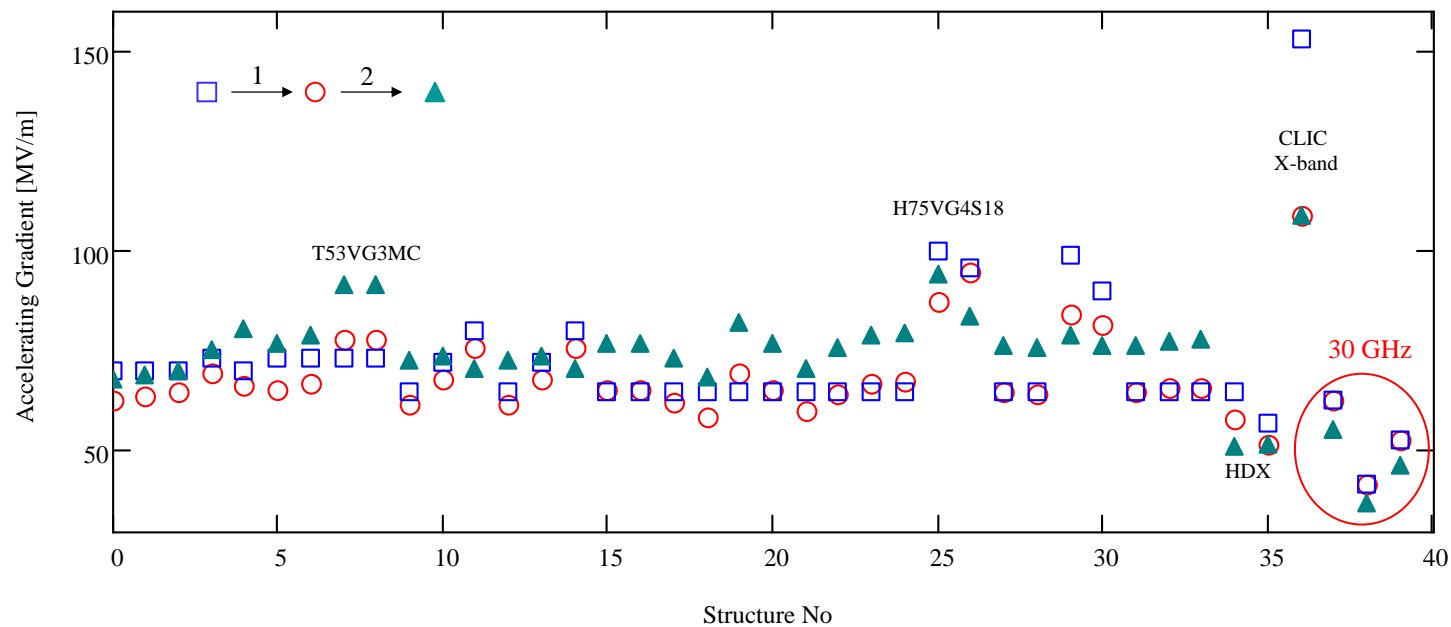


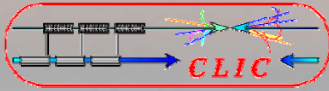
## Analysis of available data on measured X-band and 30 GHz accelerating structures

For the moment, use only copper accelerating structures (no PETS, No other materials)

