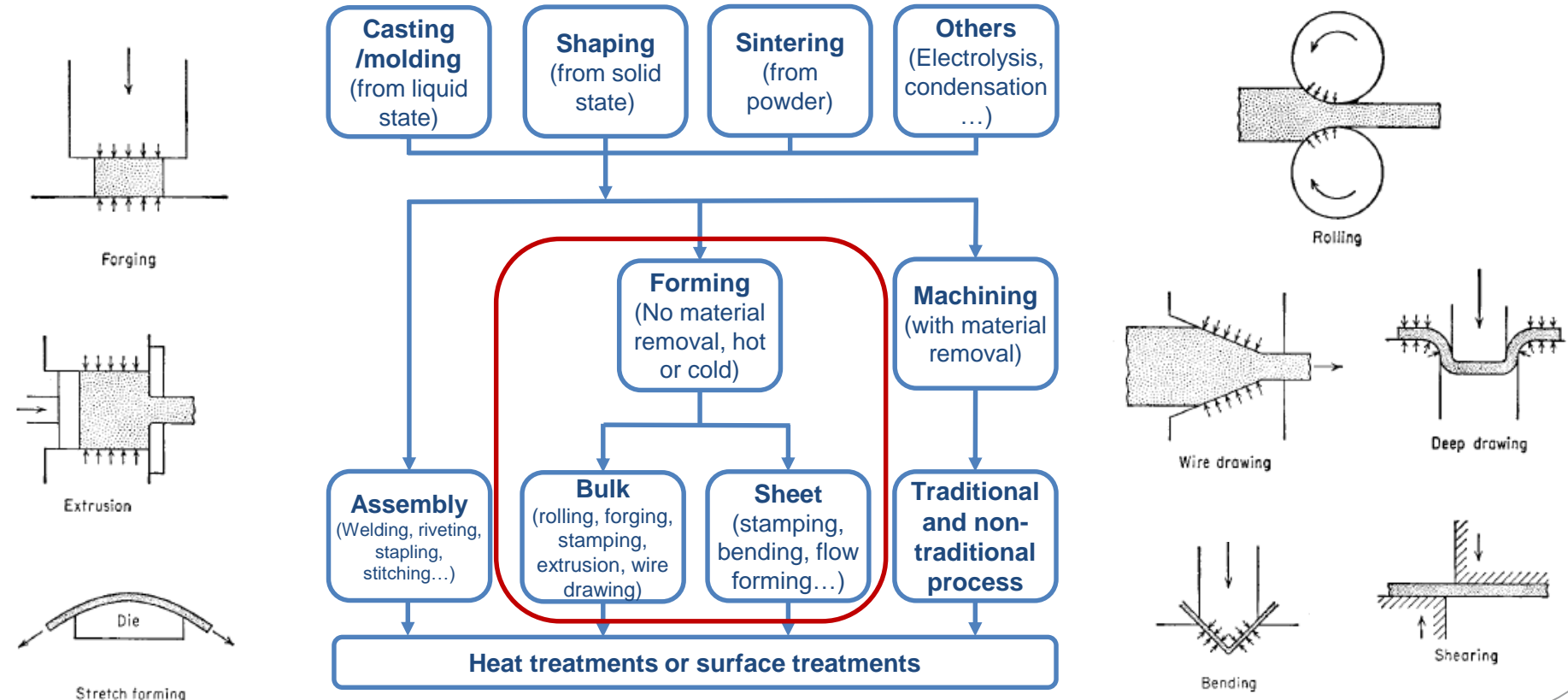


■ A short introduction to Materials forming

Charbel Moussa
charbel.moussa@minesparis.psl.eu

Objectives : shape the material and optimize the microstructure → the properties



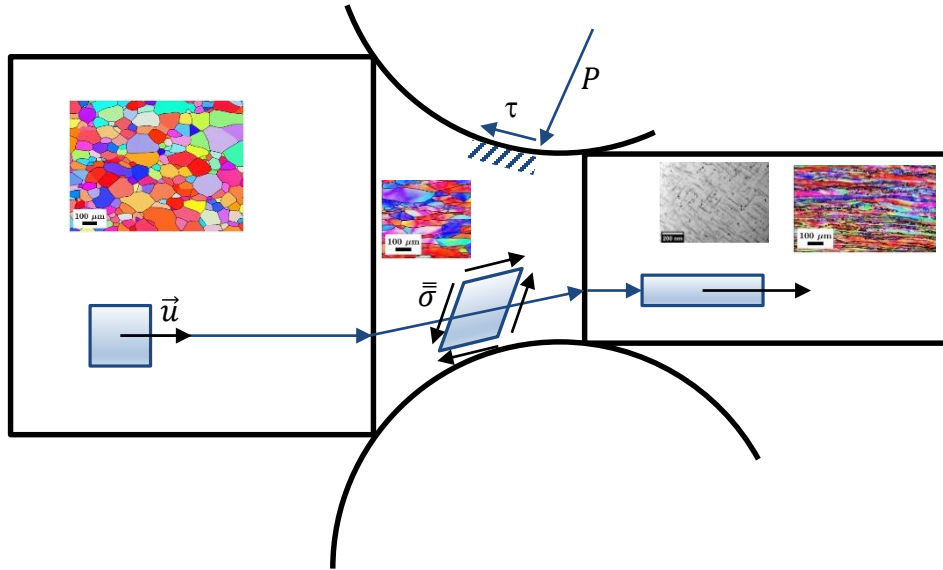
Evolution of various forms of metals and alloys forming processes

Primitive process	Date of emergence	Modern forms
Open die forging of hot product	5000 BC	Die forging, drop hammer, mechanical and hydraulic presses, cold/warm/for forging
casting	5000 BC	Pressure die casting in permanent and on-permanent molds, centrifugal castings of tubes, continuous castings of slabs, blooms and billets
Metal sheet forming by hammering, embossing	5000 BC	Stamping, shearing, bending, profiling, heavy sheet metal work, flowforming hydroforming, ironing of tubular products
Wire drawing	First centuries	Multi-passe wire drawing, profiles extrusion
Rolling	XVI century	Rolling in Tandem mill, reversible cage, universal cage, Sendzimir mill, Pilger mill for tubes, Mannesmann piercing mill
Cold extrusion of Pb and soft metals	XIX century	Hot and cold extrusion

Necessity to improve processes, for energy reduction, production cost, more complex geometric shapes and microstructural/properties control

Comparison of various processes of hot, warm and cold forming

	Cold ($T/T_M \approx 0.15$)	Warm ($T/T_M \approx 0.5$)	Hot ($T/T_M \approx 0.7-0.85$)
Processes	Rolling, forging, stamping, wire drawing, shearing, cutting	Forging, deep drawing	Rolling, forging, stretching, extrusion
Yield strength (steels)	200-1500 MPa	100-500 MPa	50 MPa
Product quality:			
- Dimensional tolerances	High	Average	Weak
- Surface condition	Very good	Good	Very bad
- Microstructure	Strain hardened	Strain hardened	Recovered or recrystallized
Lubrication	Various : emulsions, oils, soaps, soft metals (Sn...), polymers		Difficult: water, oils, graphite grease, glass



Material flow
Forces involved in the forming process
→ final shape of the product
Plasticity, ductility, damage ...

Heat flow
→ T evolution
Adiabatic heating, radiation, convection...

- Determines the energies involved in the forming process
→ various internal and surface defects (cracks, porosities, wrinkles orange peel effect...)
→ microstructure evolution (phases, grain size and shape, crystallographic texture, dislocations density...)
→ mechanical properties of the product, residual stresses...

Thermomechanical interactions material – lubricant – tools

→ surface state

Mechanical stresses (friction shear and contact pressure) and thermal stresses → modifies deformation conditions and tools wear

Lubricant → reduces those effects

Tool deformation → alteration of final dimensions

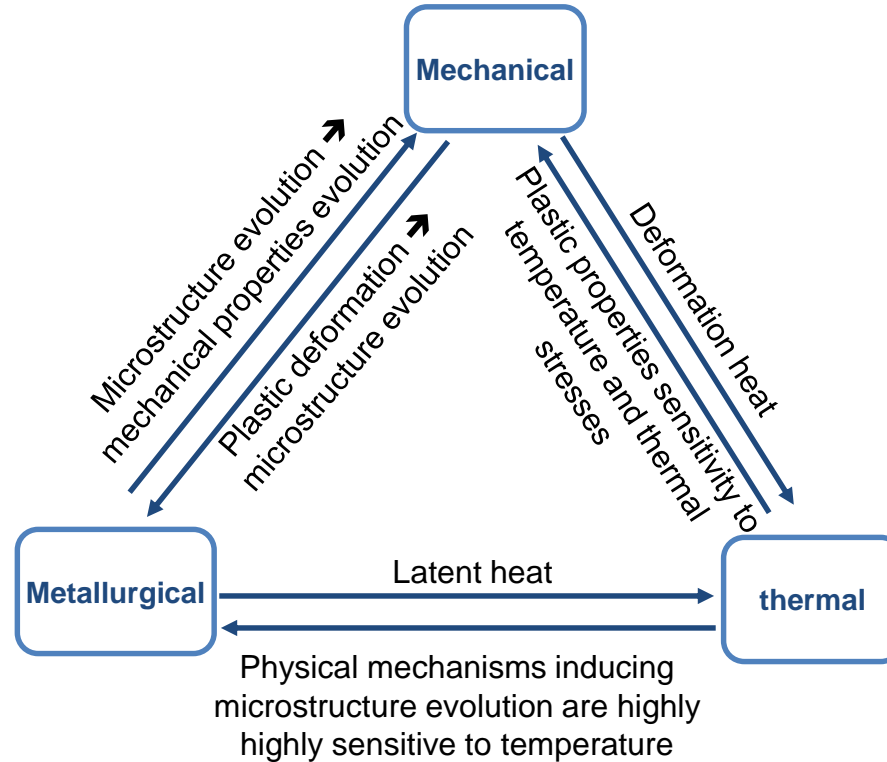
Thermal conduction, friction → T evolution

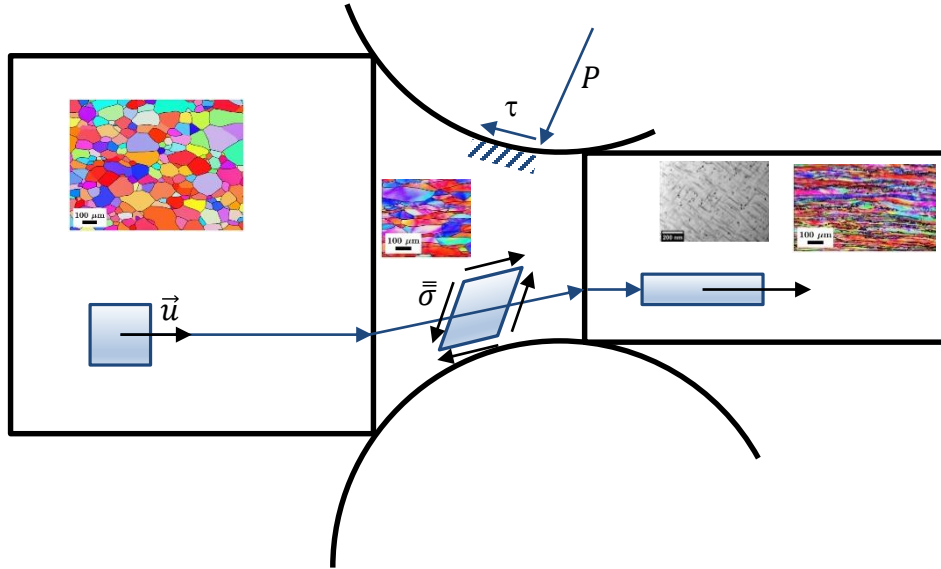
Microstructural evolution

Plasticity, recovery, recrystallization and phase transformation (diffusive and displacive)

→ Phases (volume fraction, size and shape), grain size and shape, crystallographic texture, dislocations density and sub-structures...),

→ Mechanical properties of the product, residual stresses...





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→ Phases (volume fraction, size and shape), grain size and shape, crystallographic texture, dislocations density and sub-structures...),

→ Mechanical properties of the product, residual stresses...

Steady or permanent flow if the velocity vector does not depend on time → the deformation zone does not change

Transient state : forging, stamping

Steady state: Rolling, wire drawing

High plastic deformation → plastic flow

Stress tensor ($\underline{\underline{\sigma}}_{ij}$), strain tensor ($\underline{\underline{\sigma}}_{ij}$) and strain rate tensor ($\underline{\underline{\dot{\epsilon}}}_{ij}$)

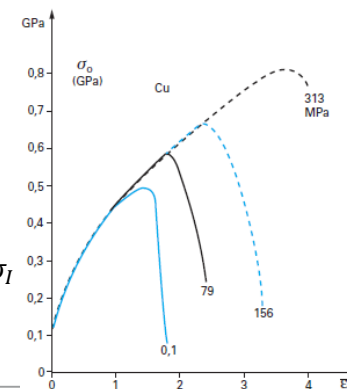
$$\underline{\underline{\sigma}}_{ij} = \underline{\underline{\sigma}} = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{pmatrix}_{(\vec{x}_1, \vec{x}_2, \vec{x}_3)} = \begin{pmatrix} \sigma_I & 0 & 0 \\ 0 & \sigma_{II} & 0 \\ 0 & 0 & \sigma_{III} \end{pmatrix}_{(\vec{1}, \vec{2}, \vec{3})}$$

Metallic materials → incompressible, no density evolution
 → Hydrostatic pressure → increase of material forming capacities

Hydrostatic stress tensor $\underline{\underline{\sigma}}_S$ and Deviatoric stress tensor $\underline{\underline{\sigma}}_D$

$$\left\{ \begin{array}{l} \underline{\underline{\sigma}} = \underline{\underline{\sigma}}_S + \underline{\underline{\sigma}}_D \\ tr(\underline{\underline{\sigma}}_D) = 0 \\ tr(\underline{\underline{\sigma}}_S) = tr(\underline{\underline{\sigma}}) = \sigma_{11} + \sigma_{22} + \sigma_{33} \\ \underline{\underline{\sigma}}_S = \frac{1}{3} tr(\underline{\underline{\sigma}}) \underline{\underline{I}} \\ \underline{\underline{\sigma}}_D = \underline{\underline{\sigma}} - \frac{1}{3} tr(\underline{\underline{\sigma}}) \underline{\underline{I}} \end{array} \right. \quad \left\{ \begin{array}{l} L_1 = tr(\underline{\underline{\sigma}}) = \sigma_{11} + \sigma_{22} + \sigma_{33} = \sigma_I + \sigma_{II} + \sigma_{III} \\ L_2 = \frac{1}{2} (tr^2(\underline{\underline{\sigma}}) - tr(\underline{\underline{\sigma}}^2)) = \frac{1}{2} (\sigma_{ii}\sigma_{jj} - \sigma_{ij}\sigma_{ij}) = \sigma_I\sigma_{II} + \sigma_{II}\sigma_{III} + \sigma_{III}\sigma_I \\ L_3 = det|\underline{\underline{\sigma}}| = \sigma_I\sigma_{II}\sigma_{III} \end{array} \right.$$

