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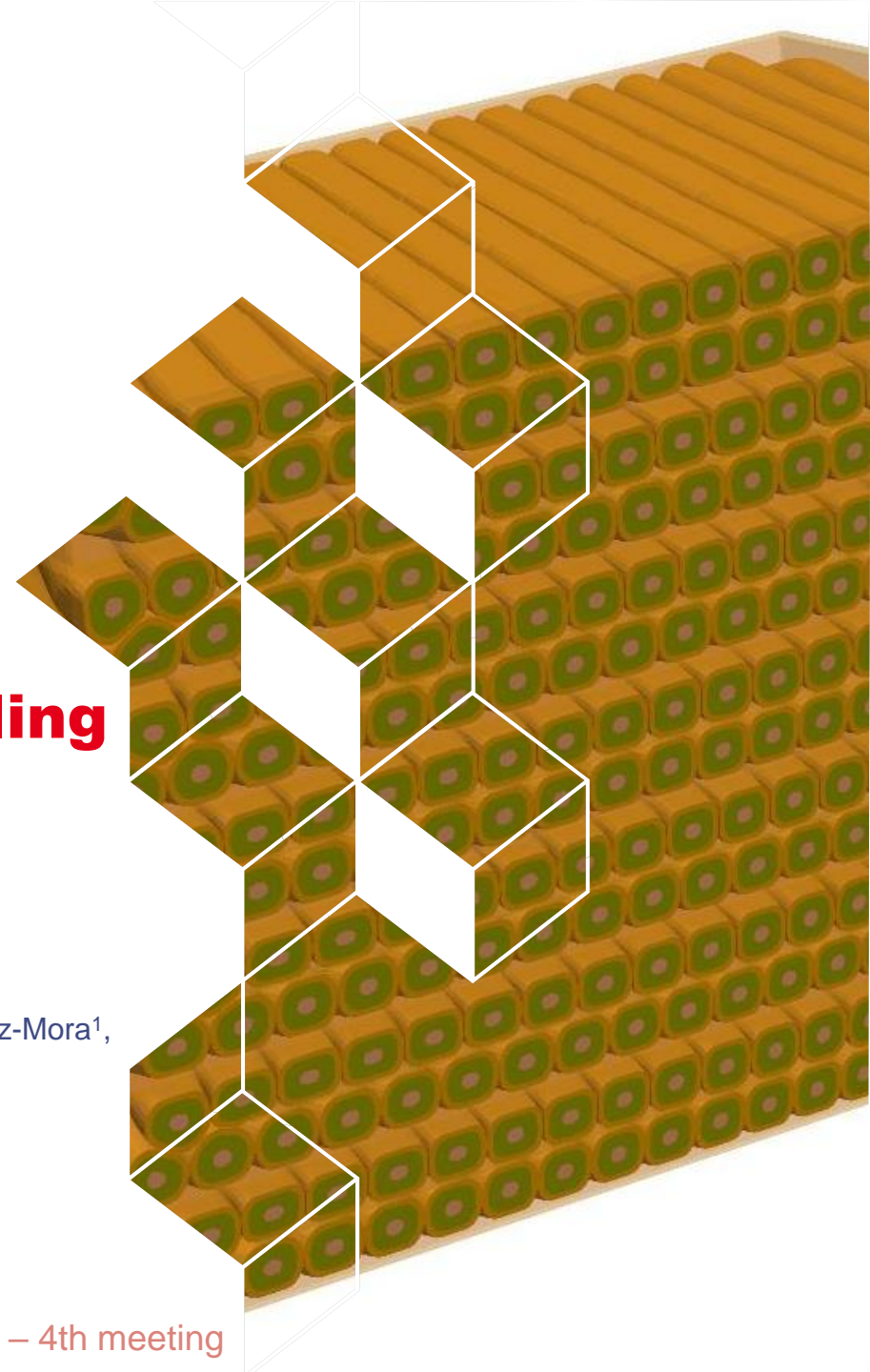
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# Characterization and modeling of Nb<sub>3</sub>Sn conductors for accelerator magnets at CEA Paris-Saclay

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# Outline

## 1. Characterization and modeling program for Nb<sub>3</sub>Sn conductors @ CEA Paris-Saclay

## 2. CoCaSCOPE

Mesh Generator

Behavior representation

Experimental characterization

Single stack simulations

## 3. Summary and perspectives

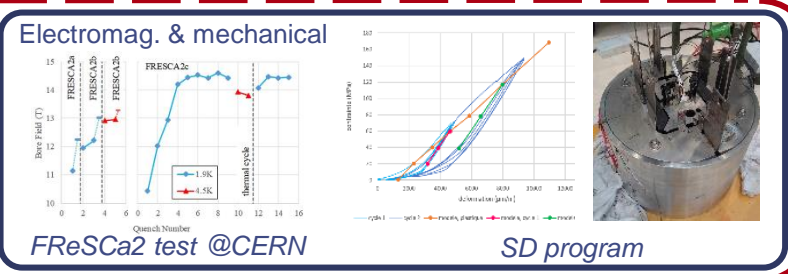
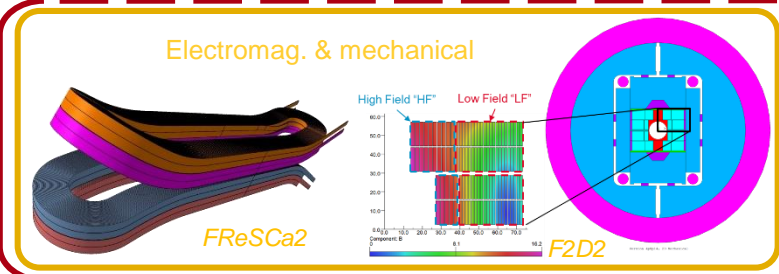


# Overview of CEA's Nb<sub>3</sub>Sn modeling program

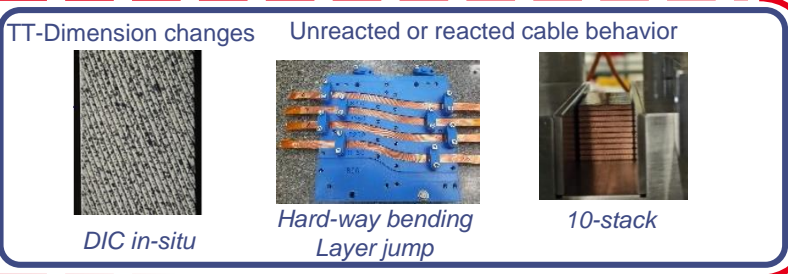
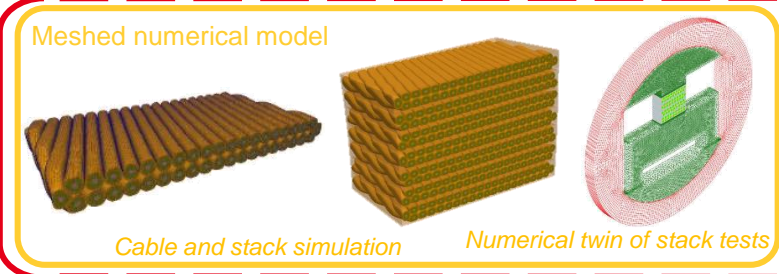
Magnet scale

Model

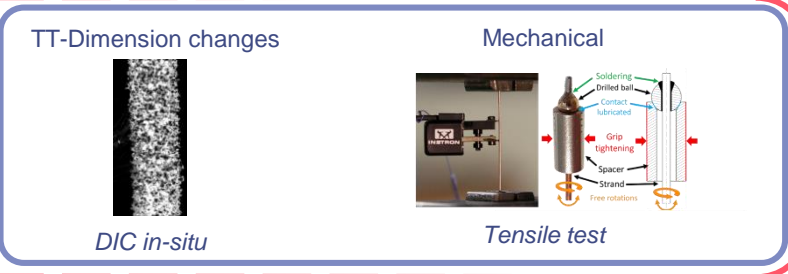
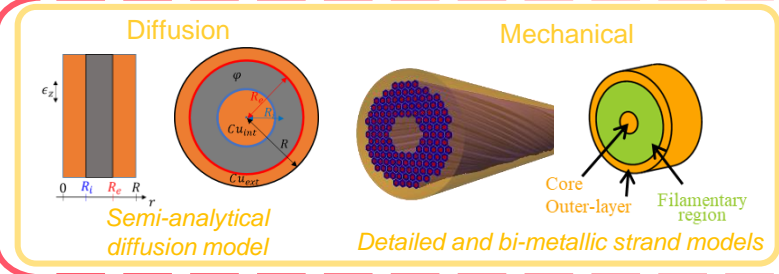
Experimental



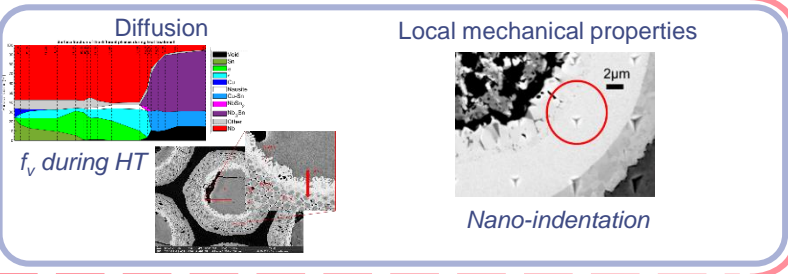
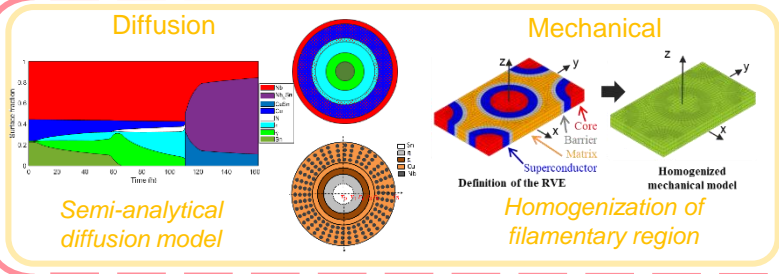
Cable scale



