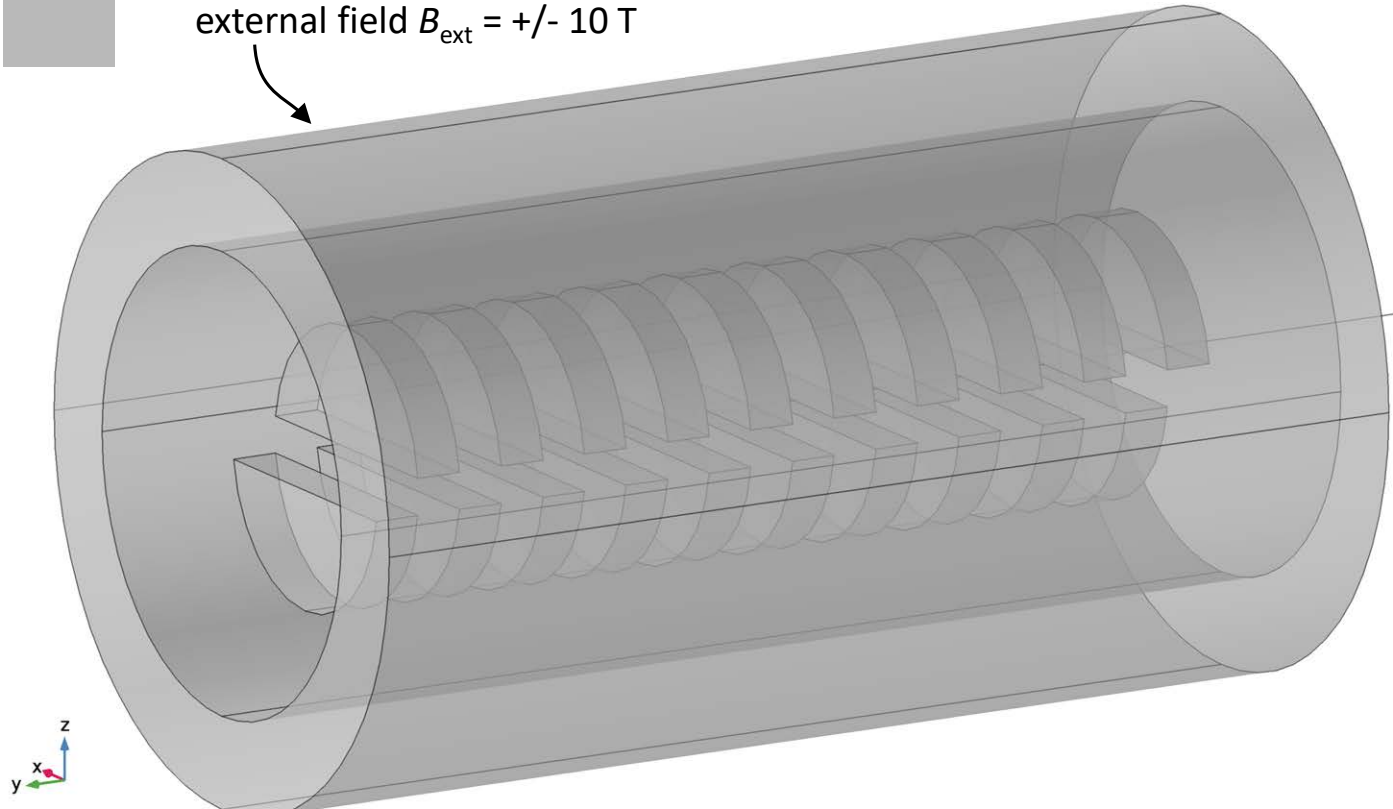
Field cooling is what fits better for this application

# Superconducting Staggered Array



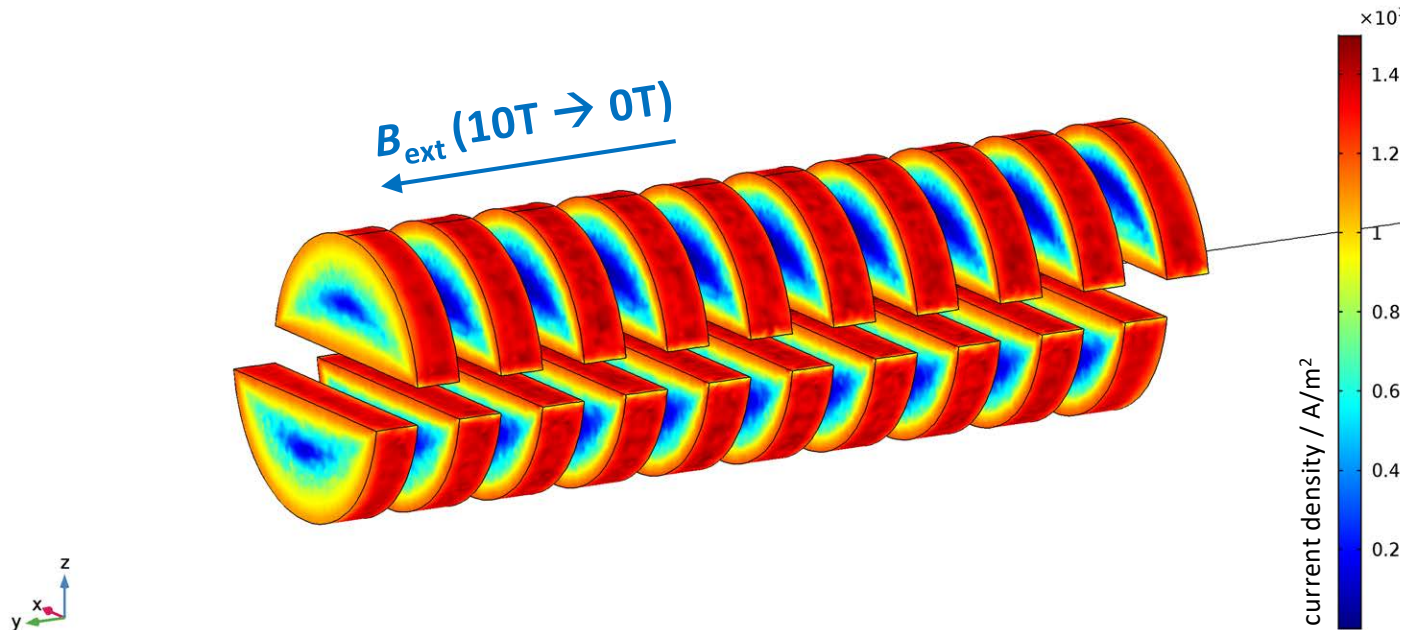
# Superconducting Staggered Array

- Superconducting solenoid providing external field  $B_{\text{ext}} = \pm 10 \text{ T}$



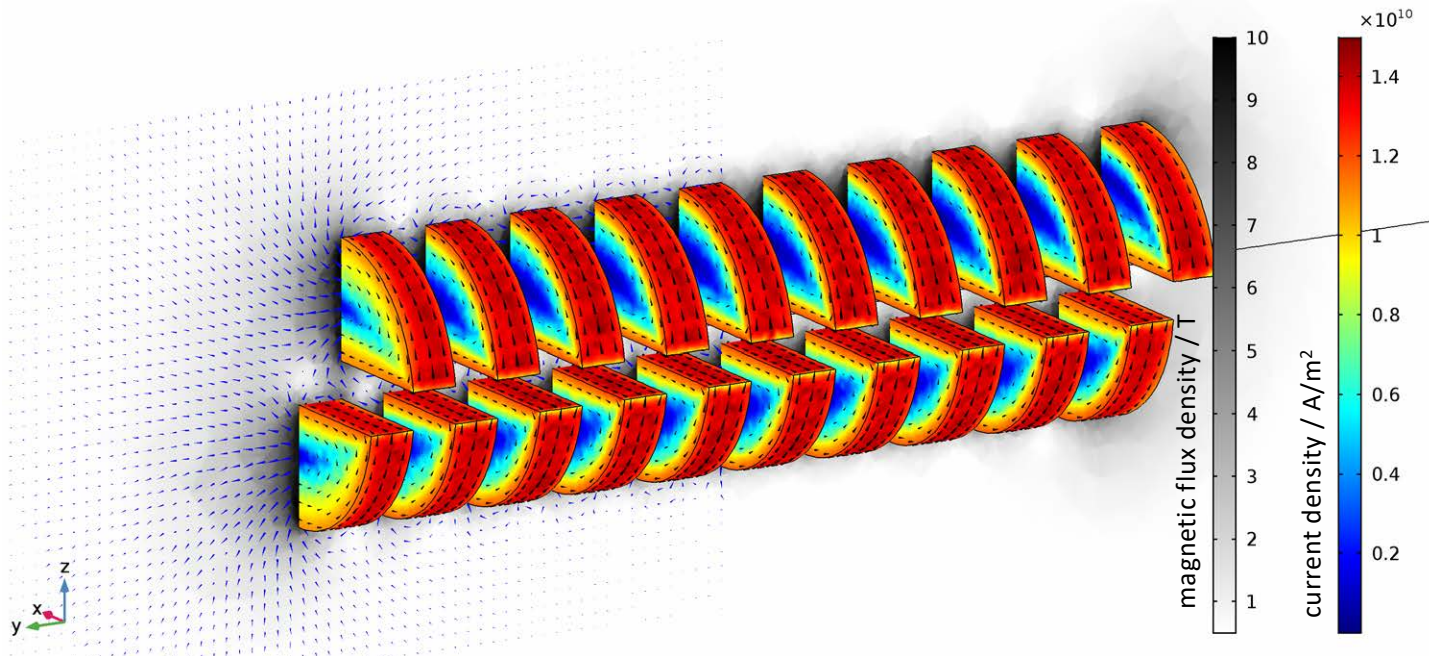
# Superconducting Staggered Array

- Surface current density after magnetization with field 10T  $\rightarrow$  0T:



# Superconducting Staggered Array

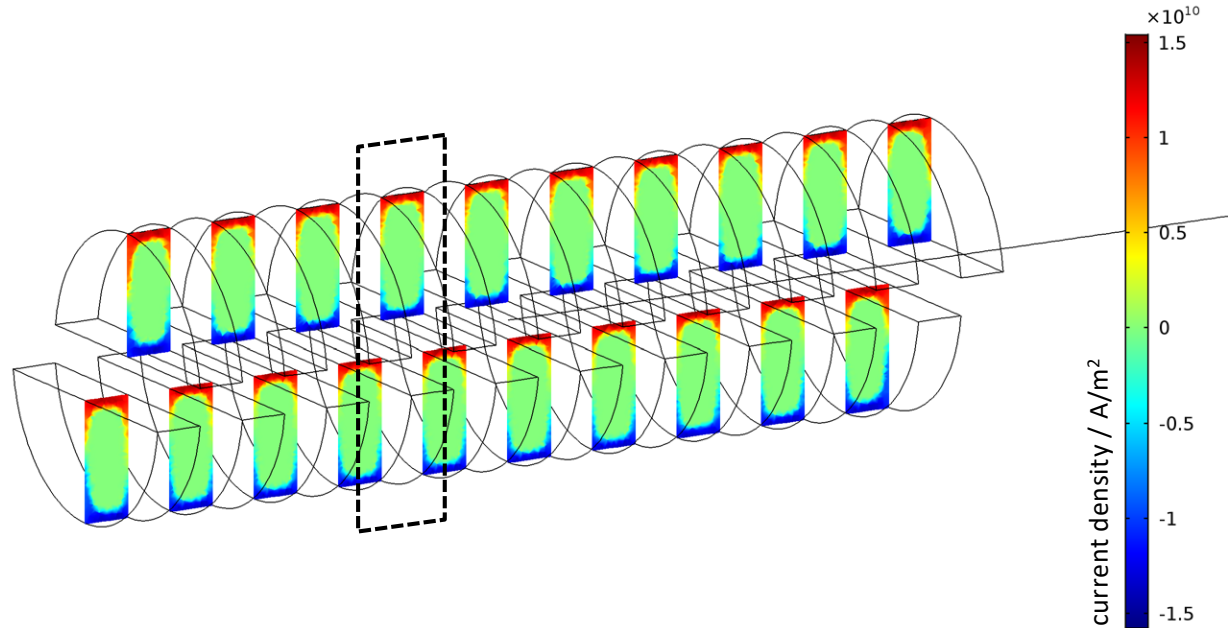
- Surface current density and trapped magnetic field after magnetization with field 10T  $\rightarrow$  0T:



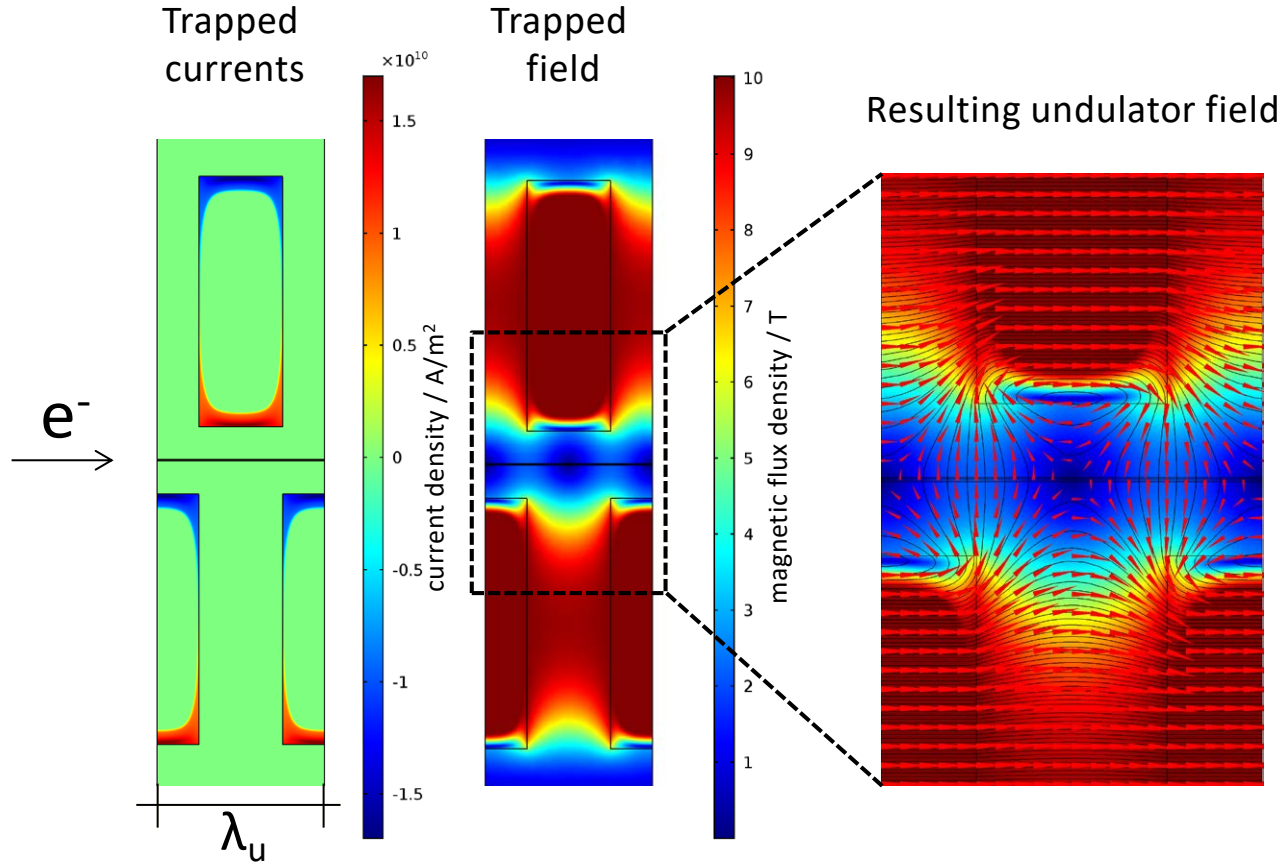


# Superconducting Staggered Array

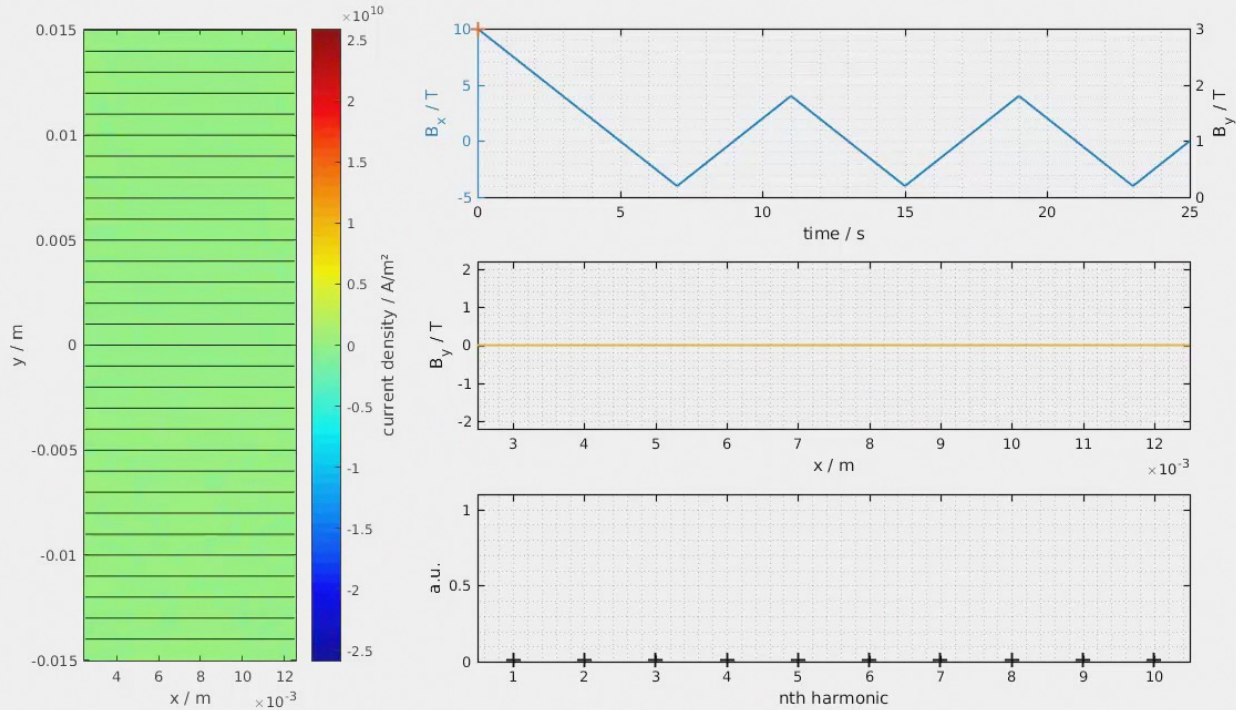
- Internal current density after magnetization with field 10T  $\rightarrow$  0T:



# Superconducting Staggered Array



# Example of operation: K-tuning

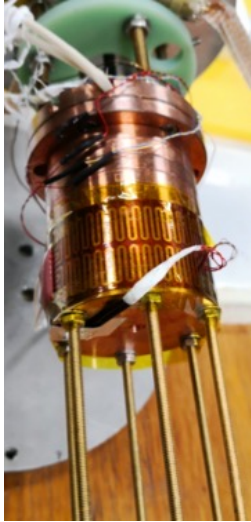


- Brief introduction to accelerator based light sources
- The Tomographic Microscopy beamline: TOMCAT → I-TOMCAT
- The HTS (REBCO) bulk Staggered Array undulator
- The results on short samples:
  - Bulks & Tapes
- The status of the meter long HTS Undulator prototype
- Conclusions

- Brief introduction to accelerator based light sources
- The Tomographic Microscopy beamline: TOMCAT → I-TOMCAT
- The HTS (REBCO) bulk Staggered Array undulator
- The results on short samples:
  - Bulks & Tapes
- The status of the meter long HTS Undulator prototype
- Conclusions

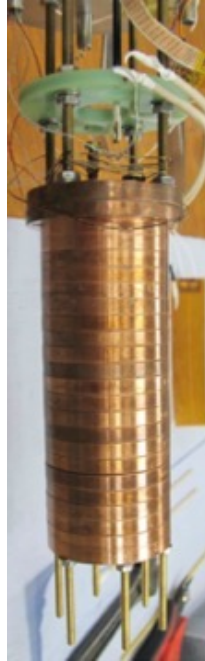
# Samples Overview

1<sup>st</sup> Bulk Sample



6mm gap

2<sup>nd</sup> Bulk Sample



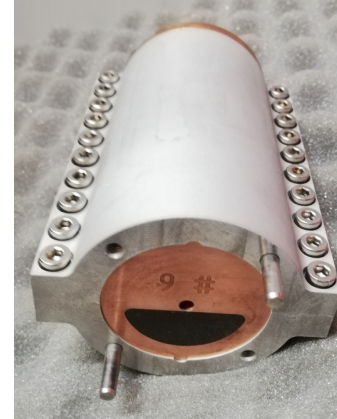
4mm gap

Bulk Industrial Sample



4mm gap

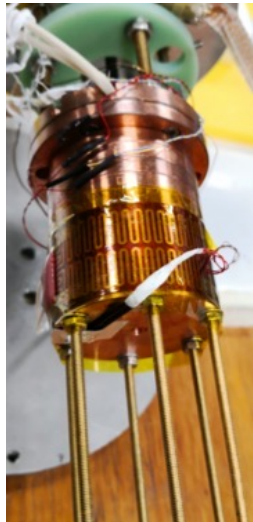
Bulk Simplified Sample



4mm gap

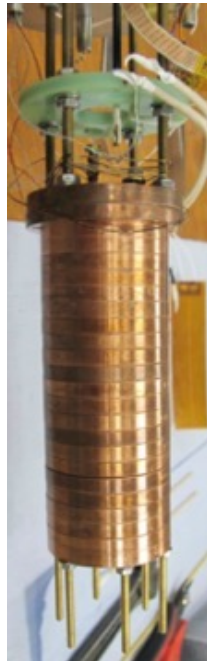
# Samples Overview

1<sup>st</sup> Bulk Sample



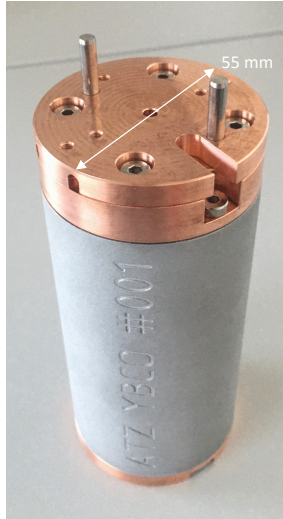
6mm gap

2<sup>nd</sup> Bulk Sample



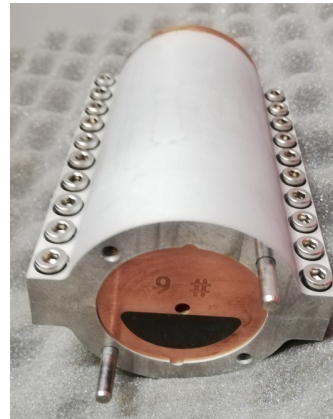
4mm gap

Bulk Industrial Sample



4mm gap

Bulk Simplified Sample



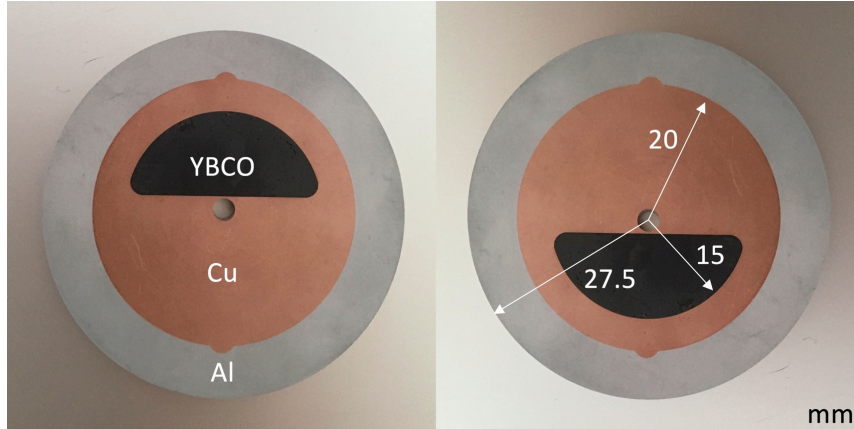
4mm gap

The "Good" Sample

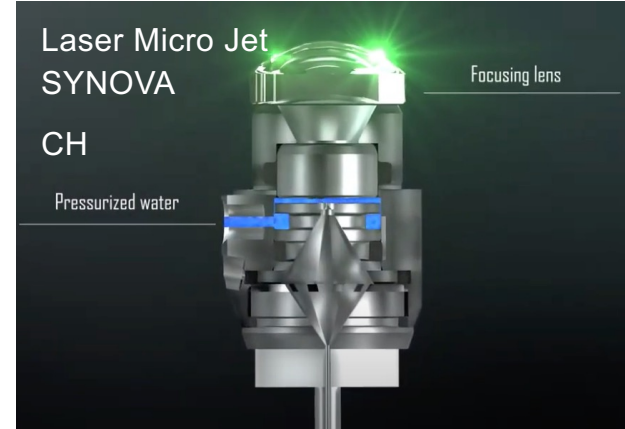


4mm gap

# Industrial Sample

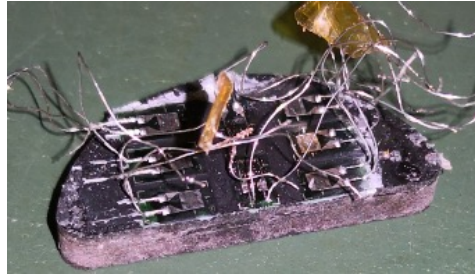
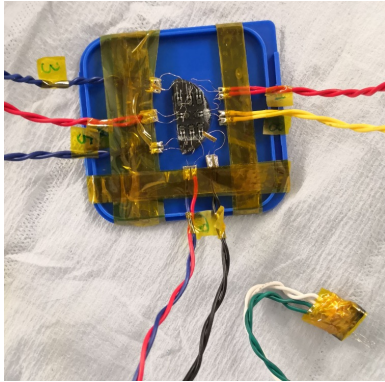
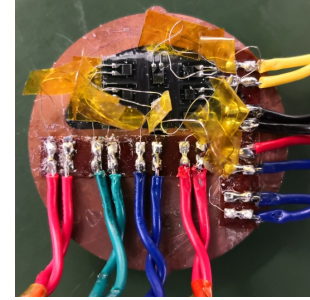
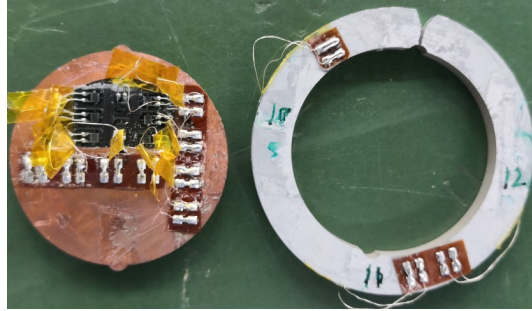
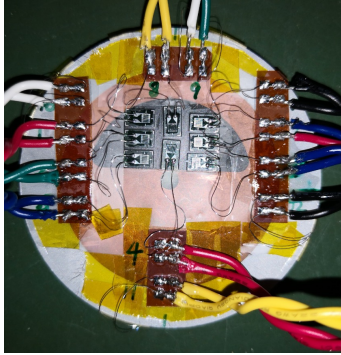