Tension tests under different hydrostatic pressures (Pugh, Sc. Publ. Ltd. London, 1971)



Steady or permanent flow if the velocity vector v does not depend on time \rightarrow the deformation zone does not change

Transient state : forging, stamping

Steady state: Rolling, wire drawing

High plastic deformation \rightarrow plastic flow

Stress tensor (σ_{ij}), strain tensor (σ_{ij}) and strain rate tensor ($\dot{\epsilon}_{ij}$)

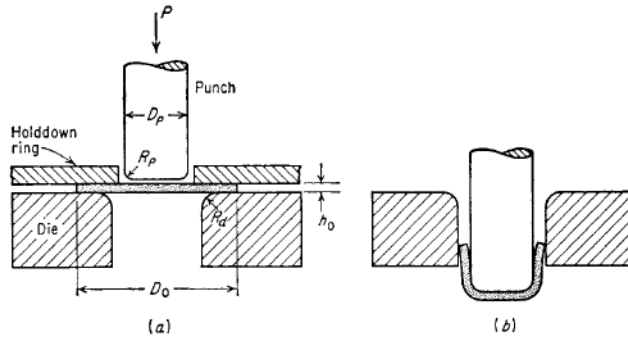
$$\underline{\underline{\sigma}}_{ij} = \underline{\underline{\sigma}} = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{pmatrix}_{(\vec{x}_1, \vec{x}_2, \vec{x}_3)} = \begin{pmatrix} \sigma_I & 0 & 0 \\ 0 & \sigma_{II} & 0 \\ 0 & 0 & \sigma_{III} \end{pmatrix}_{(\vec{1}, \vec{2}, \vec{3})}$$

Stress triaxiality represents the relative degree of hydrostatic pressure

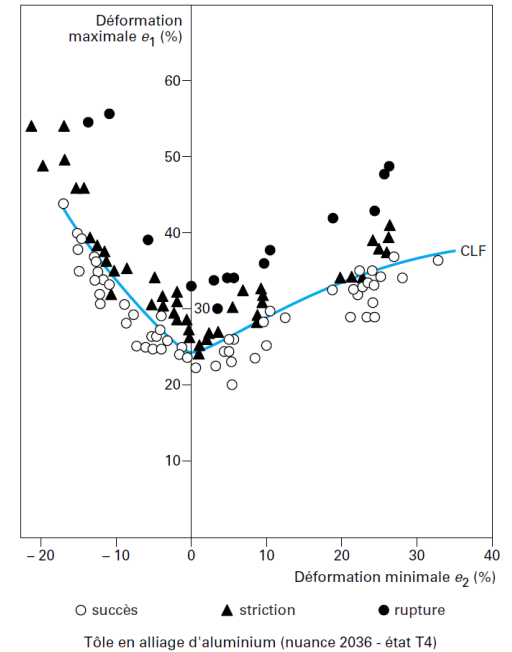
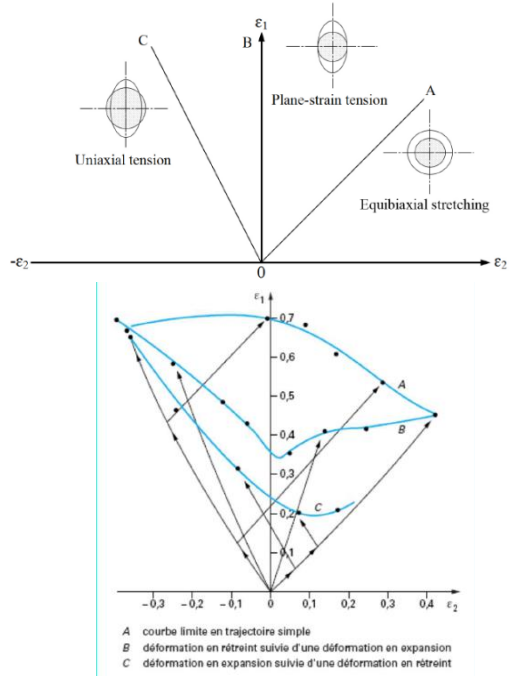
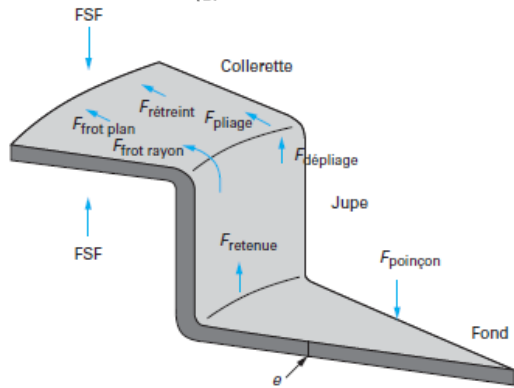
$$\eta = \frac{\frac{1}{3} Tr(\underline{\underline{\sigma}})}{\sigma_{eq}^{VM}}$$

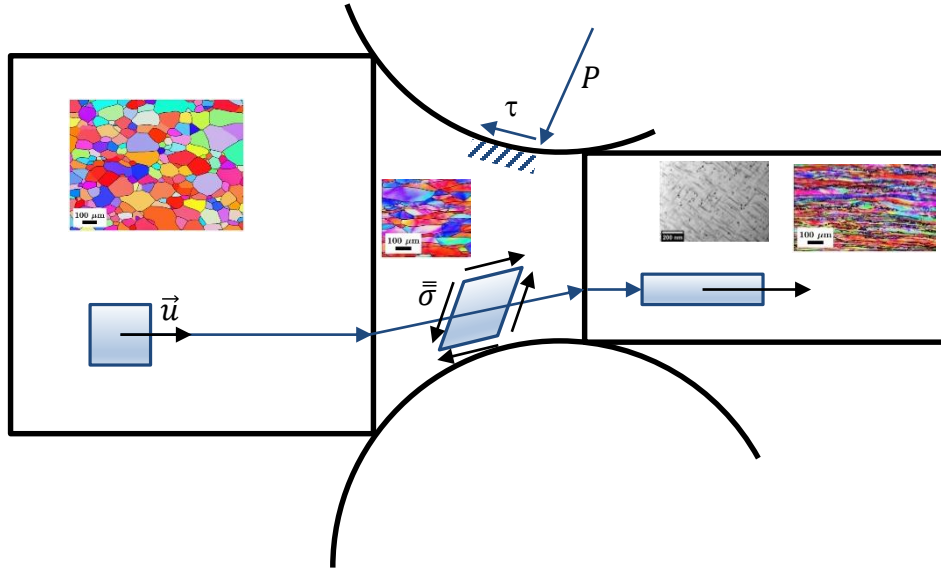
Materials forming processes are generally under negative triaxiality to increase ductility (forging rolling, extrusion...). For the ones under positive triaxiality (stamping), only small strains can be applied

- $\eta = 0$ \rightarrow Pure shear
- $\eta = 0,33$ \rightarrow Uniaxial tension
- $\eta = 0,66$ \rightarrow Equi-biaxial tension
- $\eta = -0,33$ \rightarrow Uniaxial compression
- $\eta = -0,66$ \rightarrow Equi-biaxial compression
- $\eta = -\infty$ \rightarrow Hydrostatic compression



Main deformation mode : Tension → small strain rates
 High sensitivity to anisotropy
 Because of effect of deformation mode (triaxiality) on ductility, simple tension test is not enough to predict failure





Material flow
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 → final shape of the product
 Plasticity, ductility, damage ...

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 → T evolution
 Adiabatic heating, radiation, convection...

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Thermomechanical interactions material – lubricant – tools

→ surface state

Mechanical stresses (friction shear and contact pressure) and thermal stresses → modifies deformation conditions and tools wear

Lubricant → reduces those effects

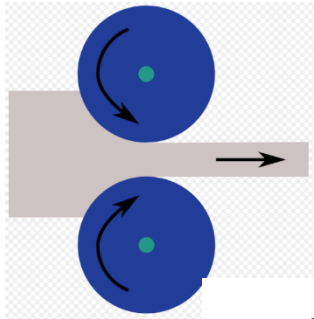
Tool deformation → alteration of final dimensions

Thermal conduction, friction → T evolution

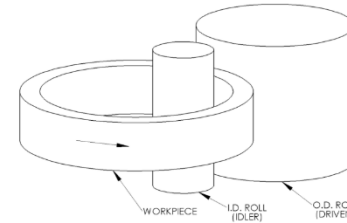
Microstructural evolution

Plasticity, recovery, recrystallization and phase transformation (diffusive and displacive)

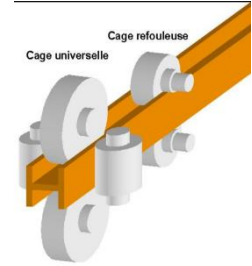
- Phases (volume fraction, size and shape), grain size and shape, crystallographic texture, dislocations density and sub-structures...)
- Mechanical properties of the product, residual stresses...



Wikipedia, 2020



Wikipedia, 2020



Wikipedia, 2020

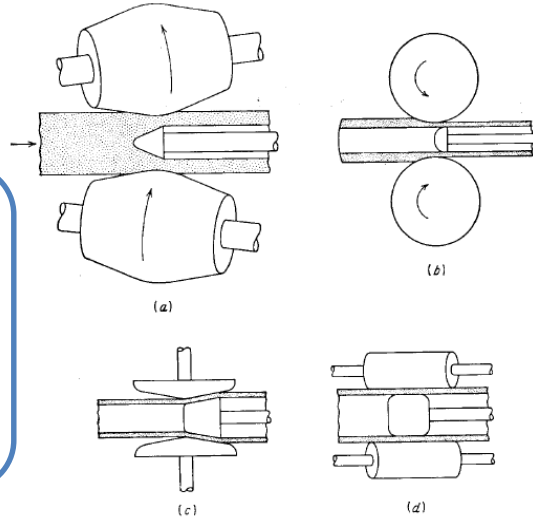


Figure 18-10 (a) Mannesmann mill; (b) plug rolling mill; (c) three-roll piercing mill; (d) reeling mill.

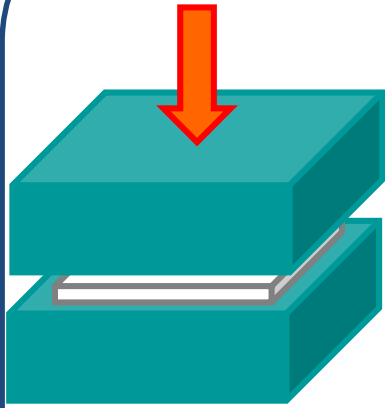
Dieter, Mechanical Metallurgy, 3rd edition, 1986

- Heavy plates
- Strips
- Bars
- Wire rod
- Beams
- Rails
- Tubes

% of total tonnage of uses and processes of semi-finished aluminum alloy products in France

Products	%	Process
Rolled	48.7	Plates casting and hot rolling
Bars and profiles	21.2	Billet casting and hot extrusion
Tubes	1	
Thin sheets	7.1	Cold rolling of hot rolled sheets
Conductive wires	14.7	Continuous casting – Hot rolling – Wire drawing
Wire rod	6	Continuous casting – Hot rolling
Poudre	1	

Flat products: Rolling vs free forging

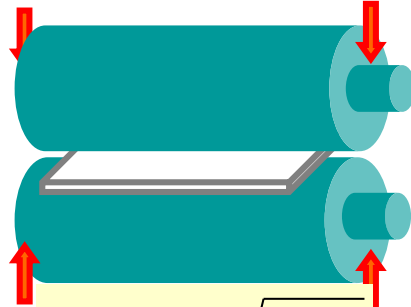


$$L = 5 \text{ m}$$

$$l = 2 \text{ m}$$

$$\sigma_0 = 100 \text{ MPa}$$

$$F = 10^9 \text{ N} = 100\,000 \text{ T} !!$$



$$L_{\text{contact}} \approx \sqrt{R \cdot \Delta h}$$

$$L_{\text{contact}} = 120 \text{ mm}$$

$$\text{if } R = 500 \text{ mm}$$

$$h \text{ } 100 \rightarrow 70 \text{ mm}$$

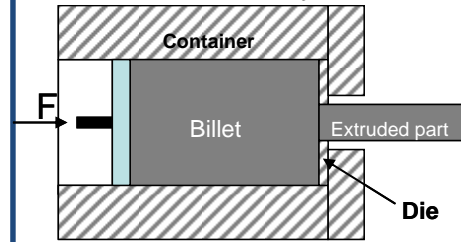
$$l = 2 \text{ m}$$

$$\sigma_0 = 100 \text{ MPa}$$

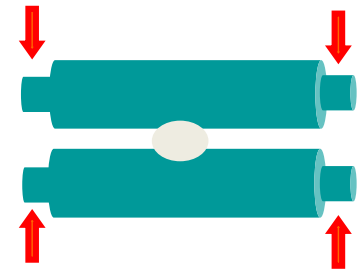
$$F = 24 \cdot 10^6 \text{ N} = 2\,400 \text{ T}$$