Strand scale



Subelement scale





# Magnet scale and global approach

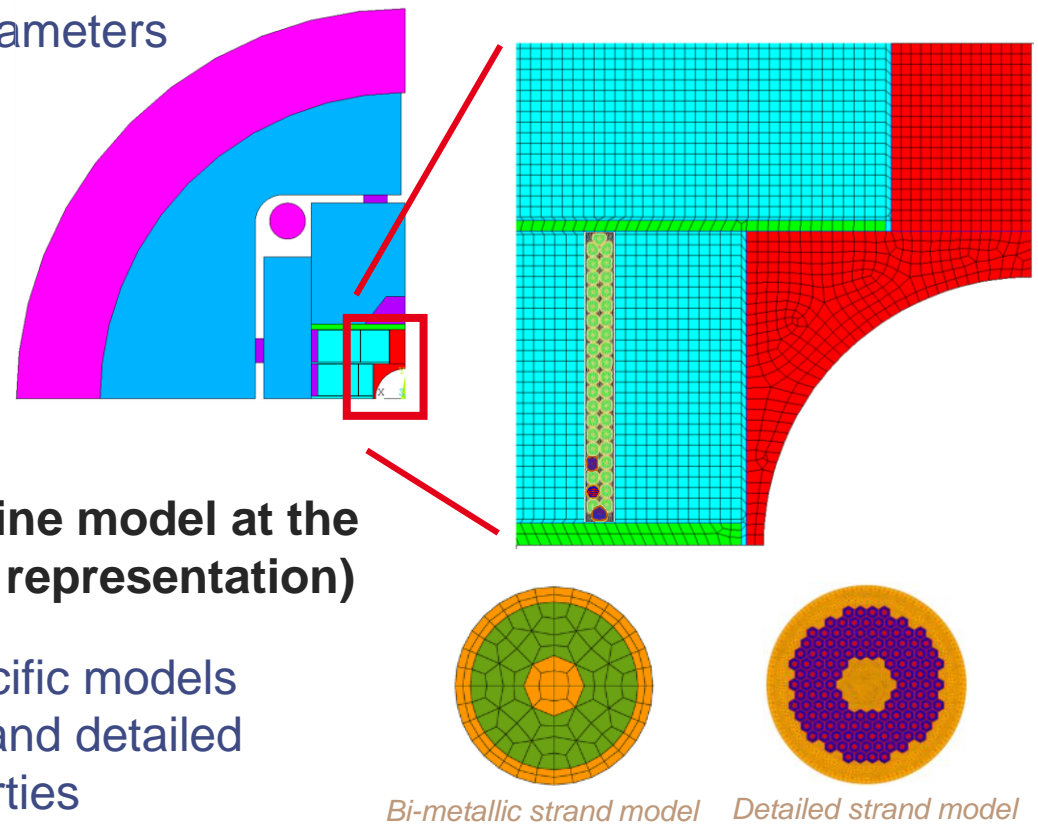
## ■ Magnet model

- Magnet behavior driven by local parameters
- Homogenized coil
  - ↳ Which behavior ?
  - ↳ Which homogenization scheme?
  - ↳ Based on which object(s) (/scale(s)) loaded under which condition(s)?

## ■ Approach

⇒ **Multi-scale modeling with baseline model at the cable scale (light mesh & adapted representation)**

- 2D pre-design steps toward 3D specific models
- Integration of detailed cable model and detailed strands to access to the local properties
- **Characterization and modeling of the lower scales to understand and choose relevant level of details (mechanical and geometrical)**



*Bi-metallic strand model    Detailed strand model*

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Experimental characterization

Single stack simulations

## 3. Summary and perspectives



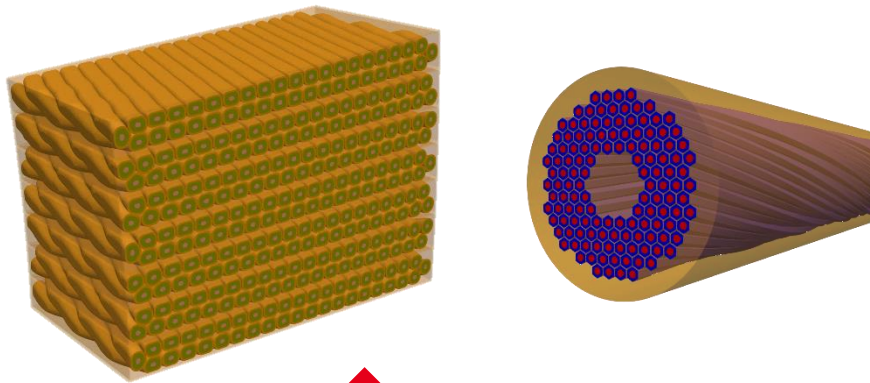




# CoCaSCOPE approach

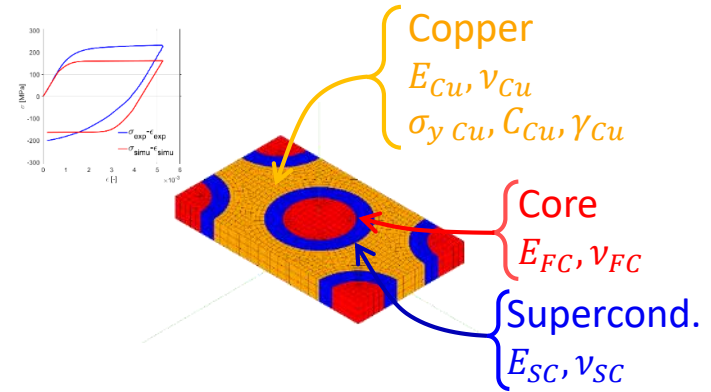
## ■ Mesh Generator - MG

↳ Tool for the generation of representative Rutherford cable model and detailed strand



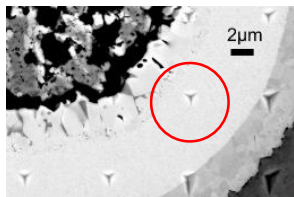
## ■ Behavior Representation - BR

↳ Objective oriented representation

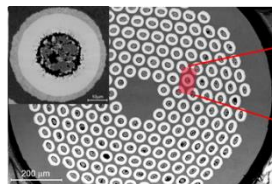


## ■ Experimental Characterization - EC

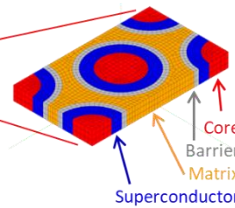
↳ Define modelling strategy  
 ↳ Identify models parameters  
 ↳ Validate models



Nano-indentation test



Analysis of strand observations and material properties

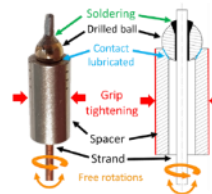
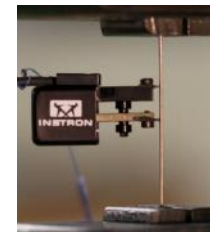


Definition of the RVE

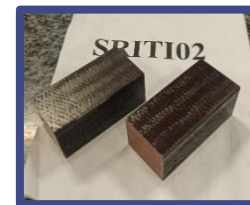
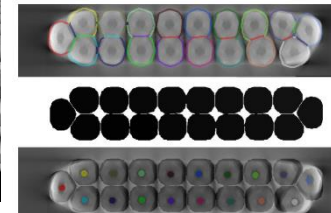
Metallography to define models



Tensile test on strand



X-ray tomography



Compressive test on stack

# Experimental characterization



## ■ Objectives

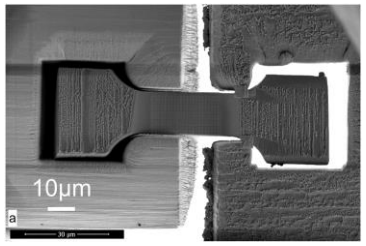
- Characterization of the mechanical behavior
  - Strain rate, hold, unloadings, cyclic behavior
  - Investigation of damage (impregnation matrix and conductors)
- Data for the identification and the validation of mechanical models

## ■ Available tests and scales

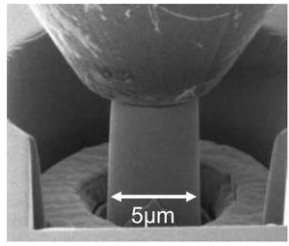
- Subscale dipole
- 10-stack compressive test
- Strand
  - Nano-indentation
  - Tensile test

## ■ Perspectives

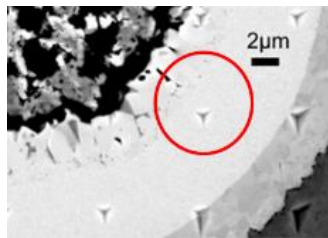
- Transverse tests on strands
- Nano-indentation @ 77 K
- Micro and nano-mechanical testing



Micro-sample martensitic steel [Ben Salem 19]



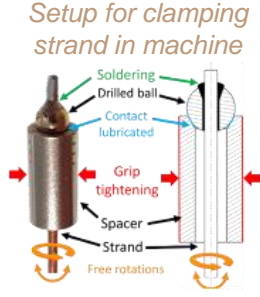
Micro-pillar compression [Breumier 20]



