

# Specific requirements for CLIC RF structures

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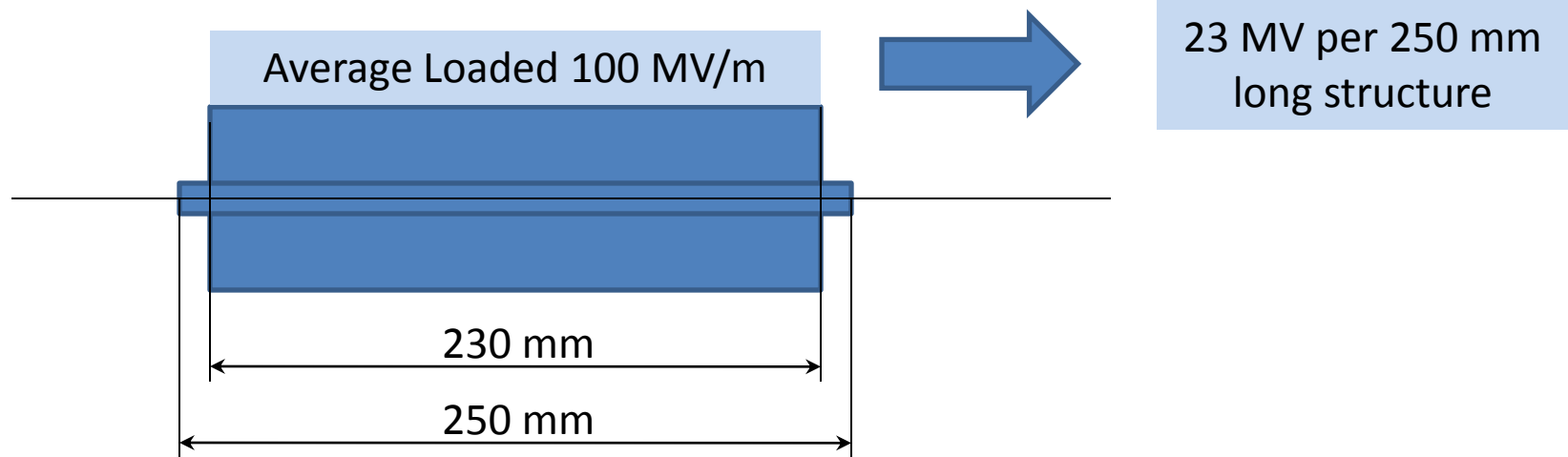
# Outline

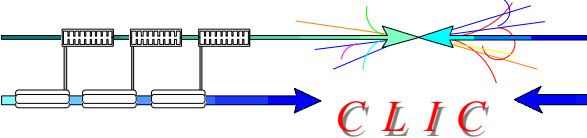
- CLIC main linac accelerating structure (AS)
- CLIC crab-cavity (CC)

N.B. Most of the information is already well known to our UK collaborators. Even more, for the crab-cavity, most of it came from them ! Nevertheless, it is an attempt to summarize it and to get common understanding of the problems.

Acknowledgements to D. Schulte and R. Thomas for useful discussions

# CLIC AS layout and space constraints





Beam dynamics (BD) constraints based on the simulation of the main linac, BDS and beam-beam collision at the IP:

- $N$  - bunch population depends on  $\langle a \rangle / \lambda$ ,  $\Delta a / \langle a \rangle$ ,  $f$  and  $\langle E_a \rangle$  because of short-range wakes
- $N_s$  - bunch separation depends on the long-range dipole wake and is determined by the condition:

$$W_{\pm 2} \cdot N / E_a = 10 \text{ V/pC/mm/m} \cdot 4 \times 10^9 / 150 \text{ MV/m}$$

RF breakdown and pulsed surface heating (rf) constraints:

- $\Delta T^{\max}(H_{\text{surf}}^{\max}, t_p) < 56 \text{ K}$
- $E_{\text{surf}}^{\max} < 250 \text{ MV/m}$
- $P_{\text{in}} / C_{\text{in}} \cdot (t_p^{\text{P}})^{1/3} < 18 \text{ MW/mm} \cdot \text{ns}^{1/3}$

These constraints have been used in 2008 in the design of the CLIC baseline structure: CLIC\_G.