The HTS crystals are embedded (shrink-fit) into a copper matrix with micro-meter accuracy, to be mechanical and thermally stabilised. An additional Aluminium shrinking cylinder is used to precisely assemble the undulator array (in the picture only a cross section)

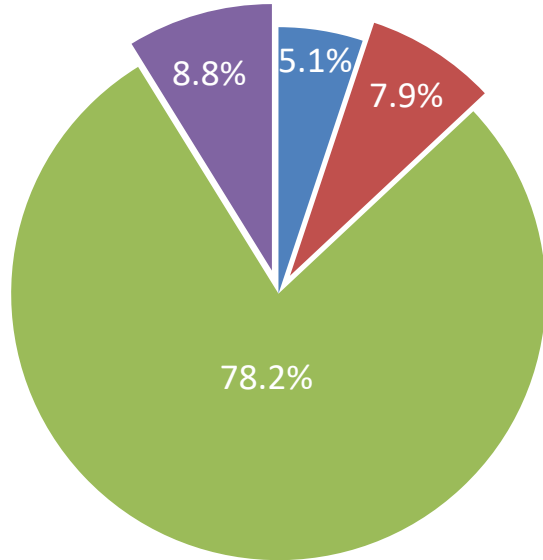




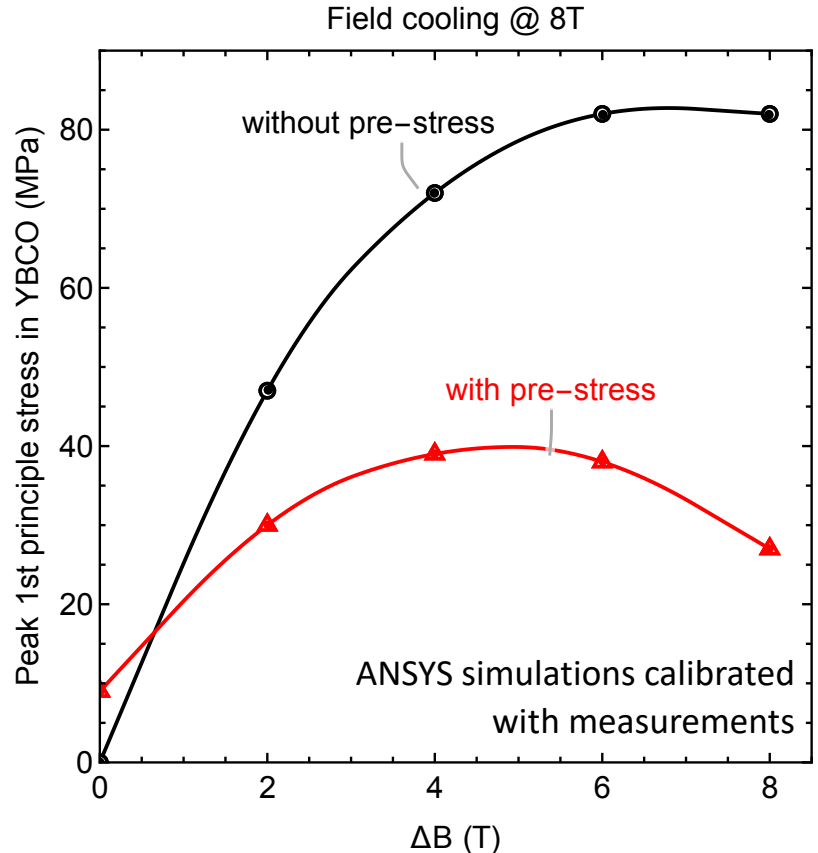
# Prestress Measurements @ 77K



# Contributions to the pre-stress in YBCO bulk



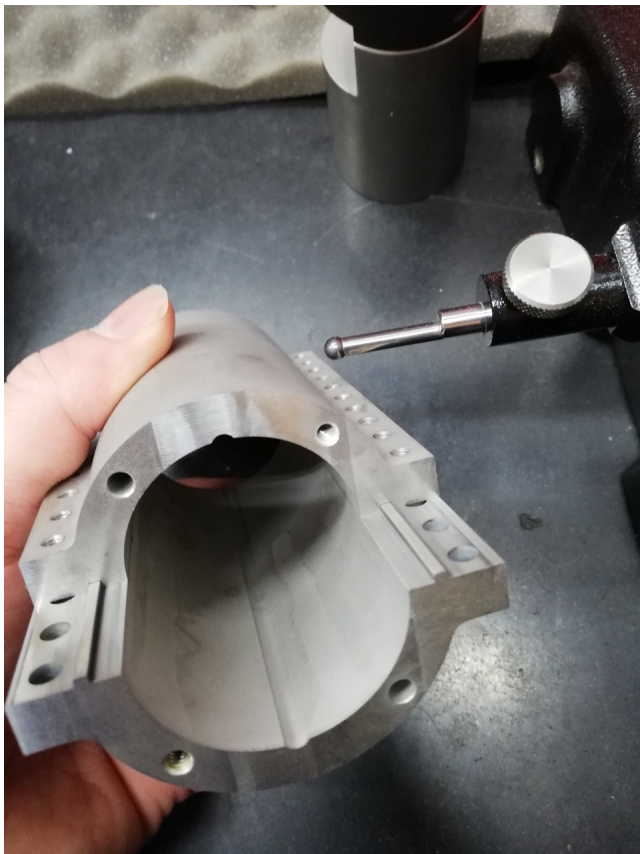
- by the shrink-fit into the Cu disk
- by the shrink-fit into the Al shell
- by the shrinking force provided by the Cu disk @ 77 K
- by the shrinking force provided by the Al shell @ 77 K

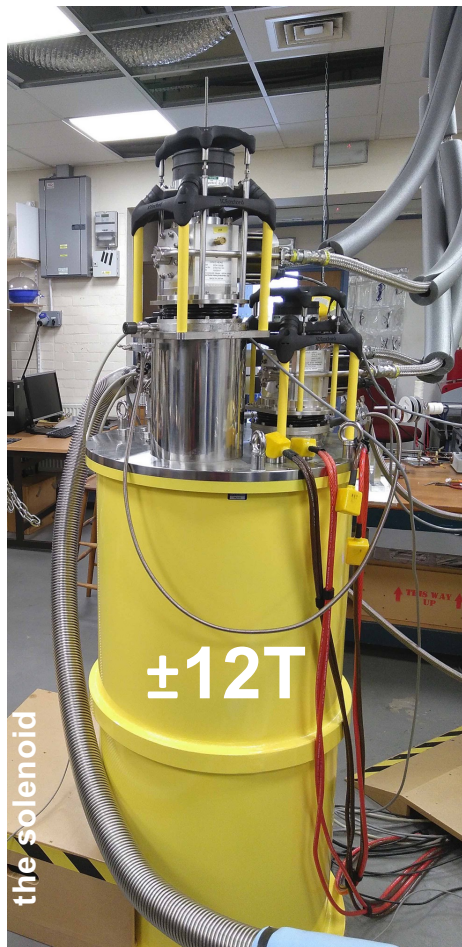


# Industrial Sample

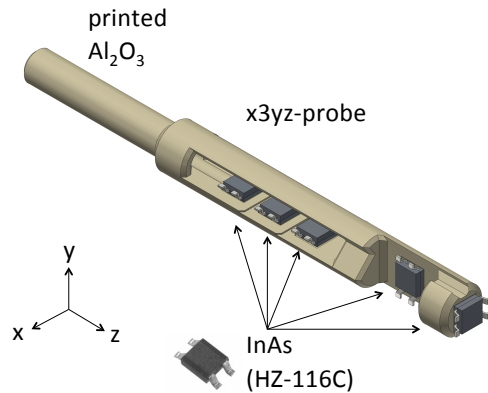
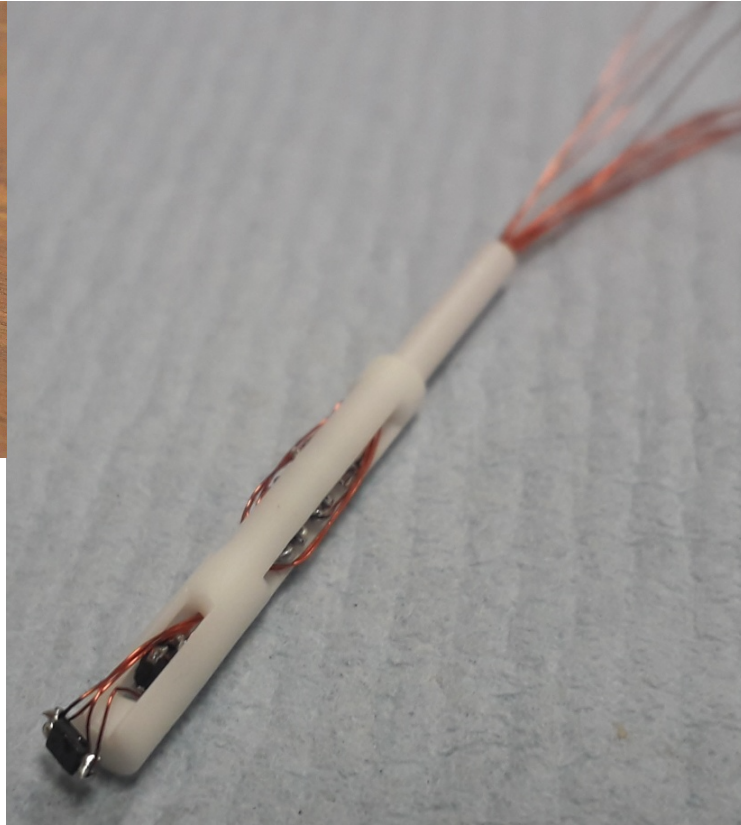
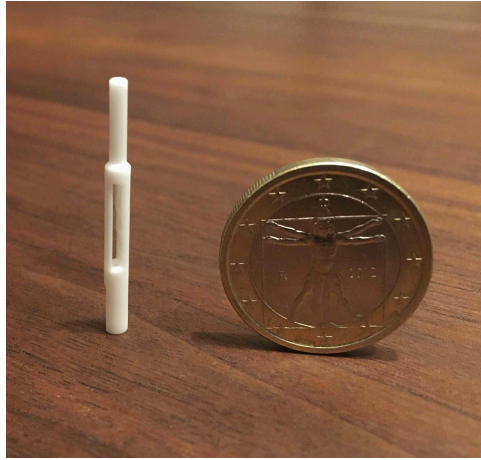


# Simplified Industrial Sample



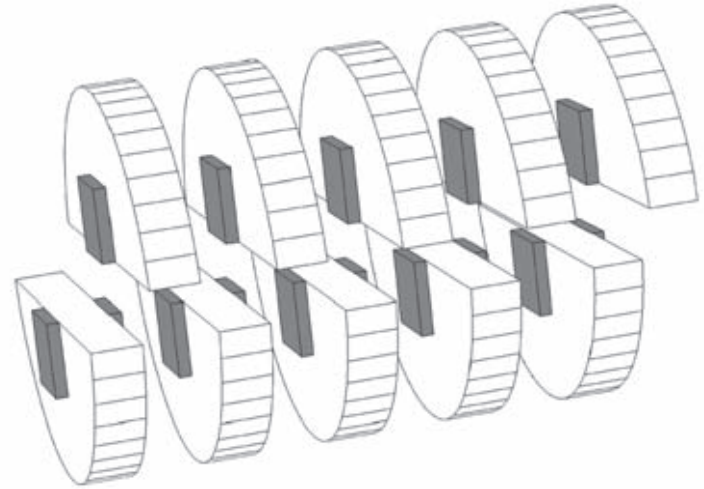
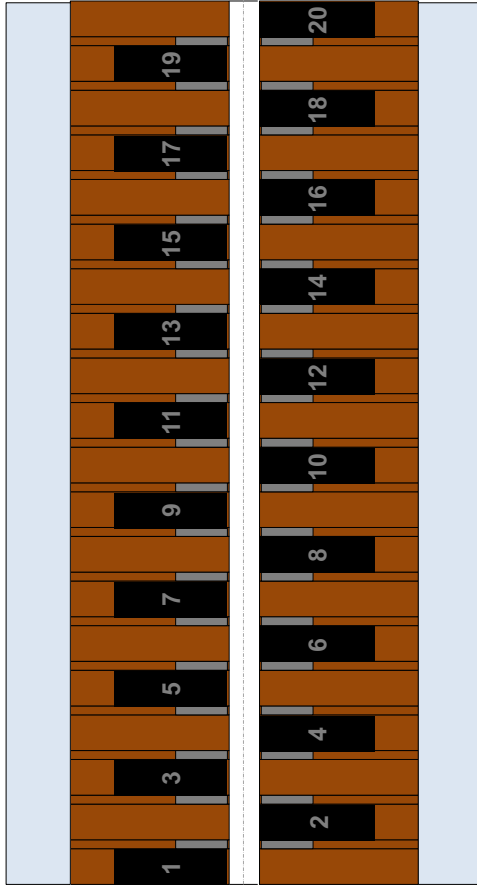


# Cryogenic probe with 5 Hall elements



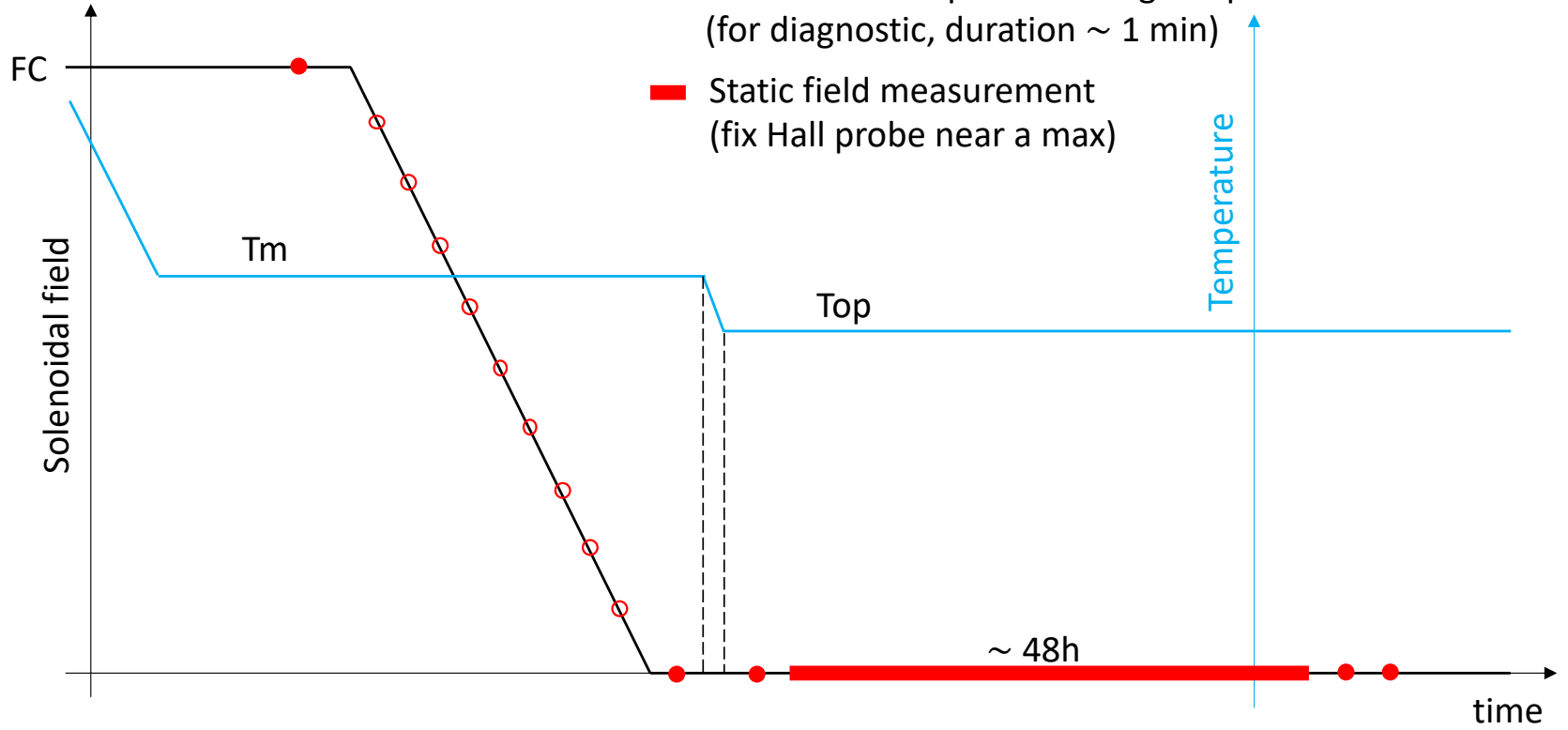
# Staggered Array With CoFe Poles

4mm gap  
10 mm period



With additional ferromagnetic poles :

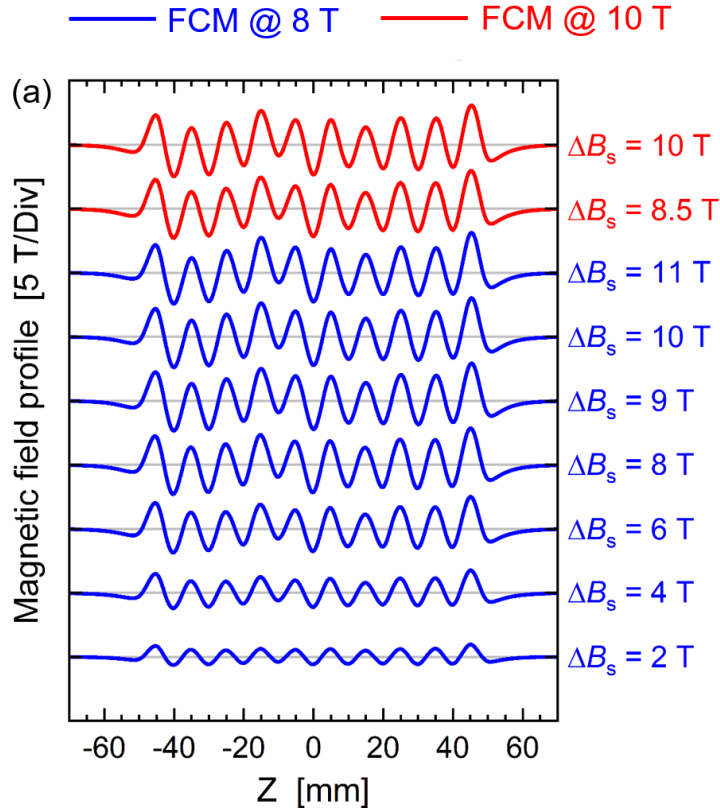
CoFe  $\Delta B_0 = +0.20 \text{ T}$



- Undulator field profile during plateau
- Undulator field profile during ramp (for diagnostic, duration ~ 1 min)
- Static field measurement (fix Hall probe near a max)

FC, Field Cooling magnetisation level, 10T  
 Tm, magnetisation temperature ~ 10K  
 Top, operational temperature ~ 7K





### Inverse analysis of critical current density in a bulk high-temperature superconducting undulator


Ryota Kinjo<sup>✉</sup>

*RIKEN SPring-8 Center, 1-1-1, Koto, Sayo-cho, Sayo-gun, Hyogo, Japan*

Marco Calvi<sup>✉</sup>, Kai Zhang<sup>✉</sup>, Sebastian Hellmann<sup>✉</sup>, Xiaoyang Liang<sup>✉</sup>, and Thomas Schmidt  
*Paul Scherrer Institut, Forschungsstrasse 111, 5232 Villigen PSI, Switzerland*

Mark D. Ainslie<sup>✉</sup>, Anthony R. Dennis<sup>✉</sup>, and John H. Durrell<sup>✉</sup>

*Department of Engineering, University of Cambridge,  
Trumpington Street, Cambridge CB2 1PZ, United Kingdom*

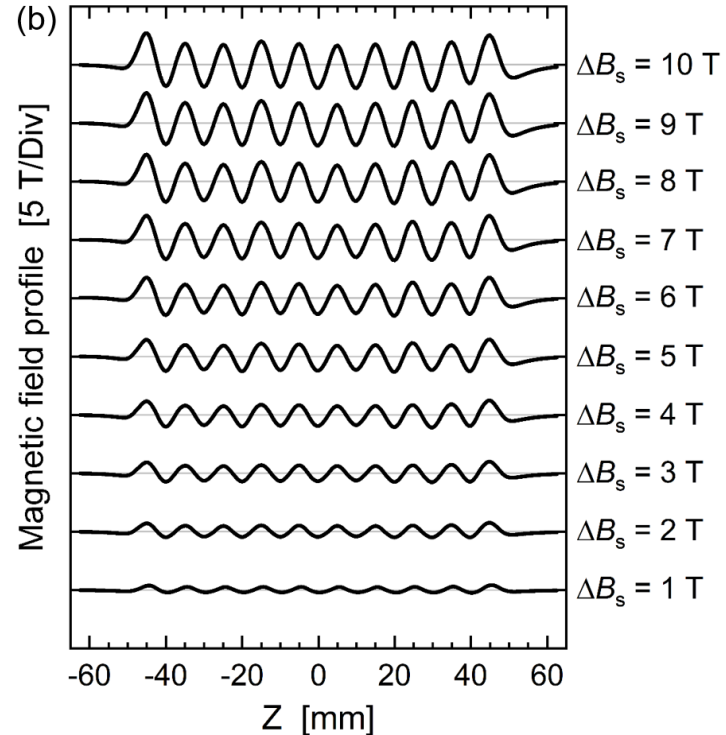
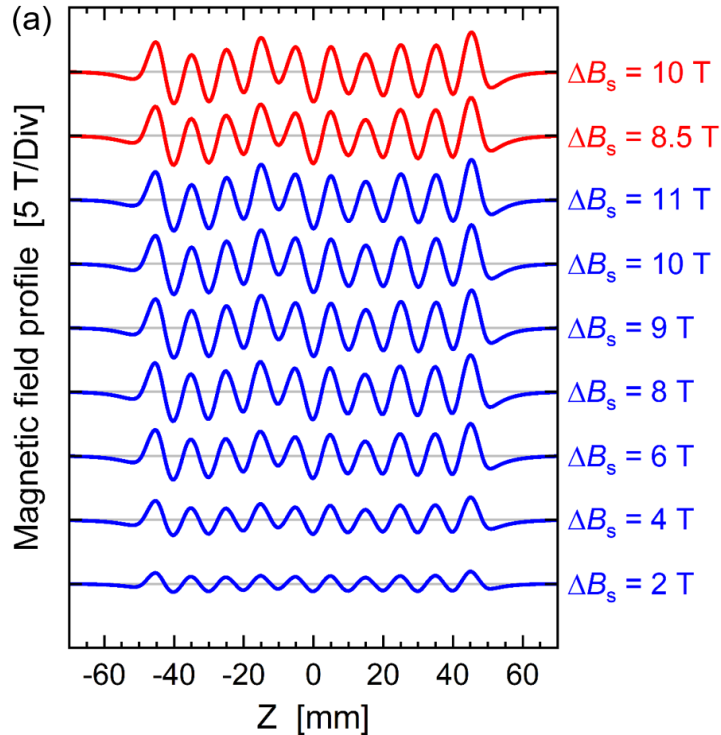
 (Received 9 September 2021; accepted 31 January 2022; published 8 April 2022)

In order to optimize the design of undulators using high-temperature superconductor (HTS) bulks we have developed a method to estimate the critical current density ( $J_c$ ) of each bulk from the overall measured magnetic field of an undulator. The vertical magnetic field was measured along the electron-beam axis in a HTS bulk-based undulator consisting of twenty Gd-Ba-Cu-O (GdBCO) bulks inserted in a 12-T solenoid. The  $J_c$  values of the bulks were estimated by an inverse analysis approach in which the magnetic field was calculated by the forward simulation of the shielding currents in each HTS bulk with a given  $J_c$ . Subsequently the  $J_c$  values were iteratively updated using the precalculated response matrix of the undulator magnetic field to  $J_c$ . We demonstrate that it is possible to determine the  $J_c$  of each HTS bulk with sufficient accuracy for practical application within around 10 iterations. The precalculated response matrix, created in advance, enables the inverse analysis to be performed within a practically short time, on the order of several hours. The measurement error, which destroys the uniqueness of the solution, was investigated and the points to be noted for future magnetic field measurements were clarified. The results show that this inverse-analysis method allows the estimation of the  $J_c$  of each bulk comprising an HTS bulk undulator.