Nano-indentation in  $Nb_3Sn$  phase of a PIT strand [Lenoir 17]



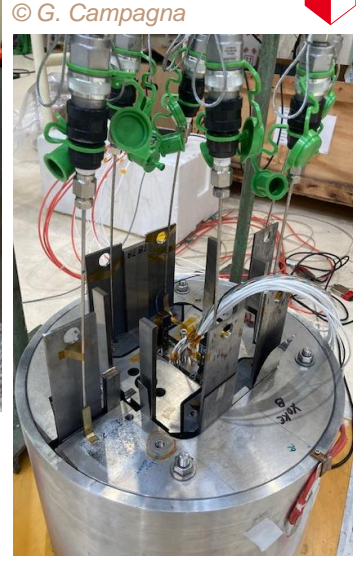
$Nb_3Sn$  strand w/ extensometer for tensile test



Setup for clamping strand in machine



Instrumented coil segment

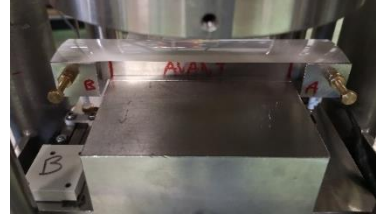


Mechanical loading in a structure

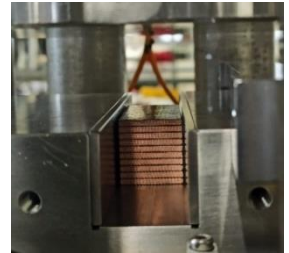
© S. Perraud



Cryostat & machine for 10-stack test

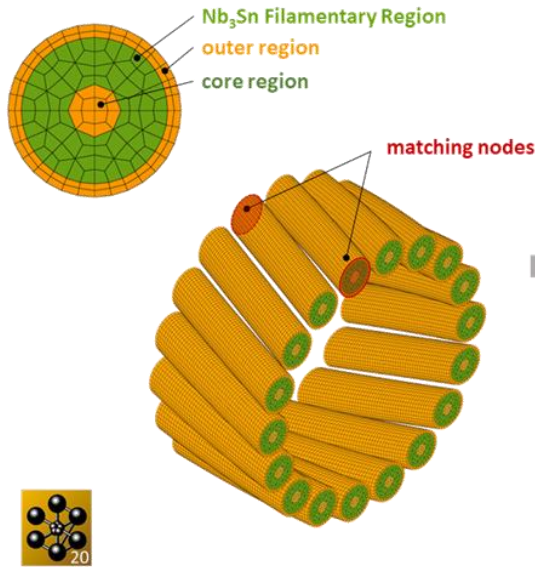


10-stack test setup

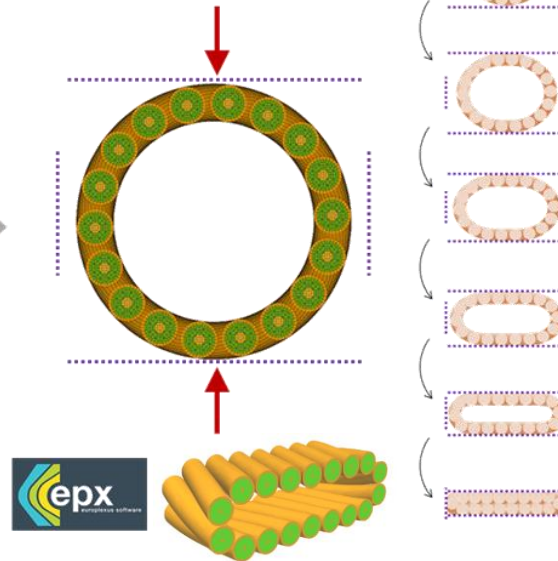




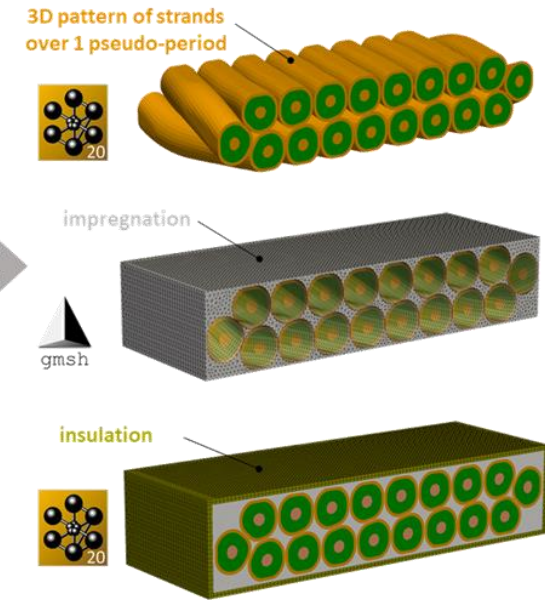
## initial mesh (a)



## cable shaping (b)



## conductor block meshing (c)

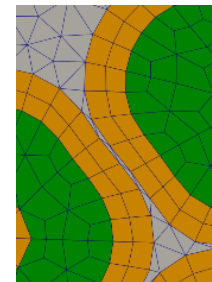


### ■ Initial model

- Helical geometry
- One pseudo-period
- Bi-metallic description
- 8-node brick elements
- Parameters
  - Strand parameters
    - ↳ Diameters (strand, core & filamentary area)
  - Cable parameters
    - ↳ # of strands / twist pitch / width & height
  - Mesh density
  - Gap between strands

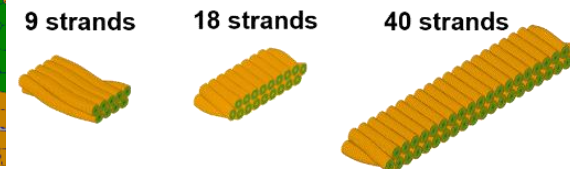
### ■ Cable shaping

- Simplified cabling process
  - ↳ Compaction by 4 rigid planes
- Parallelized explicit dynamic simulation
- Coupled displacement of front and rear faces of adjacent strands
- Clearance gap between strands to avoid interpenetration and ease meshing of impregnation
- Mechanical state after shaping not considered



### ■ Conductor block mesh

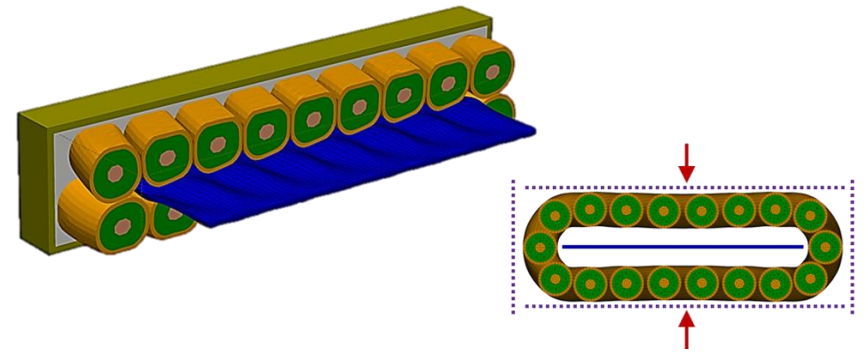
- Impregnation meshed with 4-node tetrahedral elements
- Insulation meshed with 6-node pentahedron elements
- Node conformal
- Homeomorphic faces
  - ↳ concatenation of blocks



