

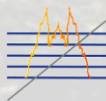
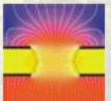
# XVII Conference on Resistive Plate Chambers and Related Detectors

Simulating MRPCs with Garfield++ and time-dependent weighting potentials

Djunes Janssens

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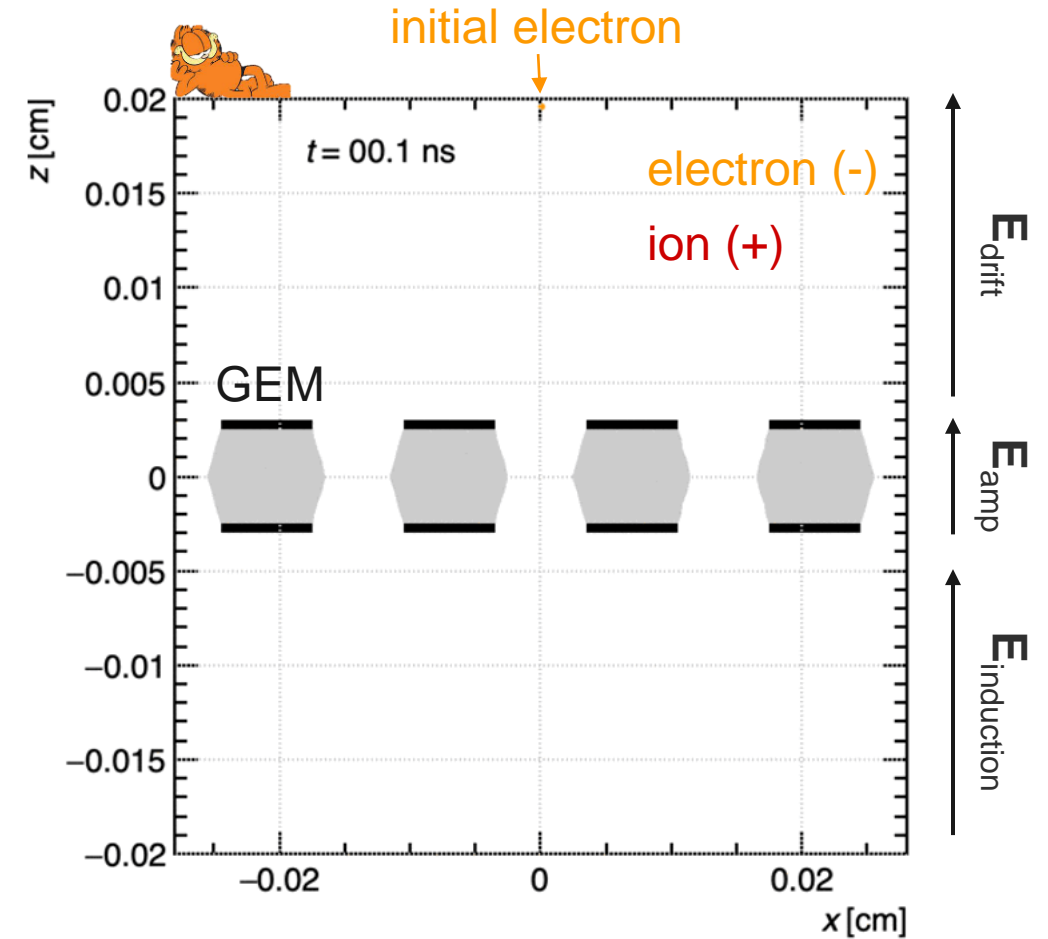
September 12<sup>th</sup>, 2024



# Introduction

## Outline:

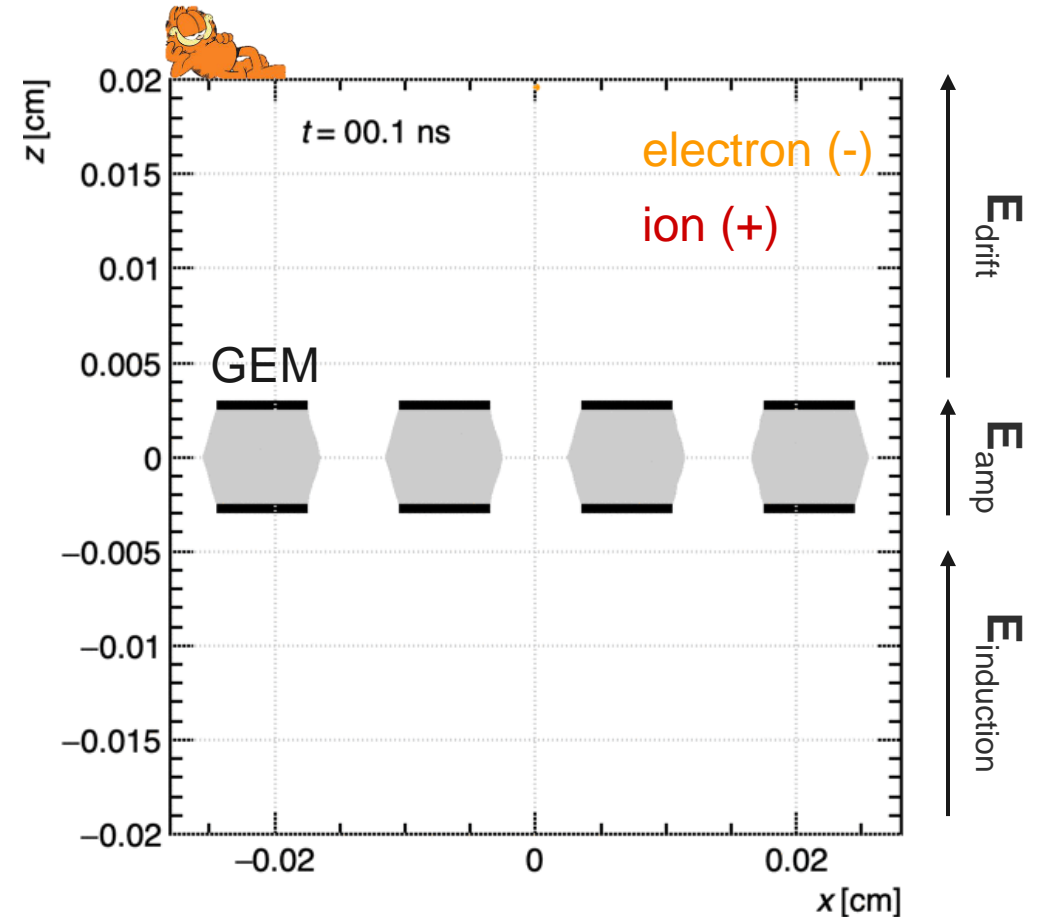
- **Garfield++ MRPC simulation**
  - Grid-based avalanche method
  - Mixed method approach
- **Signal formation**
  - Ramo-Shockley theorem
  - Ramo-Shockley theorem extension for conductive media
  - Weighting potentials and signals in (M)RPCs
  - Signals in the presence of a thin resistive layer
- **Conclusion**



