

# RW impedance and CBI

**FCC Booster**

Ali Rajabi

Rome, 13 November, 2023

**HELMHOLTZ**



This project has received funding from the European Union's Horizon 2020 research and innovation program under grant agreement No 951754



**FUTURE  
CIRCULAR  
COLLIDER**



# Table of content

## Collective Effects and Instabilities

### 1 Collective Effects

1. Introduction
2. Resistive wall impedance
3. VACI CODE
4. Results

### 2 Instabilities

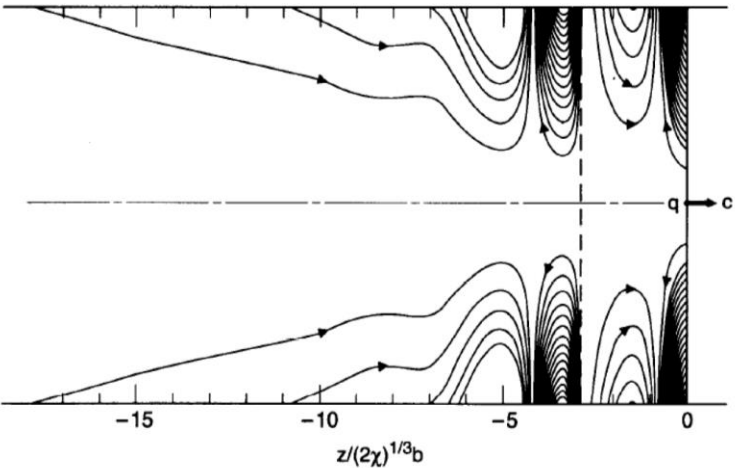
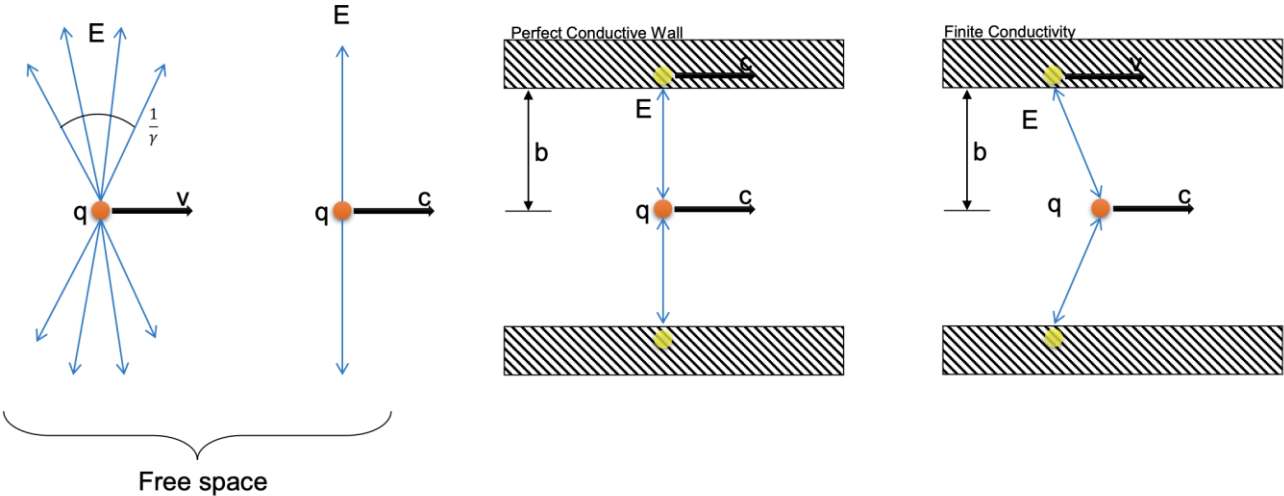
1. Introduction
2. Single-Bunch
3. Multi-bunch

# Collective Effects

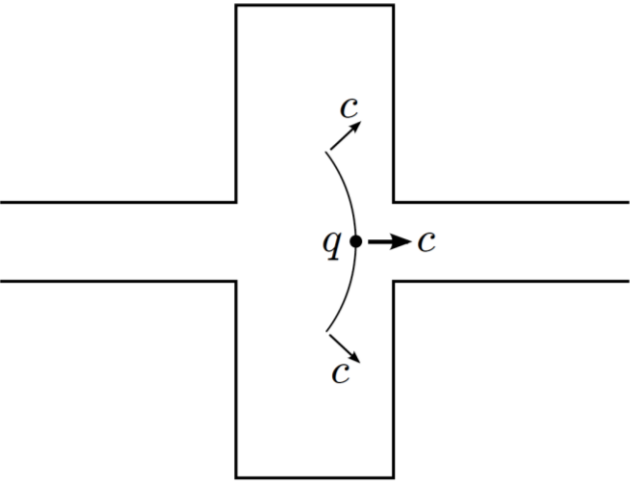
# Introduction

## What are collective effects?

- Interactions between particles within a beam are generally known as collective effects
  1. Incoherent
    - ❖ Space-charge
    - ❖ Scattering
  2. Coherent
    - ❖ Wake-fields