# Cable scale - CoCaSCOPE Mesh Generator

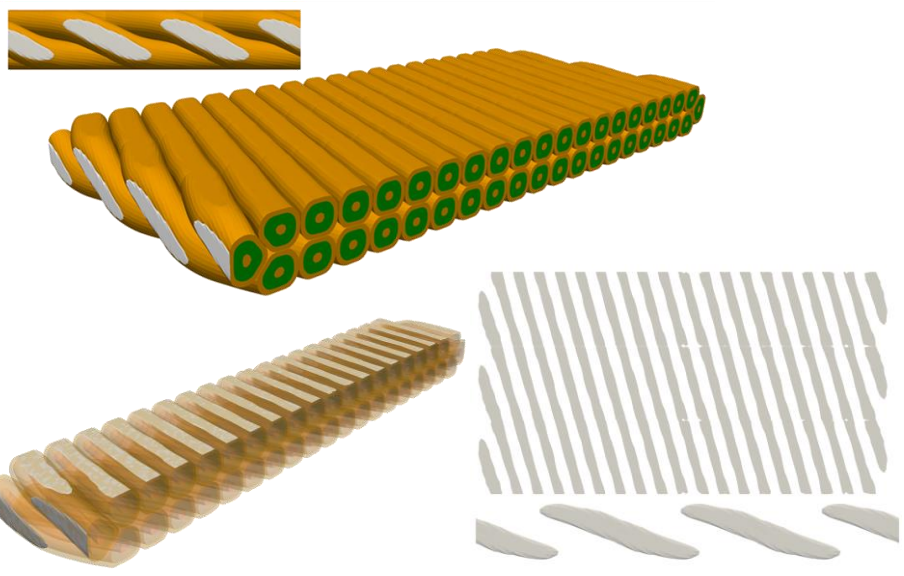
## Options

- Steel core

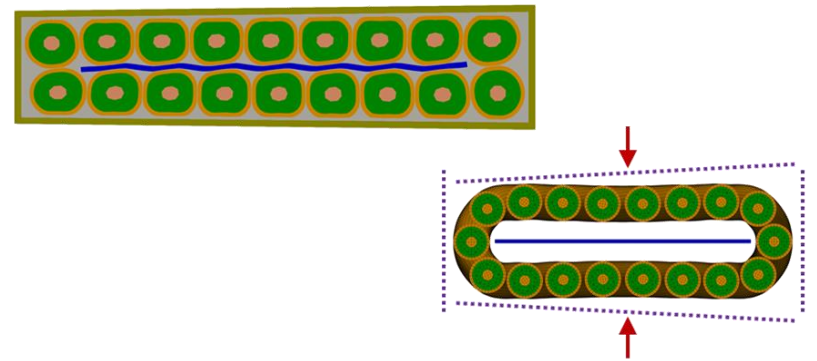


## Features

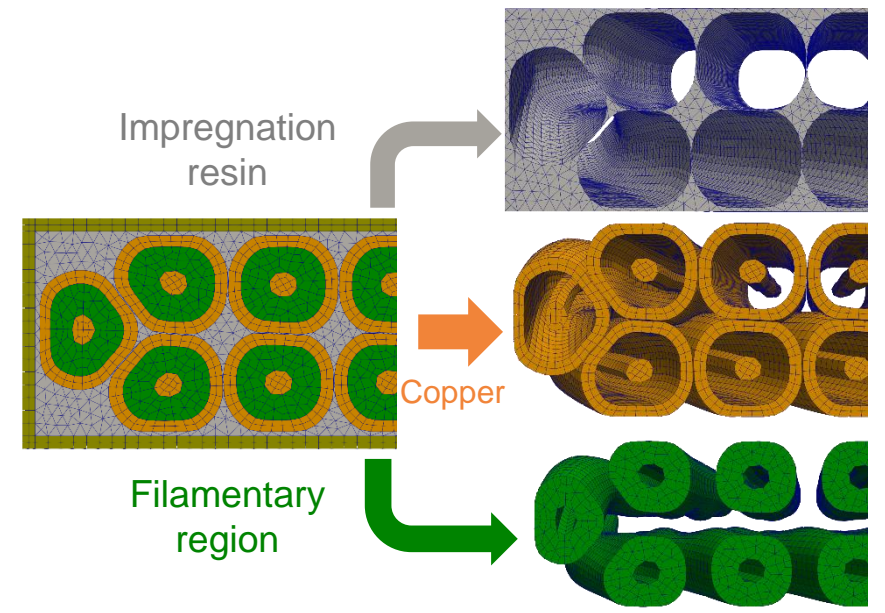
- Facets of bare conductor



## Keystone



## Access to the different materials



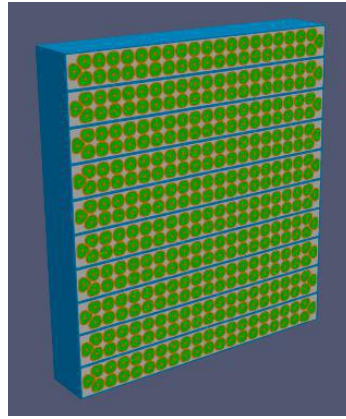
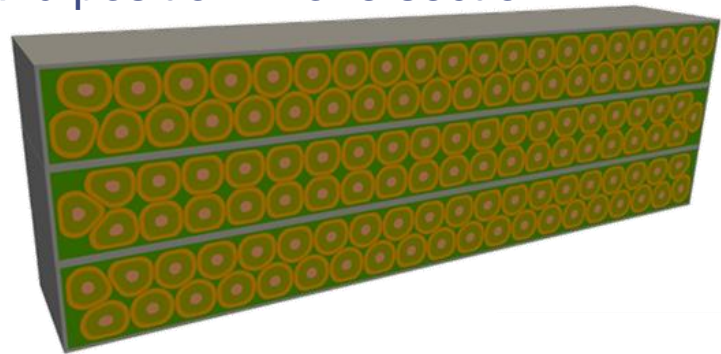
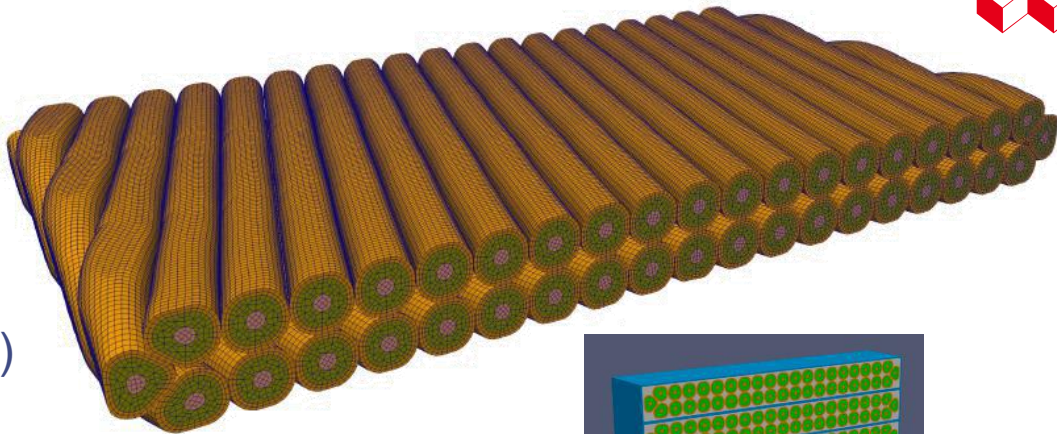




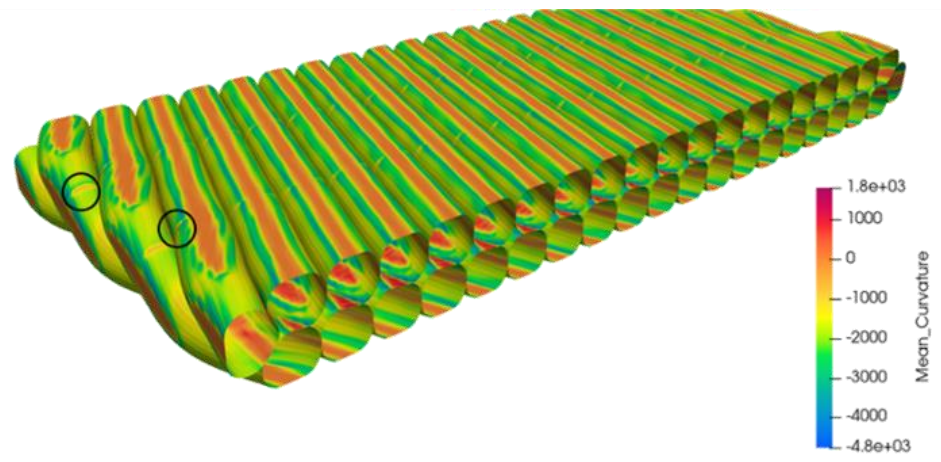
# Cable scale - CoCaSCOPE Mesh Generator

## ■ Concatenation of blocks

- Mesh block of one pseudo period
  - ↳ twist-pitch divided by # strands
- Homeomorphic meshes
  - ➔ Concatenation of blocks in length to obtain complete period (or more)
  - ➔ Stacking to reproduce cable stack w/ different strand position in one section



- ⚙ □ Discontinuity of the curvature of the outer surface of strands
  - ↳ Poisson effect due to transverse compression concentrated at the ends of the strands





# Mesh validation

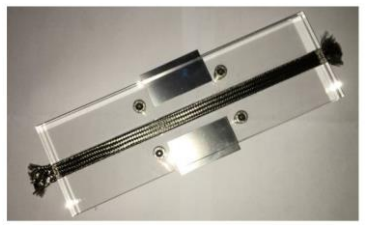
■ Mesh generator validated over X-ray tomographies and image analysis of existing cables

■ Overall shape

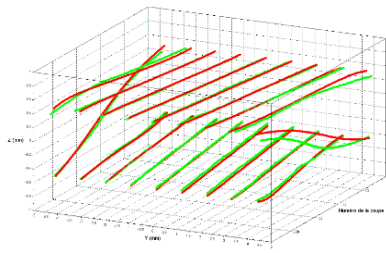
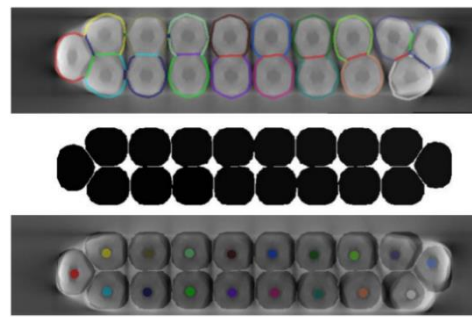
- Strand cross-section similar to those from real samples
- Cable facets consistent with those observed on bare cables

■ Strands centroids and cross-section

- X-ray tomography of cables (15 μm resolution)
  - ↳ 9, 18 and 40 strands cables
- Automatic extraction
  - Centroids
  - Skin of strands
- Comparison with numerical model
  - Strand by strand centroid error
  - Inter-strands distance error
  - Global strand deformed shape