Long products: Rolling extrusion

$$F \geq S_0 \cdot L_n \frac{S_0}{S_f} \cdot \sigma_0$$



$$\Phi 100 \rightarrow \Phi 70$$



$$F \geq l \cdot L \cdot \sigma_0$$

With 2 passes:

$$\Phi 100$$

$$110 \times 60$$

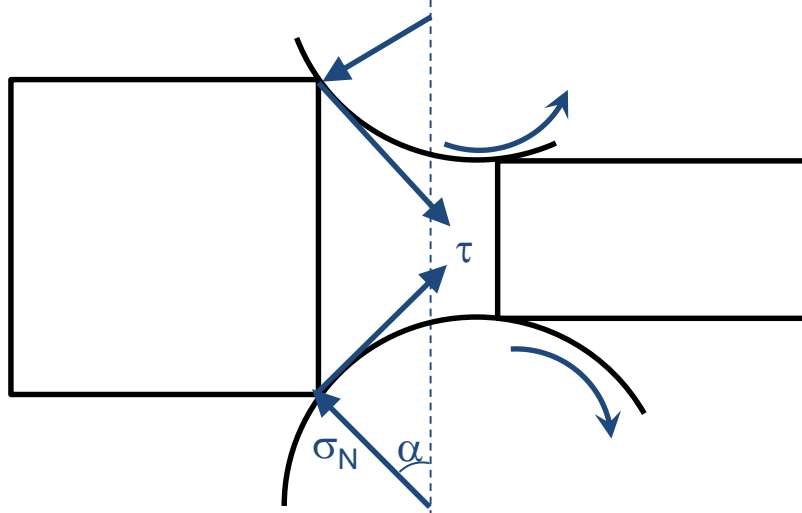
$$F > 56 \text{ T}$$

$$60 \times 110$$

$$\Phi 70$$

$$77 \text{ T}$$

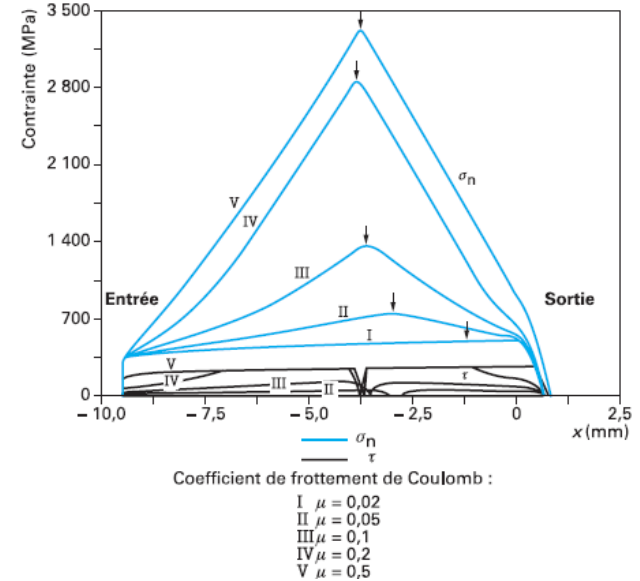
$$49 \text{ T}$$



$$\tau \cos \alpha - \sigma_N \sin \alpha \geq 0$$

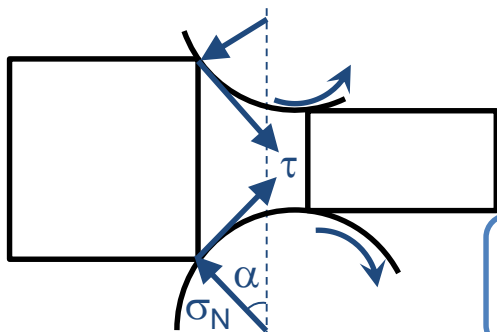
→ Friction coefficient $\mu = \frac{\tau}{\sigma_N} \geq \tan \alpha \approx \sqrt{\frac{\Delta h}{R}}$

A minimal amount of friction is necessary so the sheet can advance



- ↗ Reduction and /or ↗ friction → ↗ Load
- ↗ Tools deformation
- ↘ Geometrical precision
- ↗ Tools degradation (wear for example)

Effect of friction : Case of rolling



$$\tau \cos \alpha - \sigma_N \sin \alpha \geq 0$$

$$\Rightarrow \text{Friction coefficient } \mu = \frac{\tau}{\sigma_N} \geq \tan \alpha \approx \sqrt{\frac{\Delta h}{R}}$$

Small rollers for limited forces \rightarrow may fail to entrain the strip and may not be rigid enough

Example:

$\sigma_y = 100 \text{ MPa}$
 $R = 500 \text{ mm}$
 $V = 1.2 \text{ m/s}$
 $h = w = 400 \text{ mm}$
 25% reduction $\rightarrow \Delta h = 100 \text{ mm}$

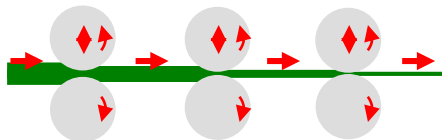


$$L_{\text{contact}} \approx \sqrt{R \times \Delta h} \approx 220 \text{ mm}$$

$$F \approx \sigma_y \times w \times L_{\text{contact}} \approx 8.8 \times 10^6 \text{ N} = 880 \text{ T}$$

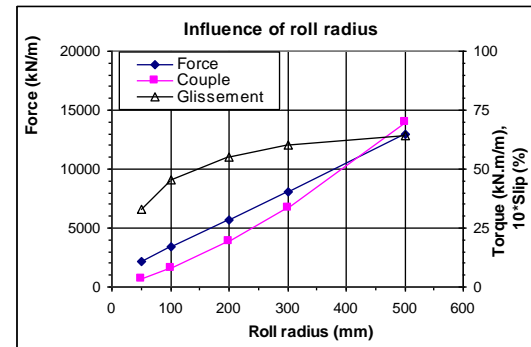
$$P \approx 10^7 W = 13000 \text{ HP}$$

$$\text{Torque} = \frac{P}{\omega} = 2.5 \times 10^6 \text{ N.m}$$



Multi-stand mill, single stand reversing mill, tandem mill

$\mu > 0.5$
 Only moderate reductions are possible
 \rightarrow ↗ number of passes

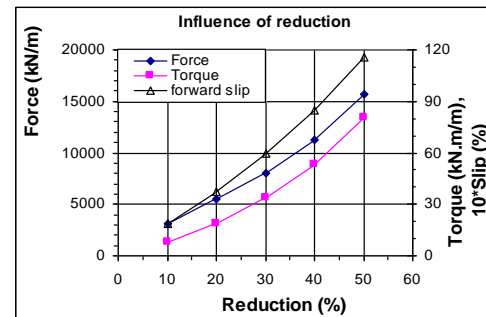


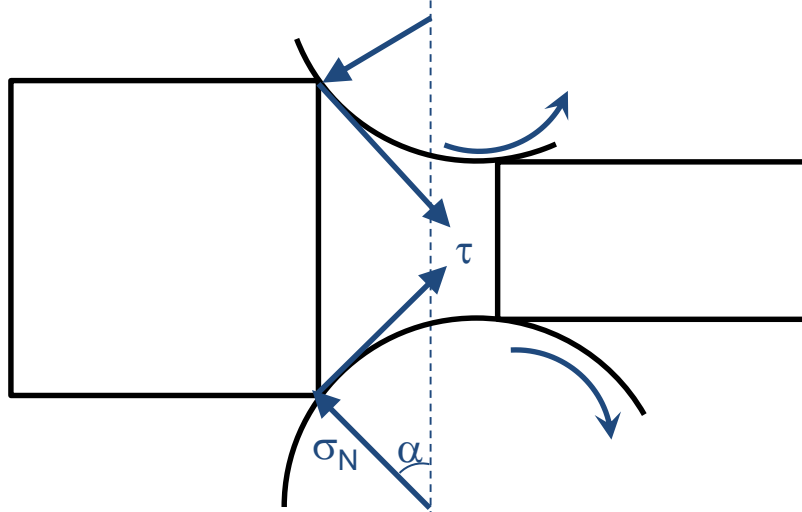
$$E = 210 \text{ GPa}, \nu = 0.3$$

$$\sigma (\text{MPa}) = 300(1 + 50\varepsilon)^{0.1}$$

$$\mu = 0.1$$

$$R = 300 \text{ mm}$$



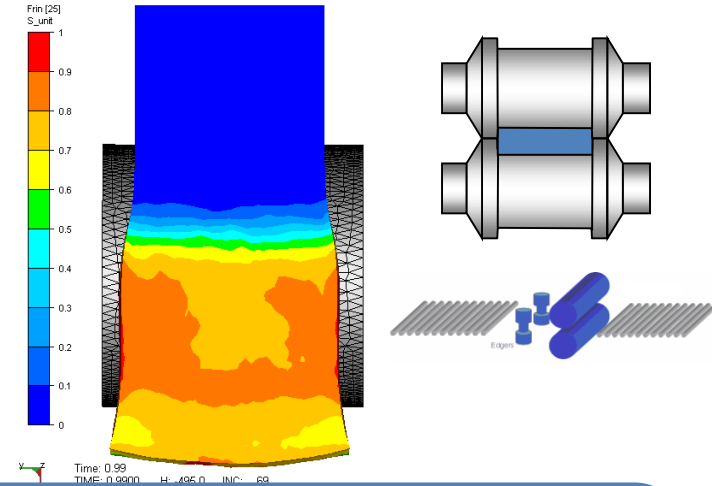


$$\tau \cos \alpha - \sigma_N \sin \alpha \geq 0$$

→ Friction coefficient $\mu = \frac{\tau}{\sigma_N} \geq \tan \alpha \approx \sqrt{\frac{\Delta h}{R}}$

Tribological condition: Minimum friction

Competition during the flow :
Compromise between geometric tolerance
and acceptable forces



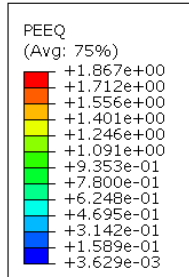
Lateral flow depends on anisotropy, friction and dimensions (Width W, bite length L and thickness H)

↗ W/H (flat) → ↘ lateral flow (spread)

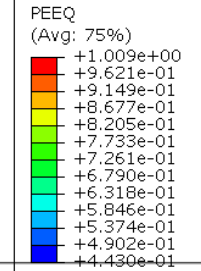
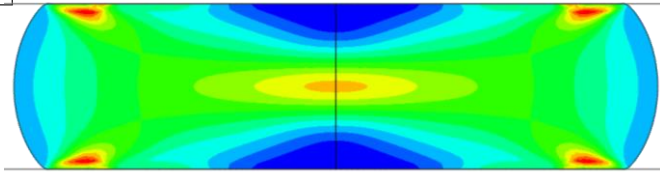
For W/L >> 1 (flat): ↗ friction → ↘ spread

For W/L ≈ 1 (long): ↗ friction → ↗ spread

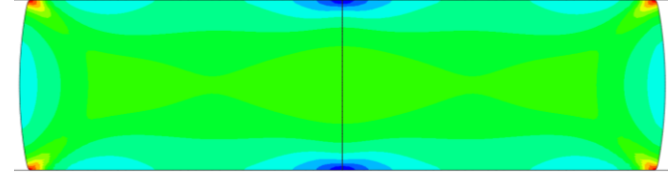
Plastic flow is mainly defined by boundary conditions and friction



Friction $\mu=0.4$



Friction $\mu=0.05$



↗ friction → ↗ shear in the contact region → ↗ plastic heterogeneity in terms of plastic deformation and deformation mode

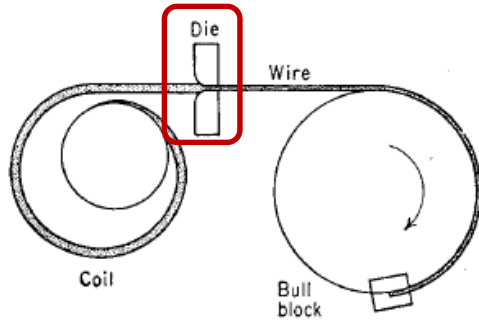
→ may induce some macroscopic defects

→ will induce microstructural heterogeneities and probably some properties heterogeneities

Hot rolling for wire until $D \approx 5\text{mm}$ then Wire drawing for $D < 5\text{mm}$

Series of cold operation followed by heat treatment to regain ductility (recovery and recrystallization)

Friction has an extreme importance



Dieter, Mechanical Metallurgy, 3rd edition, 1986

A : Die (diamond or carbides : CW, CCo)

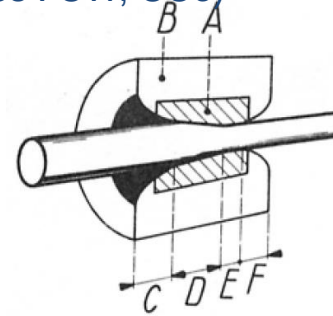
B: Steel casing

C: Bell radius

D: Entrance angle

E: Land

F: Back relief

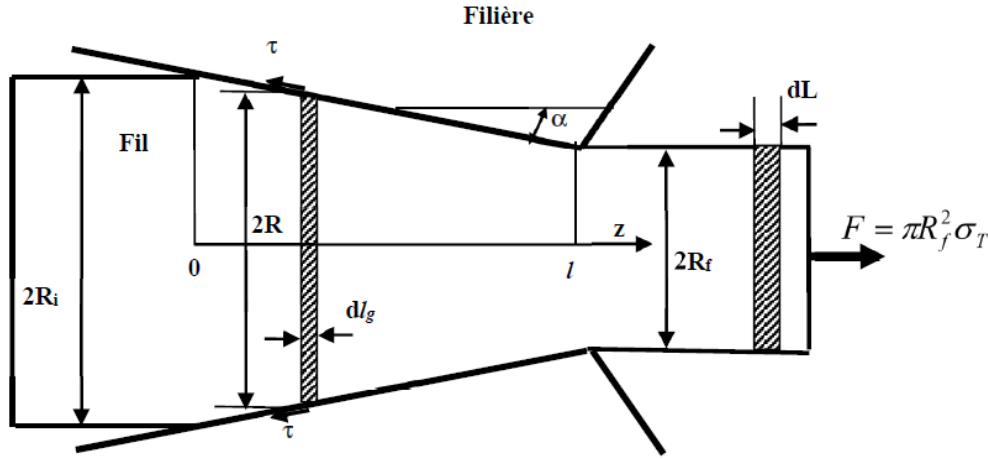


Complex geometries



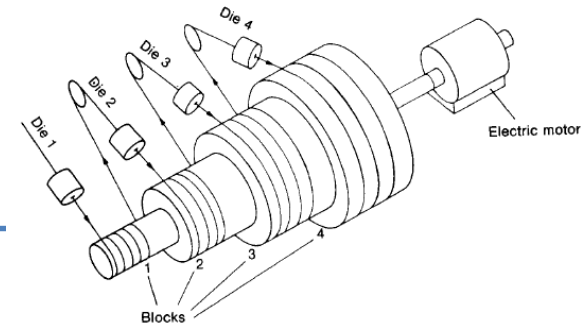
b





Wire drawing force

$$F = \pi R_f^2 \sigma_0 \left(1 + \frac{\bar{m}}{\sqrt{3}} \cot \alpha \right) \ln \left(\frac{R_i^2}{R_f^2} \right)$$