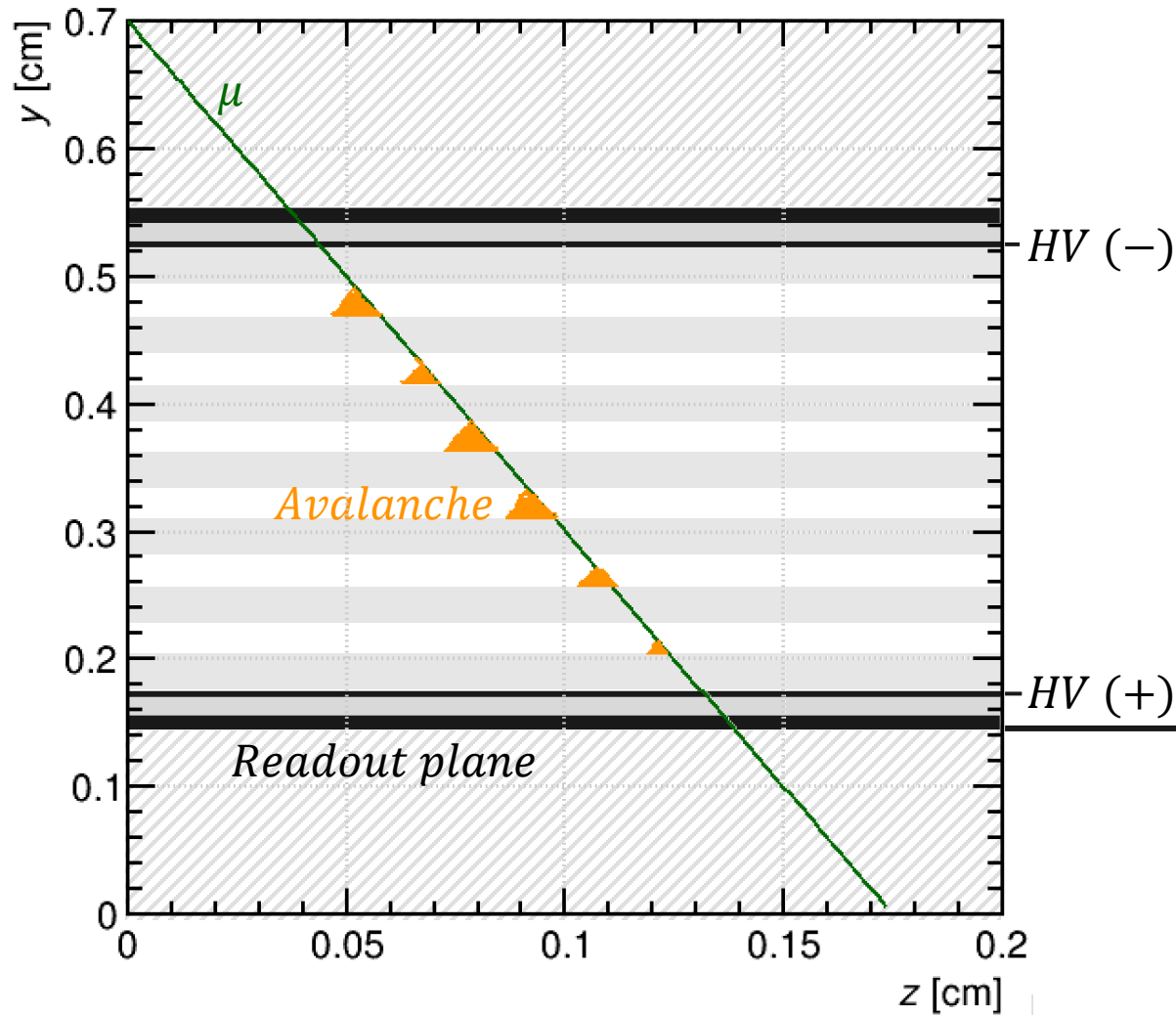
# Introduction

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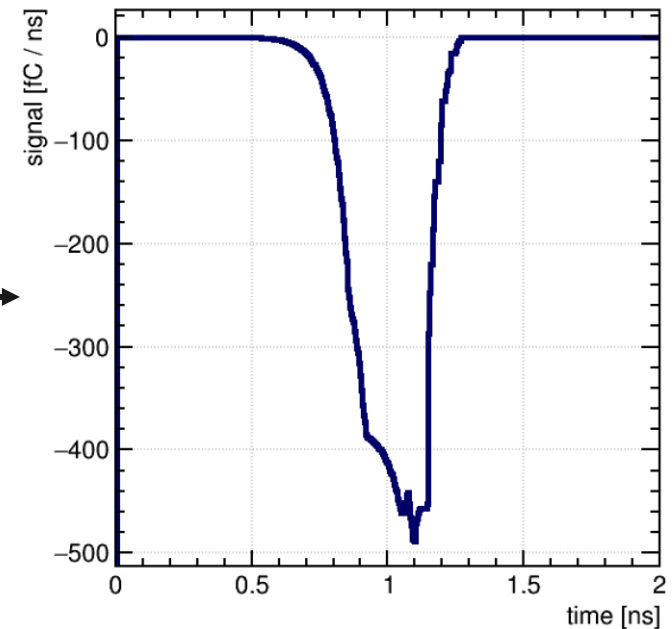


# Introduction



Using Garfield++, electron avalanches can be simulated **microscopically** on a collision-by-collision basis, where we consider the proportional regime of amplification.

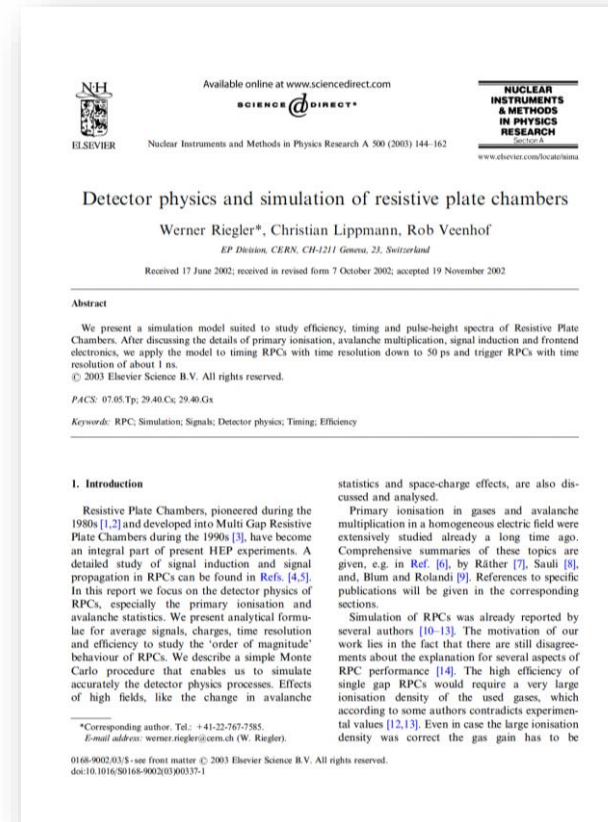
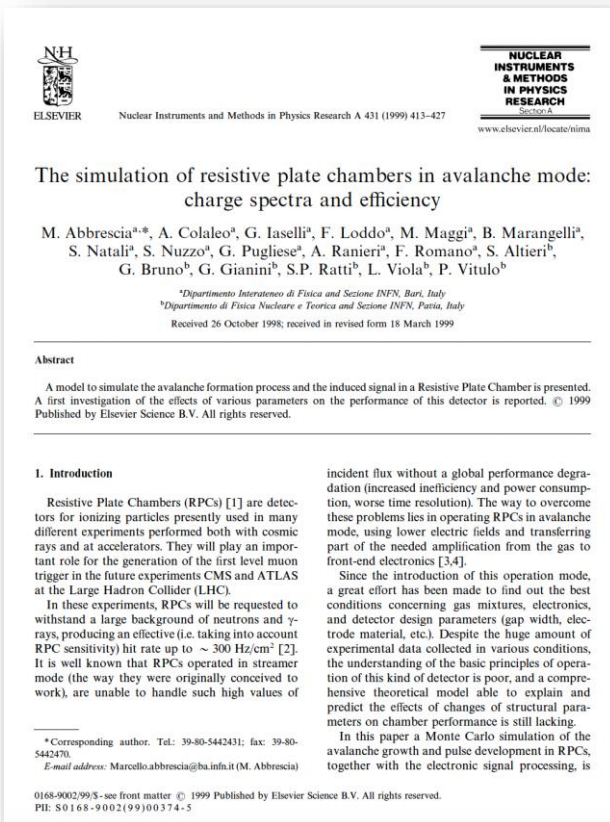
Our goal is to “efficiently” calculate the signal response, including the contribution from resistive materials.



# Grid-based avalanche calculation

# Grid-based avalanche calculation

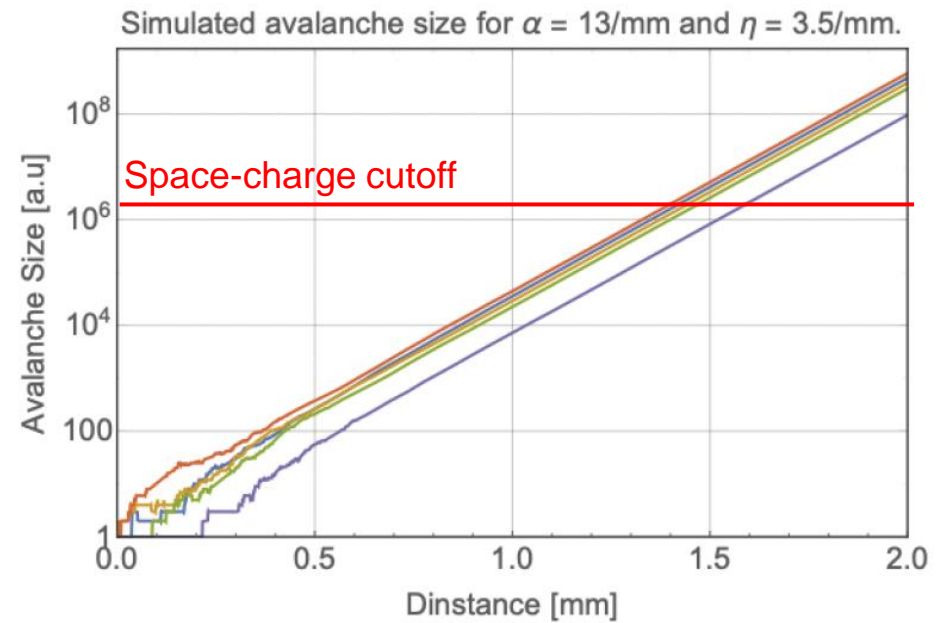
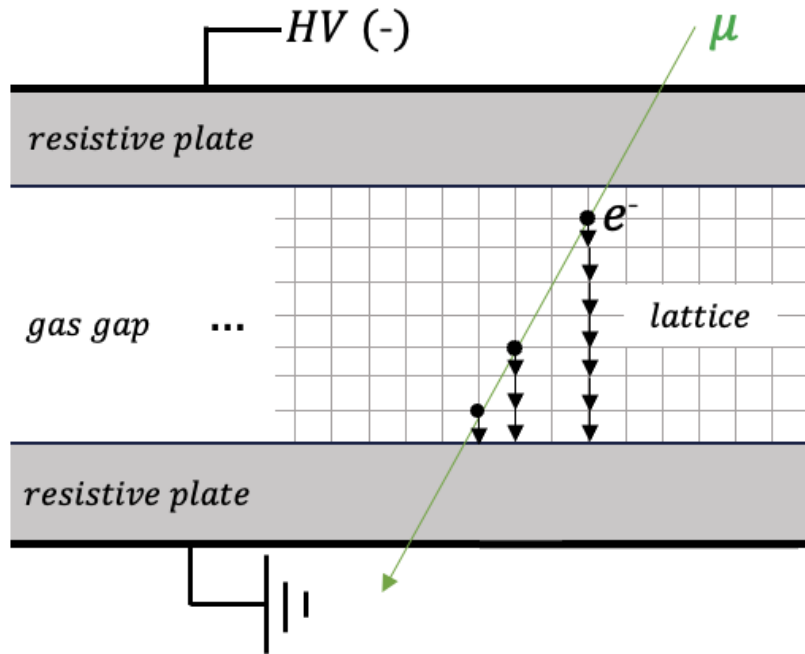
The simulation approach for MRPCs relies heavily on a developed method that provide a one-dimensional description of avalanche dynamics using a grid-based approach.