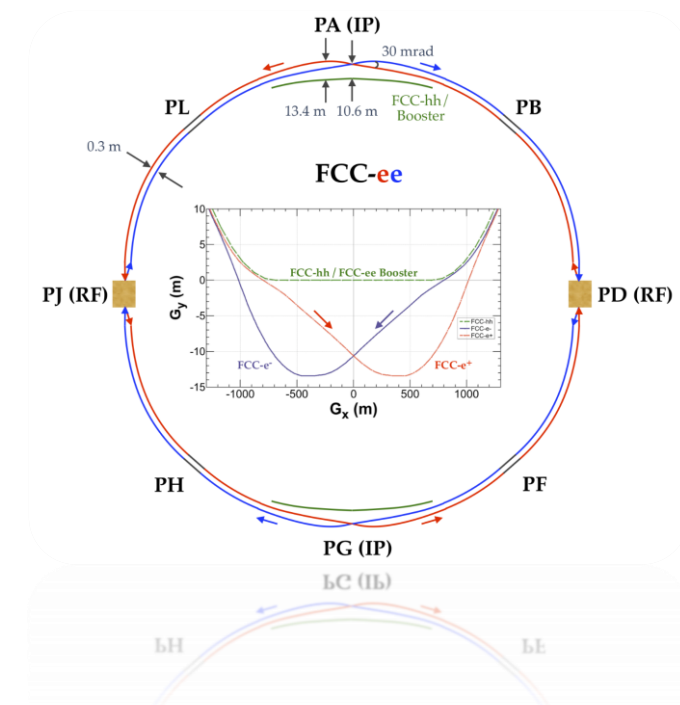
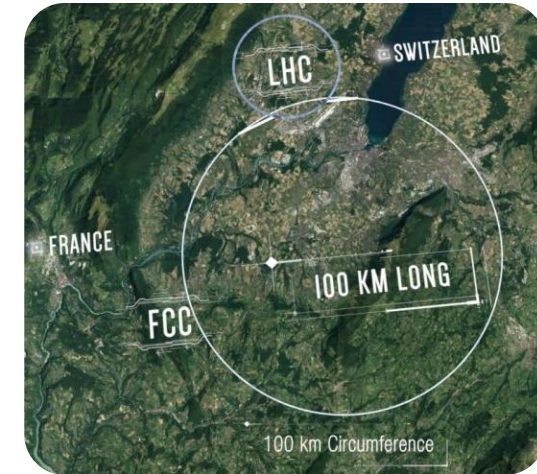
Wake fields following a point charge in a cylindrical beam pipe with resistive walls. (K. Bane)



# Source of Impedance in the Ring

## FCC Rings (old parameters, CDR)

- Beam pipes (Resistive Wall Impedance,  $\sim 92$  km)
- RF Cavities (No. 56 in a 4-cell array)
- RF Cavity Tapers (No. 14 double tapers)
- Synchrotron Radiation Absorbers
- Collimators (No. 20)
- BPMs (No. 4000)
- Bellows (No. 8000)



# Wake-field

## Maxwell's equation

$$\begin{aligned}\operatorname{div} \vec{D} &= \rho_m, \\ \operatorname{curl} \vec{H} - j\omega \vec{D} &= \vec{J}_m, \\ \operatorname{curl} \vec{E} + j\omega \vec{B} &= 0, \\ \operatorname{div} \vec{B} &= 0,\end{aligned}$$

$$\rho(r, z; \omega) = J_z(r, z; \omega)$$

$$J_n = \frac{Q_n}{A} \sigma(r; a, b) e^{in\theta} e^{-iks}$$

where:

$\sigma(r; a, b)$  means particles are in a ring with a thickness of (b-a)

A is the ring area

$\theta$  is the angle distribution of electrons around the ring

$$\vec{E} = -\vec{\nabla}\varphi - \frac{\partial}{\partial t}\vec{A} \quad \text{And} \quad \vec{B} = \vec{\nabla} \times \vec{A}$$

$$\vec{\nabla} \cdot \vec{A} = 0 \quad \text{Coulomb gauge}$$

$$\partial_t \Rightarrow -i\omega \quad \text{Fourier Transform}$$

$$\partial_z \Rightarrow -i\omega/v \quad \text{long pipe Appr.}$$

**Boundary Condition**

$$\begin{cases} \vec{\nabla} \cdot (\epsilon \vec{\nabla} \varphi) = \rho_m \\ \vec{\nabla} \times (1/\mu \vec{\nabla} \times \vec{A}) - \epsilon \omega^2 \vec{A} = -J_n \hat{e}_z + i\epsilon \omega \vec{\nabla} \varphi \end{cases}$$

# Resistive wall wake-field

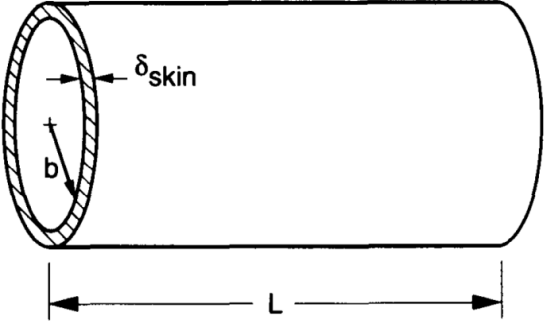
## Simple Geometries

$$E_s = -\frac{16q}{4\pi\epsilon_0 b^2} \left( \frac{e^u}{3} \cos(\sqrt{3}u) - \frac{\sqrt{2}}{\pi} \int_0^\infty \frac{x^2 e^{ux^2}}{x^6 + 8} dx \right), \quad (14.114)$$

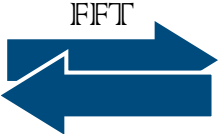
$$E_r = cB_\theta = \frac{8qr}{4\pi\epsilon_0 b^3 \xi^{2/3}} \times \left( \frac{e^u}{3} \cos(\sqrt{3}u) - \frac{e^u}{\sqrt{3}} \sin(\sqrt{3}u) - \frac{\sqrt{2}}{\pi} \int_0^\infty \frac{x^4 e^{ux^2}}{x^6 + 8} dx \right), \quad (14.115)$$

where:

$$u = \frac{z}{b\xi^{2/3}}. \quad (14.116)$$



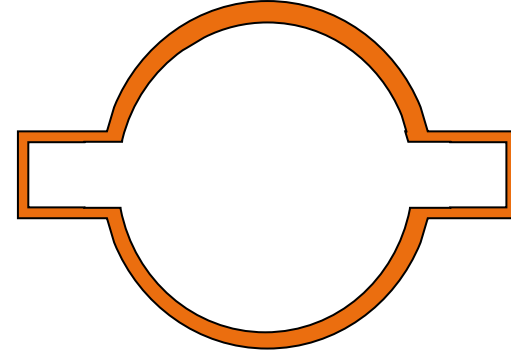
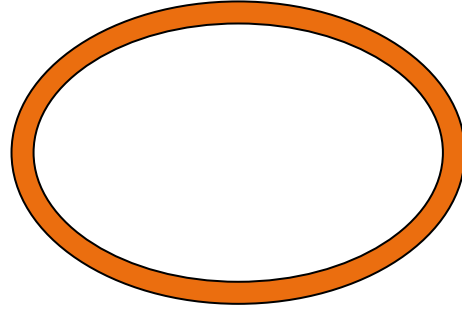
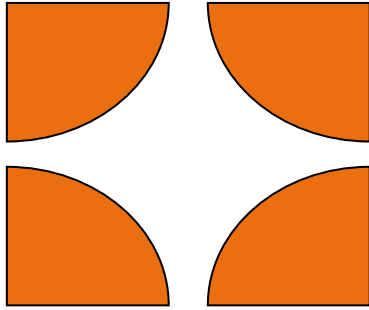
Wakefield