DOI: 10.1103/PhysRevAccelBeams.25.043502

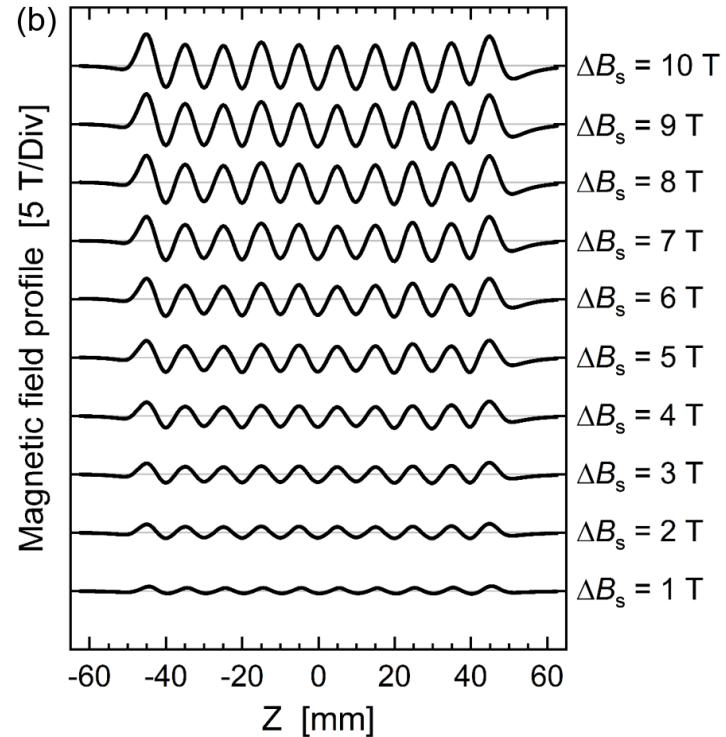
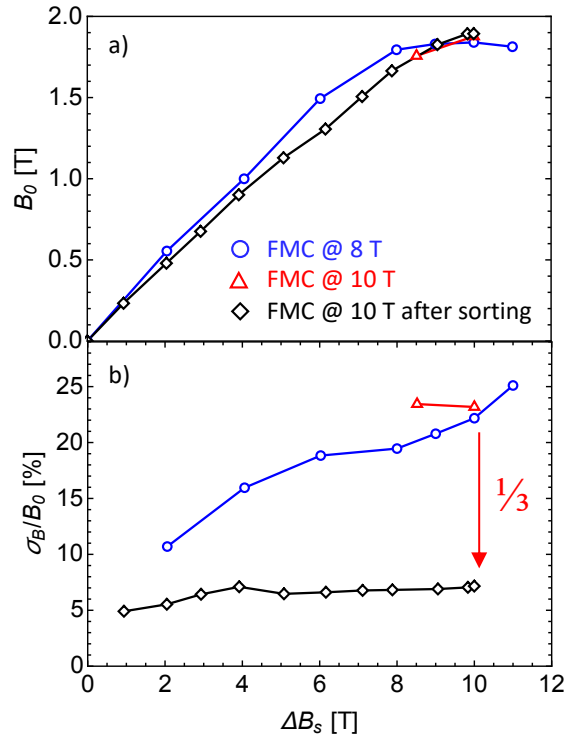
# Experimental results - YBCO from ATZ

— FCM @ 8 T    — FCM @ 10 T    — FCM @ 10 T after sorting



# Experimental results - YBCO from ATZ

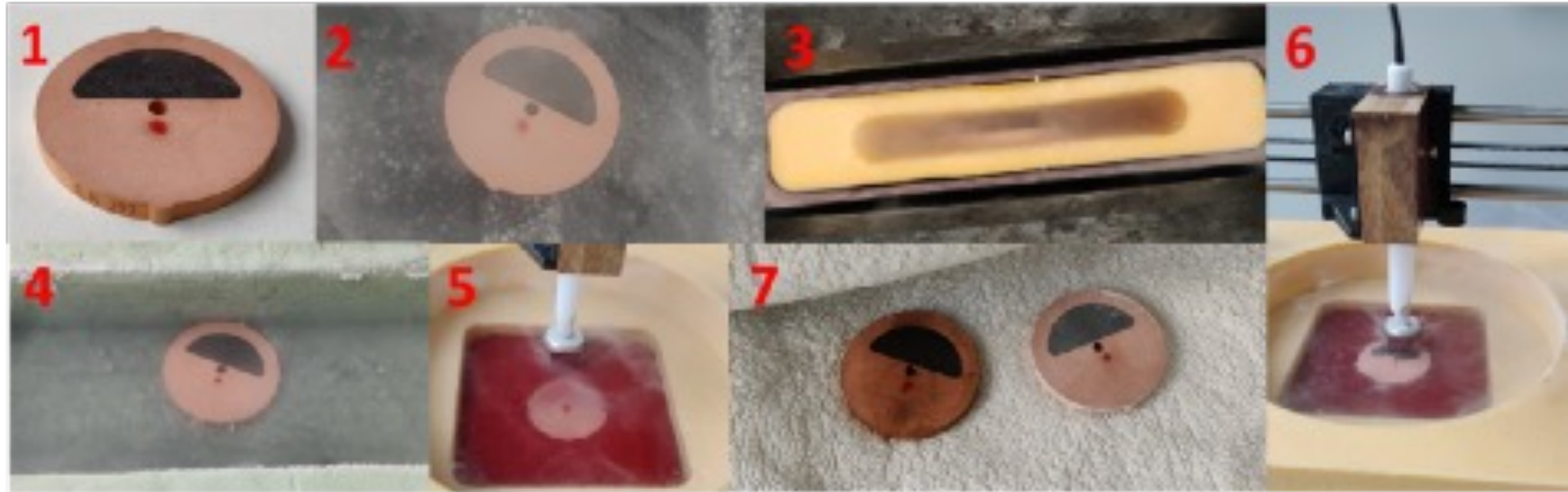
— FCM @ 8 T    — FCM @ 10 T    — FCM @ 10 T after sorting



# Single Disk characterisation

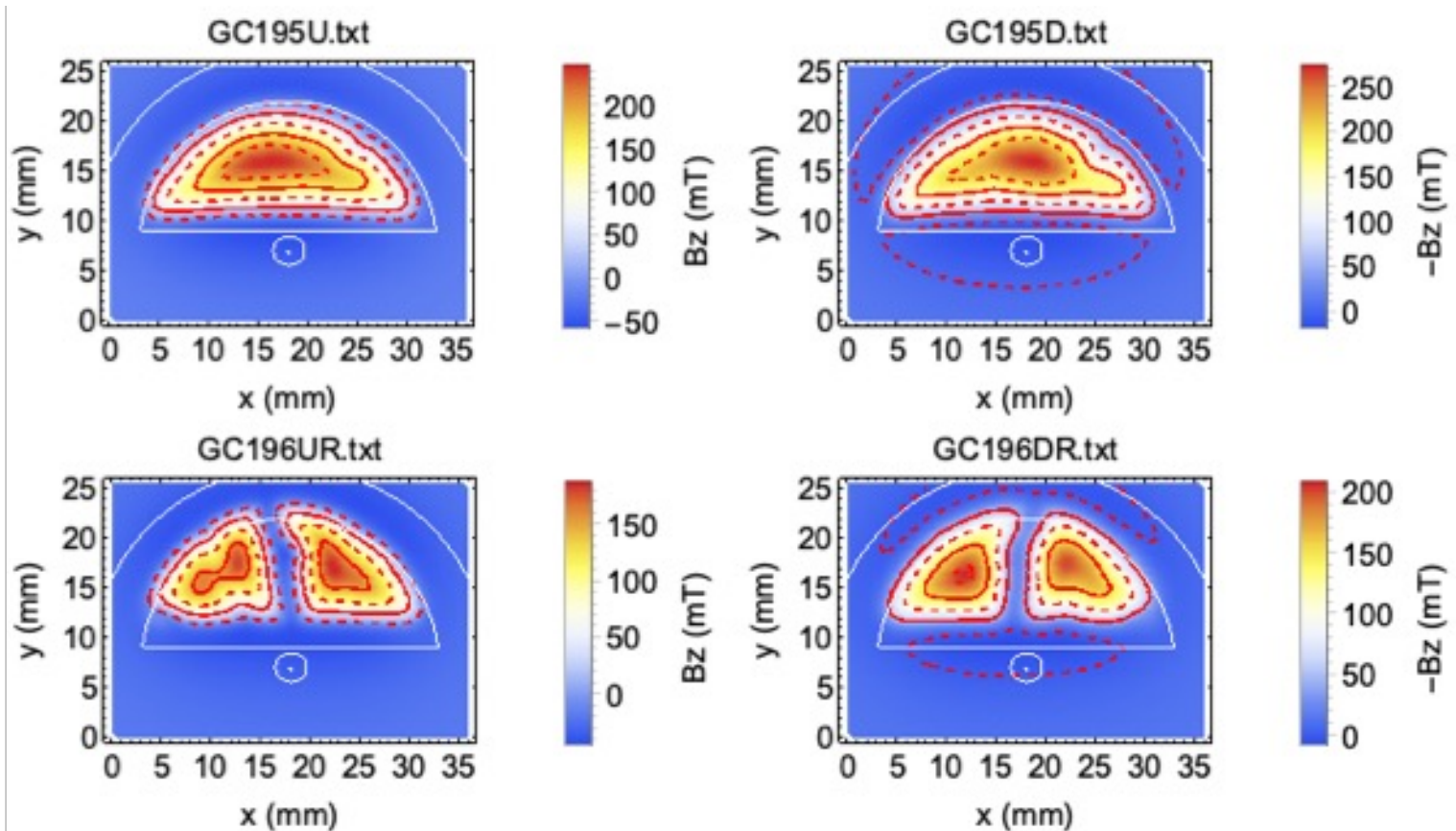
We have manufactured additional 200 disks from CAN-GdBCO / EuBCO & NS-GdBCO

All of them will be individually cooled in 1T down to LN2 and 2D field mapped, on both sides, with the aim to spot the broken ones / and to pre-sort them with respect to their strength

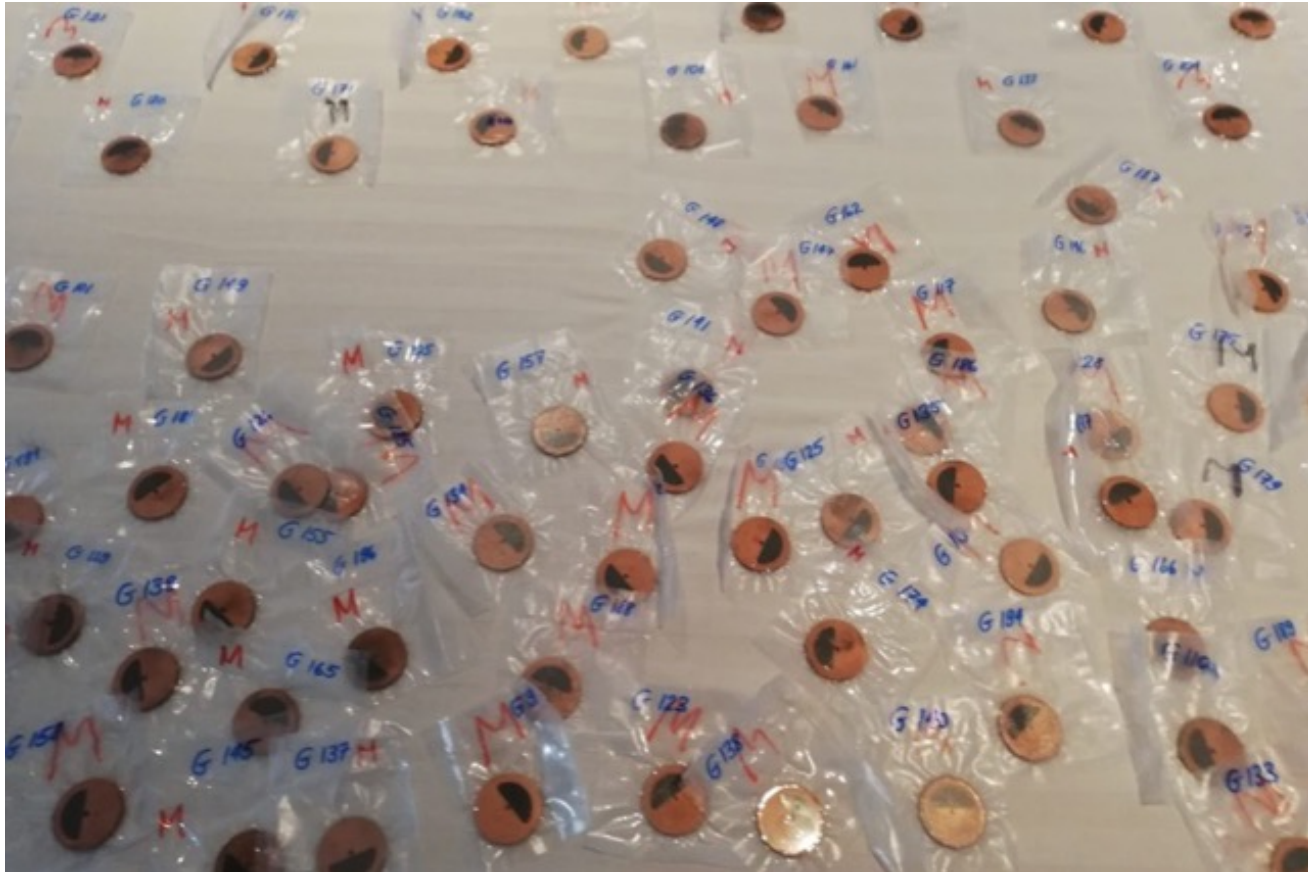


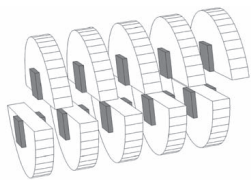
1 the disk 2 pre-cooling 3 field Cooling 4 flux creep 5 disk support 6 2D field map 7 drying

## 2D Field map

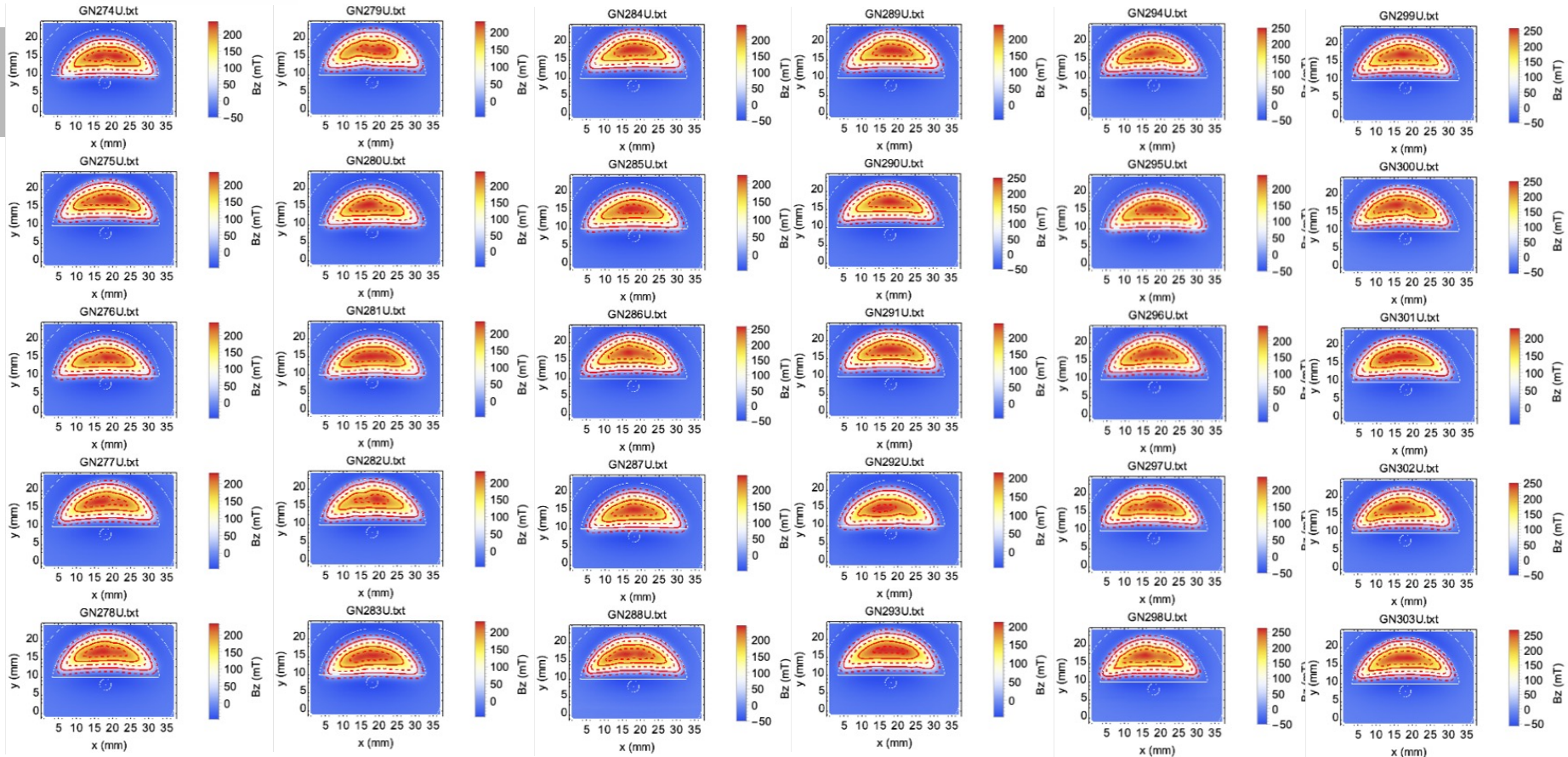


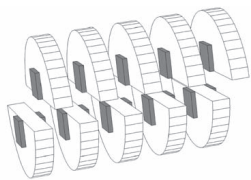
# Pre-sorting / Stacking



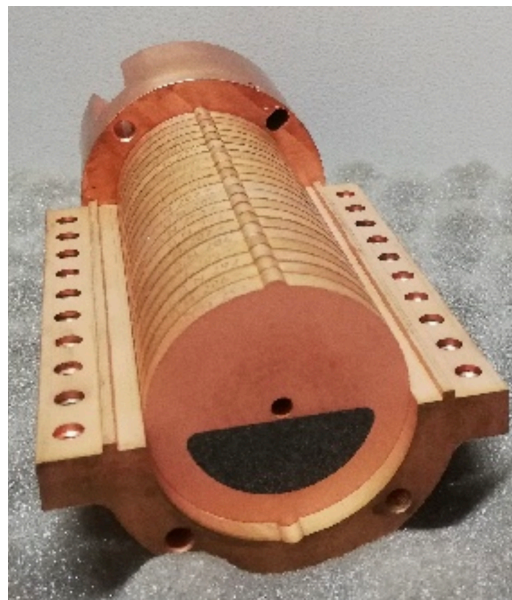
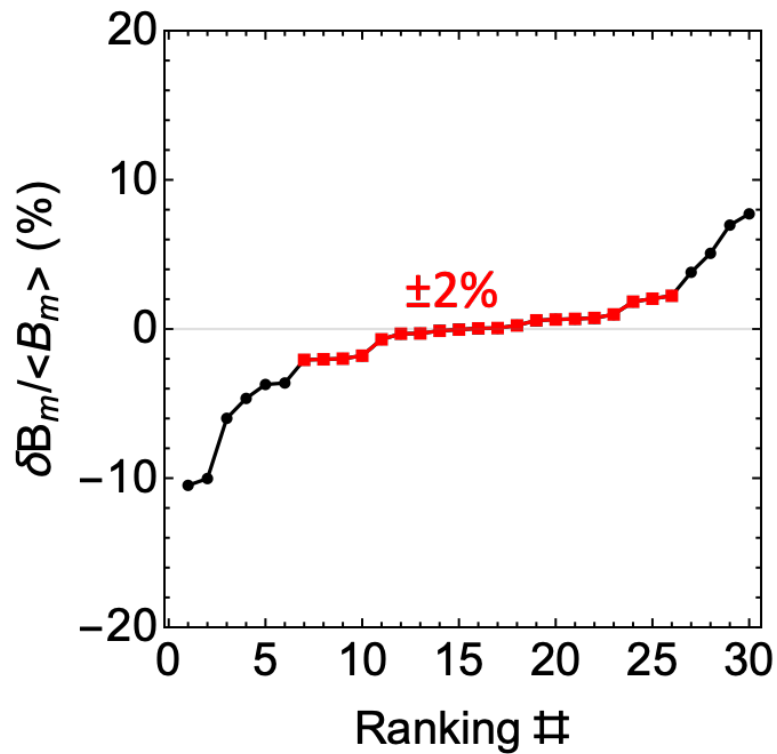


