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I.FAST task 7.5: CompactLight Prototype Accelerating Structure

3rd I.FAST Annual Meeting - 18/04/24

G. D'Aura on behalf of Task 7.5 Collaboration





CompactLight Prototype Accelerating Structures

Objective:

Build and test, at low and high RF power, two prototypes of the X-band (12 GHz) accelerating structure designed for the CompactLight (XLS) project, a new class of linac-driven FEL facility.

Deliverables:

D7.5: Construction of the XLS accelerating structure pre-prototype.
Development of production process and RF tests of the pre-prototype, Dic. 2023
D7.6: Construction of the XLS accelerating structure full prototype.
Production process analysis and validation, RF tests of the full prototype, Apr. 2025

Task 7.5 partners:



| Parameter | Units | Value |
|------------------------------------|-------|------------------|
| Frequency | GHz | 11.994 |
| Phase advance per cell | rad | 2π/3 |
| Average iris radius a | mm | 3.5 |
| Iris radius a | mm | 4.3-2.7 |
| Iris thickness t | mm | 2.0-2.24 |
| Number of cells per structure | No | 109 |
| Accelerating cell length | mm | 8.332 |
| Structure length Ls | m | 0.9 |
| Group velocity vg /c | % | 4. <u>7-0</u> .9 |
| Filling time tf | ns | 146 |
| Peak klystron power (100 - 250 Hz) | MW | 50 |
| Peak klystron power (1000 Hz) | MW | 10 |
| RF pulse-length (250 Hz) | μs | 1.5 (0.15) |
| Waveguide power attenuation | % | ≈ 10 |
| Unloaded SLED Q-factor | Qo | 180000 |
| External SLED Q-factor | Qe | 23300 |
| Shunt impedance R | MΩ/m | 85-111 |
| Effective shunt impedance Rs | MΩ/m | 349 |
| Peak modified Poynting vector | W/µm | 3.4 |
| Repetition rate | Hz | 100 - 250 - 10 |
| SLED | | ON - OFF - OI |
| Required klystron power | MW | 44 - 44 - 9 |
| Available klystron output power | MW | 50 - 50 - 10 |
| RF pulse-length | μs | 1.5 - 0.15 - 1. |
| Average accelerating gradient | MV/m | 65 - 30 - 30 |
| Energy gain per module | MeV | 234 - 108 - 10 |

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Courtesy M. Diomede

G. D'Auria_3rd I.FAST Annual Meeting_18-04-2024_Task 7.5 CompactLight accelerating structure

First prototype production at VDL



Courtesy M. van den Berg

Cell tests

The main purpose of the test:

- Verify the shrink-fit assembly
- Validate the assembly method
- Check the correct positioning of the cells after the heat cycle
- Check the BFM to be used in the final prototype (material composition and ratio)











Brazing tests

3 Trials have been carried out with different conditions:

- Machinability
- Interlocking alignment
- Brazing material
- Leak tightness
- Weight



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• The alignment and flatness of the structure were kept as expected after the cycle with the 40kg on top.



End stack brazes





End stack brazes II

- One end stack brazed well, and both stacks had visible evidence of the braze flowing.
- Clear evidence however of the braze eating into the copper in second end stack.
- Visible hole in cavity wall in 2 places, not present in other side of disk.







End stack brazes III



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End stack brazes IV

- Unsure exactly why the braze ate into the copper
- Concern however that braze channel appears to touch inner cavity wall



End stack brazes results

- Waveguides run individually, OK (4 runs)
- Stack ends constructed using the same braze material and run simultaneously with the same braze program, however 1 stack end brazed very well, 1 stack end had less visible braze run but some braze has eaten the copper and exposed the braze channel through the cavity wall
- > Visible hole in cavity wall in 2 places.
- Unsure exactly why the braze ate into the copper (temperature too high?), but the fact the braze channel appears to touch inner cavity wall appears to be an issue.
- > Three problems were found on the furnace used for brazing:
 - vacuum leaks;

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- hydrogen contamination with oxygen;
- large differences and low accuracy in the measurement of the temperature profile (made at different heights in the furnace).

Fournace leaks

The hydrogen inlet of the furnace might also have introduced bubbles of Air, which caused the oxidation of the flange (Blueing ~300°C).

- A leak in the hydrogen piping would cause the formation of air bubbles which would be pumped in together with the Hydrogen during the brazing process.
- This might have weakened/influenced the bonding strength of the braze
- Further tests are required before proceeding: Introduce a stainless steel part into the furnace and carry out a similar brazing cycle.

The furnace shouldn't be vented until circa 100°C (as a precaution)

If no blueing occurs then this phenomenon has been caused by early venting which should be avoided for the next brazing cycles

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TMD jig modifications

The use of screws in a jig furnace is unrecommended.

The difference in mass between the RF structure and the steel jig leads to a sensible difference in thermal inertia that could cause the structure to get free of the jig during both the heating and cooling phases.

• Heating Phase:

The jig heats up and deforms faster than the RF structure, the rods lengthen faster, and the top of the RF structure is no longer in contact with the jig

• Cooling Phase:

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Jig cools down faster than the RF structure compressing it more than anticipated, potentially resulting in the deformation of the RF structure due to buckling strength

Waveguides should be adequately supported during brazing to avoid unnecessary deformations



Conclusion and next steps

- The two couplers will be shipped by TMD to COMEB, which will attempt to re-braze them with the CuSil ABA (end of May).
- In the event that the new brazing fails, COMEB will attempt to dismantle the steel flanges to recover the couplers brazing two new flanges (in June).
- In the meantime, VDL, which is completing the accelerating cells for the second structure (expected by the end of June), will prepare the parts for two new couplers, which should be ready by the end of June 2024.
- July/August will see the brazing of the new couplers and the first accelerating structure.
- We expect to braze the second structure by the end of 2024, after validating the brazing procedures of the first structure.

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Thank you!



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