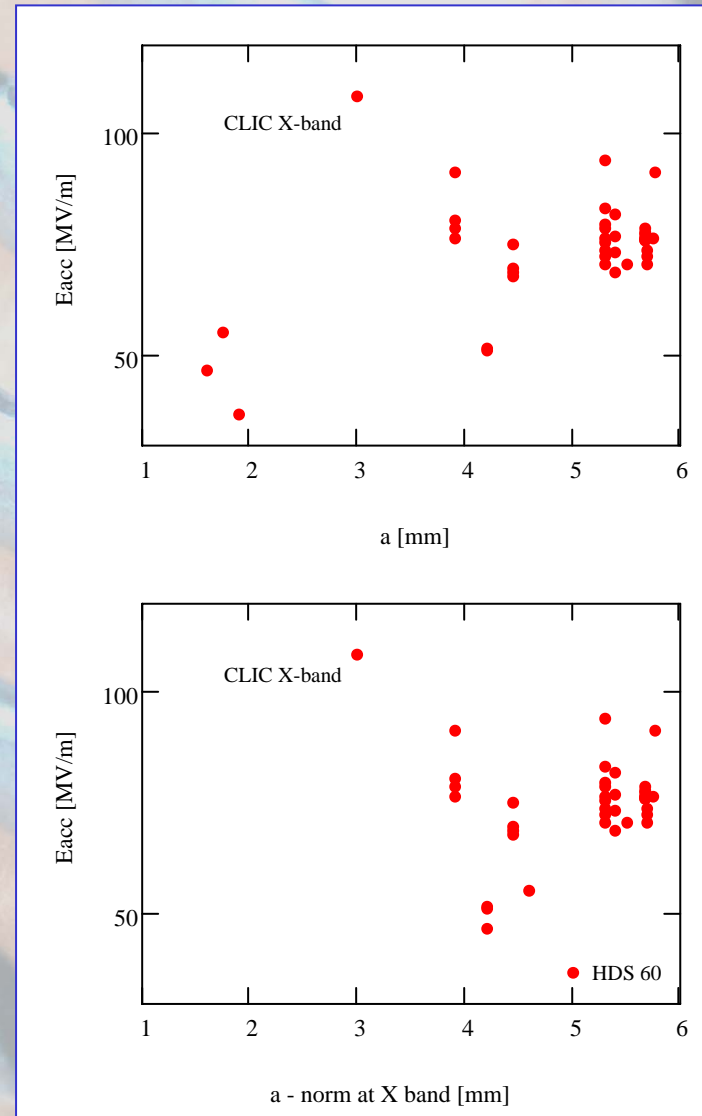
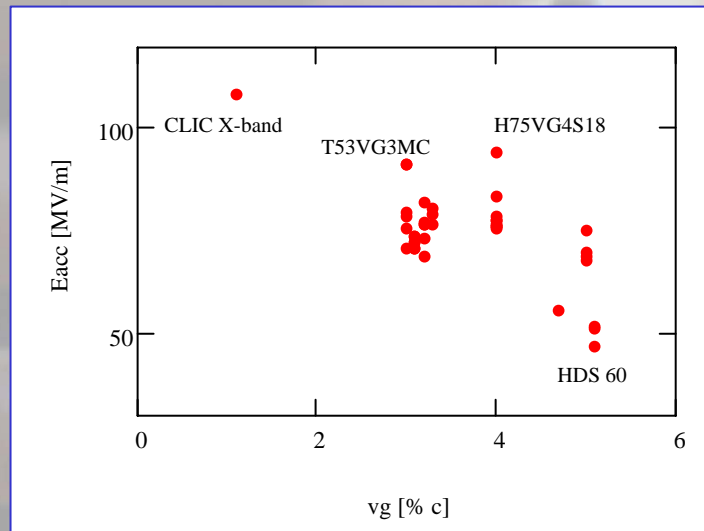
Normalization of measured gradient

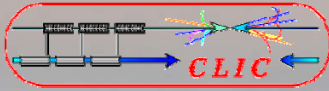
1. Normalize to 10<sup>-6</sup> (assume “typical” copper slope, relative)
2. Normalize to pulse length (use 150 ns as “standard”)