Impedance

# Resistive wall wake-field

## General Geometries



---

### Simulation Codes

CST   GDFIDL   IW2D   BeamImpedance2D  
VACI



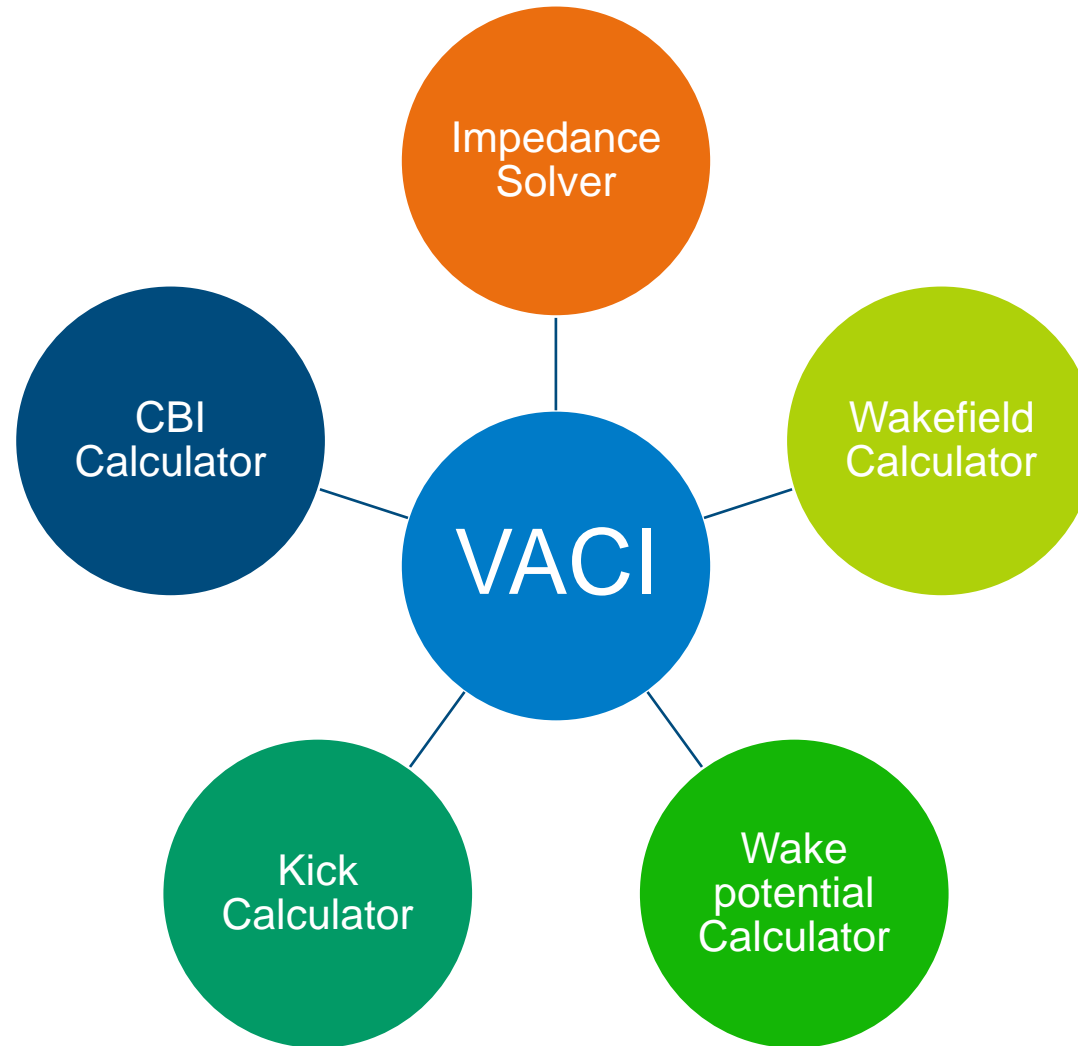


# VACI Suite

A versatile tool for calculating the RW impedance in arbitrary pipe cross-sections