# Planar Hybrid: Nippon Steel

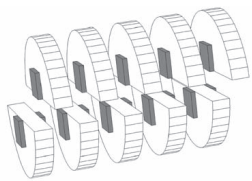




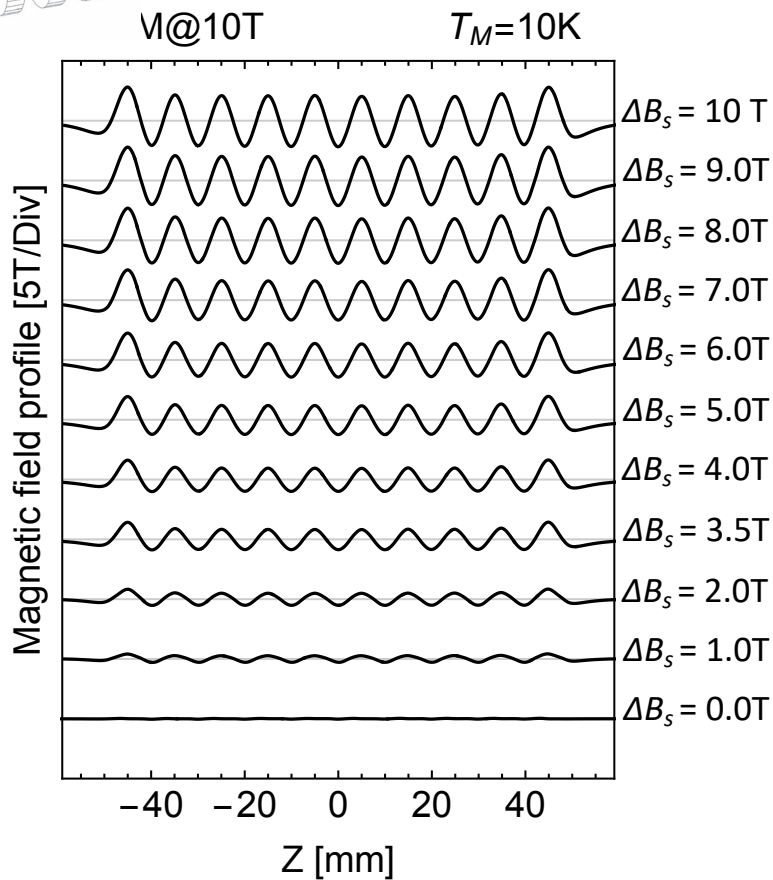
# Planar Hybrid: Nippon Steel

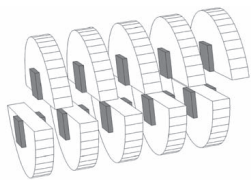




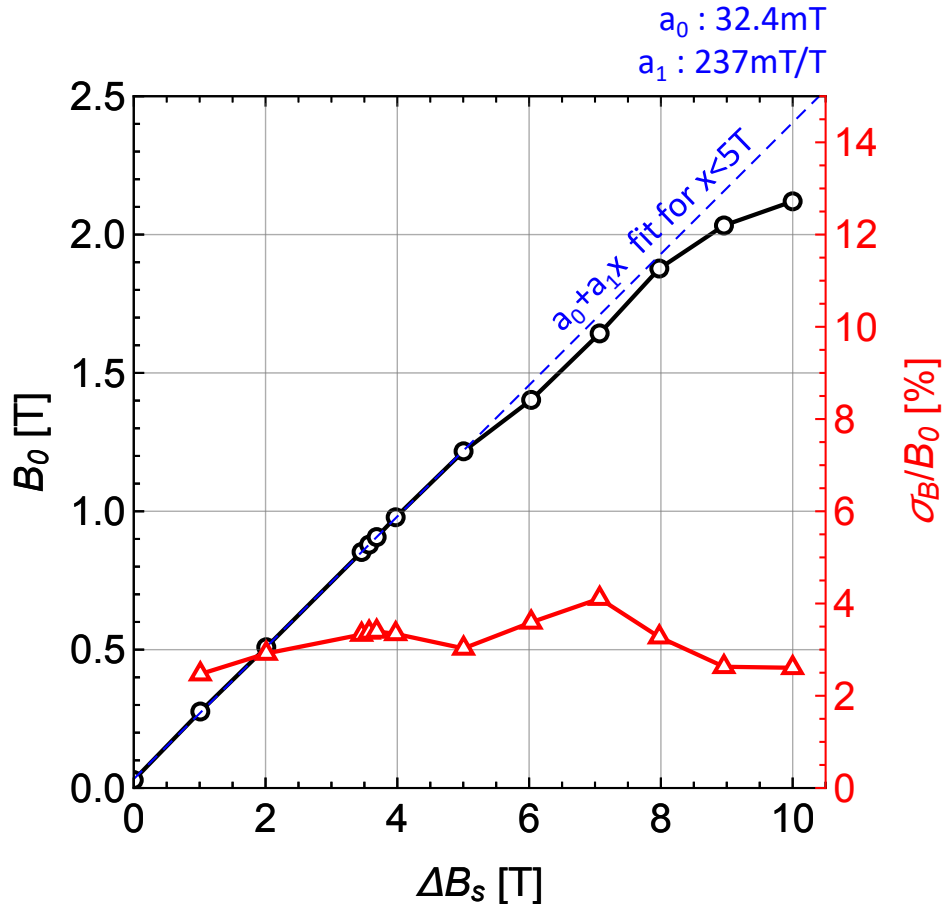


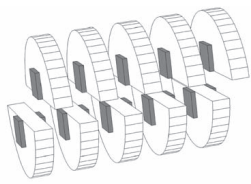
# Planar Hybrid: Nippon Steel





# Planar Hybrid: Nippon Steel





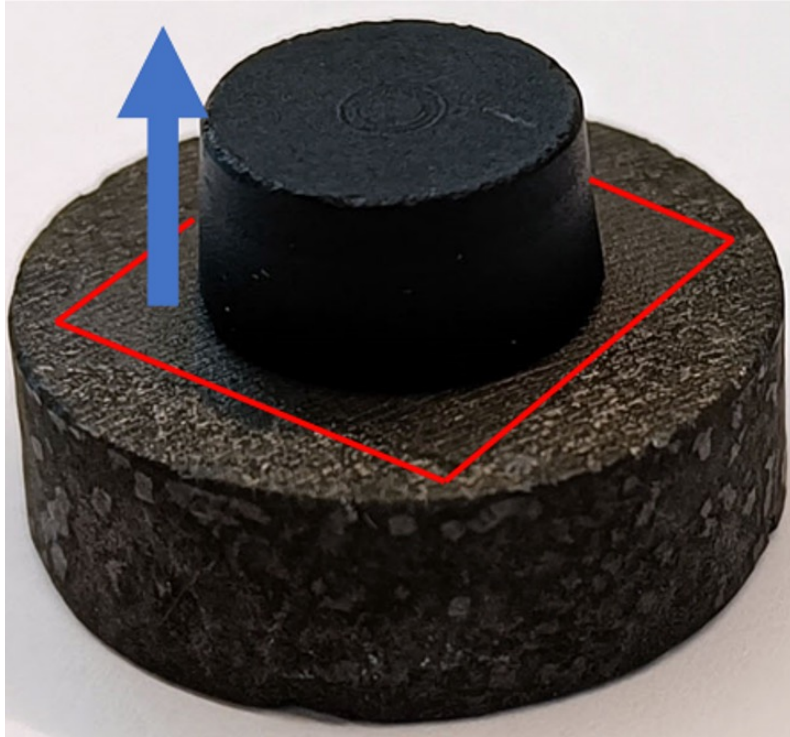
## Planar Hybrid: Nippon Steel

It looks a perfect result... BUT:

- “We” paid the raw-bulks about 2600 € each
- NS does not deliver REBCO bulks outside Japan...
- Since 2023 NS decided not to deliver anymore bulks to customers also in Japan... they are keeping this activity as an internal R&D.

→ ARE WE BACK TO SQUARE ONE????

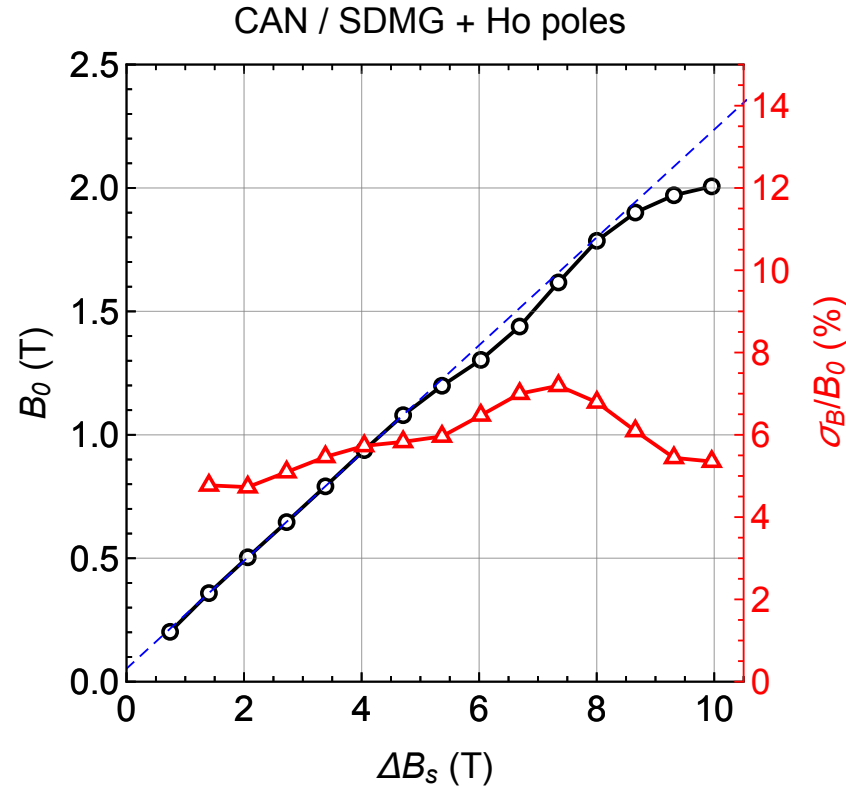
# CAN-SUPERCONDUCTOR: SDMG



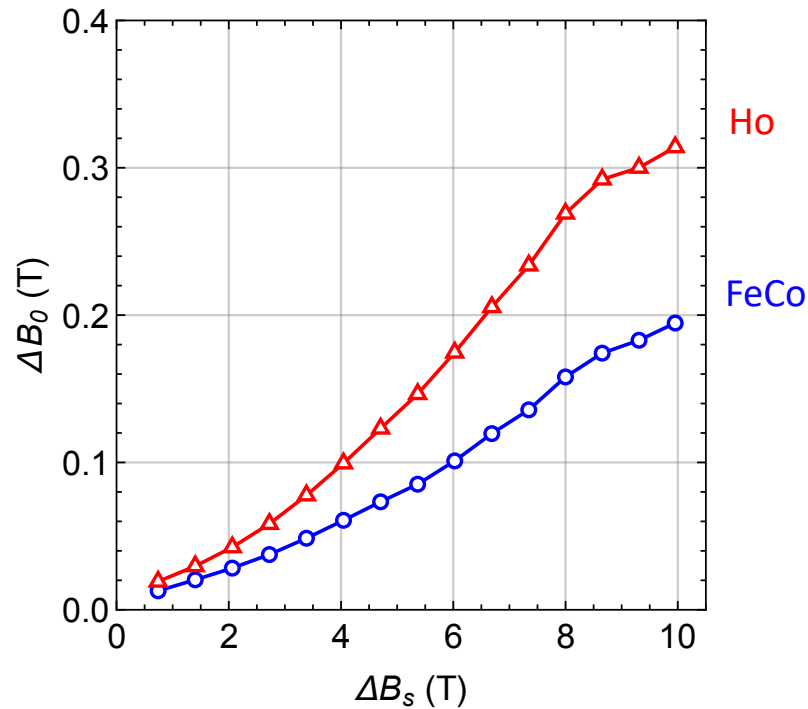
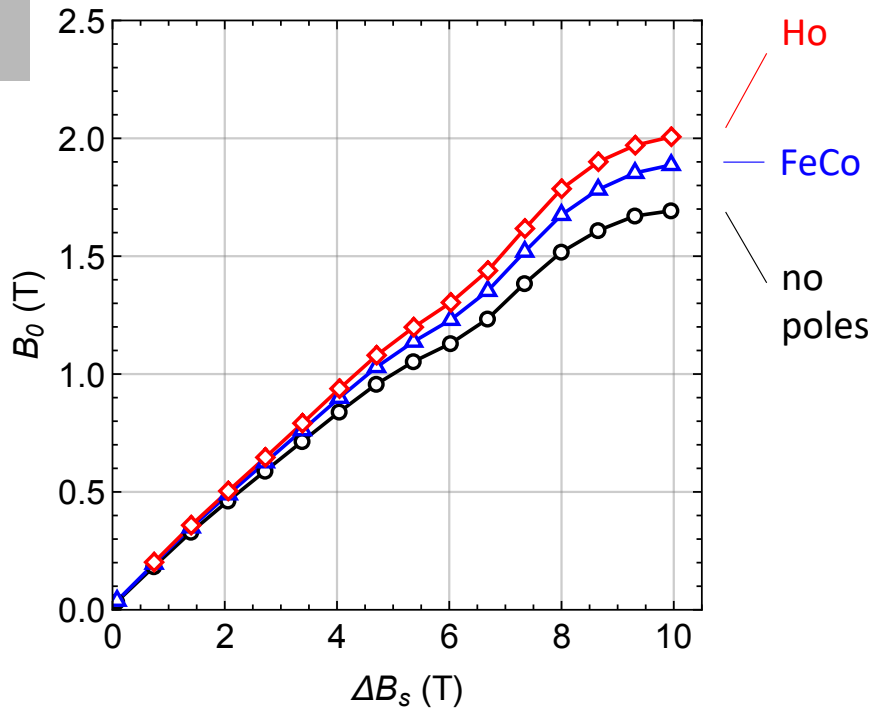
- **Single-direction Melt Growth (SDMG)** is a novel approach for REBCO single-domain bulk growth, where a grown bulk from a REBCO system with higher peritectic temperature is used to seed the grown bulk (instead of a NdBCO thin-film seed, which is used for both TSMG and TSIG). The main advantage of this approach is that the bulk is composed exclusively of the c-growth region, unlike TSMG-grown bulks. Therefore, the expected homogeneity is significantly higher in SDMG-grown bulks, as no growth interfaces are present in the bulks.

*Courtesy of Dr Tomáš Hlášek (CAN)*

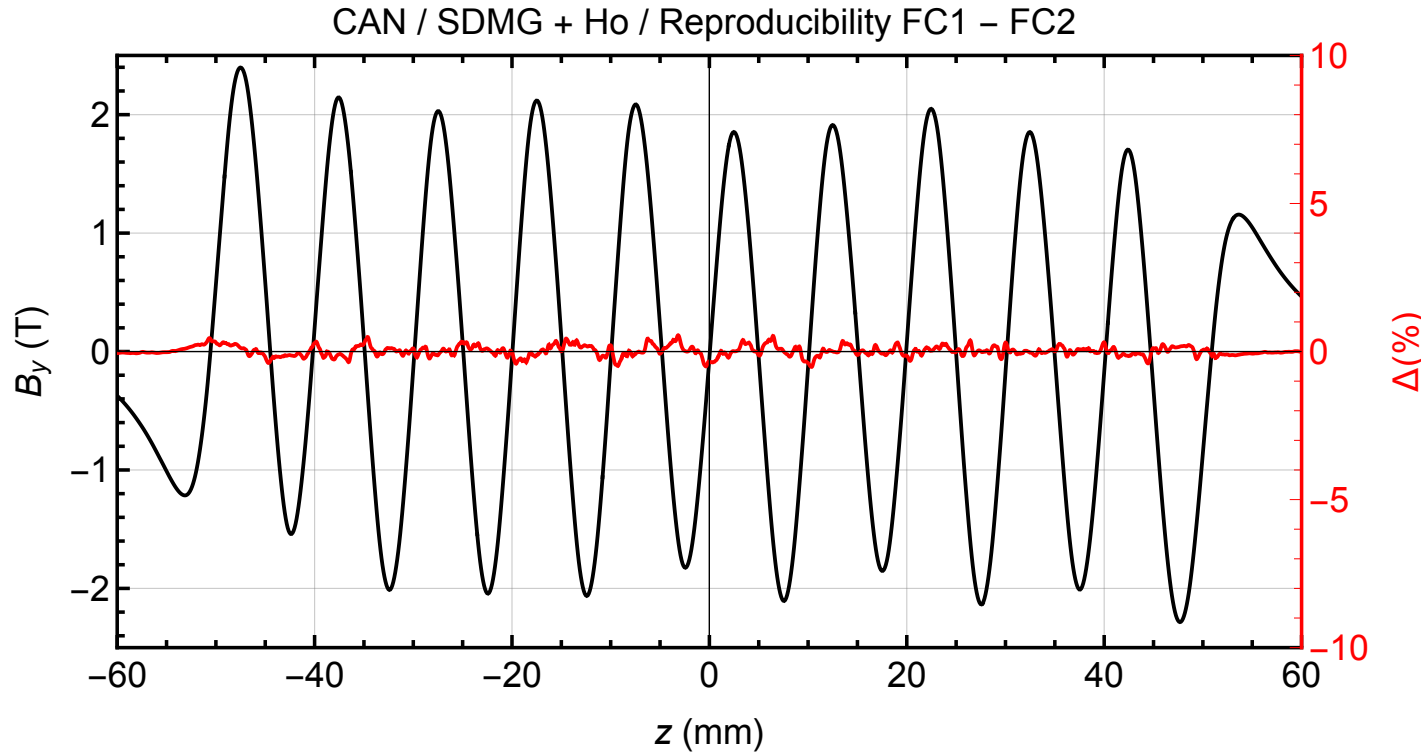
# CAN / SDMG + Ho poles



CAN / SDMG at 10K

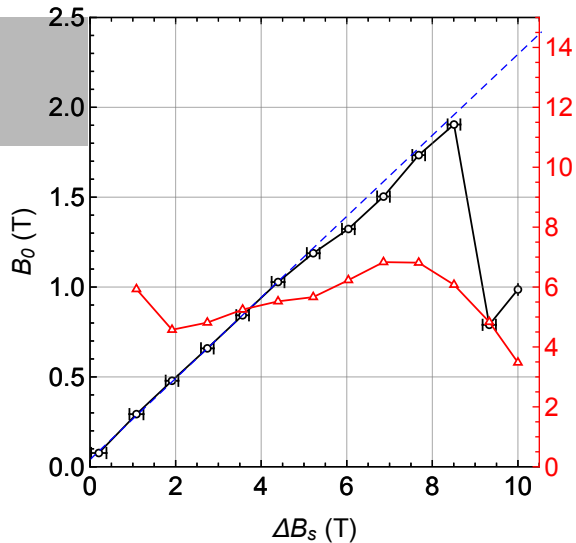


# FC reproducibility study

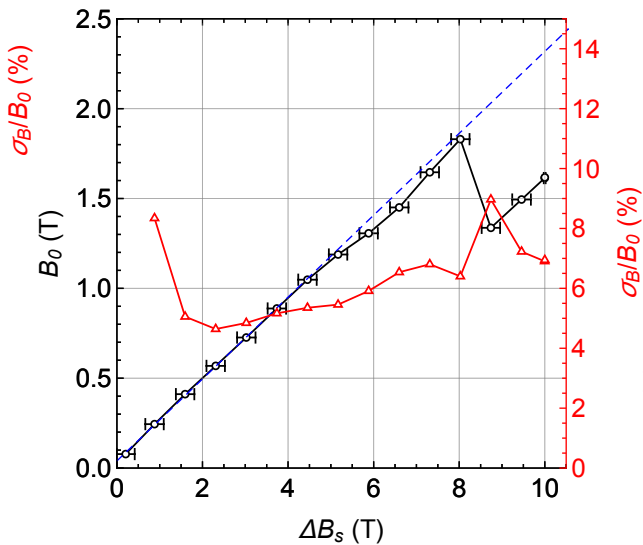


# Ramp rate studies: our baseline is 1T/h

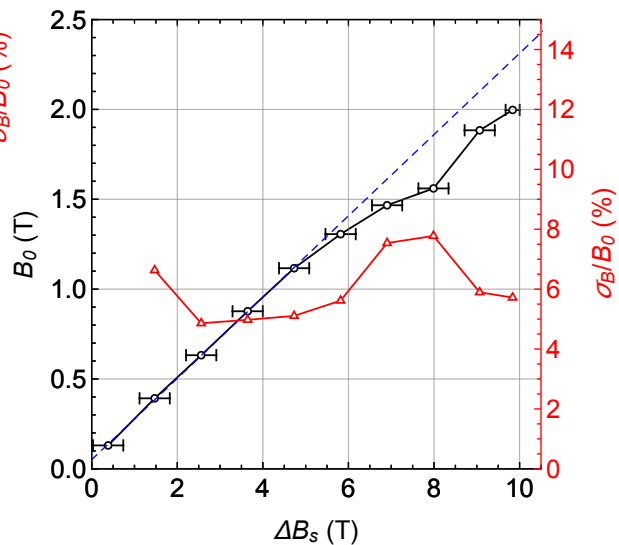
CAN SDMG Ho 2T/h 2nd-run



CAN SDMG Ho 3T/h 1st-run



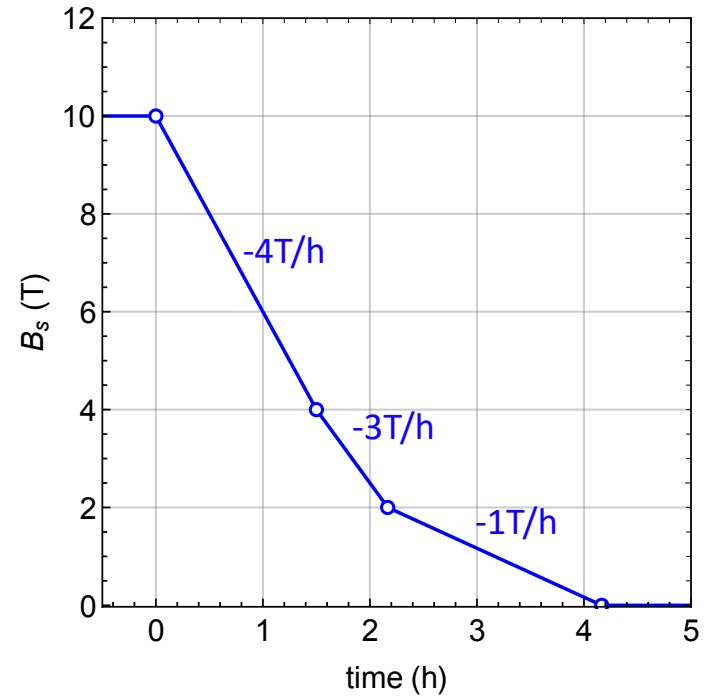
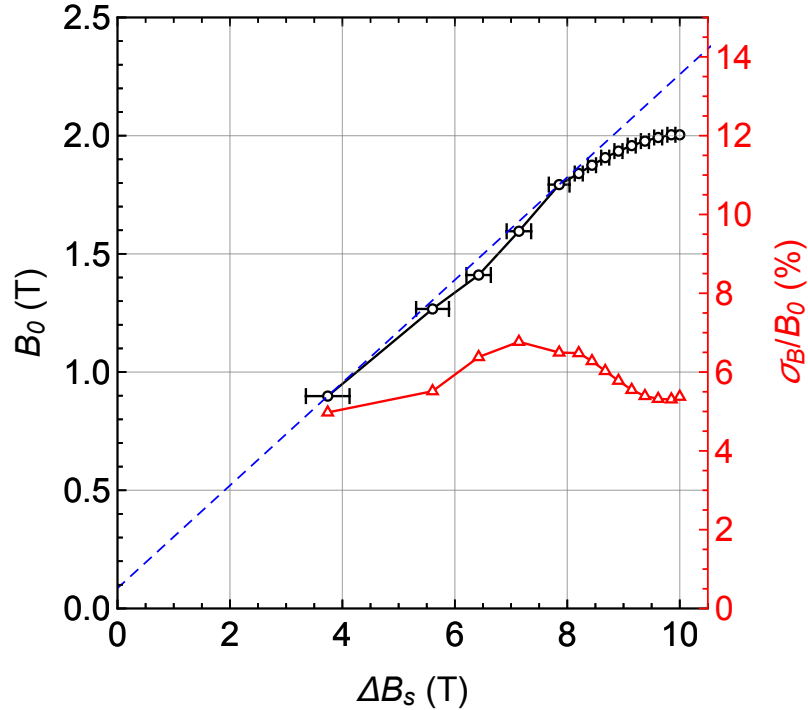
CAN SDMG Ho 4T/h 1st-run