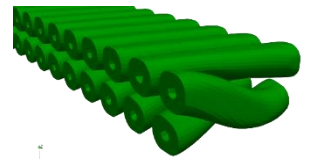
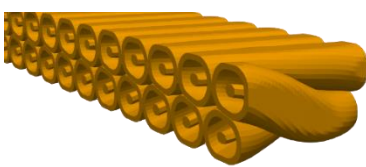
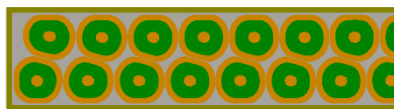
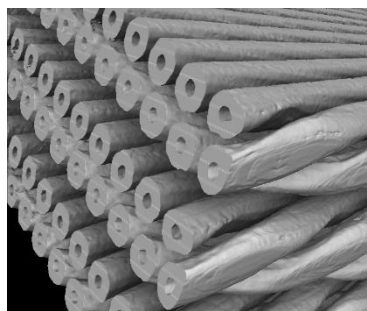
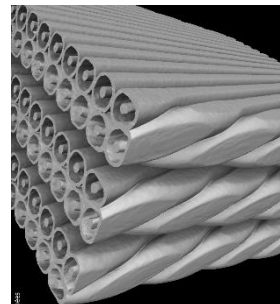
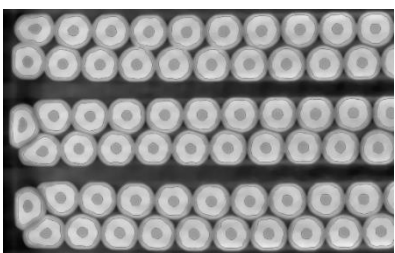


Tomographies performed @ MATEIS lab. INSA Lyon



■ On-going analysis

- Imaging of FRESCA2 10-stack & HF/LF R2D2 conductors
- Quantitative comparison with facets from cabling

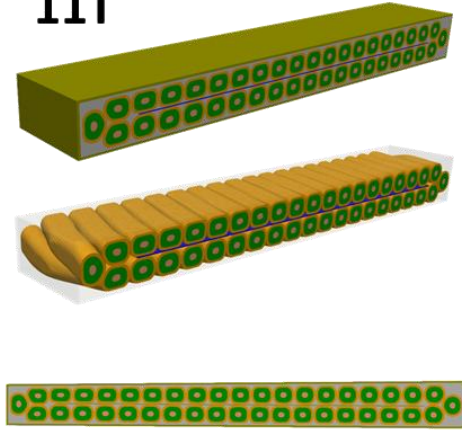


Tomographies courtesy of G. Touzé, CEA Paris-Saclay, DES/ISAS/DRMP

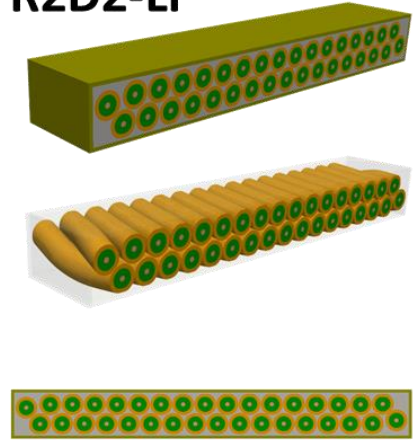




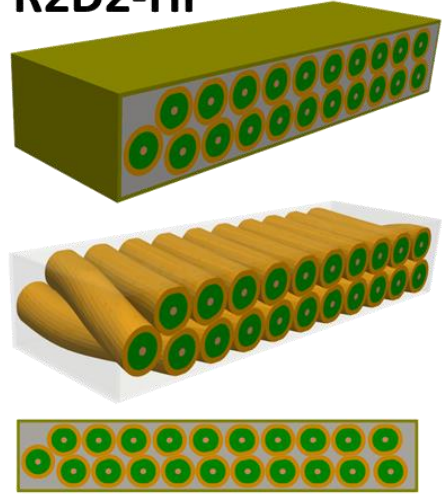
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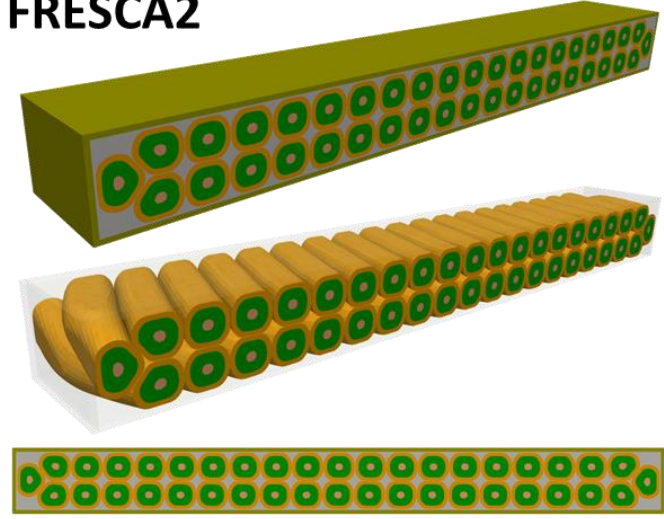
R2D2-LF



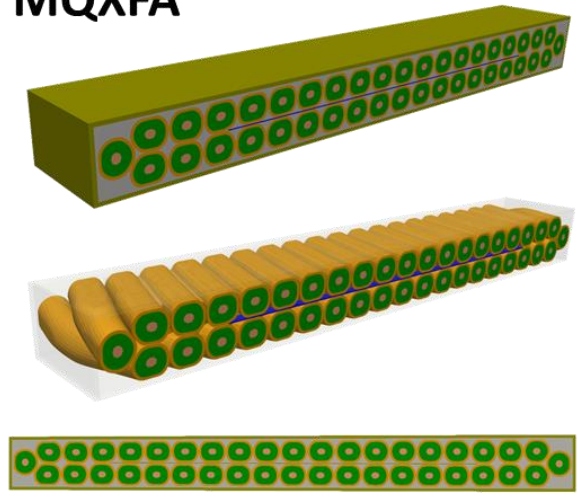
R2D2-HF



FRESCA2



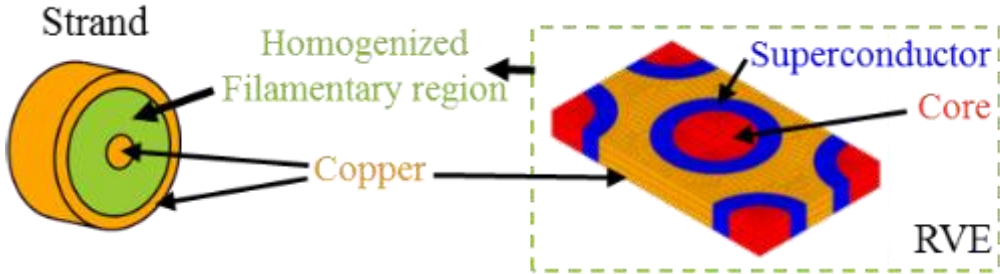
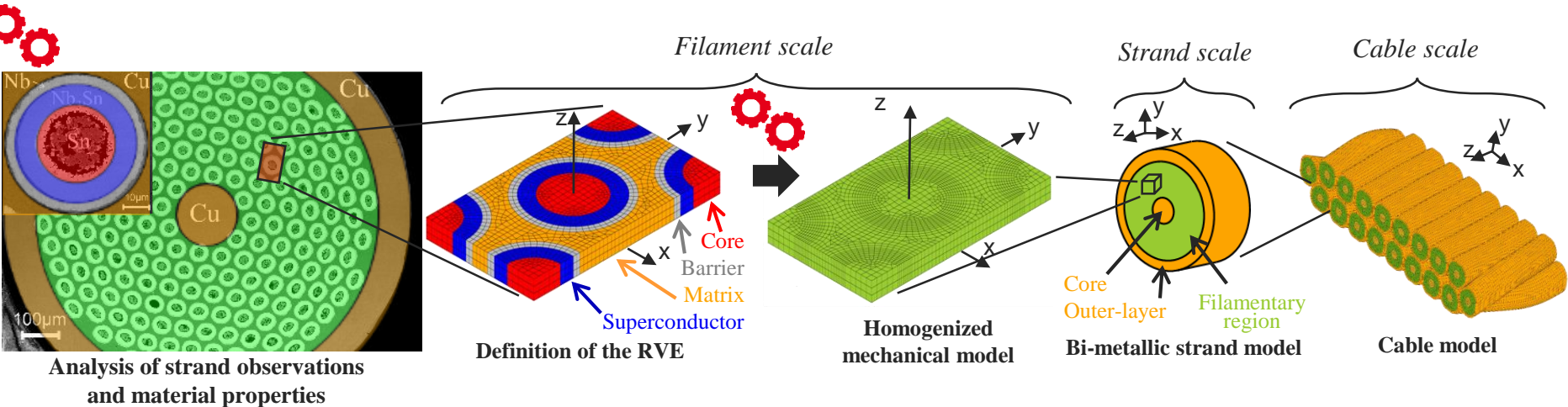
MQXFA



