Implementation of fully analytic orbit response analysis in python

Formulas used in this slides are derived from: https://arxiv.org/abs/1711.06589v2



S.Liuzzo, A.Franchi, February 13th 2024

The European Synchrotron

Analytic formulas for the rapid evaluation of the orbit response matrix and chromatic functions from lattice parameters in circular accelerators

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OUTLINE

- Part 1: The implementation (12')
- Part 2: The repository (1')
- Part 3: outlook (3')



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$$M_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \sin \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \cos \pi Q} \cos \left(|\phi_j - \phi_i| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \cos \pi Q} \cos \left(|\phi_j - \phi_j| - \pi Q \right) + C_{ij} = \frac{\sqrt{\beta_j \beta_i}}{2 \cos \pi Q} \cos \left(|\phi_j - \phi_j| - \pi Q \right) + C_{i$$



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 - Cons: no analytic formulas for off-diagonal ORM blocks (coupling), it can fail if optics or orbit unstable for quadrupole variation.
- Fully analytic Jacobian: evaluate directly the Jacobian from Twiss parameters of the initial model (ideal or from beam-based measurements)
 - Pros: coupling & dispersion included, only one computation of Twiss parameters needed, no orbit calculation needed, faster than pseudo-analytic, can be parallelized
 - ✓ Cons: tedious to code.



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• Numeri strengt
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N^(xx) =
$$-\frac{\sqrt{\beta_{j,x}^{(mod)}\beta_{w,x}^{(mod)}\beta_{m,x}^{(mod)}}}{2\sin(\pi Q_x^{(mod)})} \left\{ \frac{\cos(\tau_{x,wj}^{(mod)})}{4\sin(2\pi Q_x^{(mod)})} \left[\cos(2\tau_{x,mj}^{(mod)}) + \cos(2\tau_{x,mw}^{(mod)}) \right] \right\}$$
• Pros: ac
• Cons: til
w -> steerer
+ $\frac{\sin(\tau_{x,wj}^{(mod)})}{4\sin(2\pi Q_x^{(mod)})} \left[\sin(2\tau_{x,mj}^{(mod)}) - \sin(2\tau_{x,mw}^{(mod)}) \right]$
• Pseudo
each qu
m -> magnet
+ $\frac{1}{2}\sin(\tau_{x,wj}^{(mod)}) \left[\Pi(m,j) - \Pi(m,w) + \Pi(j,w) \right] + \frac{\cos(\Delta\phi_{x,wj}^{(mod)})}{4\sin(\pi Q_x^{(mod)})} \right\}$
• Fully analytic Jacobian: evaluate directly the Jacobian from beam-based measurements)
If $(a,b) = 1$ if $s_a < s_b$, $\Pi(a,b) = 0$ if $s_a \ge s_b$

Pros: coupling & dispersion included, only one computation of Twiss $au_{z,ab} = \Delta \phi_{z,ab} - \pi Q_z , \quad z = x, y$ pseudo-analytic, can be parallelized

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- Fully analytic Jacobian: evaluate directly the Ja from beam-based measurements)
 - Pros: coupling & dispersion included, only one computation pseudo-analytic, can be parallelized
 - ✓ Cons: tedious to code.
- Observation: the accuracy of the two analytic approaches can be poor if thin-element model is used. Corrections to <u>account for the variation of Twiss parameters across magnets</u> have been included which reduce dramatically the errors w.r.t. the numerical version (see next slide).