50 K

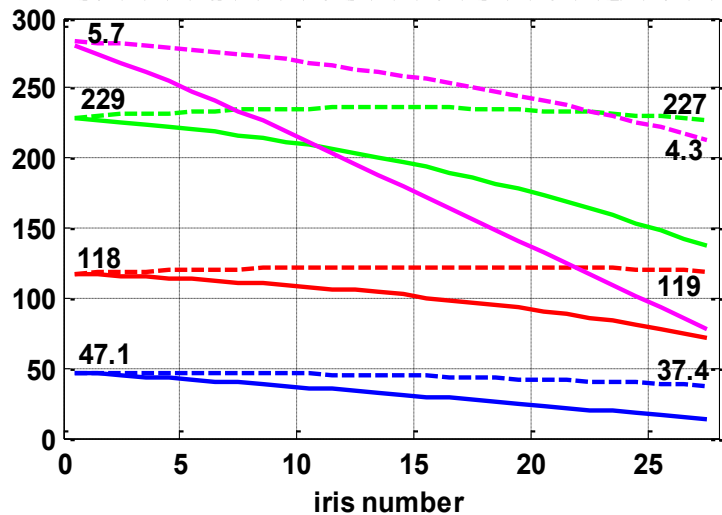
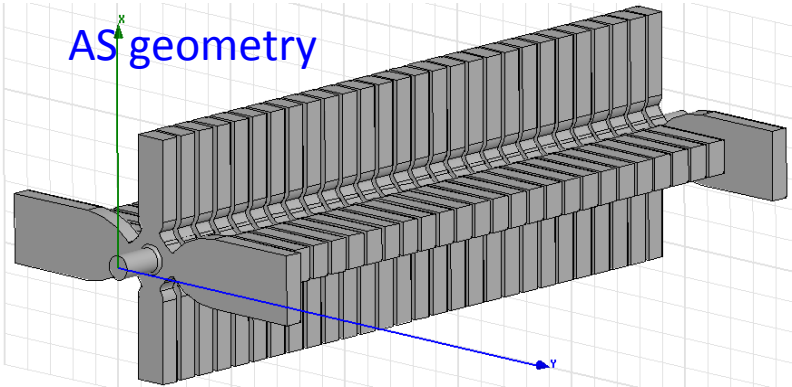
220 - 250 MV/m

15 - 17 MW/mm·ns<sup>1/3</sup>

$S_c < 4 - 4.5 \text{ MW/mm}^2$

These are the values which correspond to the current (2011) understanding of the RF breakdown constraints

# CLIC baseline AS for the CDR



$$P/C * t_p^{1/3} = 17$$

$$\text{MW/mm} * \text{ns}^{1/3}$$

The fundamental mode properties are shown.

The traces from top to bottom are:

$S_c \cdot 40$  [W/ $\mu\text{m}^2$ ](pink),

Surface electric field [MV/m](green),

Accelerating gradient [MV/m](red),

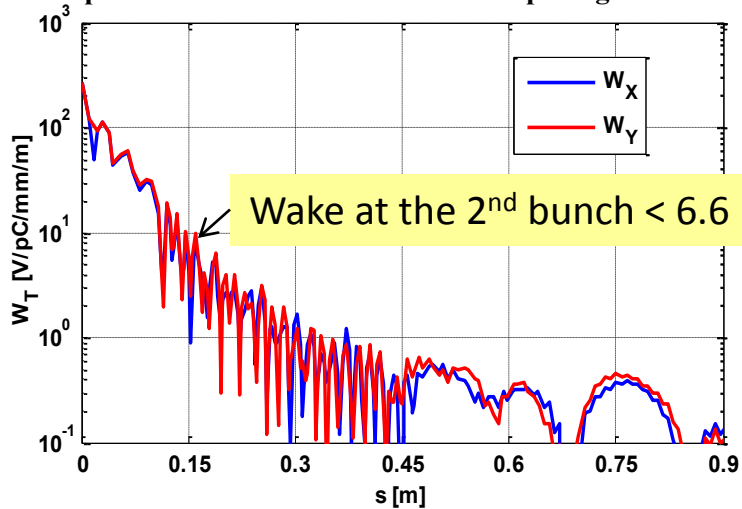
Pulse surface temperature rise [K](blue).

