NOVEL MATERIALS AND PROCESSES TOWARDS A FULL CARBON COMPOSITE CRYOSTAT



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Novel Carbon Composite Cryostats for Future Experiments at CERN

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Future Circular Collider (2048)

State of the art

Superconductor magnets bends particles after collision in the accelerator and liquid argon calorimeter works as an energy detector to identify particles



Cryostats in HEP are still the purview of metals.

New design aims to ultralight cryostats for both magnets and calorimeters.



ATLAS

Barrel

and LArCal:

warm and cold vessel.

and it houses both the superconductor magnet (green) and the cold vessel (blue). The cold vessel houses the calorimeter (orange) which works into a LAr bath

Aluminium 5083 double wall,

The warm vessel (pink) provides

vacuum for thermal insulation,

Hypothesis and Objectives

✓ Future experiments, FCC-ee (2048) and FCC-hh (2070), will require cryostats with a similar design but lower material budget compared to the state of the art

CRYOSTAT DESIGN REQUIREMENTS

1) He leak tightness for validation He leak rate: 10⁻⁹ mbar.I / s (UHV) Ultra High Vacuum design

2) Operating conditions Cold vessel: T= 87 K; P_{int, max} = 2.8 bar x 1.25 (SF) Warm vessel: T_{room} ; P_{int} =10⁻⁵ mbar

> 3) Radiation Resistance Total lifetime dose ~ 0.1 MGy

4) Minimize material budget Liner-less full carbon composite walls

5) Large Scale manufacturing Automated Fiber Placement, OoA curing

Main Scope of the R&D :

Decrease thickness and material budget of the next generation cryostats using Carbon Fibre Reinforced Plastic instead of metals



Definition: The material budget is the relation between the thickness of material that particles see when going through and the the length of that material (in cm) to reduce the energy of an electron by the factor 1/e

FCC-ee ALLEGRO Baseline

- One cryostat to service both the SC magnet and the LArCal
 - ✓ <u>More transparent to particles</u>, to improve the performance of the detectors (low material budget)
 - ✓ <u>Thin walls</u> for more compact design

R&D to adapt aerospace technology to low material budget cryostats

EP R&D



Key Technologies Identified

✓ Linerless tank manufactured with wet filament winding (L=1m, D=0,30m) as result of process development for CERN specification.



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FEA: Requirements

Schematic view of Future ALLEGRO cryostat cross section

Material: Carbon Composite



Finite Element Analysis

Minimum wall thickness and Material Budget to guarantee:



Profits of Carbon Composite compared to metal

Technology

✓ Full carbon composite design offers: 64% savings in Mat Budget, 30% savings in Optimal Thickness, and one order of magnitude lower CTE.

Full carbon honeycomb for walls with structural, mass and thermal constraints: Hand Lay-Up Honeycomb

| *Tested by CERN-MME-MM | | | |
|------------------------|--|----------------------------|--|
| | Results | S: | V |
| | -293 K- | Carbon HC (Preliminary) | Aluminium HC Hexcel CRIII-3/16-5056-3.1 of Plane 1NS |
| | Density [Kg/m3] | 36 | 49.7 |
| | X ₀ [mm] | 6000 | 88.9 |
| | CTE [µm/m*K] | 2.5 <mark>!!!!</mark> | 24 |
| с | <i>E_z</i> [MPa] Compression Modulus | 890 | 669 |
| | <i>E_{xy}</i> [MPa] Shear Modulus | 380 | 310 |
| 7 | | | |

| Honeycomb (Core) | CFRP | | Aluminium | | | | | |
|-------------------------|-------|-------|-----------|-------|-----------|-------|------------------------|--|
| Skin | CFRP | | CFRP | | Aluminium | | Current Baseline: | |
| Wall | OWC | ICC | OWC | ICC | OWC | ICC | Material budget saving | |
| material budget X/X0 | 0.026 | 0.028 | 0.028 | 0.032 | 0.073 | 0.077 | respect to traditional | |
| savings X/X0 [%] | -64% | -64% | -61% | -57% | REF | REF | | |
| | | | | | | | | |
| Skin Th. [mm] | 3.2 | 3.2 | 3.2 | 3.2 | 3 | 3 | R&D Baseline: | |
| Core Th. [mm] | 19.5 | 40 | 21.5 | 42 | 35 | 58 | tull-carbon composite | |
| (Optimal)Total Th. [mm] | 25.9 | 46.4 | 27.9 | 48.4 | 41 | 64 | material budget | |
| savings Th. [%] | -37% | -28% | -32% | -24% | REF | REF | savings | |