# Grid-based avalanche calculation

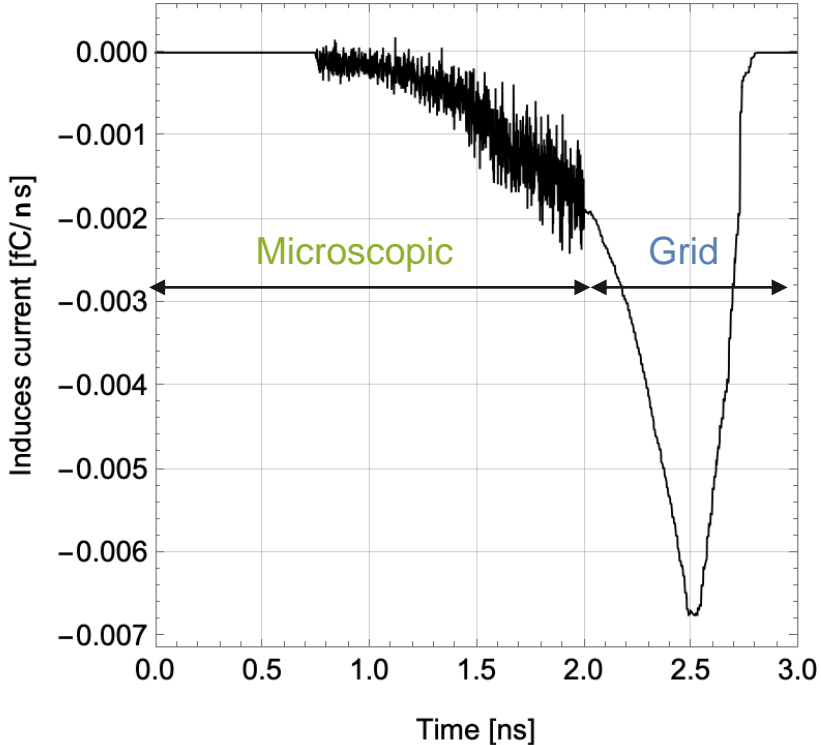
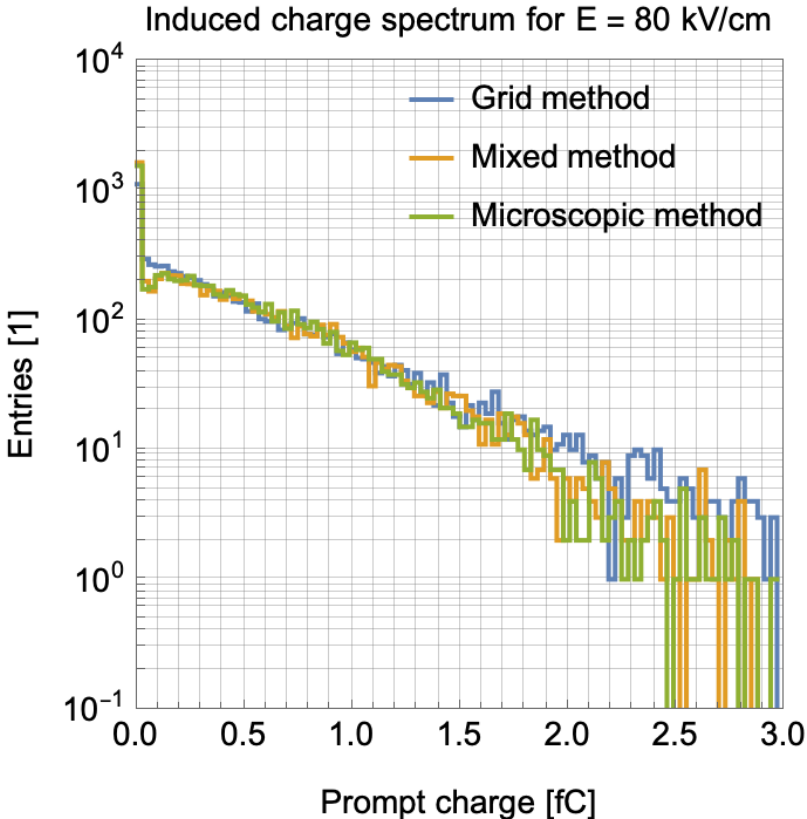
The gas volume is subdivided into a 3D grid, with electrons snapped to the nodes and propagated along the drift direction. The avalanche development is modeled using swarm parameters and the **Legler model**.

To approximate space-charge suppression, growth is capped at  $1.6 \cdot 10^7$  electrons.



# Grid-based avalanche calculation

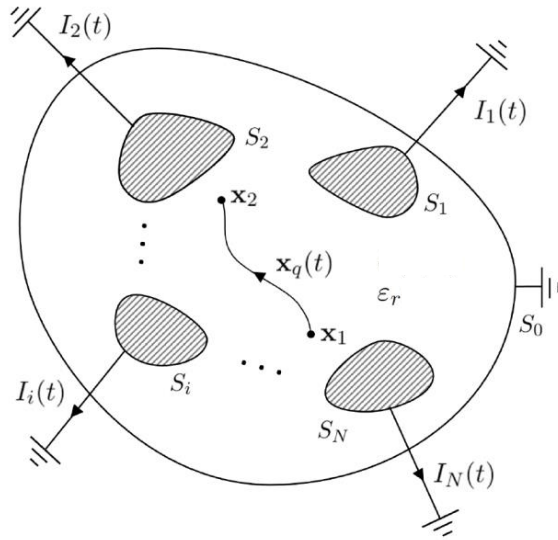
To accurately represent the early fluctuations' impact on the induced charge distribution, **microscopic** tracking in Garfield++ is used. After a set time (~ 50 - 100 electrons), the method switches to the **grid model**, forming a **'mixed method'** approach.





# Ramo-Shockley theorem

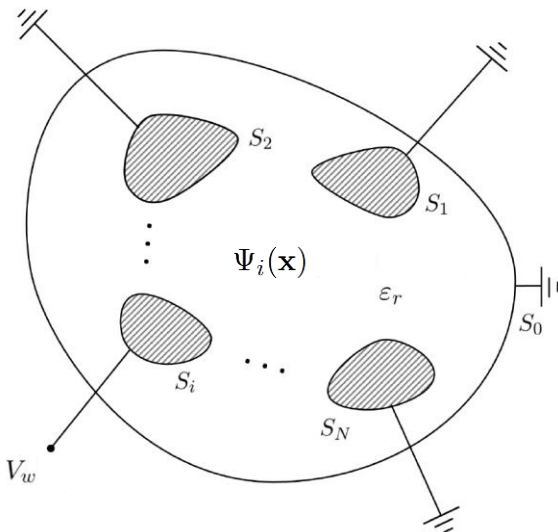
# Ramo-Shockley theorem



The Ramo-Shockley theorem allows the current induced by an externally impressed charge density on any electrode to be calculated using a so-called **weighting potential  $\psi(\mathbf{x})$** .