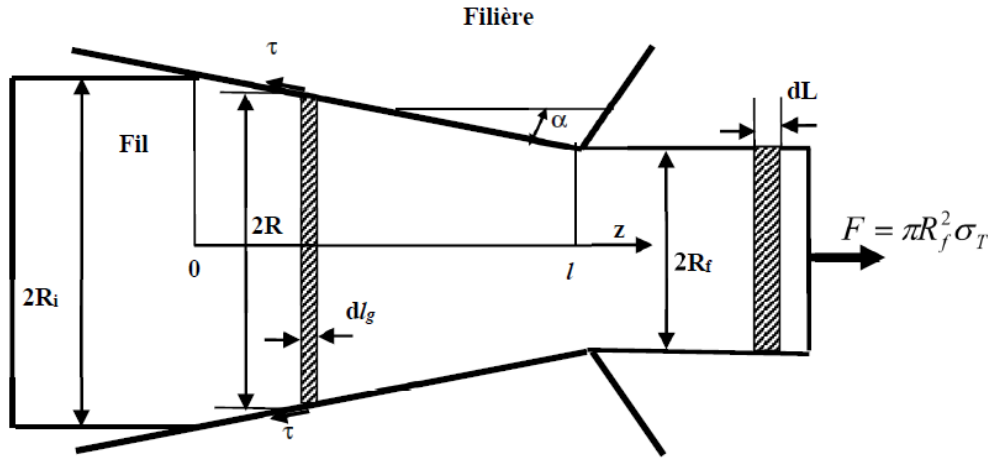


Dieter, Mechanical Metallurgy, 3rd edition, 1986

- ↗ Diameter reduction → ↗ Force
- ↗ Friction → ↗ Force (α small $\approx 6^\circ$ so $\cot \alpha$ is high $\approx 9,5$)
- To avoid that the operation transforms into a tensile test (negative triaxiality leading to damage) $\sigma_T = F / (\pi R_f^2) < \sigma_0$

→ The reduction should be smaller than a given value, the highest is the friction, the smallest is this value and the smallest is the reduction

→ Reduction is generally $1 - (R_f / R_i)^2 < 30\%$

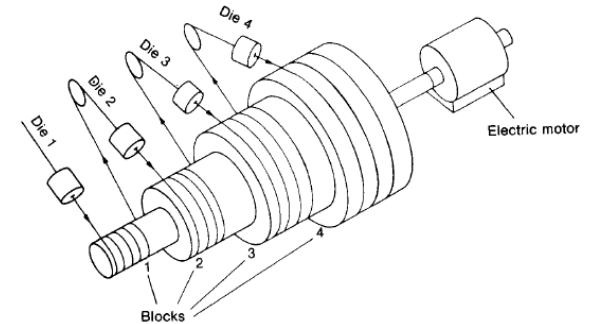


$$\text{Wire drawing force: } F = \pi R_f^2 \sigma_0 \left(1 + \frac{\bar{m}}{\sqrt{3}} \cot \alpha \right) \ln \left(\frac{R_i^2}{R_f^2} \right)$$

$$\text{Angle } \alpha \approx \left[\frac{\bar{m}}{0.77\sqrt{3}} \ln \left(\frac{R_i^2}{R_f^2} \right) \right]^{1/2}$$

$$\text{Plastic strain } \bar{\epsilon} = 2 \ln(R_i/R_f) + 0.77\alpha$$

- ↗ friction → ↗ α_{opt}
- For a reduction $r = 30\%$ and a friction coefficient $\bar{m} = 0,1$
 - $\alpha_{opt} = 9,3^\circ$ → consistent with experimental observations
 - $\bar{\epsilon} = 0,48$



Dieter, Mechanical Metallurgy, 3rd edition, 1986

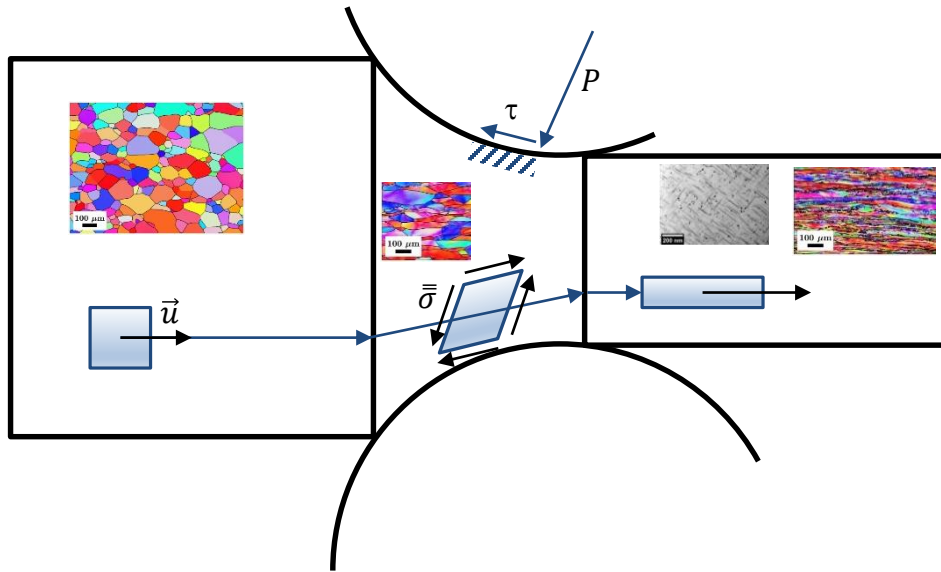
Effect of Friction:

- unavoidable during materials forming
- Increases the necessary forces and torques → increases stresses on tools
 - Increases temperature and Wear
- Modifies plastic flow by adding shear components → heterogeneous flow
- Heterogeneity of plastic flow and temperature → heterogeneous microstructure and properties

Friction depends on :

- The nature of the materials in contact : Workpiece, tool
- The surface state of these materials: roughness, surface treatments...
 - The lubricant: chemical nature, viscosity, quantity...
- Contact conditions, temperature,, sliding speed, normal stress...

Tribology consist in controlling friction and wear using lubrication and surface coatings



Material flow

Forces involved in the forming process
→ final shape of the product
Plasticity, ductility, damage ...

Heat flow

→ T evolution
Adiabatic heating, radiation,
convection...

- Determines the energies involved in the forming process
→ various internal and surface defects (cracks, porosities, wrinkles orange peel effect...)
→ microstructure evolution (phases, grain size and shape, crystallographic texture, dislocations density...)
→ mechanical properties of the product, residual stresses...

Thermomechanical interactions material – lubricant – tools

→ surface state

- Mechanical stresses (friction shear and contact pressure) and thermal stresses → modifies deformation conditions and tools wear
Lubricant → reduces those effects
Tool deformation → alteration of final dimensions
Thermal conduction, friction → T evolution

Microstructural evolution

- Plasticity, recovery, recrystallization and phase transformation (diffusive and displacive)
→ Phases (volume fraction, size and shape), grain size and shape, crystallographic texture, dislocations density and sub-structures...
→ Mechanical properties of the product, residual stresses...

Thermoplastic effect

$$\dot{Q}_{plastique} = \beta \cdot \sigma_0 \cdot \dot{\epsilon}$$

Heat transfer towards the tools

$$\phi_{contact} = h_{contact} \cdot (T - T_{tools})$$

Heat transfer by radiation

$$\phi_{radiation} = \epsilon_{emissivity} \cdot \sigma_{stefan} \cdot (T^4 - T_{\infty}^4)$$

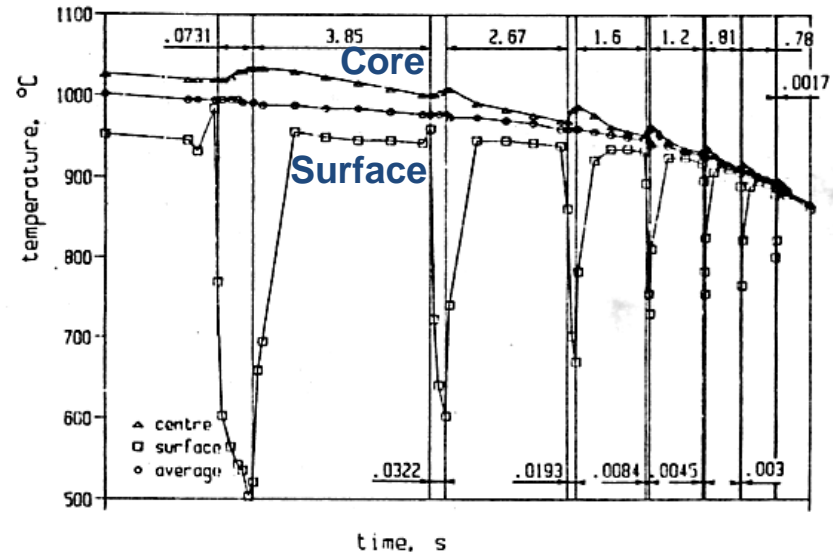
Heating by friction

$$\dot{Q}_{friction} = \tau \cdot \Delta v =$$

Heat transfer by convection

$$\phi_{convection} = h_{convection} \cdot (T - T_{\infty})$$

Generally, 5-10°C per pass in hot rolling
Up to 100°C per pass in cold rolling by

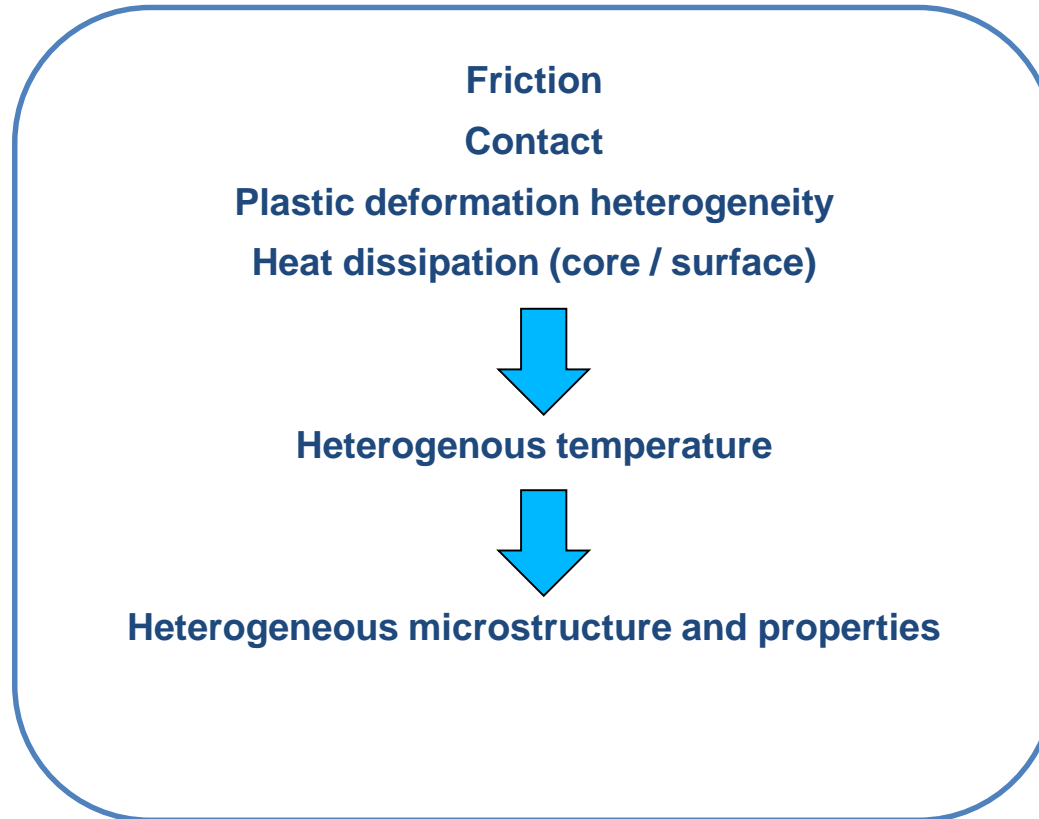


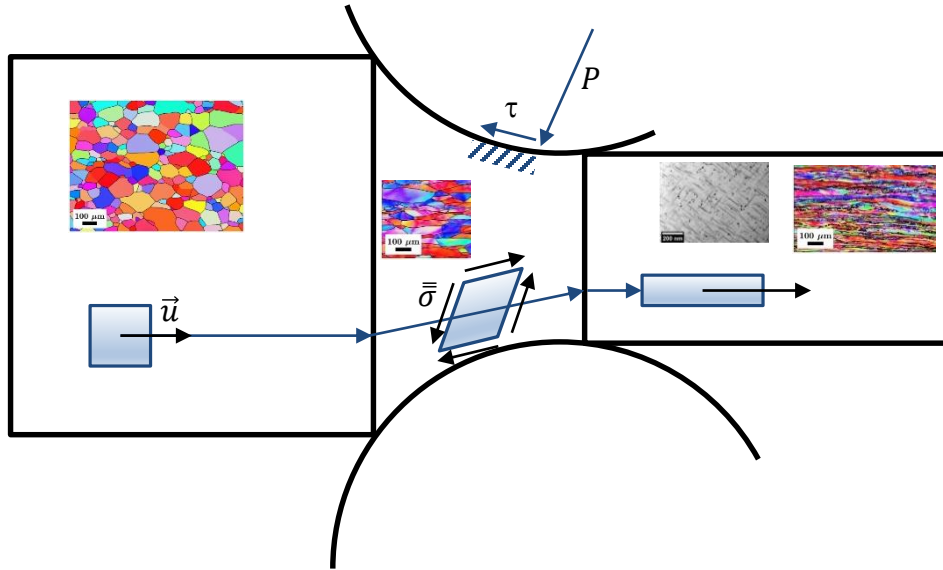
Advantages of hot forming:

- ⚡ hardness → ⚡ necessary Forces → ↗ workpiece dimensions
 - ↗ ductility → ↗ plastic strains and reductions
- Activation of recovery and recrystallisation → renew of the microstructure and ↗ ductility

Advantages of cold forming:

- Work hardening → ↗ mechanical resistance of final piece
 - Higher geometrical precisions
 - Better surface (no oxides for ex.)





Material flow
 Forces involved in the forming process
 → final shape of the product
 Plasticity, ductility, damage ...

Heat flow
 → T evolution
 Adiabatic heating, radiation, convection...

- Determines the energies involved in the forming process
- various internal and surface defects (cracks, porosities, wrinkles orange peel effect...)
- microstructure evolution (phases, grain size and shape, crystallographic texture, dislocations density...)
- mechanical properties of the product, residual stresses...

Thermomechanical interactions material – lubricant – tools

→ surface state

Mechanical stresses (friction shear and contact pressure) and thermal stresses → modifies deformation conditions and tools wear

Lubricant → reduces those effects

Tool deformation → alteration of final dimensions

Thermal conduction, friction → T evolution

Microstructural evolution

Plasticity, recovery, recrystallization and phase transformation (diffusive and displacive)

- Phases (volume fraction, size and shape), grain size and shape, crystallographic texture, dislocations density and sub-structures...)
- Mechanical properties of the product, residual stresses...

