

Windows for final cooling

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MuCol



Introduction







Final Cooling

- \Box Absorber \rightarrow H₂ best candidate
- □ For liquid/gas absorber → Vacuum windows are required
 □ Windows may be required even for solids (thermal desorption)

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 \Box Low energy \rightarrow Thin windows

Stage [N]	P [MeV/c]	Energy spread σ_E [MeV]	LH ₂ thickness [cm]	Drift length [m]	rf length [m]	rf frequency [MHz]	Field flig
1	135.0	2.29	65	0.434	2.25	325	Yes
2	130.0	2.48	60	0.459	2.25	250	Yes
3	129.0	2.78	60	0.450	2.5	220	No
4	129.0	3.10	59	0.458	2.5	201	No
5	122.0	3.60	57	1.629	5.0	201	Yes
6	124.0	4.90	53	2.22	4.5	180	No
7	116.0	3.40	42	2.21	3.25	150	No
8	111.0	3.90	40	2.0	3.5	150	No
9	106.0	3.50	40	3.13	5.0	125	Yes
10	98.0	3.07	35	3.13	5.0	120	No
11	89.4	3.11	20	3.12	5.0	110	No
12	87.9	2.76	20	3.1	8.0	100	No
13	85.9	2.67	20	3.0	7.5	100	Yes
14	79.7	3.08	15	2.7	7.0	70	No
15	71.1	4.0	15	2.6	6.0	50	No
16	71.0	3.80	13	2.5	6.0	20	No
17	70.0	3.80	10			20	



Parameters: > 20 to 5 MeV cooling > 4e12 muons/pulse > 5 Hz repetition rate > $\sigma_{RMS}=0.6 \text{ mm}$





Final Cooling



\Box At 5 MeV \rightarrow Be range <1.5 mm [3]

□ Conventional windows typical at CERN 0.254 mm >15% muon range



Thin windows

- Possible materials:
 Be, Si₃N₄, C, SiC, etc.?
- To limit beam perturbation <15µm (approx. <1% of power absorbed in the window for 3keV/µm)
- Thin window \rightarrow Small window \rightarrow 10× $\sigma_{\rm RMS}$

$$\left\langle -\frac{dE}{dx}\right\rangle_{\text{electronic}} = K\frac{Z}{A}\frac{1}{\beta^2} \left[\frac{1}{2}\ln\frac{2m_e c^2 \beta^2 \gamma^2 Q_{\text{max}}}{I^2} - \beta^2 - \frac{\delta}{2} + \frac{1}{8}\frac{Q_{\text{max}}^2}{\left(\gamma M c^2\right)^2} \right] + \Delta \left| \frac{dE}{dx} \right|$$

		5 MeV	20 MeV
Po	Stopping power [MeV×cm²/g]	11.2	4.0
ве	Linear stopping power [keV/µm]	2.1	0.7
C	Stopping power [MeV×cm²/g]	12.2	4.3
L	Linear stopping power [keV/µm]	2.7	1.0
Si ₃ N ₄	Stopping power [MeV×cm²/g]	11.2	4.0
	Linear stopping power [keV/µm]	3.1	1.1
SiC	Stopping power [MeV×cm²/g]	11.1	4.0
	Linear stopping power [keV/µm]	3.5	1.3





Thin windows: Be

□ Well known material

- \Box As thin as 8 μ m in commercial x-ray windows[5]
- □ Aperture 7 mm
- $\Box \Delta P > 1$ bar
- □ Commercial, but no many suppliers



Figure 1 Typical Assembly of Beryllium Window



Figure 2 Conflat Flange Geometry

Table 1 Dimensions of Conflat Flange Options (Refer to Figure 2 above)									
CF	Foil Thickness (µm)	Foil Diameter (mm) - A	Through Hole Diameter (mm) - B	CF Outer Diameter (mm) - C	CF Thickness (mm) - D	Window Height (mm) - E	Coating	Part ID	
1-1/3"	8.0	9.2	7.0	33.8	7.2	0.5	DuraCoat Plus	DBM-08-9.2-CF1.3-P	
OD	25.0	16.0	13.0	33.8	7.2	0.5	DuraCoat	DBM-25-16.0-CF1.3	
2-1/8"	8.0	9.2	7.0	53.6	11.9	6.5	DuraCoat Plus	DBM-08-9.2-CF2.1-P	
OD	25.0	16.0	13.0	53.6	11.9	6.5	DuraCoat	DBM-25-16.0-CF2.1	





Thin windows: C

- \Box Thickness <1 μ m
- Different options: Graphenic carbon [6] or diamond
 [7]
- □ Research phase



Fig. 4. Measured thickness dependent burst strength of fabricated GC transmission windows with a diameter of 7 mm.