$$I_i(t) = -\frac{q}{V_w} \mathbf{E}_i(\mathbf{x}_q(t)) \cdot \dot{\mathbf{x}}_q(t)$$

$$\mathbf{E}_i(\mathbf{x}) = -\nabla \Psi_i(\mathbf{x})$$

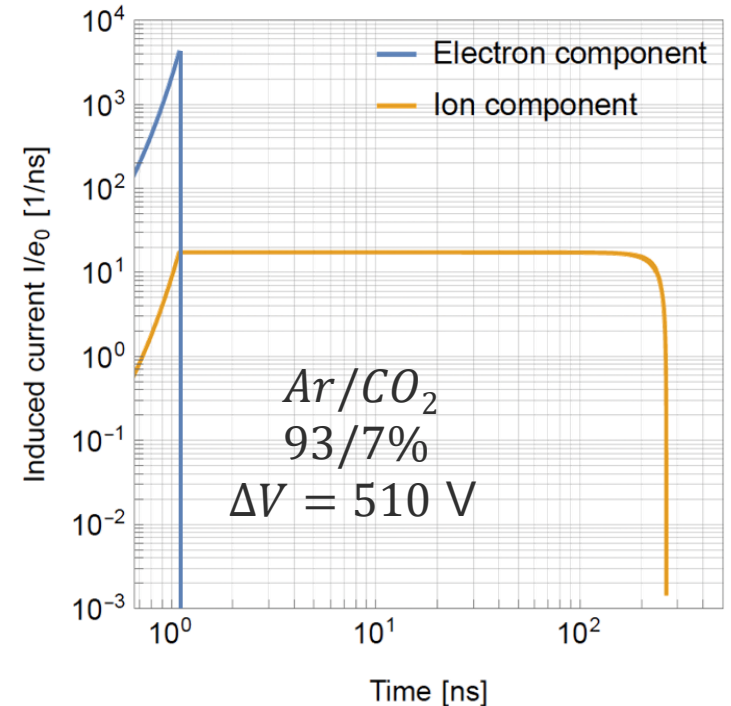
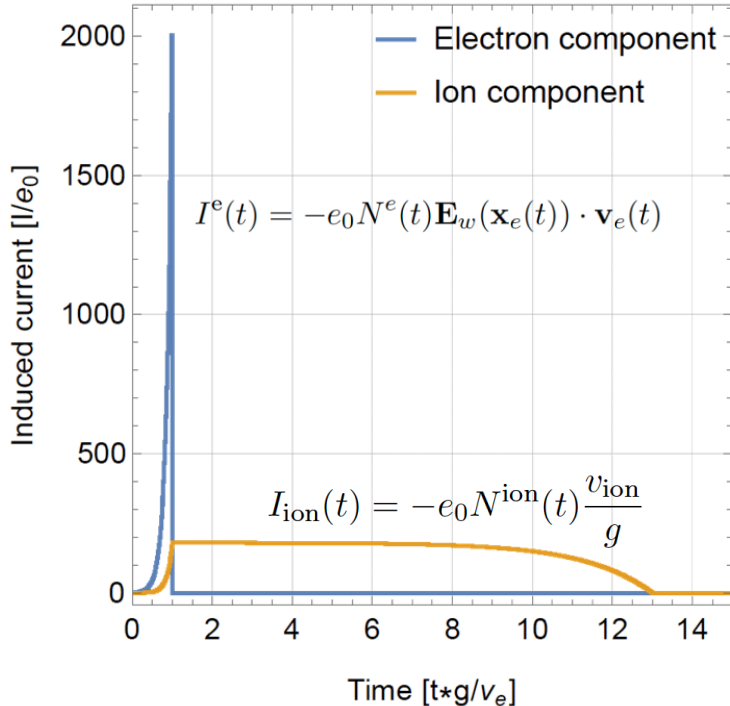
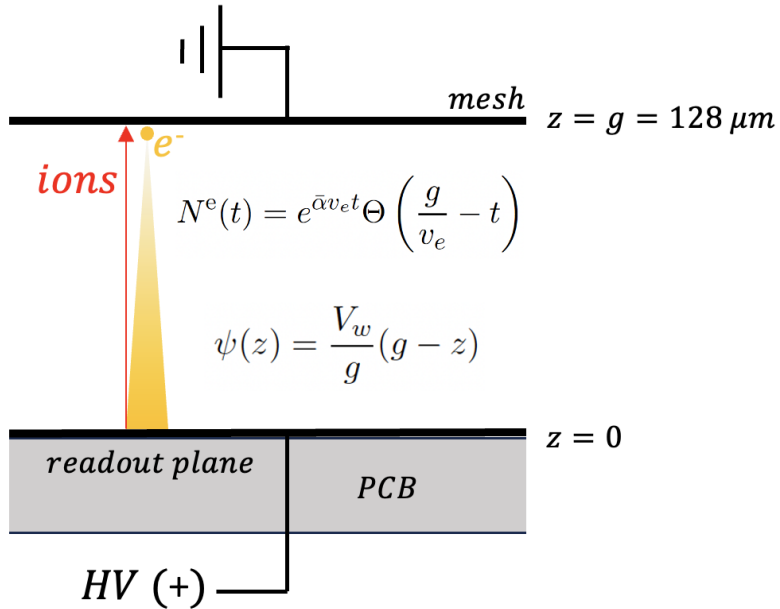


This static  $\psi(\mathbf{x})$  can be calculated for a grounded electrode using the following step:

- Remove the drifting charges
- Put the electrode at potential  $V_w$
- Grounding all other electrodes

# Signal in a non-resistive Micromegas

Let us consider a Townsend avalanche inside the amplification gap of a parallel plate-type detector that induces a signal on the anode plane.



# Ramo-Shockley theorem extension for conducting media

# Ramo-Shockley theorem extension for conducting media

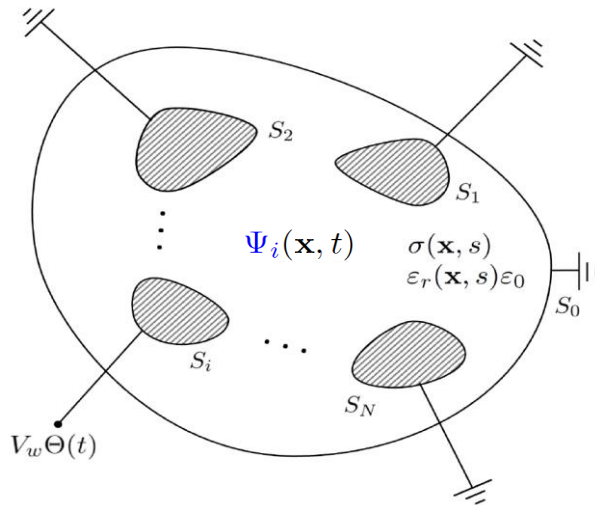
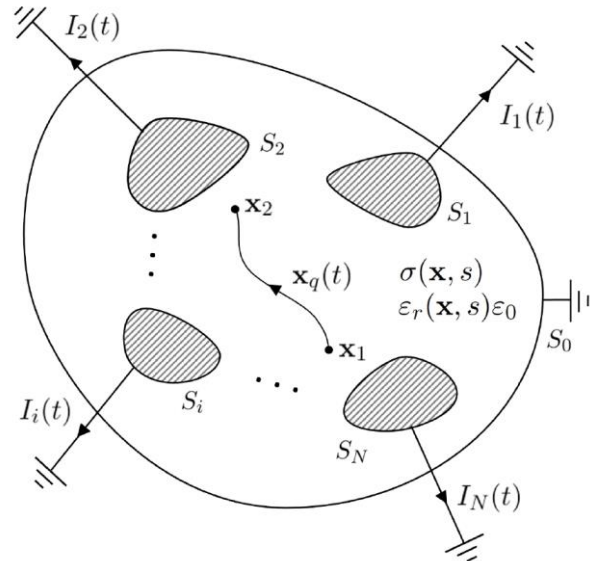
In detectors with resistive elements, signal timing depends on both charge movement in the drift medium and the time-dependent reaction of resistive materials.

$$I_i(t) = -\frac{q}{V_w} \int_0^t \mathbf{H}_i [\mathbf{x}_q(t'), t - t'] \cdot \dot{\mathbf{x}}_q(t') dt'$$

$$\mathbf{H}_i(\mathbf{x}, t) := -\nabla \frac{\partial \Psi_i(\mathbf{x}, t) \Theta(t)}{\partial t}$$

The **dynamic weighting potential**  $\Psi_i(\mathbf{x}, t)$  can be calculated:

- Remove the drifting charges
- Put the electrode at potential  $V_w$  at time  $t = 0$
- Grounding all other electrodes