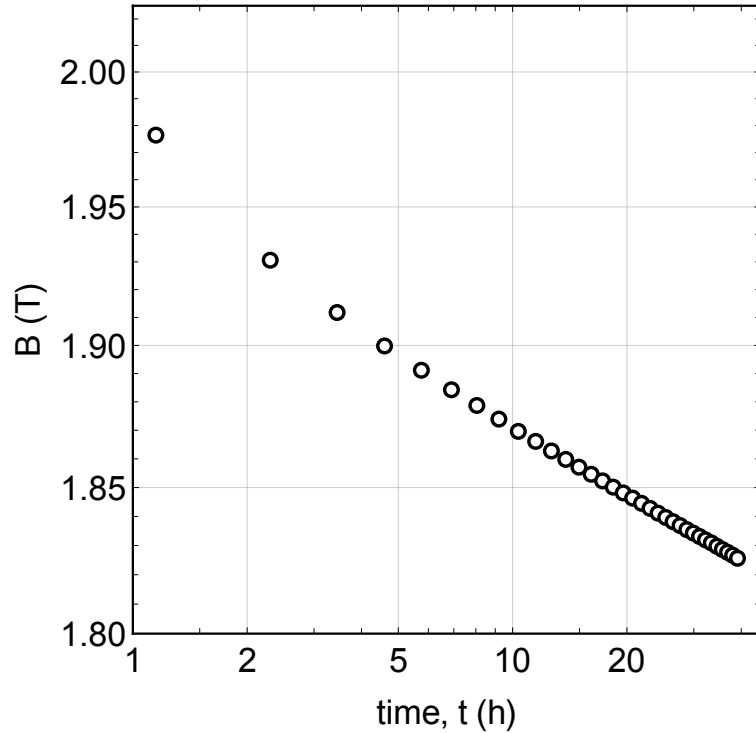
# Towards a quasi-optimum charging time

CAN SDMG Ho optimum charging



## Flux creep and flux freezing

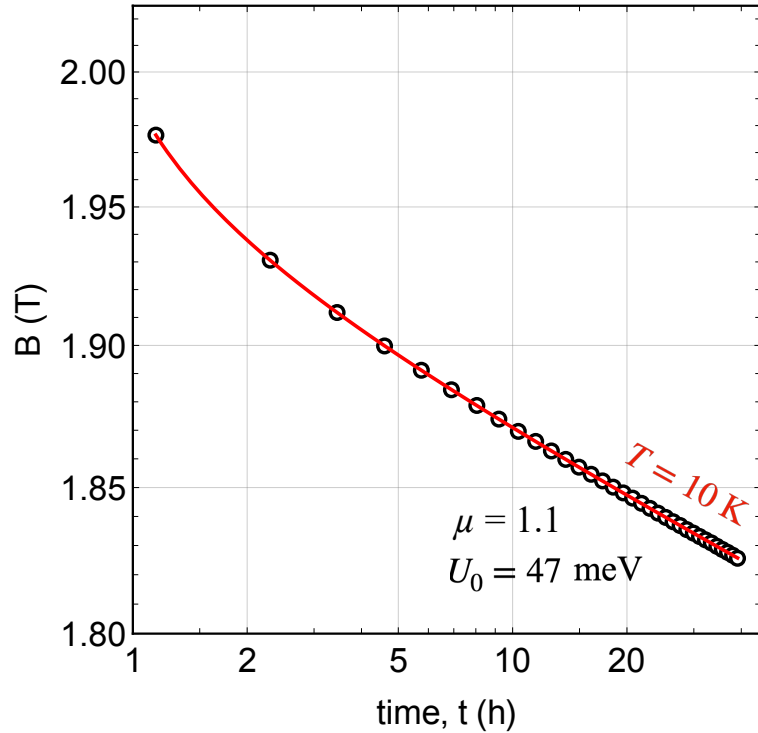
$$T_M = 10 \text{ K}$$

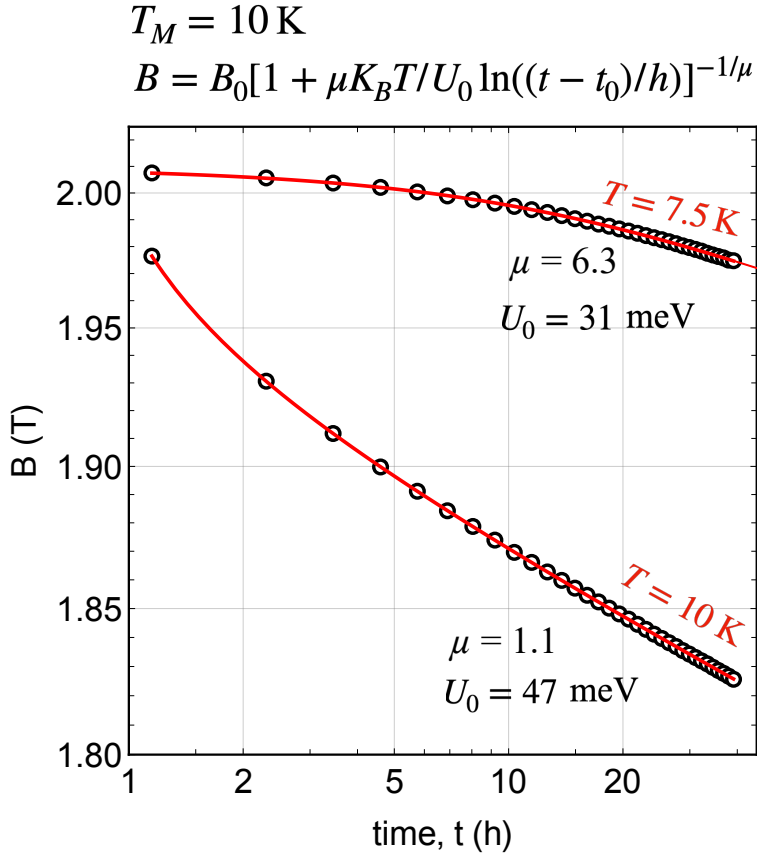


# Flux creep and flux freezing

$$T_M = 10 \text{ K}$$

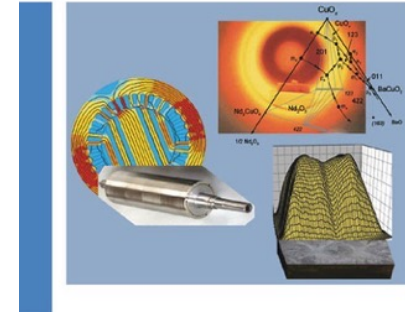
$$B = B_0 [1 + \mu K_B T / U_0 \ln((t - t_0)/h)]^{-1/\mu}$$





*Extrapolate to 1 year the field would be around 1.82T*

**NB:** Experiment in preparation to actively stabilise the field amplitude introducing an “acceptable” solenoidal field component.

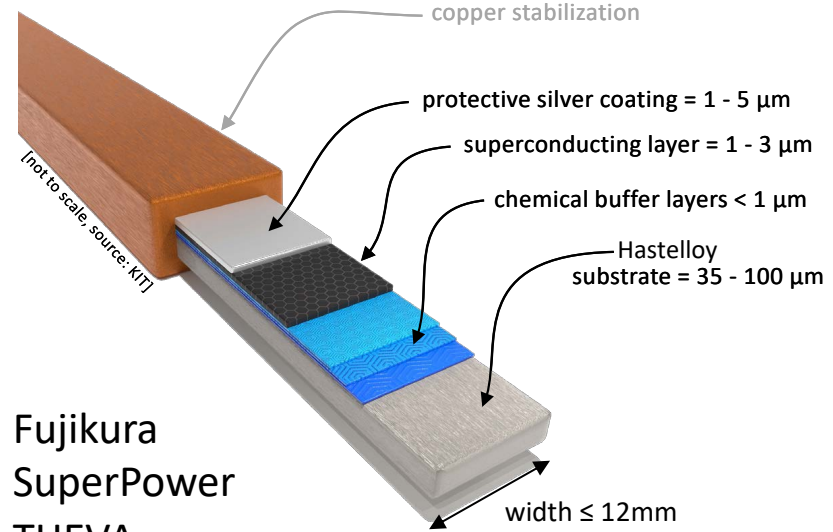


- Brief introduction to accelerator based light sources
- The Tomographic Microscopy beamline: TOMCAT → I-TOMCAT
- The HTS (REBCO) bulk Staggered Array undulator
- The results on short samples:
  - Bulks & Stack-Tapes
- The status of the meter long HTS Undulator prototype
- Conclusions

- Brief introduction to accelerator based light sources
- The Tomographic Microscopy beamline: TOMCAT → I-TOMCAT
- The HTS (REBCO) bulk Staggered Array undulator
- The results on short samples:
  - Bulks & Stack-Tapes
- The status of the meter long HTS Undulator prototype
- Conclusions

# HTS → REBCO

## 2nd generation (2G) thin-film HTS tapes

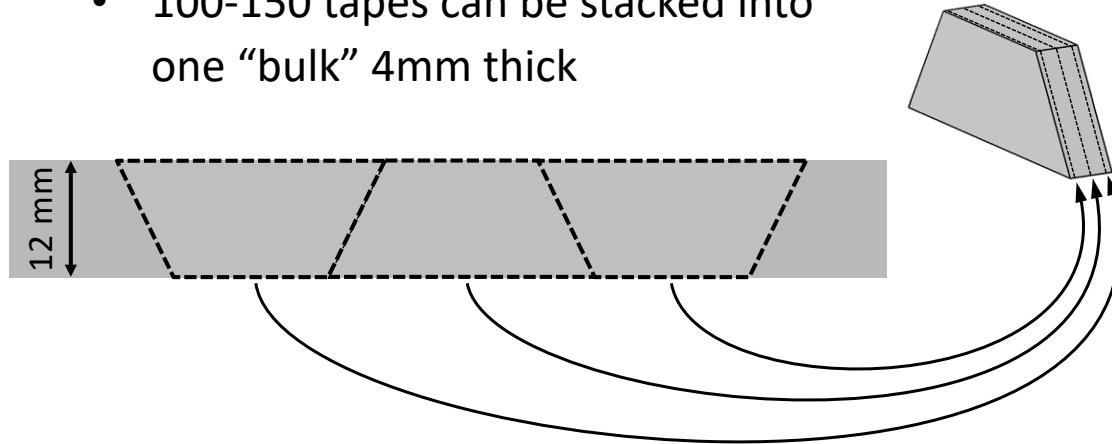


- ➔ • CAN Superconductor
- ➔ • Adelwitz Technologiezentrum
- ➔ • Nippon Steel

- Fujikura
- SuperPower
- ➔ • THEVA
- SuNAM
- AMSC
- Deutsche Nanoschicht/BASF
- ➔ • SuperOX
- BRUKER

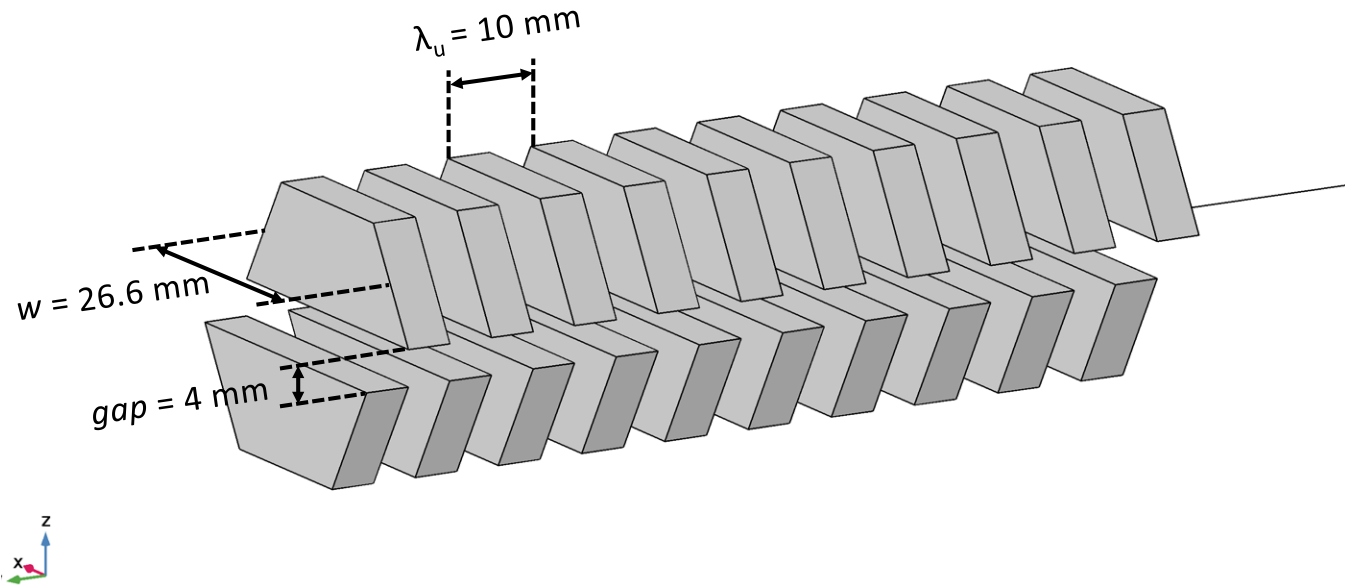
# HTS Tape Option

- Tapes are mostly stainless steel: easy to machine by spark erosion or laser cutting
- 100-150 tapes can be stacked into one “bulk” 4mm thick