Plasticity + temperature



Plasticity : dislocation slip, Twinning induced plasticity and Transformation induced plasticity

→ ↗ of dislocation density, texture evolution, twin boundaries and phases volume fraction

Recovery and recrystallization

→ ↘ of dislocation density, evolution of texture, grain size and grains shape

Phase transformation

→ Modifies the phase volume fraction

All those mechanisms are coupled

Deformation textures

Deformation occurs on the most favorably oriented slip → Preferred orientation during plastic deformation
 → Deformation texture

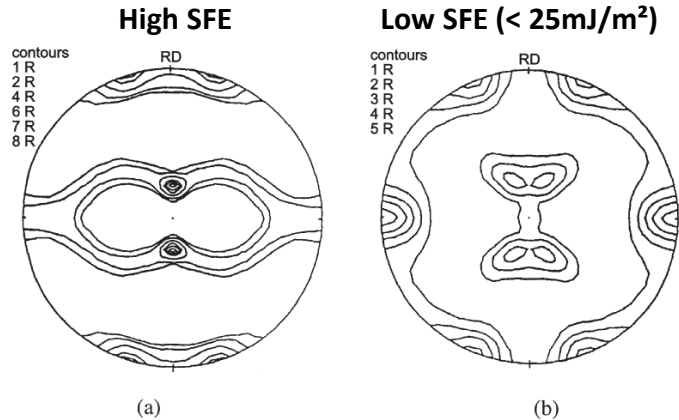


Fig. 3.1. 111 Pole figures of 95% cold rolled fcc metals; (a) copper; (b) 70:30 brass, (Hirsch and Lücke 1988a).

FCC

Depends on the alloy and the deformation conditions
 Abundant literature on rolling texture

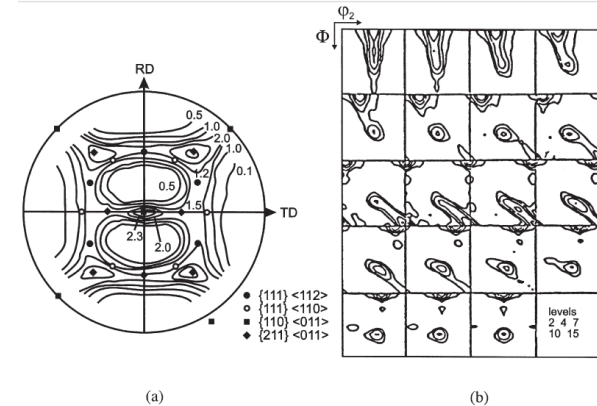


Fig. 3.9. Rolling texture of 90% cold rolled low carbon steel; (a) 200 pole figure (Hutchinson 1984); (b) ODF (Lücke and Hölscher 1991).

BCC

Factors influencing deformation textures

SFE and purity level

Texture of the initial state

Deformation conditions

Rolling: Theoretically plane deformation → uniform texture in the thickness

Rolling geometry and friction → Texture gradient in the thickness

↘ D roller, ↘ reduction per pass, ↗ thickness of the sheet → ↗ texture gradient in the thickness

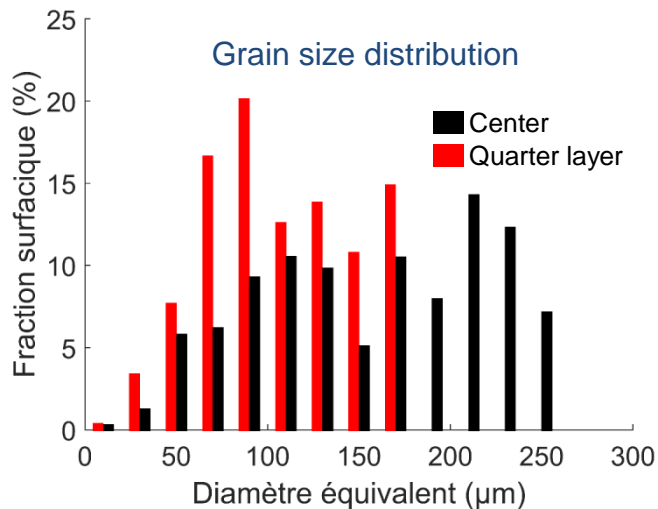
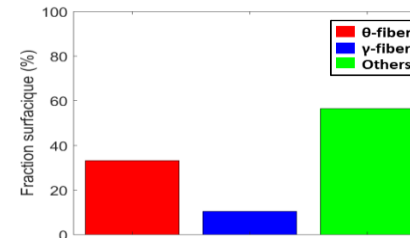
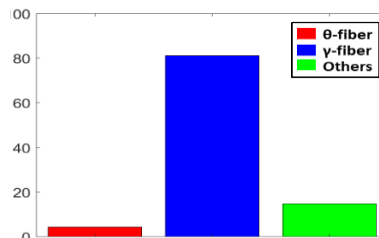
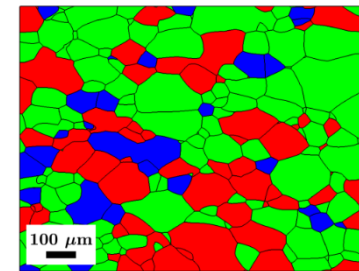
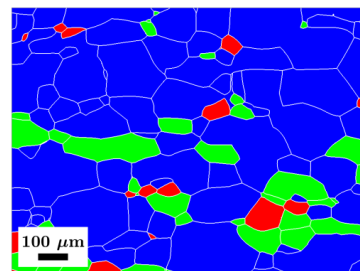
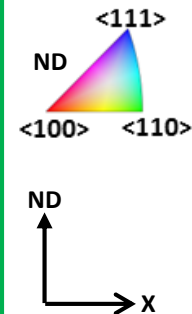
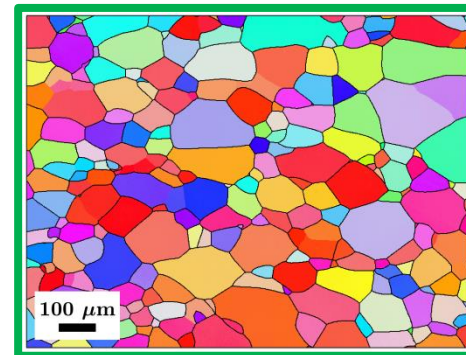
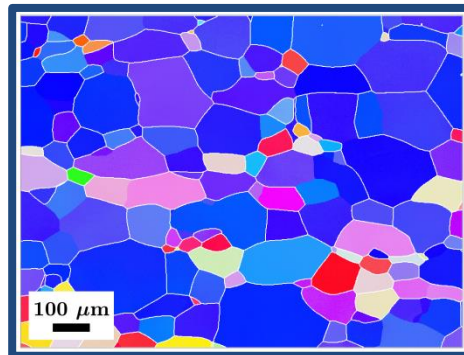
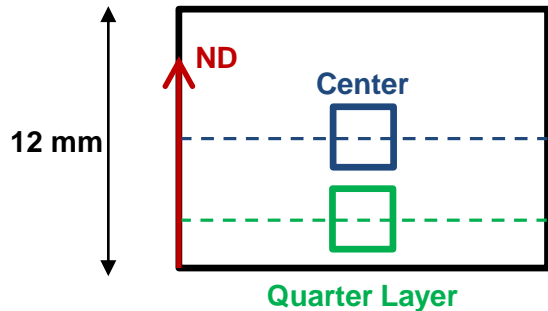
↗ Friction → ↗ texture gradients

Deformation temperature

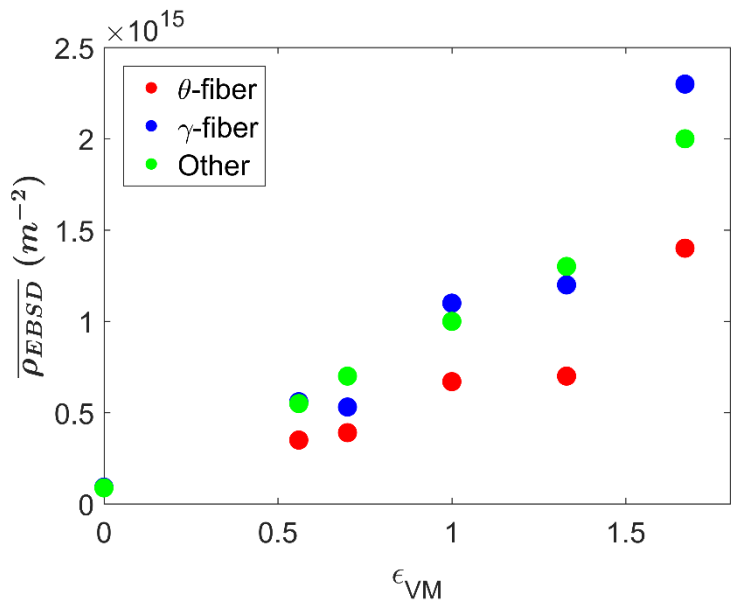
Grain size

Second phase particles

Pure Tantalum BCC

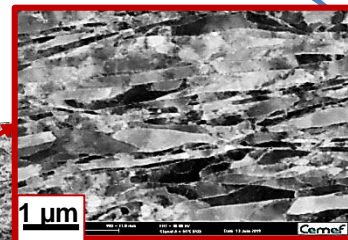
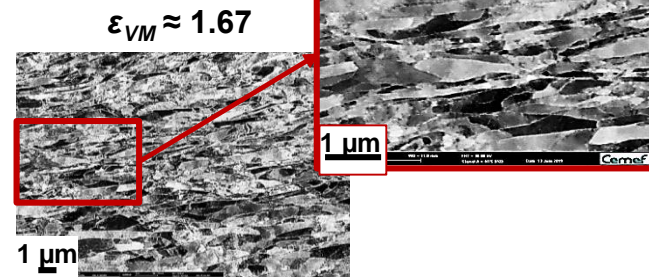
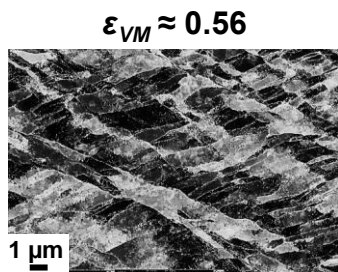


Anisotropic behavior: dislocation content after cold deformation

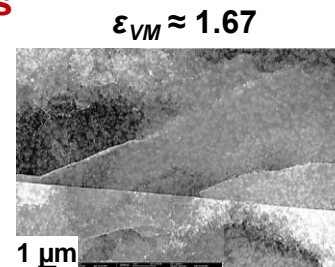
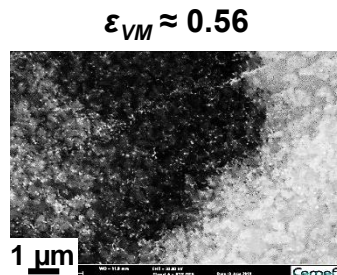


Higher dislocation density in γ fiber grains

γ fiber grains

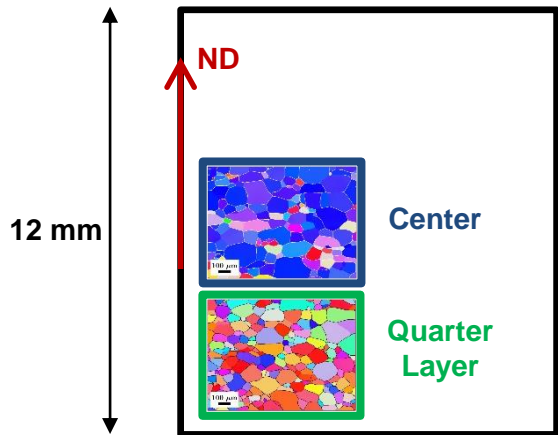


θ fiber grains

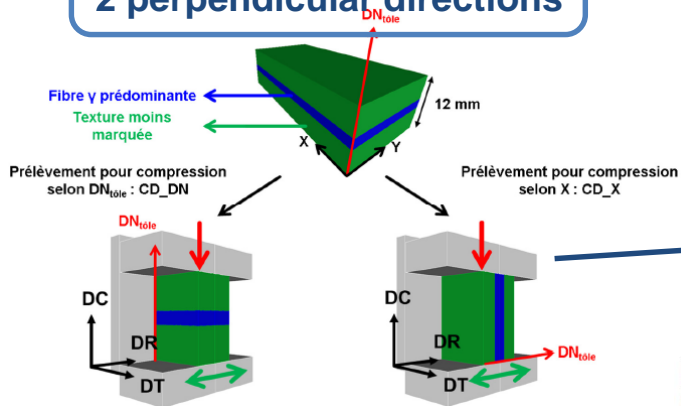


Spatial distribution of dislocation affected by crystal orientation (sub-boundaries)