# VACI Suite

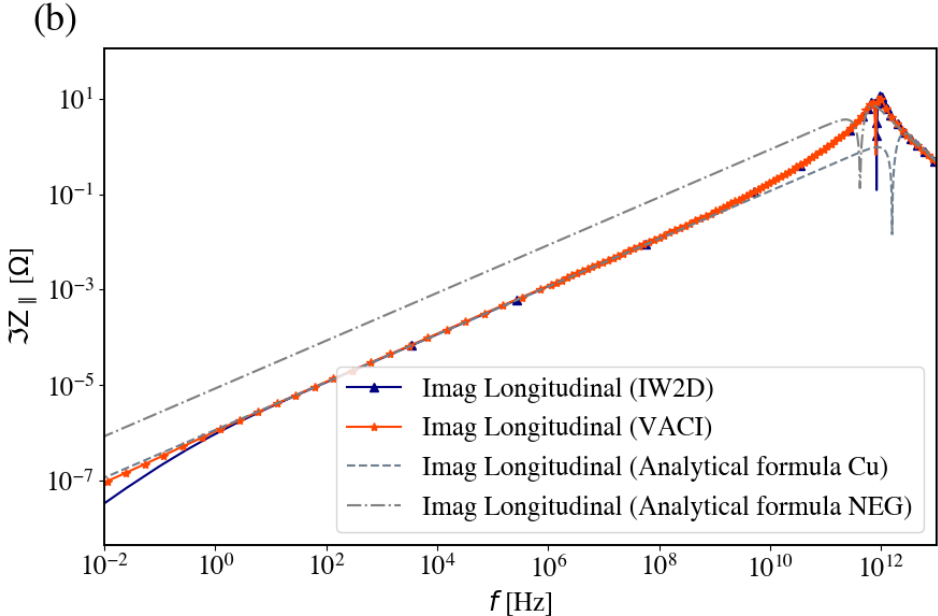
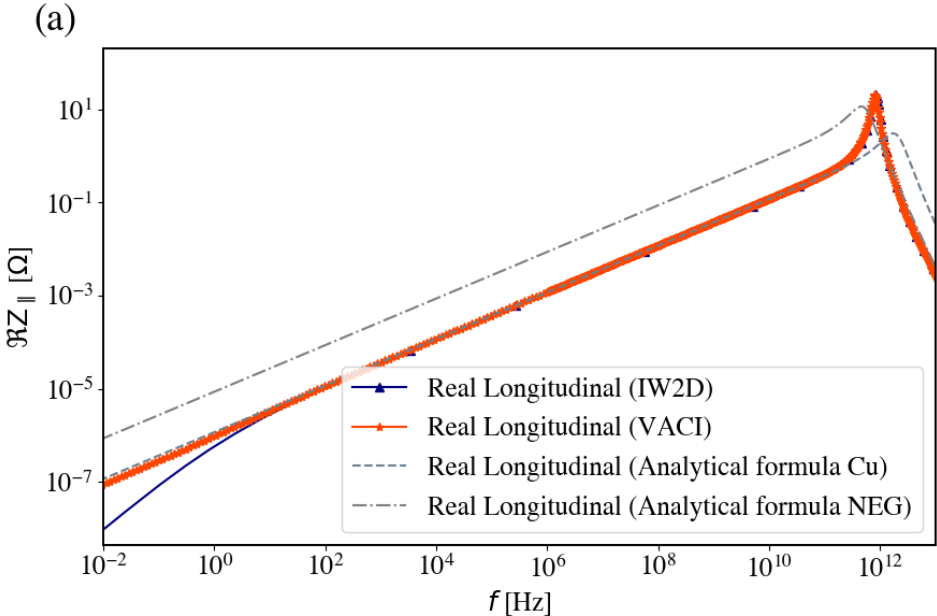
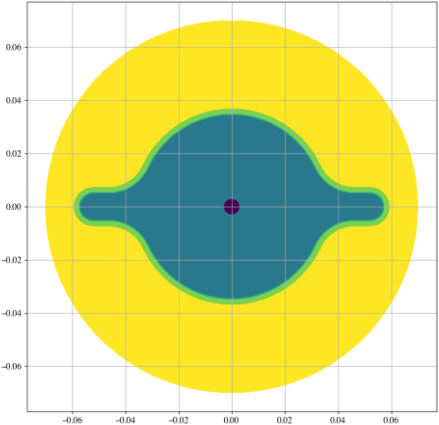
## Modules



# FCC main Ring

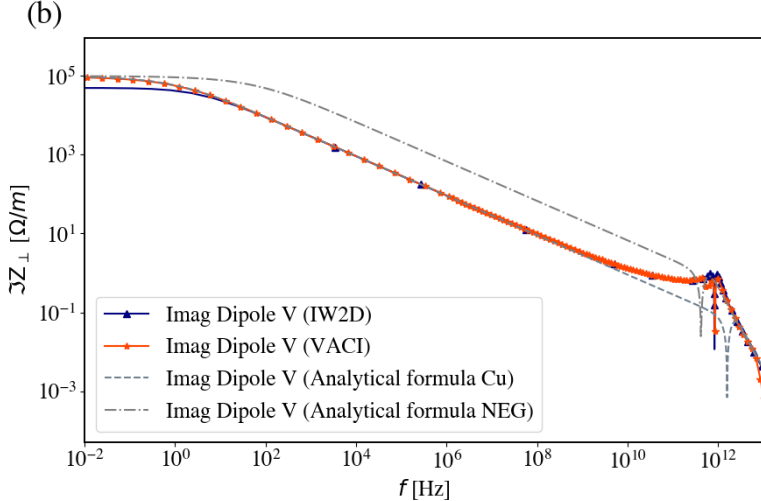
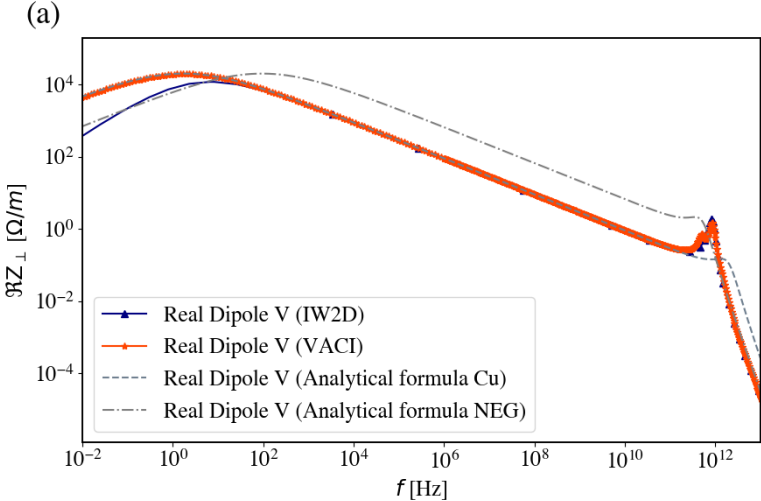
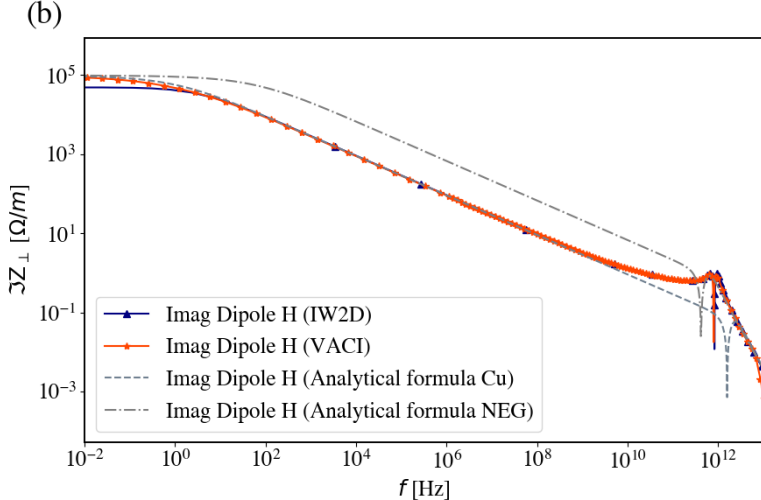
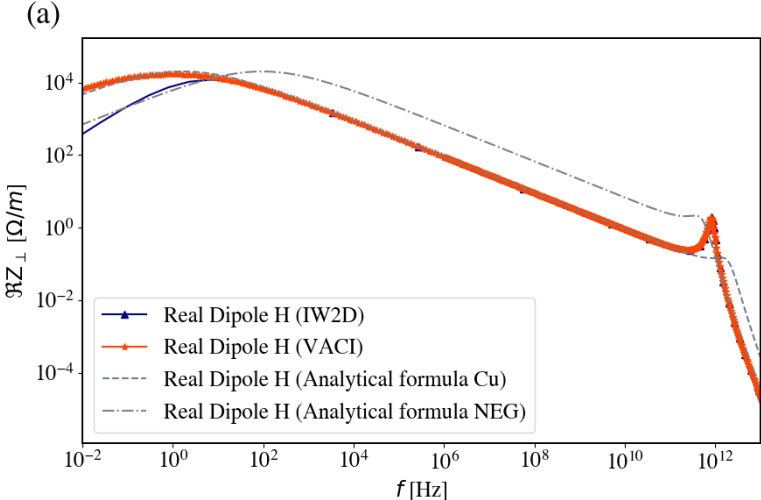
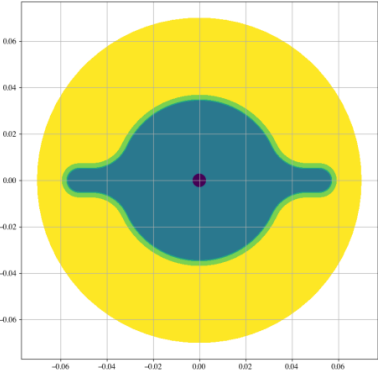
## Monopolar Impedance