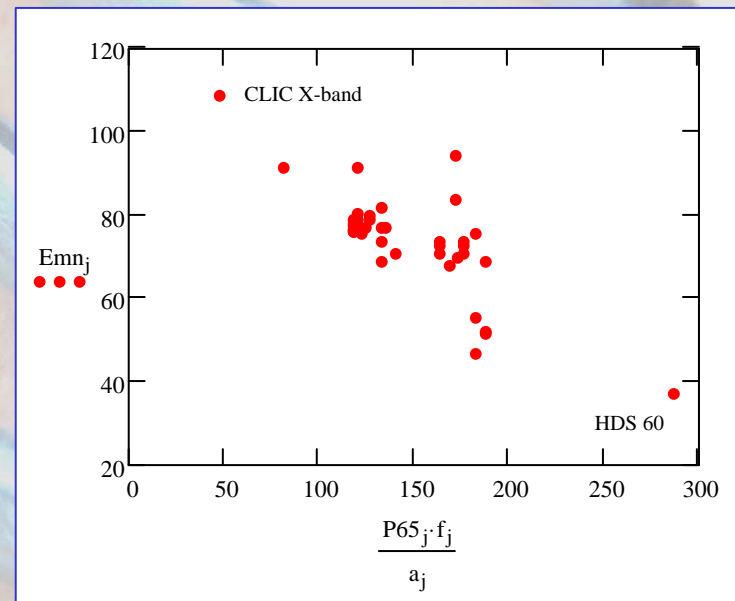
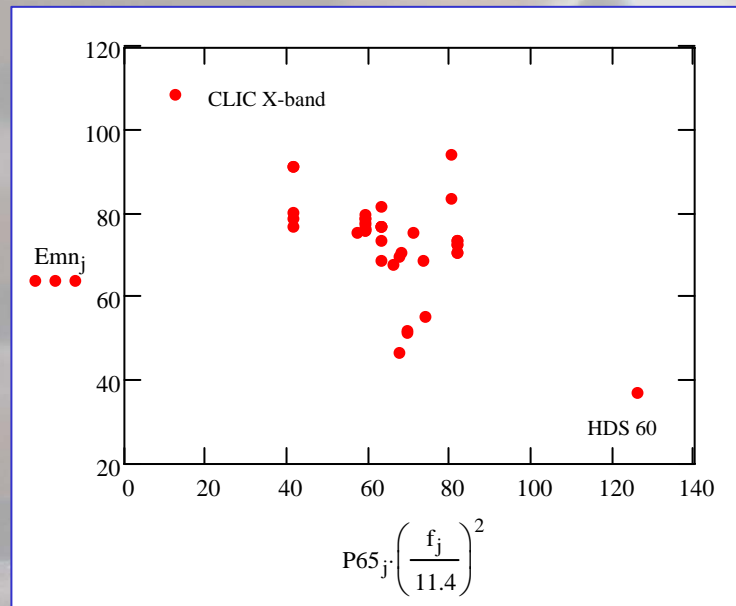