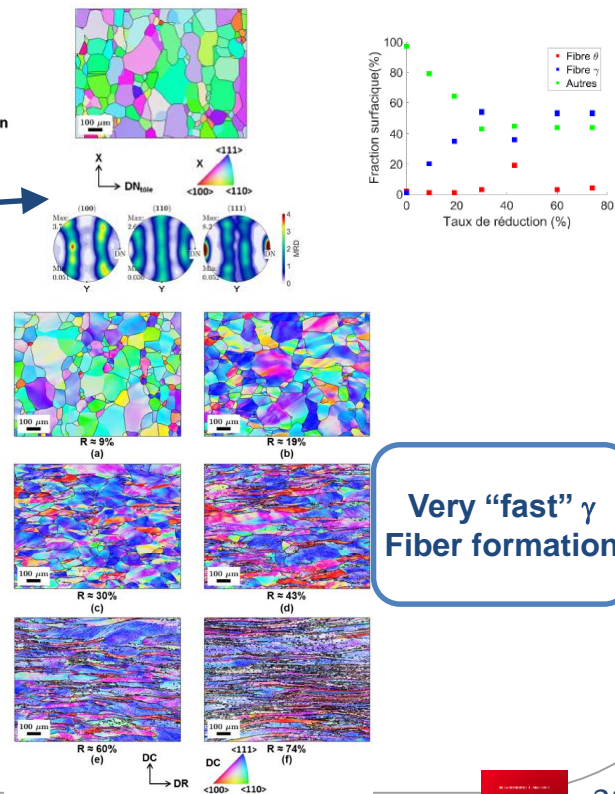
Pure Tantalum BCC



Chanel Die compression in 2 perpendicular directions

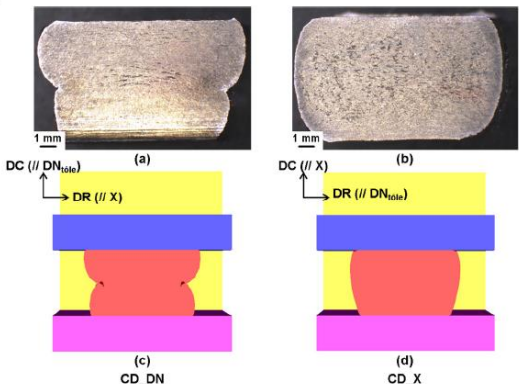


Texture evolution during channel die compression

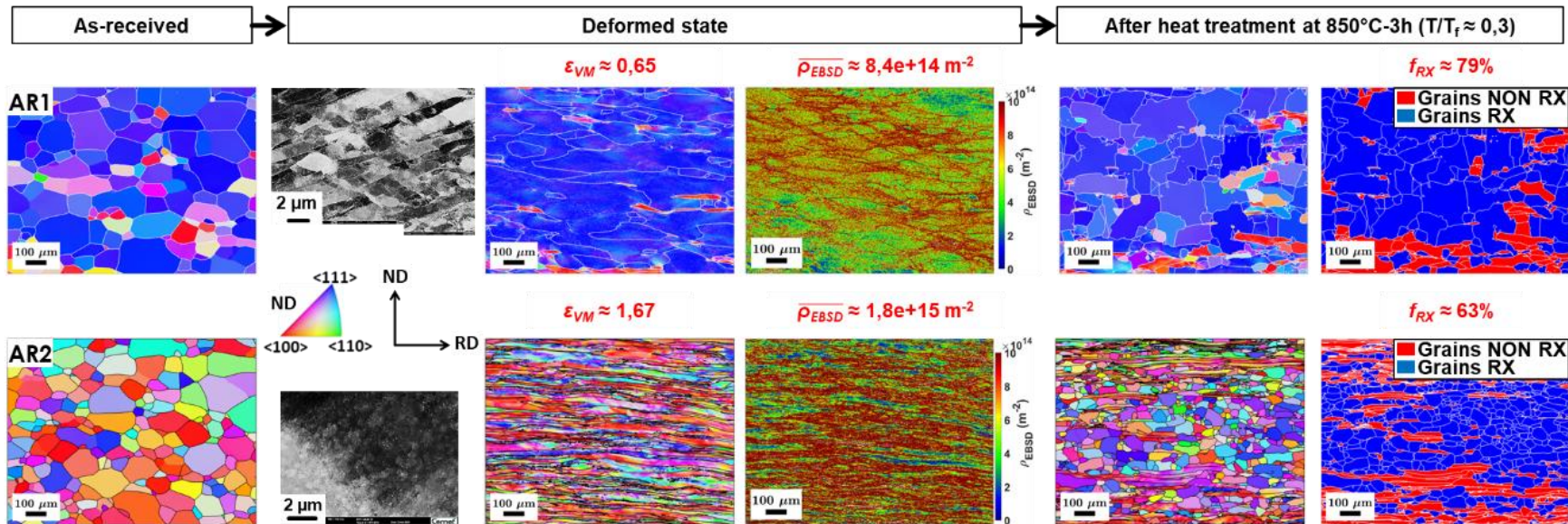


Very "fast" γ Fiber formation

γ Fiber is very stable in BCC materials
 → High mechanical resistance and small plastic deformations (not necessarily smaller dislocation density)



What does this heterogenous plastic deformation implies?



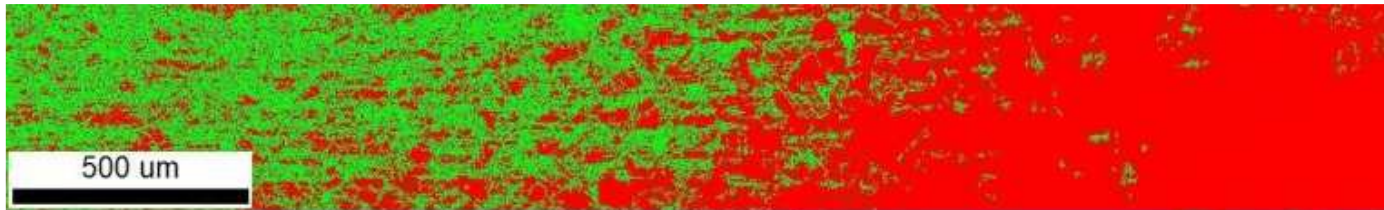
Different static recrystallization behavior → different final microstructures

TRIP effect and forming conditions

Plasticity : dislocation slip, Twinning induced plasticity and Transformation induced plasticity

In austenitic stainless steel with low Ni content like 304L (9-11%) Plastic deformation can induce by shearing the transformation

Austenite γ (FCC) \rightarrow ϵ martensite (HCP) or α' martensite (body centered tetragonal \sim BCC)



α' -martensite 

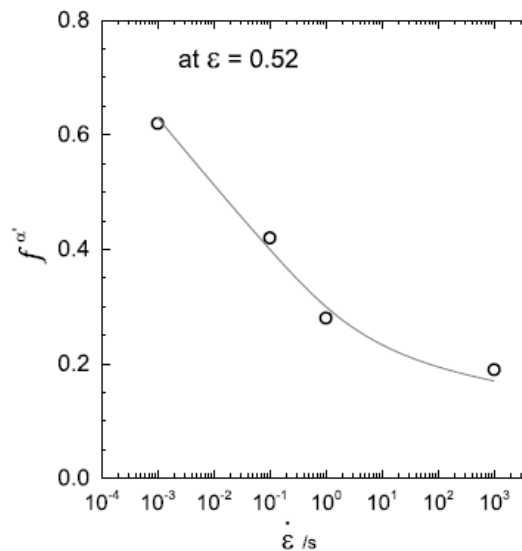
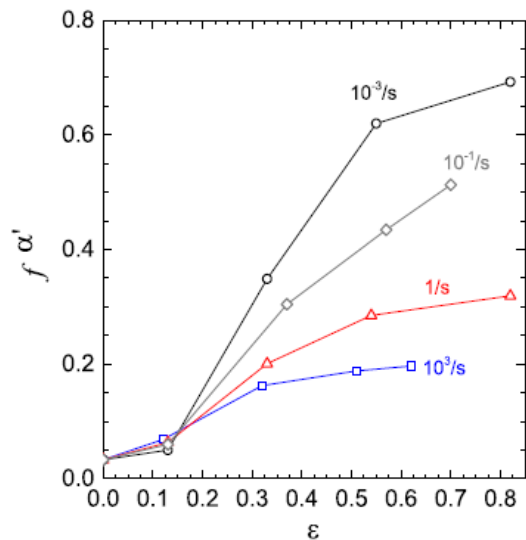
γ austenite 


 ϵ gradient

The amount of α' martensite increases with strain

TRIP effect and forming conditions

How to control it?



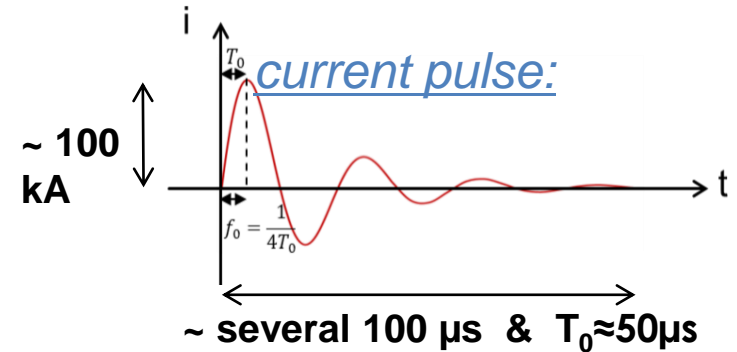
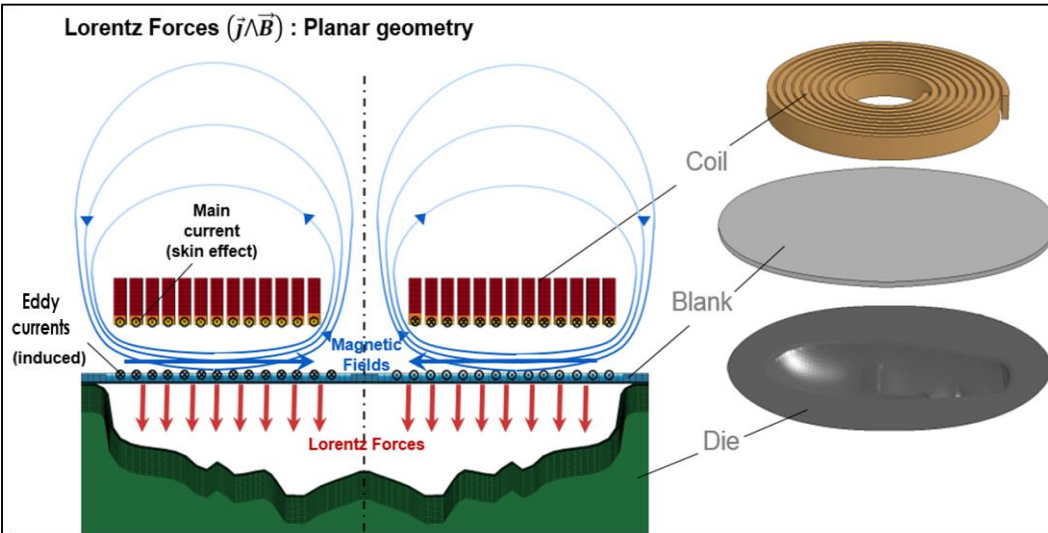
High strain rate forming processes may be a solution

↗ strain rate, ↗ T → ↘ TRIP effect and the amount of α' martensite

Magnetic Pulse Forming (MPF)

High-speed forming process that consists of generating a strong magnetic field, which rapidly changes when it passes through the coil → this changing induces Eddy currents which generates its own magnetic field to oppose the original one → the interaction between the two magnetic fields creates Lorentz forces that deform the metallic material

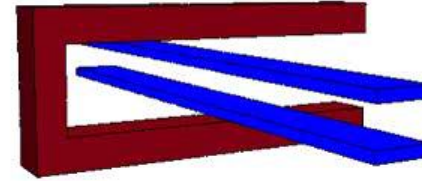
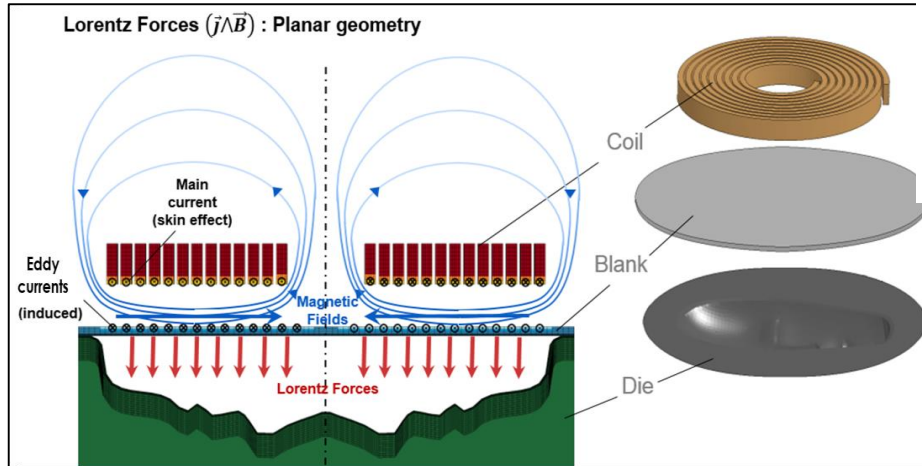
Lorentz Forces ($\vec{j} \wedge \vec{B}$) : Planar geometry



Particularities: No contact, reduces springback and very high strain rate ($\sim 10^3 \text{s}^{-1}$)

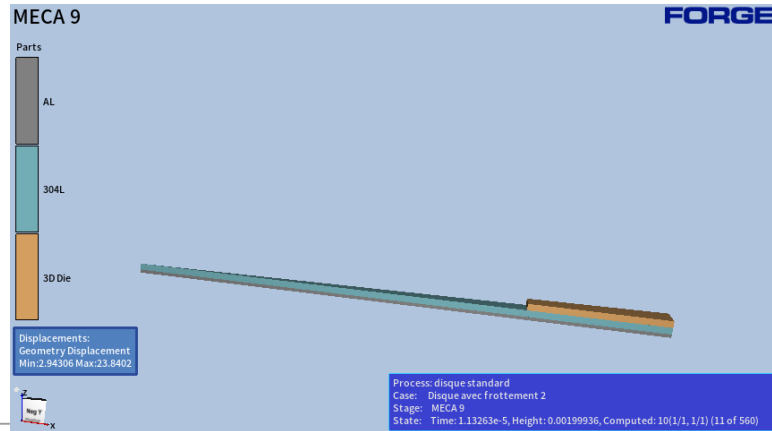
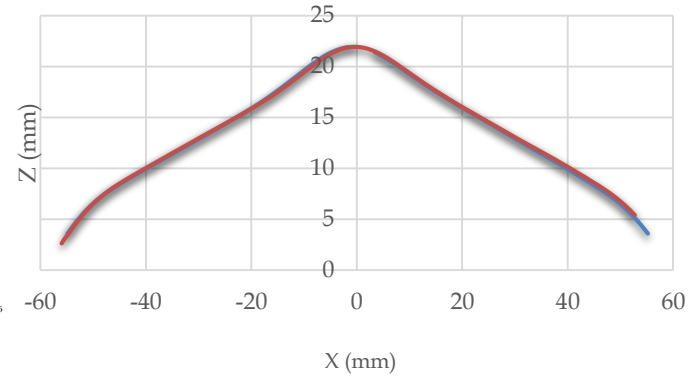
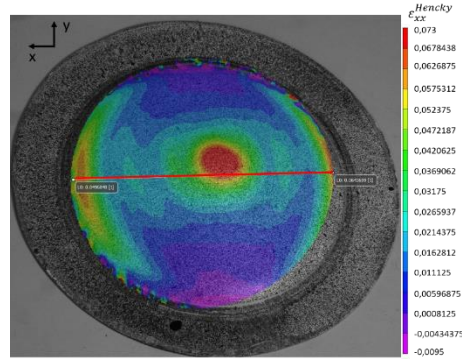
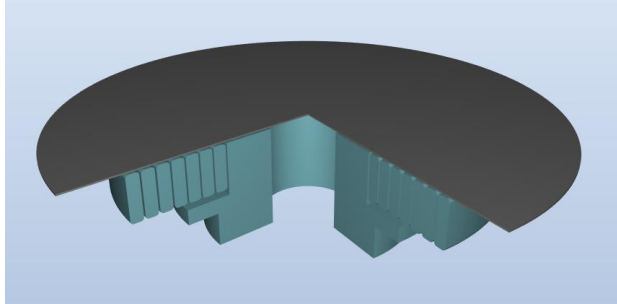
Magnetic Pulse Forming (MPF)

Opportunities for cold welding



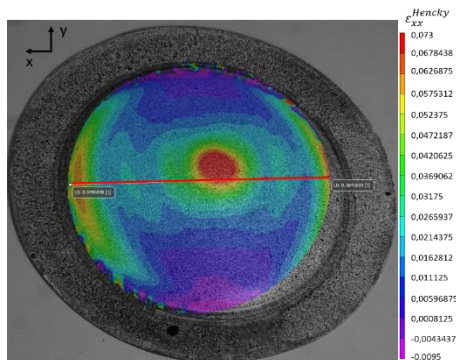
Zittel, a historical review of high speed metal forming, 2010