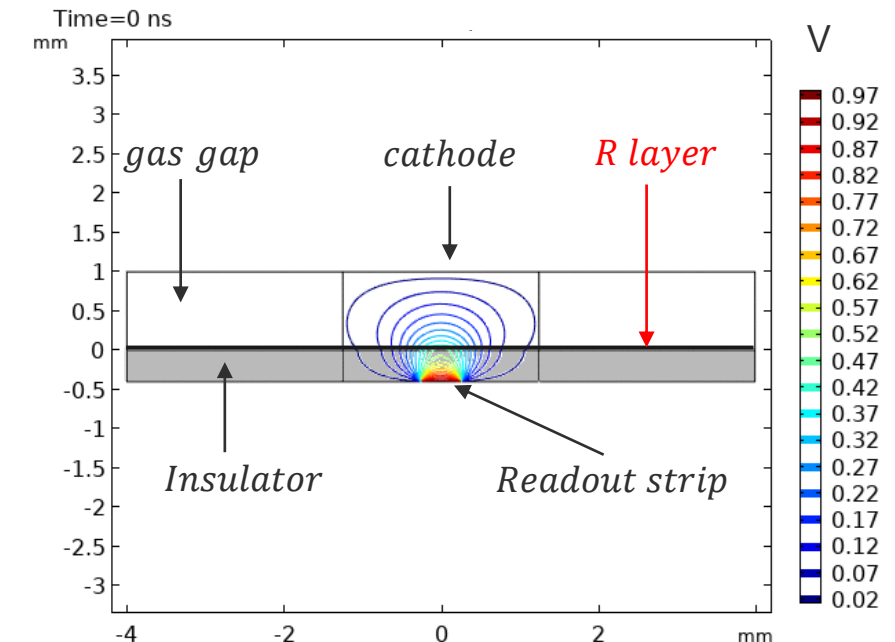
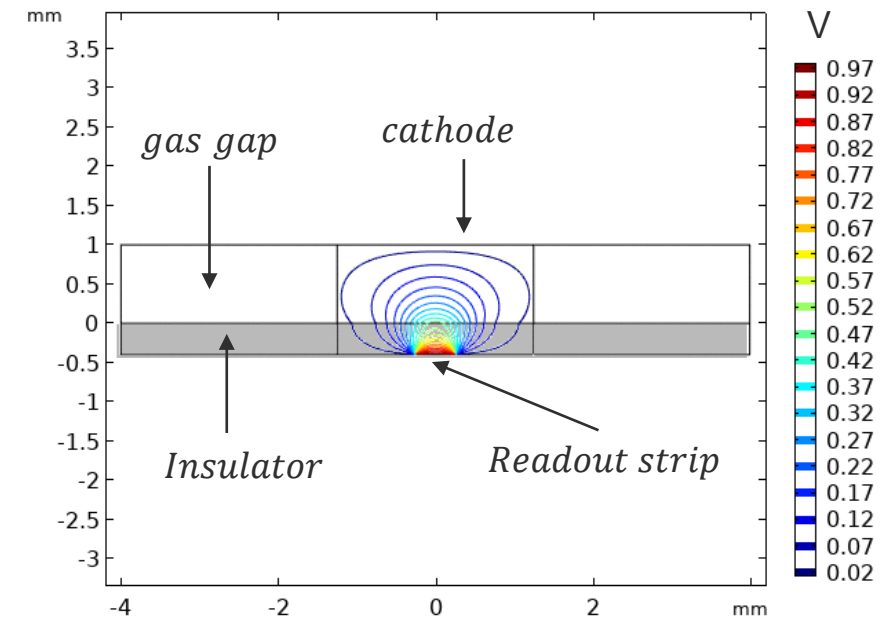
# Ramo-Shockley theorem extension for conducting media

The time-dependent weighting potential is comprised of a static **prompt** and a dynamic **delayed** component:

$$\psi_i(\mathbf{x}, t) \doteq \psi_i^p(\mathbf{x}) + \psi_i^d(\mathbf{x}, t) \quad \text{where} \quad \psi_i^d(\mathbf{x}, 0) = 0$$

The current induced by a point charge  $q$  is given by:

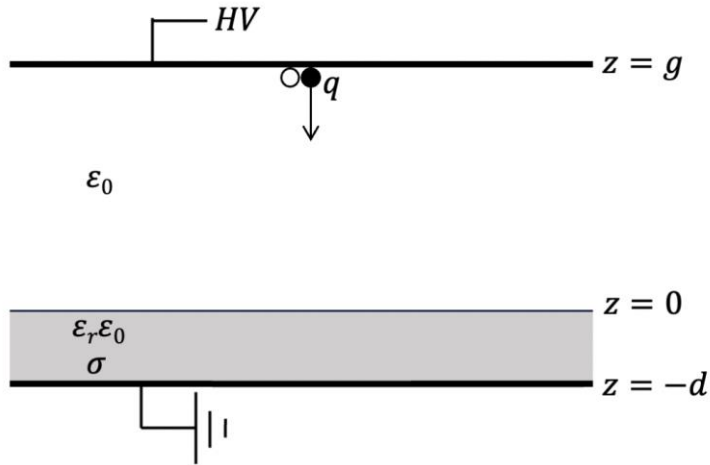
$$I_i(t) = \underbrace{-\frac{q}{V_w} \mathbf{E}_i^p(\mathbf{x}_q(t)) \cdot \dot{\mathbf{x}}_p(t)}_{\text{Direct induction}} - \underbrace{\frac{q}{V_w} \int_0^t dt' \mathbf{H}_i^d[\mathbf{x}_q(t'), t - t'] \cdot \dot{\mathbf{x}}_q(t')}_{\text{Reaction from resistive material}}$$



# Weighting potentials of (M)RPCs

# Delayed component of the signal

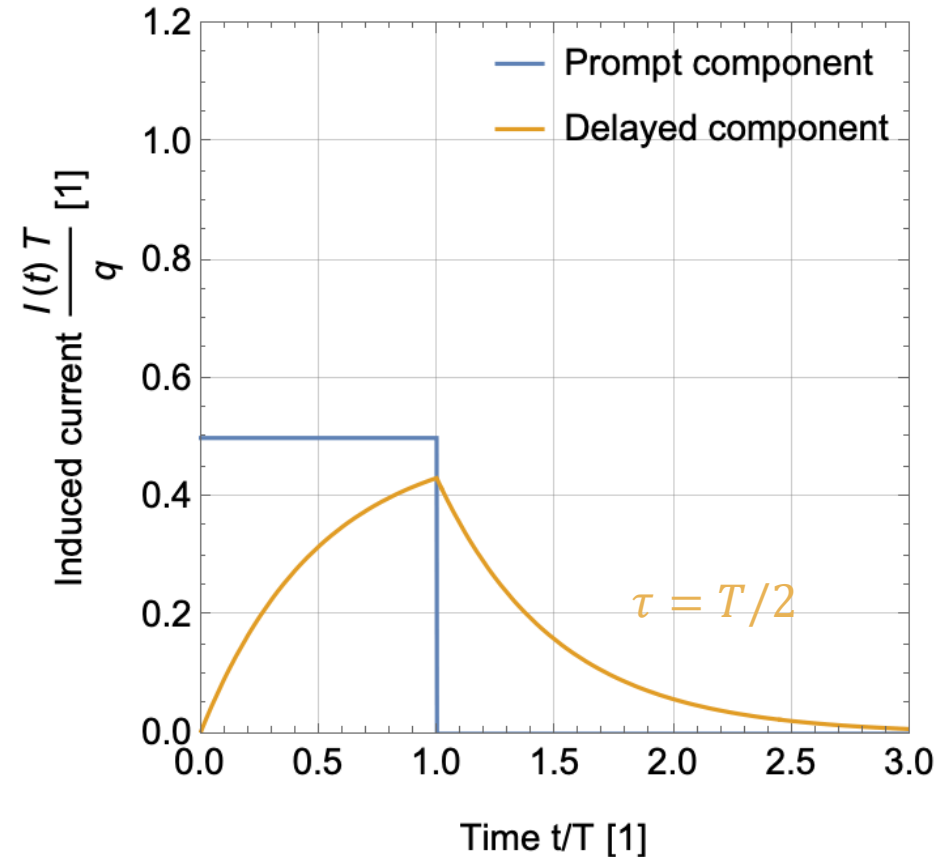
A charge  $q$  moves at a constant velocity through the gas gap before reaching the bulk resistive layer that separates it from the anode.



$$\mathbf{H}(z, t) = \hat{\mathbf{z}} \frac{V_w \epsilon_r}{d + \epsilon_r g} \delta(t) + \hat{\mathbf{z}} \frac{V_w}{g\tau} \frac{d}{d + \epsilon_r g} e^{-t/\tau} \Theta(t)$$

The dynamics is governed by the time constant:

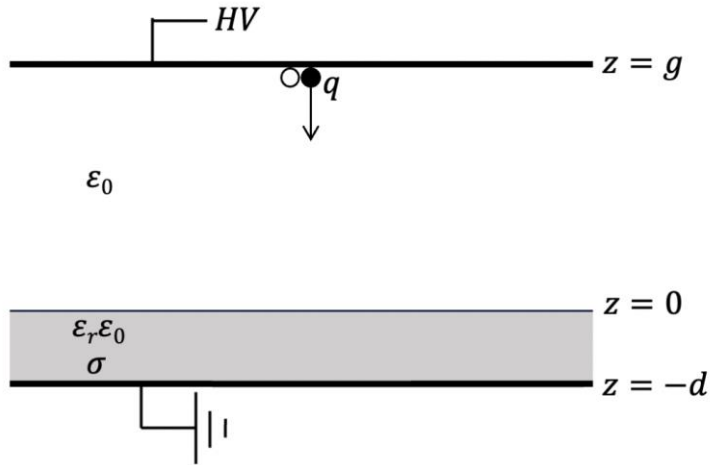
$$\tau := \frac{\epsilon_0}{\sigma} \frac{d + \epsilon_r g}{g}$$