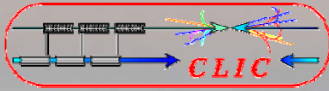
## Correlation plots





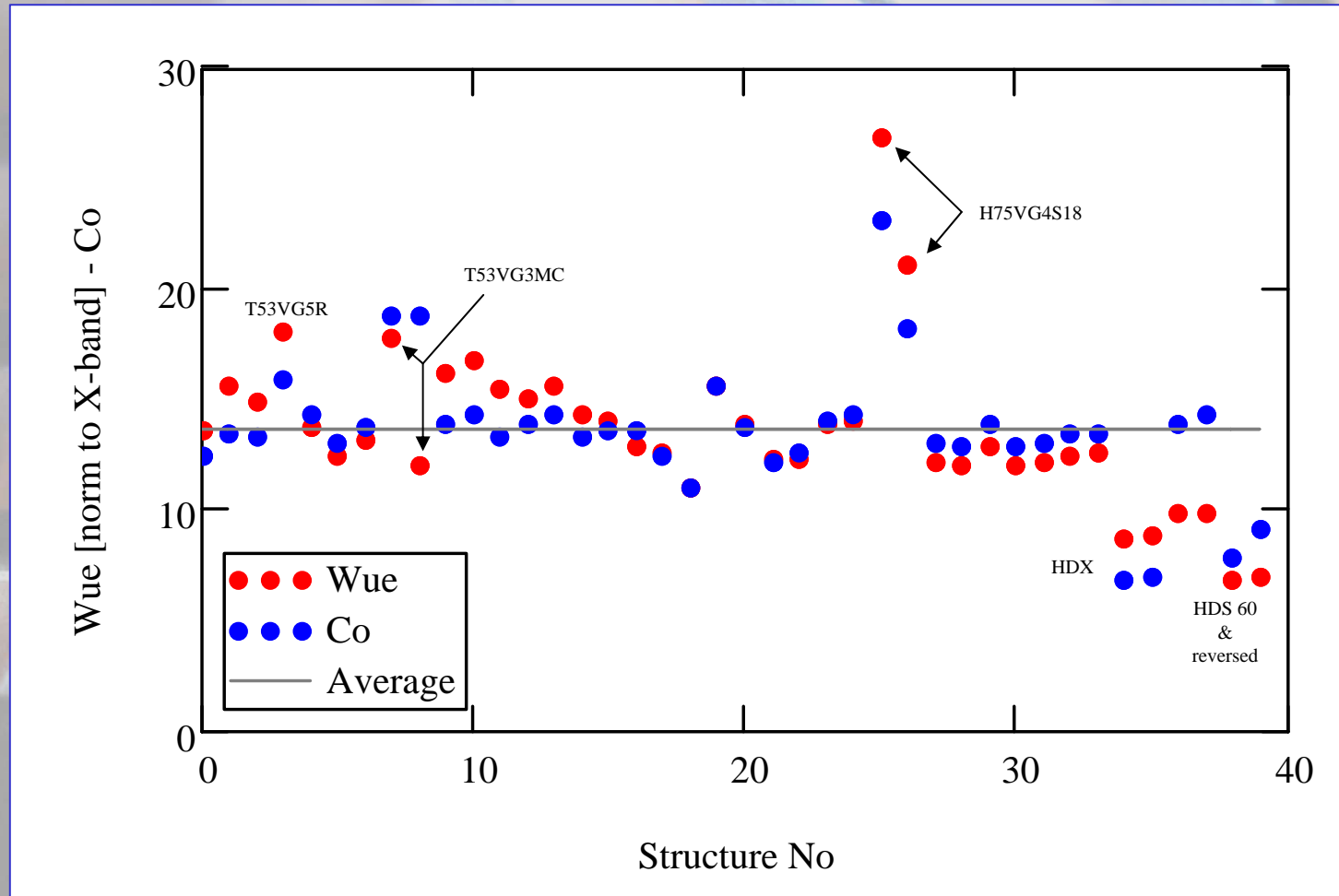
### Correlation plots

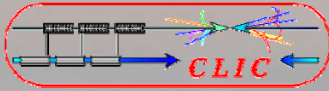




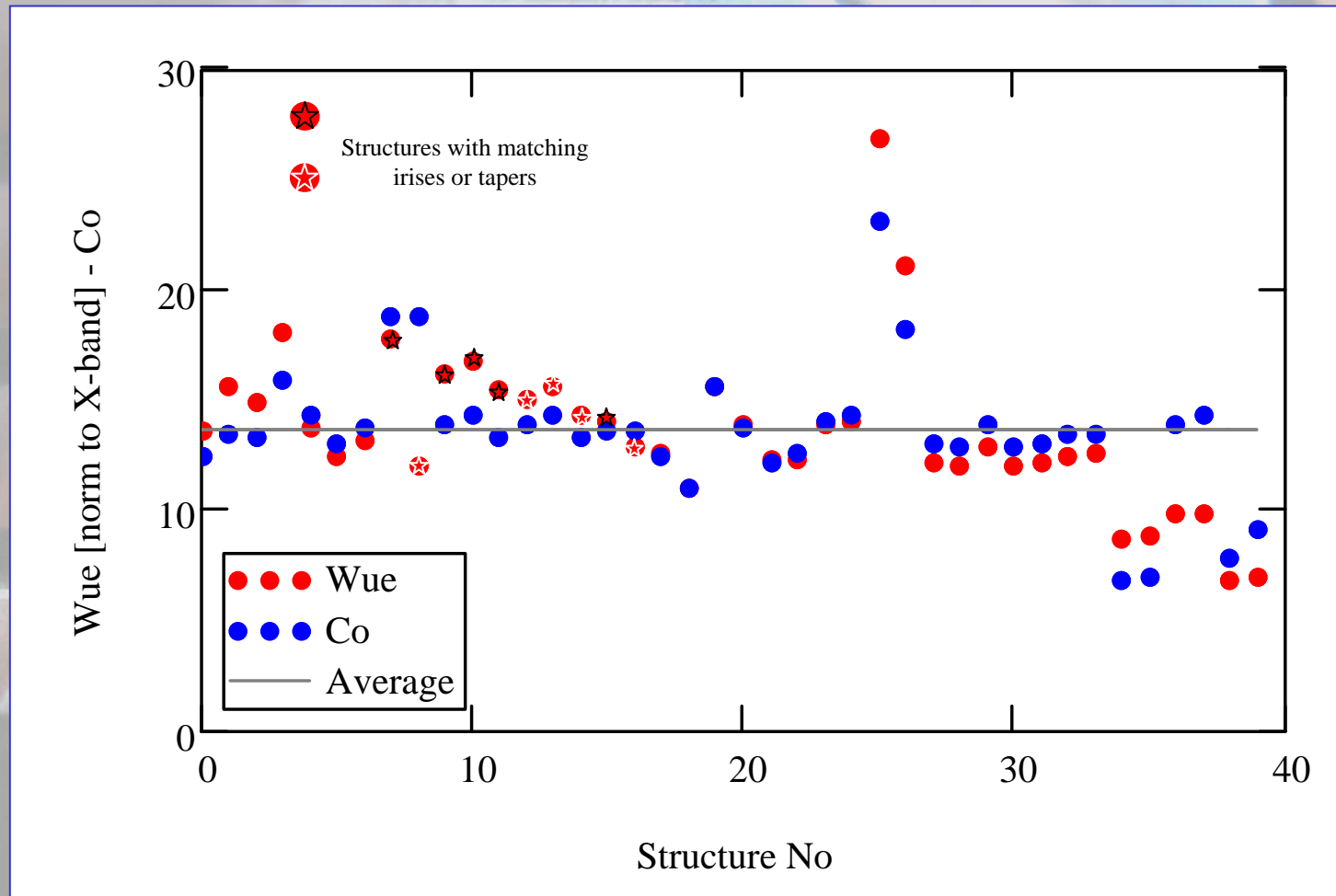
Wuenshes & Corsinis

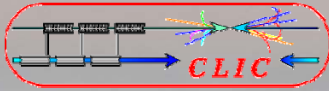
$$Co = \frac{(E_{acc})^2 \cdot (v_g)^{0.1} \cdot (f)^{1.5} \cdot (P65)^{0.5}}{\left( \frac{\phi \sin(\phi) + 2 \cdot v_g \cdot \cos(\phi)}{\sin(\phi)} \right)^{0.1}}$$