Magnetic Pulse Forming (MPF) application on 304L steel to reduce TRIP effect



$$\dot{\epsilon} \approx 10^4 s^{-1}$$

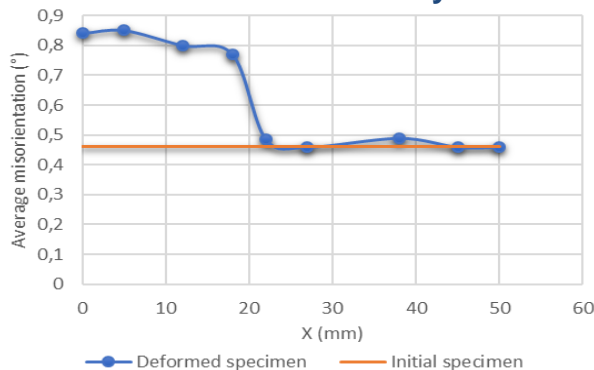
Magnetic Pulse Forming (MPF) application on 304L steel to reduce TRIP effect



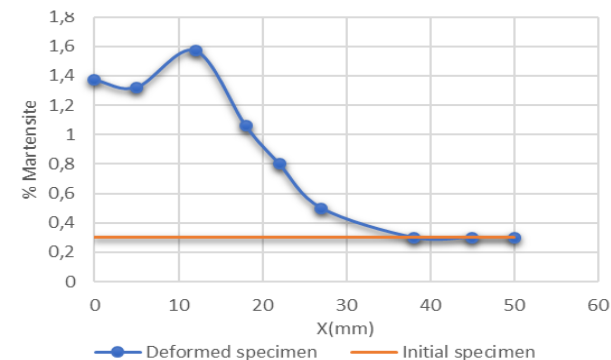
Early stages of transformation



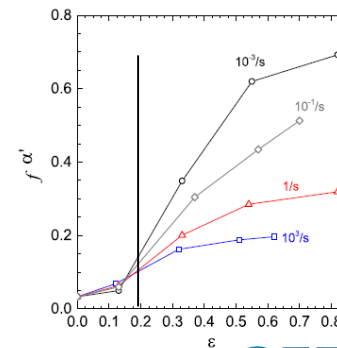
Intragranular disorientations ~ dislocation density



% of martensite



Compared to literature for similar plastic strains, smaller amount of martensite is obtained (1.5% vs 5%)



Dynamic recrystallization occurs during hot deformation

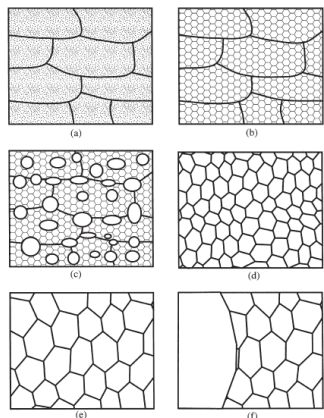
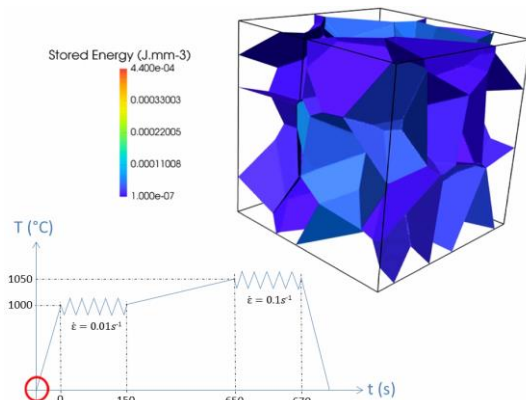
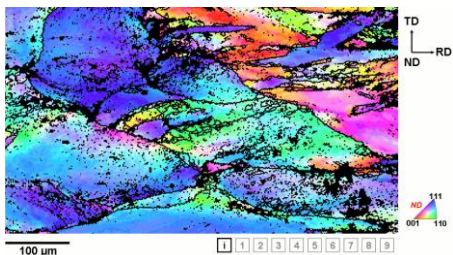


Fig. 1.1. Schematic diagram of the main annealing processes: (a) Deformed state, (b) Recovered, (c) Partially recrystallized, (d) Fully recrystallized, (e) Grain growth and (f) Abnormal grain growth.

Humphreys et Hatherly, Recrystallization and related annealing phenomena, 2nd edition, 2004.



Maire PhD, Mines Paris, 2018

Highly sensitive to T and $\dot{\epsilon}$
Defines the final grain size

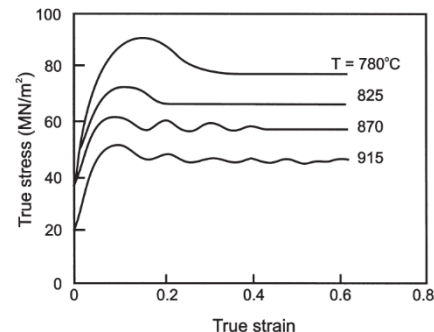


Fig. 13.12. The effect of temperature on the stress-strain curves for 0.68%C steel, deformed in axisymmetric compression, $\dot{\epsilon} = 1.3 \times 10^{-3} \text{ s}^{-1}$, (Petkovic et al. 1975).

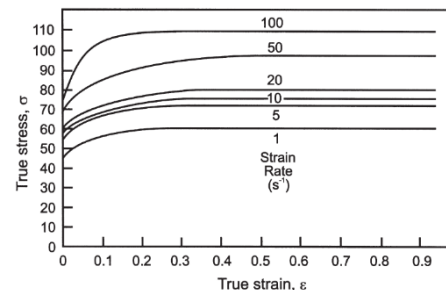


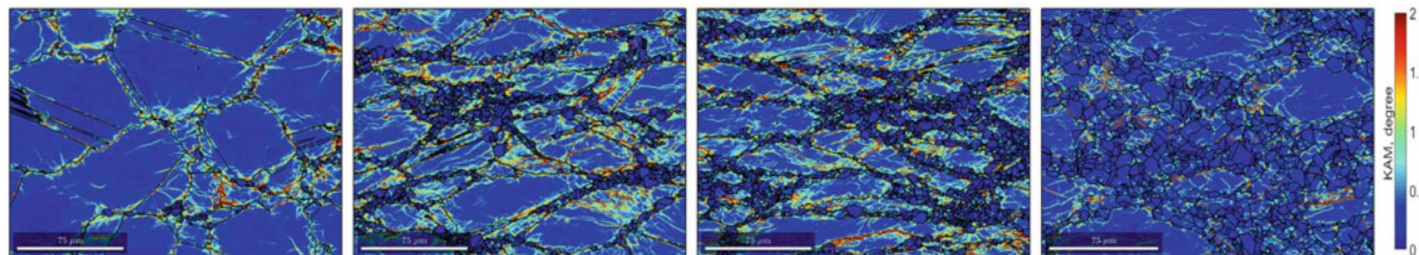
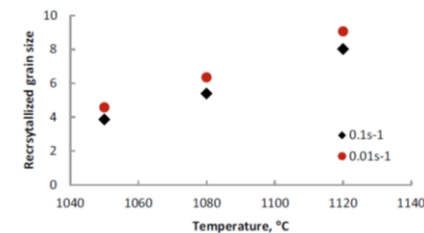
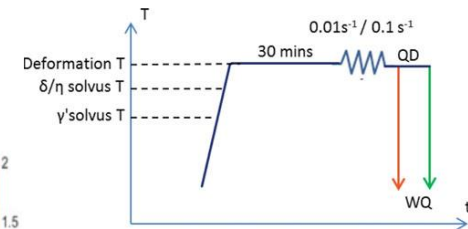
Fig. 13.1. Stress-strain curves for Al-1%Mg at 400°C, (Puchi et al. 1988)

High T
low $\dot{\epsilon}$
High SFE



Low T
high $\dot{\epsilon}$
High SFE

Dynamic recrystallization occurs during hot deformation: Application to VDM780 Nickel base superalloy

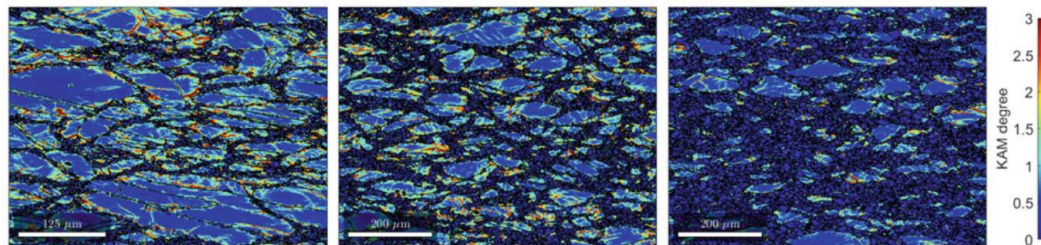
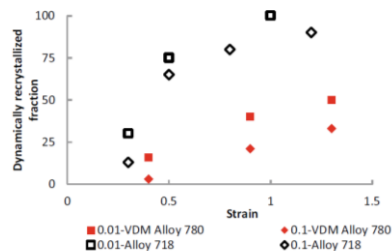


(a) $\epsilon = 0.4$ at 0.1 s^{-1}
 $f_r = 3 \%$ $D_r = 5 \mu\text{m}$

(b) $\epsilon = 0.9$ at 0.1 s^{-1}
 $f_r = 21 \%$ $D_r = 5 \mu\text{m}$

(c) $\epsilon = 1.3$ at 0.1 s^{-1}
 $f_r = 33 \%$ $D_r = 4 \mu\text{m}$

(d) $\epsilon = 1.3$ at 0.01 s^{-1}
 $f_r = 50 \%$ $D_r = 6 \mu\text{m}$

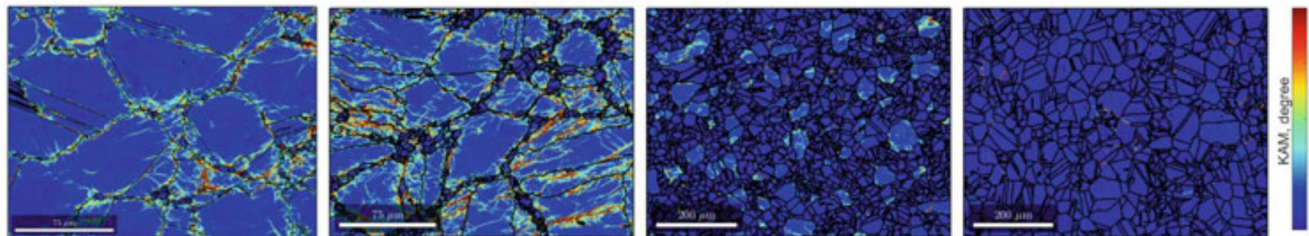
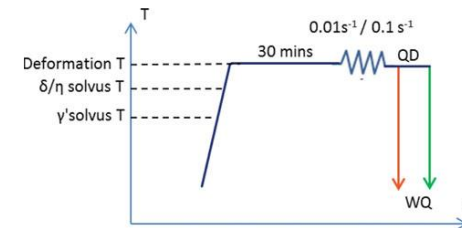


(a) $T = 1050 \text{ }^\circ\text{C}$

(b) $T = 1080 \text{ }^\circ\text{C}$

(c) $T = 1120 \text{ }^\circ\text{C}$

Post dynamic recrystallization occurs after dynamic recrystallization (Meta or static recrystallization): Application to VDM780 Nickel base superalloy



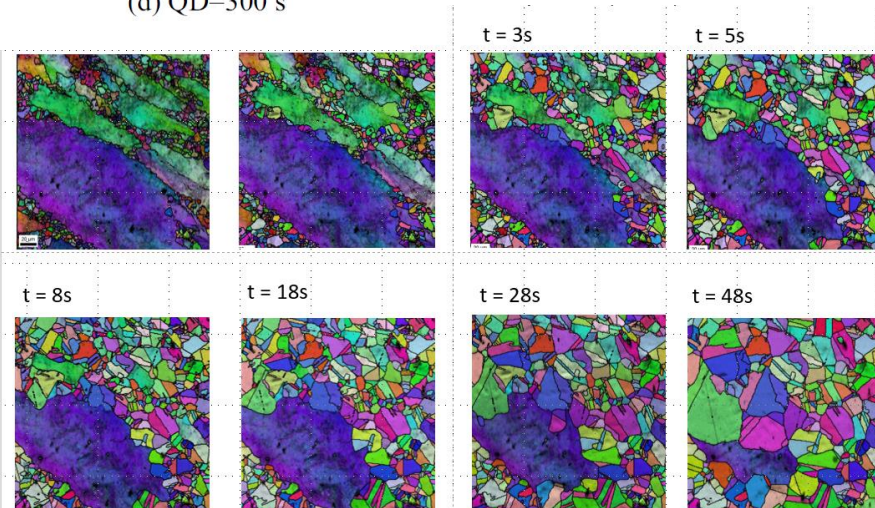
(a) QD=3 s

(b) QD=6 s

(c) QD=30 s

(d) QD=300 s

Very fast post dynamic recrystallization in unstable transient partially recrystallized microstructures



Heterogeneous thermo-mechanical conditions → heterogeneous microstructure:

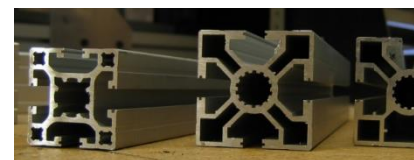
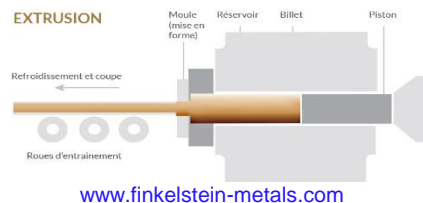
Application to Extrusion of Inconel 718

Difficulties:

- Tool design difficulties
- Tool manufacturing cost
- Time required for die development through successive trials (including simulations) to achieve dimensional tolerances and to eliminate various geometric defects
- Die Lifespan
- Tool kinematics
- Tool – material contact conditions

Advantages:

- Material savings
- Hot or cold, solid or hollow parts
- Robust tools and powerful presses
- High geometric accuracy without machining
- Satisfactory surface finish
- Work hardened material