E -> 45.6 GeV  
Pipe -> Cu (5.96e7 S/m)  
NEG -> 1e6 (S/m)  
R -> 35 mm



# FCC main Ring

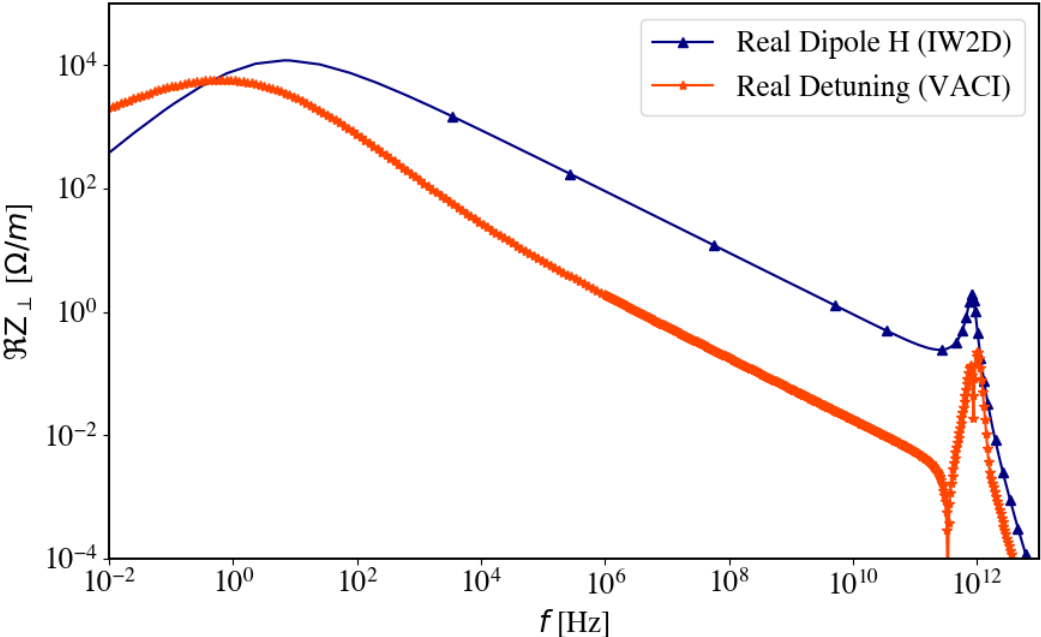
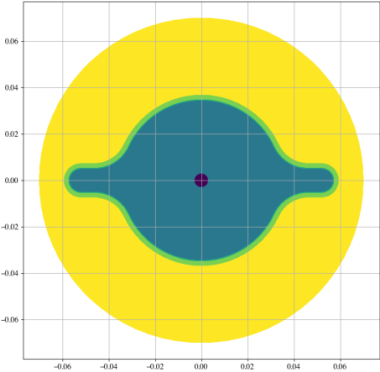
## Dipolar Impedance