*CFRP: Carbon Fiber Reinforced Polymer *CTE: Coefficient of Thermal Expansion

| | | Result | | | |
|----------------------------|----------|----------|----------|----------|------------------------|
| Buckling Sensitive * | Optimal | | | | |
| _ | OWC | 000 | ICC | IWC | Thicknes: calculate |
| Wall Configuration | Sandwich | Solid | Sandwich | Sandwich | with FEA |
| Skin Th. [mm] | 3.2 | | 3.2 | 1.6 | / |
| Core Th_[mm] | 19 | | 40 | 30 | |
| (Optimal) Total Th. [mm] | 25.4 | 27.2 | 46.4 | 33.2 | , <i>K</i> |
| | | | | | |
| Material Budget X/X0 | 0.026 | 0.105 | 0.028 | 0.015 | |
| | | | | | |
| Buckling Safety Factor | 2.3 | - | 2.1 | - | |
| | | | | | |
| Min. Failure Safety Factor | 2.7 | 5.1 | 2.38 | 4.7 | |
| SF Max Stress | 7.47 | 6.64 | 2.6 | 7.3 | |
| SF Max Strain | 15.9 | 6.59 | 5.5 | 5.4 | |
| SF Tsai-Wu | 8.2 | 5.1 | 2.38 | 4.7 | |
| SF Core Failure | 2.7 | - | 2.8 | 4.8 | |
| | | | | | |
| Max. total def. [mm] | 1 | 4 | 2.6 | 1.7 | |
| Max. vertical def. [mm] | 1 | 1.5 | 2 | 1.3 | |
| | | | | | |
| Equivalent Stress [Pa] | 6.20E+07 | 7.33E+07 | 1.80E+08 | 9.60E+07 | |
| Shear YZ top skin [Pa] | 4.39E+05 | - | 2.10E+03 | 6.80E+00 | |
| Shear XZ top skin [Pa] | 4.39E+05 | - | 7.90E+05 | 2.20E+05 | |
| Shear YZ bottom skin [Pa] | 4.39E+05 | - | 2.10E+03 | 5.00E+04 | |
| Shear XZ bottom skin [Pa] | 4.39E+05 | - | 7.97E+05 | 2.50E+05 | |

To calculate Material Budget Radiation length X₀[mm] AI = 88.9 HM CFRP = 260Honeycomb Al= 6000 Honeycomb CFRP = 12545



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Sandwich Shell

Skin 0,45,-45,90]s Core : Honeycomb Skin [0,45,-45,90]s

Preliminary Design: CAD Model

✓ The material and processes technology identified will be used to build a CAD model of a full carbon composite large-scale cryostat





-All parts are designed to be manufacture using carbon composite (filament winding mainly, hand lay-up)

Each cylindrical wall is composed of:

- -Multipiece load-bearing mould *
- -Two end-flanges (2 in each side)
- -8 quarter counter-ring (4 in each end)
- -Continuous laminate on top to seal the joints by filament winding

Preliminary Design: CAD Model

✓ The multipiece mould has been engineered to deal with structural demands, while the final wound laminate on top guarantee leak-tightness.

Mould pieces are designed to be manufacture by filament winding using an ellipsoidal metallic tool. This will simplify serial production







Bonded Joint: nominal thickness honeycomb to simplify production. This approach aligns with min material budget and continuity criteria-

Preliminary Design: CAD Model

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Assembly Sequence

CERN



08/11/2023

Conclusions and Benefits for Aerospace

CERN technology will focus on carbon composite leak-tight design that can operates at cryogenic temperature in a long-term application.





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Low Mass Cryostat for Future Experiments at CERN

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THANK YOU

Maria Soledad Molina González CERN EP-DT-EO



Back Up

Maria Soledad Molina González | Carbon Composite Cryostat













OPTION 1:

2x insert while winding, they can be glued **Step brings complexity, high mat budget**

OPTION 2:

1x insert while winding, 1 insert for gluing **Simpler, higher material budget**

OPTION 3:

carbon plates inserted and locked in location after installation **Optimal**

Several other options possible but they require some preassembly on the moulds -> nominal thickness honeycomb to simplify production. This approach aligns with min material budget and continuity criteria->bonded joint

Validation Campaign

✓ A experimental setup to carry on leak test with pressurized He at both room and low temperature has been build in collaboration with CERN Cryolab





Test Procedure :

$Q_{rad} = \mathcal{E} \times \sigma \times (T_1 - T_2)$

- 1. Pressurize with GHe and He leak test at Troom (1h30 min)
- 2. Cooling down with LN2 radiation thermal shield, down to 110 K (5 days)*
- 3. Cooling down filling the test-unit with LN2, down to 77K
- 4. Evacuate LN2 from test unit using an electric heater to evaporate LN2
- 5. Pressurize with GHe and He leak test at 77 K (1h30min)
- 6. Warming up (1 week aprox.)



CERN



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