$$\beta_m \longrightarrow I_{\beta,m} = \frac{1}{L_m} \int_0^{L_m} \beta(s) \, ds ,$$

$$\beta_m \sin(2\tau_{mj}) \longrightarrow I_{S,mj} = \frac{1}{L_m} \int_0^{L_m} \beta(s) \sin(2\tau_{sj}) \, ds$$

$$\beta_m \cos(2\tau_{mj}) \longrightarrow I_{C,mj} = \frac{1}{L_m} \int_0^{L_m} \beta(s) \cos(2\tau_{sj}) \, ds$$

$$\sqrt{\beta_m} \sin(\tau_{mj}) \longrightarrow J_{C,mj} = \frac{1}{L_m} \int_0^{L_m} \sqrt{\beta(s)} \sin(\tau_{sj}) \, ds$$

$$\sqrt{\beta_m} \cos(\tau_{mj}) \longrightarrow J_{C,mj} = \frac{1}{L_m} \int_0^{L_m} \sqrt{\beta(s)} \cos(\tau_{sj}) \, ds$$

or



Example: FCC quadrupole ORM Jacobian with

- 1600 BPMs
- 8 steerers
- 1 quadrupole QC1L1_1





Example: FCC quadrupole ORM Jacobian with

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Example: FCC quadrupole ORM Jacobian with

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Example: FCC quadrupole ORM Jacobian with



• RMS & MAX error computed over all columns & rows of the diagonal ORM blocks O^(xx) & O^(yy).



NUMERICAL VS ANALYTIC JACOBIAN OF THE ORM: CPU TIME

Example: FCC quadrupole ORM Jacobian N (diagonal blocks only) with

- 1600 BPMs
- 8 steerers
- 360 quadrupoles parallelized over 64 cores CPUs (for both numerical and analytic tests)

Results

- Numeric: 1807.1 s [100%]
- fully analytic: 221.1 s [12%] (room for further optimization)



NUMERICAL VS ANALYTIC JACOBIAN OF THE ORM: OPTICS CORRECTION

Table 2: β -beating, dispersion and emittances after correction of 10 μ m random alignment errors on dipole quadrupole and sextupole magnets for the EBS and FCC-ee lattices using analytic or numeric ORM derivative.

$\langle std \rangle_{50}$	$rac{\Deltaeta_h}{eta_{h,0}}$	$\frac{\Delta eta_{v}}{eta_{v,0}}$	$\Delta \eta_h$	$\Delta \eta_{v}$	$\Delta \epsilon_v$				
units	%	%	mm	mm	pm rad				
EBS									
err.	19.37	11.08	17.33	6.91	94.17				
ana.	0.2	0.2	0.18	0.05	0.003				
num.	0.2	0.2	0.18	0.05	0.003				
FCC-ee Z									
err.	3.6	59.4	120.5	82.45	-				
ana.	0.81	4.29	26.0	9.57	0.17				
num.	0.82	4.30	25.98	9.64	0.18				

From IPAC23 MOPL069

Table 3: β -beating, dispersion and emittances after correction of 10 µm random alignment errors on dipole quadrupole and sextupole magnets for the FCC-ee lattice using analytic ORM derivative (1856 BPMs, 18 steerers). The input lattice is tested: without radiation, with radiation and with radiation and tapering. Reference lattice is in all cases without radiation.

$\langle std \rangle_{50}$ units	$rac{\Deltaoldsymbol{eta}_h}{oldsymbol{eta}_{h,0}} \ \%$	$\frac{\underline{\Delta \beta_{\nu}}}{\beta_{\nu,0}}$	$\Delta \eta_h$ mm	$\Delta \eta_{ u}$ mm	$\Delta \epsilon_v$ pm rad
4D err 4D cor	3.63 0.84	61.37 4.24	118.7 25.67	82.36 9.58	- 0.71
6D err 6D cor	3.60 0.81	59.45 4.29	120.54 26.0	82.45 9.57	- 0.17
6D err + tapering 6D cor	3.61	61.33	119.59	82.96	-
+ tapering	0.82	4.22	26.03	9.65	0.18







THICK STEERERS IN CLASSIC ANALYTIC ORM FORMULA





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WHERE YOU CAN FIND US

https://gitlab.esrf.fr/BeamDynamics/commissioningsimulations

Commissioning tools are still poor in terms of documentation, and debugging. The inclusion into the pyAT repository is pending such extensive validation tests.