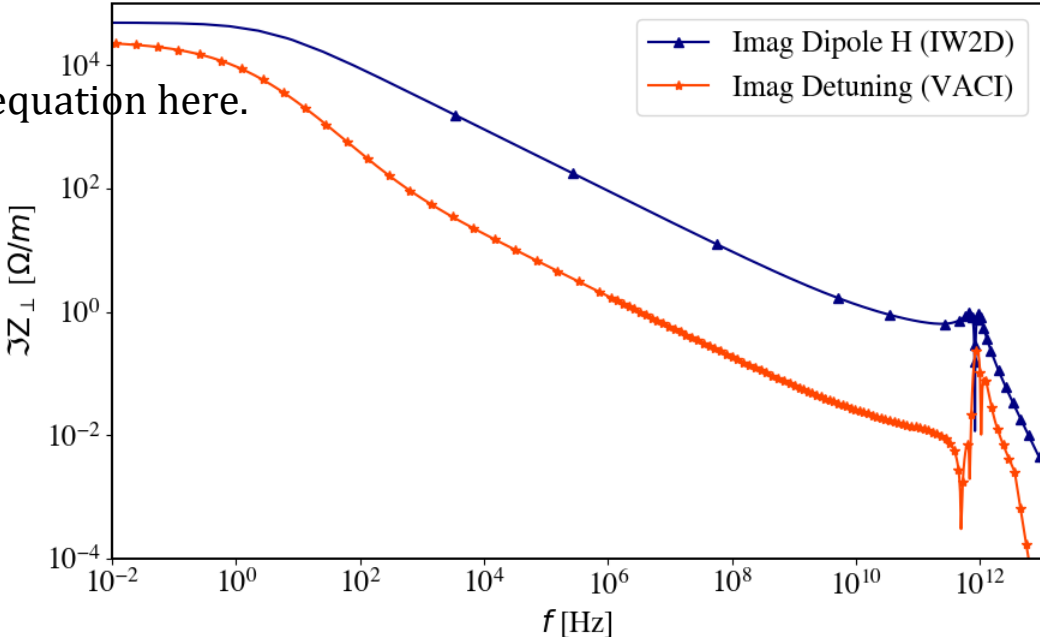
# FCC main Ring

## Detuning Impedance

$$W_x = x_s W_x^{dip} + x_w W_x^{det}$$

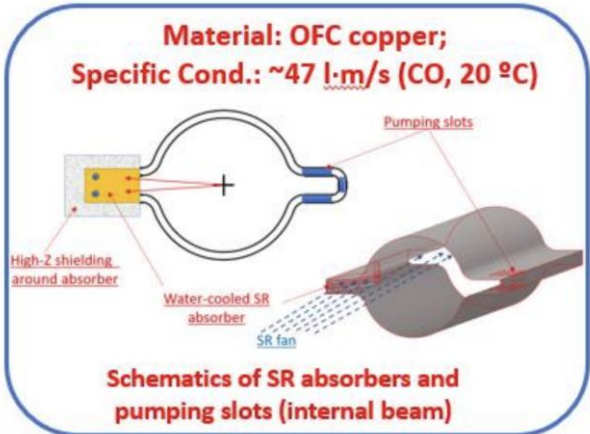
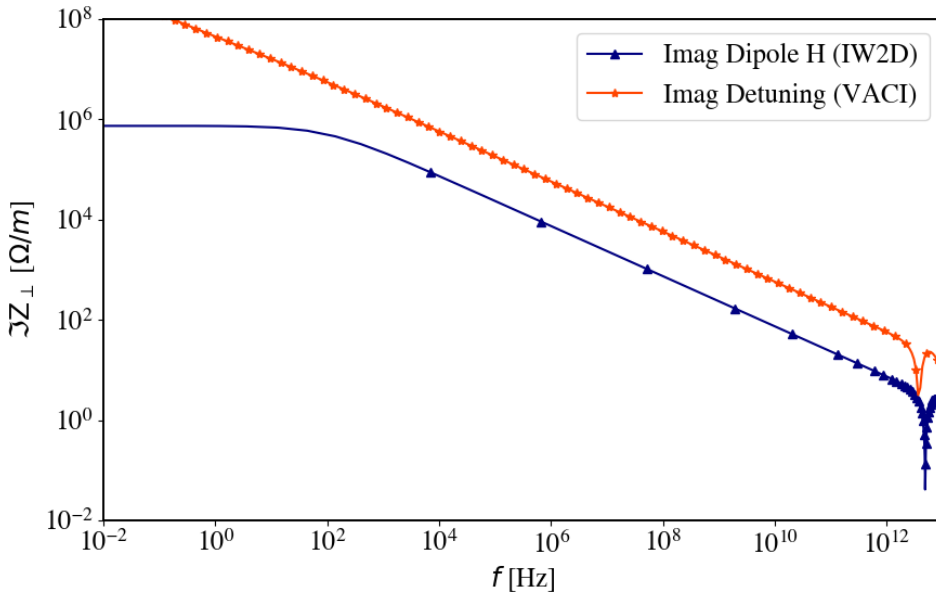
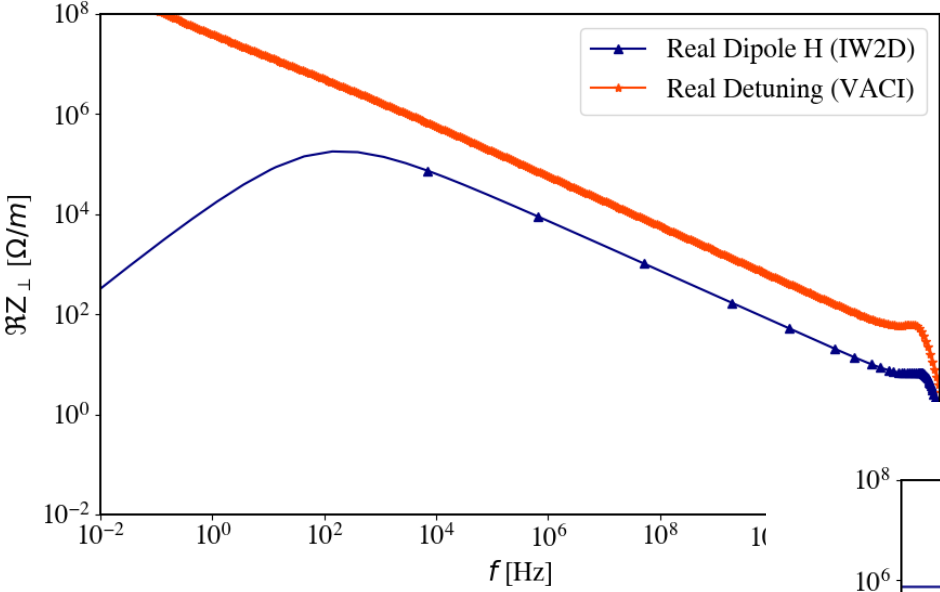


Type equation here.