# Delayed component of the signal

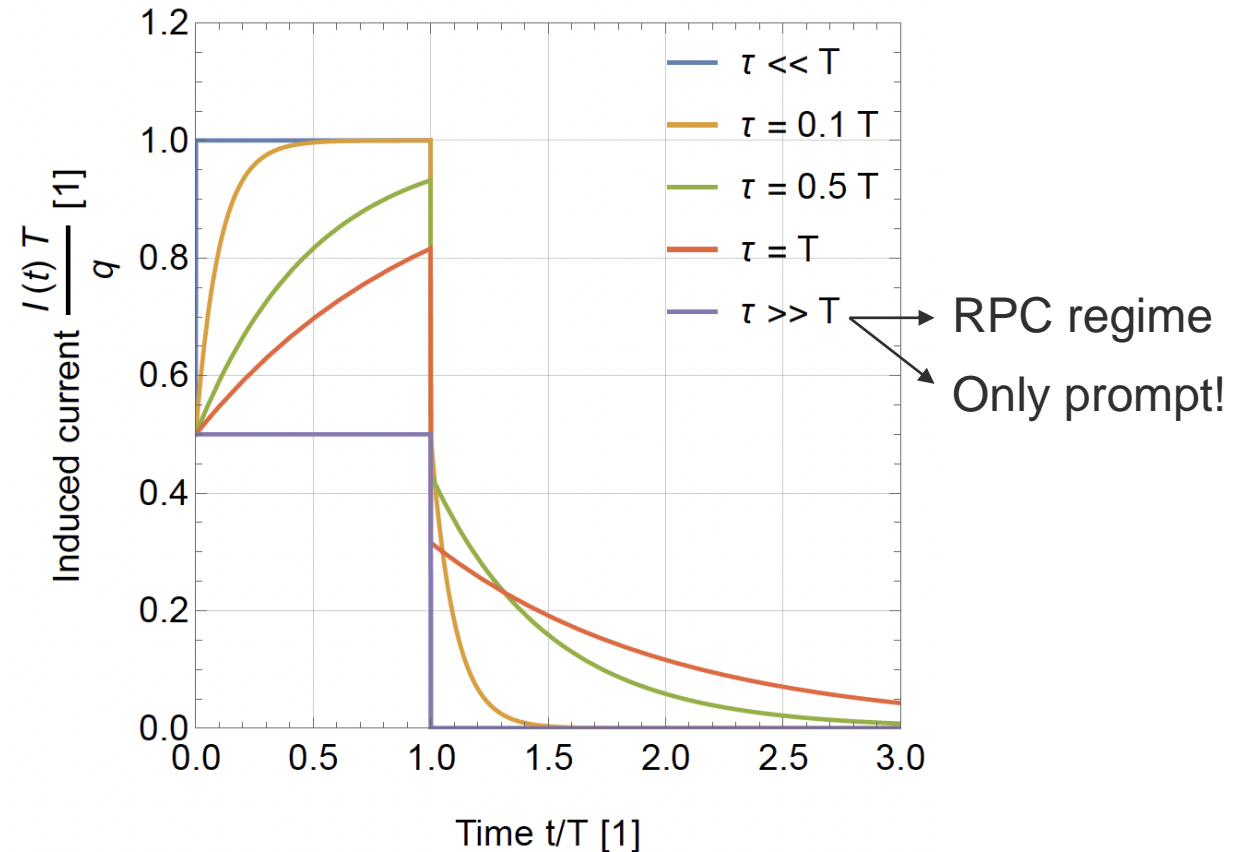
Given the typically high volume resistivities of  $O(10^9 - 10^{12}) \Omega \cdot \text{cm}$  in RPCs, the delayed component is negligible.



$$\mathbf{H}(z, t) = \hat{\mathbf{z}} \frac{V_w \epsilon_r}{d + \epsilon_r g} \delta(t) + \hat{\mathbf{z}} \frac{V_w}{g\tau} \frac{d}{d + \epsilon_r g} e^{-t/\tau} \Theta(t)$$

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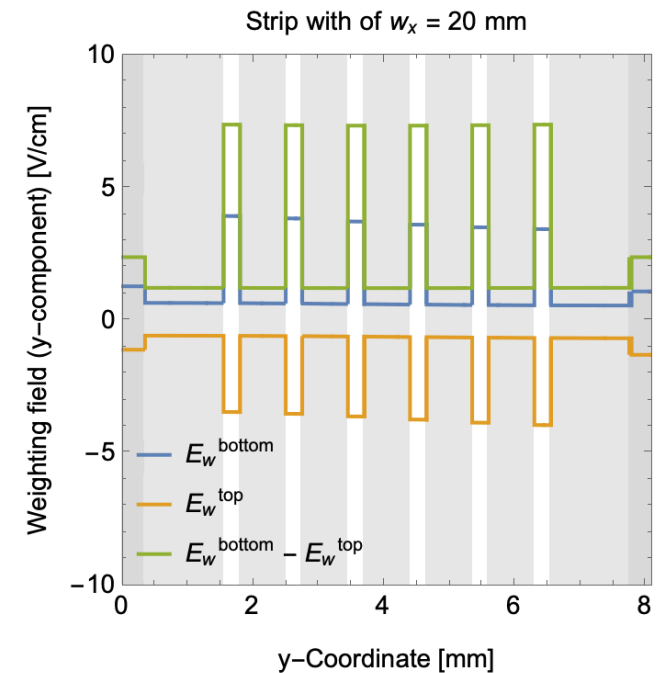
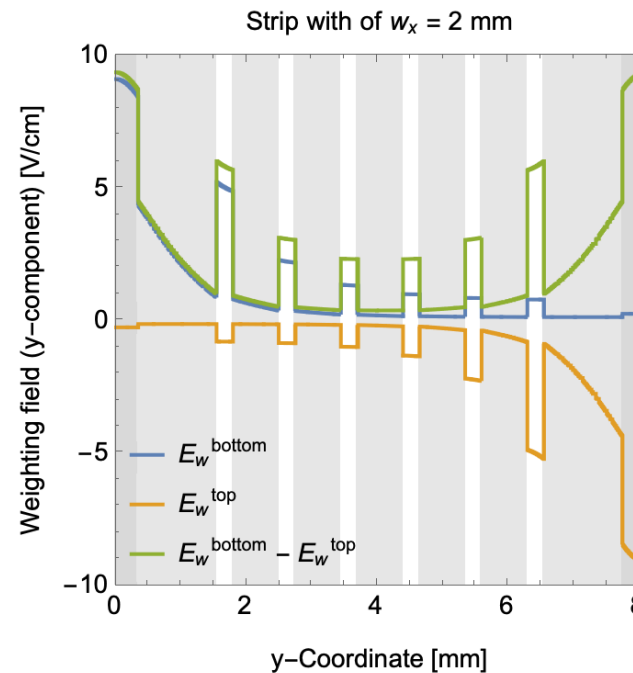
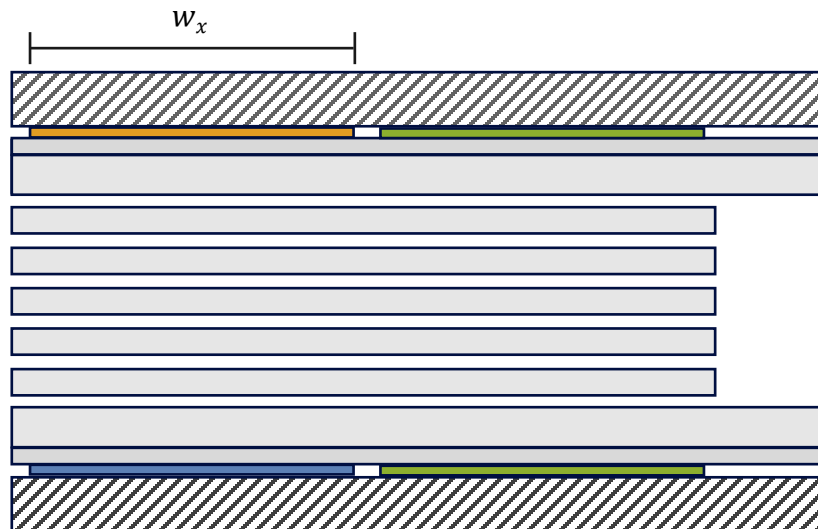
$$\tau := \frac{\epsilon_0}{\sigma} \frac{d + \epsilon_r g}{g}$$



# Weighting potentials of (M)RPCs

The analytical expression for the prompt weighting potential of rectangular electrodes within an N-layer geometry has been implemented in the new 'ComponentParallelPlate' class in Garfield++.