Fig. 2. (a) sketches the fabrication process of the transmission window. (b) shows a top view image of a fabricated GC window. (c) depicts a TO8 housing with a GC window glued into the top of the housing



Fig. 4. SEM picture of the diamond film 345[#].

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Thin windows: SiC

 $\Box \, \mbox{Thickness}$ <1 $\mu \mbox{m}$

- Bulk material has excellent mechanical properties
- □No many commercial suppliers [8]





Thin windows: Si_3N_4

- □ Commercially available: Xray windows i.e. [9]
- □ Thickness <1 µm
- □ They can work at cryogenic temperature [10]
- □ Bulk material has excellent mechanical properties [11]
- \Box Expected ΔT at the conditions described before estimated 460κ
- Stress during the pulse reasonable level according to first rough estimate.
- \Box 1 µm 6×6mm window \rightarrow >5 bar pressure (tested in lab)
- $\hfill\square$ Thermal cycles at 77K





Maximum differential pressure v membrane size (membrane thickness 30 nm to 1000 nm)





Test of 1 μm thick Si_3N_4 window in HiRadMat (Baby-SMAUG)





 $\left\langle -\frac{dE}{dx}\right\rangle_{\text{electronic}} = K \frac{Z}{A} \frac{1}{\beta^2} \left[\frac{1}{2} \ln \frac{2m_e c^2 \beta^2 \gamma^2 Q_{\text{max}}}{I^2} - \beta^2 - \frac{\delta}{2} + \frac{1}{8} \frac{Q_{\text{max}}^2}{\left(\gamma M c^2\right)^2} \right] + \Delta \left| \frac{dE}{dx} \right| \quad \text{Brightness} \equiv \frac{N_b I_b}{\sigma_x^2 + \sigma_y^2} \ p^+ / mm^2 \quad \text{[12]}$



- □ Test one membrane irradiated under vacuum
- □ 4×10^{12} muons/pulse at 5MeV $\sigma_{\rm RMS}$ =0.6 mm → Maximum power deposited 0.89 kJ/cm³
- □ p⁺ equivalent with σ_{RMS}=0.25 mm at 440 GeV → 3.2×10¹² p⁺/pulse that corresponds to 2.6×10¹³ p⁺/mm²
- > Objective: Few shots increasing intensity up to failure. Optics Fp2 0.25 mm





¹ μm 6×6mm window



Results







Results





Experimental proposal

- □ Continuation of HRMT-59 (SMAUG)
- □ Test Nb-Ti coated PF-60 diffusion-bonded windows and Si₃N₄
- □ Brightness range between 288 bunches 1.2×10¹¹ ppb σ_{RMS}=0.4 mm (5 and 50 pulses)
- □ Highest possible brightness fp2 0.25 mm, 288 bunches >2.1×10¹¹ ppb (5 and 50 pulses)
- □ Test fp2 0.25 mm >2.1×10¹¹ ppb 72+72 bunches with separations 0.22 and 23 µs



Modifications:

- > DN100 \rightarrow Glue 6 Si₃N₄ windows (10×10 mm frame)
- \succ Low vacuum (10-2 mbar) \rightarrow Pressure difference even with large leaks
- Remotely operated isolation valves
- \succ He/O₂ (Heliox). Oxidation and high sensitivity using leak detector (20% O₂ 80% He) → Early detection of any failure
- ▶ Pirani gauges → Leak rate by accumulation
- > Remote control: Leak detector, valves and gauges



- \square Mechanical characterization of ${\rm Si_3N_4}$ membranes at different temperatures (from cryogenic to high temperature) \rightarrow Use inputs to better validate thermomechanical models
- \Box For thin membranes Bulge testing is the easiest setup. Measurements of ${\rm Si_3N_4}$ membranes at room temperature in [13]









-1- :-





-1- :





- Pressure tests were performed on square membranes with the following geometry:
 - \square Si frame: 10 mm x 10 mm, thickness=200 μm ,
 - \Box Si₃N₄ membrane: 6mm x 6mm, thickness=1000nm.
- Leak-tight tests of the bulge test setup were successfully performed.
- Different glues were used to bond the sample to the copper flange. This considerably affects the mechanical response of the membrane against the maximum pressure it can withstand.
- □ Two different ways to mount the membrane (positive and negative orientation in the figure) were investigated.
- □ Results from pressure tests are shown in the table:

Z Y	NEGAT	IVE 24
*	POSIT	z, y TVE

Sample #	Membrane orientation	Glue	Temperature	Max pressure before failure
1	NEGATIVE	Superglue (instantaneous)	295 К	< 1 bar
2	POSITIVE	Superglue (instantaneous)	295 K	2 bar
3	POSITIVE	Araldite bi-component (curing time: 2 h)	295 K	6 bar
4	POSITIVE	Araldite bi-component (curing time: 2 h)	77 K	2 bar











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Si_3N_4 windows

- Low energy muons would require very thin windows to limit the impact of the window itself
- \clubsuit Si₃N₄ windows seem a good candidate:
 - ✤ Cheap and available
 - ✤ Good properties already with on the shelf products
 - ✤ Compatible with bright beams
 - ✤ Compatible at cryogenic temperature
- Thermomechanical characterization is ongoing, and more beam tests are planned
- The window should separate vacuum from the absorber, at low energy ideally hydrogen. The configuration of the absorber will define the maximum differential pressure the window should sustain



Absorber

$$\epsilon_{min,N} \propto \frac{E}{BL_R(dE/ds)}$$
 [2]

- □ H₂ best absorber material (out of the scope of MuCol?)
- □ What is the required density?
- □ Which length can we expect?
- □ What is the effect on the window?



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Absorber length

20 → 5 MeV from [14][15]. 9.6 J, not including heat load from muon decay



H ₂ Absorber	Length	Max P (bar)	Max T (K)	P at 3×σ _{RMS} (bar) (gaussian beam shape)	T at 3×σ _{RMS} (K) (gaussian beam shape)		
RT@1bar	124 m	1.3	373	1.04	303		
RT@4bar	31 m	5.2	373	4.18	303		
20.3K@1bar vapor	8 m	7.5	140	1.8	34		
26.1K@4bar vapor	2.1 m	29.2	143	7	40		
20.3K@1bar liquid	15 cm	833	128	125	35		
$\left\langle -\frac{dE}{dx} \right\rangle_{\text{electronic}} = K \frac{Z}{A} \frac{1}{\beta^2} \left[\frac{1}{2} \ln \frac{2m_e c^2 \beta^2 \gamma^2 Q_{\text{max}}}{I^2} - \beta^2 - \frac{\delta}{2} + \frac{1}{8} \frac{Q_{\text{max}}^2}{\left(\gamma M c^2\right)^2} \right] \qquad \mathbf{L} = \int_{E_f}^{E_s} \frac{1}{dE/ds} dE$							

Summary



- Several window candidates for final cooling. Si₃N₄ seems very promising
 Commercially available as vacuum window for x-ray transmission
 - First irradiation tests showed excellent performance, well beyond the requirements
 - Ongoing effort to better characterise the thermomechanical properties of the membranes at different temperatures and understand its behaviour and produce better models.
 - □ Irradiation in proton facilities
- □ High density absorber required to have a short solenoid, but high power deposition \rightarrow High pressure. Compatible with thin window?
- \Box Shock wave and phase change after power deposition in liquid hydrogen \rightarrow Very challenging CFD problem out of reach of commercial codes
- \Box The design of the H₂ absorber will define the requirements and lifetime of the window, is this out of the scope of MuCol?
- \Box Decouple window and absorber \rightarrow even thinner windows
 - Pulsed high density vapor?
 - □ Leidenfrost effect?
 - □ Staging of steps with different densities (lower at the end)



THANK YOU FOR YOUR ATTENTION!



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Thin windows

- > Approx 1 mm stops the beam completely at 5MeV (1.3 mm for Be)
- Several candidates for thin windows
- Better characterization and evaluation required but first numbers look promising
- Measure mechanical properties (cryogenic to high temperature) for precise thermomechanical simulations. Bulge test [14] with interferometry?
- Pressure in the absorber is critical for the window definition

		5 MeV	20 MeV
Ве	ΔT _{inst} [K]	174	61
	Cyclic Thermal Stress (MPa)	485	171
c: N	ΔT_{inst} [K]	470	169
51 ₃ N ₄	Cyclic Thermal Stress (MPa)	228	82
С	ΔT_{inst} [K]	507	180
	Cyclic Thermal Stress (MPa)	1013	360
SiC	ΔT_{inst} [K]	467	168
	Cyclic Thermal Stress (MPa)	224	81



Si $_3N_4$ Ø 7 mm 1 μ m at 5 MeV – 0.6 mm gaussian beam Only room temperature ambient radiation

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$$\sigma_{cyc} \approx \frac{1}{2} \alpha E \Delta T$$
 $\Delta T_{inst} = \left(\frac{dE}{dx}\right) \frac{N}{2\pi \sigma^2 \rho c}$