# CoCaSCOPE – Behavior Representation

## Methodology to build the bi-metallic representation

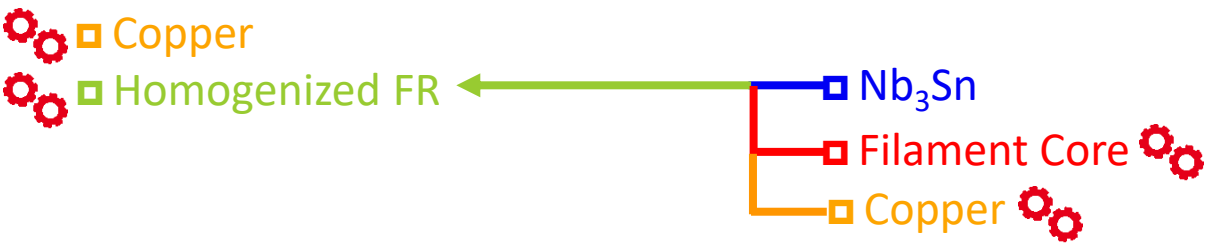
G. Lenoir, IEEE TAS 2019



*Defined by mechanical characterization & image analysis*

■ Strand scale

■ RVE scale



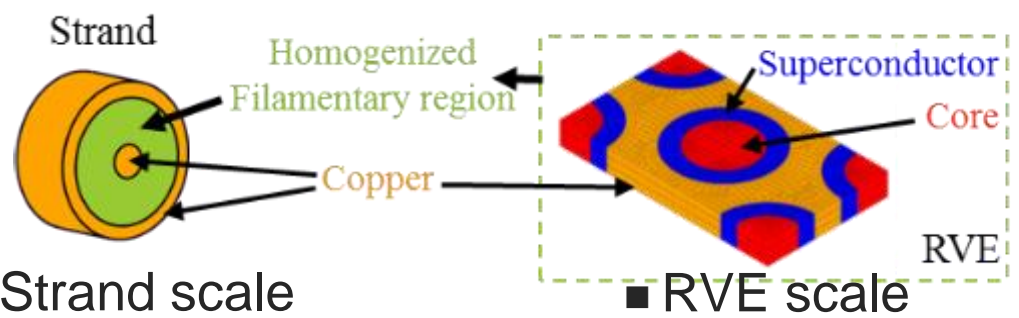


# CoCaSCOPE – Behavior Representation Methodology to build the bi-metallic representation 2/2



## Single material model

- Von Mises yield criterion  $f(\sigma, X, R)$
- Elasticity with Hooke's law:  $\sigma = E * \varepsilon$
- Chaboche's model:
  - Isotropic:  $\dot{R} = b * (Q - R) * \dot{p}$
  - Kinematic:  $\dot{X} = C * \dot{\varepsilon}^p - \gamma * X * \dot{p}$
- Choices & assumptions
  - Based on tensile test  $\Rightarrow R = 0$  for Nb<sub>3</sub>Sn strands
  - ↳ Only one kinematic hardening (simple representation)
  - ↳ Possibility to add several kinematic hardenings (better representation of non-linearities, Ratchetting and shakedown effects, etc.)



*Defined by mechanical characterization & image analysis*

□ Copper  $\Rightarrow$  Elasto-plastic with hardening

$$E_{Cu}, \nu_{Cu}, \sigma_{yCu}, C_{Cu}, \gamma_{Cu}$$

□ Homogenized FR

$\Rightarrow$  Elastio-plastic bilinear (in simulation dir.)

$$E_{zz}^{eff}, \nu_{zz}^{eff}, \sigma_{yzz}^{eff}, K_{zz}^{eff}$$

□ Nb<sub>3</sub>Sn  $\Rightarrow$  Elastic -  $E_{SC}, \nu_{SC}$

□ Filament Core  $\Rightarrow$  Elastic -  $E_{FC}, \nu_{FC}$

□ Copper  $\Rightarrow$  Elasto-plastic with hardening

$$E_{Cu}, \nu_{Cu}, \sigma_{yCu}, C_{Cu}, \gamma_{Cu}$$

$\Rightarrow$  Parameters identify by direct measurements & inverse identification

# Simulation of single stack - Model description

## ■ FReSCa2 cable model

## ■ Materials parameters

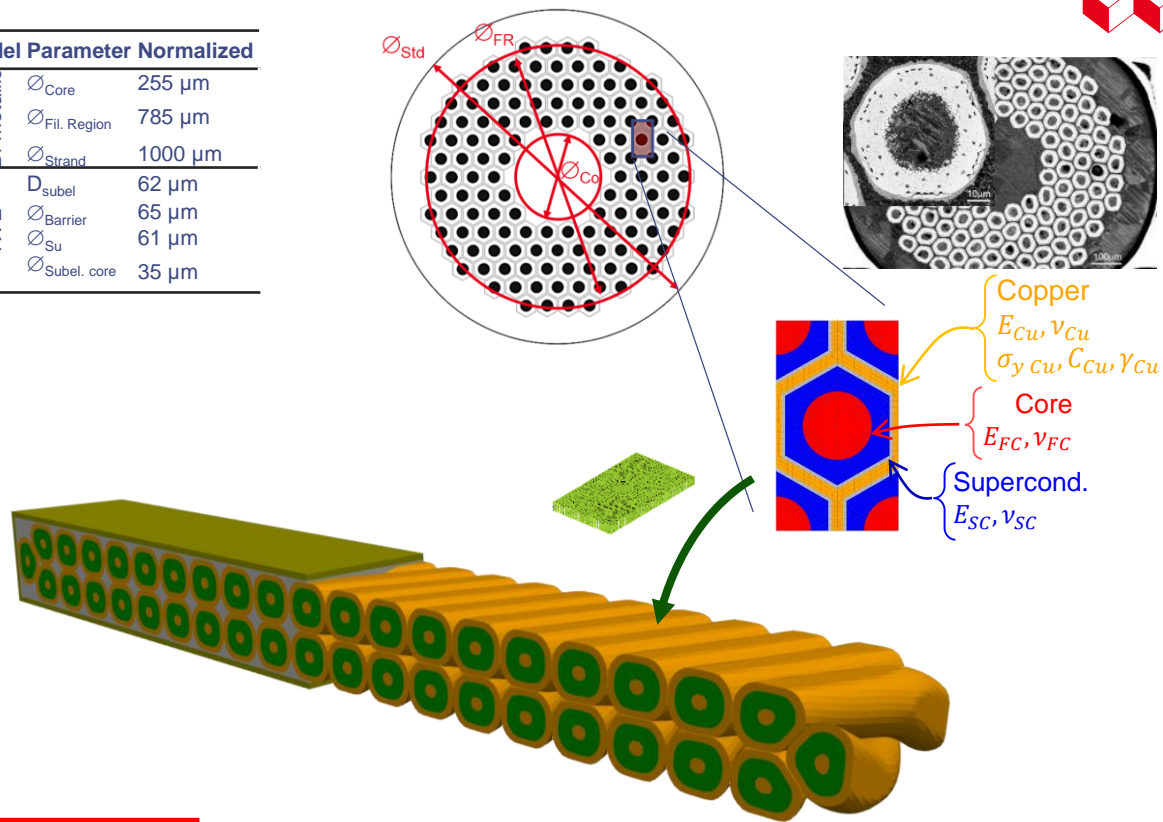
### □ Stack scale

- Impregnated insulation – elastic  
 $E_{in} = 13 \text{ GPa}$  and  $\nu_{in} = 0.35$  [Vallone 18] [Löffler 18]
- Impregnation resin – elastic  
 $E_{re} = 4 \text{ GPa}$  and  $\nu_{re} = 0.35$  [Scheuerlein 19], [Sun 22]  
 + test of a value of  $E_{re} = 1 \text{ GPa}$

### □ Strand scale

- Copper & Barrier → elasto-plastic
  - $E_{Cu} = 129 \text{ GPa}$ ,  $\nu_{Cu} = 0.33$ ,  $\sigma_y = 39 \text{ MPa}$
  - Non-linear kinematic hardening (Chaboche)  
 $\dot{X} = C * \dot{\epsilon}^p - \gamma * X * \dot{p}$   
 with  $C_{Cu} = 35960 \text{ MPa}$  and  $\gamma_{Cu} = 310$   
 ↳ identified on PIT 191 strand [Lenoir 19]
- Superconductor → elastic
  - $E_{Su} = 170 \text{ GPa}$ ,  $\nu_{Su} = 0.3$  [Lenoir 17]
  - $E_{Su} = 129 \text{ GPa}$ ,  $\nu_{Su} = 0.3$  [Scheuelein 15]
- Sub-element core → elastic  
 $E_{Co} = 3; 50; 100 \text{ GPa}$

Model Parameter Normalized		
Bi-metallic	$\varnothing_{Core}$	255 $\mu\text{m}$
	$\varnothing_{Fil. Region}$	785 $\mu\text{m}$
	$\varnothing_{Strand}$	1000 $\mu\text{m}$
RVE	$D_{subel}$	62 $\mu\text{m}$
	$\varnothing_{Barrier}$	65 $\mu\text{m}$
	$\varnothing_{Su}$	61 $\mu\text{m}$
	$\varnothing_{Subel. core}$	35 $\mu\text{m}$



## ■ Strand models

### □ Homogeneous

- Bi-linear mechanical model fitted from tensile test at 300 K
- kinematic linear hardening with  $H = \frac{E_T * E}{E - E_T}$

### □ Bi-metallic – simulations with 3 families of RVE

- RVE with  $E_{Su} = 170 \text{ GPa}$
- RVE with  $E_{Su} = 129 \text{ GPa}$
- Bimet-Vallone based on [Vallone 18]
  - Copper as bilinear  $E_{Cu} = 110 \text{ GPa}$ ,  $\sigma_y = 40 \text{ Mpa}$ ,  $E_T = 5 \text{ GPa}$
  - Filamentary region described as  $\text{Nb}_3\text{Sn}$  and matrix with  $E = 100 \text{ GPa}$

## Stack scale simulations with various mechanical descriptions

Scale	Component	E [GPa]	$\sigma_y$ [MPa]	Plastic
Strand	Copper	129 / 110	39 / 40	Chaboche / $E_T = 5 \text{ GPa}$
	Supercond.	170 / 129	-	-
	Subel. Core	3 / 50 / 100	-	-
Stack	RVE	74 / 62 / 100	24 / 23	$E_T = 32 / 28 \text{ GPa}$
	Impregnation	4 / 1	-	-
	Insulation	13	-	-