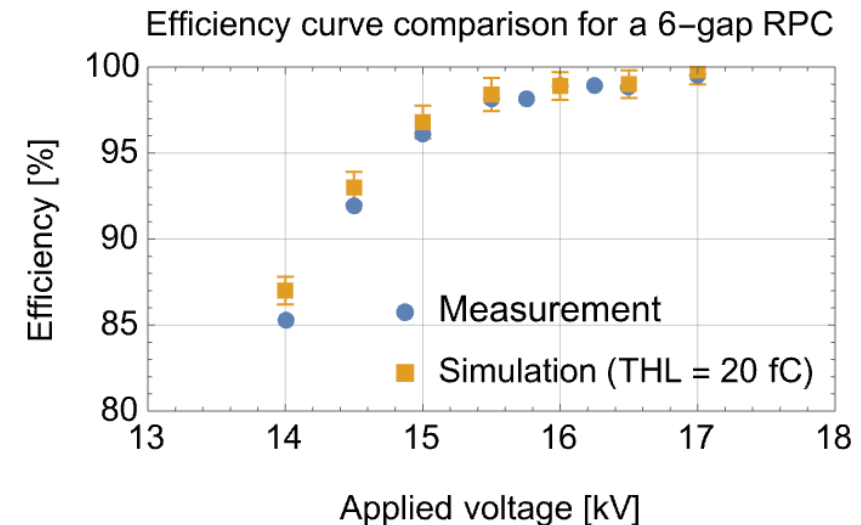
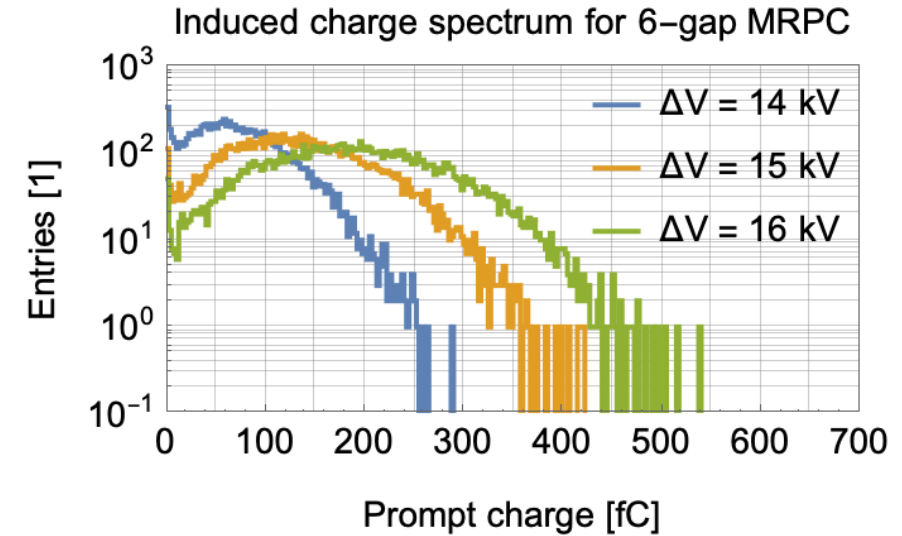
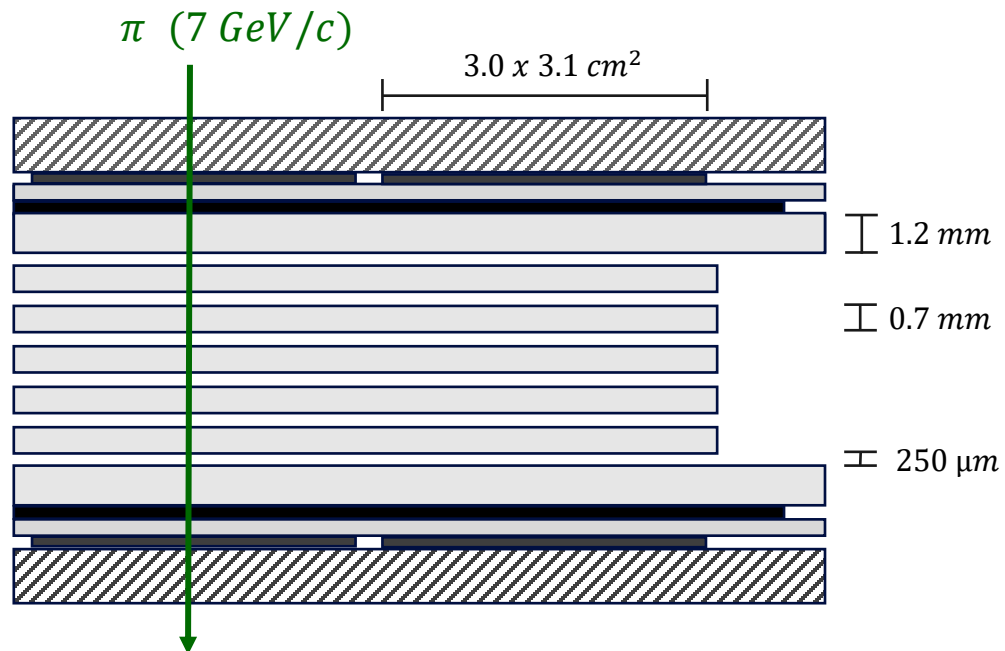
$$\psi^w(\tilde{x}', y_m) = \frac{2V_w}{\pi} \int_0^\infty \cos(k(\tilde{x} - \tilde{x}')) \sin\left(\frac{k w_x}{2}\right) \frac{\epsilon_1}{k^2} \left. \frac{\partial f_{m1}(k, y)}{\partial y} \right|_{(y=y_0)} dk$$



# An example simulation of a 6-gap MRPC

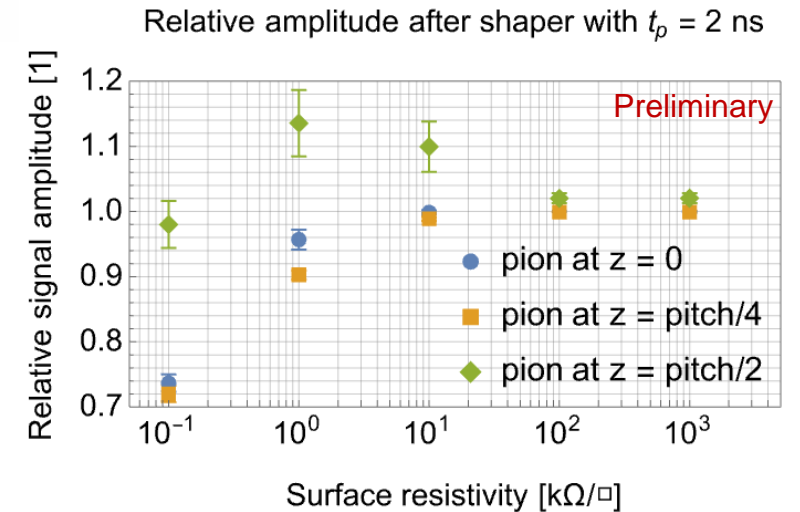
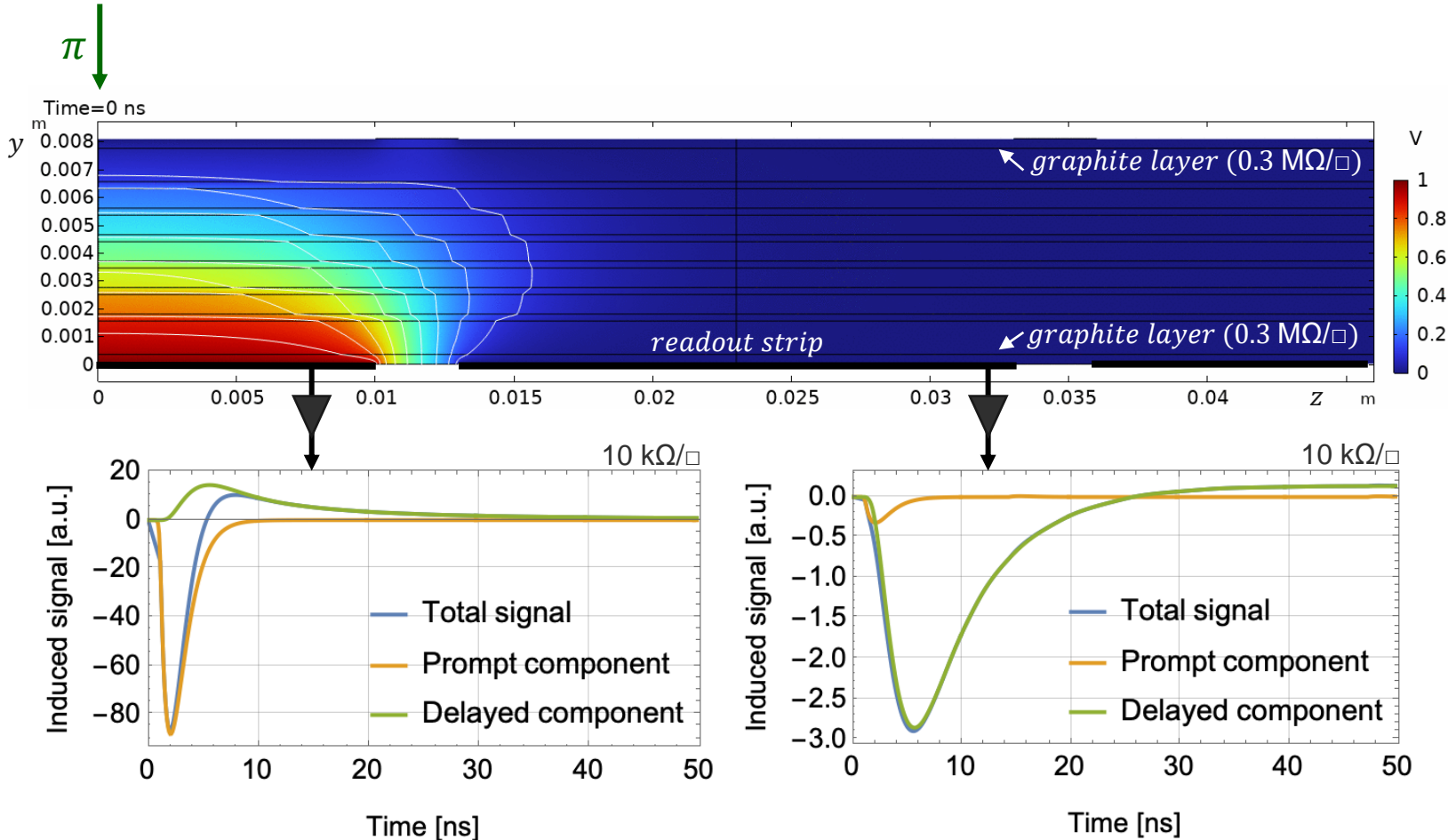
Using the mixed-method approach, an event can be simulated in less than 0.3 s.