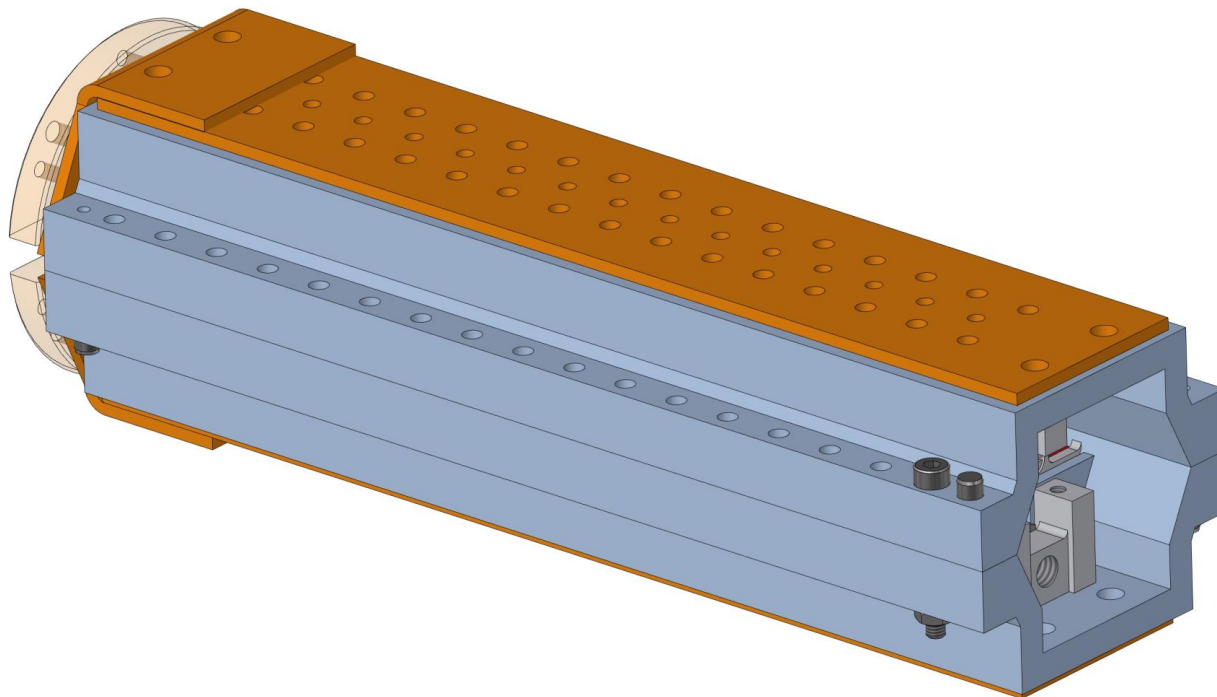




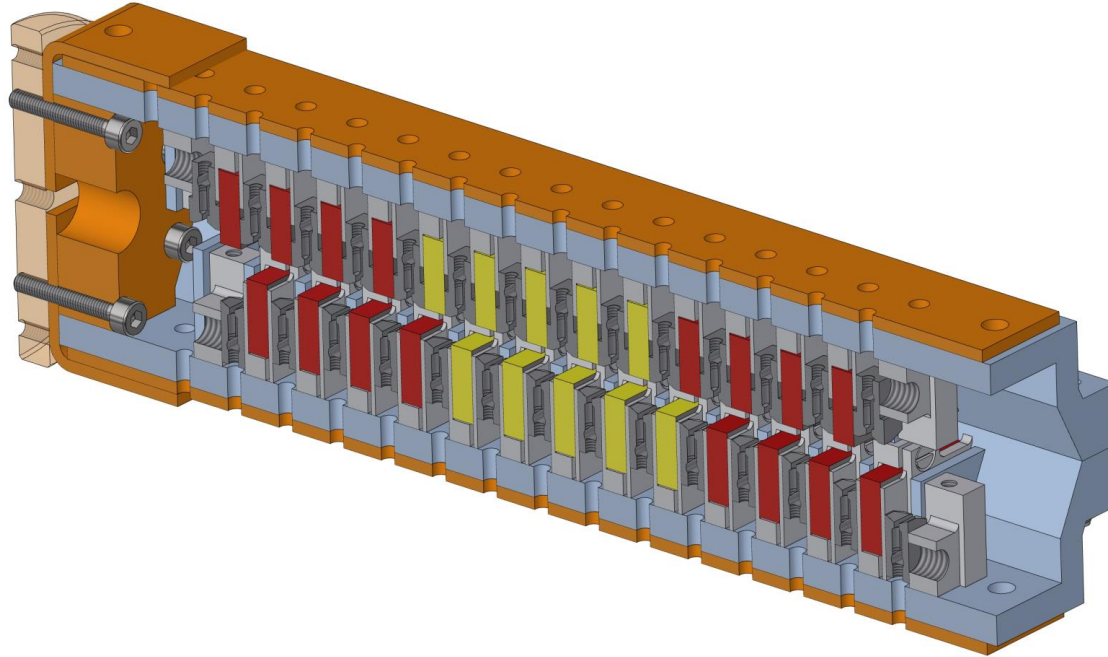
## HTS Tape Option



# HTS Tape Option



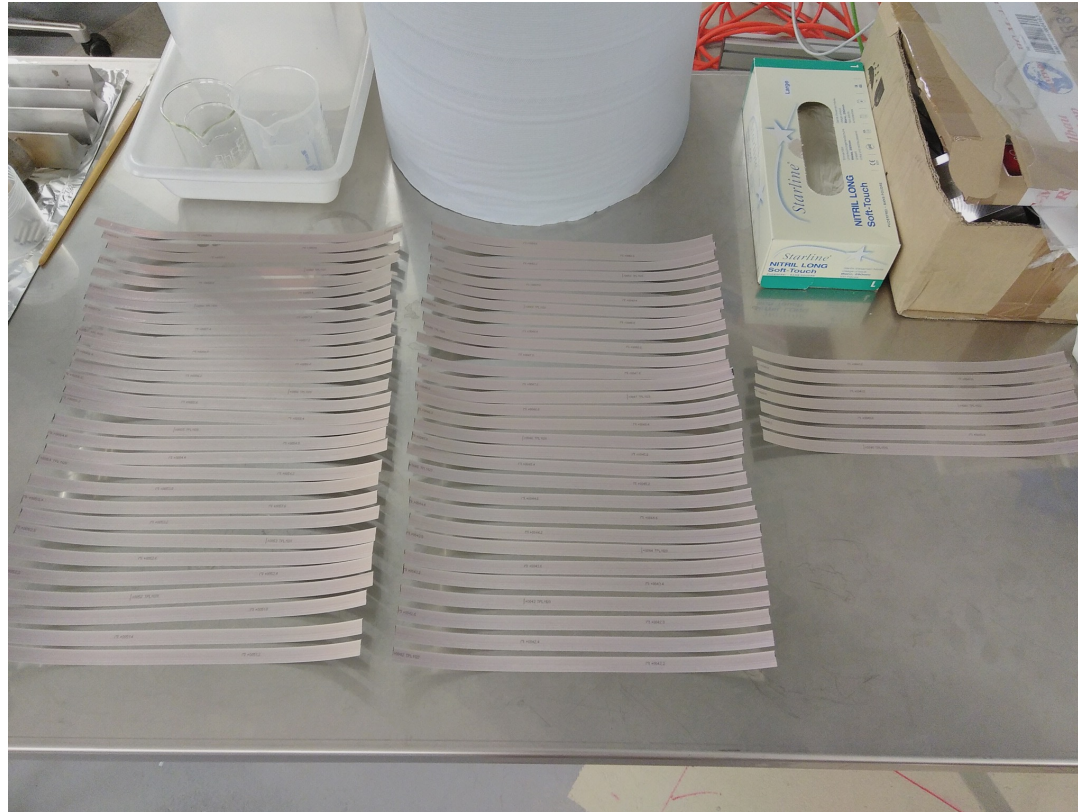
# HTS Tape Option



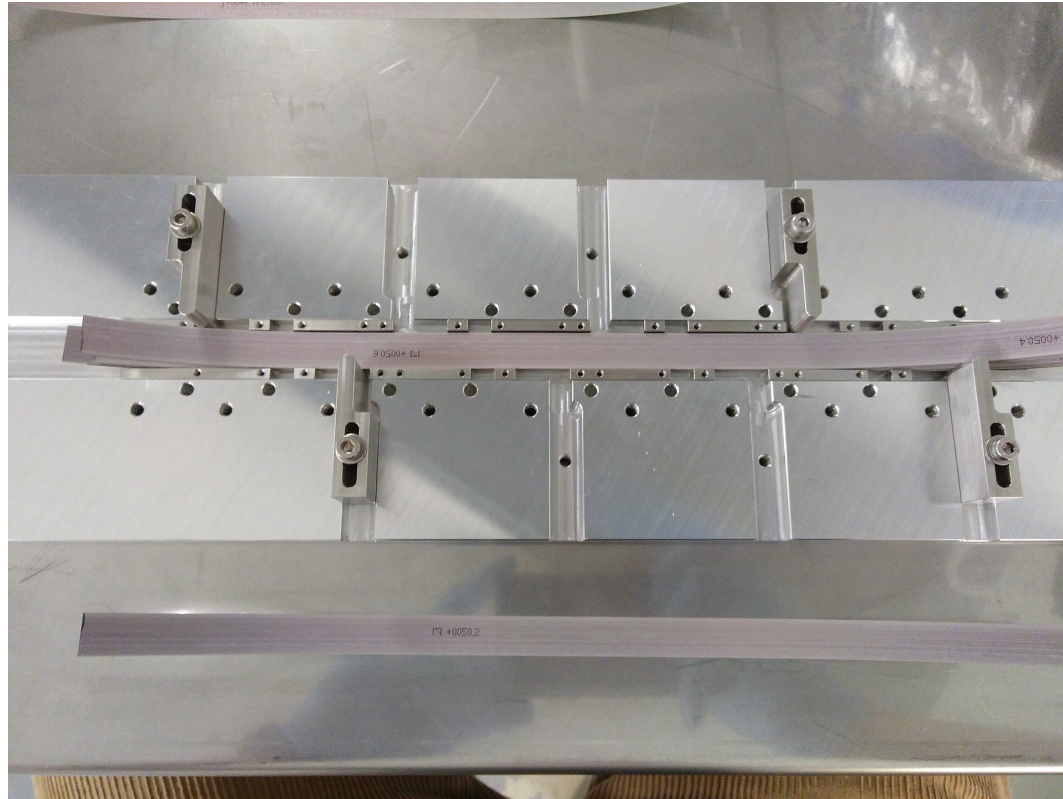
# HTS Tape Option



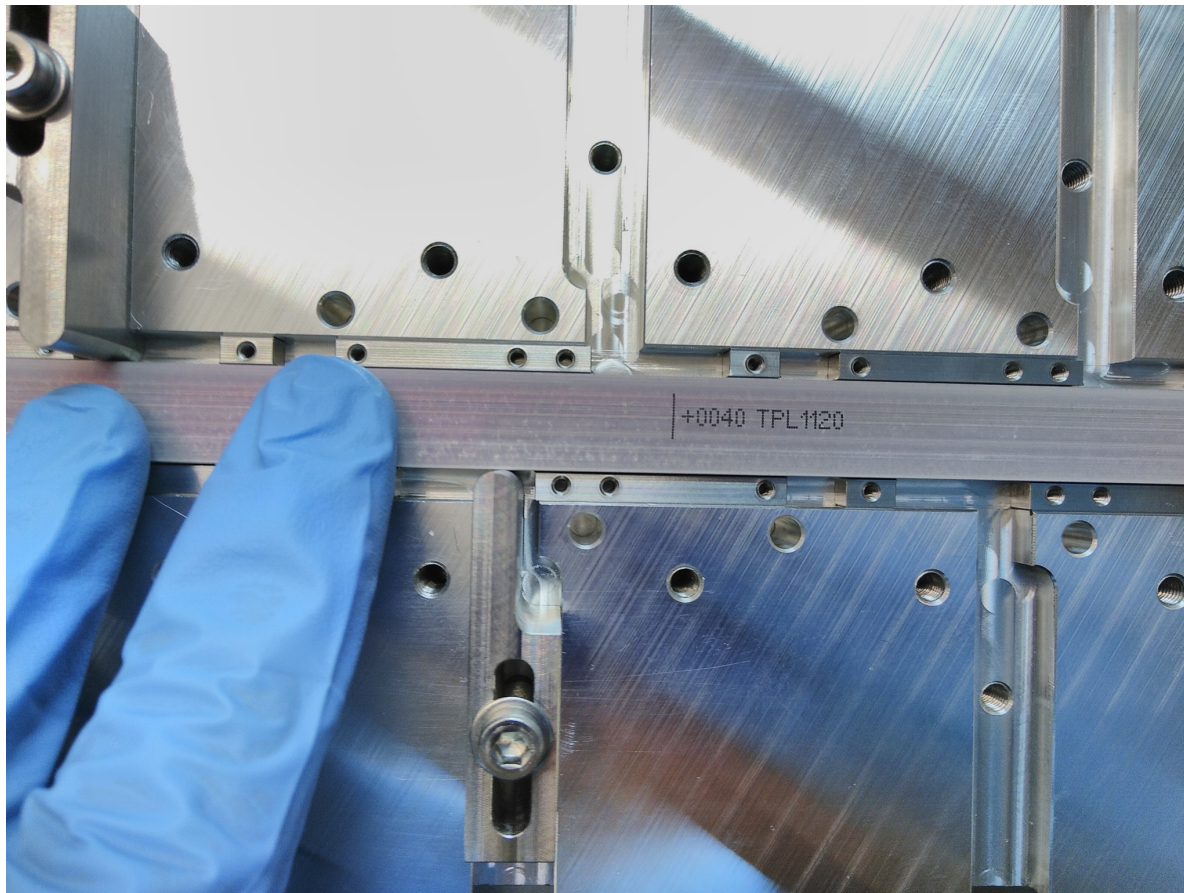
# HTS Tape Option



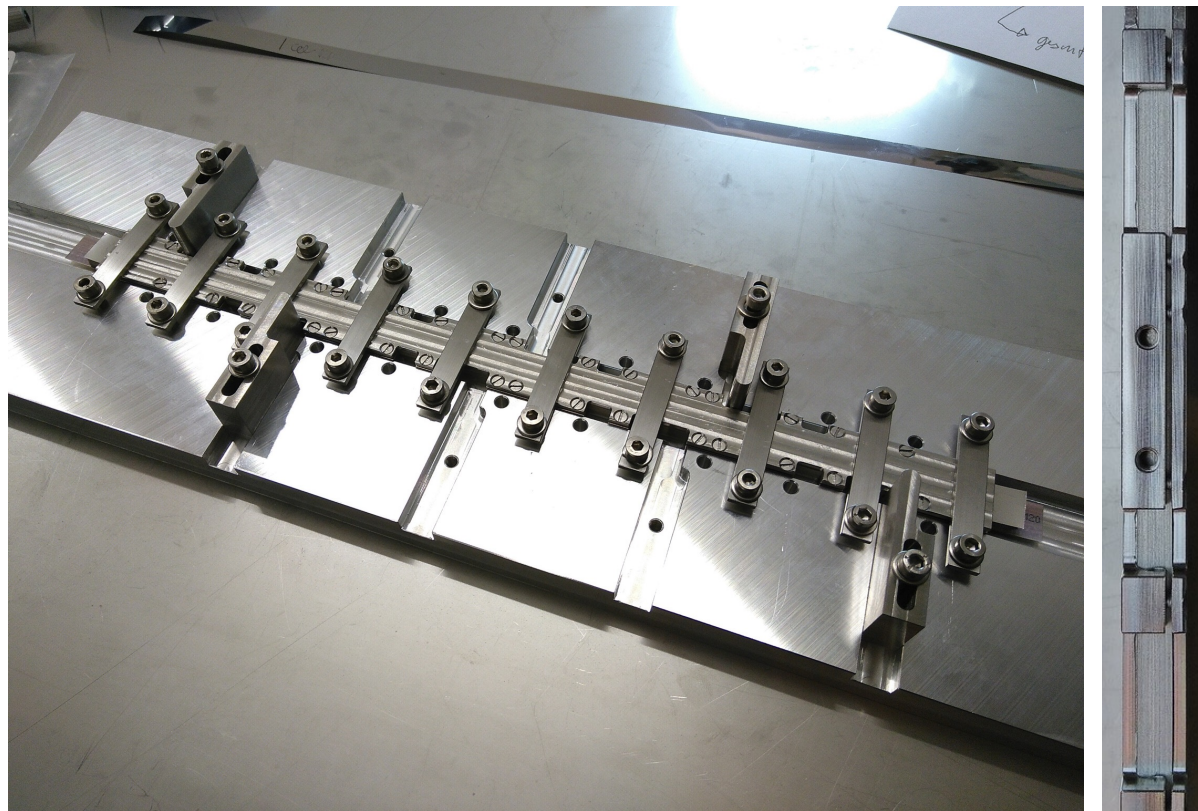
# HTS Tape Option



# HTS Tape Option

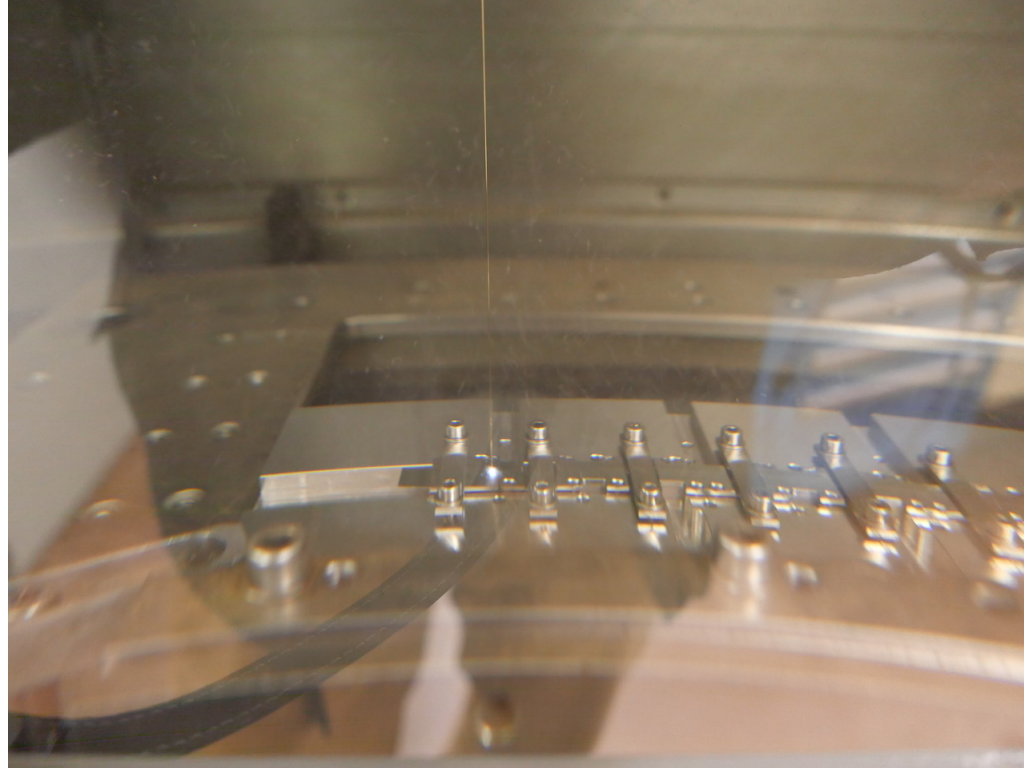


# HTS Tape Option

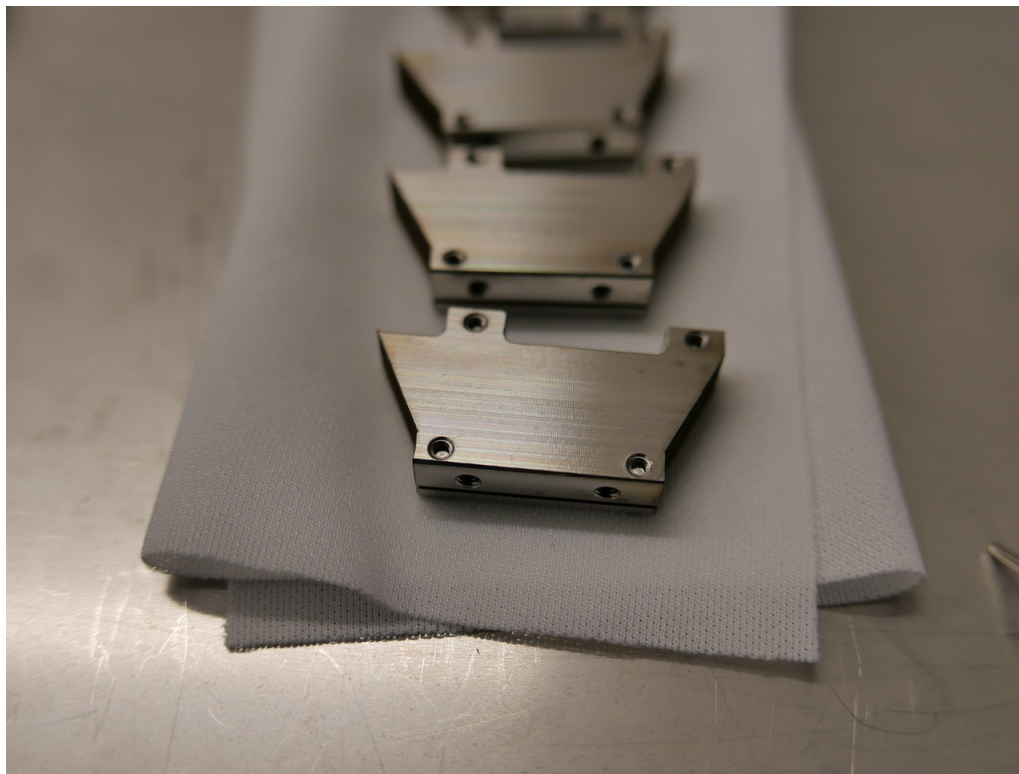




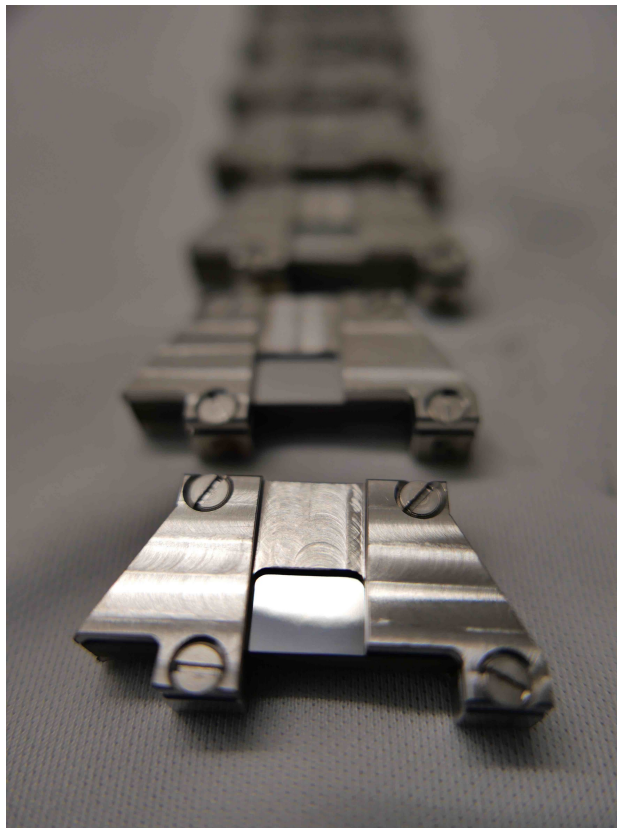
# HTS Tape Option



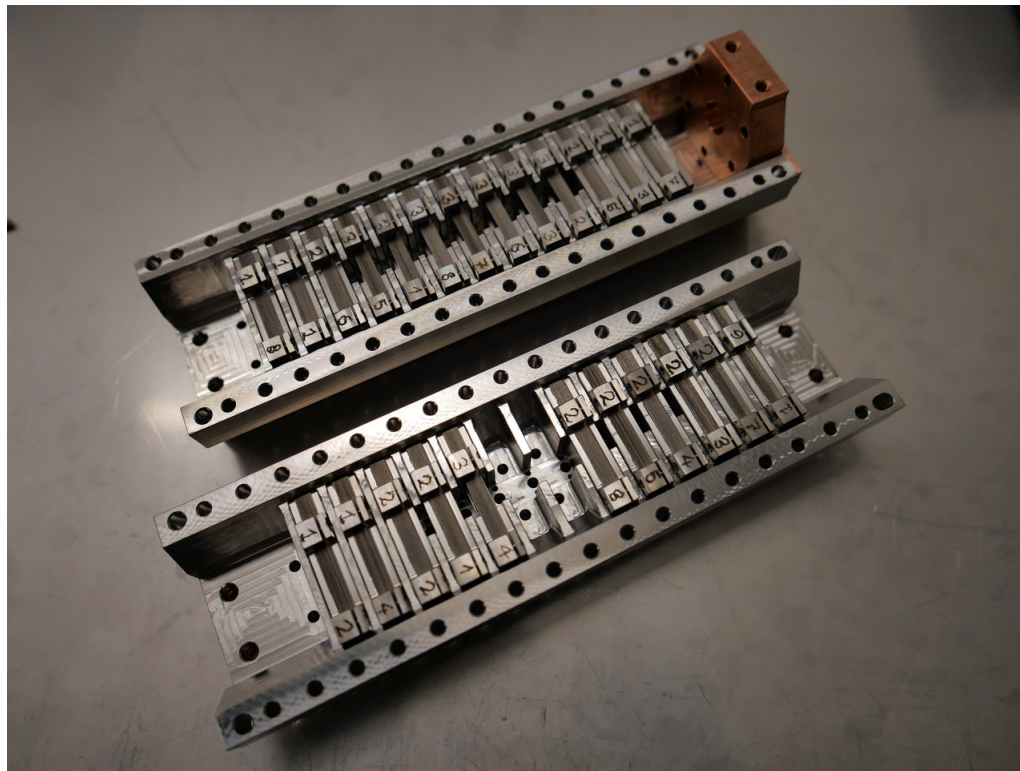
# HTS Tape Option



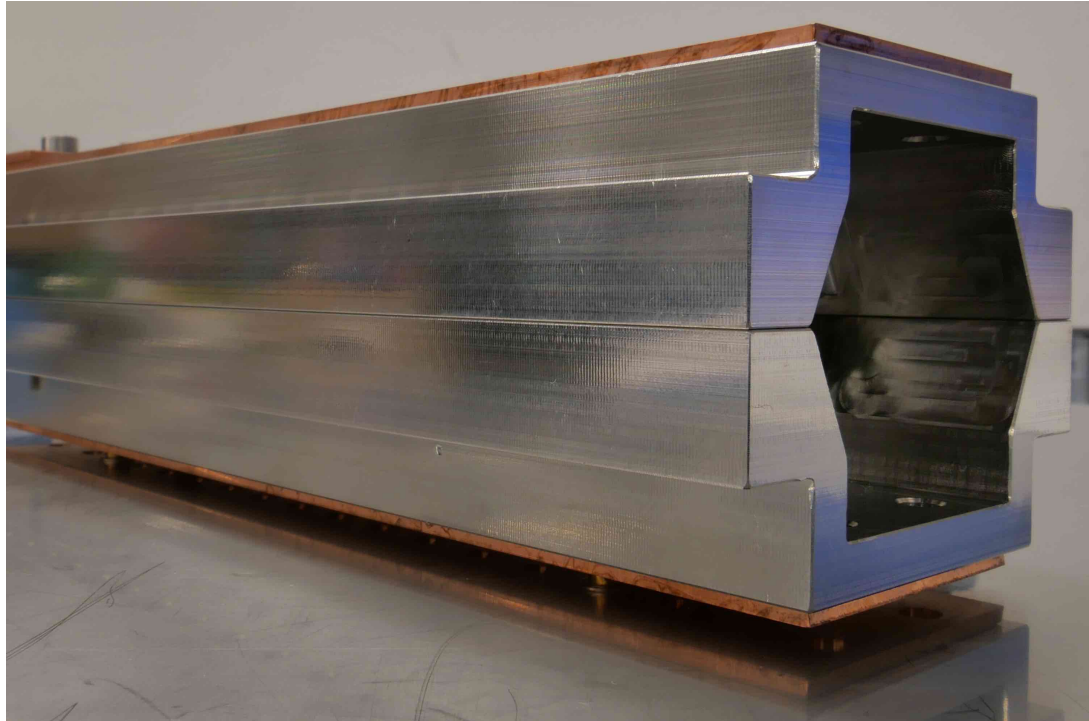
# HTS Tape Option



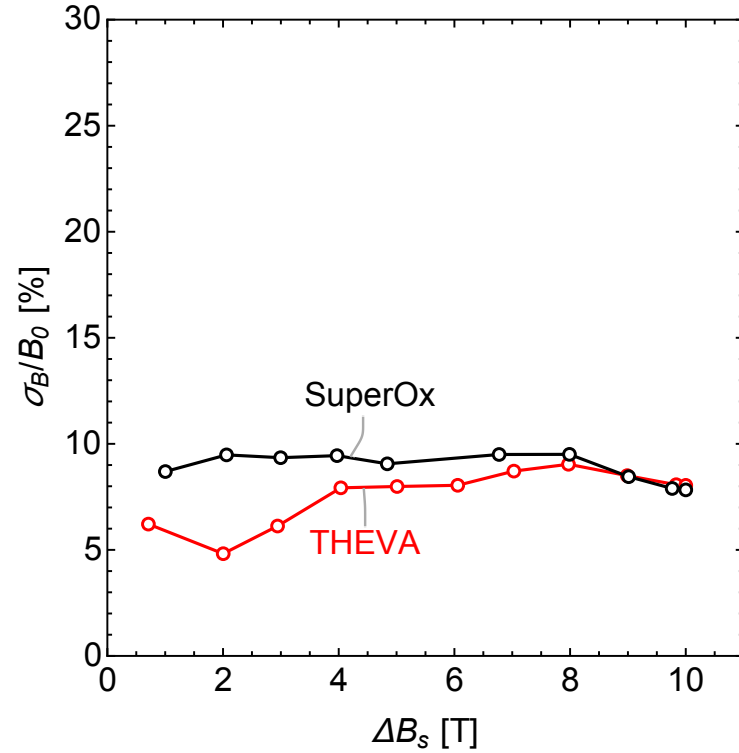
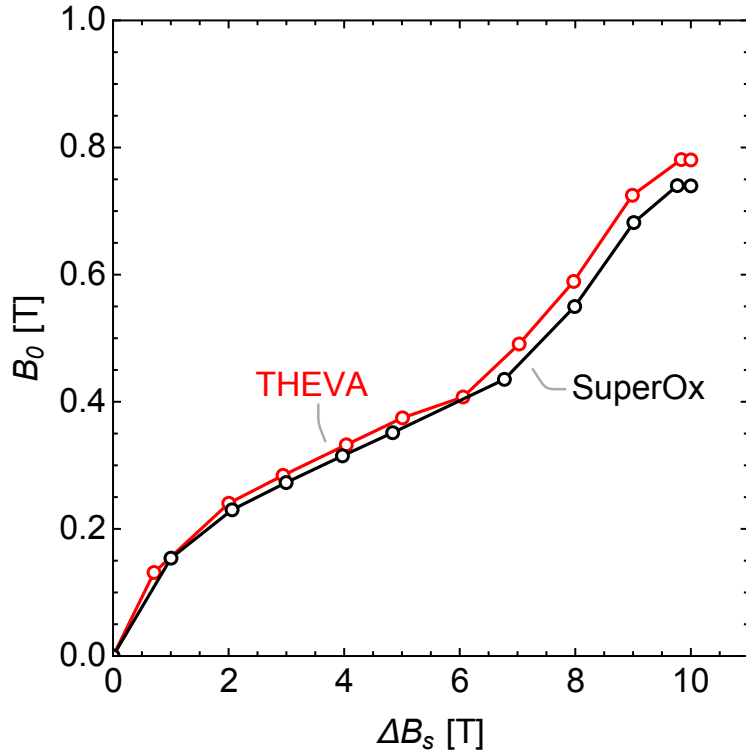
# HTS Tape Option



# HTS Tape Option



# HTS Tape Option: the results



# Summary of the planar staggered array with: $\lambda_u=10\text{mm}$ & $\text{gap}=4.0\text{mm}$

Company	RE	type	Undulator field, B (T)			$\sigma/B$
			with different pole's material			
			w/o	FeCo	Ho	
ATZ	YBCO	TSMG	1.67*	1.90	-	23%
Nippon	GdBCO	TSMG	-	2.10	-	3%
CAN	GdBCO	TSMG	-	2.02	-	7%
CAN	EuBCO	TSMG	-	1.90	-	6%
CAN	GdBCO	SDMG	1.69	1.89	2.01	5%
THEVA	GdBCO	tape	0.78	0.88	-	8%
SuperOx	YBCO	tape	0.74	-	-	8%

\*The two ATZ samples are not the same thus the one with and the one w/o poles are not directly comparable

# Summary of the planar staggered array with: $\lambda_u=10\text{mm}$ & $\text{gap}=4.0\text{mm}$

Company	RE	type	Undulator field, B (T)			$\sigma/B$
			with different pole's material			
			w/o	FeCo	Ho	
ATZ	YBCO	TSMG	1.67*	1.90	-	23%
Nippon	GdBCO	TSMG	-	2.10	-	3%
CAN	GdBCO	TSMG	-	2.02	-	7%
CAN	EuBCO	TSMG	-	1.90	-	6%
CAN	GdBCO	SDMG	1.69	1.89	2.01	5%
THEVA	GdBCO	tape	0.78	0.88	-	8%
SuperOx	YBCO	tape	0.74	-	-	8%

\*The two ATZ samples are not the same thus the one with and the one w/o poles are not directly comparable



# Summary of the planar staggered array with: $\lambda_u=10\text{mm}$ & $\text{gap}=4.0\text{mm}$

Company	RE	type	Undulator field, B (T)			$\sigma/B$
			with different pole's material			
			w/o	FeCo	Ho	
ATZ	YBCO	TSMG	1.67*	1.90	-	23%
Nippon	GdBCO	TSMG	-	2.10	-	3%
CAN	GdBCO	TSMG	-	2.02	-	7%
CAN	EuBCO	TSMG	-	1.90	-	6%
CAN	GdBCO	SDMG	1.69	1.89	2.01	5%
THEVA	GdBCO	tape	0.78	0.88	-	8%
SuperOx	YBCO	tape	0.74	-	-	8%

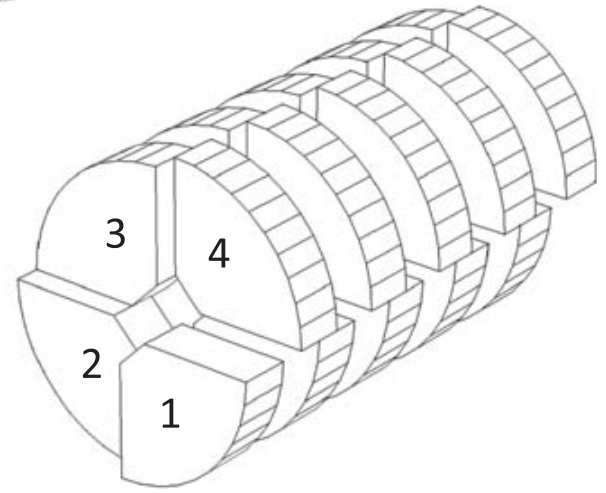
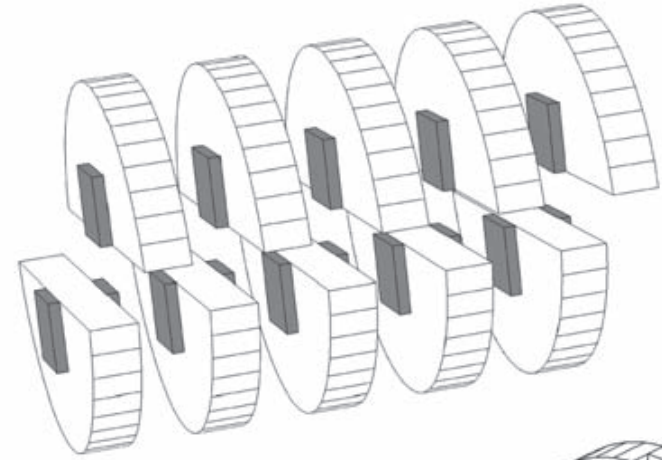
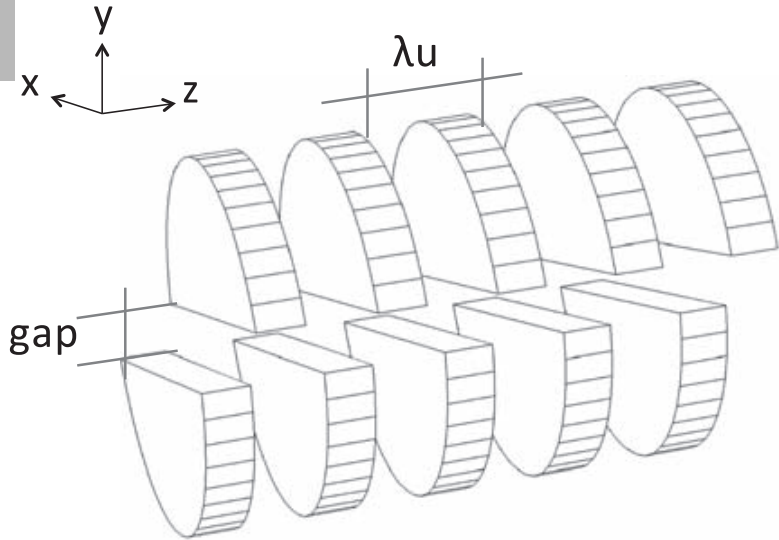
\*The two ATZ samples are not the same thus the one with and the one w/o poles are not directly comparable