Dashed traces are unloaded and solid are beam loaded conditions

Average loaded accelerating gradient	100 MV/m
Frequency	12 GHz
RF phase advance per cell	$2\pi/3$ rad.
Average iris radius to wavelength ratio	0.11
Input, Output iris radii	3.15, 2.35 mm
Input, Output iris thickness	1.67, 1.00 mm
Input, Output group velocity	1.65, 0.83 % of $c$
First and last cell $Q$ -factor (Cu)	5536, 5738
First and last cell shunt impedance	81, 103 M $\Omega$ /m
Number of regular cells	26
Structure length including couplers	230 mm (active)
<b>Bunch spacing</b>	<b>0.5 ns</b>
<b>Bunch population</b>	<b><math>3.7 \times 10^9</math></b>
Number of bunches in the train	312
Filling time, rise time	66.7 ns, 21 ns
Total pulse length	243.7 ns
<b>Peak input power</b>	<b>61.3 MW</b>
RF-to-beam efficiency	27.7 %
<b>Maximum surface electric field</b>	<b>230 MV/m</b>
<b>Maximum pulsed surface heating temperature rise</b>	<b>47 K</b>

# CLIC baseline AS for the CDR

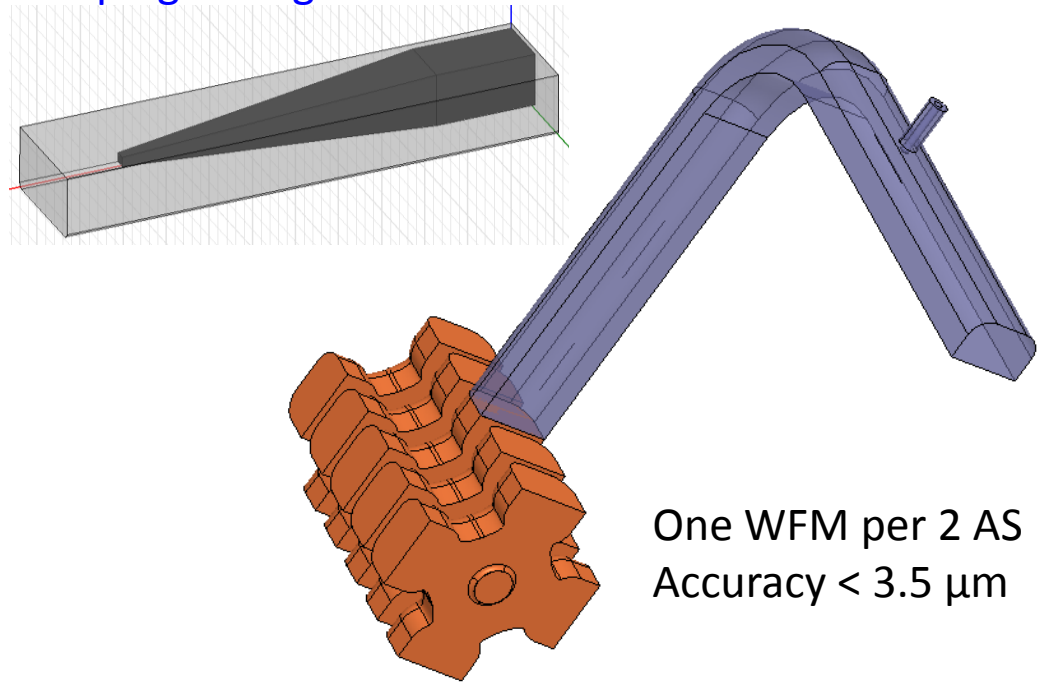
The envelope of the transverse wakefields for both planes is shown. The CLIC bunch spacing is 0.15 m.



Parameters of the lowest dipole-band modes

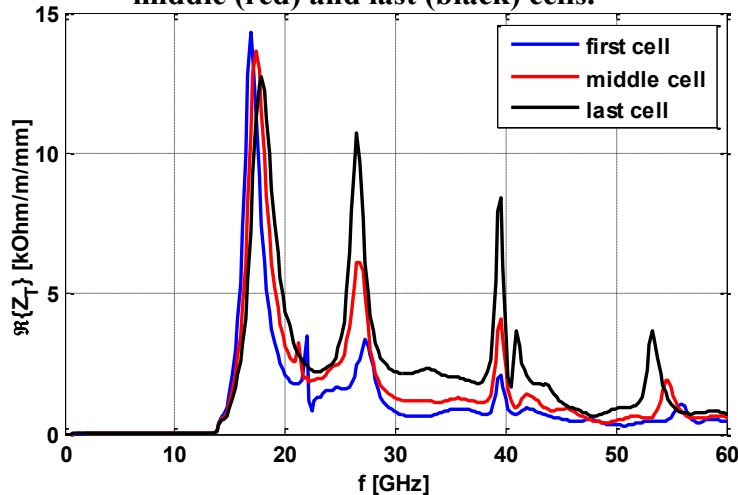
Cell	First	Middle	Last
$Q$ -factor	11.1	8.7	7.1
Amplitude [V/pC/mm/m]	125	156	182
Frequency [GHz]	16.91	17.35	17.80