Modules for the fully analytic ORM Jacobian can be found here:

commissioningsimulations/correction/optics_coupling - main - BeamDynamics / CommissioningSimulations - GitLab gitLab.esr.fr

https://gitlab.esrf.fr/BeamDynamics/commissioningsimulations/-/tree/main/commissioningsimulations/correction/optics_coupling



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OUTLOOK: THICK-ELEMENT CORRECTION FOR RDTS

$$f_{jklm}(s) \propto \sum_{m} \beta_{m,x}^{(J+k)/2} \beta_{m,y}^{(l+m)/2} e^{i[(j-k)\Delta\phi_{w,x}^{(s)} + (l-m)\Delta\phi_{w,y}^{(s)}]}$$

$$f_{1001,j} = \frac{\sum_{m=1}^{M} J_{m,1} \sqrt{\beta_{m,x} \beta_{m,y}} e^{i(\Delta \phi_{x,mj} - \Delta \phi_{y,mj})}}{4 \left[1 - e^{2\pi i (Q_x - Q_y)} \right]} + O(J_1^2)$$

$$f_{1010,j} = \frac{\sum_{m=1}^{M} J_{m,1} \sqrt{\beta_{m,x} \beta_{m,y}} e^{i(\Delta \phi_{x,mj} + \Delta \phi_{y,mj})}}{4 \left[1 - e^{2\pi i (Q_x + Q_y)} \right]} + O(J_1^2)$$

$$f_{2000,j} = -\frac{\sum_{m=1}^{M} \beta_{m,x}^{(mod)} \delta K_{m,1} e^{2i\Delta \phi_{x,mj}^{(mod)}}}{1 - e^{4\pi i Q_x^{(mod)}}} + O(\delta K_1^2)$$
$$f_{0020,j} = \frac{\sum_{m=1}^{M} \beta_{m,y}^{(mod)} \delta K_{m,1} e^{2i\Delta \phi_{y,mj}^{(mod)}}}{1 - e^{4\pi i Q_y^{(mod)}}} + O(\delta K_1^2)$$

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$$\beta_m^{\mathbf{A}} \sin \left(\mathbf{B} \Delta \phi_{mj} \right) \longrightarrow \frac{1}{L_m} \int_0^{L_m} \beta(s)^{\mathbf{A}} \sin \left(\mathbf{B} \Delta \phi_s \right) \, ds$$
$$\beta_m^{\mathbf{A}} \cos \left(\mathbf{B} \Delta \phi_{mj} \right) \longrightarrow \frac{1}{L_m} \int_0^{L_m} \beta(s)^{\mathbf{A}} \cos \left(\mathbf{B} \Delta \phi_s \right) \, ds$$

Thick-element corrections are being implemented to RDTs



From analytic formulas



From particle tracking + harmonic analysis





The European Synchrotron

recorded data damping curve



Very accurate for single-quad error (thus ok for response matrix)





Less accurate for distributed errors (2nd order & coupling terms)



New formulas for coupling RDTs from OTM are still to be derived

$$ec{X}^{(N+1)} = \mathbf{M}ec{X}^{(N)} \;, \qquad ec{X} = \left(egin{array}{c} x \\ p_x \\ y \\ p_y \end{array}
ight)$$



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Thank you!













Consequence: Minimizing cross-term (betatron+chromatic) detuning terms could be as much, if not more, effective than minimizing purely higher-order betatron or chromatic terms

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Blame path lengthening: Actually, minimizing linear chroma is still very helpful, since path lengthening and chroma are highly correlated

$$\Delta C = -2\pi (J_X \xi_X + J_Y \xi_Y). \tag{31}$$

$$Q(J_{x}(t),\delta(t)) = Q(J_{x}(0),\delta(0)) + \frac{\partial Q}{\partial J_{x}} J_{x}(t) + \frac{\partial Q}{\partial \delta} \delta(t) +$$

PHYSICAL REVIEW SPECIAL TOPICS - ACCELERATORS AND BEAMS 8, 094001 (2005)

Dependence of average path length betatron motion in a storage ring

Yoshihiko Shoji*