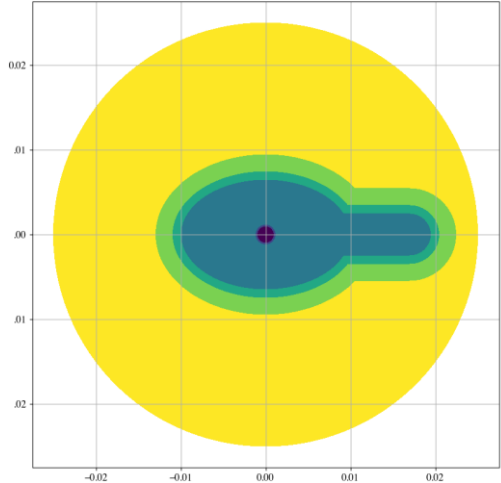


# FCC main Ring

## Considering absorbers



Presentation of R. Kersevan

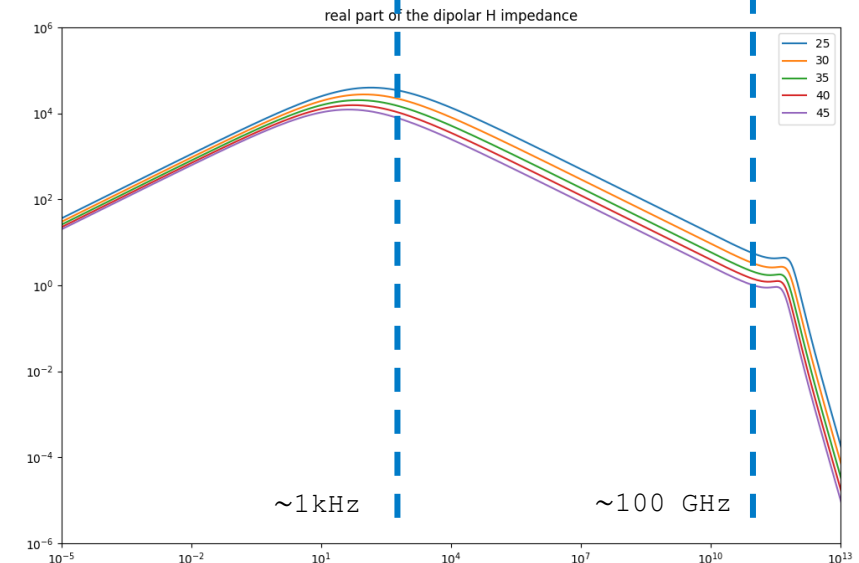
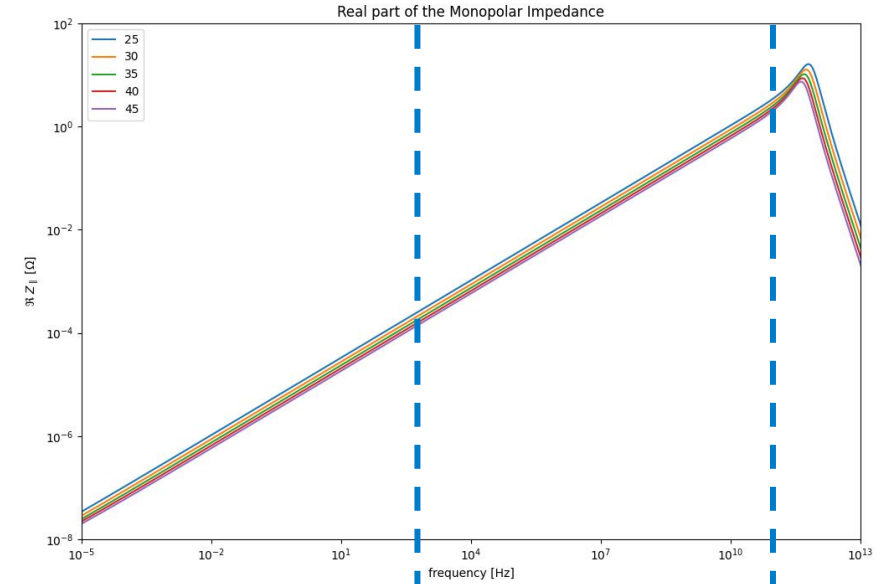


# FCC Booster Ring

Impedance, Stainless Steel, different radius

$$Z_{\parallel}(\omega) \equiv Z_0^{\parallel}(\omega) \approx (1 - i \operatorname{sgn}(\omega)) \frac{L}{2bc} \sqrt{\left(\frac{Z_0 c}{4\pi}\right) \frac{2|\omega|}{\pi\sigma}},$$

$$Z_{\perp}(\omega) \equiv Z_1^{\perp}(\omega) \approx (1 - i \operatorname{sgn}(\omega)) \frac{c L}{\omega b^3 c} \sqrt{\left(\frac{Z_0 c}{4\pi}\right) \frac{2|\omega|}{\pi\sigma}}.$$