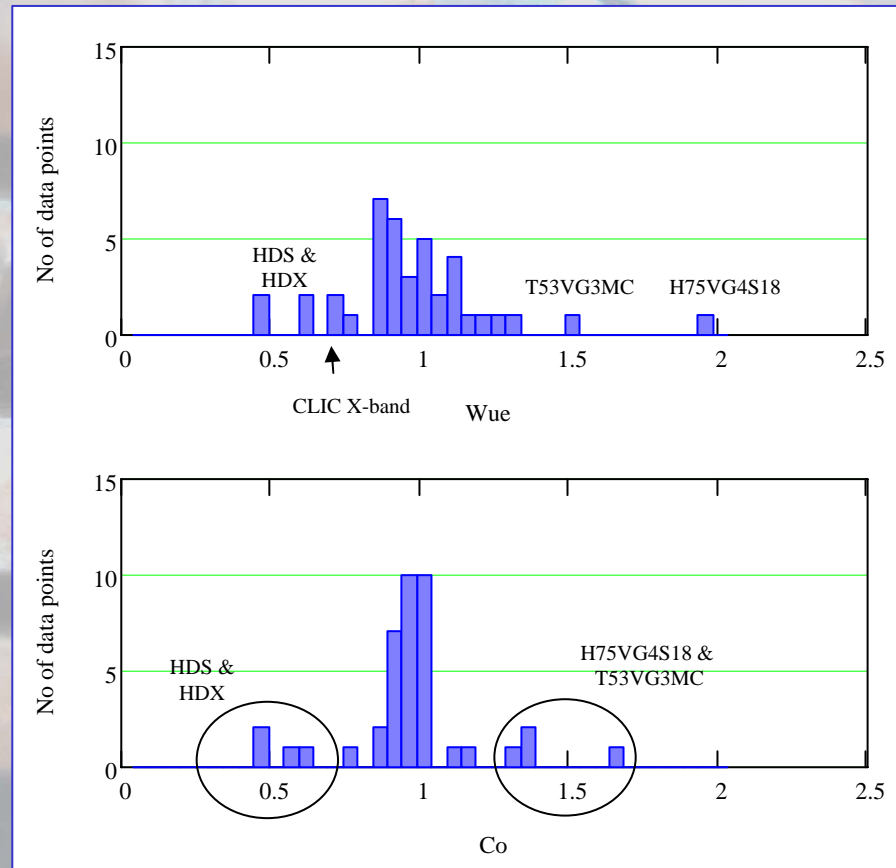


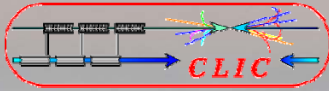
Wuenshes & Corsinis



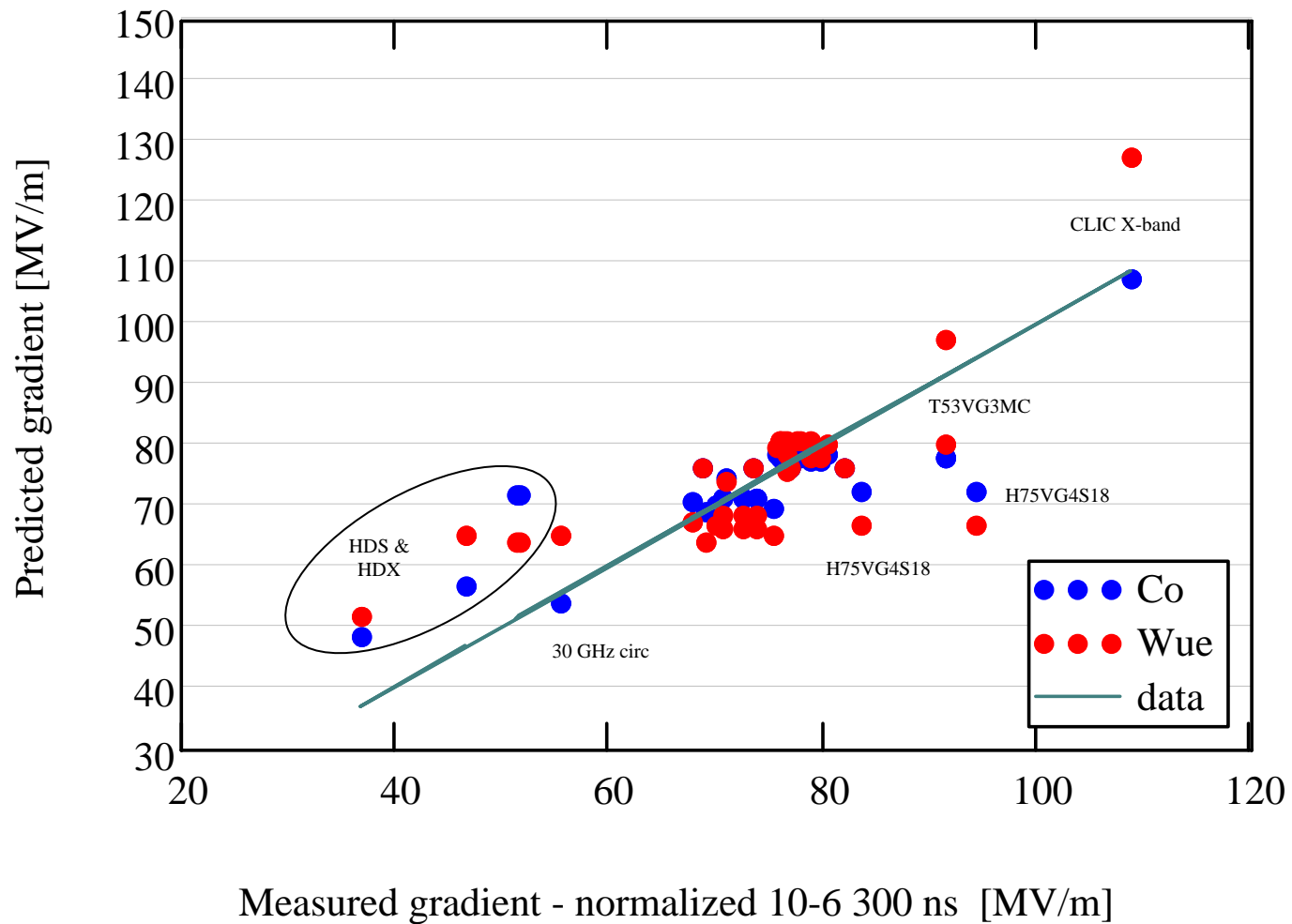


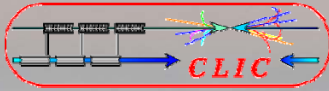
*Wuenshes & Corsinis*





*Wuenshes & Corsinis – predictive power*





## Chris' damage potential & scalings

Effective Impedance

$$Z_s \approx 2 \frac{R/Q}{k \sin(\phi)} \approx \frac{R/Q}{v_g} \frac{\phi \sin(\phi) + 2 v_g \cos(\phi)}{\sin(\phi)}$$

Power Absorbed in an Arc

$$\text{Power}_{\text{abs}} \approx 4 \frac{R_{\text{arc}}}{Z_s} \text{Power}_{\text{inc}} \approx \frac{R_{\text{arc}}}{(R/Q)^2} \frac{v_g^2}{\omega/c} \frac{4 \sin(\phi) \text{ Gradient}^2}{\phi \sin(\phi) + 2 v_g \cos(\phi)}$$

Different scaling – still miss R/Q data to test, but not very promising

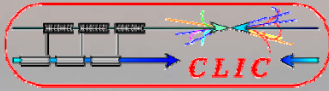
If Breakdown is Modeled as a Load Impedance,  
Power Absorbed in the Load Scales as

$$\frac{v_g^2}{(R/Q)^2} \frac{\sin(\phi)}{\phi \sin(\phi) + 2 v_g \cos(\phi)} \text{ Gradient}^2$$

where  $v_g$  = Group Velocity/c     $R$  = Shunt Impedance  
 $Q$  = Quality Factor     $\phi$  = Phase Advance