D. Stocco is extending this approach to the 2D model of C Lippmann. <https://indi.to/c9hfk>



# What about the resistive HV electrode?

The dynamic weighting potential was calculated using COMSOL and then applied in Garfield++ for induced signal calculations. For graphite layers with  $O(100 \text{ k}\Omega/\square)$ , the signal induced by electrons remains unaffected.



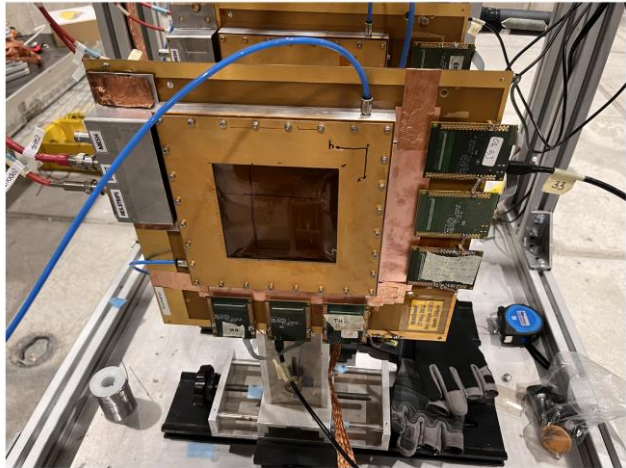
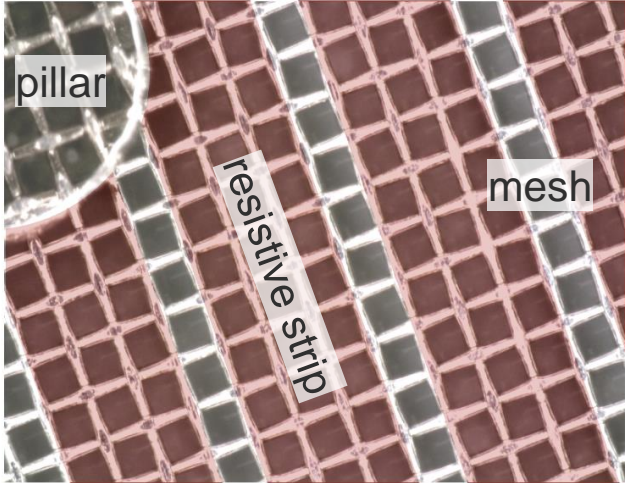
# Garfield++ simulations of resistive particle detectors

Using the finite element method, dynamic weighting potentials can be numerically obtained for a wide range of resistive detectors.

An (incomplete) list of resistive detectors:

- Multi-gap Resistive Plate Chambers (MRPC)
  - Surface Resistive Plate Counter (sRPC)
  - MicroCAT's two-dimensional interpolating readout
  - $\mu$ -Resistive WELL
  - $\mu$ -Resistive plate WELL
  - Small-pad resistive Micromegas
  - **Resistive-strip bulk Micromegas**
  - Resistive PICOSEC Micromegas
  - Un-depleted-silicon Sensors
  - Resistive Silicon Detectors (RSD)
  - 4D Diamond Sensor
- RPC
- MPGD
- Solid-state

Resistive-strip bulk Micromegas

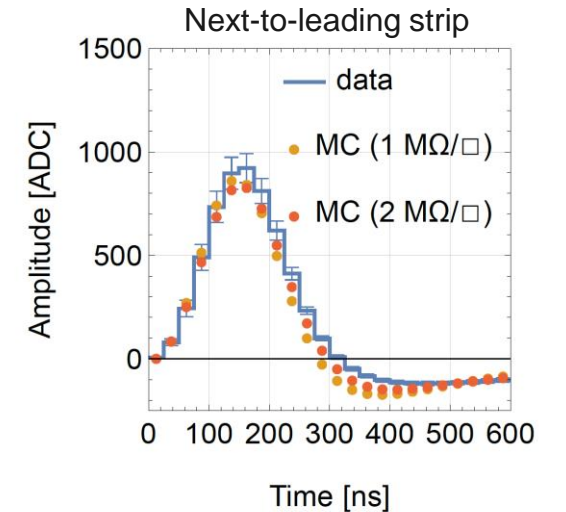
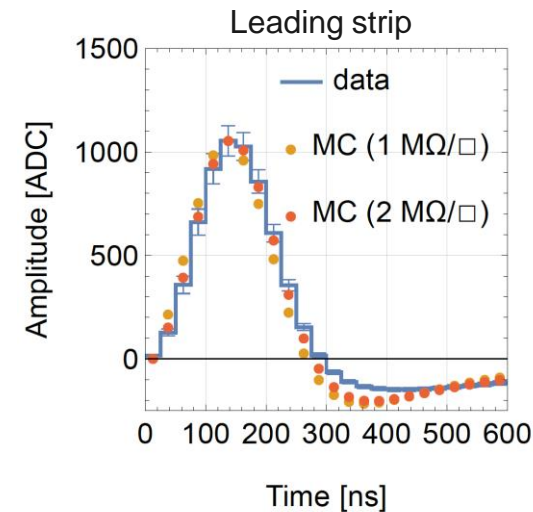
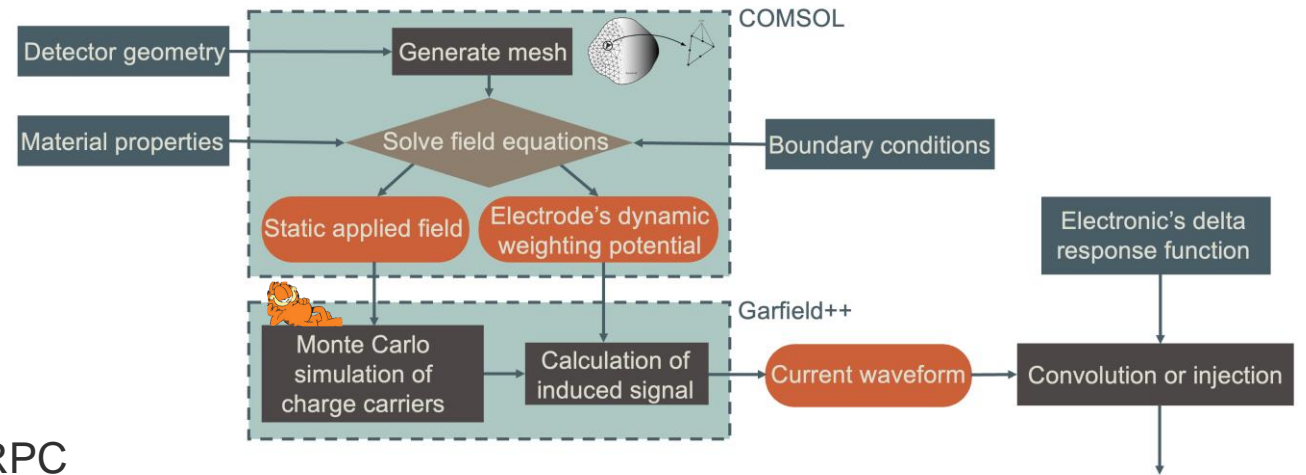


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# Conclusion

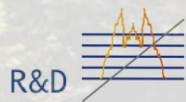
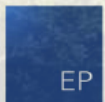
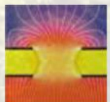
Using Garfield++, the MRPC response can be calculated from avalanche development to signal formation.

- For more efficient large-scale avalanche calculations, a mixed method is used: starting with microscopic electron tracking, followed by the Legler model.
- Garfield++ and COMSOL are used to model signal formation in detectors with resistive elements, applying an extended Ramo-Shockley theorem. A scan of different graphite layer surface resistivities showed results consistent with literature, confirming the prompt component's dominance.
- This approach applies to complex detector layouts in resistive gaseous detectors (RPCs, resistive MPGDs) and solid-state detectors.

## Outlook:

- The grid-based method can be adapted for avalanche descriptions in SiPMs.
- A combined method will be implemented, using "super charges" that can be tracked microscopically.

**Thank you for your attention!**



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