Wikipedia, Extrusion, 2020



Courtesy of E. Felder

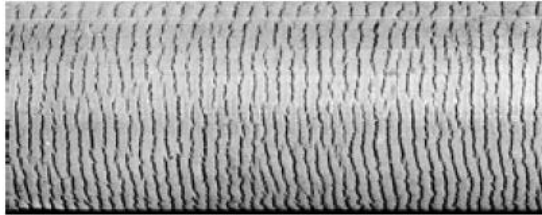
Catégorie	Section type	Exemple	Nature
A	barre simple		ouvert
B	barre complexe		
C	profilé standard		
D	profilé ouvert simple		
E	profilé semi-tubulaire		
F	profilé avec variation brutale de section et des parties fines et élancées		
G	profilé avec languettes difficiles et entrées très étroites		tubulaire
H	tubes		
J	profilés tubulaires simples		
K	profilés tubulaires avec au moins deux rétreints internes		
L	tubes avec détails externes		tubulaire
M	tubes avec détails internes ou type K-L		
N	profilés tubulaires de grande taille ou très large		

Heterogenous plastic flow associated with heterogeneous microstructure → Defects

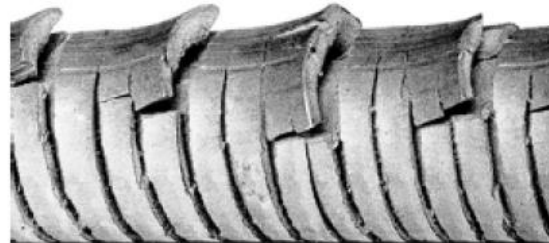


Cracks in the core and at the surface

Figure 32 : Défauts internes (chevrons) sur barres d'acier filées à froid (*Central bursting defect*)



a) Vitesse ou température faible



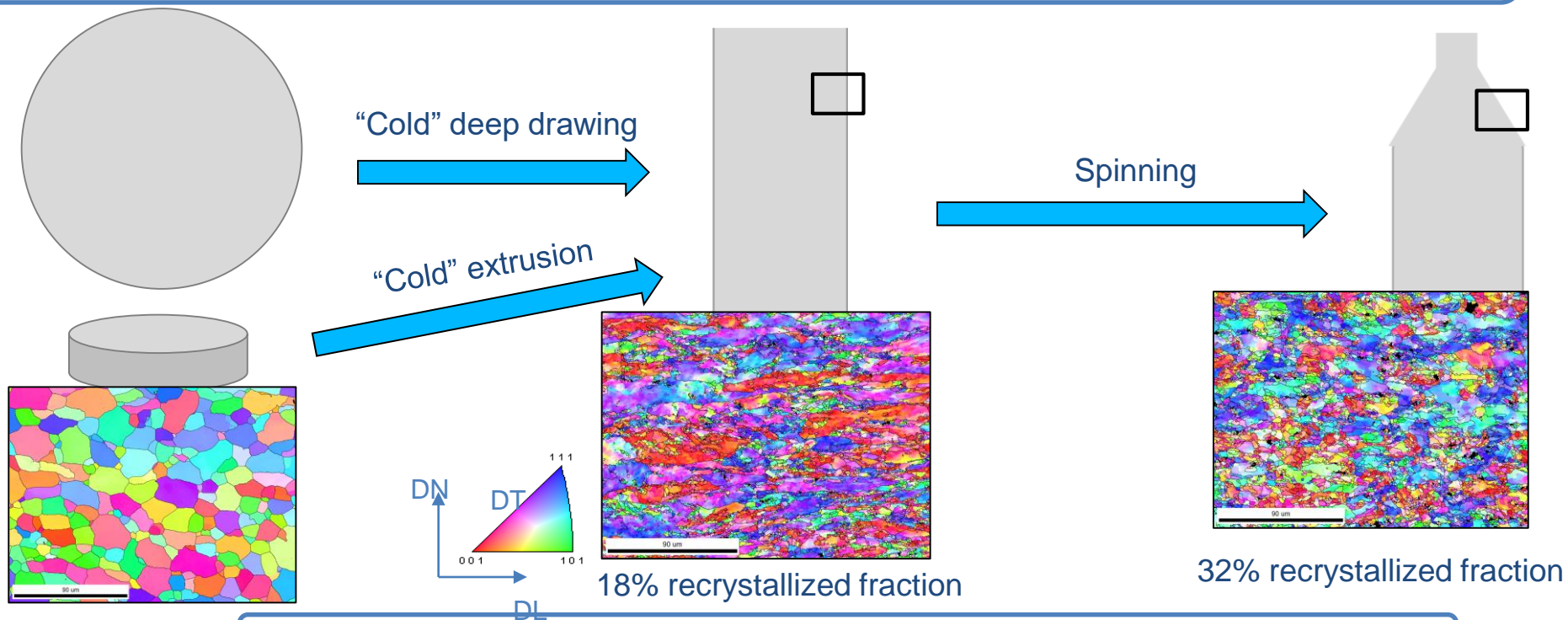
b) Vitesse ou température élevée



a) Filage avant

Thermally activated mechanisms during hot forming? What about cold forming?

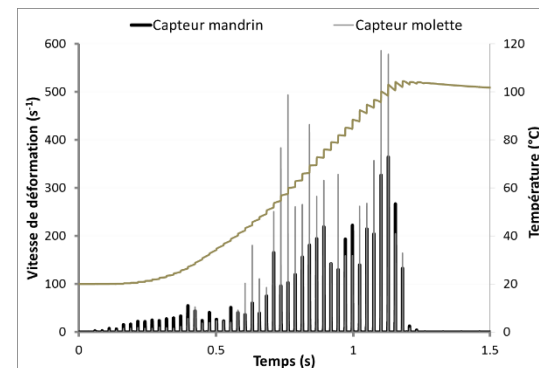
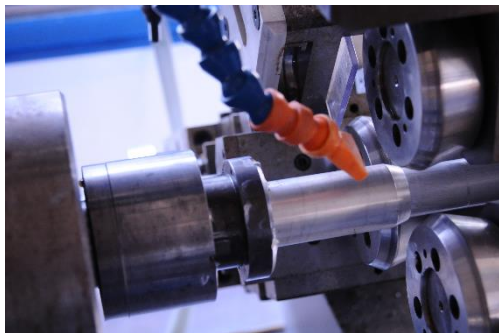
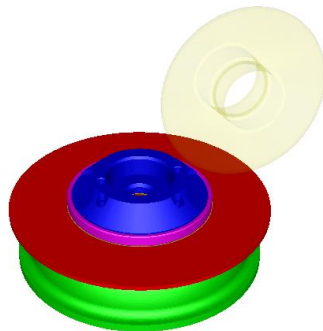
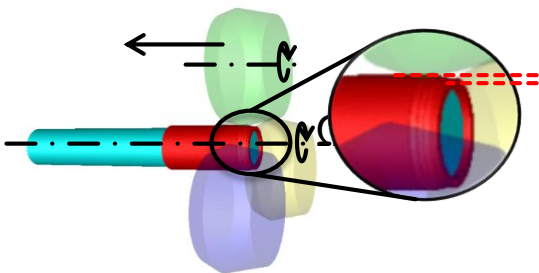
Application to deep drawing, extrusion and spinning of aluminum alloy 1050



Thermally activated mechanisms can be activated during “cold” forming

Thermally activated mechanisms during hot forming? What about cold forming?

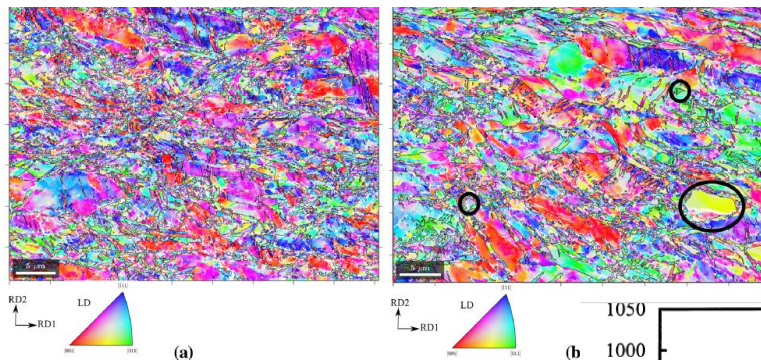
Application to flowforming of Inconel 718



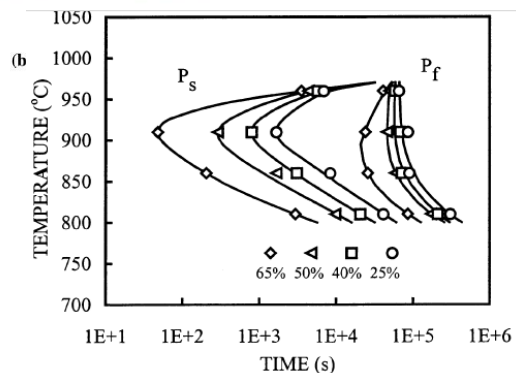
- Very high speed incremental deformation
- Mainly compressive triaxiality
- Very high strains (up to 8) and strain rates (up to 100s⁻¹)

Thermally activated mechanisms during hot forming? What about cold forming?

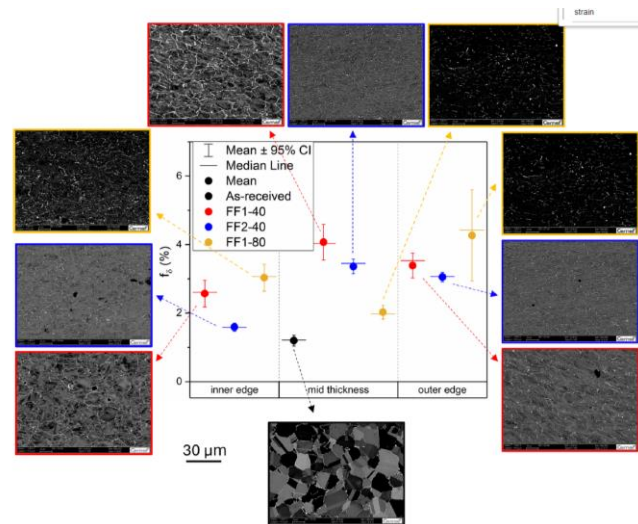
Application to flowforming of Inconel 718



Activated recrystallization



Liu et al., Met. Trans, 1997

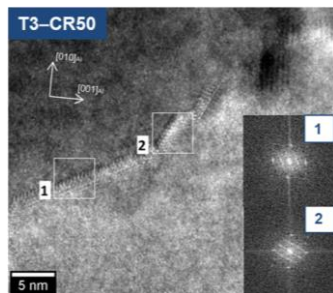


Activated δ phase transformation

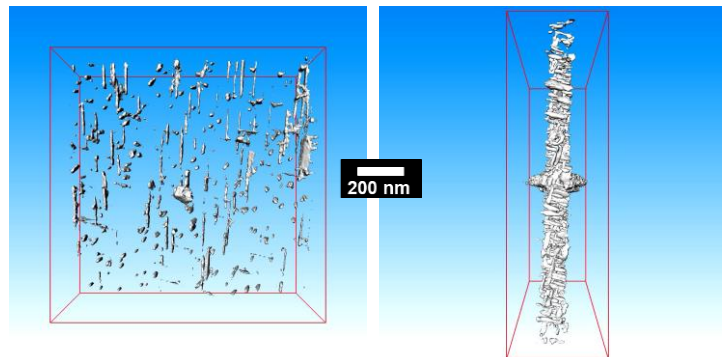
In addition to activating of thermally activated mechanisms, the kinetics are extremely accelerated

interactions between several physical mechanism

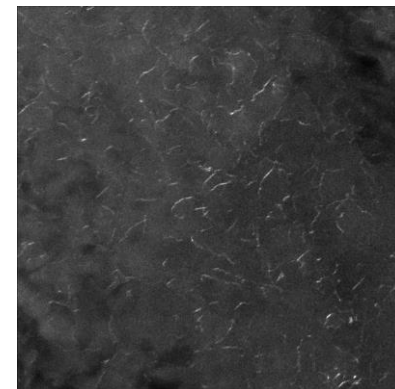
Application to AA 2024 coupling between plasticity and precipitation



S phase precipitation on dislocation lines:
Heterogeneous precipitation

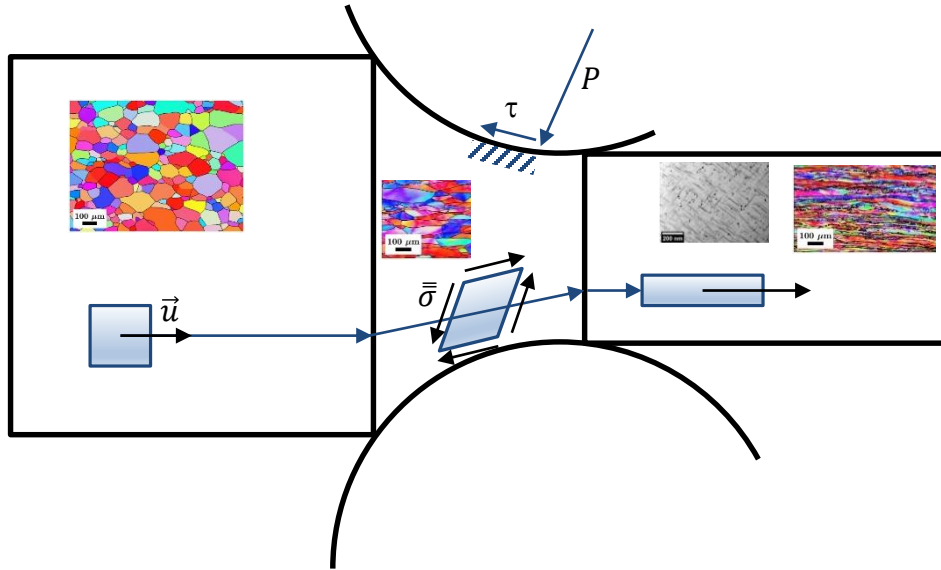


Homogeneous distribution of precipitates



Nucleation, growth and coalescence on dislocation lines

All the physical mechanisms interact, with increasing the materials forming complexity, understating and modelling microstructural evolutions increases → Future challenges



Material flow
Forces involved in the forming process
→ final shape of the product
Plasticity, ductility, damage ...

Heat flow
→ T evolution
Adiabatic heating, radiation, convection...

- Determines the energies involved in the forming process
→ various internal and surface defects (cracks, porosities, wrinkles orange peel effect...)
→ microstructure evolution (phases, grain size and shape, crystallographic texture, dislocations density...)
→ mechanical properties of the product, residual stresses...

Thermomechanical interactions material – lubricant – tools

→ surface state

Mechanical stresses (friction shear and contact pressure) and thermal stresses → modifies deformation conditions and tools wear

Lubricant → reduces those effects

Tool deformation → alteration of final dimensions

Thermal conduction, friction → T evolution

Microstructural evolution

Plasticity, recovery, recrystallization and phase transformation (diffusive and displacive)

→ Phases (volume fraction, size and shape), grain size and shape, crystallographic texture, dislocations density and sub-structures...),

→ Mechanical properties of the product, residual stresses...



Thank you for your attention

charbel.moussa@minesparis.psl.eu