Damping waveguide load



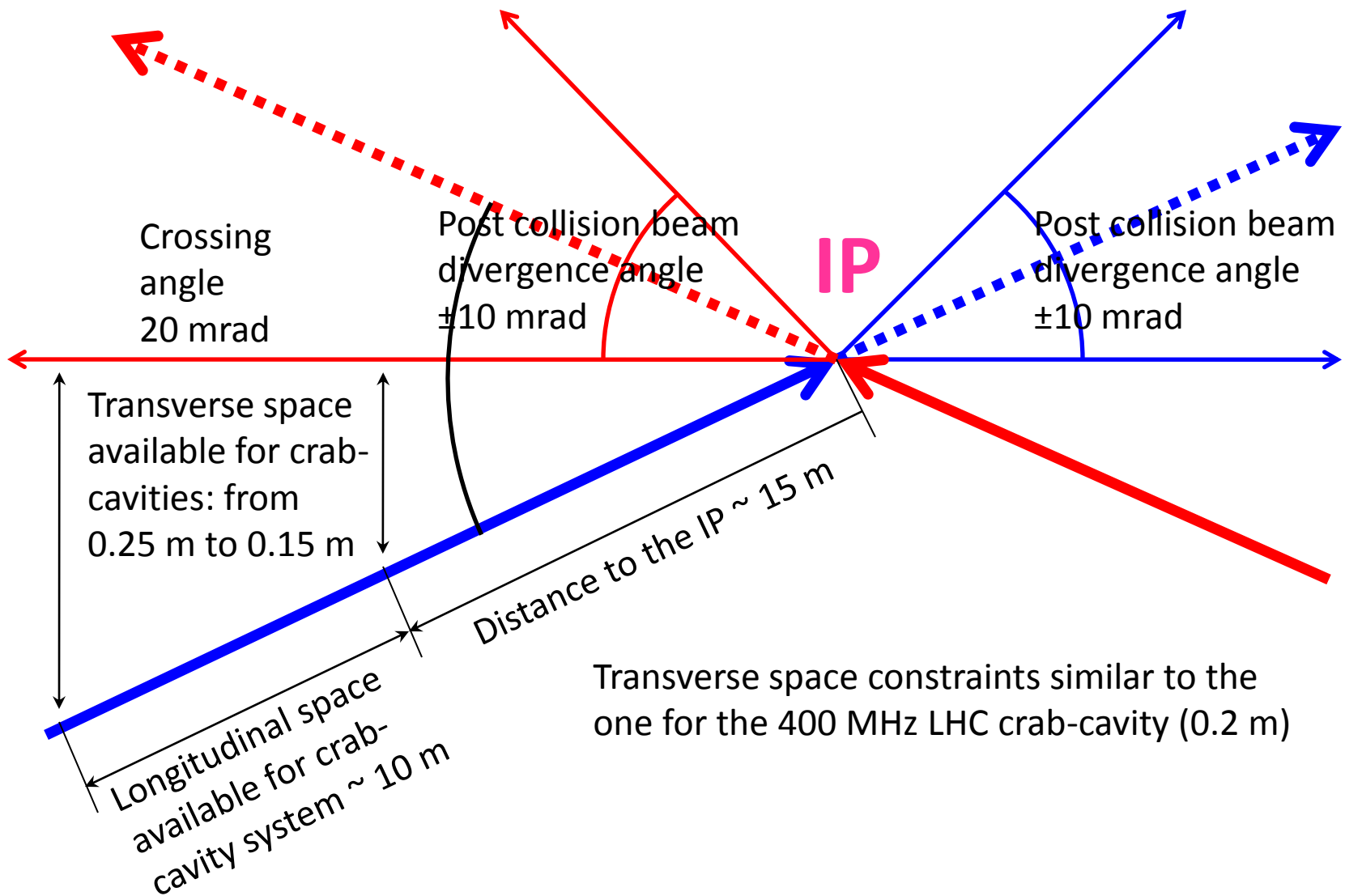
One WFM per 2 AS  
Accuracy < 3.5  $\mu\text{m}$

Transverse impedances of the first (blue), middle (red) and last (black) cells.



Geometry of one of the four arms of the wakefield monitor.  
(Courtesy of F. Peauger, CEA, France).