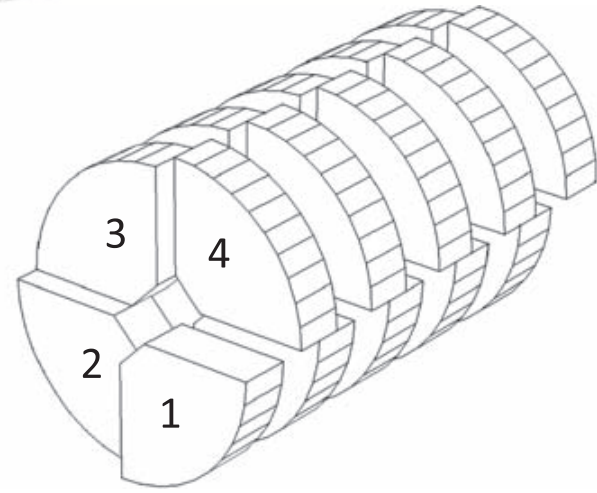
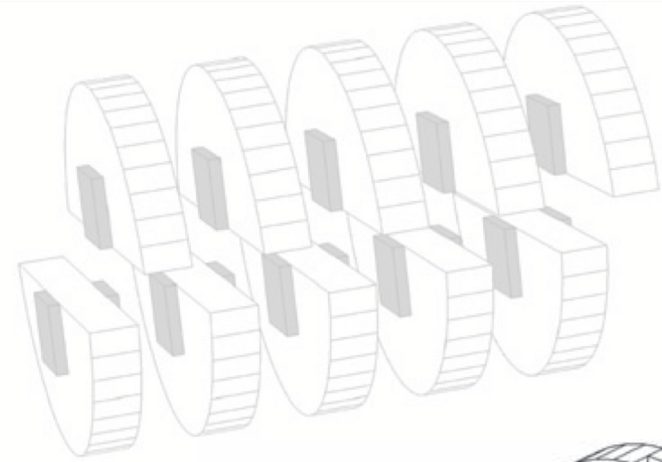
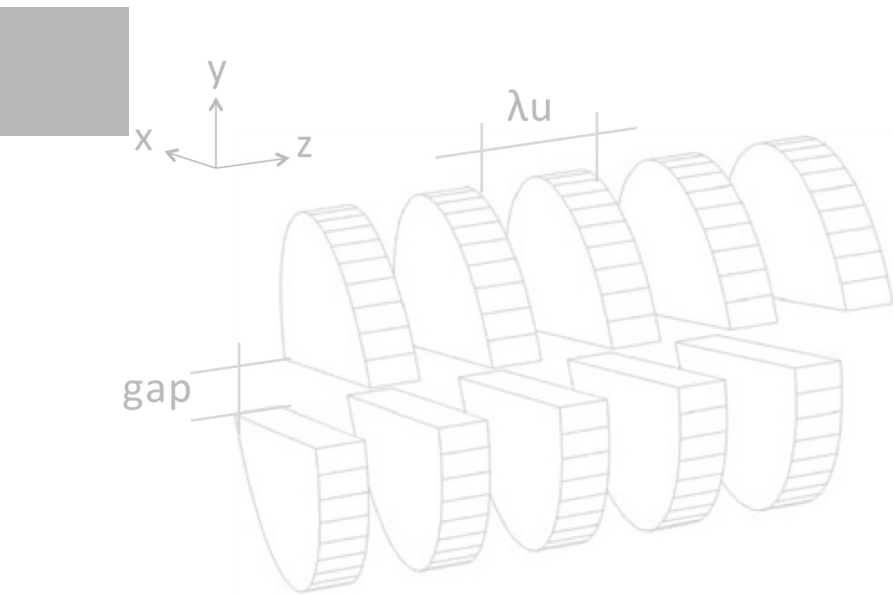
# Summary of the planar staggered array with: $\lambda_u=10\text{mm}$ & $\text{gap}=4.0\text{mm}$

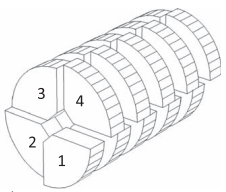
Company	RE	type	Undulator field, B (T)			$\sigma/B$
			with different pole's material			
			w/o	FeCo	Ho	
ATZ	YBCO	TSMG	1.67*	1.90	-	23%
Nippon	GdBCO	TSMG	-	2.10	2.20 <sup>†</sup>	3%
CAN	GdBCO	TSMG	-	2.02	2.12 <sup>†</sup>	7%
CAN	EuBCO	TSMG	-	1.90	2.00 <sup>†</sup>	6%
CAN	GdBCO	SDMG	1.69	1.89	2.01	5%
THEVA	GdBCO	tape	0.78	0.88	-	8%
SuperOx	YBCO	tape	0.74	-	-	8%

\*The two ATZ samples are not the same thus the one with and the one w/o poles are not directly comparable

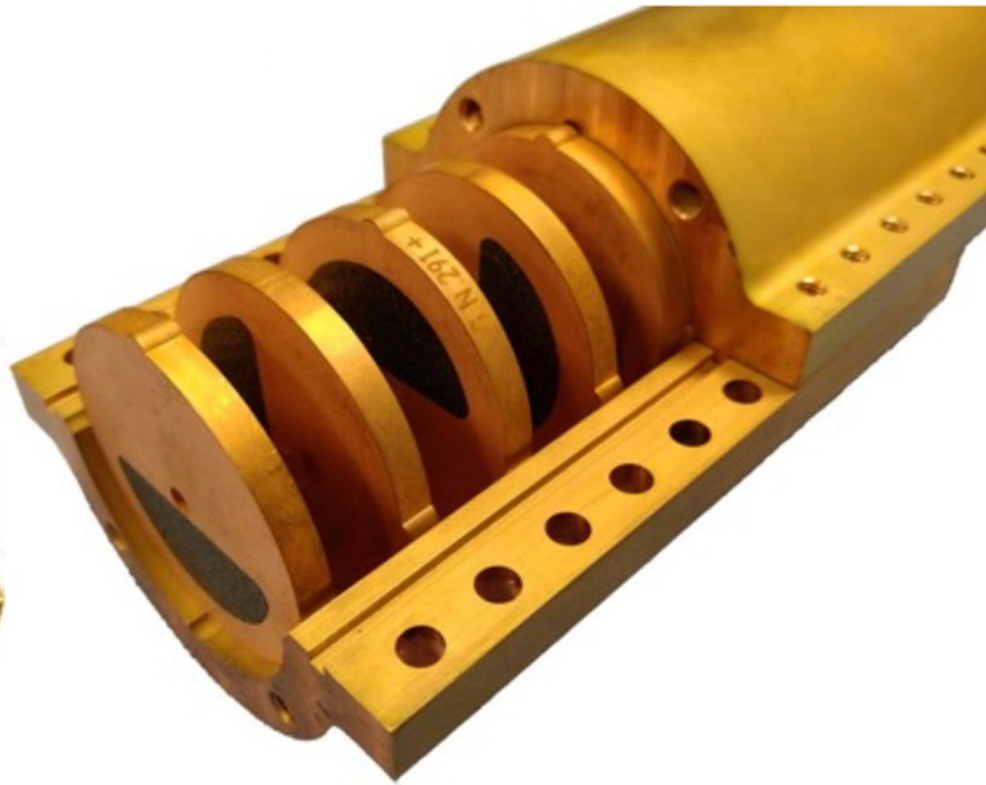
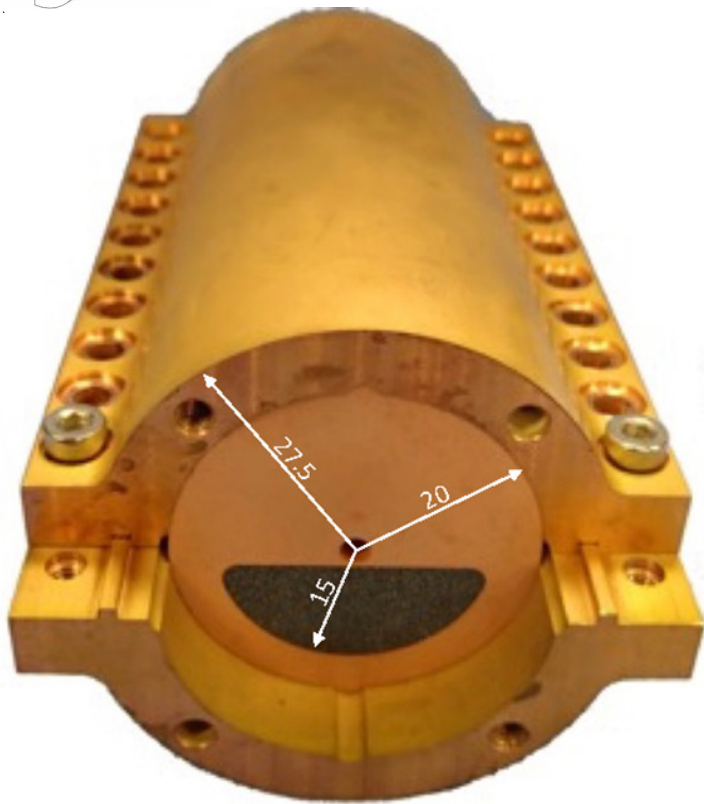
<sup>†</sup>Those are not measurements but just extrapolations

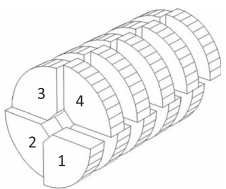




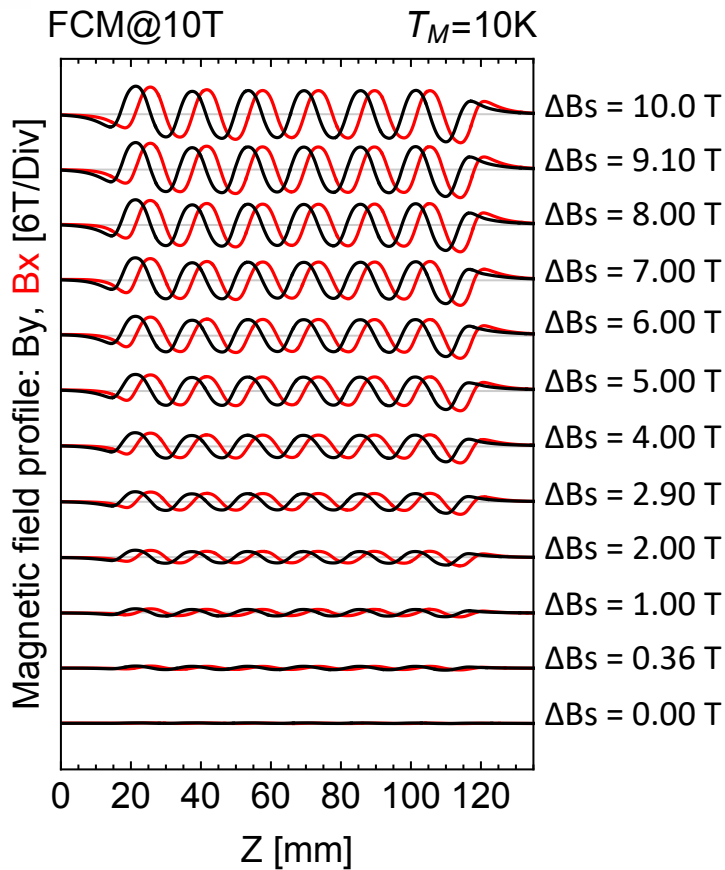


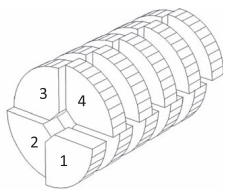
# Helical: Nippon Steel



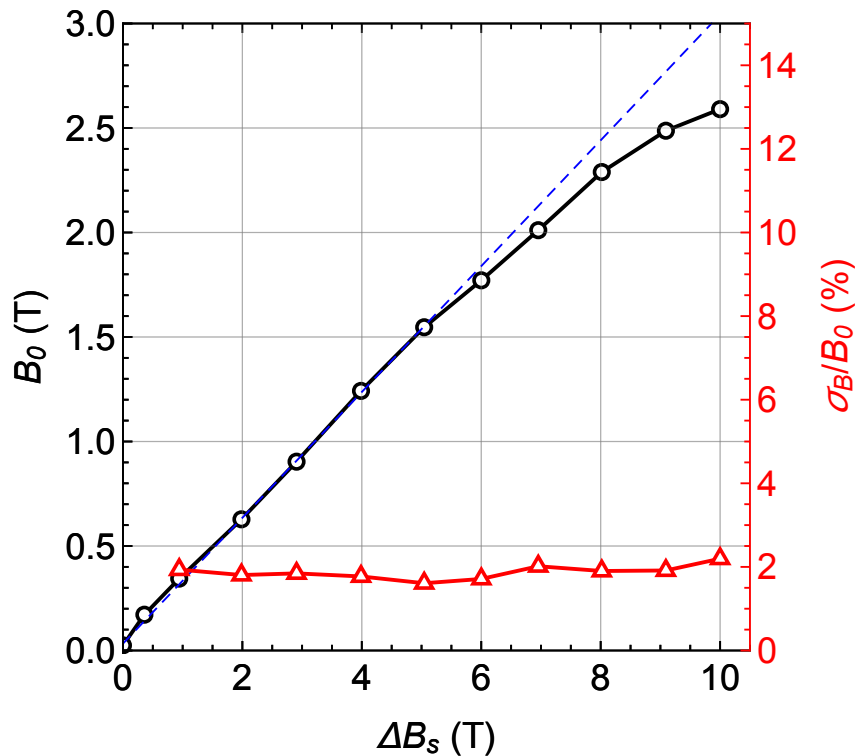
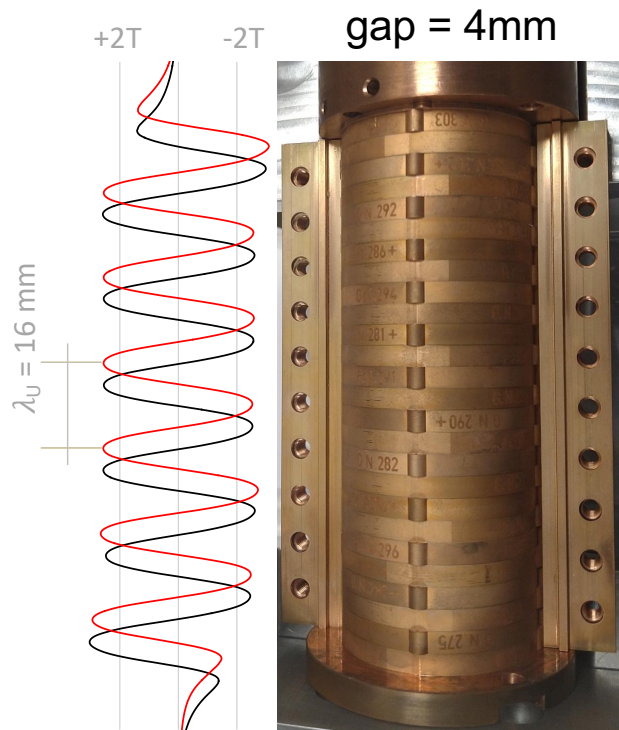


# Helical: Nippon Steel



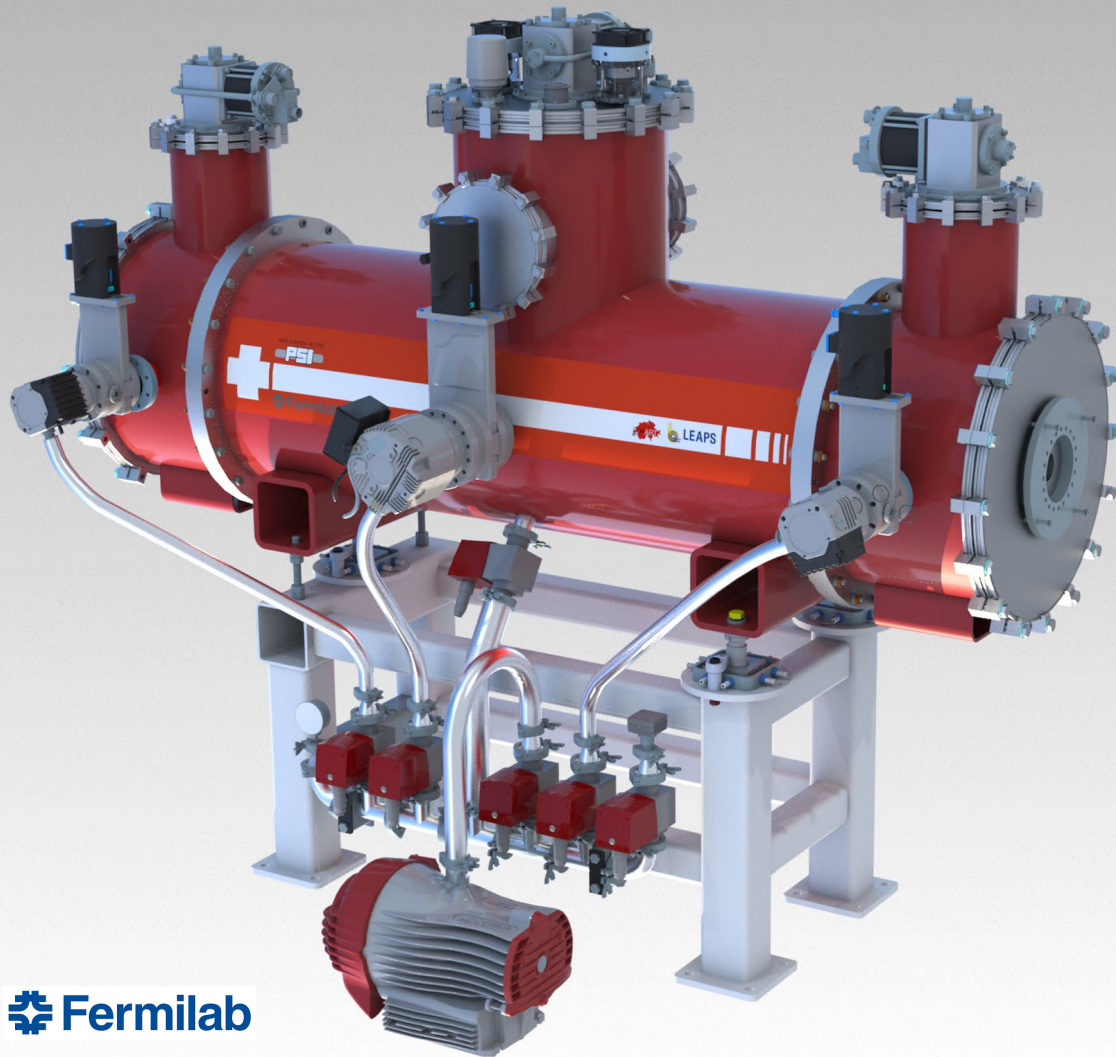


# Helical: Nippon Steel



- Brief introduction to accelerator based light sources
- The Tomographic Microscopy beamline: TOMCAT → I-TOMCAT
- The HTS (REBCO) bulk Staggered Array undulator
- The results on short samples:
  - Bulks & Tapes
- The status of the meter long HTS Undulator prototype
- Conclusions





# THE METER LONG PROTOTYPE

Active length : 1.0 m

Total length : < 2m

period length : 10 mm

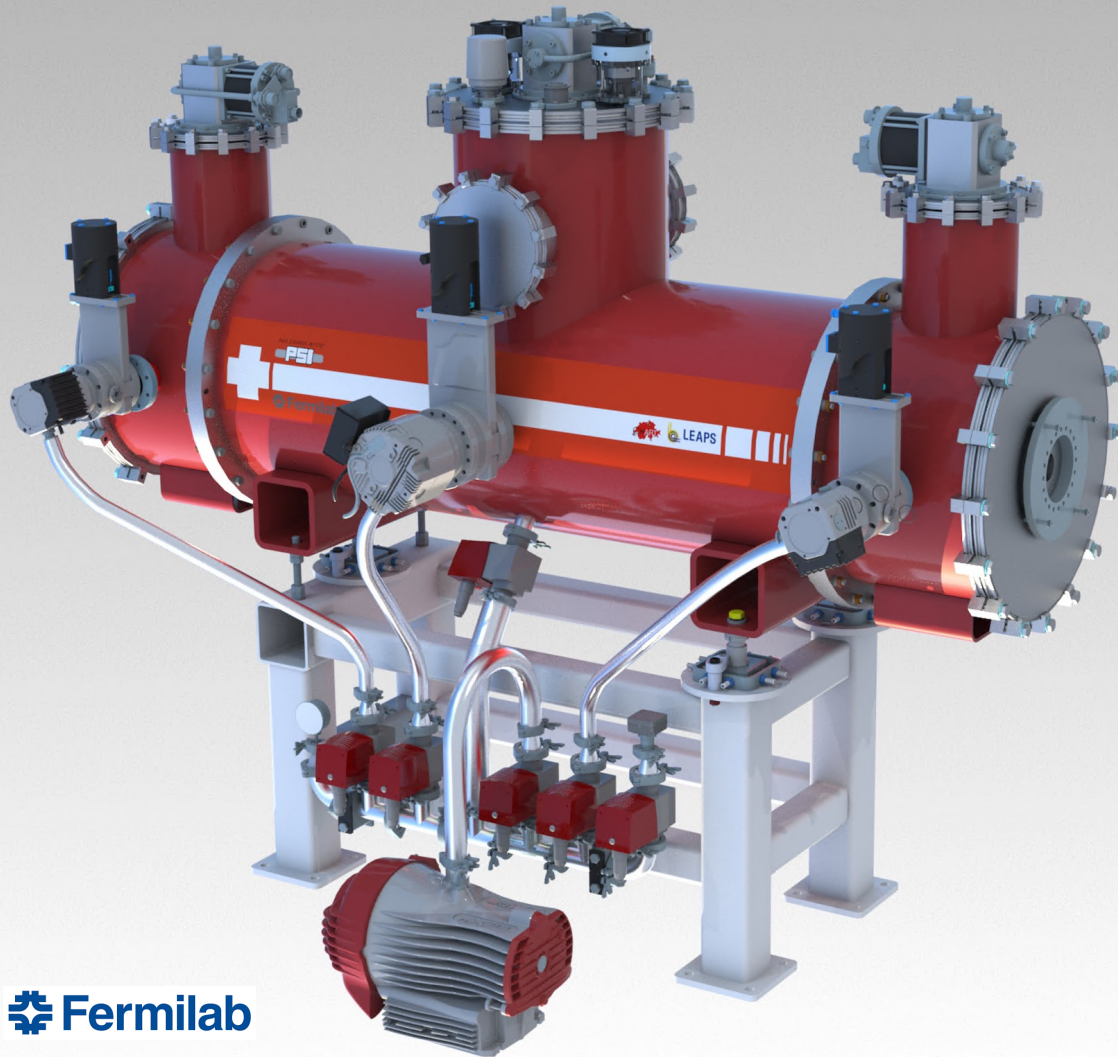
magnetic gap : 4.0mm

$B_0 \sim 2.0$

Cryocoolers

HTS Mag-temp 10K

LTS temp 4.0K



# THE METER LONG PROTOTYPE

Active length : 1.0 m

Total length : < 2m

period length : **10.5** mm

magnetic gap : **4.5** mm

$B_0 \sim 1.8$  T

Cryocoolers

HTS Mag-temp 10K

LTS temp 4.0K

# High Temperature Superconducting Undulator for iTomcat beamline at PSI

FERMLAB-POSTER-21-120-YD

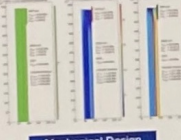
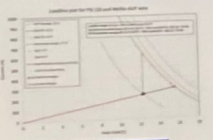
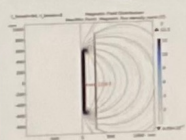
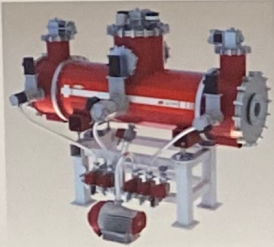
## Superconducting Undulators

Superconducting Undulators (SCUs) are the natural continuation in the evolution of insertion devices. The use of permanent magnets has been pushed to the limit by installing the arrays directly in the beam UHV to reduce the gap (in-Vacuum Undulators (IVU)) and even further by cooling them down to cryogenic temperatures to increase the remanence field (Cryogenic Permanent Magnet Undulators (CPMU)). In order to further increase the magnetic field of these devices, a jump in technology is required, hence the implementation of superconductivity. Development programs both in the US and in Europe have shown that SCUs generate stronger field on axis than comparable permanent magnet-based devices and that the use of superconductivity does not compromise the operation of synchronization storage rings or FELs. For period lengths above 13 mm, SCUs made out of NbTi show a significant improvement in field on axis compared to CPMUs; furthermore, a large portion of the superconducting technology potential, Nb<sub>3</sub>Sn and HTS, has yet to be exploited. Such HTS undulators, as proposed by PSI, allow to extend the functional capability of these devices below 10 mm period length.