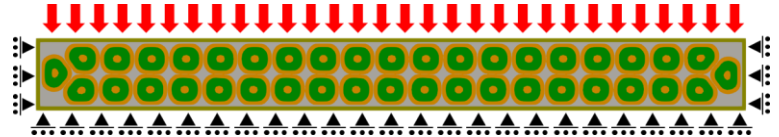
# Simulation of single stack

## Impact of boundary conditions

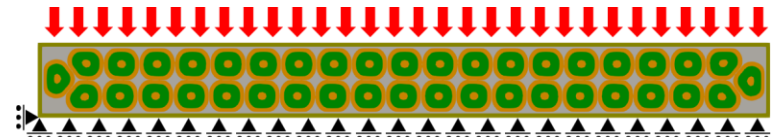


- Boundary conditions

- Blocked sides



- Free sides

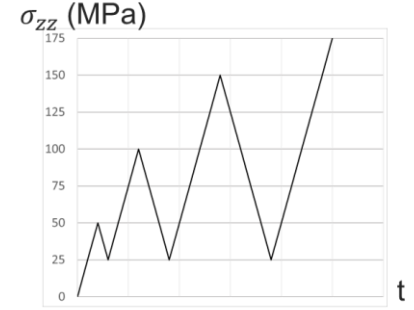


- Mechanical descriptions

Scale	Component	E [GPa]	$\sigma_y$ [MPa]	Plastic
Strand	Copper	129	39	Chaboche
	Supercond.	170	-	-
	Subel. Core	3	-	-
Stack	RVE	74	23	$E_T=32\text{GPa}$
	Impregnation	4	-	-
	Insulation	13	-	-

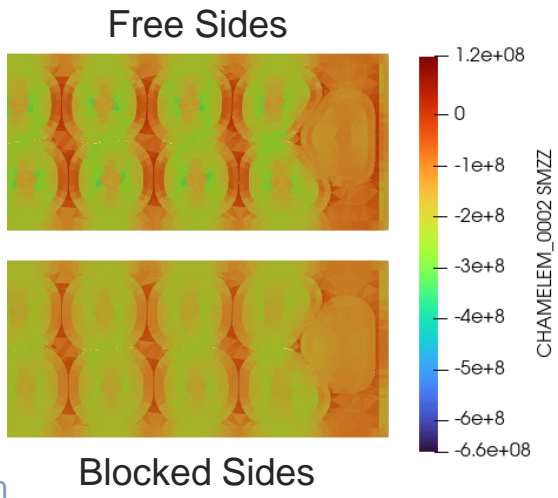
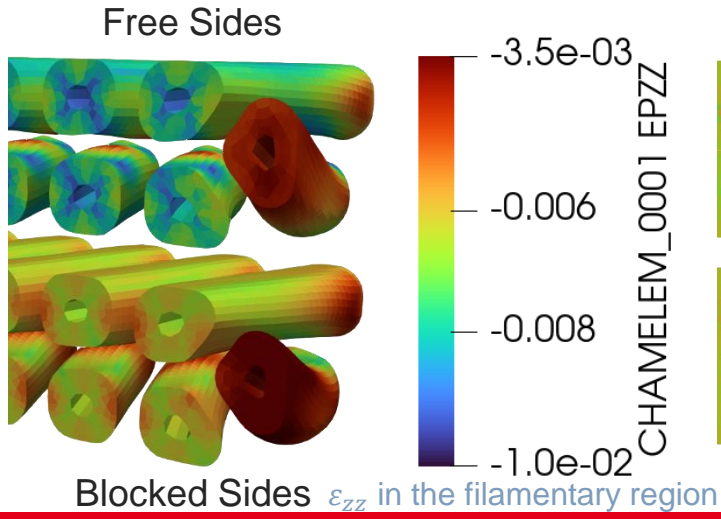
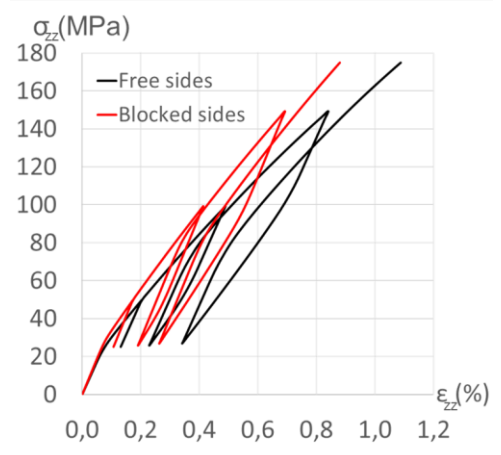
- Loading

- ↳ Monotonic with unloads



→ BCs directly impact the global and the local mechanical values

- Results





# Simulation of a single stack

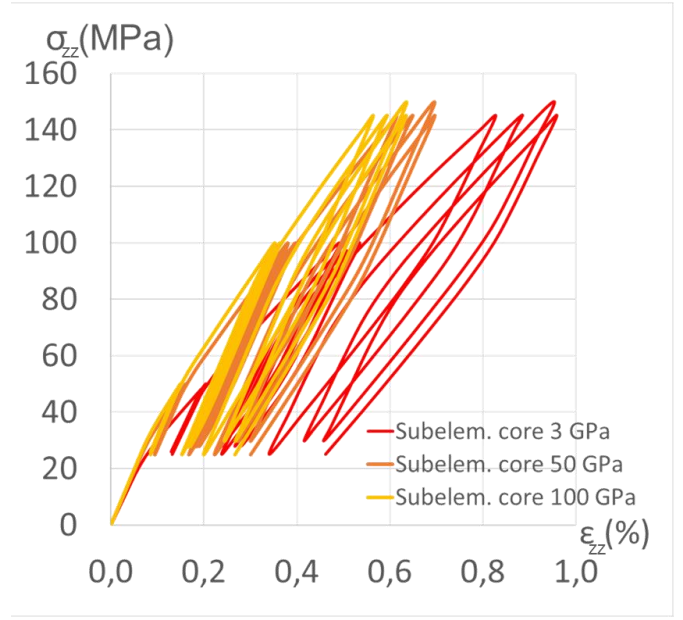
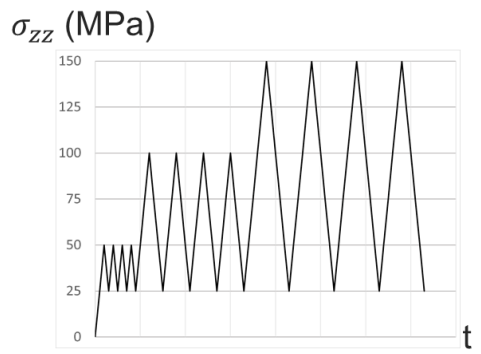
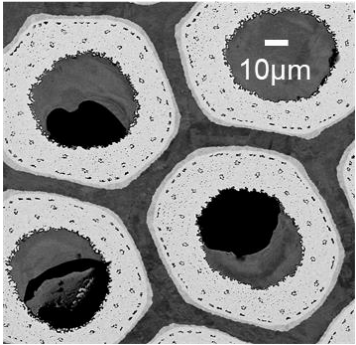
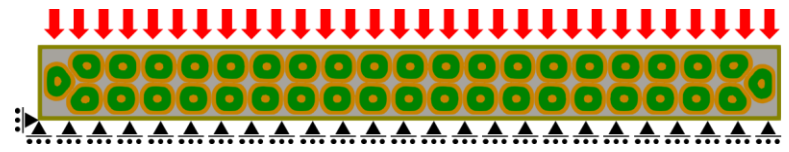
## Impact of $E_{\text{subel. core}}$

### BCs

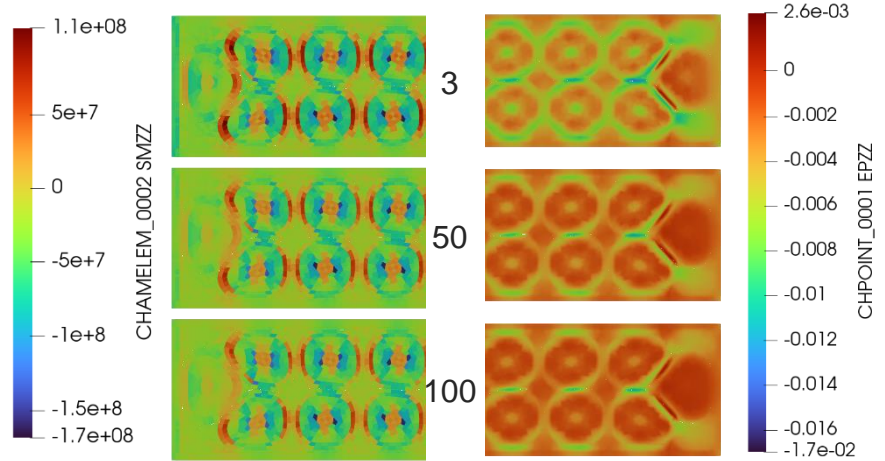
- Free sides
- (Pseudo)-cyclic
  - Increasing unload level
  - 4 cycles / level

### Mechanical description

Scale	Component	E [GPa]	$\sigma_y$ [MPa]	Plastic
Strand	Copper	129	39	Chaboche
	Supercond.	170	-	-
	Subel. Core	3/50/100	-	-
Stack	RVE	74/110/133	24/38/45	$E_T=32/62/76$ GPa
	Impregnation	4	-	-
	Insulation	13	-	-