# Crab-cavity system layout and space constraints



# CLIC parameters and specifications for the CC system

## Relevant CLIC parameters:

- Beam energy at the IP:  $E_0 = 1.5 \text{ TeV}$
- Crossing angle:  $\theta_c = 20 \text{ mrad}$
- Beam normalized emittance:  $\epsilon_x = 660 \text{ nm}$ ,  $\epsilon_y = 20 \text{ nm}$
- Beta-function at the position of CC system:  $\beta_{CC} \approx 100 \text{ km}$
- => Beam spot size at the position of the CC:  $\sigma_x \approx 150 \mu\text{m}$ ,  $\sigma_y \approx 25 \mu\text{m}$

## Specifications for CC system:

- Frequency:  $f = n \cdot 2 \text{ GHz}$ ,  $n = 1, 2, 3, 4, 5, 6, \dots$
- Kick strength versus frequency:

$$V_t * f = \theta_c \cdot E_0 \cdot c / 2\pi R_{12} \approx \mathbf{2.5 \text{ MV} * 12 \text{ GHz} = 7.5 \text{ MV} * 4 \text{ GHz}}$$

- Maximum beam offset horizontal:  $dx \approx 4\sigma_x \approx 0.6 \text{ mm}$
- Maximum beam loading:  $V_l = dx * \theta_c \cdot E_0 / R_{12} \approx 370 \text{ kV}$

$$\Rightarrow \text{peak: } P_b = I_b * V_l \approx \mathbf{0.4 \text{ MW}}$$

$$\Rightarrow \text{average: } \langle P_b \rangle = P_b * 50 \text{ Hz} * 156 \text{ ns} \approx \mathbf{3 \text{ W}}$$

**Can be relaxed to  
½ if it is critical**

- Kick amplitude and time stability:  $\sim 2\%$  and  $\sim \mathbf{5 \text{ fs}}$  for  $\sim 2\%$  Luminosity reduction (CLIC CDR, Crab-cavity system)
- **RF constraint for AS design can be applied here to be verified with high power test**



# Wakefields in the CC system

- No detailed beam dynamics (BD) simulations have been done at CERN on the acceptable level of the wakefields from the CC system
- It is very desirable (In my opinion, absolutely necessary) to do the BD study in order to get the acceptable level of the wakefields in the CC system.
- Below, an attempt to estimate the threshold level for the long-range wakefields (probably the most critical ones) is presented.

Multi-bunch wake field effect  
is proportional to

$$W_t N e^2 \int \frac{\beta(s) ds}{2 E(s)};$$

D. Schulte, PAC09

For the main linac:  $\langle \beta(s) \rangle \sim \sqrt{E(s)}$ ; E goes linear from 9 to 1500 GeV

=> integral  $\approx 380 \text{ m}^2/\text{GeV}$  (D. Schulte)

$W_t @ 2^{\text{nd}}$  bunch  $< 6.6 \text{ kV/pCm}^2$ , and “no” wake for the others

For the CC system:  $\langle \beta \rangle = 100 \text{ km}$ ;  $E = 1500 \text{ GeV}$

=> integral  $\approx L_{\text{CC}} * 33 \text{ m}^2/\text{GeV}$ ; about 10 times smaller for 1 m long CC

If **undamped**:  $L_{\text{CC}} * W_t = L_{\text{CC}} * W_{t0} = 1\text{m} * 66 \text{ kV/pCm}^2 / (312/2) \text{ bunches} \approx 1\text{m} * \mathbf{0.4 \text{ kV/pCm}^2}$

**12 GHz CC**: Typical level of  $W_{t0} \approx 50 \text{ kV/pCm}^2$ ;  $L_{\text{CC}} \approx 1/4\text{m}$ ; **strong damping is needed**

4 GHz CC: Typical level of  $W_{t0} \approx 2 \text{ kV/pCm}^2$ ;  $L_{\text{CC}} \approx 10\text{m}$ ; some damping is needed (?)

2 GHz CC: Typical level of  $W_{t0} \approx 1/4 \text{ kV/pCm}^2$ ;  $L_{\text{CC}} \approx \mathbf{20\text{m}}$ ; no damping is needed (?)

# Conclusion

- ❑ Requirements for the main linac accelerating structure are well known both from the point of view of beam dynamics and high power RF.
- ❑ Requirements for crab-cavity system are also well known, maybe with one exception. Namely, the acceptable level of the wakefields in the crab-cavity is still to be obtained from the beam dynamics simulations both for horizontal and vertical planes together with required alignment tolerances.
- ❑ Collaborators are welcome to present this work if it is already done. This is critical for the damped crab-cavity design. Build-in wakefield monitor for crab-cavity alignment may be considered.
- ❑ Collaborators are also welcome to present considerations on the frequency choice between 12 GHz pulse system (CDR baseline) and 4 (or 2) GHz CW system (possible alternative).