Permanent Magnet	In-Vacuum	Cryogenic	Superconducting
Treatment stage	UHV vacuum stage	Increased B field	Highest B field
Controlled axis	Required distance of magnets	Increased efficiency	10 X design efficiency
Compact design	Good performance	Better performance	Best performance
Low performance			10 X design

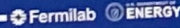
Superconducting coil conductor	Nb <sub>3</sub> Sn & NbTi
Maximum magnetic field	12T
Nominal magnetic field	10T
Nominal ramp rate (<math>\dot{B}</math>)	3mT/s
Ramp rate (>10T)	1mT/s
Warm bore diameter	50mm
Length of the good field (<math> B_z  > 15\text{mT}</math>)	5m
Stray field along the beam axis (> 1.5m from the center)	<math>< 0.1\text{mT}</math>
Radial stray field from the center outside the crystal	<math>< 1\text{mT}</math>
Current leads conductor	HTS
Maximum current	1.0 MA
Cooling system	Cryocooler
Operating temperature	<math>4\text{K}</math>
Permanent made	NO



Magnetic Design

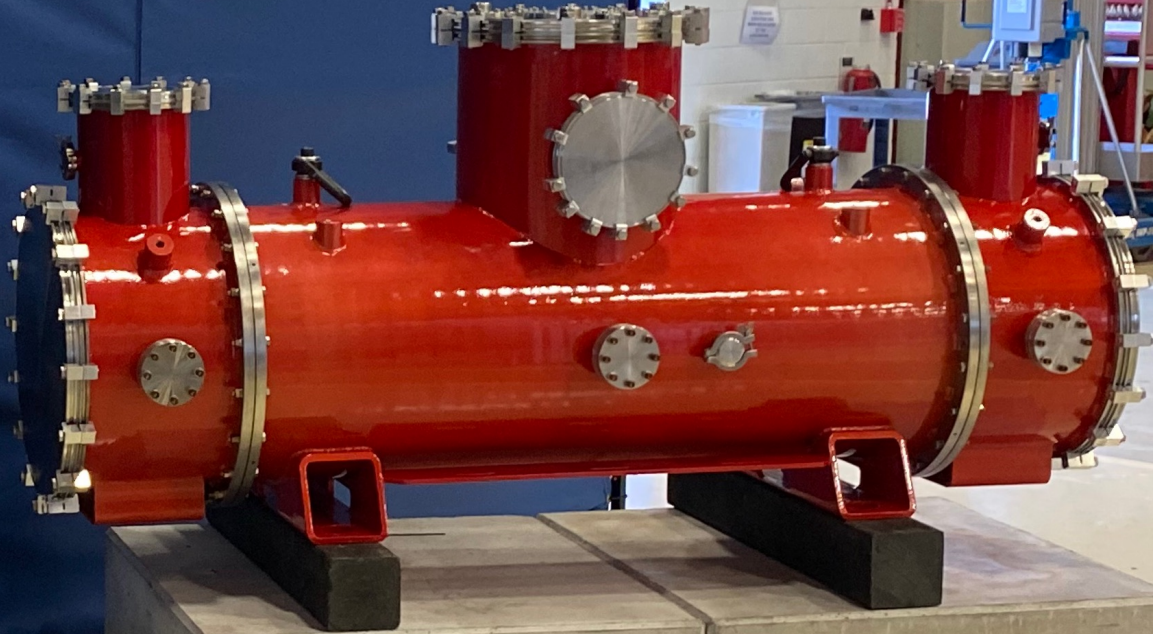
Superconductor Design

Mechanical Design



Fermilab National Accelerator Laboratory

This manuscript has been authored by Fermilab Research Alliance, LLC under Contract No. DE-AC02-07OR21400 with the U.S. Department of Energy, Office of Science, Office of High Energy Physics.



## High Temperature Superconducting Undulator for ITomcat beamline at PSI

FERMILAB-ATM-2018-01-138-00

### Superconducting Undulators

Superconducting undulators (SUs) are a type of undulator that uses superconducting magnets to generate a periodic magnetic field. This field causes a beam of electrons to oscillate and emit synchrotron radiation. SUs are used in a variety of applications, including X-ray free electron lasers (XFELs) and synchrotron light sources.



The undulator is designed to operate at a temperature of 4.2 K. It is made of niobium-titanium (Nb-Ti) superconducting wire. The undulator is designed to operate at a current of 100 A. The undulator is designed to operate at a length of 1.5 m. The undulator is designed to operate at a period of 1.5 cm. The undulator is designed to operate at a gap of 1.5 cm. The undulator is designed to operate at a magnetic field of 1.5 T. The undulator is designed to operate at a radiation wavelength of 1.5 nm. The undulator is designed to operate at a radiation flux of 1.5 x 10^18 photons/s. The undulator is designed to operate at a radiation energy of 1.5 keV. The undulator is designed to operate at a radiation divergence of 1.5 mrad. The undulator is designed to operate at a radiation emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2. The undulator is designed to operate at a radiation peak current of 1.5 A. The undulator is designed to operate at a radiation peak energy of 1.5 keV. The undulator is designed to operate at a radiation peak divergence of 1.5 mrad. The undulator is designed to operate at a radiation peak emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation peak brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2. The undulator is designed to operate at a radiation peak current of 1.5 A. The undulator is designed to operate at a radiation peak energy of 1.5 keV. The undulator is designed to operate at a radiation peak divergence of 1.5 mrad. The undulator is designed to operate at a radiation peak emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation peak brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2.

Parameter	Value
Operating Temperature	4.2 K
Operating Current	100 A
Operating Length	1.5 m
Operating Period	1.5 cm
Operating Gap	1.5 cm
Operating Magnetic Field	1.5 T
Operating Radiation Wavelength	1.5 nm
Operating Radiation Flux	1.5 x 10^18 photons/s
Operating Radiation Energy	1.5 keV
Operating Radiation Divergence	1.5 mrad
Operating Radiation Emittance	1.5 nm-rad
Operating Radiation Brightness	1.5 x 10^20 photons/s/mm^2/mrad^2
Operating Radiation Peak Current	1.5 A
Operating Radiation Peak Energy	1.5 keV
Operating Radiation Peak Divergence	1.5 mrad
Operating Radiation Peak Emittance	1.5 nm-rad
Operating Radiation Peak Brightness	1.5 x 10^20 photons/s/mm^2/mrad^2

The undulator is designed to operate at a temperature of 4.2 K. It is made of niobium-titanium (Nb-Ti) superconducting wire. The undulator is designed to operate at a current of 100 A. The undulator is designed to operate at a length of 1.5 m. The undulator is designed to operate at a period of 1.5 cm. The undulator is designed to operate at a gap of 1.5 cm. The undulator is designed to operate at a magnetic field of 1.5 T. The undulator is designed to operate at a radiation wavelength of 1.5 nm. The undulator is designed to operate at a radiation flux of 1.5 x 10^18 photons/s. The undulator is designed to operate at a radiation energy of 1.5 keV. The undulator is designed to operate at a radiation divergence of 1.5 mrad. The undulator is designed to operate at a radiation emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2. The undulator is designed to operate at a radiation peak current of 1.5 A. The undulator is designed to operate at a radiation peak energy of 1.5 keV. The undulator is designed to operate at a radiation peak divergence of 1.5 mrad. The undulator is designed to operate at a radiation peak emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation peak brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2.

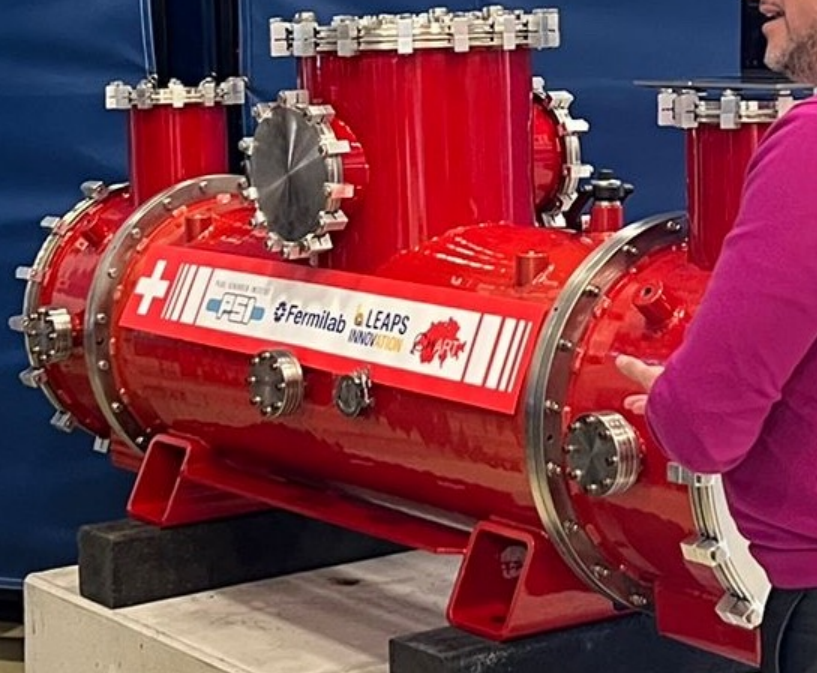
The undulator is designed to operate at a temperature of 4.2 K. It is made of niobium-titanium (Nb-Ti) superconducting wire. The undulator is designed to operate at a current of 100 A. The undulator is designed to operate at a length of 1.5 m. The undulator is designed to operate at a period of 1.5 cm. The undulator is designed to operate at a gap of 1.5 cm. The undulator is designed to operate at a magnetic field of 1.5 T. The undulator is designed to operate at a radiation wavelength of 1.5 nm. The undulator is designed to operate at a radiation flux of 1.5 x 10^18 photons/s. The undulator is designed to operate at a radiation energy of 1.5 keV. The undulator is designed to operate at a radiation divergence of 1.5 mrad. The undulator is designed to operate at a radiation emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2. The undulator is designed to operate at a radiation peak current of 1.5 A. The undulator is designed to operate at a radiation peak energy of 1.5 keV. The undulator is designed to operate at a radiation peak divergence of 1.5 mrad. The undulator is designed to operate at a radiation peak emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation peak brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2.

The undulator is designed to operate at a temperature of 4.2 K. It is made of niobium-titanium (Nb-Ti) superconducting wire. The undulator is designed to operate at a current of 100 A. The undulator is designed to operate at a length of 1.5 m. The undulator is designed to operate at a period of 1.5 cm. The undulator is designed to operate at a gap of 1.5 cm. The undulator is designed to operate at a magnetic field of 1.5 T. The undulator is designed to operate at a radiation wavelength of 1.5 nm. The undulator is designed to operate at a radiation flux of 1.5 x 10^18 photons/s. The undulator is designed to operate at a radiation energy of 1.5 keV. The undulator is designed to operate at a radiation divergence of 1.5 mrad. The undulator is designed to operate at a radiation emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2. The undulator is designed to operate at a radiation peak current of 1.5 A. The undulator is designed to operate at a radiation peak energy of 1.5 keV. The undulator is designed to operate at a radiation peak divergence of 1.5 mrad. The undulator is designed to operate at a radiation peak emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation peak brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2.

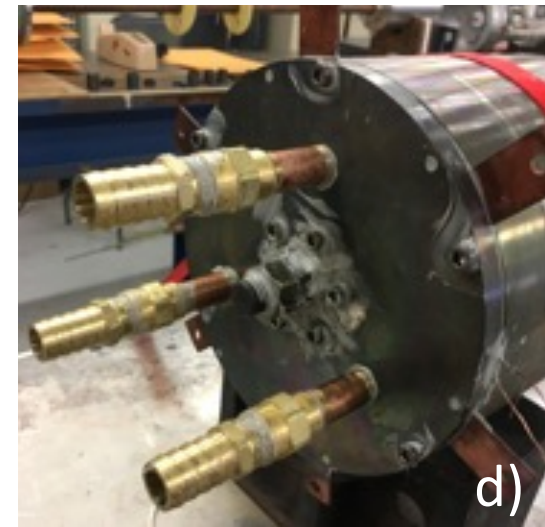
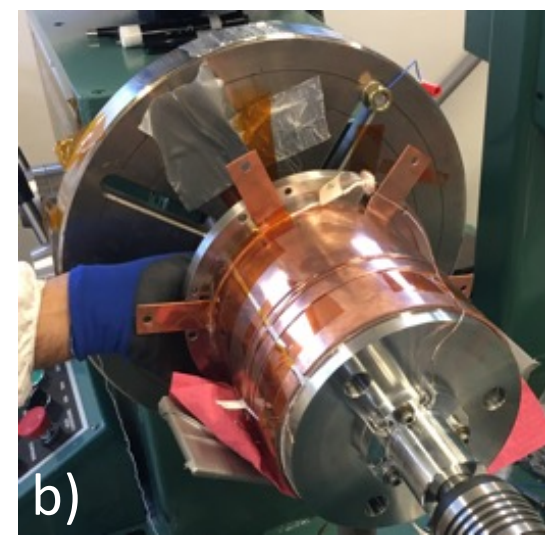
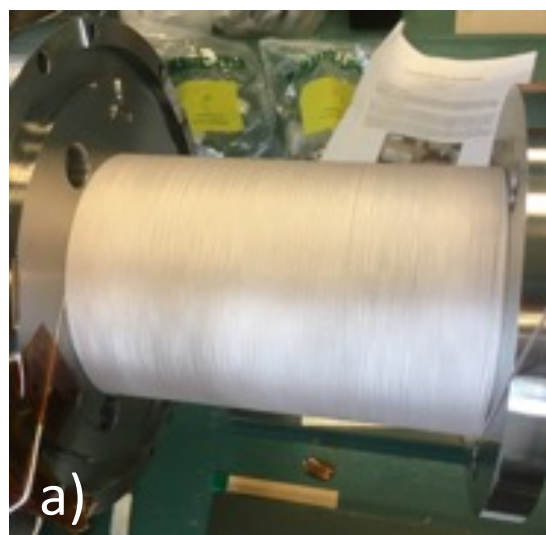
The undulator is designed to operate at a temperature of 4.2 K. It is made of niobium-titanium (Nb-Ti) superconducting wire. The undulator is designed to operate at a current of 100 A. The undulator is designed to operate at a length of 1.5 m. The undulator is designed to operate at a period of 1.5 cm. The undulator is designed to operate at a gap of 1.5 cm. The undulator is designed to operate at a magnetic field of 1.5 T. The undulator is designed to operate at a radiation wavelength of 1.5 nm. The undulator is designed to operate at a radiation flux of 1.5 x 10^18 photons/s. The undulator is designed to operate at a radiation energy of 1.5 keV. The undulator is designed to operate at a radiation divergence of 1.5 mrad. The undulator is designed to operate at a radiation emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2. The undulator is designed to operate at a radiation peak current of 1.5 A. The undulator is designed to operate at a radiation peak energy of 1.5 keV. The undulator is designed to operate at a radiation peak divergence of 1.5 mrad. The undulator is designed to operate at a radiation peak emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation peak brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2.

The undulator is designed to operate at a temperature of 4.2 K. It is made of niobium-titanium (Nb-Ti) superconducting wire. The undulator is designed to operate at a current of 100 A. The undulator is designed to operate at a length of 1.5 m. The undulator is designed to operate at a period of 1.5 cm. The undulator is designed to operate at a gap of 1.5 cm. The undulator is designed to operate at a magnetic field of 1.5 T. The undulator is designed to operate at a radiation wavelength of 1.5 nm. The undulator is designed to operate at a radiation flux of 1.5 x 10^18 photons/s. The undulator is designed to operate at a radiation energy of 1.5 keV. The undulator is designed to operate at a radiation divergence of 1.5 mrad. The undulator is designed to operate at a radiation emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2. The undulator is designed to operate at a radiation peak current of 1.5 A. The undulator is designed to operate at a radiation peak energy of 1.5 keV. The undulator is designed to operate at a radiation peak divergence of 1.5 mrad. The undulator is designed to operate at a radiation peak emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation peak brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2.

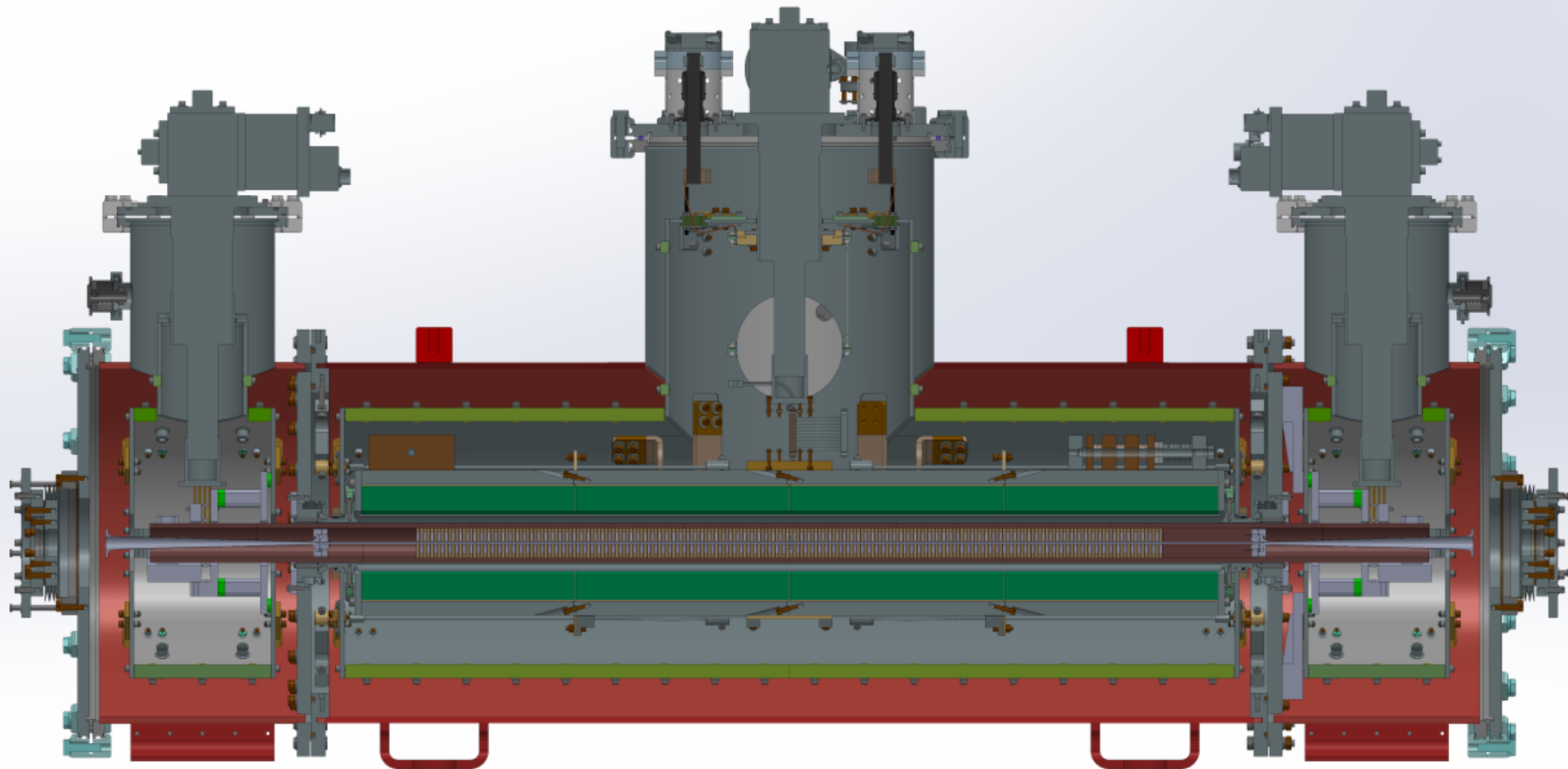
The undulator is designed to operate at a temperature of 4.2 K. It is made of niobium-titanium (Nb-Ti) superconducting wire. The undulator is designed to operate at a current of 100 A. The undulator is designed to operate at a length of 1.5 m. The undulator is designed to operate at a period of 1.5 cm. The undulator is designed to operate at a gap of 1.5 cm. The undulator is designed to operate at a magnetic field of 1.5 T. The undulator is designed to operate at a radiation wavelength of 1.5 nm. The undulator is designed to operate at a radiation flux of 1.5 x 10^18 photons/s. The undulator is designed to operate at a radiation energy of 1.5 keV. The undulator is designed to operate at a radiation divergence of 1.5 mrad. The undulator is designed to operate at a radiation emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2. The undulator is designed to operate at a radiation peak current of 1.5 A. The undulator is designed to operate at a radiation peak energy of 1.5 keV. The undulator is designed to operate at a radiation peak divergence of 1.5 mrad. The undulator is designed to operate at a radiation peak emittance of 1.5 nm-rad. The undulator is designed to operate at a radiation peak brightness of 1.5 x 10^20 photons/s/mm^2/mrad^2.



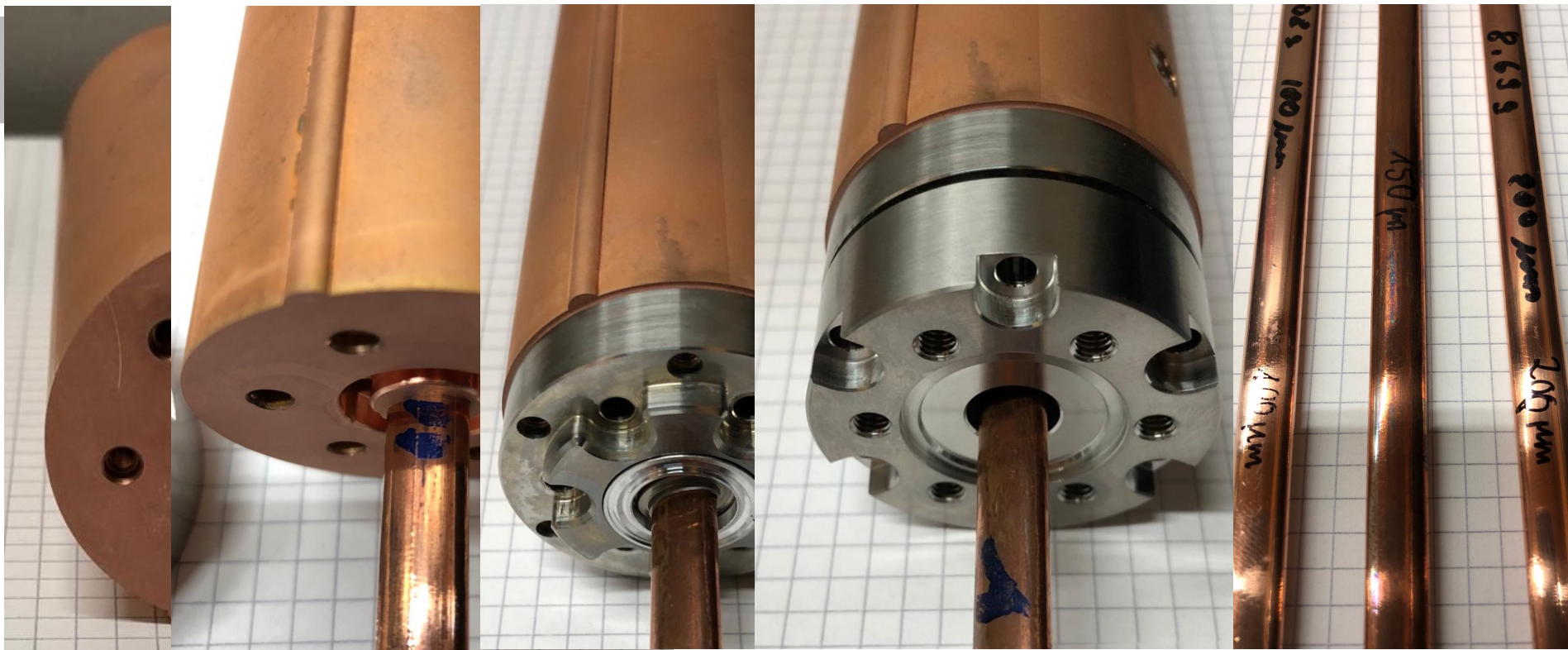
- a) Winding phase of the solenoid with a glass fiber insulated RRP Nb<sub>3</sub>Sn wire;
- b) assembly of the copper sleeve for conduction cooling;
- c) after the installation of the SS outer cylinder, ready for the Heat Treatment (650°C);
- d) after HT, ready for potting with epoxy resin;



# Vacuum chamber R&D



# Vacuum chamber R&D



# Conclusions & Outlooks

- We demonstrated high magnetic field (2T) in a short sample staggered array undulator made of GdBCO bulks HTS with 10mm period length and 4mm gap.
- Tape stacking is not giving the expected lower phase error and the field strength is substantially lower than bulks.
- The GdBCO bulk made by CAN out of the novel SDMG process are now our baseline
- Holmium poles deliver higher fields than FeCo even if they are not single crystals...
- A preliminary optimisation of the charging reduced the time required from 10 to 4h
- The delivery of the "Cryo-Solenoid" to PSI is planned for 3Q 2024, then we will start an intense measurement campaign to demonstrate a phase error as low as few degrees before installing the device in SLS2.0 at the beginning of 2026.



# Acknowledgements

- PSI : A.Arsenault, K.Zhang, X.Liang, S.Hellmann, Th.Schmidt, L.Huber, S.Reiche, M.Bartkowiak, C.Calzolaio, Prof. M. Stampanoni, Prof L.Patthey, F. Marone & G.Lovric
- CHART : Prof. H.R.Ott & Prof. L.Rivkin
- Uni Cambridge : J.Durrell, A.Dennis, Y. Shi
- Uni Malta : C.Gafas, N.Sammut, A.Sammut, J.Cassar
- King's College London: M.Ainslie
- ESRF : G. Le Bec
- Spring8 : T.Ishikawa, M.Yabashi, H.Tanaka
- UniKyoto : R.Kinjo, T.Kii, H.Ohgaki
- SENIS : Prof.R.Popovic, S.Spasic, S.Dimitrijevic
- KIT : Prof. M.Noel
- Fermilab: C.Boffo, M.Turenne, F.McConologue, V.Martinez, J.Hayman
- CERN: L.Bottura & B.Bordini