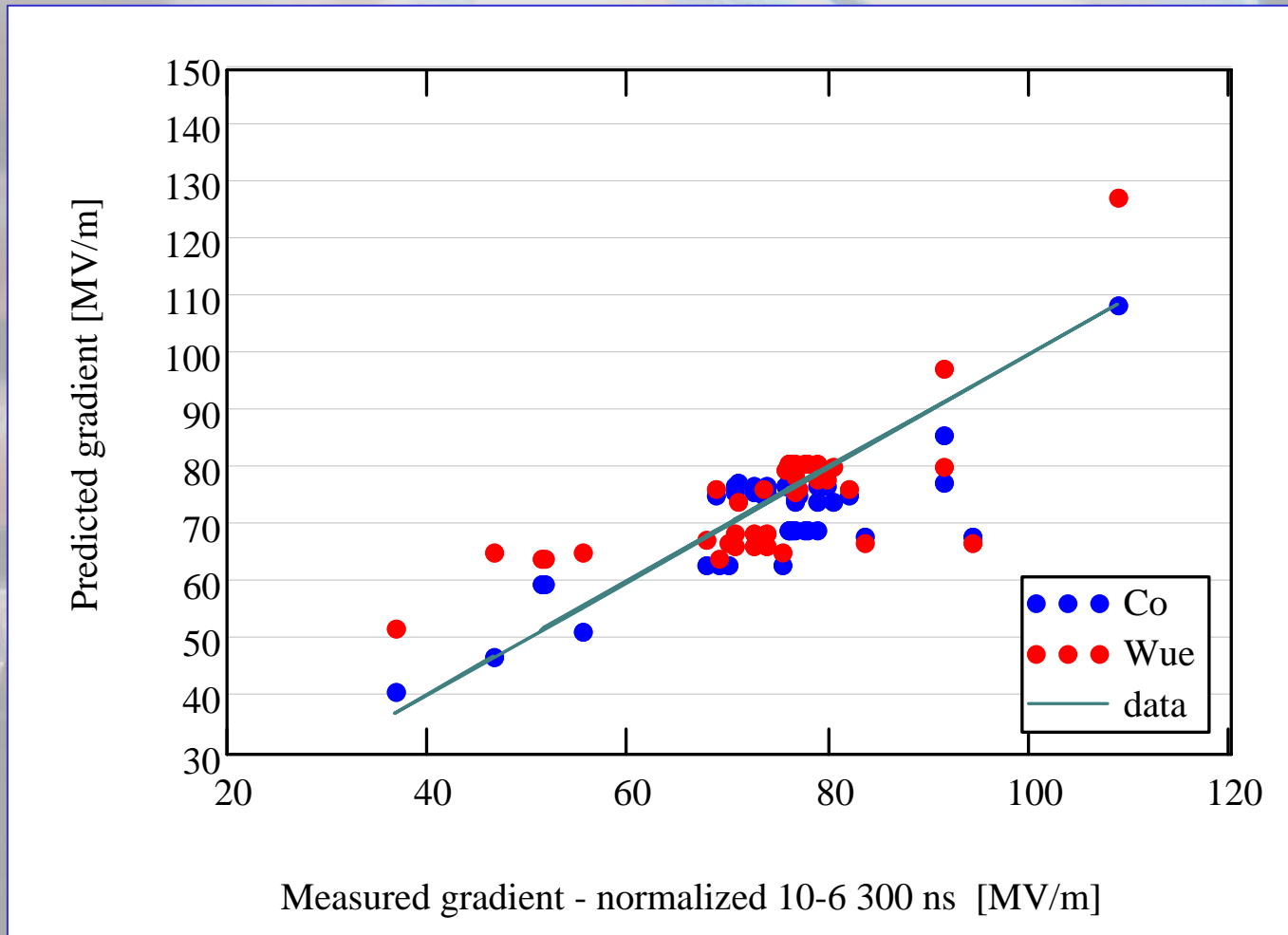


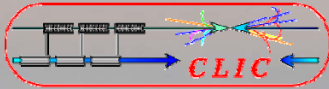




Another Corsini definition

$$Co = \frac{\left[ (E_{acc})^2 \cdot (v_g)^{0.75} \cdot (\phi)^{0.1} \right]}{(a)^{0.5}}$$





...to cut or not to cut...