# Instabilities



# Introduction

## Classification of beam instabilities

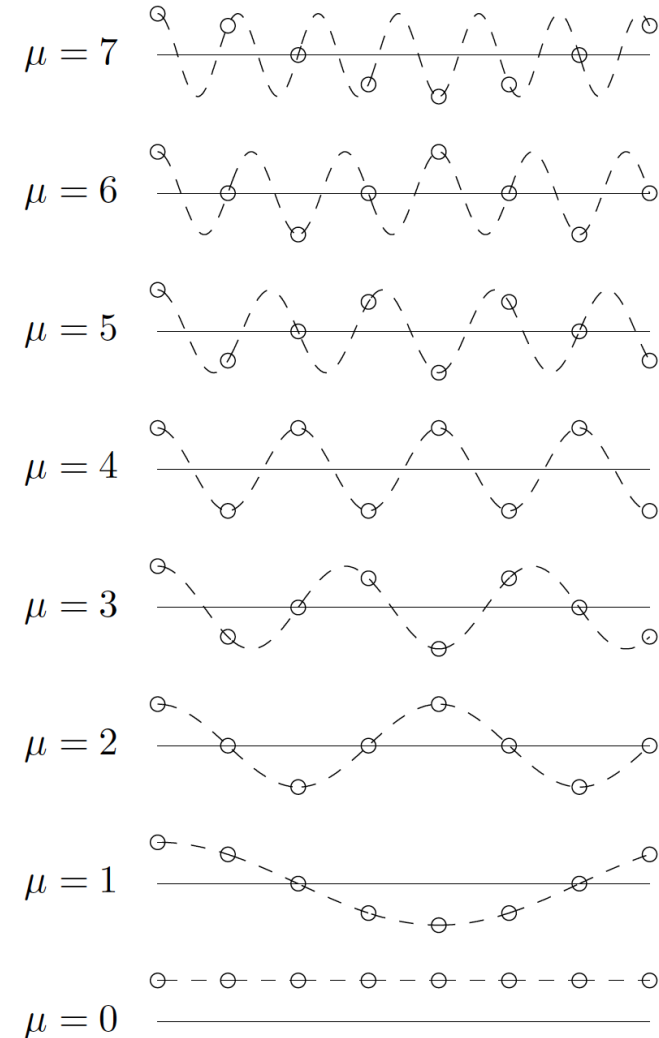
- Single-Bunch instabilities
  - Longitudinal single bunch collective effects
    1. Short-range longitudinal wakefields and broadband impedance
    2. Potential well distortion
    3. Longitudinal microwave instability
    4. Measurements
    5. CSR microbunching instability
  - Transverse single bunch collective effects
    1. Short-range transverse wakefields and broadband impedance
    2. Head-tail modes (e.g. TMCI) and chromaticity
    3. Measurements
    4. Damping with feedback
  - Intrabeam (IBS) and Touschek scattering
- Multi-bunch instabilities
  - Longitudinal Multibunch collective effects and cures
    1. Longitudinal coupled bunch instabilities
    2. Measurements
    3. Passive cures
    4. The Robinson Instability
    5. Harmonic RF systems
    6. Feedback systems
  - Transverse multibunch collective effects and cures
    1. Transverse coupled bunch instabilities
    2. Measurements
    3. Passive cures
    4. Feedback systems
  - Beam-Ion instabilities
  - Electron cloud instabilities

# Transverse coupled bunch instabilities

Due to RW impedance

$$\left\{ \begin{aligned} \frac{d^2 x_n}{dt^2} + \omega_\beta^2 x_n &= \frac{F_x}{\gamma_0 m N_b} \\ F_x &= -\frac{(q N_b)^2}{C_0} \sum_{k=0}^{\infty} \sum_{n'=0}^{n_b-1} W_1(z) x_{n'} \left( t + \frac{z}{c} \right) \\ z &= -\frac{(n' - n) C_0}{n_b} - k C_0 \end{aligned} \right.$$

$$\omega_\beta^2 - \Omega_\mu^2 = -\frac{q^2 N_b c^2}{E_0 C_0} \sum_{k=-\infty}^{\infty} \sum_{n'=0}^{n_b-1} W_1(z) e^{2\pi i \mu (n' - n) / n_b} e^{-i \Omega_\mu z / c}$$



# Transverse coupled bunch instabilities

Due to RW impedance

$$\omega_\beta^2 - \Omega_\mu^2 = -\frac{q^2 N_b c^2}{E_0 C_0} \sum_{k=-\infty}^{\infty} \sum_{n'=0}^{n_b-1} W_1(z) e^{2\pi i \mu (n' - n) / n_b} e^{-i \Omega_\mu z / c}$$

---

$$\Omega_\mu - \omega_\beta = -i \frac{4\pi}{Z_0 c} \frac{n_b N_b r_0 \omega_0 c}{8\pi^2 \gamma_0 \nu_x} \sum_{p=-\infty}^{\infty} Z_1^\perp(\omega_\beta + (\mu - n_b p) \omega_0) \quad n_b p = \frac{\Omega_\mu - \omega_p}{\omega_0} + \mu \quad \nu_x = \omega_\beta / \omega_0$$

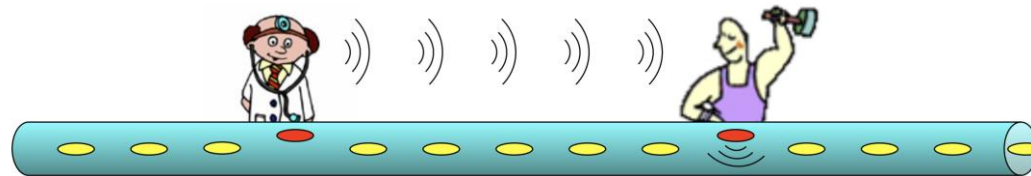
$$\mu - n_b p = -\text{int}(\nu_x) - 1 \quad \frac{1}{\tau} = \text{Im}(\Omega_\mu) = \frac{n_b N_b r_0 c}{4\pi^2 \gamma_0 \nu_x b^3} \sqrt{\left(\frac{4\pi}{Z_0 c}\right) \frac{c C_0}{\sigma} \frac{1}{\sqrt{1 - \text{frac}(\nu_x)}}}$$

# Transverse coupled bunch instabilities

## Due to RW impedance

$$\frac{1}{\tau} = \text{Im}(\Omega_{\mu}) = \frac{n_b N_b r_0 c}{4\pi^2 \gamma_0 \nu_x b^3} \sqrt{\left(\frac{4\pi}{Z_0 c}\right) \frac{c C_0}{\sigma} \frac{1}{\sqrt{1 - \text{frac}(\nu_x)}}$$

- Growth rate for transverse resistive wall CBI depends:
    - Strongly on the beam pipe radius  $\propto 1/b^3$
    - Weakly on the conductivity  $\propto \sqrt{1/\sigma}$
- Therefore, replacing the booster's beam pipe from copper (or stainless steel with a copper coating) to stainless steel, wherein we need to augment the beam pipe radius to offset the effects of TMCI, would be advantageous for CBI



Courtesy: Marco Lonza

# Outlooks

## Beam Dynamics with XSuite

- Impedance budget of booster ring (with Mauro Migliorati and Adnan Ghribi)
- TMCI for the main and booster rings with Xsuite (One turn Matrix)
- Distributed Wakefields and physical apertures with local wakefields (maybe, full Ring)
- Intrabeam scattering
- Multibunch tracking
- Feedback system
- Ramp-up

**Thank you**

**Contact**

Deutsches Elektronen-  
Synchrotron DESY

Ali Rajabi

Ali.rajabi@desy.de

[www.desy.de](http://www.desy.de)

+49 40 8998 3071