### Results



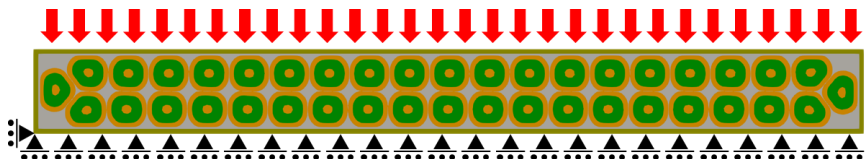
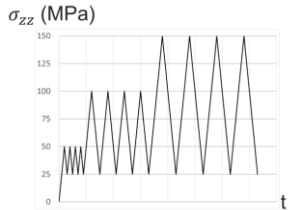
➔ The core of the RRP's subelement require characterization as it can have a large impact on the mechanical behavior of the stack



# Simulation of a single stack

## Comparison of various mech. models

- BCs
  - Free sides
  - (Pseudo-)cyclic
    - Increasing unload level
    - 4 cycles / level



### Mechanical description

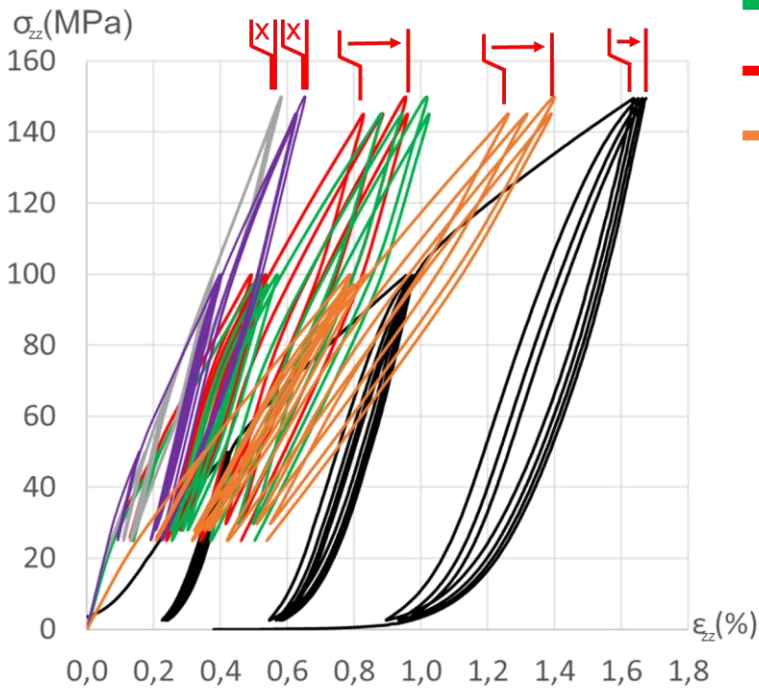
- Homog.
  - $E=127$  GPa,  $\nu=0,36$ ,
  - $\sigma_y=25$  Mpa,  $E_T=47$  Gpa

Scale	Component	E [GPa]	$\sigma_y$ [MPa]	Plastic
Strand	Copper	129 / 110	39 / 40	Chaboche / $E_T=5$ GPa
	Supercond.	170 / 129	-	-
	Subel. Core	3	-	-
Stack	RVE	74 / 62	24 / 23	$E_T=32 / 28$ GPa
	Impregnation	4 / 1	-	-
	Insulation	13	-	-

### Results

Stack equivalent parameters derived from curves

	$E^{eq}$ GPa	$\sigma_y^{eq}$ MPa	$E_T^{eq}$ GPa
10-stack test	38,7	40	8.3
Homog.	38,9	18	24,6
Vallone	39,1	30	20
Esu(129)/Eco(3)	33,1	36	16,6
Esu(171)/Eco(3)	34,6	35	17,5
Esu(171)/Eco(3) + Ere(1)	17,5	30	11,6



- 10-stack test
- Homog.
- Vallone
- $E_{Su}(129)/E_{Co}(3)$
- $E_{Su}(170)/E_{Co}(3)$
- $+ E_{Re}(1)$



# Summary

## ■ Results of simulation

- Conditions of the simulation has a direct impact
  - ↳ BCs, monotonic/cyclic, 2D / 3D
- Accurate mechanical properties are required to build robust and predictive models
- Adapted mechanical descriptions have to be used to reproduce the observed behavior
  - ↳ non linearities / accumulation of strain / damage

## ■ Characterization

- 10-stack campaign
  - ↳ More data for model comparison
  - ↳ Understanding of experimental artefact and representativeness of 10-stack tests for coil behavior
- Strand scale
  - Core behavior
  - Homogenization scheme
  - Transverse compressive tests & model comparison

## ■ CoCaSCOPE

- Access to the different entities of the stack
- Access to various parameters in any geometrical configuration
  - useful to understand the behavior
- Implementation of various mechanical models
- Can be used with any Finite Element code

➔ Mesh Generator available for the community to generate any kind of model!



# Outline

## 1. Characterization and modeling program for Nb<sub>3</sub>Sn conductors @ CEA Paris-Saclay

## 2. CoCaSCOPE

Mesh Generator

Behavior representation

Experimental characterization

Single stack simulations

## 3. Summary and perspectives



# Overview of CEA's Nb<sub>3</sub>Sn modeling program

Magnet scale

Model

Experimental

Electromag. & mechanical

FReSCa2

High Field "HF" Low Field "LF"

F2D2

Electromag. & mechanical

FReSCa2 test @ CERN

SD program

Cable scale

Meshed numerical model

Cable and stack simulation

Numerical twin of stack test

HT dilatation Unreacted or reacted cable behavior Cracks and electromag. perf.

DIC in-situ

Hard bending 10-stack Layer jump

+ Characterization under elementary loadings (Transverse / bending)

Impact of transverse pressure on a double stack @ CERN

Strand scale

Diffusion Mechanical

Semi-analytical diffusion model

Detailed and bi-metallic strand models

Core Outer-layer Filamentary region

HT dilatation Mechanical

DIC in-situ

Tensile test

+ Characterization under elementary loadings (Transverse / bending)

Subelement scale

Diffusion Mechanical

Semi-analytical diffusion model

Homogenization of filamentary region

Definition of the RVE

Homogenized mechanical model

Diffusion Local mechanical properties

f<sub>v</sub> during HT

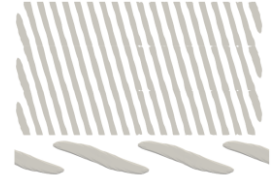
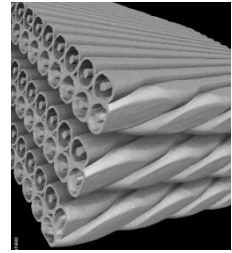
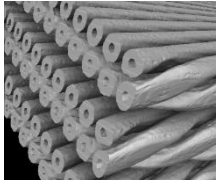
Nano-indentation

+ μ-sample & μ-pillar

# On-going work 11/2023

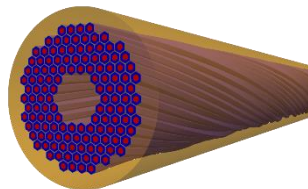
## Comparison of numerical models with real conductors

- ↳ Facets from cabling QC and extracted from model
- ↳ X-ray tomographies
- ↳ Metallographic observations



## Identification of material parameters

- ↳ Tensile data and mechanical representation of other architectures (RRP 108/127 Ø0.7 mm Ø0.85 mm, RRP 132/169 Ø1 mm)
- ↳ Inverse identification using detailed numerical model of strand w/ twisted sub-elements and experimental data



## Thermomechanical

- ↳ Use of thermomechanical semi-analytical model development in cable / stack models
- Following of the PhD of M. Abel-Hafiz*

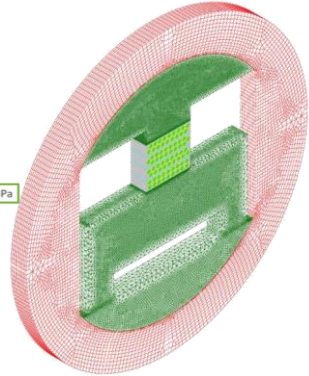
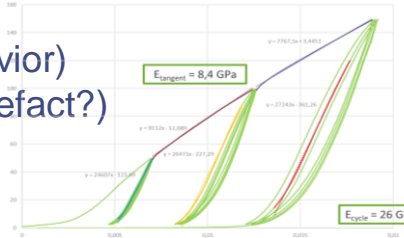
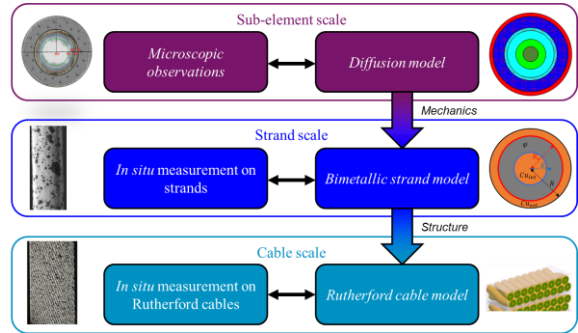
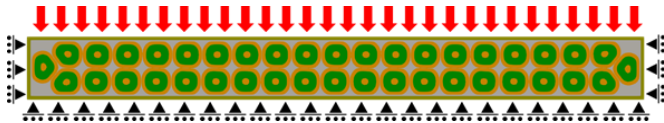


## 10-stack characterization campaign

- Continuity of 10-stack tests @ CEA
- Extend mechanical study (strain rate, hold, unloadings, cyclic behavior)
- ↳ Highly non-linear behavior at low stress (viscosity, experimental artefact?)

## Simulation program

- 10-stack tests (mechanical)
- FRESCA tests (double-stack & fracture)
- Subscale Dipole – SD (coil segment / 5-stack & thermo-mechanic)





irfu

**Merci !**  
**Thank you !**

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 Gilles\_Lenoir